The Maintenance Agreement will be completed upon final engineering

General Maintenance Information

Maintenance of Structural BMP Basins (Biofiltration, Partial Infiltration, Infiltration):

Inspection. Perform inspections monthly of the basins for sediment/trash accumulation, inlet and outlet structures, vegetation health, basin erosion, and standing water in basins.

INSPECTION ITEMS	TYPICAL MAINTENANCE INDICATOR(S)	MAINTENANCE ACTIONS
Trash and Debris	Trash and debris accumulation in area.	Remove and dispose of properly.
Sedimentation	Accumulation of sediment. (Overflow inlets should be at least 6-inches above bottom of basin.)	Remove and properly dispose of accumulated materials, without damage to the vegetation. Maintain integrity of side slopes. Do not drive heavy equipment on bottom of basins. Use ramps for staging equipment.
Vegetation	Poor vegetation establishment	Re-seed, re-plant, or re-establish vegetation per original plans. Maintain vegetation health.
	Overgrown vegetation	Mow or trim as appropriate.
	Presence of weeds	Remove weeds.
Erosion	Erosion due to concentrated irrigation flow or storm water flow.	Inspect soil and repair/re-seed/re-plant eroded areas after big storm events or as needed. Repair energy dissipation (riprap or splashblock).
Inlet and Outlet Structures	Check for clogging.	Clear obstructions. Inspect underdrain via cleanout(s) and outlet structure. Remove removable orifice place on downstream end of underdrain and cleanout underdrain and replace orifice plate.
Standing Water (beyond 96 hours after a rain event)	Inspect perforated underdrain pipe using cleanout riser and inspect downstream connection.	Make appropriate corrective measures such as adjusting irrigation system, removing obstructions of debris or invasive vegetation, unclogging perforated underdrain, loosening or replacing top soil to allow for better infiltration, or minor re-grading for proper drainage. If the issue is not corrected by restoring the BMP to the original plan and grade, the City Engineer shall be contacted prior to any additional repairs or reconstruction.

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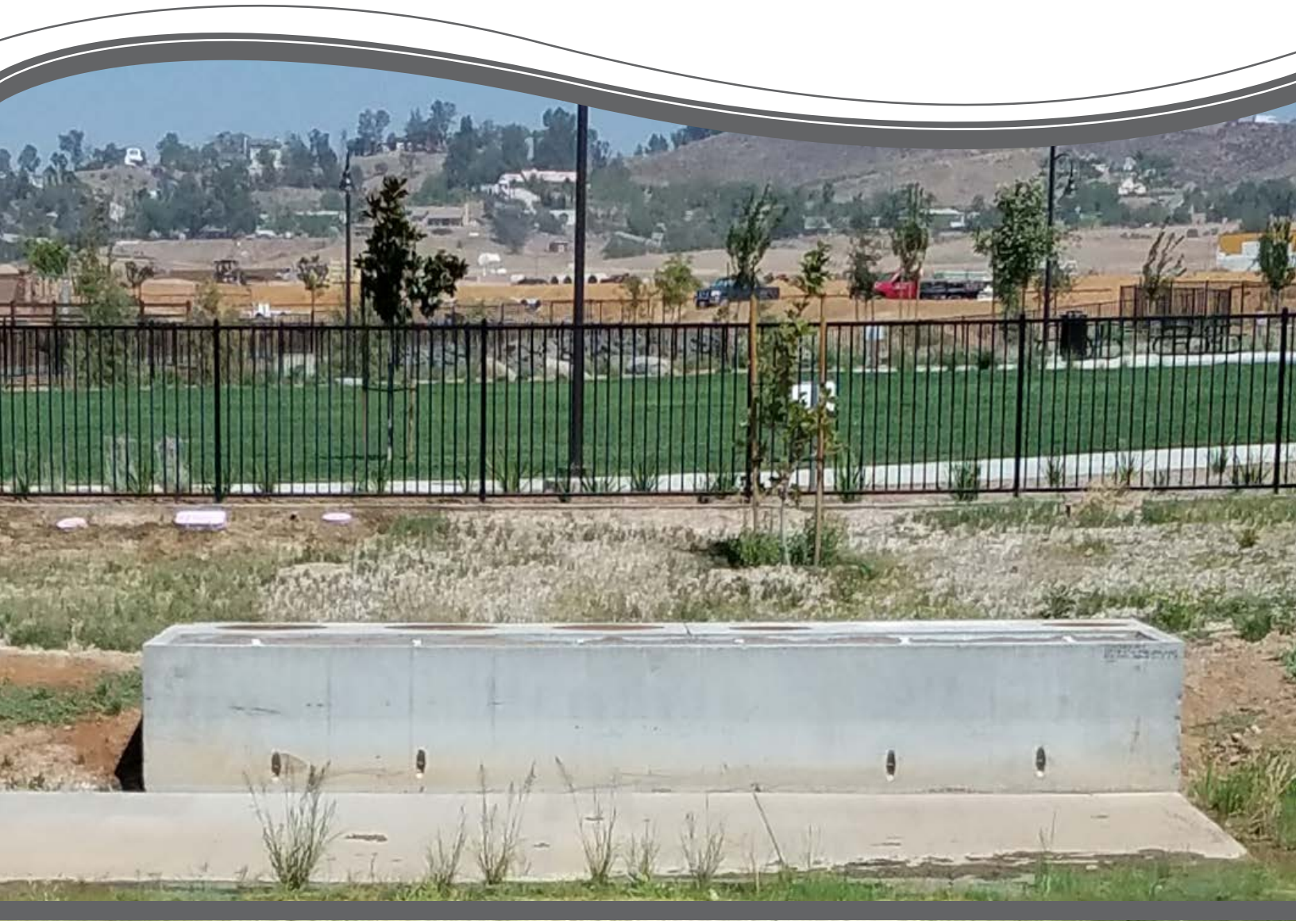
Modular Wetlands® Linear Operatons & Maintenance Manual



MODULAR WETLANDS®

MODULAR WETLANDS LINEAR
OPERATION & MAINTENANCE MANUAL

TABLE OF CONTENTS

Overview 3
Safety Notice & Personal Safety Equipment 4
Modular Wetlands Linear Components List 5
Inspection Summary & Equipment List 6
Inspection & Maintenance Notes 7
Inspection Process 7
Maintenance Indicators 9
Maintenance Summary & Equipment List 9
Maintenance Instructions 11
Replacing Biofiltration Media if Required 14
Replacing Drain Down Filter Media (Only on Older California Models) 16
Notes 17
Inspection Report 18
Cleaning & Maintenance Report 19

OVERVIEW

This operation and maintenance (O&M) manual is for the Modular Wetlands Linear Biofilter (MWL). Please read the instructions and equipment lists closely prior to starting. It is important to follow all necessary safety procedures associated with state and local regulations. Please contact Contech for more information on pre-authorized third-party service providers who can provide inspection and maintenance services in your area. For a list of service providers in your area, please visit www.conteches.com/maintenance.

WARNING

Confined space entry may be required. Contractor to obtain all equipment and training to meet applicable local and OSHA regulations regarding confined space entry. It is the Contractor's or entry personnel's responsibility to always proceed safely.

SAFETY NOTICE & PERSONAL SAFETY EQUIPMENT

Job site safety is a topic and a practice addressed comprehensively by others. The inclusions here are merely reminders to whole areas of Safety Practice that are the responsibility of the Owner(s), Manager(s), and Service Provider(s). OSHA and Canadian OSH, Federal, State/Provincial, and Local Jurisdiction Safety Standards apply on any given site or project. The knowledge and applicability of those responsibilities is the Service Provider's responsibility and outside the scope of Contech Engineered Solutions.

Safety Boots

Gloves

Hard Hat

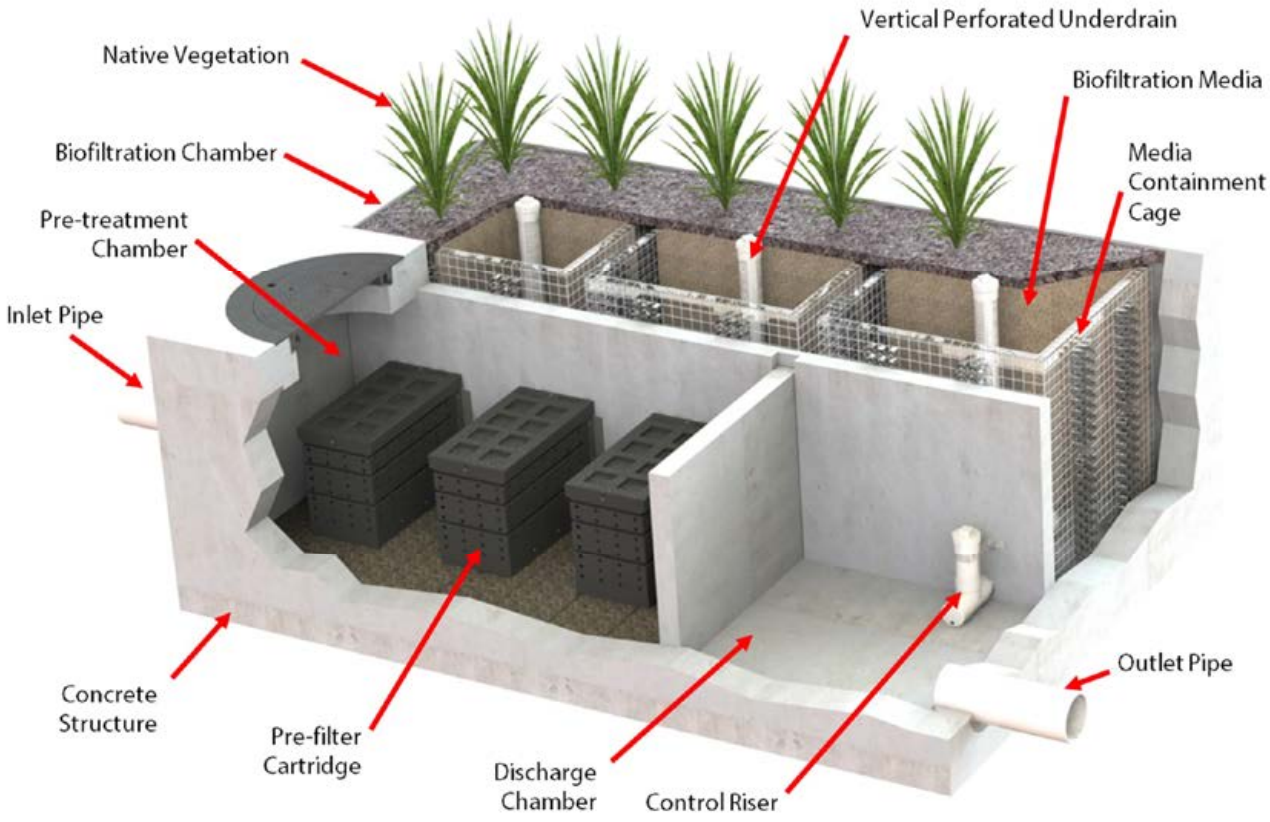
Eye Protection

Maintenance and Protection of Traffic Plan

MODULAR WETLANDS LINEAR COMPONENTS LIST

The MWL system comes in multiple sizes and configurations, including side by side or end to end layouts, both as open planters or underground systems. See shop drawings (plans) for project specific details.

The standard MWL system is comprised of the following components:



INSPECTION SUMMARY & EQUIPMENT LIST

Stormwater regulations require BMPs be inspected and maintained to ensure they are operating as designed to allow for effective pollutant removal and provide protection to receiving water bodies. It is recommended that inspections be performed multiple times during the first year to assess the site-specific loading conditions. The first year of inspections can be used to set inspection and maintenance intervals for subsequent years to ensure appropriate maintenance is provided.

- Inspect pre-treatment, biofiltration, and discharge chambers an average of once every six to twelve months. Varies based on site specific and local conditions.
- Average inspection time is approximately 15 minutes. Always ensure appropriate safety protocol and procedures are followed.

The following is a list of equipment required to allow for simple and effective inspection of the MWL:

Modular Wetlands Linear Inspection Form

Flashlight

Tape Measure

Access Cover Hook

Ratchet
& 7/16" Socket
(if required for older pre-filter cartridges that have two bolts holding the lids on)

INSPECTION & MAINTENANCE NOTES

1. Following maintenance and/or inspection, it is recommended that the maintenance operator prepare a maintenance/inspection record. The record should include any maintenance activities performed, amount and description of debris collected, and condition of the system and its various filter mechanisms.
2. The owner should keep maintenance/inspection record(s) for a minimum of five years from the date of maintenance. These records should be made available to the governing municipality for inspection upon request at any time.
3. Transport all debris, trash, organics, and sediments to approved facility for disposal in accordance with local and state requirements.
4. Entry into chambers may require confined space training based on state and local regulations.
5. No fertilizer shall be used in the biofiltration chamber.
6. Irrigation should be provided as recommended by manufacturer and/or landscape architect. Amount of irrigation required is dependent on plant species. Some plants may not require irrigation after initial establishment.

INSPECTION PROCESS

1. Prepare the inspection form by writing in the necessary information including project name, location, date & time, unit number and other information (see inspection form).
2. Observe the inside of the system through the access covers. If minimal light is available and vision into the unit is impaired, utilize a flashlight to see inside the system and all chambers.
3. Look for any out of the ordinary obstructions in the inflow pipe, pre-treatment chamber, biofiltration chamber, discharge chamber or outflow pipe. Write down any observations on the inspection form.
4. Through observation and/or digital photographs, estimate the amount of trash, debris accumulated in the pre-treatment chamber. Utilizing a tape measure or measuring stick, estimate the amount of sediment in this chamber. Record this depth on the inspection form.
5. Through visual observation, inspect the condition of the pre-filter cartridges. Look for excessive build-up of sediment on the cartridges, any build-up on the tops of the cartridges, or clogging of the holes. Record this information on the inspection form. The pre-filter cartridges can be further inspected by removing the cartridge tops and assessing the color of the BioMediaGREEN filter cubes (requires entry into pre-treatment chamber - see notes previous notes regarding confined space entry). Record the color of the material. New material is a light green color. As the media becomes clogged, it will turn darker in color, eventually becoming dark brown or black. The closer to black the media is the higher percentage that the media is exhausted and in need of replacement.

6. The biofiltration chamber is generally maintenance-free due to the system's advanced pre-treatment chamber. For units which have open planters with vegetation, it is recommended that the vegetation be inspected. Look for any plants that are dead or showing signs of disease or other negative stressors. Record the general health of the plants on the inspection form and indicate through visual observation or digital photographs if trimming of the vegetation is required.

7. The discharge chamber houses the control riser (if applicable), drain down filter (only in California - older models), and is connected to the outflow pipe. It is important to check to ensure the orifice is in proper operating condition and free of any obstructions. It is also important to assess the condition of the drain down filter media which utilizes a block form of the BioMediaGREEN. Assess in the same manner as the cubes in the pre-filter cartridge as mentioned above.

8. Finalize the inspection report for analysis by the maintenance manager to determine if maintenance is required.

MAINTENANCE INDICATORS

Based upon the observations made during inspection, maintenance of the system may be required based on the following indicators:

- Missing or damaged internal components or cartridges.
- Obstructions in the system or its inlet and/or outlet pipes.
- Excessive accumulation of floatables in the pre-treatment chamber in which the length and width of the chamber is fully impacted more than 18".
- Excessive accumulation of sediment in the pre-treatment chamber of more than 6" in depth.
- Excessive accumulation of sediment on the BioMediaGREEN media housed within the pretreatment cartridges. When media is more than 85% clogged, replacement is required. The darker the BioMediaGREEN, the more clogged it is and in need of replacement.
- Excessive accumulation of sediment on the BioMediaGREEN media housed within the drain down filter (California only - older models).
- Overgrown vegetation.

MAINTENANCE SUMMARY & EQUIPMENT LIST

The time has come to maintain your MWL. All necessary pre-maintenance steps must be carried out before maintenance occurs. Once traffic control has been set up per local and state regulations and access covers have been safely opened, the maintenance process can begin. It should be noted that some maintenance activities require confined space entry. All confined space requirements must be strictly followed before entry into the system. In addition, the following is recommended:

- Prepare the maintenance form by writing in the necessary information including project name, location, date & time, unit number and other info (see maintenance form).
- Set up all appropriate safety and maintenance equipment.
- Ensure traffic control is set up and properly positioned.
- Prepared pre-checks (OSHA, safety, confined space entry) are performed.
    - A gas meter should be used to detect the presence of any hazardous gases prior to entering the system. If hazardous gases are present, do not enter the vault. Following appropriate confined space procedures, take steps such as utilizing a venting system to address the hazard. Once it is determined to be safe, enter the system utilizing appropriate entry equipment such as a ladder and tripod with harness.

The following is a list of equipment required for maintenance of the MWL:

Modular Wetlands Linear Maintenance Form

Flashlight

Access Cover Hook

Ratchet
& 7/16" Socket
(if required for older pre-filter cartridges that have two bolts holding the lids on)

Vacuum Assisted Truck with Pressure Washer

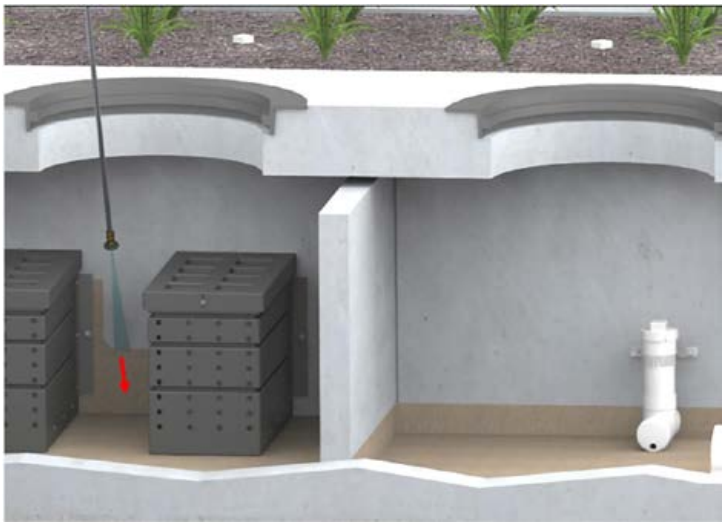
Replacement
BioMediaGREEN
(If Required)

(order BioMediaGREEN from Contech's Maintenance Team members at https://www.conteches.com/maintenance)

MAINTENANCE INSTRUCTIONS

1. ACCESS COVER REMOVAL

Upon determining that the vault is safe for entry, remove all access cover(s) and position the vacuum truck accordingly.



2. PRESSURE WASH SYSTEM CHAMBERS

With the pressure washer, spray down pollutants accumulated on the walls and floors of the pre-treatment and discharge chambers. Then wash any accumulated sediment from the pre-filter cartridge(s).

3. VACUUM SYSTEM CHAMBERS

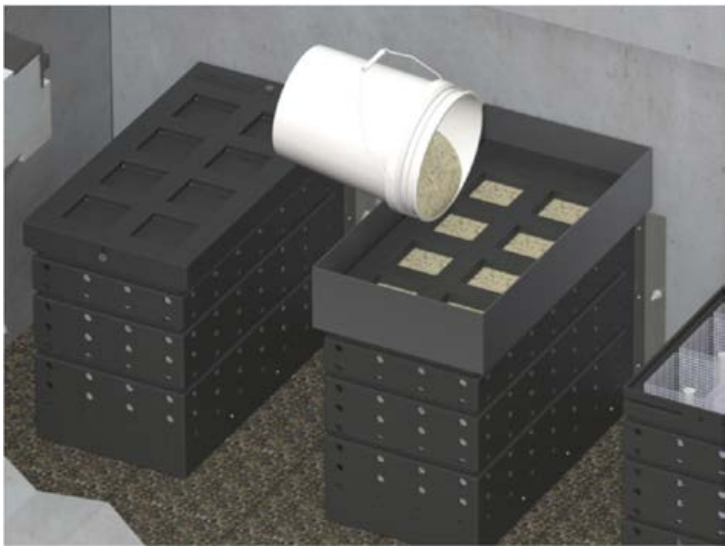
Vacuum out pre-treatment and discharge chambers and remove all accumulated pollutants including trash, debris, and sediments. Be sure to vacuum the pre-treatment floor until the pervious pavers are visible and clean. **(MWL systems outside of California may or may not have pervious pavers on the floor in the pre-treatment chamber)** If pre-filter cartridges require media replacement, proceed to **Step 4**. If not, replace the access cover(s) and proceed to **Step 7**.

4. PRE-FILTER CARTRIDGE LID REMOVAL

After successfully cleaning out the pre-treatment chamber, enter the chamber and remove the lid(s) from the pre-filter cartridge(s) by removing the two thumb screws. (Older pre-filter cartridges have two bolts holding the lids on that require a 7/16" socket to remove)

5. VACUUM EXISTING PRE-FILTER MEDIA

Utilize the vacuum truck hose or hose extension to remove the filter media from each of the individual media cages. Once filter media has been sucked out, use a pressure washer to spray down the inside of the cartridge and its media cages. Remove cleaned media cages and place to the side. Once removed, the vacuum hose can be inserted into the cartridge to vacuum out any remaining material near the bottom of the cartridge.



6. PRE-FILTER MEDIA REPLACEMENT

Reinstall media cages and fill with new media from the manufacturer or outside supplier. Manufacturer will provide specification of media and sources to purchase. The easiest way to fill the media cages is to utilize a refilling tray that can also be sourced from the manufacturer. Place the refilling tray on top of the cartridge and fill with new bulk media shaking it down into the cages. Using your hands, lightly compact the media into each filter cage. Once the cages are full (each cartridge will hold five heaping 5gal buckets of bulk media), remove the refilling tray and replace the cartridge top, ensuring fasteners are properly tightened.

7. MAINTAINING VEGETATION

In general, the biofiltration chamber is maintenance-free with the exception of maintaining the vegetation. The MWL utilizes vegetation similar to surrounding landscape areas, therefore, trim vegetation to match surrounding vegetation. If any plants have died, replace them with new ones.

8. INSPECT UNDERDRAIN SYSTEM

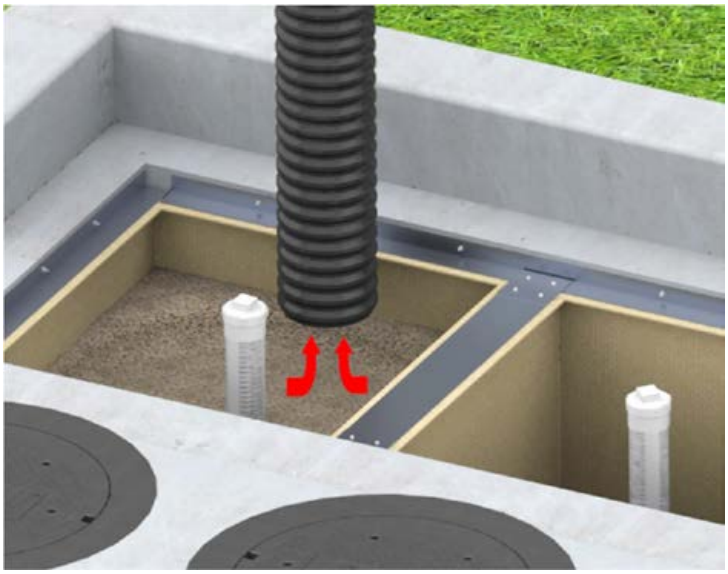
Each vertical under drain on the biofiltration chamber has a removable threaded cap that can be taken off to check for any blockages or root growth. Once removed, a jetting attachment to the pressure washer can be used to clean out the under drain and orifice riser if needed.

9. REPLACE ACCESS COVERS

Once maintenance is complete, replace all access cover(s)

REPLACING BIOFILTRATION MEDIA IF REQUIRED

As with all biofilter systems, at some point the biofiltration media will need to be replaced, either due to physical clogging or sorptive exhaustion (for dissolved pollutants) of the media ion exchange capacity (to remove dissolved metals and phosphorous). The general life of this media is 10 to 20 years based on site specific conditions and pollutant loading, so replacing the biofiltration media should not be a common occurrence. In the event that the biofiltration media requires replacement, contact one of Contech's Maintenance Team members at https://www.conteches.com/maintenance to order new biofiltration media. The quantity of media needed can be determined by providing the model number and unit depth. Media will be provided in super sacks for easy installation. Each sack will weigh between 1,000 and 2,000 lbs. Biofiltration media replacement can be done following the steps below:



1. VACUUM EXISTING BIOFILTRATION MEDIA

Remove the mulch and vegetation to access the biofiltration media, and then position the vacuum truck accordingly. Utilize the vacuum truck to vacuum out all the media. Once all media is removed, use the pressure washer to spray down all the netting and underdrain systems on the inside of the media containment cage. Vacuum out any remaining debris after spraying down netting. Inspect the netting for any damage or holes. If the netting is damaged, it can be repaired or replaced with guidance by the manufacturer.

2. INSTALLING NEW BIOFILTRATION MEDIA

Ensure that the chamber is fully cleaned prior to installation of new media into the media containment cage(s). Media will be provided in super sacks for easy installation. A lifting apparatus (forklift, backhoe, boom truck, or other) is recommended to position the super sack over the biofiltration chamber. Add media in lifts to ensure that the riser pipes remain vertical. Be sure to only fill the media cage(s) up to the same level as the old media.

3. REPLANT VEGETATION

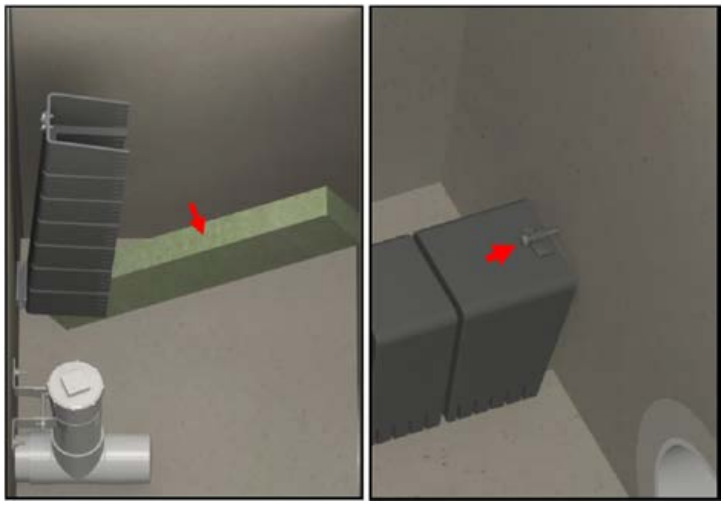
Once the media has been replaced, replant the vegetation and cover biofiltration chamber with approved mulch (if applicable). If the existing vegetation is not being reused, and new vegetation is being planted, you will need to acquire new plant establishment media that will be installed just below the mulch layer at each plant location. (see plan drawings for details). Contact one of Contech's Maintenance Team members at https://www.conteches.com/maintenance to order new plant establishment media.

REPLACING DRAIN DOWN FILTER MEDIA (ONLY ON OLDER CALIFORNIA MODELS)

NOTE: The drain down filter is only found on units installed in California prior to 2023
If during inspection it was determined that the drain down filter media requires replacement, contact one of Contech's Maintenance Team members at https://www.conteches.com/maintenance to order new media.

1. REMOVE EXISTING DRAIN DOWN MEDIA

Pull knob back to unlock the locking mechanism and lift the drain down filter housing to remove the used BioMediaGREEN filter block.



2. INSTALL NEW DRAIN DOWN MEDIA

Ensure that the chamber and housing are fully cleaned prior to installation of new media, and then insert the new BioMediaGREEN filter block. The media filter block should fit snugly between the chamber walls and be centered under the filter housing. Lower the housing over the filter block and secure the locking mechanism.

NOTES

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Inspection Report
Modular Wetlands Linear

Project Name _____

Project Address _____
(city) (Zip Code)

Owner / Management Company _____

Contact _____ Phone ( ) –

For Office Use Only
(Reviewed By)
(Date)
Office personnel to complete section to the left.

Inspector Name _____ Date ____/____/____ Time _____ AM / PM

Type of Inspection ☐ Routine ☐ Follow Up ☐ Complaint ☐ Storm Storm Event in Last 72-hours? ☐ No ☐ Yes

Weather Condition _____ Additional Notes _____

Inspection Checklist

Modular Wetland System Type (Curb, Grate or UG Vault): _____ Size (22', 14' or etc.): _____

Structural Integrity:	**Yes**	**No**	**Comments**
Damage to pre-treatment access cover (manhole cover/grate) or cannot be opened using normal lifting pressure?			
Damage to discharge chamber access cover (manhole cover/grate) or cannot be opened using normal lifting pressure?			
Does the MWS unit show signs of structural deterioration (cracks in the wall, damage to frame)?			
Is the inlet/outlet pipe or drain down pipe damaged or otherwise not functioning properly?			
Working Condition:			
Is there evidence of illicit discharge or excessive oil, grease, or other automobile fluids entering and clogging the unit?			
Is there standing water in inappropriate areas after a dry period?			
Is the filter insert (if applicable) at capacity and/or is there an accumulation of debris/trash on the shelf system?			
Does the depth of sediment/trash/debris suggest a blockage of the inflow pipe, bypass or cartridge filter? If yes, specify which one in the comments section. Note depth of accumulation in in pre-treatment chamber.			Depth:
Does the cartridge filter media need replacement in pre-treatment chamber and/or discharge chamber?			Chamber:
Any signs of improper functioning in the discharge chamber? Note issues in comments section.			
Other Inspection Items:			
Is there an accumulation of sediment/trash/debris in the wetland media (if applicable)?			
Is it evident that the plants are alive and healthy (if applicable)? Please note Plant Information below.			
Is there a septic or foul odor coming from inside the system?			

Waste:	**Yes**	**No**
Sediment / Silt / Clay		
Trash / Bags / Bottles		
Green Waste / Leaves / Foliage		

Recommended Maintenance	
No Cleaning Needed	
Schedule Maintenance as Planned	
Needs Immediate Maintenance	

Plant Information	
Damage to Plants	
Plant Replacement	
Plant Trimming	

Additional Notes: _____

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Cleaning and Maintenance Report
Modular Wetlands Linear

Project Name _____

Project Address _____
(city) (Zip Code)

Owner / Management Company _____

Contact _____ Phone ( ) –

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(Reviewed By)
(Date)
Office personnel to complete section to the left.

Inspector Name _____ Date ____/____/____ Time _____ AM / PM

Type of Inspection ☐ Routine ☐ Follow Up ☐ Complaint ☐ Storm Storm Event in Last 72-hours? ☐ No ☐ Yes

Weather Condition _____ Additional Notes _____

Site Map #	GPS Coordinates of Insert	Manufacturer / Description / Sizing	Trash Accumulation	Foliage Accumulation	Sediment Accumulation	Total Debris Accumulation	Condition of Media 25/50/75/100 (will be changed @ 75%)	Operational Per Manufactures' Specifications (If not, why?)
	Lat: Long:	MWS Catch Basins						
		MWS Sedimentation Basin						
		Media Filter Condition						
		Plant Condition						
		Drain Down Media Condition						
		Discharge Chamber Condition						
		Drain Down Pipe Condition						
		Inlet and Outlet Pipe Condition						

Comments:

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SUPPORT

DRAWINGS AND SPECIFICATIONS ARE AVAILABLE AT WWW.CONTECHES.COM

ModWetLinear OM Manual 03/24

Attachment 4
Copy of Plan Sheets Showing Permanent Storm Water BMPs

This is the cover sheet for Attachment 4.

Project Name: Collection at Cactus

Use this checklist to ensure the required information has been included on the plans:

The plans must identify:

- ☑ Structural BMP(s) with ID numbers matching Form I-6 Summary of PDP Structural BMPs
- ☑ The grading and drainage design shown on the plans must be consistent with the delineation of DMAs shown on the DMA exhibit
- ☑ Details and specifications for construction of structural BMP(s)
- ☑ Signage indicating the location and boundary of structural BMP(s) as required by the City Engineer
- ☑ How to access the structural BMP(s) to inspect and perform maintenance
- ☑ Features that are provided to facilitate inspection (e.g., observation ports, cleanouts, silt posts, or other features that allow the inspector to view necessary components of the structural BMP and compare to maintenance thresholds)
- ☑ Manufacturer and part number for proprietary parts of structural BMP(s) when applicable
- ☑ Maintenance thresholds specific to the structural BMP(s), with a location-specific frame of reference (e.g., level of accumulated materials that triggers removal of the materials, to be identified based on viewing marks on silt posts or measured with a survey rod with respect to a fixed benchmark within the BMP)
- ☑ Recommended equipment to perform maintenance
- ☑ When applicable, necessary special training or certification requirements for inspection and maintenance personnel such as confined space entry or hazardous waste management
- ☑ Include landscaping plan sheets showing vegetation requirements for vegetated structural BMP(s)
- ☑ All BMPs must be fully dimensioned on the plans
- ☑ When proprietary BMPs are used, site specific cross section with outflow, inflow and model number shall be provided. Broucher photocopies are not allowed.

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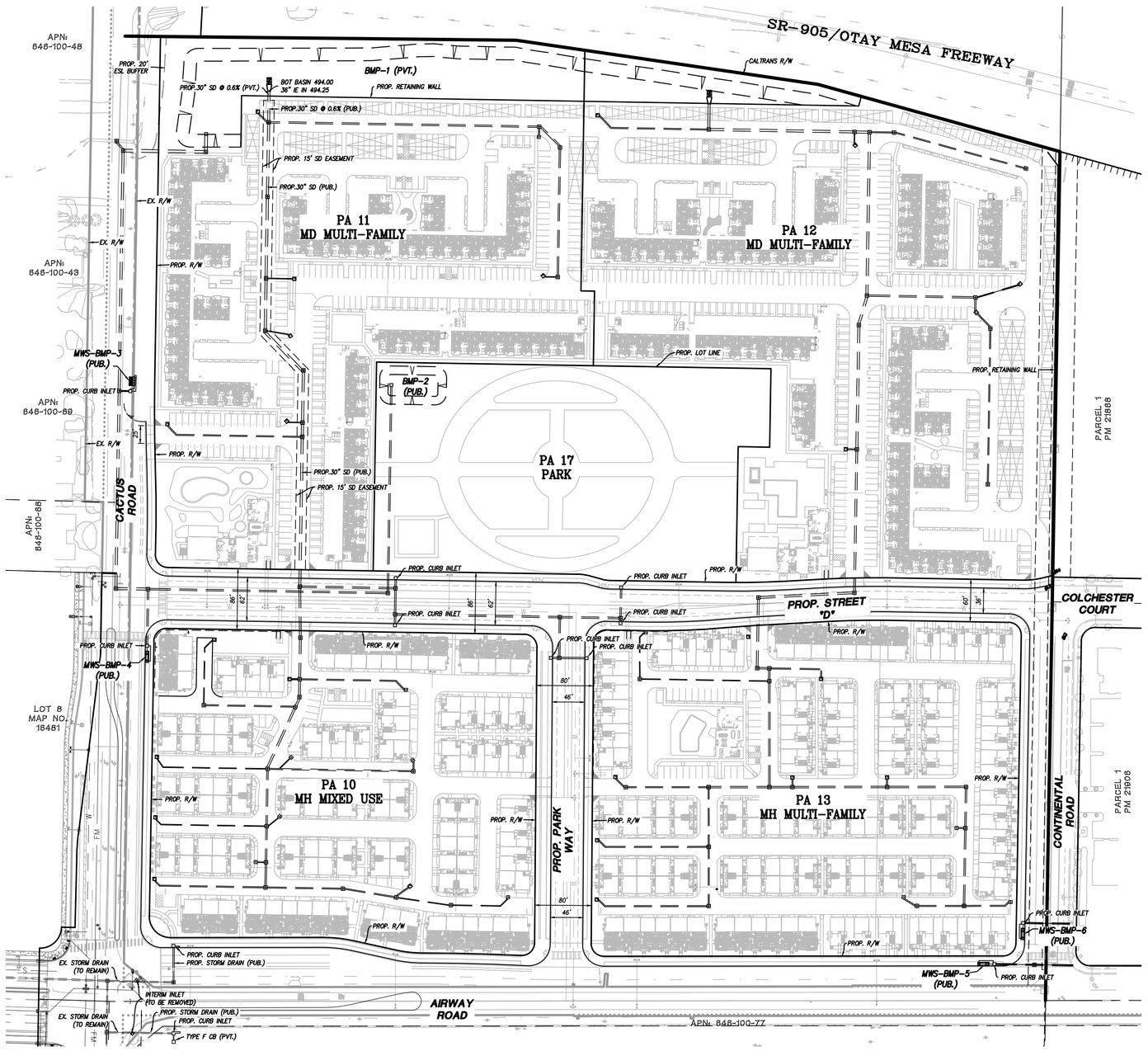
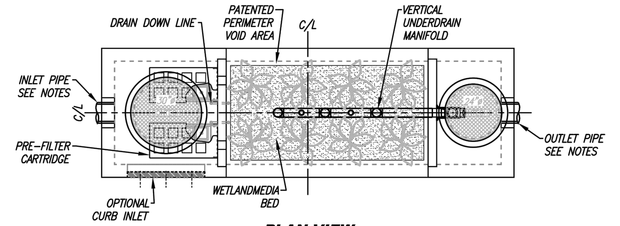


BMP SUMMARY TABLE

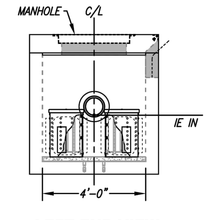
BMP ID	TREATMENT TYPE	BASIN AREA (SF)
1	BF-1	38,925
2	BF-1	2049
3	BF-3 (MWS-L-8-12)	–
4	BF-3 (MWS-L-4-15)	–
5	BF-3 (MWS-L-4-15)	–
6	BF-3 (MWS-L-4-15)	–

SITE SPECIFIC DATA			
PROJECT NUMBER			
PROJECT NAME			
PROJECT LOCATION			
STRUCTURE ID			
TREATMENT REQUIRED			
TREATMENT FLOW (CFS)			
PRETREATMENT LOADING RATE (GPM/SF)			2.1 GPM/SF
WETLAND MEDIA LOADING RATE (GPM/SF)			1.0
PEAK BYPASS REQUIRED (CFS) – IF APPLICABLE			_____ (CFS)
PIPE DATA	I.E.	MATERIAL	DIAMETER
INLET PIPE 1			
INLET PIPE 2			
OUTLET PIPE			
	PRETREATMENT	BIOFILTRATION	DISCHARGE
RIM ELEVATION			
SURFACE LOAD	PEDESTRIAN		
NOTES:			

* PRELIMINARY ONLY - NOT FOR CONSTRUCTION



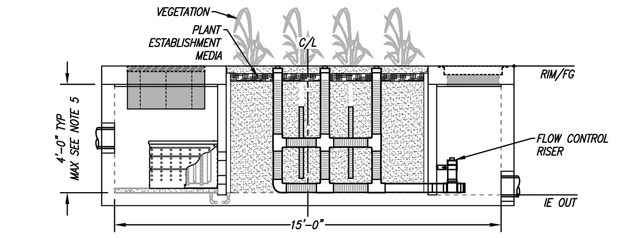
PLAN VIEW



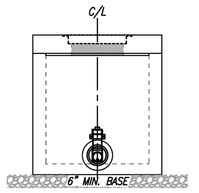
LEFT END VIEW

INSTALLATION NOTES

1. CONTRACTOR TO PROVIDE ALL LABOR, EQUIPMENT, MATERIALS AND INCIDENTALS REQUIRED TO OFFLOAD AND INSTALL THE SYSTEM AND APPURTENANCES IN ACCORDANCE WITH THIS DRAWING AND THE MANUFACTURER'S SPECIFICATIONS, UNLESS OTHERWISE STATED IN MANUFACTURER'S CONTRACT.
2. UNIT MUST BE INSTALLED ON LEVEL BASE. MANUFACTURER RECOMMENDS A MINIMUM 6" LEVEL ROCK BASE UNLESS SPECIFIED BY THE PROJECT ENGINEER. CONTRACTOR IS RESPONSIBLE FOR VERIFYING PROJECT ENGINEER'S RECOMMENDED BASE SPECIFICATIONS.
3. CONTRACTOR TO SUPPLY AND INSTALL ALL EXTERNAL CONNECTING PIPES. ALL PIPES MUST BE FLUSH WITH INSIDE SURFACE OF CONCRETE (PIPES CANNOT INTRUDE BEYOND FLUSH). INVERT OF OUTFLOW PIPE MUST BE FLUSH WITH DISCHARGE CHAMBER FLOOR. ALL PIPES SHALL BE SEALED WATERTIGHT PER MANUFACTURER'S STANDARD CONNECTION DETAIL.
4. CONTRACTOR RESPONSIBLE FOR CONTACTING CONTECH FOR ACTIVATION OF UNIT. MANUFACTURER'S WARRANTY IS VOID WITHOUT PROPER ACTIVATION BY A CONTECH REPRESENTATIVE.
5. VERTICAL HEIGHT VARIES BASED ON SITE SPECIFIC REQUIREMENTS.



ELEVATION VIEW



RIGHT END VIEW

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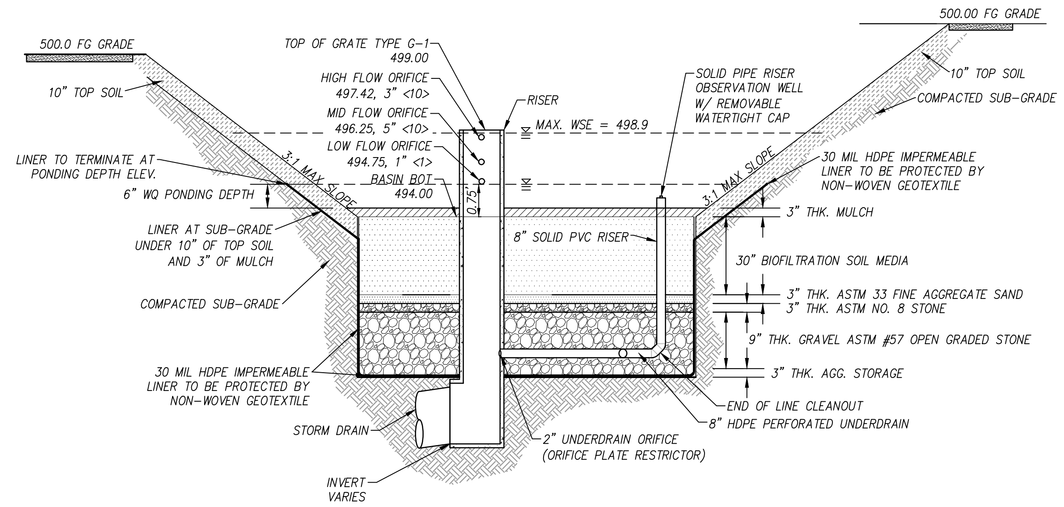
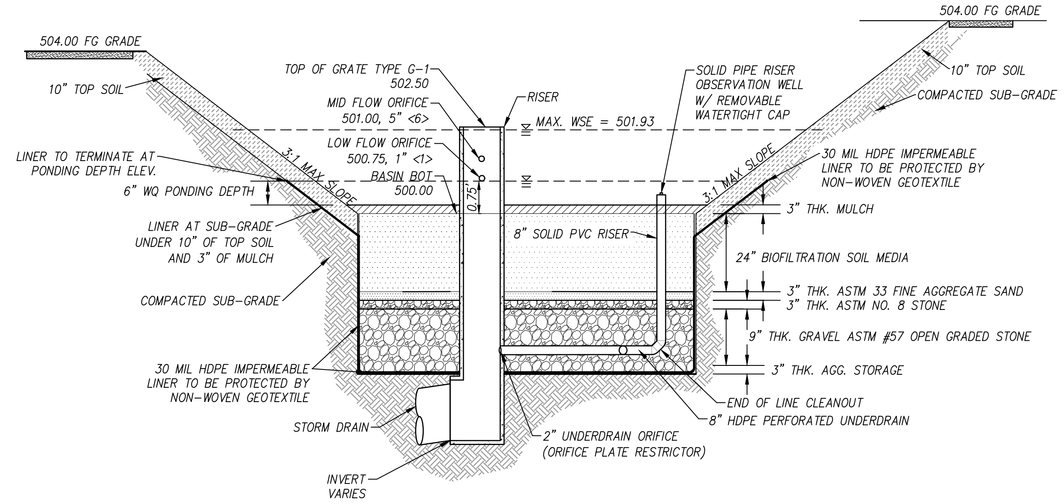
MWS-L-4-15-V
STORMWATER BIOFILTRATION SYSTEM
STANDARD DETAIL



BMP-1 DETAIL

NOT TO SCALE

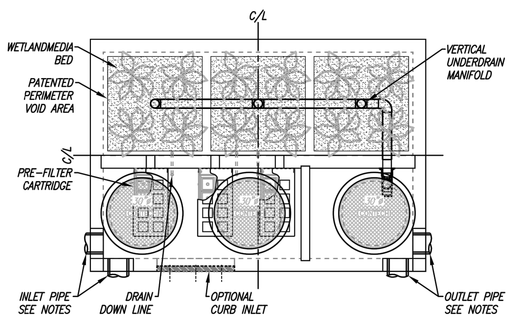


BMP-2 DETAIL

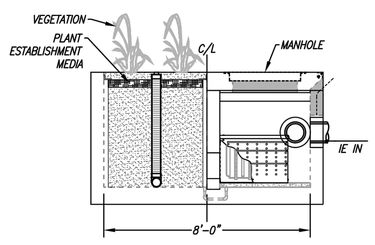
NOT TO SCALE

SITE SPECIFIC DATA			
PROJECT NUMBER			
PROJECT NAME			
PROJECT LOCATION			
STRUCTURE ID			
TREATMENT REQUIRED			
TREATMENT FLOW (CFS)			
PRETREATMENT LOADING RATE (GPM/SF)			2.1 GPM/SF
WETLAND MEDIA LOADING RATE (GPM/SF)			1.0
PEAK BYPASS REQUIRED (CFS) – IF APPLICABLE			_____ (CFS)
PIPE DATA	I.E.	MATERIAL	DIAMETER
INLET PIPE 1			
INLET PIPE 2			
OUTLET PIPE			
	PRETREATMENT	BIOFILTRATION	DISCHARGE
RIM ELEVATION			
SURFACE LOAD	PEDESTRIAN		
NOTES:			

* PRELIMINARY ONLY - NOT FOR CONSTRUCTION



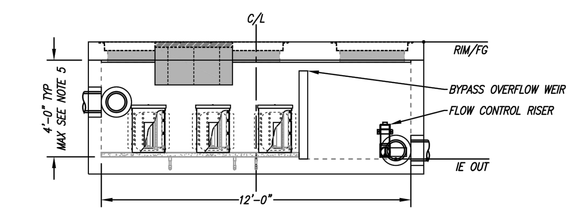
PLAN VIEW



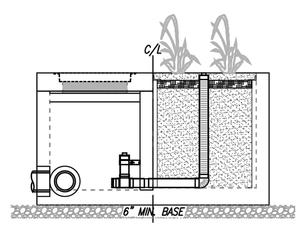
LEFT END VIEW

INSTALLATION NOTES

1. CONTRACTOR TO PROVIDE ALL LABOR, EQUIPMENT, MATERIALS AND INCIDENTALS REQUIRED TO OFFLOAD AND INSTALL THE SYSTEM AND APPURTENANCES IN ACCORDANCE WITH THIS DRAWING AND THE MANUFACTURER'S SPECIFICATIONS, UNLESS OTHERWISE STATED IN MANUFACTURER'S CONTRACT.
2. UNIT MUST BE INSTALLED ON LEVEL BASE. MANUFACTURER RECOMMENDS A MINIMUM 6" LEVEL ROCK BASE UNLESS SPECIFIED BY THE PROJECT ENGINEER. CONTRACTOR IS RESPONSIBLE FOR VERIFYING PROJECT ENGINEER'S RECOMMENDED BASE SPECIFICATIONS.
3. CONTRACTOR TO SUPPLY AND INSTALL ALL EXTERNAL CONNECTING PIPES. ALL PIPES MUST BE FLUSH WITH INSIDE SURFACE OF CONCRETE (PIPES CANNOT INTRUDE BEYOND FLUSH). INVERT OF OUTFLOW PIPE MUST BE FLUSH WITH DISCHARGE CHAMBER FLOOR. ALL PIPES SHALL BE SEALED WATERTIGHT PER MANUFACTURER'S STANDARD CONNECTION DETAIL.
4. CONTRACTOR RESPONSIBLE FOR CONTACTING CONTECH FOR ACTIVATION OF UNIT. MANUFACTURER'S WARRANTY IS VOID WITHOUT PROPER ACTIVATION BY A CONTECH REPRESENTATIVE.
5. VERTICAL HEIGHT VARIES BASED ON SITE SPECIFIC REQUIREMENTS.



ELEVATION VIEW



RIGHT END VIEW

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MWS-L-8-12-V
STORMWATER BIOFILTRATION SYSTEM
STANDARD DETAIL

100 50 0 100 200 300
SCALE: 1"=100'

N

architecture design collaborative
23231 SOUTH POINTE DR.
LAGUNA HILLS, CA 92653
949.267.1660
CHRIS WEIMHOLT

JPI
JPI Companies
Contact: Conner Kloeppel
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23098 OTAY MESA MULTI-FAMILY
SAN DIEGO, CA

1ST SUBMITTAL	01/29/2024
2ND SUBMITTAL	08/08/2024
3RD SUBMITTAL	11/25/2024

PROJECT NAME:
COLLECTION AT CACTUS – NEIGHBORHOOD DEVELOPMENT PERMIT

SHEET TITLE:
BMP PLAN

SHEET C022 OF C022

PAGES FROM THE EPOCA MASS GRADING PLAN (DWG #41791-D) ARE INCLUDED TO SHOW HOW DMA 10 IS BEING TREATED AT AN OFFSITE BMP

SEE SHEET 22 FOR CONTINUATION

SEE SHEET 19 FOR CONTINUATION

PROP. 3' RISER RIM 493.5

SE-2 BASIN 1 BOTTOM AREA 9088 SF BOTTOM ELEV. 490.0 DEPTH 6'

MHPA LINE

EX. FENCE (TYP.) (TO BE REMOVED PER SEPARATE PERMIT)

EX. STRUCTURE (TYP.) (TO BE REMOVED PER SEPARATE PERMIT)

FG:503.25

PROP. 9' 'TYPE B-1' INLET PER SDRSD SDD-116 (CURB PROFILE PER DWG 41802-D)

PROP. LOT LINE

APN 646-100-76

LOT 1 OF MAP NO.

LOT 2 OF MAP NO.

LOT 3 OF MAP NO.

LOT 4 OF MAP NO.

LOT 6 OF MAP NO.

APN 646-100-21

APN 646-100-20

EX. LOT LINE

PROP. R/W (PER FINAL MAP# _____)

EX. R/W

49' R/W DED.(PER FINAL MAP# _____)

EX. CENTERLINE

17' R/W DED. (PER SEPARATE DOC)

PROP. R/W / LIMITS OF GRADING

PROP. AC BERM

CACTUS ROAD

AIRWAY ROAD

EX. SURVEY MONUMENT IF DESTROYED OR DISTURBED, WILL BE RESET WITH GEAR SPIKE IN ASPHALT WITH DISC "LS 7019"

PROP. TYPE 'A-4' CLEANOUT PER SDRSD D-09

SWR MH-19 (SEE SHEET 36)

18" SD LINE 'A-4' (SEE SD SHEET 36&37)

36" SD LINE 'A' (SEE SD SHEET 36)

PROP. TYPE 'J' MEDIAN INLET PER SDD-118 (CURB PROFILE PER DWG 41802-D)

PROP. TYPE 'A-5' CLEANOUT PER SDRSD D-09

30" SD LINE 'A' (SEE SD SHEET 37)

PROP. 12" SEWER (SEE SHEET 37)

18" SD LINE 'A-8' (PVT) (PER EMRA 2408926) (SEE SD SHEET 37)

PROP. TYPE 'A-4' CLEANOUT PER SDRSD D-09

SWR MH-20 (SEE SHEET 36)

SWR MH-21 (SEE SHEET 37)

30" SD LINE 'A-2' (SEE SD SHEET 36&44)

PROP. 15' TYPE B-1' INLET PER SDRSD SDD-116 (CURB PROFILE PER DWG 41802-D)

30" SD LINE 'A-2' (PVT.) (SEE SD SHEET 36&44)

PROP. 3' RISER (SEE DETAIL SHEET 49) RIM 501.5

FG:504.55

PROP. CLEANOUT (SEE P-TRAP NOTE)

PROP. 6" PVT. SEWER LATERAL IE 495.88 (PER EMRA 2408926)

SE-2 BASIN 3 BOTTOM AREA 5088 SF BOTTOM ELEV. 498.0 DEPTH 5'

FG:505.80

PROP. R/W (PER FINAL MAP# _____)

FG:508.58

STA 88+65.00 BVC:507.11

STA 89+85.00 EVC:508.54

PROP. 16" WATER PER OWD PLAN

18" SD LINE 'A-7' (SEE SD SHEET 38&45)

PROP. TYPE 'A-4' CLEANOUT PER SDRSD D-09

EX. AT&T PEDESTAL TO BE RELOCATED

SWR MH-22 (SEE SHEET 38)

24" SD LINE 'A-3' (SEE SD SHEET 38&44)

PROP. 11' 'TYPE B-1' INLET PER SDRSD SDD-116

RIGHT OF WAY PARCEL 33278-1 PER CALTRANS RIGHT OF WAY MAP NO. 34014.2M, RECORDED IN DOC NO. 2010-0547452, 10/12/2010.

PROP. 11' 'TYPE B-1' INLET PER SDRSD SDD-116

PROP. TYPE 'A-4' CLEANOUT PER SDRSD D-09

RIGHT OF WAY PARCEL 33086-1 PER CALTRANS RIGHT OF WAY MAP NO. 34014.2M, RECORDED IN DOC NO. 2009-0310110, 06/09/2009.

PROP. 12' 'TYPE B-1' INLET PER SDRSD SDD-116

PROP. 5' 'TYPE B' INLET PER SDRSD SDD-116 W/ F-TYPE OPENING AT BACK

EX. OVERHEAD ELECTRIC TO BE RELOCATED UNDERGROUND (TYP)

PROP. 12' 'TYPE B' INLET PER SDRSD SDD-116

PROP. TYPE 'A-4' CLEANOUT PER SDRSD D-09

PROJECT BOUNDARY

EX. 16" FORCE MAIN (PER DWG 21305-D TO REMAIN)

EX. 10" WATER (PER DWG 25183-D TO BE ABANDONED)

PROP. 12" WATER PER OWD PLAN D1021-090448

PROP. R/W (PER FINAL MAP# _____)

EX. POWER POLE (TYP)

EX. R/W

PROP. R/W / LIMITS OF GRADING

PROP. AC BERM (PER DWG 41885-D)

EX. POWER POLE (TYP)

PROP. TYPE 'J' MEDIAN INLET PER SDD-118 (CURB PROFILE PER DWG 41802-D)

PROP. TEMP. SWALE (SEE SHEET 13)

497.95 FL

498.43 FL

500.15 FL

1.0% MIN.

1.5%

1.0%

NOTE:
SEE EMRA APPROVAL NO. 2408926 FOR SEWER LATERALS AND STORM DRAIN WITHIN CITY RIGHT-OF-WAY.

CAUTION !!!
EXISTING UNDERGROUND UTILITIES AND FACILITIES SHOWN ON THESE PLANS HAVE BEEN OBTAINED FROM AVAILABLE RECORDS AND A POTHOLE REPORT AND ARE SCHEMATIC IN NATURE. THE PLANS MAY NOT REFLECT ALL EXISTING UTILITIES. CONTRACTOR TO CONFIRM LOCATIONS OF ALL EXISTING UTILITIES PRIOR TO START OF WORK AND NOTIFY ENGINEER OF WORK OF ANY DISCREPANCIES.

CAUTION !!!
EXACT LOCATION AND DEPTH OF EXISTING UTILITIES IS UNKNOWN. CONTRACTOR TO VERIFY AND PROTECT DURING CONSTRUCTION WHERE NECESSARY.

NOTE:
P-TRAP TO BE INSTALLED FOR ALL PRIVATE SEWER LATERALS AS PART OF THE PRIVATE WATER AND SEWER PLAN

NOTES

1. FOR STORM DRAIN AND SEWER PLAN, PROFILE, AND DESIGN INFORMATION SEE SHEETS 23-45.
2. STREET ELEVATIONS ARE FINISHED SURFACE AFTER FINAL PAVING ONLY WHERE STREETS ARE SHOWN, SEE SECTIONS SHEET 12.
3. WATER SHOWN FOR REFERENCE ONLY (SEE OWD PLAN D1021-090448).
4. ALL CENTERLINE ELEVATIONS ARE FINISHED SURFACE. SEE SHEET 12 FOR UNDERCUT INFORMATION.
5. PRECISE LOCATIONS OF BUTTRESS/STABILIZATION KEYWAYS SHALL BE SHOWN ON THE FINAL AS-GRADED PLAN SET.
6. PRECISE LOCATION OF KEYWAY AND CANYON SUBDRAINS SHALL BE SHOWN ON THE FINAL AS-GRADED PLAN SET.

OTAY WATER DISTRICT NOTE

THE PROJECT SITE IS LOCATED WITHIN THE OTAY WATER DISTRICT (OWD) SERVICE AREA. IT IS THE SOLE RESPONSIBILITY OF THE APPLICANT TO APPLY FOR WATER SERVICE WITH OWD AND MEET OWD'S STANDARDS FOR SERVICE INSTALLATIONS.

N

40 20 0 40 80 120

SCALE: 1"=40'

SEE SHEET 18 FOR CONTINUATION

REGISTERED PROFESSIONAL ENGINEER GREGORY M. SHIELDS No. 42951 Exp. 03-31-22 CIVIL STATE OF CALIFORNIA

PROJECT DESIGN CONSULTANTS
Planning | Landscape Architecture | Engineering | Survey
701 B Street, Suite 800
San Diego, CA 92101
619.235.6471 Tel
619.234.0349 Fax

GREGORY M. SHIELDS, R.C.E. 42951	DATE	REGISTRATION EXPIRES 3-31-22	DESIGNED BY:	PM REVIEW:	SURVEY REVIEW:

PRIVATE CONTRACT

GRADING PLAN FOR:

EPOCA

LOTS 1 THRU 7 OF MAP NO._____
LOTS 1 THRU 10 OF MAP NO._____

CITY OF SAN DIEGO, CALIFORNIA
DEVELOPMENT SERVICES DEPARTMENT
SHEET 20 OF 77 SHEETS

PROJECT NO. 658080

FOR CITY ENGINEER _____ DATE _____

T.M. 1972222

DESCRIPTION	BY	APPROVED	DATE	FILMED
ORIGINAL	PDC			
AS-BUILTS				

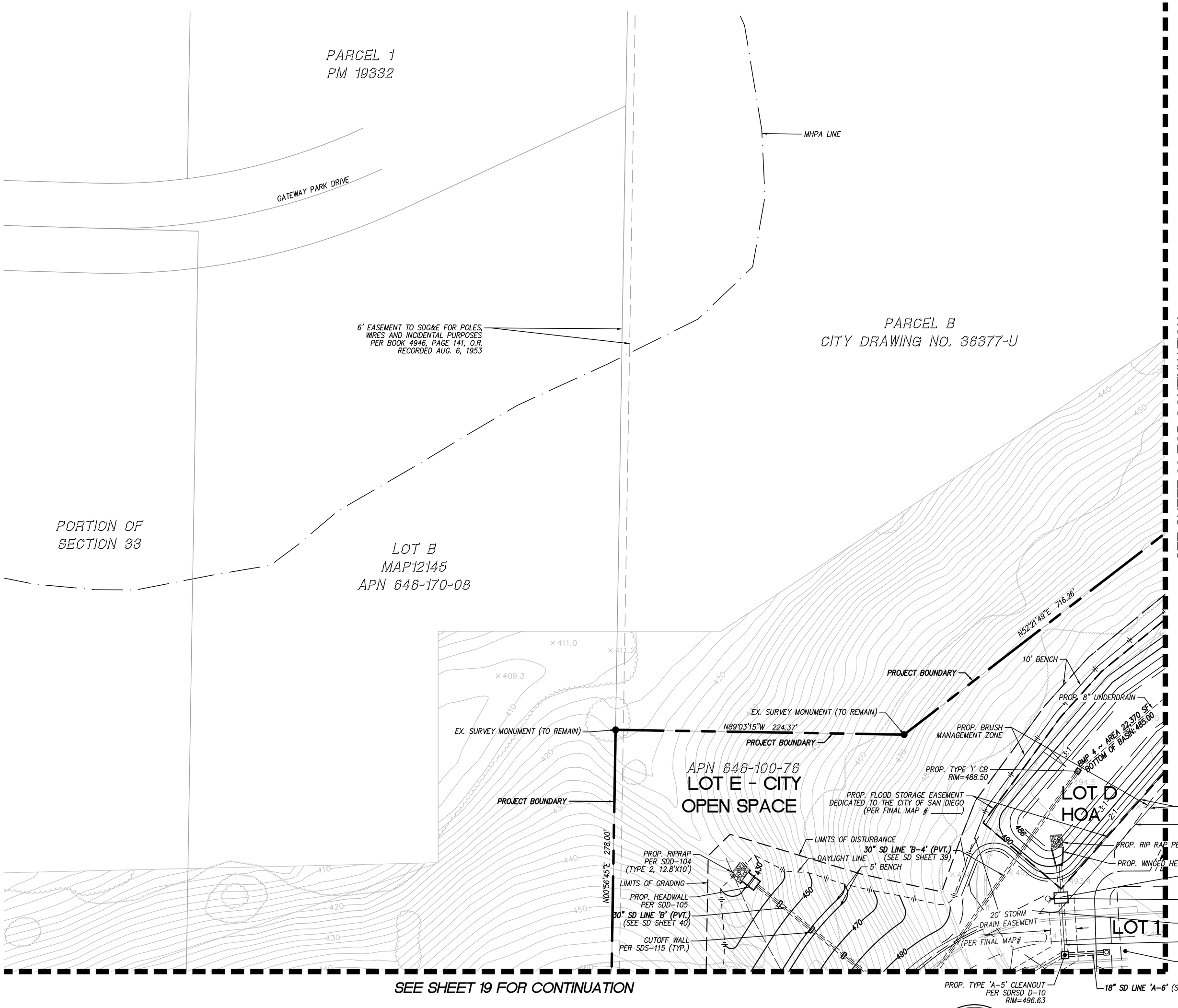
1780-6331 NAD83 COORDINATES

140-1771 LAMBERT COORDINATES

CONTRACTOR _____ DATE STARTED _____

INSPECTOR _____ DATE COMPLETED _____

41791- 20-D



NOTE:
SEE EMRA APPROVAL NO. 2408926 FOR STORM DRAIN AND DIVERSION STRUCTURE'S WITHIN THE CITY EASEMENT.

NOTES

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2. FOR BMP DETAILS, SEE SHEETS 46-50.
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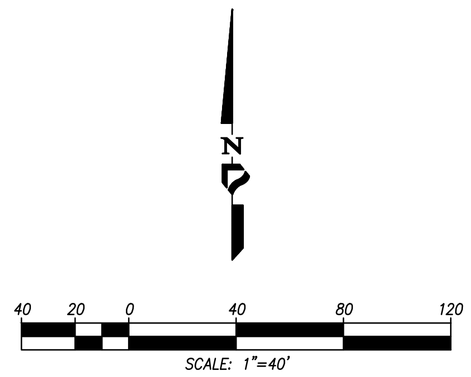

PRIVATE CONTRACT

GRADING PLAN FOR:

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LOTS 1 THRU 7 OF MAP NO._____
LOTS 1 THRU 10 OF MAP NO._____

CITY OF SAN DIEGO, CALIFORNIA
DEVELOPMENT SERVICES DEPARTMENT
SHEET 21 OF 77 SHEETS

PROJECT NO.____658080____

FOR CITY ENGINEER _____ DATE _____

T.M.____1972222____

DESCRIPTION	BY	APPROVED	DATE	FILMED
ORIGINAL	PDC			
AS-BUILTS				

1780-6331
NAD83 COORDINATES

140-1771
LAMBERT COORDINATES

CONTRACTOR _____ DATE STARTED _____
INSPECTOR _____ DATE COMPLETED _____

41791- 21-D

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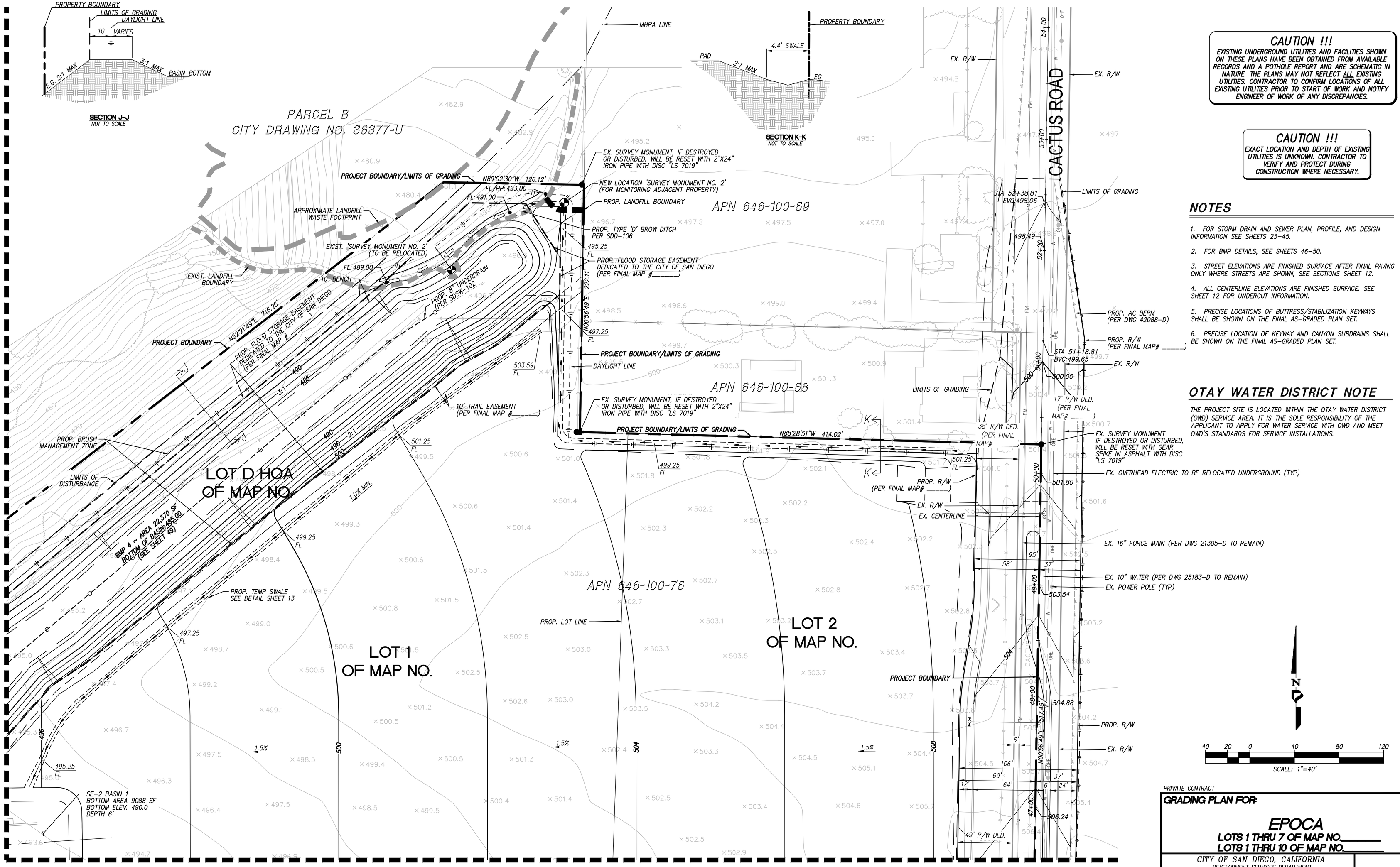
619.234.0349 Fax

GREGORY M. SHIELDS, R.C.E. 42951	DATE REGISTRATION EXPIRES 3-31-22	DESIGNED BY:	PM REVIEW:	SURVEY REVIEW:



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N

40 20 0 40 80 120

SCALE: 1"=40'

PRIVATE CONTRACT

GRADING PLAN FOR:

EPOCA

LOTS 1 THRU 7 OF MAP NO._____
LOTS 1 THRU 10 OF MAP NO._____

CITY OF SAN DIEGO, CALIFORNIA
DEVELOPMENT SERVICES DEPARTMENT
SHEET **22** OF **77** SHEETS

PROJECT NO. 658080

FOR CITY ENGINEER _____ DATE _____

T.M. 1972222

DESCRIPTION	BY	APPROVED	DATE	FILMED
ORIGINAL	PDC			
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1780-6331 NAD83 COORDINATES

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41791- 22-D

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Exp. 03-31-22
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GREGORY M. SHIELDS, R.C.E. 42951	DATE	REGISTRATION EXPIRES 3-31-22	DESIGNED BY:	PM REVIEW:	SURVEY REVIEW:

Attachment 5
Drainage Report

Attach project's drainage report. Refer to Drainage Design Manual to determine the reporting requirements.

PRELIMINARY DRAINAGE REPORT
COLLECTION AT CACTUS

CITY OF SAN DIEGO, CA
November 25, 2024
PRJ# 1111415

Prepared For:

JPI REAL ESTATE ACQUISITION II, LLC
11988 El Camino Real, Suite 200
San Diego, CA 92130
conner.kloeppel@jpi.com
314-302-2469

Prepared By:

PROJECT DESIGN CONSULTANTS
a Bowman company

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619.235.6471

PDC Job No. 4481/ 360107-01-010

Prepared by: J. Maynard
Under the supervision of

Chelisa Pack, PE RCE 71026
Registration Expires 06/30/25

TABLE OF CONTENTS

1. INTRODUCTION 1

2. PROJECT BACKGROUND & RELATION TO PREVIOUS STUDIES 3

3. EXISTING AND PROPOSED DRAINAGE PATTERNS AND IMPROVEMENTS 6

3.1 Floodplains 6

3.2 Existing Drainage Patterns 6

3.3 Proposed Drainage Improvements 7

4. HYDROLOGY CRITERIA, METHODOLOGY, AND RESULTS 8

4.1 Hydrology Criteria 9

4.2 Hydrologic Methodology 9

4.3 Description of Hydrologic Modeling Software 9

4.4 Hydrology Results 10

4.5 Detention Basins 11

4.6 Hydraulics 12

4.7 Water Quality Calculations and Hydromodification 12

5. CONCLUSION 13

TABLES

Table 1: Hydrology Criteria 9
Table 2: Hydrology Results 10

APPENDICES

1 Mannings and Runoff Coefficients, FEMA Map, Web Soil Survey, Rain Isopluvials

2 Existing Conditions Rational Method Computer Output

3 Proposed Conditions Rational Method Computer Output

4 Detention Basin Routing Analysis

5 Hydraulic Calculations

6 Drainage Exhibits

7 Record Drawings

8 Epoca and Airway Gardens Proposed Drainage Maps

9 *Drainage Study for the Otay Mesa Community Plan Update Report* was prepared by Kimley-Horn and Associates in April 2007

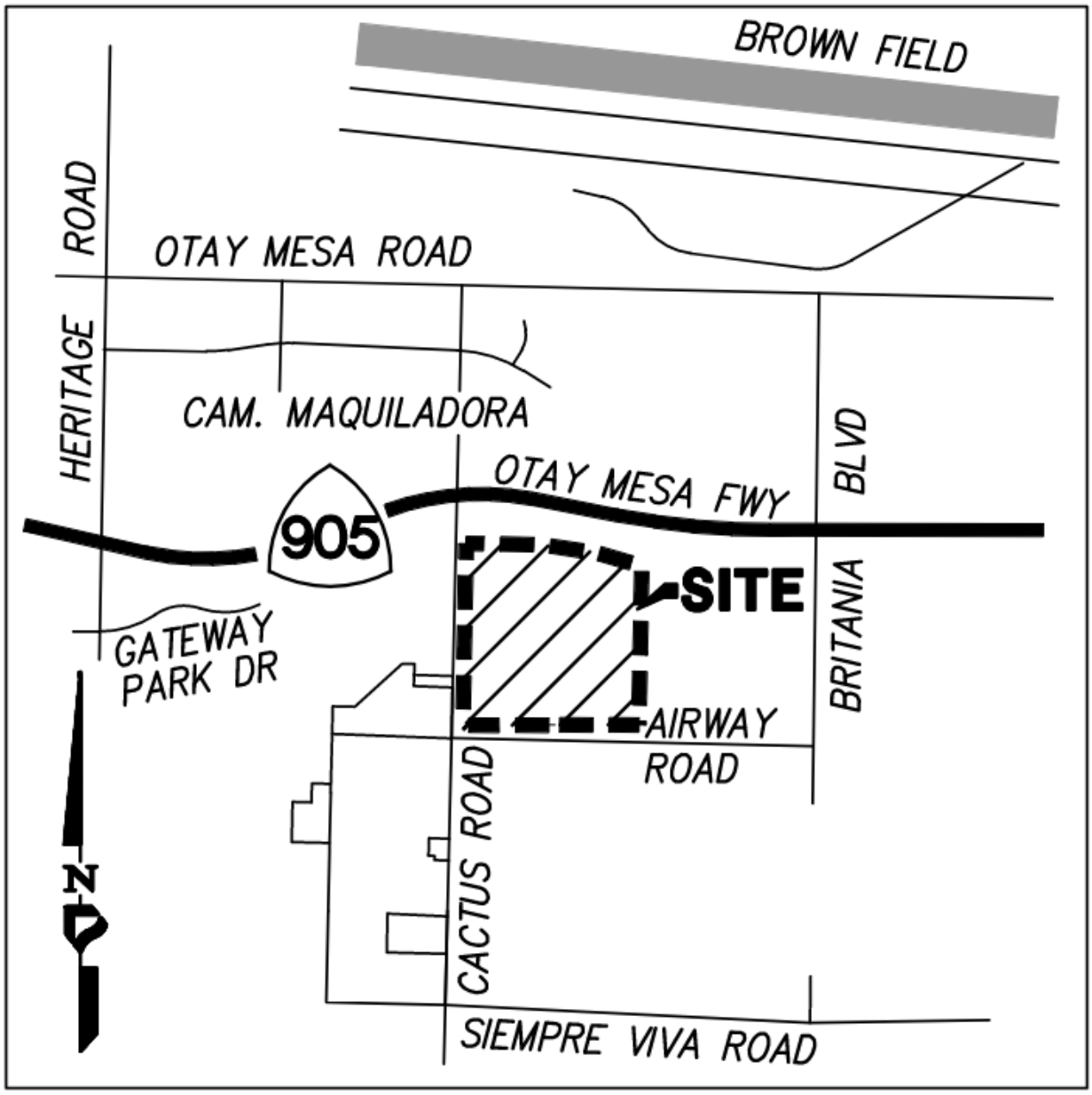
1. INTRODUCTION

This report describes the existing and proposed storm water drainage improvements for the Collection at Cactus entitlement submittal. The Collection at Cactus project (formerly known as the Paez project) is proposed for development by JPI Real Estate and represents a portion of the Otay Mesa Central Village Specific Plan (CVSP) area. The project proposes development consistent with the land use designations of the recently approved Specific Plan. The overall drainage criteria for the project was identified in the technical report for the Specific Plan, entitled *Preliminary Drainage and Water Quality Summary for the Otay Mesa Central Village Specific Plan* (PTS 408329), which was prepared by Project Design Consultants and is dated January 22, 2016. The Specific Plan designated land uses within the proposed village area to accommodate future development consistent with the Otay Mesa Community Plan Update. Consistent with the land use designations applied to the site by the CVSP, the project proposes development of residential land use.

The drainage analysis presented herein reflects a preliminary engineering effort for the project, which includes peak 100-year event hydrologic analyses.

The project proposes an application for a 39.62 acre site located north of Airway Road and east of Cactus Road in the Otay Mesa community of the City of San Diego within the CVSP area. See Figure 1 for a Vicinity Map. The vast majority of the project discharges to an existing 48" storm drain on Cactus Road. This pipe then discharges to an existing channel located on the neighboring property west of Cactus Road (Drawing No. 37010-20-D). This existing offsite channel eventually flows to Spring Canyon Creek.

There may be mapped jurisdictional non-wetland Waters of the US (WUS) north of the site, but the project avoids impacts to the existing channel. As such, agency permits are currently not anticipated for this project. (Corps 404, CDFW 1602, and RWQCB 401).



VICINITY MAP

NO SCALE

Figure 1: Vicinity Map

2. PROJECT BACKGROUND & RELATION TO PREVIOUS STUDIES

This report builds on the work done previously for the CVSP. The work done for the CVSP was based on the Otay Mesa Community Plan Update (CPU) and its associated EIR. Specifically, the Otay Mesa CPU Drainage Study that was part of the EIR outlined the drainage and water quality requirements for future development within Otay Mesa and identified some of the regional drainage and flooding issues within the area. The report is titled *Drainage Study for the Otay Mesa Community Plan Update* and was prepared by Kimley-Horn and Associates in April 2007. Included in that report is as a companion study entitled *Review of Otay Mesa Drainage Studies*, prepared by Tetratech.

The report outlines the history and drainage challenges associated with the development of the Otay Mesa Community Plan Area. For example, for most of its early history, Otay Mesa was used for agriculture and farming. As industrial and commercial development started taking place in the 1960s, the City of San Diego recognized the need for a comprehensive drainage Master Plan for the Mesa. The topography of the majority of the area is mostly flat and some of the areas experience flooding during moderate storm events, particularly within the East Watershed (per the Watershed Map in the CPU Drainage Study). There was concern that the new development would increase the stormwater runoff crossing the border into Mexico. In 1987, the City Council approved a contract to prepare the Otay Mesa Master Drainage Plan and published a Notice to "All Private Engineers" that established drainage requirements for development within the East Watershed of Otay Mesa. (Refer to page 2 of the CPU Drainage Study). The Notice required no increase in the rate of stormwater runoff from the property after development, by construction of stormwater detention basins. Most of the drainage analysis associated with the CPU Drainage Study focused on the East Watershed, but the CPU Drainage Study also addressed the other areas within the CPU boundary. The Central Village Specific Plan is within the West Watershed, which is less developed than the East Watershed but still has some of the same drainage challenges. Per Section VII of the CPU Drainage report, the following describes the recommended drainage design criteria for future development within the West Watershed (which includes the Specific Plan Area):

> The West Watershed consists of smaller Mesa-top watersheds that drain into the tributary canyons of Spring Canyon. All of the flow from the watershed flows into Mexico at the

Spring Canyon concentration point. Detention basins will be required to reduce the post-development peak flows to predevelopment levels for the 50-year and 100-year storm. If the detention basins concentrate flows at the upper edge of canyons, care must be taken to ensure that erosion potential is not increased downstream.

Therefore, the requirements of the West and East watersheds are different. While developments in the East watershed requires conformance with the Notice to "All Private Engineers", the West watershed is not subject to the same requirements, but it is subject to the 50-year and 100-year storm detention requirement, as outlined in the above paragraph.

Subsequent to the preparation of the previous Otay Mesa Drainage Studies, Caltrans has built the new State Route 905 and there have been other changes and development within the watershed. Some of the regional drainage improvements proposed in the original studies and master plans to alleviate regional flooding issues have still not been resolved. Therefore, this report follows the guidance for future development established with the Specific Plan, specifically the requirement for detention. The guidance will require compliance with the overall goals of the CPU (reduce post-development peak flows) and will also require compliance with the applicable stormwater quality regulations.

Additionally, the developments to the east and the west of the proposed project site, have a direct impact on the proposed project site.

The development to the west is the project called Epoca. It is a project that is also represented in the Otay Mesa Central Village Specific Plan (CSVP) area. The project has proposed to have a mix of Medium High Density Mixed-Use, Medium Density Multi-Family, Low Density Multi-Family, Public School Facilities, Recreation, and Open Space land uses. Currently, this project has completed its mass grading with all basins included. It is currently in construction of homes to the south. The north contains a combined hydromodification, detention, and water quality basin named BMP #4. This existing basin has been designed to accept an area on Airway Road that is part of this project's improvements. See Appendix 6 for the Drainage Exhibits that delineate this area.

Furthermore, the developments to the east, called Airway Gardens and Brownfield Tech Park have been completed (or are currently in construction). Airway Gardens is a residential community and

is the western portion of the Brown Field Tech Park Unit 2 project, which was mass graded per Drawing #33876-D. The developer for Brown Field Tech Park Unit 2 project sheet graded each of the lots and the built the treatment control and hydromodification BMPs. The southeast corner of the Brown Field Tech Park has an existing basin called "South Basin." This basin has been designed to accept an area this project's improvements, specifically the remaining improvements on Continental Street. The proposed design is that the remaining portion of Continental Street will be treated by two proposed modular wetland systems that will tie-in to an existing storm drain that discharges to an existing "South Basin." "South Basin" has been sized for hydromodification and detention. See Appendix 8 for the Drainage Exhibits that delineate this area.

Most of the Collection at Cactus site drains to the northwest. The existing outlet, the 48" storm drain that crosses Cactus Road (DWG 37010-20-D), outlets to a riprap lined channel on the neighboring Sesi property to the west, that eventually discharges to a point in Spring Canyon. The Sesi property is a landfill closure project that comprised a landfill cap and the addition of a rip rap lined channel. The report for this closure is the "Hydrology/Hydraulic Analysis Sesi Property Landfill Closure Project" dated August 2012. This report was obtained from City files, but the drainage study was not detailed to the point where one could see if the Highway 905 was complete or not.

Furthermore, a Public Information Request was submitted to Caltrans for the Highway 905 study, but Caltrans was not able to provide a copy of the Highway 905 Drainage Study, therefore, the run-on from Caltrans and the area north of the Caltrans was modeled for the purposes of this study, based on SanGIS topo, SanGIS storm drain information, and the Caltrans As-Built plans. (See Appendix 7 for Record Drawings).

3. EXISTING AND PROPOSED DRAINAGE PATTERNS AND IMPROVEMENTS

The following sections provide descriptions of the existing and proposed drainage patterns and improvements for the project.

3.1 Floodplains

The project is located within an area of the non-printed FEMA Firm Panel 06073C2200G. Per the FIRM index sheet, the panel is not printed is because there are no special flood hazard areas within the panel sheet. Therefore, there are no FEMA special flood hazard areas within the project. However, although there is no FEMA special flood hazard areas, there may be areas of localized flooding in the canyon and other drainage concentration points.

3.2 Existing Drainage Patterns

The site is currently used for agriculture and farming, as it has been for most of its early history in Otay Mesa. Topography within the project site is characterized by mostly gently sloping areas and there are currently minimal drainage improvements within the project boundary.

The majority of the project site drains to the north to an existing channel. From here, onsite water comingles with other runoff draining from upstream areas including Caltrans right-of-way. The existing channels flows around the northwestern perimeter of the site to an existing 48" storm drain (Drawing No. 37010-20-D) on Cactus Road. This existing 48" storm drain discharges to an existing channel on the neighboring property to the west. This existing channel drains to the upstream point of the North Fork of Spring Canyon.

See Exhibit A in Appendix 6 for the existing condition hydrology maps. Drainage is divided into two main drainage areas, North and South. The Southern system is represented by System 100 and the Northern system is represented by System 200. System 200 includes the results of System 100 in the model, with a user-defined input of flow, area, flowrate, and time of concentration. Both systems drain to the existing 48" storm drain that crosses Cactus Road (DWG 37010-20-D). They include the following areas:

System 100: System 100 represents the project site, an area south of Airway Road, and a portion of Cactus Road that drains toward the System 100 outlet. The 48" storm drain is located at the northeastern corner of the project site at Node 103.

System 200: System 200 represents the area north of the project site. It is comprised of an existing drainage channel to Node 103, a portion of State Route 905, and an area bounded by Otay Mesa Road to the north, Cactus Road to the West and Continental Street to the East. This area is predominantly developed, and the remaining may be developed in the future. System 200 is subject to the Notice to "All Private Engineers" as mentioned in Section 2 of this report. Therefore, System 200 is subject to storm water detention requirements and the C values chosen for calculations in this report reflects this.

3.3 Proposed Drainage Improvements

The proposed drainage patterns and drainage improvements have been designed to mimic existing drainage patterns. The proposed project will include a storm drain system consisting of inlets, pipes, brow ditches, roof drains, and water quality features/detention basins.

The proposed drainage improvements include public storm drain infrastructure for a proposed park onsite, public streets, and private storm drain improvements serving the private project site.

Refer to Exhibit B for the proposed conditions hydrology map. The system for the proposed conditions are Systems 3000, 5000, and 6000 and existing System 200. They are as follows:

System 3000: System 3000 represents the area that drains north to Planning Areas 11 and 12 to proposed Basin BMP-1, a combined biofiltration/hydromodification/detention basin. The area draining to BMP-1 in this system is Planning Areas (PA-X) 10, 11, 12, and 13 and the eastern portion of Street D. The outlet of BMP-1 drains towards a proposed storm drain on Cactus Road in System 6000.

System 5000: System 5000 represents the proposed Public Park. This system drains to BMP-2, a combined biofiltration/hydromodification/detention basin. The outlet of BMP-2 drains towards Public Street D in System 6000.

System 6000: System 6000 represents the areas inclusive of Systems 3000 and 5000 (before and after detention), the remaining area of public Street D, and area on Cactus Road. System 6000 represents the area that routes to the final Node 103, the existing 48" storm drain. (Drawing No. 37010-20-D).

System 200: System 200 represents the area above the project site. It is comprised of the tributary area to an existing drainage channel to Node 103, a portion of State Route 905, and an area bounded by Otay Mesa Road to the north, Cactus Road to the West and Continental Street to the East. This area is predominantly developed, and the remaining may be developed in the future. System 200 is subject to the Notice to "All Private Engineers" as mentioned in Section 2 of this report. Therefore, System 200 is subject to storm water detention requirements and the C values chosen for used in the calculations of this report reflects this.

4. HYDROLOGY CRITERIA, METHODOLOGY, AND RESULTS

The site was modeled for existing and proposed conditions to prevent any downstream impacts or increase in flow rates. Site hydrology was assessed to generate hydrographs to route through the basins being designed in concert with hydromodification criteria.

4.1 Hydrology Criteria

Table 1 summarizes the key hydrology assumptions and criteria used for the hydrologic modeling.

Table 1: Hydrology Criteria

Existing and Proposed Hydrology:	100-year storm frequency for storm drain design
Soil Type:	Hydrologic Soil Group D
Land Use / Runoff Coefficients:	Assigned for each drainage area based on estimated percent imperviousness (C values range from C=0.45 to C=0.95).
Rainfall intensity:	Based on the City of San Diego Intensity Frequency Duration Curves presented in the 2017 City of San Diego Drainage Design Manual.
Detention Requirements	50-year and 100-year not to exceed pre-project levels (per CVSP requirements)

4.2 Hydrologic Methodology

Hydrology calculations were completed for existing and proposed conditions accounting for all areas draining to the onsite storm drain systems. Drainage areas were defined from existing and proposed topographic maps of the area. Hydrologic analysis was completed utilizing the Rational Method, outlined in the 2017 City of San Diego Drainage Design Manual. The goal of the Rational Method analysis was to determine the peak 100-year and 50-year flow rates for the storm drain pipes by developing a node link model of the contributing drainage area and applying the intensity-duration-frequency (IDF) curve to the areas. See Appendix 1 for the City of San Diego IDF curve.

4.3 Description of Hydrologic Modeling Software

The Civil-D Rational Method Program was used to perform the Rational Method hydrologic calculations. This section provides a brief explanation of the computational procedure used in the computer model.

The Civil-D Modified Rational Method Hydrology Program is a computer-aided design program where the user develops a node link model of the watershed. Developing independent node link

models for each interior watershed and linking these sub-models together at confluence points creates the node link model. The intensity-duration-frequency relationships are applied to each of the drainage areas in the model to get the peak flow rates at each point of interest.

4.4 Hydrology Results

The results of the Rational Method hydrology modeling are provided in Appendices 2 and 3 and the results are summarized in this section. Development of the project site increased the 100-year runoff from the site, but peak flows after detention are less than the overall project existing condition peak flows.

For the results of the analysis, see Exhibit A for the existing conditions hydrology map and Exhibit B for the proposed conditions hydrology map in Appendix 6. Refer to the appendices for the hydrology calculations. Table 2 summarizes the hydrology results and compares existing and proposed conditions. The calculations below include the 100-year condition due to the preliminary nature of this report. Both the 100-year and the 50-year calculations for detention will be included in final engineering.

Table 2: Hydrology Results

	EXISTING CONDITIONS			PROPOSED CONDITIONS			
Outfall of Interest	***System***	***Q100 (cfs)***	***Contributing Area (acres)***	***System***	***Q100 (cfs)***	***Q100-Detained(cfs)***	***Contributing Area (acres)***
Sesi Property Storm Drain Outfall of 48" Pipe	*System 100 Node 103*	103.7	105.2	*System 100 Node 103*	132.8	92.2	98.2

Note that the areas for pre-development and post-development do *not* match. This is due to areas being removed in the post-development condition. The area removed is an area south of Airway Road as shown on the Exhibit B in Appendix 6. This area in the pre-development condition, is routed through a pipe across the Airway Road (Per Caltrans 11-288804, D-21) and picked up in a swale that is routed to an existing 48" storm drain on Cactus Road. In the post-development

condition, this area will be routed to an inlet that drains to BMP#4 on the neighboring Epoca site. This area is approximately 5.37 acres. This area was previously included in the Epoca project's drainage study, so the flow was previously anticipated to drain westerly. Furthermore, the proposed raised median on Cactus Road will change the drainage area from the existing condition area. This is accounted for in Epoca's ultimate drainage study as seen on the Epoca Proposed Drainage Map in Appendix 8.

4.5 Detention Basins

There are two detention basins proposed for the project site for water quality treatment, hydromodification management and detention (BMPs 1 and 2). From the Rational Method results for each of the systems draining to a basin, the proposed condition peak inflow hydrographs were generated with Rick Engineering Rational Method Hydrograph Generator. This program develops a synthetic hydrograph per the 2003 County Hydrology Manual using the results of the Rational Method output.

The inflow hydrograph for each system was then entered into Haestad Method's PondPack software and the detention routing was performed with the design of the detention basin and the proposed outlet structure. The 100-year hydrograph was routed through the basin to demonstrate that the post-development peak flow rate will comply with the detention requirements and that the detention facility will not overtop during the 100-year event.

The time of concentration coinciding with the basin outflow peak was established by adding the inflow hydrograph time of concentration plus the lag time of the detained flow within the basin. This combined time of concentration accounts for the time of concentration to get to the basin and the detention time within the basin. The riser for each basin was designed to ensure that riser size, rim elevation, and orifice placement will work in conjunction to properly mitigate the increased flow rate.

Preliminary detention modeling has been completed for BMPs 1 and 2, and the hydrograph routing calculations and detention models are included in Appendix 4. With detention, the proposed 100-

year flow rates at the project outfalls are less than the existing flow rates. The 50-year calculations for detention will be included in final engineering.

4.6 Hydraulics

Hydraulic calculations for the storm drains will be completed during final engineering. However, given the extensive drainage area that drains to the existing 48" storm drain on Cactus Road, a preliminary analysis of the area has been conducted.

To analyze the existing 48" storm drain on Cactus Road, Bentley's Culvert Master program was used to identify water surface elevations. The existing surface on Cactus Road is approximately 495.0'. To ensure that the proposed condition will not cause any detrimental damage downstream, the proposed flow (which includes the upstream run-on and the detained onsite flow) was routed through the existing 48" pipe in the program. In conclusion, the proposed water surface elevation is below 495' and thus, water is not expected to overtop the road during the 100-year storm event.

Furthermore, the existing drainage ditch north of proposed basin BMP-3, collects offsite flow and directs water to the existing 48" storm drain. To ensure that the flow in this drainage ditch will not overtop and flow into proposed BMP-1, a cross-section analysis was conducted. Bentley's Flow Master program was used to analyze upstream and downstream cross sections for the existing drainage channel. In conclusion, the water elevation in the channel stays within the limits of the channel and will not overtop. See Appendix 5 for calculations. Furthermore, the preliminary design for all detention basins, including BMP-1, includes additional depth for freeboard. See Appendix 4 for detention basin calculations.

4.7 Water Quality Calculations and Hydromodification

The water quality calculations are included, under a separate cover, in the Storm Water Quality Management Plan (SWQMP) prepared by PDC. Two proposed biofiltration basins will be combined hydromodification/biofiltration/detention basins. All the biofiltration basins also address hydromodification requirements, since both biofiltration basins and hydromodification basins produce similar alterations to the flow regime for the smaller, more frequent storm events.

The majority of all onsite water will be treated with biofiltration/hydromodification basins, which will detain the smaller, more frequent events. Four modular wetland units are also proposed, and they are located on Cactus Road, Airway Road, and Continental Street. Refer to the SWQMP report prepared by PDC for detailed calculations.

5. CONCLUSION

Proposed project development complies with detention criteria outlined in previous studies, and therefore, should not adversely affect downstream drainage conditions. The proposed onsite storm drain infrastructure will be adequate to convey the design flows. The storm drain detention facilities are designed as combined facilities for hydromodification and water quality purposes in addition to peak flow detention.

APPENDIX 1

Mannings and Runoff Coefficients, FEMA Map, Web Soil Survey, Rain Isopluvials

MANNINGS AND C COEFFICIENTS

Table A-1. Runoff Coefficients for Rational Method

Land Use	Runoff Coefficient (C)
	Soil Type [1]
Residential:	
Single Family	0.55
Multi-Units	0.70
Mobile Homes	0.65
Rural (lots greater than ½ acre)	0.45
Commercial [2]	
80% Impervious	0.85
Industrial [2]	
90% Impervious	0.95

Note:
[1] Type D soil to be used for all areas.
[2] Where actual conditions deviate significantly from the tabulated imperviousness values of 80% or 90%, the values given for coefficient C, may be revised by multiplying 80% or 90% by the ratio of actual imperviousness to the tabulated imperviousness. However, in case shall the final coefficient be less than 0.50. For example: Consider commercial property on D soil.

Actual imperviousness = 50%
Tabulated imperviousness = 80%
Revised C = (50/80) x 0.85 = 0.53

The values in Table A–1 are typical for urban areas. However, if the basin contains rural or agricultural land use, parks, golf courses, or other types of nonurban land use that are expected to be permanent, the appropriate value should be selected based upon the soil and cover and approved by the City.

A.1.3. Rainfall Intensity

The rainfall intensity (I) is the rainfall in inches per hour (in/hr.) for a duration equal to the T_c for a selected storm frequency. Once a particular storm frequency has been selected for design and a T_c calculated for the drainage area, the rainfall intensity can be determined from the Intensity-Duration-Frequency Design Chart (Figure A-1).

Table C-3. Average Manning Roughness Coefficients for Small Open Channels Conveying Less than 50 cfs[1]

Lining Type	Design Flow Depth		
	0 – 0.5 ft	0.5 – 2.0 ft	> 2.0 ft
Concrete (Poured)	0.015	0.013	0.013
Air Blown Concrete	0.023	0.019	0.016
Grouted Riprap	0.040	0.030	0.028
Stone Masonry	0.042	0.032	0.030
Soil Cement	0.025	0.022	0.020
Bare Soil	0.023	0.020	0.020
Rock Cut	0.045	0.035	0.025
Rock Riprap	Based on Rock Size (See Chapter 7, Section 7.6.17)		

[1] Based on materials and workmanship required by standard specifications.

Table C-4. Average Manning Roughness Coefficients for Larger Open Channels

Channel	Manning Roughness Coefficient(n)
Unlined Channels	
Clay Loam	0.023
Sand	0.020
Lined Channels	
Grass Lined (well maintained)	0.035
Grass Lined (not maintained)	0.045
Wetland-Bottom Channels (New Channel)	0.023
Wetland-Bottom Channels (Mature Channel)	See Table A–5
Riprap-Lined Channels	See Chapter 7, Section 7.6.17
Concrete (Poured)	0.014
Air Blown Mortar (Gunite or Shotcrete)[1]	0.016
Asphaltic Concrete or Bituminous Plant Mix	0.018

[1] For air blown concrete, use n=0.012 (if troweled) and n=0.025 if purposely roughened.
Note: For channels with revetments or multiple lining types, use composite Manning roughness coefficient based on component lining materials.

FROM DRAINAGE STUDY FOR THE OTAY MESA COMMUNITY PLAN UPDATE PREPARED BY KIMLEY-HORN AND ASSOCIATES DATED APRIL 2007

EXPLANATION OF WEST WATERSHED

VII. RECOMMENDED DRAINAGE DESIGN CRITERIA

Since the five watershed areas on the Mesa flow in every direction except east, they flow into different watersheds with different constraints and impacts. The runoff from the five watersheds will have different criteria for design of drainage facilities.

West Perimeter Watershed

This watershed consists of smaller Mesa-top watersheds with a total area of approximately 254 acres that drain to the west to three separate creeks in canyons and gullies. These creeks are carried under the SD&AE and Trolley tracks and through San Ysidro in buried storm drain systems. The storm drains under the tracks have hydraulic capacities of 30 cfs (18" RCP) and 125 cfs (36" RCP) based on the San Ysidro Boulevard Area Master Drainage plan prepared by BSI Consultants, February 15, 1996. Sub-basins OT3-7 and OT3-8 combine downstream into a single creek that flows to the 36" RCP. The current study estimates 140 cfs (Q100) will flow off of the Mesa into this sub-basin. This study does not address the capacity of the downstream system or include the hydrologic analysis for areas to the west of the Mesa, but clearly the 125 cfs capacity of the existing system will be exceeded. This area will need to be addressed in more detail during design of the upstream tributary development. Detention Basins are recommended which will reduce peak flows in the sub-basin to minimize impacts on the downstream system. These detention basins will reduce the peak, 50-year, and 100-year flow to predevelopment levels. Because of the unstable soils in this area, care should be taken that the proposed detention basins and relocated drainage facilities do not contribute to an increase in the risk of slides through increased saturation of the soil.

West Watershed

The West Watershed consists of smaller Mesa-top watersheds that drain into the tributary canyons of Spring Canyon. All of the flow from the watershed flows into Mexico at the Spring Canyon concentration point. Detention basins will be required to reduce the post-development peak flows to predevelopment levels for the 50-year and 100-year storm. If the detention basins concentrate flows at the upper edge of canyons, care must be taken to ensure that erosion potential is not increased downstream.

East Watershed

The East Watershed flows to Mexico at a single concentration point between Britannia and La Media roads. Requirements for the control of peak runoff from development in this watershed already exist. The "Notice" dated August 7, 1987 (page 2), sets criteria for detention basins and for storm drain sizing. As part of the future storm drain project in this watershed, a single detention basin will be constructed at the border. The construction of this basin will eliminate the need for individual on-site detention basins for subsequent development.

North Perimeter Watershed

These small watersheds along the northern edge of the Mesa flow into small canyons that flow into the Otay River. There are no peak flow attenuation requirements for flows from these watersheds. There may be water quality issues with the Otay River, and there may be erosion issues from storm drains on the Mesa. Only approximately 14 acres of Neighborhood 6 are in this watershed.

FEMA

National Flood Hazard Layer FIRMette

FEMA

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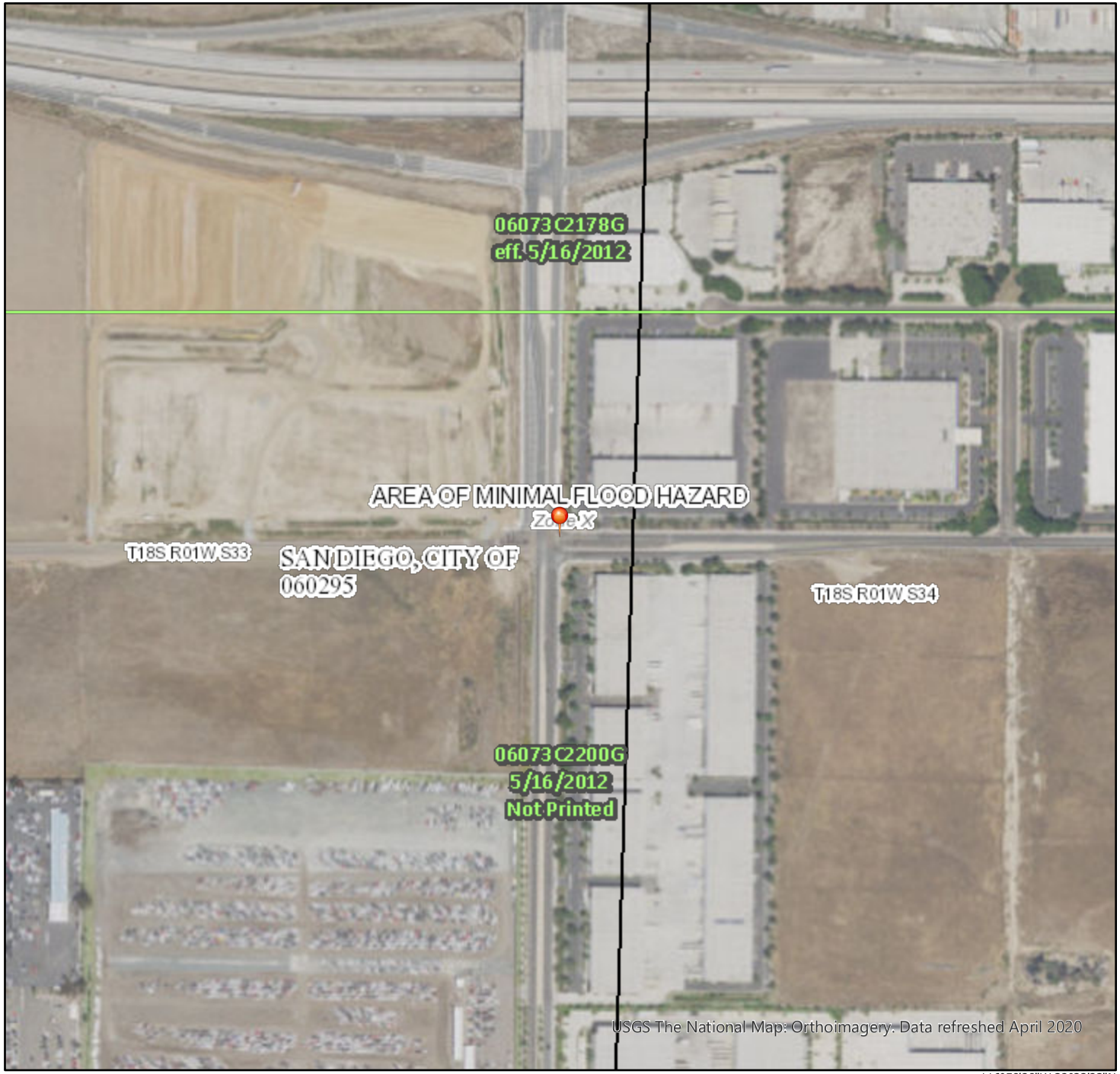

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Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

SPECIAL FLOOD HAZARD AREAS
- Without Base Flood Elevation (BFE) *Zone A, V, A99*
- With BFE or Depth *Zone AE, AO, AH, VE, AR*
- Regulatory Floodway

OTHER AREAS OF FLOOD HAZARD
- 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile *Zone X*
- Future Conditions 1% Annual Chance Flood Hazard *Zone X*
- Area with Reduced Flood Risk due to Levee. See Notes. *Zone X*
- Area with Flood Risk due to Levee *Zone D*

OTHER AREAS
- NO SCREEN Area of Minimal Flood Hazard *Zone X*
- Effective LOMRs
- Area of Undetermined Flood Hazard *Zone D*

GENERAL STRUCTURES
- Channel, Culvert, or Storm Sewer
- Levee, Dike, or Floodwall

OTHER FEATURES
- 20.2 / 17.5 Cross Sections with 1% Annual Chance / Water Surface Elevation
- Coastal Transect
- 513 Base Flood Elevation Line (BFE)
- Limit of Study
- Jurisdiction Boundary
- Coastal Transect Baseline
- Profile Baseline
- Hydrographic Feature

MAP PANELS
- Digital Data Available
- No Digital Data Available
- Unmapped

N

The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 8/24/2020 at 1:29 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

National Flood Hazard Layer FIRMette

FEMA

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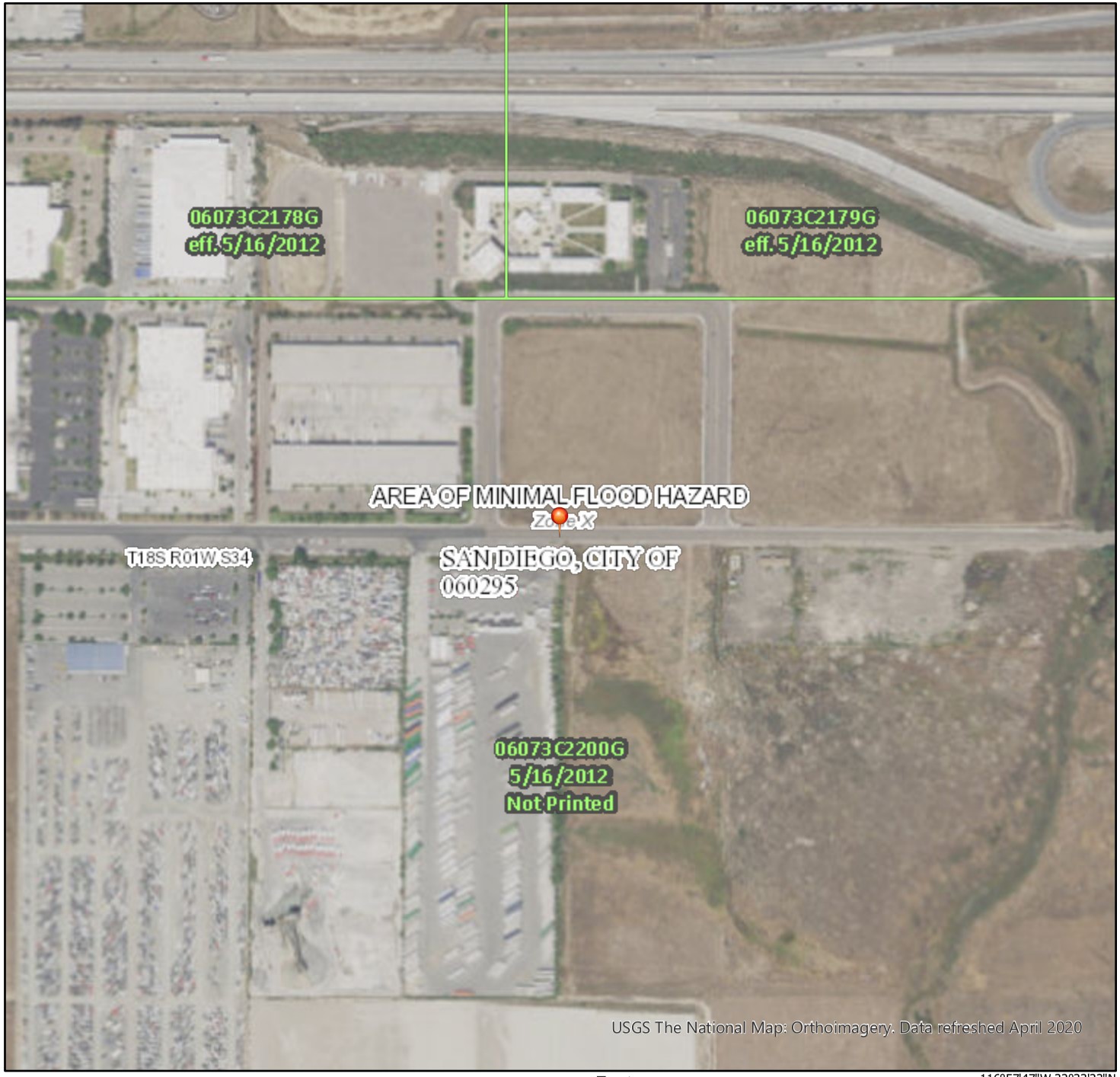

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Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

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- Future Conditions 1% Annual Chance Flood Hazard *Zone X*
- Area with Reduced Flood Risk due to Levee. See Notes. *Zone X*
- Area with Flood Risk due to Levee *Zone D*

OTHER AREAS
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- Effective LOMRs
- Area of Undetermined Flood Hazard *Zone D*

GENERAL STRUCTURES
- Channel, Culvert, or Storm Sewer
- Levee, Dike, or Floodwall

OTHER FEATURES
- 20.2 / 17.5 Cross Sections with 1% Annual Chance / Water Surface Elevation
- Coastal Transect
- 513 Base Flood Elevation Line (BFE)
- Limit of Study
- Jurisdiction Boundary
- Coastal Transect Baseline
- Profile Baseline
- Hydrographic Feature

MAP PANELS
- Digital Data Available
- No Digital Data Available
- Unmapped

N

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National Flood Hazard Layer FIRMette

FEMA

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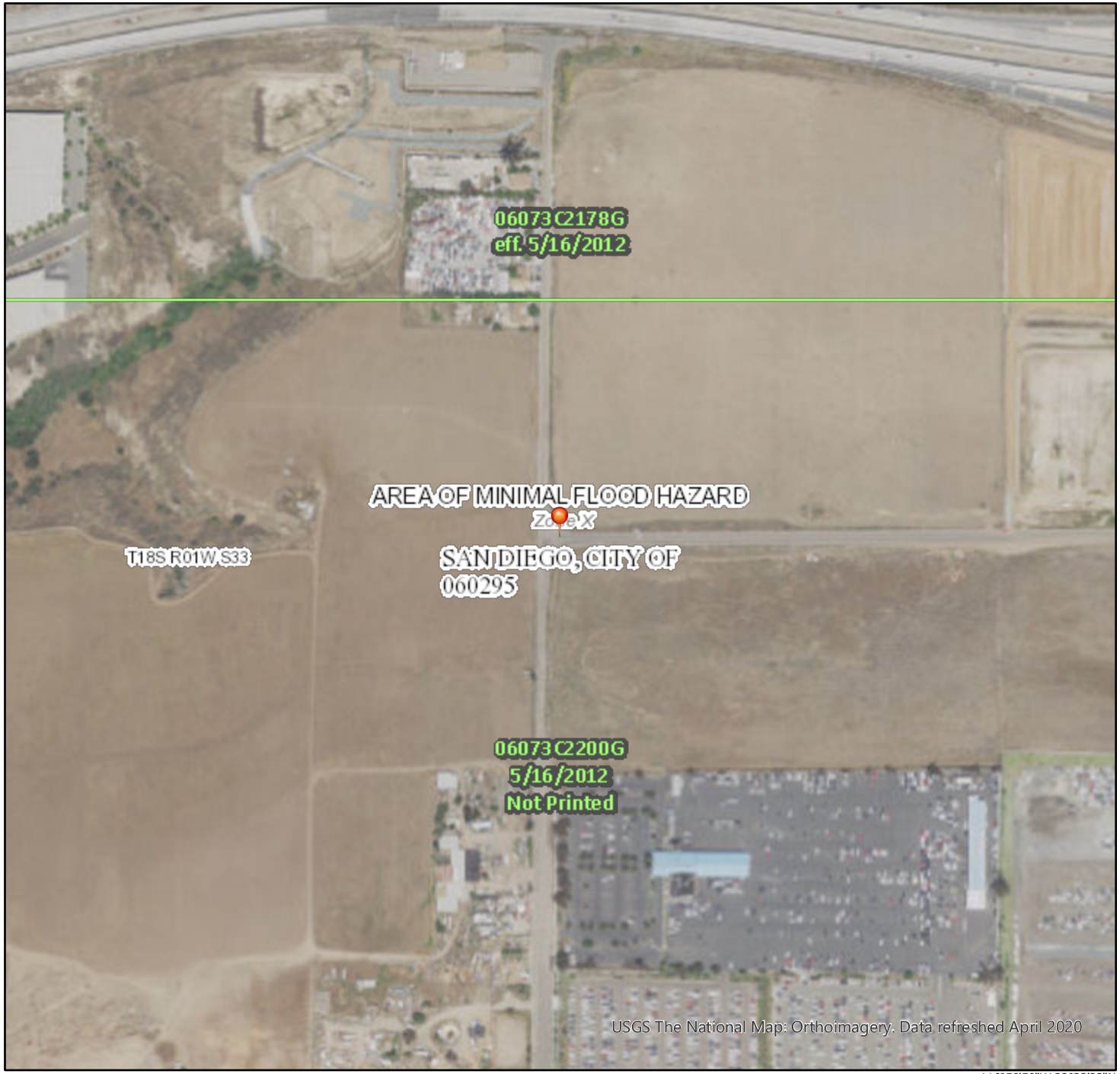

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Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

SPECIAL FLOOD HAZARD AREAS
- Without Base Flood Elevation (BFE) *Zone A, V, A99*
- With BFE or Depth *Zone AE, AO, AH, VE, AR*
- Regulatory Floodway

OTHER AREAS OF FLOOD HAZARD
- 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile *Zone X*
- Future Conditions 1% Annual Chance Flood Hazard *Zone X*
- Area with Reduced Flood Risk due to Levee. See Notes. *Zone X*
- Area with Flood Risk due to Levee *Zone D*

OTHER AREAS
- NO SCREEN Area of Minimal Flood Hazard *Zone X*
- Effective LOMRs
- Area of Undetermined Flood Hazard *Zone D*

GENERAL STRUCTURES
- Channel, Culvert, or Storm Sewer
- Levee, Dike, or Floodwall

OTHER FEATURES
- 20.2 Cross Sections with 1% Annual Chance
- 17.5 Water Surface Elevation
- Coastal Transect
- 513 Base Flood Elevation Line (BFE)
- Limit of Study
- Jurisdiction Boundary
- Coastal Transect Baseline
- Profile Baseline
- Hydrographic Feature

MAP PANELS
- Digital Data Available
- No Digital Data Available
- Unmapped

N

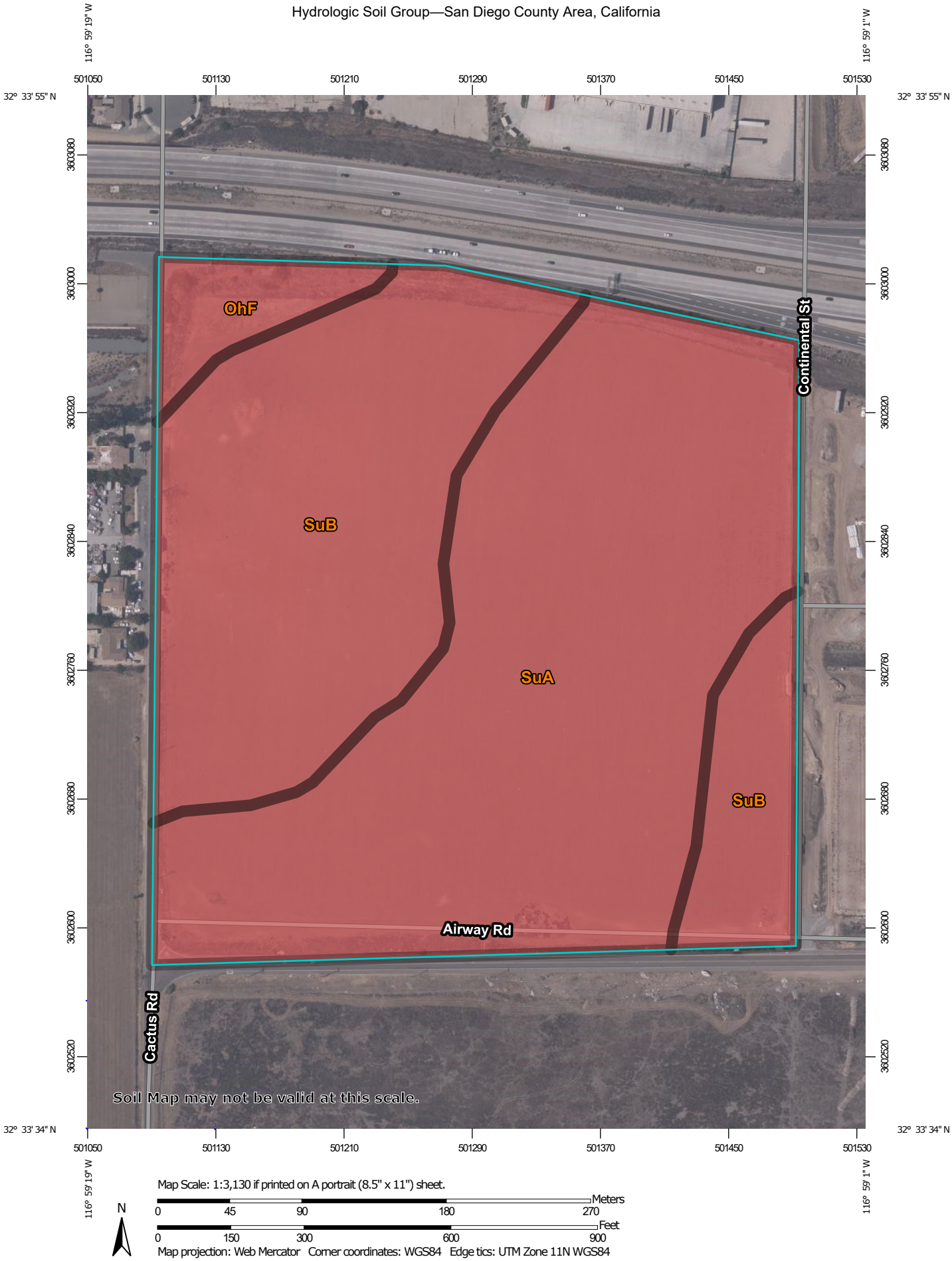
The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 8/24/2020 at 1:31 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

WEB SOIL SURVEY


116° 59' 19" W
116° 59' 1" W
501050
501130
501210
501290
501370
501450
501530
32° 33' 55" N
32° 33' 34" N
3603080
3603000
3602920
3602840
3602760
3602680
3602600
3602520
OhF
SuB
SuA
SuB
Continental St
Airway Rd
Cactus Rd
Soil Map may not be valid at this scale.
Map Scale: 1:3,130 if printed on A portrait (8.5" x 11") sheet.
N
Meters
0 45 90 180 270
Feet
0 150 300 600 900
Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 11N WGS84

MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Rating Polygons

A

A/D

B

B/D

C

C/D

D

Not rated or not available

Soil Rating Lines

A

A/D

B

B/D

C

C/D

D

Not rated or not available

Soil Rating Points

A

A/D

B

B/D

C

C/D

D

Not rated or not available

Water Features

Streams and Canals

Transportation

Rails

Interstate Highways

US Routes

Major Roads

Local Roads

Background

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL:
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: San Diego County Area, California
Survey Area Data: Version 16, Sep 13, 2021

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Aug 18, 2018—Aug 22, 2018

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
OhF	Olivenhain cobbly loam, 30 to 50 percent slopes	D	1.7	4.2%
SuA	Stockpen gravelly clay loam, 0 to 2 percent slopes	D	23.0	55.5%
SuB	Stockpen gravelly clay loam, 2 to 5 percent slopes	D	16.7	40.4%
Totals for Area of Interest			**41.5**	**100.0%**

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

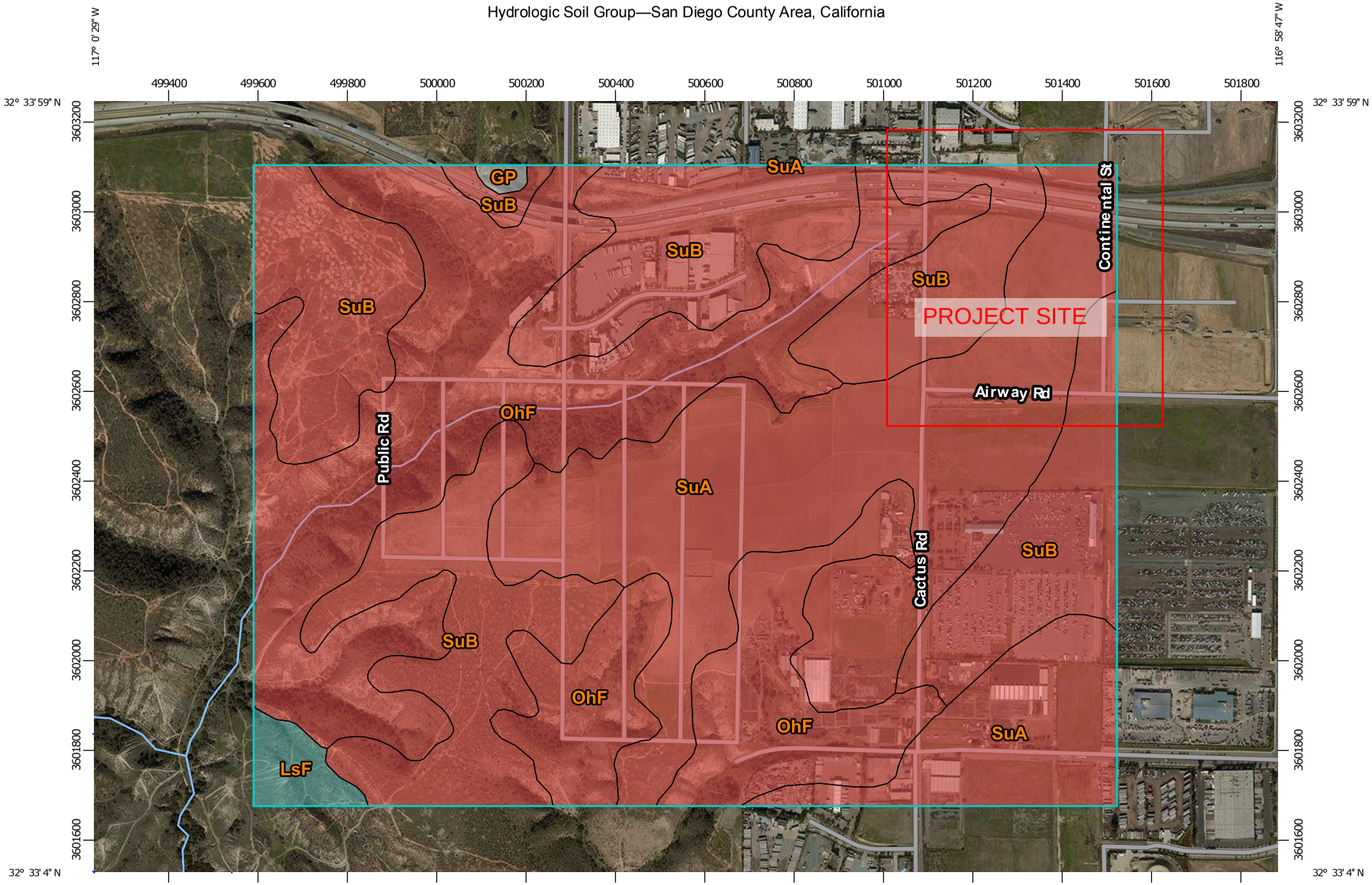
Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

Hydrologic Soil Group—San Diego County Area, California



Map Scale: 1:12,100 if printed on A landscape (11" x 8.5") sheet.

N

Meters: 0 150 300 600 900

Feet: 0 500 1000 2000 3000

Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 11N WGS84

MAP LEGEND

Area of Interest (AOI)

- Area of Interest (AOI)

Soils

Soil Rating Polygons

- A
- A/D
- B
- B/D
- C
- C/D
- D
- Not rated or not available

Soil Rating Lines

- A
- A/D
- B
- B/D
- C
- C/D
- D
- Not rated or not available

Soil Rating Points

- A
- A/D
- B
- B/D
- C
- C/D
- D
- Not rated or not available

Water Features

- Streams and Canals

Transportation

- Rails
- Interstate Highways
- US Routes
- Major Roads
- Local Roads

Background

- Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL: http://websoilsurvey.nrcs.usda.gov
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: San Diego County Area, California
Survey Area Data: Version 8, Sep 17, 2014

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Dec 7, 2014—Jan 4, 2015

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Hydrologic Soil Group

Hydrologic Soil Group— Summary by Map Unit — San Diego County Area, California (CA638)				
Map unit symbol	**Map unit name**	**Rating**	**Acres in AOI**	**Percent of AOI**
GP	Gravel pits		1.5	0.2%
LsF	Linne clay loam, 30 to 50 percent slopes	C	8.5	1.2%
OhF	Olivenhain cobbly loam, 30 to 50 percent slopes	D	236.4	34.5%
SuA	Stockpen gravelly clay loam, 0 to 2 percent slopes	D	205.2	30.0%
SuB	Stockpen gravelly clay loam, 2 to 5 percent slopes	D	233.4	34.1%
Totals for Area of Interest			**684.9**	**100.0%**

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

RAINFALL ISOPLUVIALS

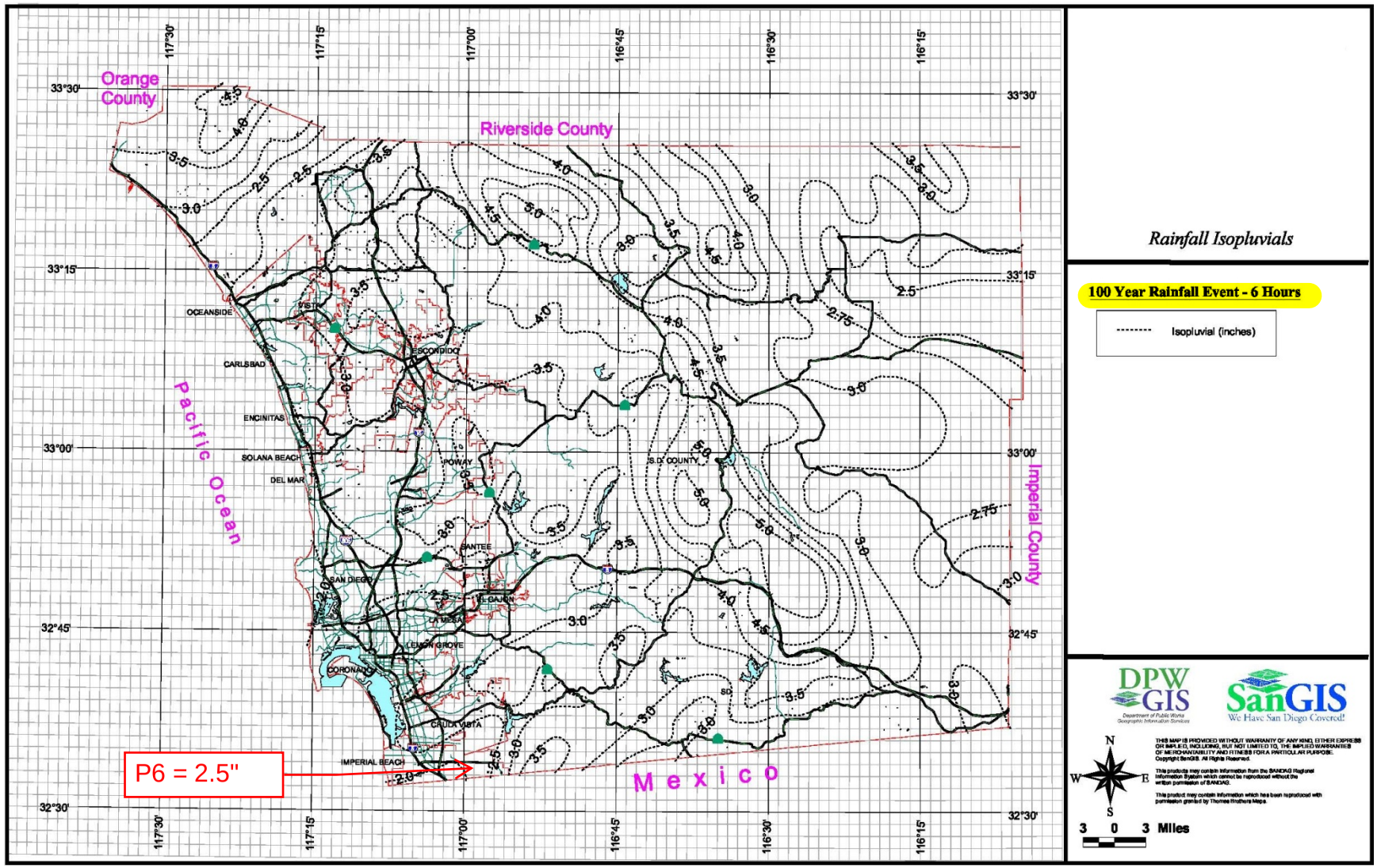


Figure B-2. 100-Year 6-Hour Isopluvials.

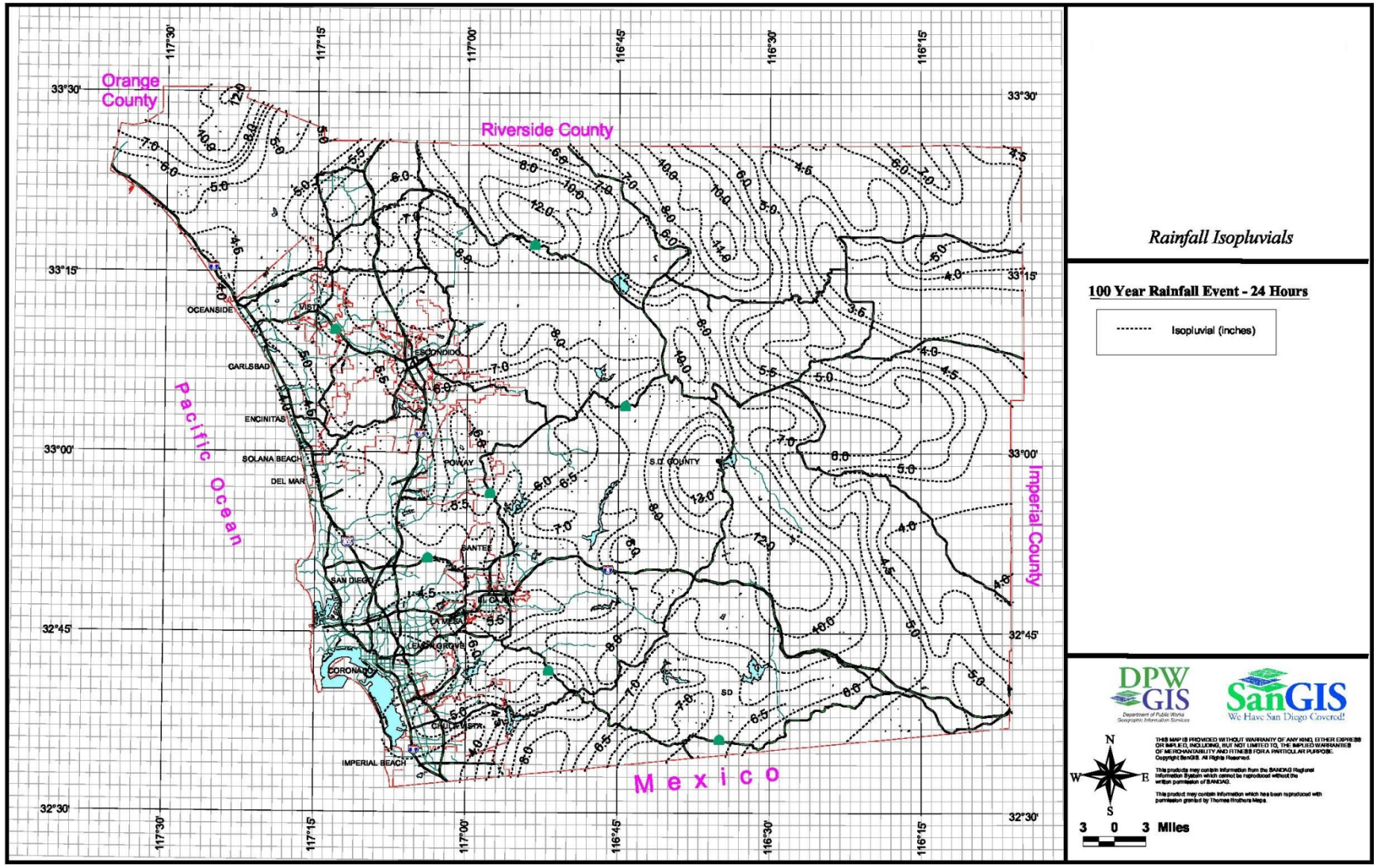


Figure B-3. 100-Year 24-Hour Isopluvials

APPENDIX 2

Existing Conditions Rational Method Computer Output

```
                San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2003 Version 6.3

Rational method hydrology  program based on
San Diego County Flood Control Division 1985 hydrology manual
        Rational Hydrology Study        Date: 01/31/24
------------------------------------------------------------------------
4481 COLLECTION AT CACTUS
EXISTING CONDITIONS
100-YEAR
FILE:S100E100
------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

------------------------------------------------------------------------


Program License Serial Number 4049

------------------------------------------------------------------------
Rational hydrology study storm event year is   100.0
English (in-lb) input data Units used
English (in) rainfall data used

Standard intensity of Appendix I-B used for year and
Elevation 0 - 1500 feet
Factor (to multiply * intensity)  =  1.000
Only used if inside City of San Diego
San Diego hydrology manual 'C' values used
Runoff coefficients by rational method



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      101.000 to Point/Station      102.000
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[RURAL(greater than 0.5 Ac, 0.2 ha) area type]
Initial subarea flow distance  =  100.000(Ft.)
Highest elevation =  510.000(Ft.)
Lowest elevation =  509.700(Ft.)
Elevation difference =    0.300(Ft.)
Time of concentration calculated by the urban
areas overland flow method (App X-C) =    17.48 min.
TC = [1.8*(1.1-C)*distance(Ft.)^.5)/(% slope^(1/3)]
TC = [1.8*(1.1-0.4500)*( 100.000^.5)/( 0.300^(1/3)]=  17.48
Rainfall intensity (I) =      2.733(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.450
Subarea runoff =      0.320(CFS)
Total initial stream area =        0.260(Ac.)



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      102.000 to Point/Station      103.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****
```



```
------------------------------------------------------------------------
Estimated mean flow rate at midpoint of channel =     23.272(CFS)
Depth of flow =   0.657(Ft.), Average velocity =   1.352(Ft/s)
       ******* Irregular Channel Data ***********
------------------------------------------------------------------------
Information entered for subchannel number 1 :
Point number      'X' coordinate     'Y' coordinate
        1              0.00             1.25
        2            112.00             0.25
        3            119.00             0.00
        4            126.00             0.25
        5            132.00             1.25
Manning's 'N' friction factor =   0.045
------------------------------------------------------------------------
Sub-Channel flow  =     23.272(CFS)
  '     '       flow top width =     62.002(Ft.)
  '     '    velocity=    1.352(Ft/s)
  '     '       area =     17.209(Sq.Ft)
  '     '       Froude number =     0.452

Upstream point elevation =   509.700(Ft.)
Downstream point elevation =   490.000(Ft.)
Flow length =  2124.610(Ft.)
Travel time  =   26.18 min.
Time of concentration =   43.66 min.
Depth of flow =   0.657(Ft.)
Average velocity =   1.352(Ft/s)
Total irregular channel flow =    23.272(CFS)
Irregular channel normal depth above invert elev. =   0.657(Ft.)
Average velocity of channel(s) =   1.352(Ft/s)

Sub-Channel No. 1 Critical depth =      0.502(Ft.)
  '     '       '     Critical flow top width =     43.730(Ft.)
  '     '       '     Critical flow velocity=    2.579(Ft/s)
  '     '       '     Critical flow area =      9.023(Sq.Ft)

 Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[RURAL(greater than 0.5 Ac, 0.2 ha) area type]
Rainfall intensity =      1.661(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.450
Subarea runoff =     27.887(CFS) for   37.320(Ac.)
Total runoff =     28.207(CFS)  Total area =       37.58(Ac.)



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      103.000 to Point/Station      103.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 1
Stream flow area =     37.580(Ac.)
Runoff from this stream =     28.207(CFS)
Time of concentration =   43.66 min.
Rainfall intensity =     1.661(In/Hr)



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
```

```
Process from Point/Station      104.000 to Point/Station      105.000
**** INITIAL AREA EVALUATION ****
----------------------------------------------------------------------
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[RURAL(greater than 0.5 Ac, 0.2 ha) area type]
Initial subarea flow distance  =  100.000(Ft.)
Highest elevation =  513.000(Ft.)
Lowest elevation =  512.000(Ft.)
Elevation difference =    1.000(Ft.)
Time of concentration calculated by the urban
areas overland flow method (App X-C) =    11.70 min.
TC = [1.8*(1.1-C)*distance(Ft.)^.5)/(% slope^(1/3)]
TC = [1.8*(1.1-0.4500)*( 100.000^.5)/( 1.000^(1/3)]=  11.70
Rainfall intensity (I) =      3.187(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.450
Subarea runoff =      0.602(CFS)
Total initial stream area =        0.420(Ac.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      105.000 to Point/Station      106.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****
----------------------------------------------------------------------
Estimated mean flow rate at midpoint of channel =      4.152(CFS)
Depth of flow =   0.625(Ft.), Average velocity =   1.180(Ft/s)
        ******* Irregular Channel Data ***********
------------------------------------------------------------------
Information entered for subchannel number 1 :
Point number      'X' coordinate     'Y' coordinate
        1              0.00              1.00
        2              9.00              0.00
        3             18.00              1.00
Manning's 'N' friction factor =   0.045
------------------------------------------------------------------
Sub-Channel flow  =      4.152(CFS)
   '      '        flow top width =     11.258(Ft.)
   '      '    velocity=    1.180(Ft/s)
   '      '        area =      3.520(Sq.Ft)
   '      '        Froude number =     0.372

Upstream point elevation =   512.000(Ft.)
Downstream point elevation =   510.000(Ft.)
Flow length =   330.000(Ft.)
Travel time  =    4.66 min.
Time of concentration =   16.36 min.
Depth of flow =   0.625(Ft.)
Average velocity =   1.180(Ft/s)
Total irregular channel flow =     4.152(CFS)
Irregular channel normal depth above invert elev. =   0.625(Ft.)
Average velocity of channel(s) =   1.180(Ft/s)

Sub-Channel No. 1 Critical depth =      0.422(Ft.)
   '      '       '     Critical flow top width =      7.594(Ft.)
   '      '       '     Critical flow velocity=    2.592(Ft/s)
   '      '       '     Critical flow area =      1.602(Sq.Ft)

 Adding area flow to channel
Decimal fraction soil group A = 0.000
```



```
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[SINGLE FAMILY area type                    ]
Rainfall intensity =      2.807(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.550
Subarea runoff =      7.643(CFS) for    4.950(Ac.)
Total runoff =      8.246(CFS)  Total area =        5.37(Ac.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      106.000 to Point/Station      107.000
**** PIPEFLOW TRAVEL TIME (User specified size) ****
----------------------------------------------------------------------
Upstream point/station elevation =   509.000(Ft.)
Downstream point/station elevation =   508.000(Ft.)
Pipe length  =    50.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     8.246(CFS)
Given pipe size =     18.00(In.)
Calculated individual pipe flow  =     8.246(CFS)
Normal flow depth in pipe =    9.57(In.)
Flow top width inside pipe =   17.96(In.)
Critical Depth =   13.35(In.)
Pipe flow velocity =      8.62(Ft/s)
Travel time through pipe =    0.10 min.
Time of concentration (TC) =    16.46 min.
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      107.000 to Point/Station      108.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****
----------------------------------------------------------------------
Estimated mean flow rate at midpoint of channel =      8.775(CFS)
Depth of flow =   0.740(Ft.), Average velocity =   1.602(Ft/s)
        ******* Irregular Channel Data ***********
------------------------------------------------------------------
Information entered for subchannel number 1 :
Point number      'X' coordinate     'Y' coordinate
        1              0.00              1.00
        2             10.00              0.00
        3             20.00              1.00
Manning's 'N' friction factor =   0.045
------------------------------------------------------------------
Sub-Channel flow  =      8.775(CFS)
   '      '        flow top width =     14.802(Ft.)
   '      '    velocity=    1.602(Ft/s)
   '      '        area =      5.478(Sq.Ft)
   '      '        Froude number =     0.464

Upstream point elevation =   508.000(Ft.)
Downstream point elevation =   501.000(Ft.)
Flow length =   785.000(Ft.)
Travel time  =    8.17 min.
Time of concentration =   24.63 min.
Depth of flow =   0.740(Ft.)
Average velocity =   1.602(Ft/s)
Total irregular channel flow =     8.775(CFS)
Irregular channel normal depth above invert elev. =   0.740(Ft.)
Average velocity of channel(s) =   1.602(Ft/s)
```

```
Sub-Channel No. 1 Critical depth =      0.543(Ft.)
   '     '       '     Critical flow top width =     10.859(Ft.)
   '     '       '     Critical flow velocity=    2.977(Ft/s)
   '     '       '     Critical flow area =      2.948(Sq.Ft)

 Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[RURAL(greater than 0.5 Ac, 0.2 ha) area type]
Rainfall intensity =      2.338(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.450
Subarea runoff =      0.726(CFS) for    0.690(Ac.)
Total runoff =      8.972(CFS)  Total area =        6.06(Ac.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      108.000 to Point/Station      103.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****
________________________________________________________________________
Depth of flow =   0.188(Ft.), Average velocity =   1.289(Ft/s)
       ******* Irregular Channel Data ***********
------------------------------------------------------------------
Information entered for subchannel number 1 :
Point number      'X' coordinate     'Y' coordinate
       1              0.00              0.40
       2             30.00              0.00
       3             60.00              0.00
Manning's 'N' friction factor =   0.045
------------------------------------------------------------------
Sub-Channel flow  =      8.972(CFS)
   '     '        flow top width =     44.092(Ft.)
   '     '    velocity=    1.289(Ft/s)
   '     '        area =      6.961(Sq.Ft)
   '     '        Froude number =     0.572

Upstream point elevation =   501.000(Ft.)
Downstream point elevation =   490.000(Ft.)
Flow length =   616.000(Ft.)
Travel time  =    7.97 min.
Time of concentration =   32.59 min.
Depth of flow =   0.188(Ft.)
Average velocity =   1.289(Ft/s)
Total irregular channel flow =     8.972(CFS)
Irregular channel normal depth above invert elev. =   0.188(Ft.)
Average velocity of channel(s) =   1.289(Ft/s)

Sub-Channel No. 1 Critical depth =      0.133(Ft.)
   '     '       '     Critical flow top width =     39.961(Ft.)
   '     '       '     Critical flow velocity=    1.931(Ft/s)
   '     '       '     Critical flow area =      4.646(Sq.Ft)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      109.000 to Point/Station      103.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
Decimal fraction soil group A = 0.000
```



```
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                        ]
Note: user entry of impervious value, Ap = 0.950
Time of concentration =    32.59 min.
Rainfall intensity =      2.000(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 1.003
Subarea runoff =      0.882(CFS) for    0.440(Ac.)
Total runoff =      9.854(CFS)  Total area =        6.50(Ac.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      103.000 to Point/Station      103.000
**** CONFLUENCE OF MINOR STREAMS ****
________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      6.500(Ac.)
Runoff from this stream =      9.854(CFS)
Time of concentration =   32.59 min.
Rainfall intensity =     2.000(In/Hr)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      208.000 to Point/Station      103.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****
________________________________________________________________________
User specified 'C' value of 0.560 given for subarea
Rainfall intensity (I) =      2.017(In/Hr) for a   100.0 year storm
User specified values are as follows:
TC =  32.14 min.  Rain intensity =       2.02(In/Hr)
Total area =       61.120(Ac.)  Total runoff =    73.260(CFS)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      103.000 to Point/Station      103.000
**** CONFLUENCE OF MINOR STREAMS ****
________________________________________________________________________
Along Main Stream number: 1 in normal stream number 3
Stream flow area =     61.120(Ac.)
Runoff from this stream =     73.260(CFS)
Time of concentration =   32.14 min.
Rainfall intensity =     2.017(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       28.207     43.66                  1.661
2        9.854     32.59                  2.000
3       73.260     32.14                  2.017
Qmax(1) =
           1.000 *    1.000 *    28.207) +
           0.830 *    1.000 *     9.854) +
           0.823 *    1.000 *    73.260) + =      96.714
Qmax(2) =
           1.000 *    0.746 *    28.207) +
           1.000 *    1.000 *     9.854) +
```

```
            0.992 *    1.000 *    73.260) + =     103.553
Qmax(3) =
            1.000 *    0.736 *    28.207) +
            1.000 *    0.986 *     9.854) +
            1.000 *    1.000 *    73.260) + =     103.741

Total of 3 streams to confluence:
Flow rates before confluence point:
      28.207       9.854      73.260
Maximum flow rates at confluence using above data:
       96.714      103.553      103.741
Area of streams before confluence:
       37.580        6.500       61.120
Results of confluence:
Total flow rate =    103.741(CFS)
Time of concentration =    32.140 min.
Effective stream area after confluence =    105.200(Ac.)
End of computations, total study area =         105.200 (Ac.)
```

```
                San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2003 Version 6.3

Rational method hydrology  program based on
San Diego County Flood Control Division 1985 hydrology manual
        Rational Hydrology Study        Date: 01/25/24
--------------------------------------------------------------------------
4481 COLLECTION AT CACTUS
EXISTING CONDITIONS
100-YEAR
FILE: S200E100
--------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

--------------------------------------------------------------------------


Program License Serial Number 4049

--------------------------------------------------------------------------
Rational hydrology study storm event year is   100.0
English (in-lb) input data Units used
English (in) rainfall data used

Standard intensity of Appendix I-B used for year and
Elevation 0 - 1500 feet
Factor (to multiply * intensity)  =  1.000
Only used if inside City of San Diego
San Diego hydrology manual 'C' values used
Runoff coefficients by rational method



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      200.000 to Point/Station      201.000
**** INITIAL AREA EVALUATION ****
--------------------------------------------------------------------------
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[SINGLE FAMILY area type                    ]
Initial subarea flow distance  =  100.000(Ft.)
Highest elevation =  516.000(Ft.)
Lowest elevation =  514.000(Ft.)
Elevation difference =    2.000(Ft.)
Time of concentration calculated by the urban
areas overland flow method (App X-C) =     7.86 min.
TC = [1.8*(1.1-C)*distance(Ft.)^.5)/(% slope^(1/3)]
TC = [1.8*(1.1-0.5500)*( 100.000^.5)/( 2.000^(1/3)]=   7.86
Rainfall intensity (I) =      3.684(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.550
Subarea runoff =      0.142(CFS)
Total initial stream area =        0.070(Ac.)



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      201.000 to Point/Station      202.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
```



```
--------------------------------------------------------------------------
Top of street segment elevation =   514.000(Ft.)
End of street segment elevation =   510.000(Ft.)
Length of street segment  =  1020.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  55.000(Ft.)
Distance from crown to crossfall grade break  =  53.500(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   1.500(Ft.)
Gutter hike from flowline =  0.125(In.)
 Manning's N in gutter =  0.0170
 Manning's N from gutter to grade break =  0.0130
 Manning's N from grade break to crown =  0.0130
Estimated mean flow rate at midpoint of street =      0.347(CFS)
Depth of flow =   0.102(Ft.), Average velocity =   0.978(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =   6.076(Ft.)
Flow velocity =   0.98(Ft/s)
Travel time =   17.37 min.     TC =   25.23  min.
 Adding area flow to street
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[SINGLE FAMILY area type                    ]
Rainfall intensity =      2.309(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.550
Subarea runoff =      3.670(CFS) for    2.890(Ac.)
Total runoff =      3.812(CFS)  Total area =        2.96(Ac.)
Street flow at end of street =      3.812(CFS)
Half street flow at end of street =      3.812(CFS)
Depth of flow =   0.268(Ft.), Average velocity =   1.854(Ft/s)
Flow width (from curb towards crown)=  14.389(Ft.)



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      202.000 to Point/Station      203.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
--------------------------------------------------------------------------
Upstream point/station elevation =   507.000(Ft.)
Downstream point/station elevation =   504.000(Ft.)
Pipe length  =   895.50(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     3.812(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =     3.812(CFS)
Normal flow depth in pipe =   10.34(In.)
Flow top width inside pipe =   17.80(In.)
Critical Depth =    8.96(In.)
Pipe flow velocity =      3.63(Ft/s)
Travel time through pipe =    4.11 min.
Time of concentration (TC) =    29.34 min.



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      204.000 to Point/Station      203.000
**** SUBAREA FLOW ADDITION ****
```

```
------------------------------------------------------------------------
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[SINGLE FAMILY area type                    ]
Time of concentration =    29.34 min.
Rainfall intensity =      2.127(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.550
Subarea runoff =     17.364(CFS) for   14.840(Ac.)
Total runoff =     21.176(CFS)  Total area =       17.80(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      205.000 to Point/Station      203.000
**** SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[SINGLE FAMILY area type                    ]
Time of concentration =    29.34 min.
Rainfall intensity =      2.127(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.550
Subarea runoff =      6.939(CFS) for    5.930(Ac.)
Total runoff =     28.115(CFS)  Total area =       23.73(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      206.000 to Point/Station      203.000
**** SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[SINGLE FAMILY area type                    ]
Time of concentration =    29.34 min.
Rainfall intensity =      2.127(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.550
Subarea runoff =     19.564(CFS) for   16.720(Ac.)
Total runoff =     47.678(CFS)  Total area =       40.45(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      207.000 to Point/Station      203.000
**** SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[SINGLE FAMILY area type                    ]
Time of concentration =    29.34 min.
Rainfall intensity =      2.127(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.550
Subarea runoff =     15.340(CFS) for   13.110(Ac.)
Total runoff =     63.018(CFS)  Total area =       53.56(Ac.)
```



```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      203.000 to Point/Station      208.000
**** PIPEFLOW TRAVEL TIME (User specified size) ****
------------------------------------------------------------------------
Upstream point/station elevation =   496.500(Ft.)
Downstream point/station elevation =   494.000(Ft.)
Pipe length  =   320.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    63.018(CFS)
Given pipe size =     36.00(In.)
NOTE: Normal flow is pressure flow in user selected pipe size.
The approximate hydraulic grade line above the pipe invert is
     2.207(Ft.)  at the headworks or inlet of the pipe(s)
 Pipe friction loss =      2.856(Ft.)
 Minor friction loss =      1.851(Ft.)  K-factor =   1.50
Pipe flow velocity =      8.92(Ft/s)
Travel time through pipe =    0.60 min.
Time of concentration (TC) =    29.94 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      209.000 to Point/Station      208.000
**** SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                       ]
Time of concentration =    29.94 min.
Rainfall intensity =      2.103(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.950
Subarea runoff =      5.873(CFS) for    2.940(Ac.)
Total runoff =     68.892(CFS)  Total area =       56.50(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      210.000 to Point/Station      208.000
**** SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[RURAL(greater than 0.5 Ac, 0.2 ha) area type]
Time of concentration =    29.94 min.
Rainfall intensity =      2.103(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.450
Subarea runoff =      4.372(CFS) for    4.620(Ac.)
Total runoff =     73.264(CFS)  Total area =       61.12(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      208.000 to Point/Station      103.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****
------------------------------------------------------------------------
Depth of flow =   1.703(Ft.), Average velocity =   2.708(Ft/s)
```

```
       ******* Irregular Channel Data ***********
------------------------------------------------------------------
Information entered for subchannel number 1 :
Point number      'X' coordinate     'Y' coordinate
       1              0.00              3.00
       2             35.00              0.00
       3             49.00              2.00
Manning's 'N' friction factor =   0.045
------------------------------------------------------------------
Sub-Channel flow  =     73.264(CFS)
  '     '        flow top width =     31.781(Ft.)
  '     '    velocity=    2.708(Ft/s)
  '     '        area =     27.054(Sq.Ft)
  '     '        Froude number =     0.517

Upstream point elevation =   493.000(Ft.)
Downstream point elevation =   490.000(Ft.)
Flow length =   357.000(Ft.)
Travel time  =    2.20 min.
Time of concentration =   32.14 min.
Depth of flow =   1.703(Ft.)
Average velocity =   2.708(Ft/s)
Total irregular channel flow =    73.264(CFS)
Irregular channel normal depth above invert elev. =   1.703(Ft.)
Average velocity of channel(s) =   2.708(Ft/s)

Sub-Channel No. 1 Critical depth =      1.313(Ft.)
  '     '       '     Critical flow top width =     24.500(Ft.)
  '     '       '     Critical flow velocity=    4.557(Ft/s)
  '     '       '     Critical flow area =     16.078(Sq.Ft)

End of computations, total study area =          61.120 (Ac.)
```

APPENDIX 3

Proposed Conditions Rational Method Computer Output

3000

```
                San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2003 Version 6.3

Rational method hydrology  program based on
San Diego County Flood Control Division 1985 hydrology manual
        Rational Hydrology Study        Date: 11/19/24
------------------------------------------------------------------------
4481 COLLECTION AT CACTUS
PROPOSED CONDITIONS
100-YEAR
FILE:S3000P100
------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

------------------------------------------------------------------------


Program License Serial Number 4049

------------------------------------------------------------------------
Rational hydrology study storm event year is   100.0
English (in-lb) input data Units used
English (in) rainfall data used

Standard intensity of Appendix I-B used for year and
Elevation 0 - 1500 feet
Factor (to multiply * intensity)  =  1.000
Only used if inside City of San Diego
San Diego hydrology manual 'C' values used
Runoff coefficients by rational method


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3007.000 to Point/Station     3008.000
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                    ]
Initial subarea flow distance  =   74.000(Ft.)
Highest elevation =  513.300(Ft.)
Lowest elevation =  512.600(Ft.)
Elevation difference =    0.700(Ft.)
Time of concentration calculated by the urban
areas overland flow method (App X-C) =     2.37 min.
TC = [1.8*(1.1-C)*distance(Ft.)^.5)/(% slope^(1/3)]
TC = [1.8*(1.1-0.9500)*(  74.000^.5)/(   0.946^(1/3)]=   2.37
Setting time of concentration to 5 minutes
Rainfall intensity (I) =      4.389(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.950
Subarea runoff =      0.125(CFS)
Total initial stream area =        0.030(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3008.000 to Point/Station     3009.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
```



```
------------------------------------------------------------------------
Top of street segment elevation =   512.600(Ft.)
End of street segment elevation =   507.000(Ft.)
Length of street segment  =   537.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.500(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  12.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   1.500(Ft.)
Gutter hike from flowline =  0.125(In.)
 Manning's N in gutter =  0.0130
 Manning's N from gutter to grade break =  0.0130
 Manning's N from grade break to crown =  0.0130
Estimated mean flow rate at midpoint of street =      0.149(CFS)
Depth of flow =   0.055(Ft.), Average velocity =   1.197(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =   3.728(Ft.)
Flow velocity =   1.20(Ft/s)
Travel time =    7.47 min.     TC =   12.47  min.
 Adding area flow to street
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                    ]
Rainfall intensity =      3.114(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.950
Subarea runoff =      1.124(CFS) for    0.380(Ac.)
Total runoff =      1.249(CFS)  Total area =        0.41(Ac.)
Street flow at end of street =      1.249(CFS)
Half street flow at end of street =      1.249(CFS)
Depth of flow =   0.137(Ft.), Average velocity =   2.080(Ft/s)
Flow width (from curb towards crown)=   7.843(Ft.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3011.000 to Point/Station     3009.000
**** SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                    ]
Time of concentration =    12.47 min.
Rainfall intensity =      3.114(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.950
Subarea runoff =      1.272(CFS) for    0.430(Ac.)
Total runoff =      2.521(CFS)  Total area =        0.84(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3009.000 to Point/Station     3010.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------
Upstream point/station elevation =   502.420(Ft.)
Downstream point/station elevation =   501.830(Ft.)
```

```
Pipe length  =    91.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     2.521(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     2.521(CFS)
Normal flow depth in pipe =    8.73(In.)
Flow top width inside pipe =   10.69(In.)
Critical Depth =    8.17(In.)
Pipe flow velocity =      4.12(Ft/s)
Travel time through pipe =    0.37 min.
Time of concentration (TC) =    12.84 min.
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3012.000 to Point/Station     3012.000
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                    ]
Time of concentration =    12.84 min.
Rainfall intensity =      3.080(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.950
Subarea runoff =      1.522(CFS) for    0.520(Ac.)
Total runoff =      4.043(CFS)  Total area =        1.36(Ac.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3013.000 to Point/Station     3010.000
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                    ]
Time of concentration =    12.84 min.
Rainfall intensity =      3.080(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.950
Subarea runoff =      1.317(CFS) for    0.450(Ac.)
Total runoff =      5.359(CFS)  Total area =        1.81(Ac.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3010.000 to Point/Station     3014.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________
Upstream point/station elevation =   501.830(Ft.)
Downstream point/station elevation =   500.360(Ft.)
Pipe length  =   233.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     5.359(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =     5.359(CFS)
Normal flow depth in pipe =   10.49(In.)
Flow top width inside pipe =   17.75(In.)
Critical Depth =   10.70(In.)
Pipe flow velocity =      5.01(Ft/s)
Travel time through pipe =    0.77 min.
Time of concentration (TC) =    13.62 min.
```



```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3016.000 to Point/Station     3014.000
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                    ]
Time of concentration =    13.62 min.
Rainfall intensity =      3.014(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.950
Subarea runoff =      0.859(CFS) for    0.300(Ac.)
Total runoff =      6.218(CFS)  Total area =        2.11(Ac.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3015.000 to Point/Station     3014.000
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                    ]
Time of concentration =    13.62 min.
Rainfall intensity =      3.014(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.950
Subarea runoff =      1.059(CFS) for    0.370(Ac.)
Total runoff =      7.278(CFS)  Total area =        2.48(Ac.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3014.000 to Point/Station     3020.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________
Upstream point/station elevation =   500.360(Ft.)
Downstream point/station elevation =   498.910(Ft.)
Pipe length  =   172.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     7.278(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =     7.278(CFS)
Normal flow depth in pipe =   11.68(In.)
Flow top width inside pipe =   17.18(In.)
Critical Depth =   12.53(In.)
Pipe flow velocity =      6.00(Ft/s)
Travel time through pipe =    0.48 min.
Time of concentration (TC) =    14.10 min.
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3019.000 to Point/Station     3020.000
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
```

```
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                    ]
Time of concentration =    14.10 min.
Rainfall intensity =      2.975(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.950
Subarea runoff =     15.544(CFS) for    5.500(Ac.)
Total runoff =     22.822(CFS)  Total area =        7.98(Ac.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3020.000 to Point/Station     3003.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------
Upstream point/station elevation =   498.910(Ft.)
Downstream point/station elevation =   494.250(Ft.)
Pipe length  =   675.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    22.822(CFS)
Nearest computed pipe diameter  =     27.00(In.)
Calculated individual pipe flow  =    22.822(CFS)
Normal flow depth in pipe =   19.78(In.)
Flow top width inside pipe =   23.90(In.)
Critical Depth =   20.06(In.)
Pipe flow velocity =      7.31(Ft/s)
Travel time through pipe =    1.54 min.
Time of concentration (TC) =    15.63 min.
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3003.000 to Point/Station     3003.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      7.980(Ac.)
Runoff from this stream =     22.822(CFS)
Time of concentration =   15.63 min.
Rainfall intensity =     2.859(In/Hr)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3000.000 to Point/Station     3001.000
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                    ]
Initial subarea flow distance  =   69.300(Ft.)
Highest elevation =  512.600(Ft.)
Lowest elevation =  512.100(Ft.)
Elevation difference =    0.500(Ft.)
Time of concentration calculated by the urban
areas overland flow method (App X-C) =     2.51 min.
TC = [1.8*(1.1-C)*distance(Ft.)^.5)/(% slope^(1/3)]
TC = [1.8*(1.1-0.9500)*(  69.300^.5)/(   0.722^(1/3)]=   2.51
Setting time of concentration to 5 minutes
Rainfall intensity (I) =      4.389(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.950
Subarea runoff =       0.500(CFS)
Total initial stream area =        0.120(Ac.)
```



```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3001.000 to Point/Station     3002.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
Top of street segment elevation =   512.100(Ft.)
End of street segment elevation =   511.100(Ft.)
Length of street segment  =   210.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  22.000(Ft.)
Distance from crown to crossfall grade break  =  20.500(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  22.500(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   1.500(Ft.)
Gutter hike from flowline =  0.125(In.)
 Manning's N in gutter =  0.0130
 Manning's N from gutter to grade break =  0.0130
 Manning's N from grade break to crown =  0.0130
Estimated mean flow rate at midpoint of street =      1.272(CFS)
Depth of flow =   0.163(Ft.), Average velocity =   1.560(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =   9.111(Ft.)
Flow velocity =   1.56(Ft/s)
Travel time =    2.24 min.     TC =    7.24  min.
 Adding area flow to street
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                    ]
Rainfall intensity =      3.797(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.950
Subarea runoff =      1.335(CFS) for    0.370(Ac.)
Total runoff =      1.835(CFS)  Total area =        0.49(Ac.)
Street flow at end of street =      1.835(CFS)
Half street flow at end of street =      1.835(CFS)
Depth of flow =   0.189(Ft.), Average velocity =   1.711(Ft/s)
Flow width (from curb towards crown)=  10.427(Ft.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3018.000 to Point/Station     3002.000
**** SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                    ]
Time of concentration =     7.24 min.
Rainfall intensity =      3.797(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.950
Subarea runoff =     21.535(CFS) for    5.970(Ac.)
Total runoff =     23.370(CFS)  Total area =        6.46(Ac.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3002.000 to Point/Station     3003.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------
Upstream point/station elevation =   496.430(Ft.)
Downstream point/station elevation =   494.500(Ft.)
Pipe length  =   327.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    23.370(CFS)
Nearest computed pipe diameter  =     27.00(In.)
Calculated individual pipe flow  =    23.370(CFS)
Normal flow depth in pipe =   21.70(In.)
Flow top width inside pipe =   21.44(In.)
Critical Depth =   20.31(In.)
Pipe flow velocity =      6.82(Ft/s)
Travel time through pipe =    0.80 min.
Time of concentration (TC) =     8.04 min.
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3017.000 to Point/Station     3003.000
**** SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                    ]
Time of concentration =     8.04 min.
Rainfall intensity =      3.652(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.950
Subarea runoff =     12.942(CFS) for    3.730(Ac.)
Total runoff =     36.313(CFS)  Total area =       10.19(Ac.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3005.000 to Point/Station     3003.000
**** SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                    ]
Time of concentration =     8.04 min.
Rainfall intensity =      3.652(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.950
Subarea runoff =     17.939(CFS) for    5.170(Ac.)
Total runoff =     54.251(CFS)  Total area =       15.36(Ac.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3004.000 to Point/Station     3003.000
**** SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                    ]
Time of concentration =     8.04 min.
```



```
Rainfall intensity =      3.652(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.950
Subarea runoff =     28.487(CFS) for    8.210(Ac.)
Total runoff =     82.739(CFS)  Total area =       23.57(Ac.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3003.000 to Point/Station     3003.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 2
Stream flow area =     23.570(Ac.)
Runoff from this stream =     82.739(CFS)
Time of concentration =    8.04 min.
Rainfall intensity =     3.652(In/Hr)
Summary of stream data:

Stream   Flow rate       TC             Rainfall Intensity
 No.       (CFS)        (min)                 (In/Hr)


1       22.822     15.63                 2.859
2       82.739      8.04                 3.652
Qmax(1) =
           1.000 *    1.000 *    22.822) +
           0.783 *    1.000 *    82.739) + =      87.576
Qmax(2) =
           1.000 *    0.514 *    22.822) +
           1.000 *    1.000 *    82.739) + =      94.479

Total of 2 streams to confluence:
Flow rates before confluence point:
      22.822      82.739
Maximum flow rates at confluence using above data:
       87.576       94.479
Area of streams before confluence:
       7.980       23.570
Results of confluence:
Total flow rate =     94.479(CFS)
Time of concentration =     8.043 min.
Effective stream area after confluence =     31.550(Ac.)
End of computations, total study area =          31.550 (Ac.)
```

5000

```
                San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2003 Version 6.3

Rational method hydrology  program based on
San Diego County Flood Control Division 1985 hydrology manual
        Rational Hydrology Study        Date: 07/30/24
--------------------------------------------------------------------------
4481 COLLECTION AT CACTUS
PROPOSED CONDITIONS
100-YEAR
FILE:S5000P100
--------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

--------------------------------------------------------------------------


Program License Serial Number 4049

--------------------------------------------------------------------------
Rational hydrology study storm event year is   100.0
English (in-lb) input data Units used
English (in) rainfall data used

Standard intensity of Appendix I-B used for year and
Elevation 0 - 1500 feet
Factor (to multiply * intensity)  =  1.000
Only used if inside City of San Diego
San Diego hydrology manual 'C' values used
Runoff coefficients by rational method


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     5000.000 to Point/Station     5001.000
**** INITIAL AREA EVALUATION ****
__________________________________________________________________________
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[RURAL(greater than 0.5 Ac, 0.2 ha) area type]
Initial subarea flow distance  =   90.000(Ft.)
Highest elevation =  509.300(Ft.)
Lowest elevation =  508.200(Ft.)
Elevation difference =    1.100(Ft.)
Time of concentration calculated by the urban
areas overland flow method (App X-C) =    10.38 min.
TC = [1.8*(1.1-C)*distance(Ft.)^.5)/(% slope^(1/3)]
TC = [1.8*(1.1-0.4500)*(  90.000^.5)/( 1.222^(1/3)]=  10.38
Rainfall intensity (I) =      3.329(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.450
Subarea runoff =      0.150(CFS)
Total initial stream area =        0.100(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     5001.000 to Point/Station     5002.000
**** SUBAREA FLOW ADDITION ****
__________________________________________________________________________
```



```
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[RURAL(greater than 0.5 Ac, 0.2 ha) area type]
Time of concentration =    10.38 min.
Rainfall intensity =      3.329(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.450
Subarea runoff =      5.273(CFS) for    3.520(Ac.)
Total runoff =      5.423(CFS)  Total area =        3.62(Ac.)
End of computations, total study area =          3.620 (Ac.)
```

6000
UNDETAINED

```
                San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2003 Version 6.3

Rational method hydrology  program based on
San Diego County Flood Control Division 1985 hydrology manual
        Rational Hydrology Study        Date: 11/20/24
------------------------------------------------------------------------
4481 COLLECTION AT CACTUS
PROPOSED CONDITIONS
100-YEAR
FILE:S6000P100
------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

------------------------------------------------------------------------


Program License Serial Number 4049

------------------------------------------------------------------------
Rational hydrology study storm event year is   100.0
English (in-lb) input data Units used
English (in) rainfall data used

Standard intensity of Appendix I-B used for year and
Elevation 0 - 1500 feet
Factor (to multiply * intensity)  =  1.000
Only used if inside City of San Diego
San Diego hydrology manual 'C' values used
Runoff coefficients by rational method


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     5002.000 to Point/Station     5002.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****
________________________________________________________________________
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[RURAL(greater than 0.5 Ac, 0.2 ha) area type]
Rainfall intensity (I) =      3.327(In/Hr) for a   100.0 year storm
User specified values are as follows:
TC =  10.40 min.  Rain intensity =       3.33(In/Hr)
Total area =        3.620(Ac.)  Total runoff =     5.400(CFS)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     6000.000 to Point/Station     6001.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =   496.490(Ft.)
Downstream point/station elevation =   494.480(Ft.)
Pipe length  =   337.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     5.400(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =     5.400(CFS)
Normal flow depth in pipe =   10.73(In.)
Flow top width inside pipe =   17.66(In.)
```



```
Critical Depth =   10.74(In.)
Pipe flow velocity =       4.91(Ft/s)
Travel time through pipe =    1.14 min.
Time of concentration (TC) =    11.54 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     6001.000 to Point/Station     6001.000
**** CONFLUENCE OF MINOR STREAMS ****
________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      3.620(Ac.)
Runoff from this stream =       5.400(CFS)
Time of concentration =   11.54 min.
Rainfall intensity =     3.203(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     7000.000 to Point/Station     7001.000
**** INITIAL AREA EVALUATION ****
________________________________________________________________________
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                       ]
Initial subarea flow distance  =   96.000(Ft.)
Highest elevation =  510.000(Ft.)
Lowest elevation =  508.500(Ft.)
Elevation difference =    1.500(Ft.)
Time of concentration calculated by the urban
areas overland flow method (App X-C) =     2.28 min.
TC = [1.8*(1.1-C)*distance(Ft.)^.5)/(% slope^(1/3)]
TC = [1.8*(1.1-0.9500)*(  96.000^.5)/(   1.563^(1/3)]=   2.28
Setting time of concentration to 5 minutes
Rainfall intensity (I) =      4.389(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.950
Subarea runoff =      0.625(CFS)
Total initial stream area =        0.150(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     7001.000 to Point/Station     7002.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
________________________________________________________________________
Top of street segment elevation =   508.500(Ft.)
End of street segment elevation =   502.900(Ft.)
Length of street segment  =   425.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  42.000(Ft.)
Distance from crown to crossfall grade break  =  40.500(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  12.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   1.500(Ft.)
Gutter hike from flowline =  0.125(In.)
 Manning's N in gutter =  0.0130
 Manning's N from gutter to grade break =  0.0130
```

```
 Manning's N from grade break to crown =  0.0130
Estimated mean flow rate at midpoint of street =      1.584(CFS)
Depth of flow =   0.144(Ft.), Average velocity =   2.411(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =   8.196(Ft.)
Flow velocity =   2.41(Ft/s)
Travel time =    2.94 min.     TC =    7.94  min.
 Adding area flow to street
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                    ]
Rainfall intensity =      3.670(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.950
Subarea runoff =      1.604(CFS) for    0.460(Ac.)
Total runoff =      2.229(CFS)  Total area =        0.61(Ac.)
Street flow at end of street =      2.229(CFS)
Half street flow at end of street =      2.229(CFS)
Depth of flow =   0.166(Ft.), Average velocity =   2.629(Ft/s)
Flow width (from curb towards crown)=   9.288(Ft.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     7002.000 to Point/Station     6001.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________
Upstream point/station elevation =   495.300(Ft.)
Downstream point/station elevation =   494.480(Ft.)
Pipe length  =   127.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     2.229(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     2.229(CFS)
Normal flow depth in pipe =    7.96(In.)
Flow top width inside pipe =   11.34(In.)
Critical Depth =    7.66(In.)
Pipe flow velocity =      4.03(Ft/s)
Travel time through pipe =    0.53 min.
Time of concentration (TC) =     8.46 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     6001.000 to Point/Station     6001.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      0.610(Ac.)
Runoff from this stream =      2.229(CFS)
Time of concentration =    8.46 min.
Rainfall intensity =     3.585(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                (In/Hr)


1        5.400     11.54                3.203
2        2.229      8.46                3.585
Qmax(1) =
          1.000 *    1.000 *     5.400) +
          0.894 *    1.000 *     2.229) + =       7.392
```



```
Qmax(2) =
          1.000 *    0.733 *     5.400) +
          1.000 *    1.000 *     2.229) + =       6.188

Total of 2 streams to confluence:
Flow rates before confluence point:
      5.400       2.229
Maximum flow rates at confluence using above data:
      7.392       6.188
Area of streams before confluence:
      3.620       0.610
Results of confluence:
Total flow rate =      7.392(CFS)
Time of concentration =    11.543 min.
Effective stream area after confluence =      4.230(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     6001.000 to Point/Station     6002.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________
Upstream point/station elevation =   493.480(Ft.)
Downstream point/station elevation =   491.380(Ft.)
Pipe length  =   322.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     7.392(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =     7.392(CFS)
Normal flow depth in pipe =   13.01(In.)
Flow top width inside pipe =   16.12(In.)
Critical Depth =   12.64(In.)
Pipe flow velocity =      5.41(Ft/s)
Travel time through pipe =    0.99 min.
Time of concentration (TC) =    12.54 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     6002.000 to Point/Station     6002.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      4.230(Ac.)
Runoff from this stream =      7.392(CFS)
Time of concentration =   12.54 min.
Rainfall intensity =     3.108(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     6004.000 to Point/Station     6005.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                    ]
Initial subarea flow distance  =   95.000(Ft.)
Highest elevation =  504.900(Ft.)
Lowest elevation =  503.600(Ft.)
Elevation difference =    1.300(Ft.)
Time of concentration calculated by the urban
```

```
areas overland flow method (App X-C) =     2.37 min.
TC = [1.8*(1.1-C)*distance(Ft.)^.5)/(% slope^(1/3)]
TC = [1.8*(1.1-0.9500)*(  95.000^.5)/(   1.368^(1/3)]=   2.37
Setting time of concentration to 5 minutes
Rainfall intensity (I) =      4.389(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.950
Subarea runoff =      0.125(CFS)
Total initial stream area =        0.030(Ac.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     6005.000 to Point/Station     6002.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
Top of street segment elevation =   503.600(Ft.)
End of street segment elevation =   495.500(Ft.)
Length of street segment  =   661.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  31.000(Ft.)
Distance from crown to crossfall grade break  =  29.500(Ft.)
Slope from gutter to grade break (v/hz) =   0.200
Slope from grade break to crown (v/hz)  =   0.200
Street flow is on [2] side(s) of the street
Distance from curb to property line  =  12.000(Ft.)
Slope from curb to property line (v/hz) =   0.200
Gutter width =   1.500(Ft.)
Gutter hike from flowline =  0.125(In.)
 Manning's N in gutter =  0.0130
 Manning's N from gutter to grade break =  0.0130
 Manning's N from grade break to crown =  0.0130
Estimated mean flow rate at midpoint of street =      0.200(CFS)
Depth of flow =   0.048(Ft.), Average velocity =   1.462(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =   1.690(Ft.)
Flow velocity =   1.46(Ft/s)
Travel time =    7.53 min.     TC =   12.53  min.
 Adding area flow to street
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                    ]
Rainfall intensity =      3.108(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.950
Subarea runoff =      3.543(CFS) for    1.200(Ac.)
Total runoff =      3.668(CFS)  Total area =        1.23(Ac.)
Street flow at end of street =      3.668(CFS)
Half street flow at end of street =      1.834(CFS)
Depth of flow =   0.239(Ft.), Average velocity =   3.815(Ft/s)
Flow width (from curb towards crown)=   2.642(Ft.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     6002.000 to Point/Station     6002.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      1.230(Ac.)
Runoff from this stream =      3.668(CFS)
Time of concentration =   12.53 min.
Rainfall intensity =     3.108(In/Hr)
```



```
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        7.392     12.54                  3.108
2        3.668     12.53                  3.108
Qmax(1) =
           1.000 *    1.000 *     7.392) +
           1.000 *    1.000 *     3.668) + =      11.060
Qmax(2) =
           1.000 *    1.000 *     7.392) +
           1.000 *    1.000 *     3.668) + =      11.060

Total of 2 streams to confluence:
Flow rates before confluence point:
       7.392       3.668
Maximum flow rates at confluence using above data:
       11.060       11.060
Area of streams before confluence:
        4.230        1.230
Results of confluence:
Total flow rate =     11.060(CFS)
Time of concentration =    12.535 min.
Effective stream area after confluence =      5.460(Ac.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     6002.000 to Point/Station      103.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------
Upstream point/station elevation =   491.380(Ft.)
Downstream point/station elevation =   489.190(Ft.)
Pipe length  =   357.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    11.060(CFS)
Nearest computed pipe diameter  =     21.00(In.)
Calculated individual pipe flow  =    11.060(CFS)
Normal flow depth in pipe =   15.45(In.)
Flow top width inside pipe =   18.52(In.)
Critical Depth =   14.88(In.)
Pipe flow velocity =      5.83(Ft/s)
Travel time through pipe =    1.02 min.
Time of concentration (TC) =    13.56 min.
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      103.000 to Point/Station      103.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      5.460(Ac.)
Runoff from this stream =     11.060(CFS)
Time of concentration =   13.56 min.
Rainfall intensity =     3.019(In/Hr)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3004.000 to Point/Station     3004.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****
```

```
------------------------------------------------------------------------
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                        ]
Note: user entry of impervious value, Ap = 0.950
Rainfall intensity (I) =      3.660(In/Hr) for a   100.0 year storm
User specified values are as follows:
TC =   8.00 min.  Rain intensity =       3.66(In/Hr)
Total area =       31.550(Ac.)  Total runoff =    94.480(CFS)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      103.000 to Point/Station      103.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 2
Stream flow area =     31.550(Ac.)
Runoff from this stream =     94.480(CFS)
Time of concentration =    8.00 min.
Rainfall intensity =     3.660(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      103.000 to Point/Station      103.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****
------------------------------------------------------------------------
User specified 'C' value of 0.550 given for subarea
Rainfall intensity (I) =      2.017(In/Hr) for a   100.0 year storm
User specified values are as follows:
TC =  32.13 min.  Rain intensity =       2.02(In/Hr)
Total area =       61.230(Ac.)  Total runoff =    73.370(CFS)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      103.000 to Point/Station      103.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 3
Stream flow area =     61.230(Ac.)
Runoff from this stream =     73.370(CFS)
Time of concentration =   32.13 min.
Rainfall intensity =     2.017(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       11.060     13.56                3.019
2       94.480      8.00                3.660
3       73.370     32.13                2.017
Qmax(1) =
           1.000 *    1.000 *    11.060) +
           0.825 *    1.000 *    94.480) +
           1.000 *    0.422 *    73.370) + =     119.954
Qmax(2) =
           1.000 *    0.590 *    11.060) +
           1.000 *    1.000 *    94.480) +
```



```
           1.000 *    0.249 *    73.370) + =     119.276
Qmax(3) =
           0.668 *    1.000 *    11.060) +
           0.551 *    1.000 *    94.480) +
           1.000 *    1.000 *    73.370) + =     132.830

Total of 3 streams to confluence:
Flow rates before confluence point:
      11.060      94.480      73.370
Maximum flow rates at confluence using above data:
      119.954     119.276     132.830
Area of streams before confluence:
       5.460      31.550      61.230
Results of confluence:
Total flow rate =    132.830(CFS)
Time of concentration =    32.130 min.
Effective stream area after confluence =     98.240(Ac.)
End of computations, total study area =          98.240 (Ac.)
```

6000 DETAINED

```
                San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2003 Version 6.3

Rational method hydrology  program based on
San Diego County Flood Control Division 1985 hydrology manual
        Rational Hydrology Study        Date: 11/20/24
--------------------------------------------------------------------------
4481 COLLECTION AT CACTUS
PROPOSED CONDITIONS-DETAINED
100-YEAR
FILE: S6000P100D
--------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

--------------------------------------------------------------------------


Program License Serial Number 4049

--------------------------------------------------------------------------
Rational hydrology study storm event year is   100.0
English (in-lb) input data Units used
English (in) rainfall data used

Standard intensity of Appendix I-B used for year and
Elevation 0 - 1500 feet
Factor (to multiply * intensity)  =  1.000
Only used if inside City of San Diego
San Diego hydrology manual 'C' values used
Runoff coefficients by rational method


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     5002.000 to Point/Station     5002.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****
________________________________________________________________________
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[RURAL(greater than 0.5 Ac, 0.2 ha) area type]
Rainfall intensity (I) =      2.875(In/Hr) for a   100.0 year storm
User specified values are as follows:
TC =  15.40 min.  Rain intensity =       2.88(In/Hr)
Total area =        3.620(Ac.)  Total runoff =     3.380(CFS)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     6000.000 to Point/Station     6001.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =   496.490(Ft.)
Downstream point/station elevation =   494.480(Ft.)
Pipe length  =   337.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     3.380(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =     3.380(CFS)
Normal flow depth in pipe =    9.05(In.)
Flow top width inside pipe =   14.68(In.)
```



```
Critical Depth =    8.89(In.)
Pipe flow velocity =       4.37(Ft/s)
Travel time through pipe =    1.29 min.
Time of concentration (TC) =    16.69 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     6001.000 to Point/Station     6001.000
**** CONFLUENCE OF MINOR STREAMS ****
________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      3.620(Ac.)
Runoff from this stream =       3.380(CFS)
Time of concentration =   16.69 min.
Rainfall intensity =     2.785(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     7000.000 to Point/Station     7001.000
**** INITIAL AREA EVALUATION ****
________________________________________________________________________
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                    ]
Initial subarea flow distance  =   96.000(Ft.)
Highest elevation =  510.000(Ft.)
Lowest elevation =  508.500(Ft.)
Elevation difference =    1.500(Ft.)
Time of concentration calculated by the urban
areas overland flow method (App X-C) =     2.28 min.
TC = [1.8*(1.1-C)*distance(Ft.)^.5)/(% slope^(1/3)]
TC = [1.8*(1.1-0.9500)*(  96.000^.5)/(   1.563^(1/3)]=   2.28
Setting time of concentration to 5 minutes
Rainfall intensity (I) =      4.389(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.950
Subarea runoff =      0.625(CFS)
Total initial stream area =        0.150(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     7001.000 to Point/Station     7002.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
________________________________________________________________________
Top of street segment elevation =   508.500(Ft.)
End of street segment elevation =   502.900(Ft.)
Length of street segment  =   425.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  42.000(Ft.)
Distance from crown to crossfall grade break  =  40.500(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  12.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   1.500(Ft.)
Gutter hike from flowline =  0.125(In.)
 Manning's N in gutter =  0.0130
 Manning's N from gutter to grade break =  0.0130
```

```
 Manning's N from grade break to crown =  0.0130
Estimated mean flow rate at midpoint of street =      1.584(CFS)
Depth of flow =   0.144(Ft.), Average velocity =   2.411(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =   8.196(Ft.)
Flow velocity =   2.41(Ft/s)
Travel time =    2.94 min.     TC =    7.94  min.
 Adding area flow to street
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                    ]
Rainfall intensity =      3.670(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.950
Subarea runoff =      1.604(CFS) for    0.460(Ac.)
Total runoff =      2.229(CFS)  Total area =        0.61(Ac.)
Street flow at end of street =      2.229(CFS)
Half street flow at end of street =      2.229(CFS)
Depth of flow =   0.166(Ft.), Average velocity =   2.629(Ft/s)
Flow width (from curb towards crown)=   9.288(Ft.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     7002.000 to Point/Station     6001.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________
Upstream point/station elevation =   495.300(Ft.)
Downstream point/station elevation =   494.480(Ft.)
Pipe length  =   127.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     2.229(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     2.229(CFS)
Normal flow depth in pipe =    7.96(In.)
Flow top width inside pipe =   11.34(In.)
Critical Depth =    7.66(In.)
Pipe flow velocity =      4.03(Ft/s)
Travel time through pipe =    0.53 min.
Time of concentration (TC) =     8.46 min.
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     6001.000 to Point/Station     6001.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      0.610(Ac.)
Runoff from this stream =      2.229(CFS)
Time of concentration =    8.46 min.
Rainfall intensity =     3.585(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        3.380     16.69                2.785
2        2.229      8.46                3.585
Qmax(1) =
          1.000 *    1.000 *     3.380) +
          0.777 *    1.000 *     2.229) + =       5.112
```



```
Qmax(2) =
          1.000 *    0.507 *     3.380) +
          1.000 *    1.000 *     2.229) + =       3.944

Total of 2 streams to confluence:
Flow rates before confluence point:
      3.380       2.229
Maximum flow rates at confluence using above data:
      5.112       3.944
Area of streams before confluence:
      3.620       0.610
Results of confluence:
Total flow rate =      5.112(CFS)
Time of concentration =    16.686 min.
Effective stream area after confluence =      4.230(Ac.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     6001.000 to Point/Station     6002.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________
Upstream point/station elevation =   493.480(Ft.)
Downstream point/station elevation =   491.380(Ft.)
Pipe length  =   322.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     5.112(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =     5.112(CFS)
Normal flow depth in pipe =   12.02(In.)
Flow top width inside pipe =   11.96(In.)
Critical Depth =   11.00(In.)
Pipe flow velocity =      4.85(Ft/s)
Travel time through pipe =    1.11 min.
Time of concentration (TC) =    17.79 min.
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     6002.000 to Point/Station     6002.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      4.230(Ac.)
Runoff from this stream =      5.112(CFS)
Time of concentration =   17.79 min.
Rainfall intensity =     2.713(In/Hr)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     6004.000 to Point/Station     6005.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                    ]
Initial subarea flow distance  =   95.000(Ft.)
Highest elevation =  504.900(Ft.)
Lowest elevation =  503.600(Ft.)
Elevation difference =    1.300(Ft.)
Time of concentration calculated by the urban
```

```
areas overland flow method (App X-C) =     2.37 min.
TC = [1.8*(1.1-C)*distance(Ft.)^.5)/(% slope^(1/3)]
TC = [1.8*(1.1-0.9500)*(  95.000^.5)/(   1.368^(1/3)]=   2.37
Setting time of concentration to 5 minutes
Rainfall intensity (I) =      4.389(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.950
Subarea runoff =      0.125(CFS)
Total initial stream area =        0.030(Ac.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     6005.000 to Point/Station     6002.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
Top of street segment elevation =   503.600(Ft.)
End of street segment elevation =   495.500(Ft.)
Length of street segment  =   661.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  31.000(Ft.)
Distance from crown to crossfall grade break  =  29.500(Ft.)
Slope from gutter to grade break (v/hz) =   0.200
Slope from grade break to crown (v/hz)  =   0.200
Street flow is on [2] side(s) of the street
Distance from curb to property line  =  12.000(Ft.)
Slope from curb to property line (v/hz) =   0.200
Gutter width =   1.500(Ft.)
Gutter hike from flowline =  0.125(In.)
 Manning's N in gutter =  0.0130
 Manning's N from gutter to grade break =  0.0130
 Manning's N from grade break to crown =  0.0130
Estimated mean flow rate at midpoint of street =      0.200(CFS)
Depth of flow =   0.048(Ft.), Average velocity =   1.462(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =   1.690(Ft.)
Flow velocity =   1.46(Ft/s)
Travel time =    7.53 min.     TC =   12.53  min.
 Adding area flow to street
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                    ]
Rainfall intensity =      3.108(In/Hr) for a   100.0 year storm
Runoff coefficient used for sub-area, Rational method,Q=KCIA, C = 0.950
Subarea runoff =      3.543(CFS) for    1.200(Ac.)
Total runoff =      3.668(CFS)  Total area =        1.23(Ac.)
Street flow at end of street =      3.668(CFS)
Half street flow at end of street =      1.834(CFS)
Depth of flow =   0.239(Ft.), Average velocity =   3.815(Ft/s)
Flow width (from curb towards crown)=   2.642(Ft.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     6002.000 to Point/Station     6002.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      1.230(Ac.)
Runoff from this stream =      3.668(CFS)
Time of concentration =   12.53 min.
Rainfall intensity =     3.108(In/Hr)
```



```
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1         5.112     17.79                  2.713
2         3.668     12.53                  3.108
Qmax(1) =
            1.000 *    1.000 *     5.112) +
            0.873 *    1.000 *     3.668) + =       8.314
Qmax(2) =
            1.000 *    0.704 *     5.112) +
            1.000 *    1.000 *     3.668) + =       7.270

Total of 2 streams to confluence:
Flow rates before confluence point:
       5.112       3.668
Maximum flow rates at confluence using above data:
        8.314       7.270
Area of streams before confluence:
        4.230       1.230
Results of confluence:
Total flow rate =      8.314(CFS)
Time of concentration =    17.794 min.
Effective stream area after confluence =      5.460(Ac.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     6002.000 to Point/Station      103.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------
Upstream point/station elevation =   491.380(Ft.)
Downstream point/station elevation =   489.190(Ft.)
Pipe length  =   357.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     8.314(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =     8.314(CFS)
Normal flow depth in pipe =   14.93(In.)
Flow top width inside pipe =   13.54(In.)
Critical Depth =   13.40(In.)
Pipe flow velocity =      5.31(Ft/s)
Travel time through pipe =    1.12 min.
Time of concentration (TC) =    18.92 min.
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      103.000 to Point/Station      103.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      5.460(Ac.)
Runoff from this stream =      8.314(CFS)
Time of concentration =   18.92 min.
Rainfall intensity =     2.644(In/Hr)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station     3004.000 to Point/Station     3004.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****
```

```
_____________________________________________________________________________
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[INDUSTRIAL area type                        ]
Note: user entry of impervious value, Ap = 0.950
Rainfall intensity (I) =      2.100(In/Hr) for a   100.0 year storm
User specified values are as follows:
TC =  30.00 min.  Rain intensity =       2.10(In/Hr)
Total area =       31.550(Ac.)  Total runoff =    13.020(CFS)



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      103.000 to Point/Station      103.000
**** CONFLUENCE OF MINOR STREAMS ****
_____________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =     31.550(Ac.)
Runoff from this stream =     13.020(CFS)
Time of concentration =   30.00 min.
Rainfall intensity =     2.100(In/Hr)



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      103.000 to Point/Station      103.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****
_____________________________________________________________________________
User specified 'C' value of 0.550 given for subarea
Rainfall intensity (I) =      2.017(In/Hr) for a   100.0 year storm
User specified values are as follows:
TC =  32.13 min.  Rain intensity =       2.02(In/Hr)
Total area =       61.230(Ac.)  Total runoff =    73.370(CFS)



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      103.000 to Point/Station      103.000
**** CONFLUENCE OF MINOR STREAMS ****
_____________________________________________________________________________
Along Main Stream number: 1 in normal stream number 3
Stream flow area =     61.230(Ac.)
Runoff from this stream =     73.370(CFS)
Time of concentration =   32.13 min.
Rainfall intensity =     2.017(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        8.314     18.92                2.644
2       13.020     30.00                2.100
3       73.370     32.13                2.017
Qmax(1) =
           1.000 *    1.000 *     8.314) +
           1.000 *    0.631 *    13.020) +
           1.000 *    0.589 *    73.370) + =      59.717
Qmax(2) =
           0.794 *    1.000 *     8.314) +
           1.000 *    1.000 *    13.020) +
```



```
           1.000 *    0.934 *    73.370) + =      88.131
Qmax(3) =
           0.763 *    1.000 *     8.314) +
           0.960 *    1.000 *    13.020) +
           1.000 *    1.000 *    73.370) + =      92.216

Total of 3 streams to confluence:
Flow rates before confluence point:
      8.314      13.020      73.370
Maximum flow rates at confluence using above data:
      59.717      88.131      92.216
Area of streams before confluence:
       5.460      31.550      61.230
Results of confluence:
Total flow rate =     92.216(CFS)
Time of concentration =    32.130 min.
Effective stream area after confluence =     98.240(Ac.)
End of computations, total study area =          98.240 (Ac.)
```

APPENDIX 4

Detention Basin Routing Analysis

DETENTION SUMMARY

P6 = 2.5"

PLACED IN TO RICK RAT HYDRO AND SYSTEM 6000 AS USER-DEFINED:

UNDETAINED

BMP-1

A	31.55
TC	8
Q	94.48
C	0.95

BMP-2

A	3.62
TC	10.4
Q	5.4
C	0.45

OUTPUT FROM POND PACK:

DETAINED

BMP-1

A	31.55
TC DIFF	22
TC	30
Q	13.02
C	0.95
Q DIFF	81.46 CFS

BMP-2

A	3.62
TC DIFF	5
TC	15.4
Q	3.38
C	0.45
Q DIFF	2.02 CFS

INFLOW HYDROGRAPHS

BMP-1 SYSTEM 3000

RATIONAL METHOD HYDROGRAPH PROGRAM

COPYRIGHT 1992, 2001 RICK ENGINEERING COMPANY

RUN DATE 10/21/2024

HYDROGRAPH FILE NAME Text1

TIME OF CONCENTRATION 8 MIN.

6 HOUR RAINFALL 2.5 INCHES

BASIN AREA 31.55 ACRES

RUNOFF COEFFICIENT 0.95

PEAK DISCHARGE 94.48 CFS

TIME	(MIN)	=	0	DISCHARGE	0
TIME	(MIN)	=	8	DISCHARGE	4.5
TIME	(MIN)	=	16	DISCHARGE	4.5
TIME	(MIN)	=	24	DISCHARGE	4.7
TIME	(MIN)	=	32	DISCHARGE	4.8
TIME	(MIN)	=	40	DISCHARGE	4.9
TIME	(MIN)	=	48	DISCHARGE	5
TIME	(MIN)	=	56	DISCHARGE	5.2
TIME	(MIN)	=	64	DISCHARGE	5.3
TIME	(MIN)	=	72	DISCHARGE	5.5
TIME	(MIN)	=	80	DISCHARGE	5.6
TIME	(MIN)	=	88	DISCHARGE	5.8
TIME	(MIN)	=	96	DISCHARGE	6
TIME	(MIN)	=	104	DISCHARGE	6.3
TIME	(MIN)	=	112	DISCHARGE	6.4
TIME	(MIN)	=	120	DISCHARGE	6.8
TIME	(MIN)	=	128	DISCHARGE	6.9
TIME	(MIN)	=	136	DISCHARGE	7.4
TIME	(MIN)	=	144	DISCHARGE	7.6
TIME	(MIN)	=	152	DISCHARGE	8.2
TIME	(MIN)	=	160	DISCHARGE	8.5
TIME	(MIN)	=	168	DISCHARGE	9.2
TIME	(MIN)	=	176	DISCHARGE	9.7
TIME	(MIN)	=	184	DISCHARGE	10.7
TIME	(MIN)	=	192	DISCHARGE	11.4
TIME	(MIN)	=	200	DISCHARGE	13
TIME	(MIN)	=	208	DISCHARGE	14.1
TIME	(MIN)	=	216	DISCHARGE	17.3
TIME	(MIN)	=	224	DISCHARGE	19.7
TIME	(MIN)	=	232	DISCHARGE	28.9
TIME	(MIN)	=	240	DISCHARGE	92
TIME	(MIN)	=	248	DISCHARGE	94.48
TIME	(MIN)	=	256	DISCHARGE	23.2
TIME	(MIN)	=	264	DISCHARGE	15.5
TIME	(MIN)	=	272	DISCHARGE	12.1
TIME	(MIN)	=	280	DISCHARGE	10.2
TIME	(MIN)	=	288	DISCHARGE	8.8
TIME	(MIN)	=	296	DISCHARGE	7.9
TIME	(MIN)	=	304	DISCHARGE	7.2
TIME	(MIN)	=	312	DISCHARGE	6.6
TIME	(MIN)	=	320	DISCHARGE	6.1
TIME	(MIN)	=	328	DISCHARGE	5.7
TIME	(MIN)	=	336	DISCHARGE	5.4
TIME	(MIN)	=	344	DISCHARGE	5.1
TIME	(MIN)	=	352	DISCHARGE	4.8
TIME	(MIN)	=	360	DISCHARGE	4.6
TIME	(MIN)	=	368	DISCHARGE	0

BMP-2

RATIONAL METHOD HYDROGRAPH PROGRAM
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RUN DATE 7/31/2024
HYDROGRAPH FILE NAME Text1
TIME OF CONCENTRATION 10 MIN.
6 HOUR RAINFALL 2.5 INCHES
BASIN AREA 3.62 ACRES
RUNOFF COEFFICIENT 0.95
PEAK DISCHARGE 5.4 CFS

TIME	(MIN)	=	0	DISCHARGE	0
TIME	(MIN)	=	10	DISCHARGE	0.2
TIME	(MIN)	=	20	DISCHARGE	0.2
TIME	(MIN)	=	30	DISCHARGE	0.3
TIME	(MIN)	=	40	DISCHARGE	0.3
TIME	(MIN)	=	50	DISCHARGE	0.3
TIME	(MIN)	=	60	DISCHARGE	0.3
TIME	(MIN)	=	70	DISCHARGE	0.3
TIME	(MIN)	=	80	DISCHARGE	0.3
TIME	(MIN)	=	90	DISCHARGE	0.3
TIME	(MIN)	=	100	DISCHARGE	0.3
TIME	(MIN)	=	110	DISCHARGE	0.3
TIME	(MIN)	=	120	DISCHARGE	0.4
TIME	(MIN)	=	130	DISCHARGE	0.4
TIME	(MIN)	=	140	DISCHARGE	0.4
TIME	(MIN)	=	150	DISCHARGE	0.4
TIME	(MIN)	=	160	DISCHARGE	0.5
TIME	(MIN)	=	170	DISCHARGE	0.5
TIME	(MIN)	=	180	DISCHARGE	0.5
TIME	(MIN)	=	190	DISCHARGE	0.6
TIME	(MIN)	=	200	DISCHARGE	0.7
TIME	(MIN)	=	210	DISCHARGE	0.8
TIME	(MIN)	=	220	DISCHARGE	0.9
TIME	(MIN)	=	230	DISCHARGE	1.4
TIME	(MIN)	=	240	DISCHARGE	3.4
TIME	(MIN)	=	250	DISCHARGE	5.4
TIME	(MIN)	=	260	DISCHARGE	1.1
TIME	(MIN)	=	270	DISCHARGE	0.7
TIME	(MIN)	=	280	DISCHARGE	0.6
TIME	(MIN)	=	290	DISCHARGE	0.5
TIME	(MIN)	=	300	DISCHARGE	0.4
TIME	(MIN)	=	310	DISCHARGE	0.4
TIME	(MIN)	=	320	DISCHARGE	0.3
TIME	(MIN)	=	330	DISCHARGE	0.3
TIME	(MIN)	=	340	DISCHARGE	0.3
TIME	(MIN)	=	350	DISCHARGE	0.3
TIME	(MIN)	=	360	DISCHARGE	0.3
TIME	(MIN)	=	370	DISCHARGE	0

BENTLEY POND PACK PROGRAM OUTPUT

BMP-1

BMP-1

Project Summary	
Title	System 3000-BMP -1
Engineer	PDC
Company	PDC
Date	11/25/2024

Notes

Bentley Systems, Inc. Haestad Methods Solution Center
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Table of Contents

	Master Network Summary	2
CM-1	Read Hydrograph	3
1	Elevation-Area Volume Curve	4
Outlet#1	Outlet Input Data	5
1		
	Elevation-Volume-Flow Table (Pond)	8
1 (IN)		
	Level Pool Pond Routing Summary	10
	Pond Inflow Summary	11

BMP-1

Subsection: Master Network Summary

Catchments Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (min)	Peak Flow (ft³/s)
CM-1	EX10	0	6.210	248.000	94.48

Node Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (min)	Peak Flow (ft³/s)
O-1	EX10	0	4.758	270.000	13.02

Pond Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (min)	Peak Flow (ft³/s)	Maximum Water Surface Elevation (ft)	Maximum Pond Storage (ac-ft)
1 (IN)	EX10	0	6.210	248.000	94.48	(N/A)	(N/A)
1 (OUT)	EX10	0	4.758	270.000	13.02	498.89	5.254

BMP-1

Subsection: Read Hydrograph
Label: CM-1
Scenario: EX10

Return Event: 100 years
Storm Event:

Peak Discharge	94.48 ft³/s
Time to Peak	248.000 min
Hydrograph Volume	6.210 ac-ft

HYDROGRAPH ORDINATES (ft³/s)
Output Time Increment = 8.000 min
Time on left represents time for first value in each row.

Time (min)	Flow (ft³/s)	Flow (ft³/s)	Flow (ft³/s)	Flow (ft³/s)	Flow (ft³/s)
0.000	0.00	4.50	4.50	4.70	4.80
40.000	4.90	5.00	5.20	5.30	5.50
80.000	5.60	5.80	6.00	6.30	6.40
120.000	6.80	6.90	7.40	7.60	8.20
160.000	8.50	9.20	9.70	10.70	11.40
200.000	13.00	14.10	17.30	19.70	28.90
240.000	92.00	94.48	23.20	15.50	12.10
280.000	10.20	8.80	7.90	7.20	6.60
320.000	6.10	5.70	5.40	5.10	4.80
360.000	4.60	0.00	(N/A)	(N/A)	(N/A)

BMP-1

Subsection: Elevation-Area Volume Curve
Label: 1
Scenario: EX10

Return Event: 100 years
Storm Event:

Elevation (ft)	Planimeter (ft²)	Area (ft²)	A1+A2+sqr (A1*A2) (ft²)	Volume (ac-ft)	Volume (Total) (ac-ft)
494.00	0.0	38,925.000	0.000	0.000	0.000
495.00	0.0	42,075.000	121,469.363	0.930	0.930
496.00	0.0	45,298.000	131,029.768	1.003	1.932
497.00	0.0	48,584.000	140,794.238	1.077	3.010
498.00	0.0	51,935.000	150,750.564	1.154	4.163
499.00	0.0	55,351.000	160,901.802	1.231	5.394
500.00	0.0	58,829.000	171,243.508	1.310	6.705

BMP-1

Subsection: Outlet Input Data
Label: Outlet#1
Scenario: EX10

Return Event: 100 years
Storm Event:

Requested Pond Water Surface Elevations	
Minimum (Headwater)	494.00 ft
Increment (Headwater)	0.10 ft
Maximum (Headwater)	500.00 ft

Outlet Connectivity

Structure Type	Outlet ID	Direction	Outfall	E1 (ft)	E2 (ft)
Orifice-Circular	1	Forward	TW	496.25	500.00
Orifice-Circular	2	Forward	TW	497.42	500.00
Inlet Box	Riser - 1	Forward	TW	499.00	500.00
Orifice-Circular	WQ	Forward	TW	494.75	500.00
Tailwater Settings	Tailwater			(N/A)	(N/A)

BMP-1

Subsection: Outlet Input Data
Label: Outlet#1
Scenario: EX10

Return Event: 100 years
Storm Event:

Structure ID: Riser - 1 Structure Type: Inlet Box	
Number of Openings	1
Elevation	499.00 ft
Orifice Area	4.7 ft²
Orifice Coefficient	0.600
Weir Length	9.20 ft
Weir Coefficient	3.00 (ft^0.5)/s
K Reverse	1.000
Manning's n	0.000
Kev, Charged Riser	0.000
Weir Submergence	False
Orifice H to crest	True

Structure ID: 1 Structure Type: Orifice-Circular	
Number of Openings	10
Elevation	496.25 ft
Orifice Diameter	5.0 in
Orifice Coefficient	0.600

Structure ID: 2 Structure Type: Orifice-Circular	
Number of Openings	10
Elevation	497.42 ft
Orifice Diameter	3.0 in
Orifice Coefficient	0.600

Structure ID: WQ Structure Type: Orifice-Circular	
Number of Openings	1
Elevation	494.75 ft
Orifice Diameter	1.0 in
Orifice Coefficient	0.600

Structure ID: TW Structure Type: TW Setup, DS Channel	
Tailwater Type	Free Outfall

Convergence Tolerances	
Maximum Iterations	30

BMP-1

Subsection: Outlet Input Data
Label: Outlet#1
Scenario: EX10

Return Event: 100 years
Storm Event:

Convergence Tolerances	
Tailwater Tolerance (Minimum)	0.01 ft
Tailwater Tolerance (Maximum)	0.50 ft
Headwater Tolerance (Minimum)	0.01 ft
Headwater Tolerance (Maximum)	0.50 ft
Flow Tolerance (Minimum)	0.001 ft³/s
Flow Tolerance (Maximum)	10.000 ft³/s

BMP-1

Subsection: Elevation-Volume-Flow Table (Pond)
Label: 1
Scenario: EX10

Return Event: 100 years
Storm Event:

Infiltration	
Infiltration Method (Computed)	No Infiltration

Initial Conditions	
Elevation (Water Surface, Initial)	494.75 ft
Volume (Initial)	0.690 ac-ft
Flow (Initial Outlet)	0.00 ft³/s
Flow (Initial Infiltration)	0.00 ft³/s
Flow (Initial, Total)	0.00 ft³/s
Time Increment	1.000 min

Elevation (ft)	Outflow (ft³/s)	Storage (ac-ft)	Area (ft²)	Infiltration (ft³/s)	Flow (Total) (ft³/s)	2S/t + O (ft³/s)
494.00	0.00	0.000	38,925.000	0.00	0.00	0.00
494.10	0.00	0.090	39,234.485	0.00	0.00	130.27
494.20	0.00	0.180	39,545.196	0.00	0.00	261.56
494.30	0.00	0.271	39,857.133	0.00	0.00	393.90
494.40	0.00	0.363	40,170.294	0.00	0.00	527.28
494.50	0.00	0.456	40,484.682	0.00	0.00	661.70
494.60	0.00	0.549	40,800.294	0.00	0.00	797.18
494.70	0.00	0.643	41,117.133	0.00	0.00	933.71
494.75	0.00	0.690	41,276.011	0.00	0.00	1,002.37
494.80	0.00	0.738	41,435.196	0.00	0.00	1,071.30
494.90	0.01	0.833	41,754.485	0.00	0.01	1,209.95
495.00	0.01	0.930	42,075.000	0.00	0.01	1,349.67
495.10	0.01	1.026	42,391.948	0.00	0.01	1,490.45
495.20	0.02	1.124	42,710.086	0.00	0.02	1,632.29
495.30	0.02	1.223	43,029.412	0.00	0.02	1,775.19
495.40	0.02	1.322	43,349.928	0.00	0.02	1,919.16
495.50	0.02	1.422	43,671.634	0.00	0.02	2,064.20
495.60	0.02	1.522	43,994.528	0.00	0.02	2,210.31
495.70	0.03	1.624	44,318.612	0.00	0.03	2,357.50
495.80	0.03	1.726	44,643.886	0.00	0.03	2,505.77
495.90	0.03	1.829	44,970.348	0.00	0.03	2,655.13
496.00	0.03	1.932	45,298.000	0.00	0.03	2,805.57
496.10	0.03	2.037	45,621.423	0.00	0.03	2,957.11
496.20	0.03	2.142	45,945.996	0.00	0.03	3,109.72
496.25	0.03	2.194	46,108.714	0.00	0.03	3,186.43
496.30	0.08	2.248	46,271.720	0.00	0.08	3,263.47
496.40	0.49	2.354	46,598.594	0.00	0.49	3,418.66
496.50	1.23	2.461	46,926.619	0.00	1.23	3,575.27
496.60	2.21	2.570	47,255.794	0.00	2.21	3,733.23

BMP-1

Subsection: Elevation-Volume-Flow Table (Pond) Return Event: 100 years
Label: 1 Storm Event:
Scenario: EX10

Elevation (ft)	Outflow (ft³/s)	Storage (ac-ft)	Area (ft²)	Infiltration (ft³/s)	Flow (Total) (ft³/s)	2S/t + O (ft³/s)
496.70	3.26	2.678	47,586.120	0.00	3.26	3,892.35
496.80	3.87	2.788	47,917.596	0.00	3.87	4,052.13
496.90	4.40	2.898	48,250.223	0.00	4.40	4,212.94
497.00	4.87	3.010	48,584.000	0.00	4.87	4,374.80
497.10	5.30	3.122	48,914.072	0.00	5.30	4,537.72
497.20	5.69	3.234	49,245.261	0.00	5.69	4,701.71
497.30	6.06	3.348	49,577.567	0.00	6.06	4,866.79
497.40	6.41	3.462	49,910.991	0.00	6.41	5,032.95
497.42	6.48	3.485	49,977.810	0.00	6.48	5,066.31
497.50	6.85	3.577	50,245.532	0.00	6.85	5,200.31
497.60	7.52	3.693	50,581.191	0.00	7.52	5,369.03
497.70	8.29	3.809	50,917.967	0.00	8.29	5,538.96
497.80	8.84	3.926	51,255.861	0.00	8.84	5,709.81
497.90	9.33	4.044	51,594.872	0.00	9.33	5,881.72
498.00	9.79	4.163	51,935.000	0.00	9.79	6,054.72
498.10	10.22	4.283	52,271.704	0.00	10.22	6,228.83
498.20	10.62	4.403	52,609.497	0.00	10.62	6,404.03
498.30	11.01	4.524	52,948.377	0.00	11.01	6,580.35
498.40	11.38	4.646	53,288.345	0.00	11.38	6,757.78
498.50	11.74	4.769	53,629.401	0.00	11.74	6,936.33
498.60	12.08	4.893	53,971.545	0.00	12.08	7,116.01
498.70	12.42	5.017	54,314.777	0.00	12.42	7,296.83
498.80	12.74	5.142	54,659.097	0.00	12.74	7,478.77
498.90	13.06	5.268	55,004.504	0.00	13.06	7,661.86
499.00	13.37	5.394	55,351.000	0.00	13.37	7,846.10
499.10	14.54	5.522	55,694.031	0.00	14.54	8,032.35
499.20	16.43	5.650	56,038.123	0.00	16.43	8,220.45
499.30	18.78	5.779	56,383.273	0.00	18.78	8,410.18
499.40	21.51	5.909	56,729.484	0.00	21.51	8,601.43
499.50	24.56	6.040	57,076.754	0.00	24.56	8,794.16
499.60	27.90	6.171	57,425.084	0.00	27.90	8,988.33
499.70	31.51	6.303	57,774.473	0.00	31.51	9,183.93
499.80	35.35	6.436	58,124.923	0.00	35.35	9,380.94
499.90	37.32	6.570	58,476.431	0.00	37.32	9,577.25
500.00	38.73	6.705	58,829.000	0.00	38.73	9,774.17

BMP-1

Subsection: Level Pool Pond Routing Summary
Label: 1 (IN)
Scenario: EX10

Return Event: 100 years
Storm Event:

Infiltration	
Infiltration Method (Computed)	No Infiltration

Initial Conditions	
Elevation (Water Surface, Initial)	494.75 ft
Volume (Initial)	0.690 ac-ft
Flow (Initial Outlet)	0.00 ft³/s
Flow (Initial Infiltration)	0.00 ft³/s
Flow (Initial, Total)	0.00 ft³/s
Time Increment	1.000 min

Inflow/Outflow Hydrograph Summary			
Flow (Peak In)	94.48 ft³/s	Time to Peak (Flow, In)	248.000 min
Flow (Peak Outlet)	13.02 ft³/s	Time to Peak (Flow, Outlet)	270.000 min

Elevation (Water Surface, Peak)	498.89 ft
Volume (Peak)	5.254 ac-ft

Mass Balance (ac-ft)	
Volume (Initial)	0.690 ac-ft
Volume (Total Inflow)	6.210 ac-ft
Volume (Total Infiltration)	0.000 ac-ft
Volume (Total Outlet Outflow)	4.758 ac-ft
Volume (Retained)	2.142 ac-ft
Volume (Unrouted)	0.000 ac-ft
Error (Mass Balance)	0.0 %

BMP-1

Subsection: Pond Inflow Summary
Label: 1 (IN)
Scenario: EX10

Return Event: 100 years
Storm Event:

Summary for Hydrograph Addition at '1'

Upstream Link	Upstream Node
<Catchment to Outflow Node>	CM-1

Node Inflows

Inflow Type	Element	Volume (ac-ft)	Time to Peak (min)	Flow (Peak) (ft^3/s)
Flow (From)	CM-1	6.210	248.000	94.48
Flow (In)	1	6.210	248.000	94.48

BMP-1

Index

1

1 (Elevation-Area Volume Curve)...

1 (Elevation-Area Volume Curve, 100 years (EX10))...4

1 (Elevation-Volume-Flow Table (Pond))...

1 (Elevation-Volume-Flow Table (Pond), 100 years (EX10))...8, 9

1 (IN) (Level Pool Pond Routing Summary)...

1 (IN) (Level Pool Pond Routing Summary, 100 years (EX10))...10

1 (IN) (Pond Inflow Summary)...

1 (IN) (Pond Inflow Summary, 100 years (EX10))...11

C

CM-1 (Read Hydrograph)...

CM-1 (Read Hydrograph, 100 years (EX10))...3

M

Master Network Summary...2

O

Outlet#1 (Outlet Input Data)...

Outlet#1 (Outlet Input Data, 100 years (EX10))...5, 6, 7

BMP-2

BMP-2

Project Summary	
Title	System 5000-BMP -2
Engineer	PDC
Company	PDC
Date	11/25/2024

Notes

Bentley Systems, Inc. Haestad Methods Solution Center
27 Siemon Company Drive Suite 200 W
Watertown, CT 06795 USA +1-203-755-1666

Table of Contents

	Master Network Summary	2
CM-1	Read Hydrograph	3
1	Elevation-Area Volume Curve	4
Outlet#1	Outlet Input Data	5
1		
	Elevation-Volume-Flow Table (Pond)	8
1 (IN)		
	Level Pool Pond Routing Summary	10
	Pond Inflow Summary	11

BMP-2

Subsection: Master Network Summary

Catchments Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (min)	Peak Flow (ft³/s)
CM-1	EX10	0	0.339	250.000	5.40

Node Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (min)	Peak Flow (ft³/s)
O-1	EX10	0	0.338	255.000	3.38

Pond Summary

Label	Scenario	Return Event (years)	Hydrograph Volume (ac-ft)	Time to Peak (min)	Peak Flow (ft³/s)	Maximum Water Surface Elevation (ft)	Maximum Pond Storage (ac-ft)
1 (IN)	EX10	0	0.339	250.000	5.40	(N/A)	(N/A)
1 (OUT)	EX10	0	0.338	255.000	3.38	501.93	0.116

BMP-2

Subsection: Read Hydrograph
Label: CM-1
Scenario: EX10

Return Event: 100 years
Storm Event:

Peak Discharge	5.40 ft³/s
Time to Peak	250.000 min
Hydrograph Volume	0.339 ac-ft

HYDROGRAPH ORDINATES (ft³/s)
Output Time Increment = 10.000 min
Time on left represents time for first value in each row.

Time (min)	Flow (ft³/s)	Flow (ft³/s)	Flow (ft³/s)	Flow (ft³/s)	Flow (ft³/s)
0.000	0.00	0.20	0.20	0.30	0.30
50.000	0.30	0.30	0.30	0.30	0.30
100.000	0.30	0.30	0.40	0.40	0.40
150.000	0.40	0.50	0.50	0.50	0.60
200.000	0.70	0.80	0.90	1.40	3.40
250.000	5.40	1.10	0.70	0.60	0.50
300.000	0.40	0.40	0.30	0.30	0.30
350.000	0.30	0.30	0.00	(N/A)	(N/A)

BMP-2

Subsection: Elevation-Area Volume Curve
Label: 1
Scenario: EX10

Return Event: 100 years
Storm Event:

Elevation (ft)	Planimeter (ft²)	Area (ft²)	A1+A2+sqr (A1*A2) (ft²)	Volume (ac-ft)	Volume (Total) (ac-ft)
500.00	0.0	2,048.470	0.000	0.000	0.000
501.00	0.0	2,627.590	6,996.090	0.054	0.054
502.00	0.0	3,278.710	8,841.450	0.068	0.121
503.00	0.0	4,001.830	10,902.810	0.083	0.205
504.00	0.0	4,796.950	13,180.170	0.101	0.305

BMP-2

Subsection: Outlet Input Data
Label: Outlet#1
Scenario: EX10

Return Event: 100 years
Storm Event:

Requested Pond Water Surface Elevations	
Minimum (Headwater)	500.00 ft
Increment (Headwater)	0.10 ft
Maximum (Headwater)	504.00 ft

Outlet Connectivity

Structure Type	Outlet ID	Direction	Outfall	E1 (ft)	E2 (ft)
Orifice-Circular	ORIFICE	Forward	TW	501.00	504.00
Inlet Box	Riser - 1	Forward	TW	502.50	504.00
Orifice-Circular	WQ	Forward	TW	500.75	504.00
Tailwater Settings	Tailwater			(N/A)	(N/A)

BMP-2

Subsection: Outlet Input Data
Label: Outlet#1
Scenario: EX10

Return Event: 100 years
Storm Event:

Structure ID: Riser - 1 Structure Type: Inlet Box	
Number of Openings	1
Elevation	502.50 ft
Orifice Area	4.7 ft²
Orifice Coefficient	0.600
Weir Length	9.20 ft
Weir Coefficient	3.00 (ft^0.5)/s
K Reverse	1.000
Manning's n	0.000
Kev, Charged Riser	0.000
Weir Submergence	False
Orifice H to crest	True

Structure ID: ORIFICE Structure Type: Orifice-Circular	
Number of Openings	6
Elevation	501.00 ft
Orifice Diameter	5.0 in
Orifice Coefficient	0.600

Structure ID: WQ Structure Type: Orifice-Circular	
Number of Openings	1
Elevation	500.75 ft
Orifice Diameter	1.0 in
Orifice Coefficient	0.600

Structure ID: TW Structure Type: TW Setup, DS Channel	
Tailwater Type	Free Outfall

Convergence Tolerances	
Maximum Iterations	30
Tailwater Tolerance (Minimum)	0.01 ft
Tailwater Tolerance (Maximum)	0.50 ft
Headwater Tolerance (Minimum)	0.01 ft
Headwater Tolerance (Maximum)	0.50 ft
Flow Tolerance (Minimum)	0.001 ft³/s

BMP-2

Subsection: Outlet Input Data
Label: Outlet#1
Scenario: EX10

Return Event: 100 years
Storm Event:

Convergence Tolerances	
Flow Tolerance (Maximum)	10.000 ft³/s

BMP-2

Subsection: Elevation-Volume-Flow Table (Pond)
Label: 1
Scenario: EX10

Return Event: 100 years
Storm Event:

Infiltration	
Infiltration Method (Computed)	No Infiltration

Initial Conditions	
Elevation (Water Surface, Initial)	500.75 ft
Volume (Initial)	0.039 ac-ft
Flow (Initial Outlet)	0.00 ft³/s
Flow (Initial Infiltration)	0.00 ft³/s
Flow (Initial, Total)	0.00 ft³/s
Time Increment	1.000 min

Elevation (ft)	Outflow (ft³/s)	Storage (ac-ft)	Area (ft²)	Infiltration (ft³/s)	Flow (Total) (ft³/s)	2S/t + O (ft³/s)
500.00	0.00	0.000	2,048.470	0.00	0.00	0.00
500.10	0.00	0.005	2,103.142	0.00	0.00	6.92
500.20	0.00	0.010	2,158.534	0.00	0.00	14.02
500.30	0.00	0.015	2,214.646	0.00	0.00	21.31
500.40	0.00	0.020	2,271.478	0.00	0.00	28.79
500.50	0.00	0.025	2,329.030	0.00	0.00	36.45
500.60	0.00	0.031	2,387.302	0.00	0.00	44.31
500.70	0.00	0.036	2,446.294	0.00	0.00	52.37
500.75	0.00	0.039	2,476.060	0.00	0.00	56.47
500.80	0.00	0.042	2,506.006	0.00	0.00	60.63
500.90	0.01	0.048	2,566.438	0.00	0.01	69.09
501.00	0.01	0.054	2,627.590	0.00	0.01	77.75
501.10	0.14	0.060	2,689.462	0.00	0.14	86.74
501.20	0.49	0.066	2,752.054	0.00	0.49	96.16
501.30	1.02	0.072	2,815.366	0.00	1.02	105.96
501.40	1.65	0.079	2,879.398	0.00	1.65	116.08
501.50	2.15	0.085	2,944.150	0.00	2.15	126.29
501.60	2.49	0.092	3,009.622	0.00	2.49	136.55
501.70	2.79	0.099	3,075.814	0.00	2.79	146.99
501.80	3.06	0.106	3,142.726	0.00	3.06	157.62
501.90	3.30	0.114	3,210.358	0.00	3.30	168.46
502.00	3.53	0.121	3,278.710	0.00	3.53	179.51
502.10	3.75	0.129	3,347.782	0.00	3.75	190.76
502.20	3.95	0.137	3,417.574	0.00	3.95	202.24
502.30	4.15	0.144	3,488.086	0.00	4.15	213.95
502.40	4.33	0.153	3,559.318	0.00	4.33	225.88
502.50	4.51	0.161	3,631.270	0.00	4.51	238.04
502.60	5.55	0.169	3,703.942	0.00	5.55	251.31
502.70	7.31	0.178	3,777.334	0.00	7.31	265.54

BMP-2

Subsection: Elevation-Volume-Flow Table (Pond) Return Event: 100 years
Label: 1 Storm Event:
Scenario: EX10

Elevation (ft)	Outflow (ft³/s)	Storage (ac-ft)	Area (ft²)	Infiltration (ft³/s)	Flow (Total) (ft³/s)	2S/t + O (ft³/s)
502.80	9.54	0.187	3,851.446	0.00	9.54	280.48
502.90	12.14	0.196	3,926.278	0.00	12.14	296.04
503.00	15.07	0.205	4,001.830	0.00	15.07	312.18
503.10	18.28	0.214	4,078.102	0.00	18.28	328.86
503.20	21.76	0.223	4,155.094	0.00	21.76	346.07
503.30	25.49	0.233	4,232.806	0.00	25.49	363.77
503.40	27.33	0.243	4,311.238	0.00	27.33	379.85
503.50	28.63	0.253	4,390.390	0.00	28.63	395.65
503.60	29.86	0.263	4,470.262	0.00	29.86	411.65
503.70	31.04	0.273	4,550.854	0.00	31.04	427.87
503.80	32.18	0.284	4,632.166	0.00	32.18	444.31
503.90	33.27	0.295	4,714.198	0.00	33.27	460.98
504.00	34.33	0.305	4,796.950	0.00	34.33	477.89

BMP-2

Subsection: Level Pool Pond Routing Summary
Label: 1 (IN)
Scenario: EX10

Return Event: 100 years
Storm Event:

Infiltration	
Infiltration Method (Computed)	No Infiltration

Initial Conditions	
Elevation (Water Surface, Initial)	500.75 ft
Volume (Initial)	0.039 ac-ft
Flow (Initial Outlet)	0.00 ft³/s
Flow (Initial Infiltration)	0.00 ft³/s
Flow (Initial, Total)	0.00 ft³/s
Time Increment	1.000 min

Inflow/Outflow Hydrograph Summary			
Flow (Peak In)	5.40 ft³/s	Time to Peak (Flow, In)	250.000 min
Flow (Peak Outlet)	3.38 ft³/s	Time to Peak (Flow, Outlet)	255.000 min

Elevation (Water Surface, Peak)	501.93 ft
Volume (Peak)	0.116 ac-ft

Mass Balance (ac-ft)	
Volume (Initial)	0.039 ac-ft
Volume (Total Inflow)	0.339 ac-ft
Volume (Total Infiltration)	0.000 ac-ft
Volume (Total Outlet Outflow)	0.338 ac-ft
Volume (Retained)	0.040 ac-ft
Volume (Unrouted)	0.000 ac-ft
Error (Mass Balance)	0.0 %

BMP-2

Subsection: Pond Inflow Summary
Label: 1 (IN)
Scenario: EX10

Return Event: 100 years
Storm Event:

Summary for Hydrograph Addition at '1'

Upstream Link	Upstream Node
<Catchment to Outflow Node>	CM-1

Node Inflows

Inflow Type	Element	Volume (ac-ft)	Time to Peak (min)	Flow (Peak) (ft^3/s)
Flow (From)	CM-1	0.339	250.000	5.40
Flow (In)	1	0.339	250.000	5.40

BMP-2

Index

1

1 (Elevation-Area Volume Curve)...

1 (Elevation-Area Volume Curve, 100 years (EX10))...4

1 (Elevation-Volume-Flow Table (Pond))...

1 (Elevation-Volume-Flow Table (Pond), 100 years (EX10))...8, 9

1 (IN) (Level Pool Pond Routing Summary)...

1 (IN) (Level Pool Pond Routing Summary, 100 years (EX10))...10

1 (IN) (Pond Inflow Summary)...

1 (IN) (Pond Inflow Summary, 100 years (EX10))...11

C

CM-1 (Read Hydrograph)...

CM-1 (Read Hydrograph, 100 years (EX10))...3

M

Master Network Summary...2

O

Outlet#1 (Outlet Input Data)...

Outlet#1 (Outlet Input Data, 100 years (EX10))...5, 6, 7

APPENDIX 5

Hydraulic Calculations

STATE ROUTE 905

OTAY MESA HWY

APPROX. LIMITS BASED ON MANNING'S NORMAL DEPTH CALCULATIONS AT CROSS SECTION

APPROX. LIMITS BASED ON MANNING'S NORMAL DEPTH CALCULATIONS AT CROSS SECTION

UPSTREAM

DOWNSTREAM

EXISTING 48" STORM DRAIN

CACTUS ROAD

CACTUS

NODE 103

BMP-3

BASIN

PA-11

BLDG 1

BLDG 2

N

LEGEND

SECTIONS

FLOW DIRECTION

DRAINAGE FLOWPATH

NOTE:

SEE PROPOSED DRAINAGE EXHIBIT FOR HYDROLOGY INFORMATION.

SCALE:	1"=30'
JOB #:	4481
CREATED:	8/5/24

PREPARED BY:

PROJECT DESIGN CONSULTANTS
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CITY OF SAN DIEGO

COLLECTION AT CACTUS

CROSS SECTIONS

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Worksheet for NODE 103-103 DOWNSTREAM DRAINAGE DITCH

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth

Input Data	
Channel Slope	0.020 ft/ft
Discharge	73.44 cfs

Section Definitions

Station (ft)	Elevation (ft)
0+00	494.31
0+20	495.87
0+33	495.87
0+35	495.69
0+42	493.73
0+46	492.00
0+48	491.00
0+51	491.00
0+55	492.91
0+59	494.00
0+85	495.00
0+95	500.00

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 494.31)	(0+95, 500.00)	0.045

Options	
Current Roughness Weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

Results	
Normal Depth	23.7 in
Roughness Coefficient	0.045
Elevation	492.97 ft
Elevation Range	491.0 to 500.0 ft
Flow Area	14.3 ft²
Wetted Perimeter	12.4 ft
Hydraulic Radius	13.8 in
Top Width	11.48 ft
Normal Depth	23.7 in

FLOW DEPTH AT SECTION

Worksheet for NODE 103-103 DOWNSTREAM DRAINAGE DITCH

Results	
Critical Depth	21.2 in
Critical Slope	0.031 ft/ft
Velocity	5.13 ft/s
Velocity Head	0.41 ft
Specific Energy	2.38 ft
Froude Number	0.811
Flow Type	Subcritical

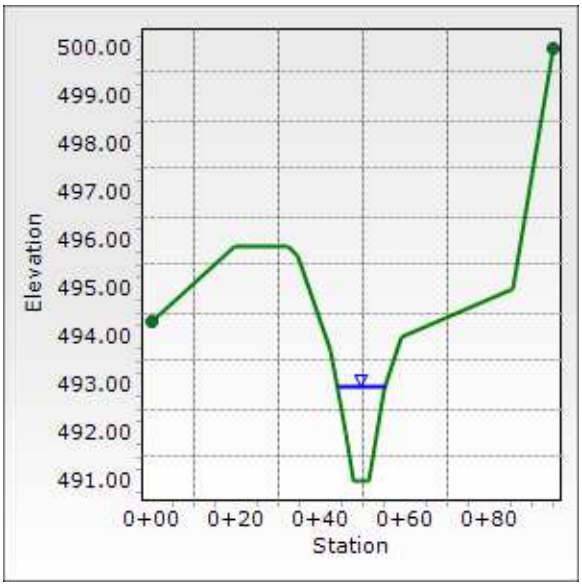
GVF Input Data	
Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0

GVF Output Data	
Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	23.7 in
Critical Depth	21.2 in
Channel Slope	0.020 ft/ft
Critical Slope	0.031 ft/ft

Cross Section for NODE 103-103 DOWNSTREAM DRAINAGE DITCH

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth

Input Data	
Channel Slope	0.020 ft/ft
Normal Depth	23.7 in
Discharge	73.44 cfs



Worksheet for NODE 103-103 UPSTREAM DRAINAGE DITCH

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth

Input Data	
Channel Slope	0.020 ft/ft
Discharge	73.44 cfs

Section Definitions

Station (ft)	Elevation (ft)
0+00	500.00
0+12	496.99
0+17	496.56
0+20	496.56
0+42	495.52
0+62	493.50
0+71	493.24
1+20	506.33

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 500.00)	(1+20, 506.33)	0.045

Options	
Current Roughness Weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

Results	
Normal Depth	15.7 in
Roughness Coefficient	0.045
Elevation	494.55 ft
Elevation Range	493.2 to 506.3 ft
Flow Area	18.7 ft²
Wetted Perimeter	24.2 ft
Hydraulic Radius	9.3 in
Top Width	24.01 ft
Normal Depth	15.7 in
Critical Depth	14.0 in
Critical Slope	0.034 ft/ft
Velocity	3.93 ft/s
Velocity Head	0.24 ft

FLOW DEPTH AT SECTION

Worksheet for NODE 103-103 UPSTREAM DRAINAGE DITCH

Results	
Specific Energy	1.55 ft
Froude Number	0.785
Flow Type	Subcritical

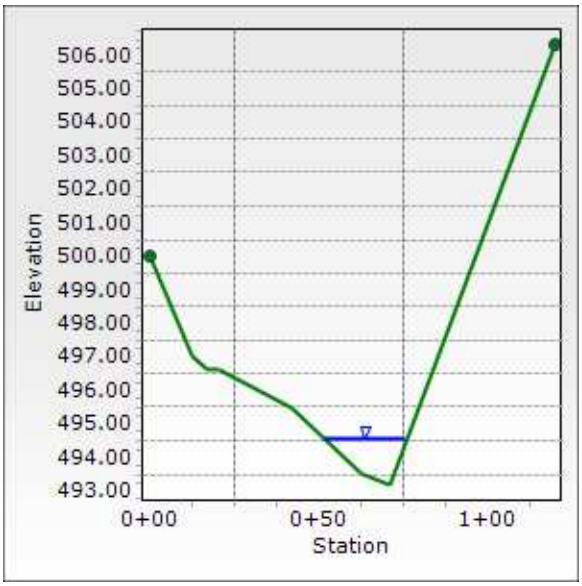
GVF Input Data	
Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0

GVF Output Data	
Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	15.7 in
Critical Depth	14.0 in
Channel Slope	0.020 ft/ft
Critical Slope	0.034 ft/ft

Cross Section for NODE 103-103 UPSTREAM DRAINAGE DITCH

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth

Input Data	
Channel Slope	0.020 ft/ft
Normal Depth	15.7 in
Discharge	73.44 cfs



Culvert Analysis Report
Culvert-1

Culvert Summary					
Computed Headwater Elev	494.13	ft	Discharge	103.70	cfs
Inlet Control HW Elev.	494.07	ft	Tailwater Elevation	N/A	ft
Outlet Control HW Elev.	494.13	ft	Control Type	Entrance Control	
Headwater Depth/Height	1.23				

Grades					
Upstream Invert	489.19	ft	Downstream Invert	486.93	ft
Length	63.00	ft	Constructed Slope	0.035873	ft/ft

Hydraulic Profile					
Profile	S2		Depth, Downstream	2.05	ft
Slope Type	Steep		Normal Depth	1.71	ft
Flow Regime	Supercritical		Critical Depth	3.08	ft
Velocity Downstream	15.99	ft/s	Critical Slope	0.005890	ft/ft

Section					
Section Shape	Circular		Mannings Coefficient	0.013	
Section Material	Concrete		Span	4.00	ft
Section Size	48 inch		Rise	4.00	ft
Number Sections	1				

Outlet Control Properties					
Outlet Control HW Elev.	494.13	ft	Upstream Velocity Head	1.55	ft
Ke	0.20		Entrance Loss	0.31	ft

Inlet Control Properties					
Inlet Control HW Elev.	494.07	ft	Flow Control	Submerged	
Inlet Type	Groove end w/headwall		Area Full	12.6	ft²
K	0.00180		HDS 5 Chart	1	
M	2.00000		HDS 5 Scale	2	
C	0.02920		Equation Form	1	
Y	0.74000				

THE EXISTING CACTUS ROAD HAS AN ELEVATION OF 495.00 WHERE THE EXISTING 48" STORM DRAIN CROSSES.

THE COMPUTED HEADWATER ELEVATION IS 494.13'

THEREFORE, THE WATER DOES NOT OVERTOP THE ROAD IN THE EXISTING CONDITION.

Culvert Designer/Analyzer Report
EXISTING 48" SD- POST DEVELOPMENT FLOW

Component:Culvert-1

Culvert Summary					
Computed Headwater Elev	493.75	ft	Discharge	92.20	cfs
Inlet Control HW Elev.	493.56	ft	Tailwater Elevation	N/A	ft
Outlet Control HW Elev.	493.75	ft	Control Type	Entrance Control	
Headwater Depth/Height	1.14				

Grades					
Upstream Invert	489.19	ft	Downstream Invert	486.93	ft
Length	63.00	ft	Constructed Slope	0.035873	ft/ft

Hydraulic Profile					
Profile	S2		Depth, Downstream	1.91	ft
Slope Type	Steep		Normal Depth	1.60	ft
Flow Regime	Supercritical		Critical Depth	2.91	ft
Velocity Downstream	15.59	ft/s	Critical Slope	0.005324	ft/ft

Section					
Section Shape	Circular		Mannings Coefficient	0.013	
Section Material	Concrete		Span	4.00	ft
Section Size	48 inch		Rise	4.00	ft
Number Sections	1				

Outlet Control Properties					
Outlet Control HW Elev.	493.75	ft	Upstream Velocity Head	1.38	ft
Ke	0.20		Entrance Loss	0.28	ft

Inlet Control Properties					
Inlet Control HW Elev.	493.56	ft	Flow Control	N/A	
Inlet Type	Groove end w/headwall		Area Full	12.6	ft²
K	0.00180		HDS 5 Chart	1	
M	2.00000		HDS 5 Scale	2	
C	0.02920		Equation Form	1	
Y	0.74000				

THE EXISTING CACTUS ROAD HAS AN ELEVATION OF 495.00 WHERE THE EXISTING 48" STORM DRAIN CROSSES.

THE COMPUTED HEADWATER ELEVATION IS 493.75'

THEREFORE, IN THE POST DEVELOPMENT CONDITION THE WATER WILL NOT OVERTOP THE ROAD.

APPENDIX 6

Drainage Exhibits

LEGEND

- DRAINAGE SUBAREA
- DRAINAGE SYSTEM
- FLOW DIRECTION
- HYDROLOGY NODE
- AREA FROM UPSTREAM TO DOWNSTREAM NODE (X.XX AC)
- DRAINAGE FLOWPATH

OTAY MESA ROAD
CONTINENTAL ST
CACTUS ROAD
CAMINO MAQUILADORA
STATE ROUTE 905
CONTINENTAL STREET
AIRWAY ROAD
BRITTANIA BOULEVARD
AIRWAY GARDENS
EPOCA

200 — 2.89 AC
201 — 0.07 AC
202 — 14.84 AC
207 — 13.11 AC
206 — 16.72 AC
16.72 AC
204 — 5.93 AC
205 — CONTINENTAL COMMERCE CENTER 34932-3D
203
209 — 2.94 AC
208 — 4.62 AC
210 — 37.32 AC
103
108
109 — 0.44 AC
107 — 0.69 AC
102 — 0.26 AC
101
106
105 — 4.95 AC N.A.P.
104 — 0.42 AC

AREA CURRENTLY UNDEVELOPED BUT WILL BE DEVELOPED IN FUTURE

EXISTING BUILDING
EXISTING DEVELOPMENT
EXISTING BASIN
PIPE
HP
WALL STARTS

EXISTING 48" STORM DRAIN

SYSTEM 100
Q = 103.7 CFS
A = 105.2 ACRES

EXISTING INTERIM INLETS TO EPOCA
EXISTING 18" SD FROM CALTRANS 11-288804
FUTURE INLETS

PARCEL 13
PARCEL 18
PARCEL 20
PARCEL 19

150 75 0 150 300 450
SCALE: 1"=150'

NOTE:

THE NODES IN THE 200S RANGE REPRESENT OFFSITE AREA. THIS AREA IS COMPRISED OF EXISTING DEVELOPMENTS AND AREAS IN WHICH FUTURE DEVELOPMENTS WILL OCCUR.

PER THE NOTICE TO ALL ENGINEERS DATED AUGUST 7, 1987 THE WATERSHED IS SUBJECT TO THE 50-YEAR AND 100-YEAR STORM DETENTION REQUIREMENTS. THEREFORE, ALTHOUGH THE AREA IS DEVELOPED THE C VALUES USED IN CALCULATIONS REPRESENT DETENTION. SEE DRAINAGE REPORT FOR MORE DETAILS.

SCALE: 1"=150'
JOB #: 4481
CREATED: 10/30/23

PREPARED BY:
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619.234.0349 Fax

CITY OF SAN DIEGO
COLLECTION AT CACTUS

DRAINAGE MAP
EXISTING CONDITIONS
EXHIBIT A

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LEGEND

DRAINAGE SUBAREA

DRAINAGE SYSTEM

SEE SHEET 2

SEE SHEET 2

FLOW DIRECTION

HYDROLOGY NODE

AREA FROM UPSTREAM TO DOWNSTREAM NODE X.XX AC

DRAINAGE FLOWPATH

HP

EXISTING DEVELOPMENT

STATE ROUTE 905

SEE SHEET 2

HP

OTAY MESA RD

OTAY MESA PKWY

CACTUS ROAD

EXISTING 48" STORM DRAIN

SEE SHEET 2 FOR RESULT

PROPOSED PUBLIC SD EASEMENT

BMP-1

3003

PA-12

3.73 AC

3017

PA-11

8.21 AC

3004

BMP-2

5002

PUBLIC PARK

3.52 AC

BMP-3

6002

5.17 AC

3005

0.10 AC

5001

5000

0.30 AC

3016

STREET D

(PUBLIC)

1.20 AC

6001

3020

6000

0.37 AC

6004

3014

3015

3010

0.43 AC

3011

0.38 AC

3009

0.03 AC

6005

3007

3008

3000

3001

3002

0.37 AC

0.12 AC

0.03 AC

7002

BMP-4

PA-10

5.50 AC

0.46 AC

0.45 AC

3019

0.52 AC

3013

3012

PA-13

3018

5.97 AC

PARK WAY

(PUBLIC)

CONTINENTAL STREET

BMP-6

STORM DRAIN CONNECTION TO AIRWAY GARDENS

AIRWAY GARDENS

EPOCA

PROPOSED INLET

7001

0.15 AC

7000

BMP-5

AIRWAY ROAD

FUTURE INLET

N.A.P. TO EPOCA

AREA NO LONGER IN POST DEVELOPMENT CONDITION. IN THE ULTIMATE CONDITION, THIS AREA IS ROUTED TO BMP#4 IN EPOCA AND THE DETETION REQUIRMENTS ARE MET THERE.

PROJECTDESIGN CONSULTANTS
PHOTOGRAMMETRY DEPARTMENT
Project Number\, Phase: 4481.00
Date of Photography: 06\09\,2022
Drawing Scale: 1"=40' & 1' C.I.

N

60 30 0 60 120 180

SCALE: 1"=60'

SCALE:	1"=60'
JOB #:	4481
CREATED:	10/30/23

PREPARED BY:

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CITY OF SAN DIEGO

COLLECTION AT CACTUS

DRAINAGE EXHIBIT
PROPOSED CONDITIONS
SHEET 1 OF 2

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OTAY MESA ROAD

CAMINO MAQUILADROA

CACTUS ROAD

CONTINENTAL ST

CAMINO MAQUILADORA

STATE ROUTE 905

2.89 AC
200
201
0.07 AC
202
EXISTING BUILDING
EXISTING DEVELOPMENT
AREA CURRENTLY UNDEVELOPED BUT WILL BE DEVELOPED IN FUTURE.
207
13.11 AC
14.84 AC
204
EXISTING BASIN
206
16.72 AC
CONTINENTAL COMMERCE CENTER 34932-3D
205
5.94 AC
203
4.73 AC
208
209
2.94 AC
210
103
EXISTING 48" STORM DRAIN
SYSTEM 6000
Q(UNDETAINED) = 132.8 CFS
Q (DETAINED) = 92.2 CFS
A = 98.2 ACRES
SPRING CANYON
BMP #4
EPOCA
PA-10
PA-11
PA-12
PA-13
PUBLIC PARK
BMP-1
BMP-2
BMP-3
STREET D
PUBLIC
PARK WAY
CONTINENTAL STREET
PROPOSED INLET
FUTURE INLET
AIRWAY ROAD
STORM DRAIN CONNECTION TO AIRWAY GARDENS
AIRWAY GARDENS
PARCEL 13
PARCEL 18
PARCEL 20
PARCEL 19
SOUTH BASIN
BRITTANIA BOULEVARD
SEE SHEET 1
N.A.P. TO EPOCA
AREA NO LONGER IN POST DEVELOPMENT CONDITION. IN THE ULTIMATE CONDITION, THIS AREA IS ROUTED TO BMP#4 IN EPOCA AND THE DETETION REQUIRMENTS ARE MET THERE.
PIPE
HP
MH

LEGEND

- DRAINAGE SUBAREA
- DRAINAGE SYSTEM
- DRAINAGE BOUNDARY TO EPOCA*
- DRAINAGE BOUNDARY TO AIRWAY GARDENS*
- EXISTING OFFSITE BASINS
- FLOW DIRECTION
- DRAINAGE FLOWPATH
- HYDROLOGY NODE (#)
- AREA FROM UPSTREAM TO DOWNSTREAM NODE (X.XX AC)

DRAINAGE BOUNDARY TO EPOCA*

THE BOUNDARY SHOWN REPRESENTS THE OVERALL DRAINAGE BOUNDARY DRAINING TO "BMP #4" ON THE EPOCA PROJECT. EXISTING "BMP #4" AS SHOWN ABOVE, IS A COMBINED WATER QUALITY, DETENTION, AND HYDROMODIFICATION BASIN. DMA-10 FOR COLLECTION AT CACTUS, ON AIRWAY ROAD, SHOWN ON SHEET 1 OF 2, IS TREATED IN "BMP#4." ALL REQUIREMENTS OF WATER QUALITY, HYDROMODIFICATION, AND DETENTION HAVE ALREADY BEEN MET WITH "BMP #4."

SEE THE APPROVED REPORTS AS FOLLOWS:
EPOCA PHASE 1 STORM WATER QUALITY MANAGEMENT REPORT DATED 11/20/2020 AND ANY SUBSEQUENT AMENDMENTS PER PTS#658080

AND

EPOCA PHASE 1 DRAINAGE REPORT DATED 01/18/2021 AND ANY SUBSEQUENT AMENDMENTS PER PTS#658080

DRAINAGE BOUNDARY TO AIRWAY GARDENS

THE BOUNDARY SHOWN REPRESENTS A PORTION OF THE OVERALL DRAINAGE BOUNDARY DRAINING TO THE "SOUTH BASIN" ON THE AIRWAY GARDENS PROJECT. AS SHOWN ABOVE, THE "SOUTH BASIN" IS A COMBINED DETENTION AND HYDROMODICATION BASIN. THEREFORE, DMA-8 AND DMA-9, LOCATED ON AIRWAY ROAD, SHOWN ON SHEET 1 OF 2, HAVE THEIR DETENTION AND HYDROMODIFICATION REQUIREMENTS ALREADY MET. TO MEET THE REMAINING REQUIREMENT FOR WATER QUALITY, TWO MODULAR WETLANDS ARE PROPOSED TO TREAT THESE DMAS. AFTER TREATMENT, THE DRAINAGE WILL FOLLOW THE SAME PATH, TO AIRWAY GARDENS AND TO THE "SOUTH BASIN."

SEE THE APPROVED REPORTS AS FOLLOWS:
AIRWAY GARDENS STORM WATER QUALITY MANAGEMENT REPORT DATED 11/24/2020 AND ANY SUBSEQUENT AMENDMENTS PER PTS#669201
AND
AIRWAY GARDENS DRAINAGE REPORT DATED 11/11/2020 AND ANY SUBSEQUENT AMENDMENTS PER PTS#669201

SCALE: 1"=150'
JOB #: 4481
CREATED: 10/30/23

PREPARED BY:

PROJECT DESIGN CONSULTANTS
Planning | Landscape Architecture | Engineering | Survey
701 B Street, Suite 800
San Diego, CA 92101
619.235.6471 Tel
619.234.0349 Fax

CITY OF SAN DIEGO

COLLECTION AT CACTUS

DRAINAGE EXHIBIT
PROPOSED CONDITIONS
SHEET 2 OF 2

APPENDIX 7

Record Drawings

INDEX OF SHEETS

SHEET No.	DESCRIPTION
1	TITLE AND LOCATION MAP
2-29	TYPICAL CROSS SECTIONS
30-52	LAYOUTS
53-77	PROFILES
78-97	SUPERELEVATION DIAGRAMS
98-137	CONSTRUCTION DETAILS
138-185	TEMPORARY WATER POLLUTION CONTROL PLANS AND DETAILS
186-214	EROSION CONTROL, DETAILS AND QUANTITIES
215-237	CONTOUR GRADING
238-392	DRAINAGE PLANS, PROFILES, DETAILS AND QUANTITIES
393-404	SANITARY SEWER PLANS, DETAILS AND QUANTITIES
405-439	UTILITY PLANS
440-500	STAGE CONSTRUCTION PLANS AND QUANTITIES
501-506	TRAFFIC HANDLING PLANS
507-513	DETOUR PLANS
514	CONSTRUCTION AREA SIGNS
515-544	PAVEMENT DELINEATION PLANS, DETAILS AND QUANTITIES
545-558	SIGN PLANS, DETAILS AND QUANTITIES
559-593	SUMMARY OF QUANTITIES
594-637	RETAINING WALLS 123 TO 158A
638-639	SOUND WALL PLANS
640-648	HIGHWAY PLANTING
649-671	ELECTRICAL PLANS
672-769	REVISED AND NEW STANDARD PLANS

STRUCTURE PLANS

770-793	CALIENTE AVENUE OC Br No. 57-1142
794-818	HERITAGE ROAD UNDERCROSSING Br No. 57-1143 L/R
819-857	SPRING CANYON BRIDGE Br No. 57-1155 L/R

THE STANDARD PLANS LIST APPLICABLE TO THIS CONTRACT IS INCLUDED IN THE NOTICE TO BIDDERS AND SPECIAL PROVISIONS BOOK.

STATE OF CALIFORNIA

DEPARTMENT OF TRANSPORTATION

HPLU-6211(078)N

PROJECT PLANS FOR CONSTRUCTION ON

STATE HIGHWAY

IN SAN DIEGO COUNTY IN SAN DIEGO FROM 1.2 KM EAST OF ROUTE 805/905 SEPARATION TO 0.8 KM EAST OF BRITANNIA BOULEVARD OVERCROSSING

TO BE SUPPLEMENTED BY STANDARD PLANS DATED JULY 2004

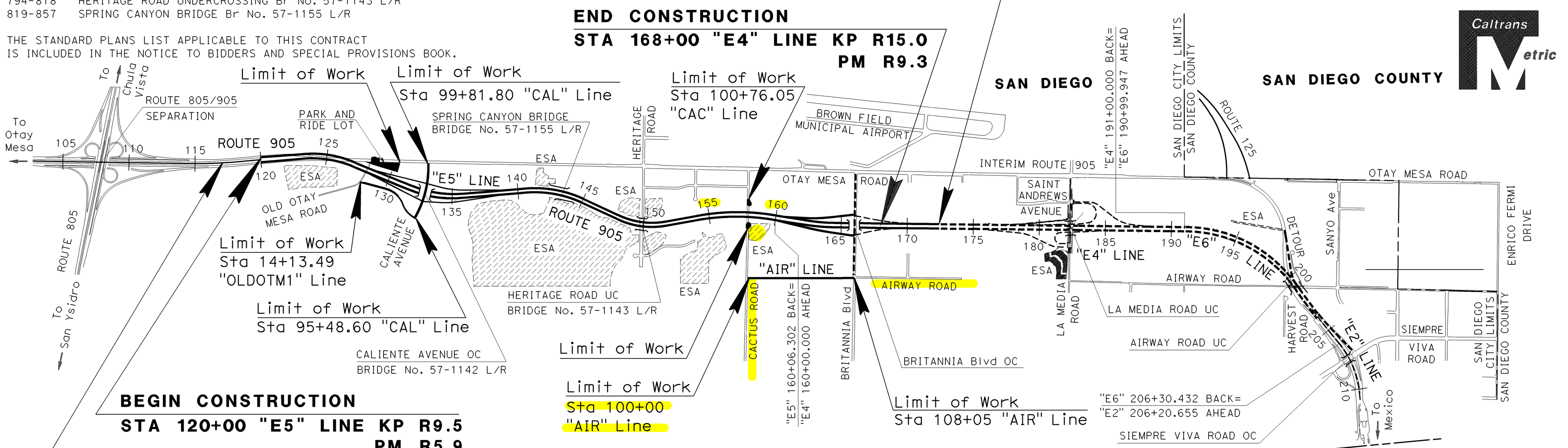
Dist	COUNTY	ROUTE	KILOMETER POST TOTAL PROJECT	SHEET No.	TOTAL SHEETS
11	SD	905	R9.5/R15.0	1	857

LOCATION MAP

Caltrans

Caltrans Metric

SAN DIEGO COUNTY



AS-BUILT PLANS

RESIDENT ENGINEER DATE

CONTRACT No.: 11-288804

C.C.A DATE: 10-04-13

REGISTERED PROFESSIONAL ENGINEER — MARLA DEYOE — No. 59141 — Exp. 06-30-17 — CIVIL — STATE OF CALIFORNIA

THE CONTRACTOR SHALL POSSESS THE CLASS (OR CLASSES) OF LICENSE AS SPECIFIED IN THE "NOTICE TO BIDDERS."

NO SCALE

------ CONCURRENT CONTRACT

ESA ENVIRONMENTALLY SENSITIVE AREA

PROJECT ENGINEER
REGISTERED CIVIL ENGINEER — 06-18-08 DATE

REGISTERED PROFESSIONAL ENGINEER — E.L. HAJJ — No. C42203 — Exp. 3-31-10 — CIVIL — STATE OF CALIFORNIA

October 20, 2008
PLANS APPROVAL DATE

THE STATE OF CALIFORNIA OR ITS OFFICERS OR AGENTS SHALL NOT BE RESPONSIBLE FOR THE ACCURACY OR COMPLETENESS OF ELECTRONIC COPIES OF THIS PLAN SHEET.

PHASE 2 PLAN

PROJECT MANAGER: I. SALAZAR

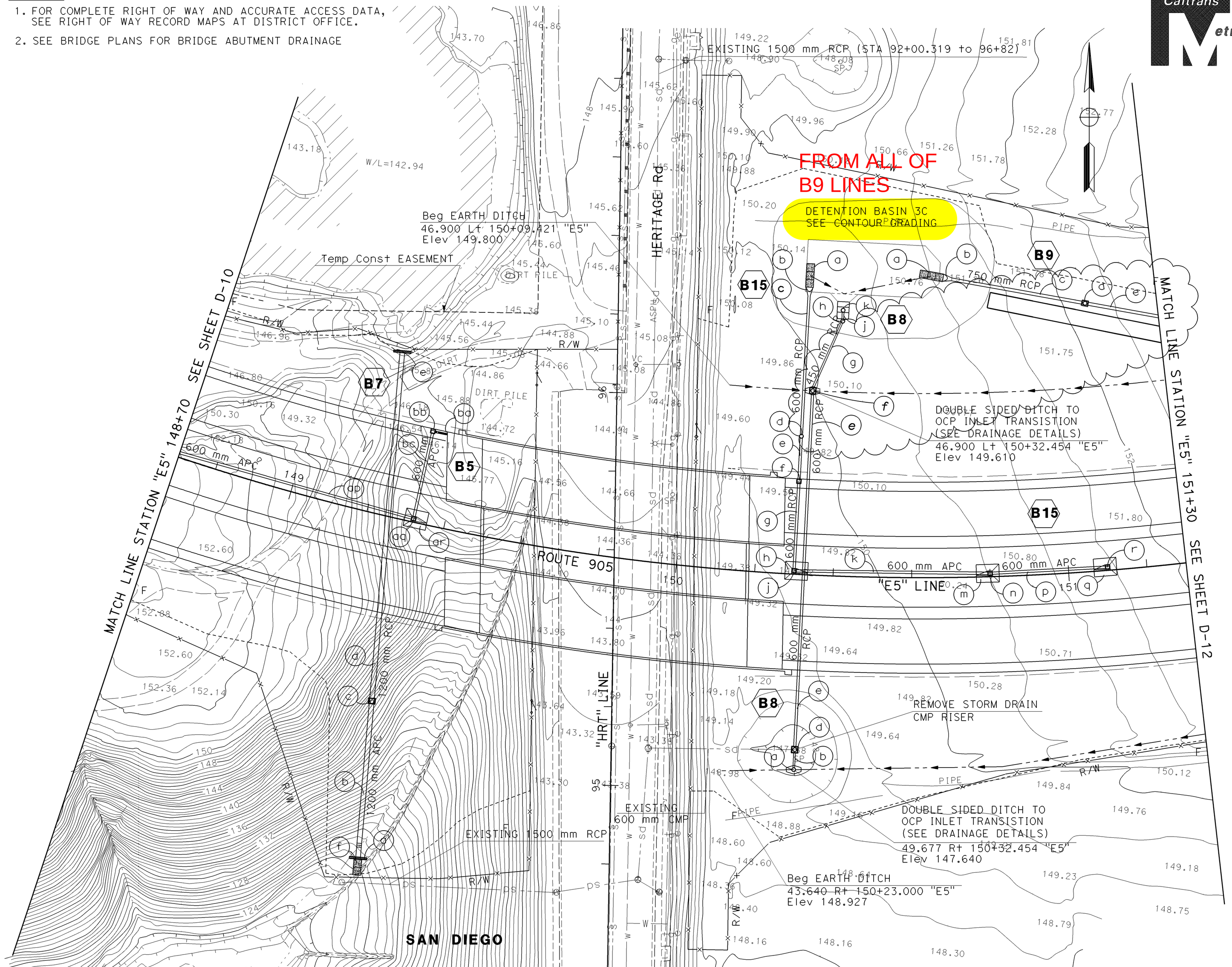
DESIGN ENGINEER: E.L. HAJJ

CONTRACT No. 11-288804

LAST REVISION: DATE PLOTTED => 26-JAN-2016 TIME PLOTTED => 07:57 — 06-19-08

NOTES:

1. FOR COMPLETE RIGHT OF WAY AND ACCURATE ACCESS DATA, SEE RIGHT OF WAY RECORD MAPS AT DISTRICT OFFICE.
2. SEE BRIDGE PLANS FOR BRIDGE ABUTMENT DRAINAGE



Dist	COUNTY	ROUTE	KILOMETER POST TOTAL PROJECT	SHEET No.	TOTAL SHEETS
11	SD	905	R9.5/R15.0	248	857

REGISTERED CIVIL ENGINEER — 06-30-09 DATE

F.BEHBOODY No. C 61478 Exp. 06-30-11 CIVIL — REGISTERED PROFESSIONAL ENGINEER — STATE OF CALIFORNIA

10-20-08
PLANS APPROVAL DATE

THE STATE OF CALIFORNIA OR ITS OFFICERS OR AGENTS SHALL NOT BE RESPONSIBLE FOR THE ACCURACY OR COMPLETENESS OF ELECTRONIC COPIES OF THIS PLAN SHEET.

AS BUILT
CONTRACT No. 11-288804
C.C.A. DATE 10-04-13
R.E. NAME M. DEYOE

PHASE 2 PLAN

B5 B7 B8 B9 B15

DRAINAGE PLAN
SCALE 1:500 **D-11**

LAST REVISION DATE PLOTTED => 26-OCT-2015
07-06-09 TIME PLOTTED => 15:22

STATE OF CALIFORNIA - DEPARTMENT OF TRANSPORTATION
Caltrans **PROJECT DEVELOPMENT**

FUNCTIONAL SUPERVISOR: E. HAJJ
CALCULATED-DESIGNED BY: F. BEHBOODY
CHECKED BY: M. OREIRO
REVISED BY
DATE REVISED

THIS PLAN ACCURATE FOR DRAINAGE WORK ONLY.

ALL DIMENSIONS ARE IN METERS UNLESS OTHERWISE SHOWN

BORDER LAST REVISED 3/1/2007

RELATIVE BORDER SCALE IS IN MILLIMETERS 0 20 40 60 80

USERNAME => s130912
DGN FILE => b28880ia011_p2_ab.dgn

CU 11223

EA 288801

NOTE:
FOR COMPLETE RIGHT OF WAY AND ACCURATE ACCESS DATA, SEE RIGHT OF WAY RECORD MAPS AT DISTRICT OFFICE.

Dist	COUNTY	ROUTE	KILOMETER POST TOTAL PROJECT	SHEET No.	TOTAL SHEETS
11	SD	905	R9.5/R15.0	249	857

06-30-09
REGISTERED CIVIL ENGINEER DATE

F.BEHBOODY
No. C 61478
Exp. 06-30-11
CIVIL
STATE OF CALIFORNIA

10-20-08
PLANS APPROVAL DATE

THE STATE OF CALIFORNIA OR ITS OFFICERS OR AGENTS SHALL NOT BE RESPONSIBLE FOR THE ACCURACY OR COMPLETENESS OF ELECTRONIC COPIES OF THIS PLAN SHEET.

Caltrans Metric

MATCH LINE STATION "E5" 151+30 SEE SHEET D-11

MATCH LINE STATION "E5" 154+30 SEE SHEET D-13

ROUTE 905

"E5" LINE

SAN DIEGO

END DITCH
36.137 Lt 151+50.000 "E5"
Elev 153.170

DOUBLE SIDED DITCH TO OCP INLET TRANSISTION (SEE DRAINAGE DETAILS)
39.900 Lt 152+00.000 "E5"
Elev 152.173

DOUBLE SIDED DITCH TO OCP INLET TRANSISTION (SEE DRAINAGE DETAILS)
40.269 Lt 154+00.000 "E5"
Elev 152.202

DITCH PI
30.951 Lt 153+26.000 "E5"
Elev 153.626

DITCH PI
39.152 Rt 151+80.000 "E5"
Elev 153.063

DOUBLE SIDED DITCH TO OCP INLET TRANSISTION (SEE DRAINAGE DETAILS)
44.945 RT 153+87.000 "E5"
Elev 150.261

Exist 600 mm RCP
FLOOD WATER STORAGE EASEMENT
Temp Const EASEMENT
600 mm RCP
750 mm RCP
750 mm APC
900 mm APC
600 mm APC
REMOVE 600 mm RCP
EXISTING CONCRETE DITCH
REMOVE CATCH BASIN
INLET FOR FUTURE RAMP
ABANDON EXISTING CATCH BASIN
EXISTING HEADWALL
DRAINAGE EASEMENT
Exist WATERLINE EASEMENT (OTAY WATER DISTRICT)
Exist DRAINAGE EASEMENT (CITY OF SAN DIEGO)
B9
B10
R/W
PIPE
DIRT
ASPH

THIS PLAN ACCURATE FOR DRAINAGE WORK ONLY.

ALL DIMENSIONS ARE IN METERS UNLESS OTHERWISE SHOWN

CCO 29

AS BUILT
CONTRACT No. 11-288804
C.C.A. DATE 10-04-13
R.E. NAME M. DEYOE

PHASE 2 PLAN

B9 B10

DRAINAGE PLAN
SCALE 1:500 **D-12**

REVISED BY	DATE REVISED

CALCULATED-DESIGNED BY: F. BEHBOODY
CHECKED BY: M. OREIRO
FUNCTIONAL SUPERVISOR: E. HAJJ

STATE OF CALIFORNIA - DEPARTMENT OF TRANSPORTATION
Caltrans PROJECT DEVELOPMENT

LAST REVISION DATE PLOTTED => 26-OCT-2015
TIME PLOTTED => 15:36
07-07-09

BORDER LAST REVISED 3/1/2007

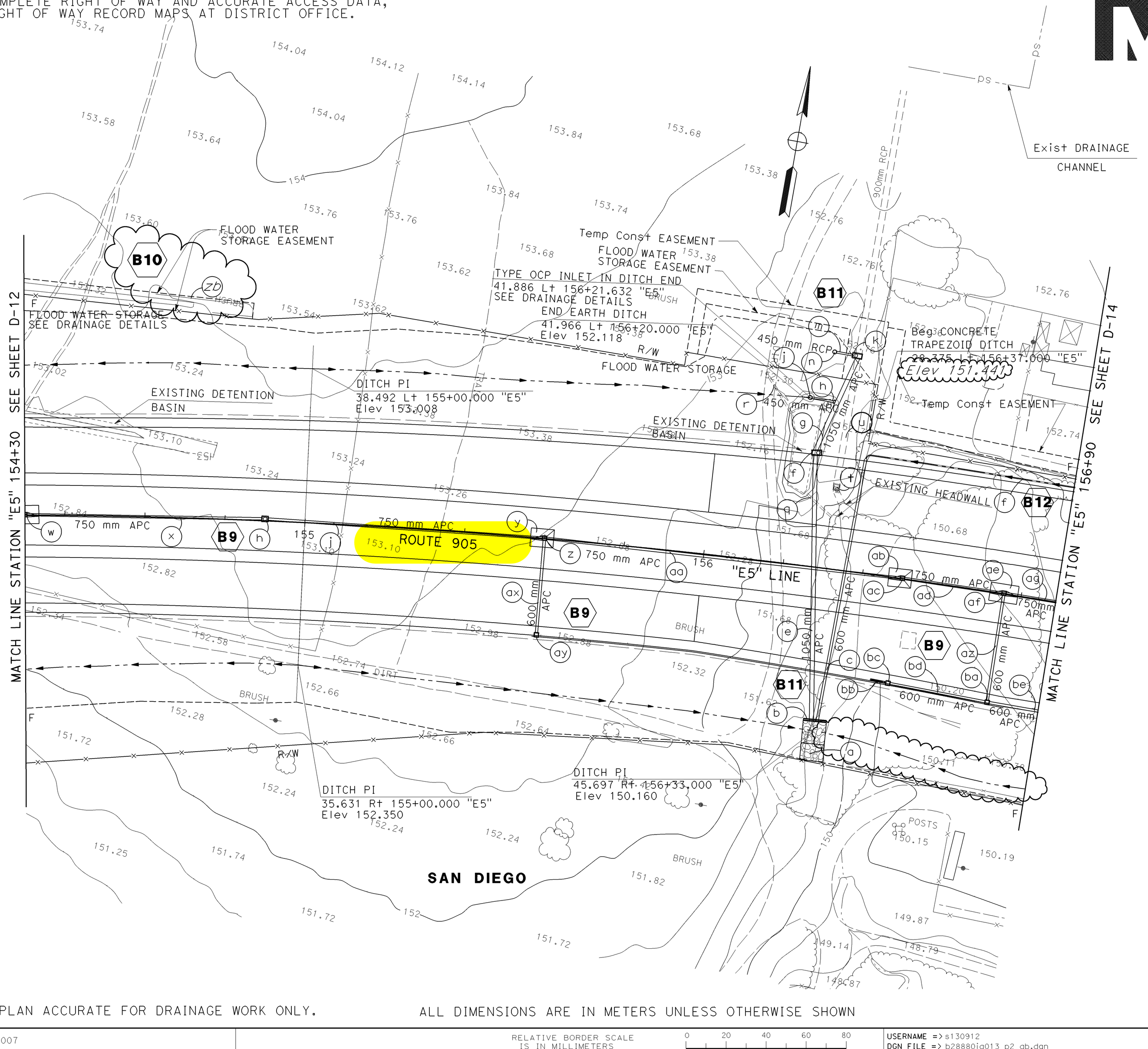
RELATIVE BORDER SCALE IS IN MILLIMETERS 0 20 40 60 80

USERNAME => s130912
DGN FILE => b28880ia012_p2_ab.dgn

CU 11223

EA 288801

NOTE:
FOR COMPLETE RIGHT OF WAY AND ACCURATE ACCESS DATA,
SEE RIGHT OF WAY RECORD MAPS AT DISTRICT OFFICE.



THIS PLAN ACCURATE FOR DRAINAGE WORK ONLY.

ALL DIMENSIONS ARE IN METERS UNLESS OTHERWISE SHOWN

Dist	COUNTY	ROUTE	KILOMETER POST TOTAL PROJECT	SHEET No.	TOTAL SHEETS
11	SD	905	R9.5/R15.0	250	857

06-30-09
REGISTERED CIVIL ENGINEER DATE

F.BEHBOODY
No. C 61478
Exp. 06-30-11
CIVIL
REGISTERED PROFESSIONAL ENGINEER
STATE OF CALIFORNIA

10-20-08
PLANS APPROVAL DATE

THE STATE OF CALIFORNIA OR ITS OFFICERS OR AGENTS SHALL NOT BE RESPONSIBLE FOR THE ACCURACY OR COMPLETENESS OF ELECTRONIC COPIES OF THIS PLAN SHEET.

CCO 29

AS BUILT
CONTRACT No. 11-288804
C.C.A. DATE 10-04-13
R.E. NAME M. DEYOE

PHASE 2 PLAN

B9 B11 B12

DRAINAGE PLAN
SCALE 1:500
D-13

LAST REVISION DATE PLOTTED => 26-OCT-2015
TIME PLOTTED => 15:39
07-07-09

REVISED BY	DATE REVISED
D. MOORE	

CALCULATED-DESIGNED BY: F. BEHBOODY
CHECKED BY: M. OREIRO
FUNCTIONAL SUPERVISOR: E. HAJJ

STATE OF CALIFORNIA - DEPARTMENT OF TRANSPORTATION
Caltrans PROJECT DEVELOPMENT

BORDER LAST REVISED 3/1/2007

RELATIVE BORDER SCALE IS IN MILLIMETERS 0 20 40 60 80

USERNAME => s130912
DGN FILE => b28880ia013_p2_ab.dgn

CU 11223

EA 288801

NOTE:
FOR COMPLETE RIGHT OF WAY AND ACCURATE ACCESS DATA, SEE RIGHT OF WAY RECORD MAPS AT DISTRICT OFFICE.

Dist	COUNTY	ROUTE	KILOMETER POST TOTAL PROJECT	SHEET No.	TOTAL SHEETS
11	SD	905	R9.5/R15.0	251	857

REGISTERED CIVIL ENGINEER — DATE: 06-30-09

F.BEHBOODY No. C 61478 Exp. 06-30-11 CIVIL — REGISTERED PROFESSIONAL ENGINEER — STATE OF CALIFORNIA

PLANS APPROVAL DATE: 10-20-08

THE STATE OF CALIFORNIA OR ITS OFFICERS OR AGENTS SHALL NOT BE RESPONSIBLE FOR THE ACCURACY OR COMPLETENESS OF ELECTRONIC COPIES OF THIS PLAN SHEET.

Caltrans Metric

EXISTING 150 mm SEWER LATERAL
EXISTING 450 mm RCP
EXISTING 600 mm RCP
EXISTING TYPE B CURB INLET
CACTUS ROAD 101
"CACT2" LINE
"CACT1" LINE
"CAC" LINE
"E5" LINE
450 mm RCP
DRAINAGE EASEMENT
END CONCRETE TRAPEZOID DITCH
BEG EARTH DITCH
40.800 Lt 158+30.000 "E5"
Elev 152.670
DITCH PI
28.975 Lt 157+80.000 "E5"
Elev 153.337
Temp Const Ease
DITCH PI
48.000 Lt 159+01.000 "E5"
Elev 151.600
45.109 Lt "E5" 160+06.300
Elev 152.090
END EARTH DITCH
48.600 Rt 157+53.000 "E5"
Elev 151.373
R/W
MATCH Exist EARTH DITCH
49.904 Rt 158+44.050 "E5"
Elev 150.723
(SEE DRAINAGE PROFILE)
38.180 Rt "E5" 160+06.300
Elev 152.999
ROUTE 905
PROJECT SITE
SAN DIEGO
MATCH LINE STATION "E5" 156+90 SEE SHEET D-13
MATCH LINE STATION "E5" 160+06.302 = "E4" 160+00 AHD SEE SHEET D-15
750 mm APC
600 mm APC
1200 mm APC
B9
B12
B13
HP

PHASE 2 PLAN
B9 B12 B13

AS BUILT
CONTRACT No. 11-288804
C.C.A. DATE 10-04-13
R.E. NAME M. DEYOE

DRAINAGE PLAN
SCALE 1:500
D-14

LAST REVISION DATE PLOTTED => 26-OCT-2015
07-07-09 TIME PLOTTED => 15:45

THIS PLAN ACCURATE FOR DRAINAGE WORK ONLY.

ALL DIMENSIONS ARE IN METERS UNLESS OTHERWISE SHOWN

STATE OF CALIFORNIA - DEPARTMENT OF TRANSPORTATION	CALCULATED-DESIGNED BY	CHECKED BY	F. BEHBOODY	M. OREIRO	REVISED BY	D. MOORE
Caltrans PROJECT DEVELOPMENT	FUNCTIONAL SUPERVISOR	E. HAJJ			DATE REVISED	

BORDER LAST REVISED 3/1/2007 | RELATIVE BORDER SCALE IS IN MILLIMETERS 0 20 40 60 80 | USERNAME => s130912 DGN FILE => b28880ia014_p2_ab.dgn | CU 11223 | EA 288801

Dist	COUNTY	ROUTE	KILOMETER POST TOTAL PROJECT	SHEET No.	TOTAL SHEETS
11	SD	905	R9.5/R15.0	252	857

Thomas M. Guerrini 06-30-09
REGISTERED CIVIL ENGINEER DATE

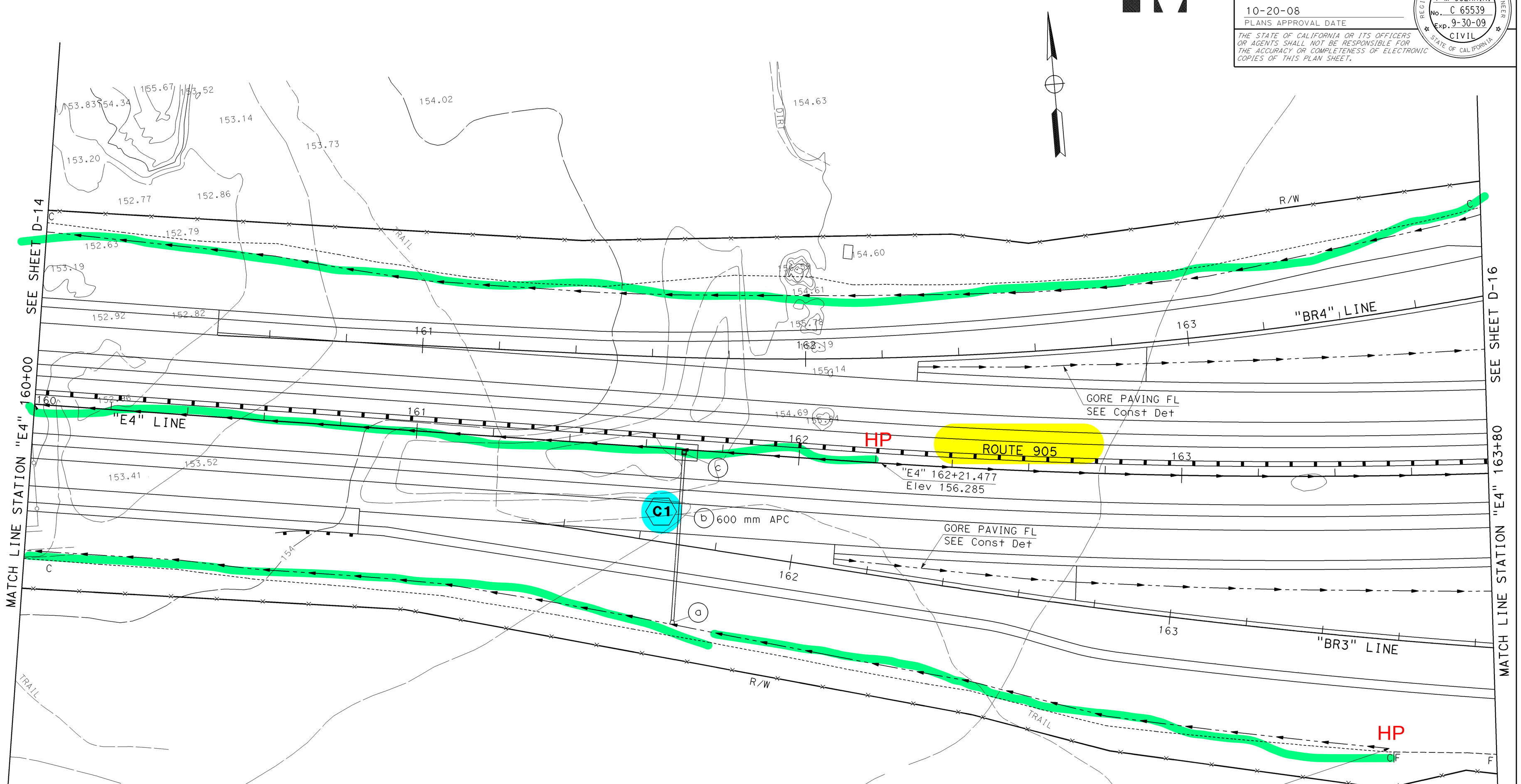
10-20-08
PLANS APPROVAL DATE

THE STATE OF CALIFORNIA OR ITS OFFICERS OR AGENTS SHALL NOT BE RESPONSIBLE FOR THE ACCURACY OR COMPLETENESS OF ELECTRONIC COPIES OF THIS PLAN SHEET.

REGISTERED PROFESSIONAL ENGINEER
T M GUERRINI
No. C 65539
Exp. 9-30-09
CIVIL
STATE OF CALIFORNIA

Caltrans Metric

NOTE:
FOR COMPLETE RIGHT OF WAY AND ACCURATE ACCESS DATA, SEE RIGHT OF WAY RECORD MAPS AT DISTRICT OFFICE.



AS BUILT
(NO CORRECTIONS ON THIS SHEET)
CONTRACT No. *11-288804*
C.C.A. DATE *10-04-13*
R.E. NAME *M. DEYOE*

C1

PHASE 2 PLAN **DRAINAGE PLAN**

THIS PLAN ACCURATE FOR DRAINAGE WORK ONLY

ALL DIMENSIONS ARE IN METERS UNLESS OTHERWISE SHOWN

SCALE: 1:500

D-15

CALCULATED-DESIGNED BY T. GUERRINI
CHECKED BY F. BEHBOODY
FUNCTIONAL SUPERVISOR E. HAJJ
STATE OF CALIFORNIA - DEPARTMENT OF TRANSPORTATION
Caltrans PROJECT DEVELOPMENT

REVISED BY | DATE REVISED

LAST REVISION DATE PLOTTED => 27-OCT-2015
TIME PLOTTED => 07:19
07-07-09

BORDER LAST REVISED 3/1/2007

RELATIVE BORDER SCALE IS IN MILLIMETERS 0 20 40 60 80

USERNAME => s130912
DGN FILE => b28880ig015_p2_ab.dgn

CU 11223

EA 288801

Dist	COUNTY	ROUTE	KILOMETER POST TOTAL PROJECT	SHEET No.	TOTAL SHEETS
11	SD	905	R9.5/R15.0	253	857

Thomas M. Guerrini 06-30-09
REGISTERED CIVIL ENGINEER DATE

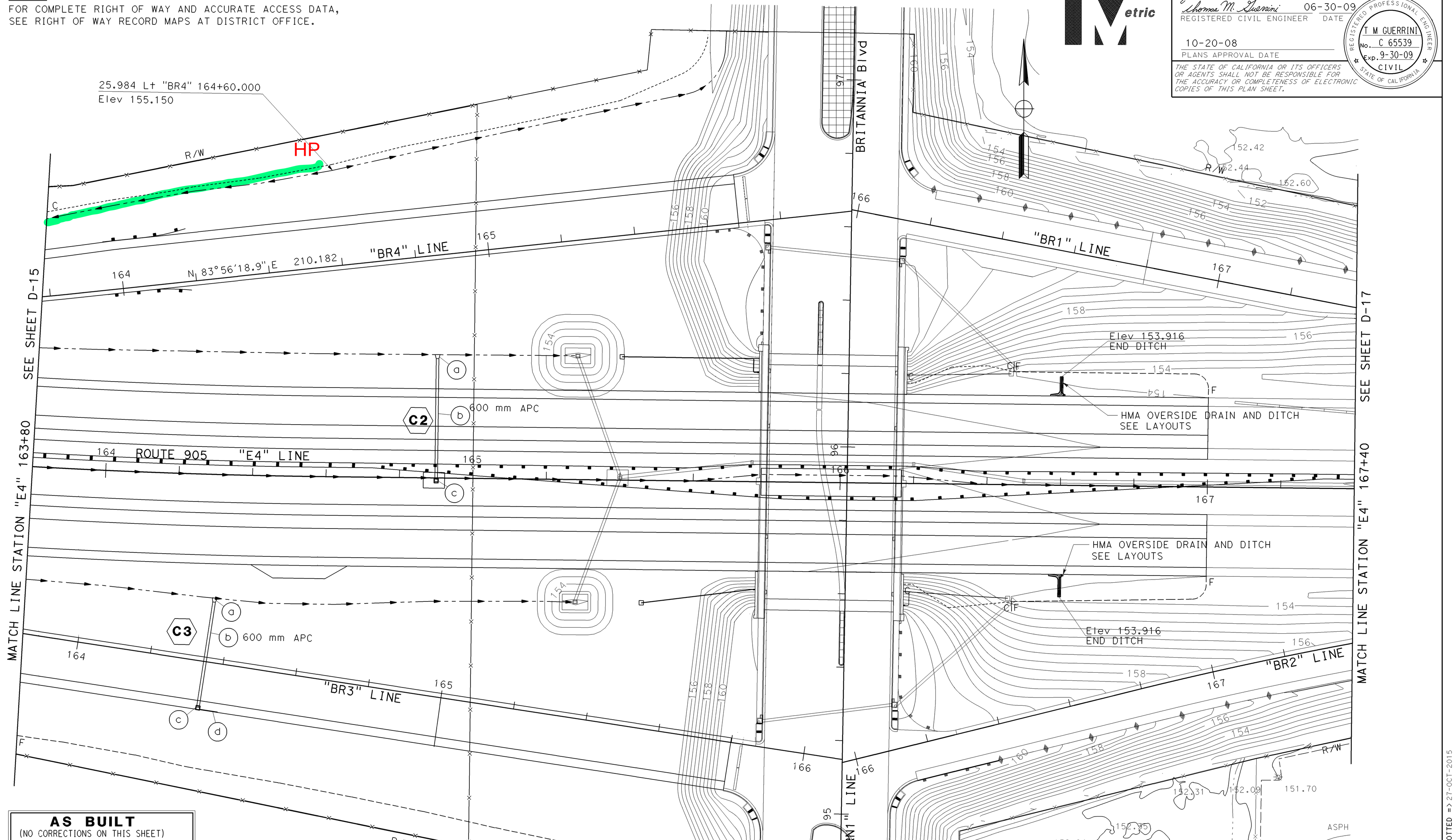
10-20-08
PLANS APPROVAL DATE

REGISTERED PROFESSIONAL ENGINEER — T M GUERRINI No. C 65539 Exp. 9-30-09 CIVIL — STATE OF CALIFORNIA

THE STATE OF CALIFORNIA OR ITS OFFICERS OR AGENTS SHALL NOT BE RESPONSIBLE FOR THE ACCURACY OR COMPLETENESS OF ELECTRONIC COPIES OF THIS PLAN SHEET.

Caltrans Metric

NOTE:
FOR COMPLETE RIGHT OF WAY AND ACCURATE ACCESS DATA, SEE RIGHT OF WAY RECORD MAPS AT DISTRICT OFFICE.



AS BUILT
(NO CORRECTIONS ON THIS SHEET)
CONTRACT No. 11-288804
C.C.A. DATE 10-04-13
R.E. NAME M. DEYOE

PHASE 2 PLAN

DRAINAGE PLAN

THIS PLAN ACCURATE FOR DRAINAGE WORK ONLY

ALL DIMENSIONS ARE IN METERS UNLESS OTHERWISE SHOWN

SCALE: 1:500

D-16

LAST REVISION DATE PLOTTED => 27-OCT-2015
07-07-09 TIME PLOTTED => 07:48

CALCULATED-DESIGNED BY T. GUERRINI
CHECKED BY F. BEHBOODY
FUNCTIONAL SUPERVISOR E. HAJJ
STATE OF CALIFORNIA - DEPARTMENT OF TRANSPORTATION
Caltrans PROJECT DEVELOPMENT
REVISED BY
DATE REVISED

BORDER LAST REVISED 3/1/2007

RELATIVE BORDER SCALE IS IN MILLIMETERS 0 20 40 60 80

USERNAME => s130912
DGN FILE => b28880ia016_p2_ab.dgn

CU 11223

EA 288801

Dist	COUNTY	ROUTE	KILOMETER POST TOTAL PROJECT	SHEET No.	TOTAL SHEETS
11	SD	905	R9.5/R15.0	335	857

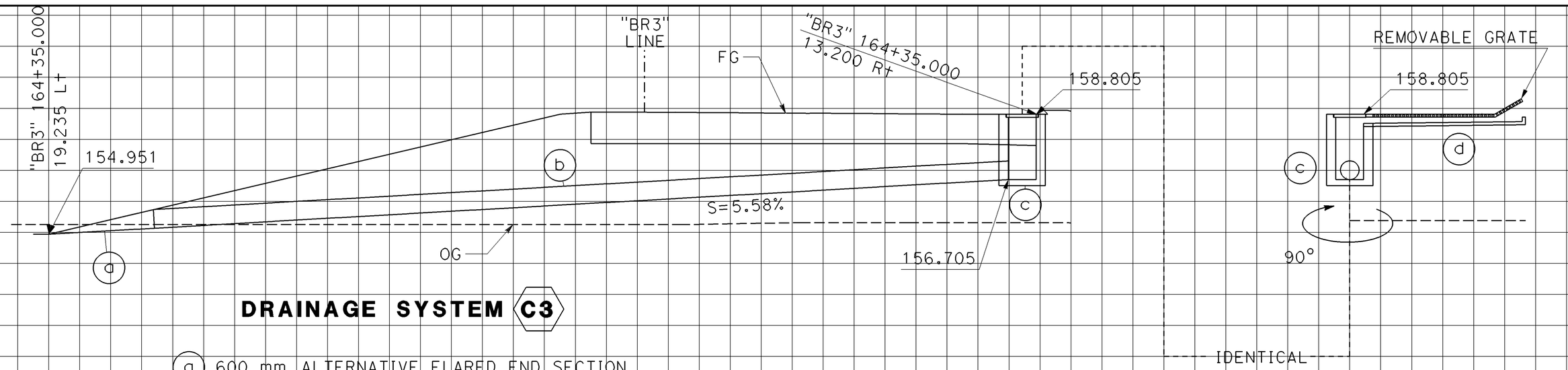
Caltrans Metric

Thomas M. Guerrini 06-30-09
REGISTERED CIVIL ENGINEER DATE

10-20-08
PLANS APPROVAL DATE

REGISTERED PROFESSIONAL ENGINEER — T M GUERRINI No. C 65539 Exp. 9-30-09 CIVIL — STATE OF CALIFORNIA

THE STATE OF CALIFORNIA OR ITS OFFICERS OR AGENTS SHALL NOT BE RESPONSIBLE FOR THE ACCURACY OR COMPLETENESS OF ELECTRONIC COPIES OF THIS PLAN SHEET.



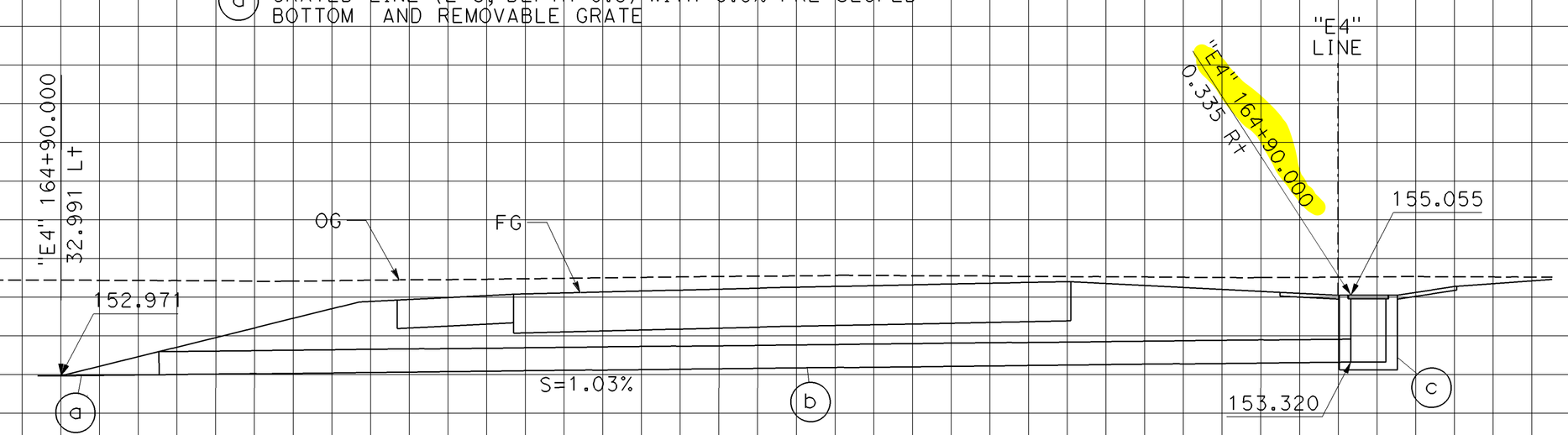
DRAINAGE SYSTEM C3

(a) 600 mm ALTERNATIVE FLARED END SECTION

(b) 600 mm × 28.7 APC

(c) G2 INLET (H=2.100) WITH 600-12X GRATE

(d) GRATED LINE (L=5, DEPTH=0.3) WITH 0.6% PRE-SLOPED BOTTOM AND REMOVABLE GRATE

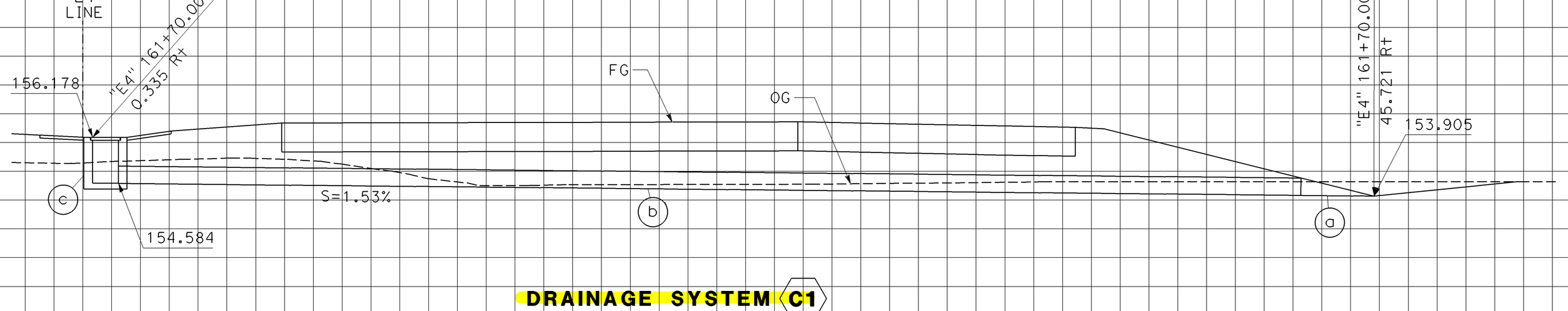


DRAINAGE SYSTEM C2

(a) 600 mm ALTERNATIVE FLARED END SECTION

(b) 600 mm × 32.8 APC

(c) G2 INLET (H=1.735) WITH 600-12X GRATE AND TYPE 3 PCC APRON (SEE DRAINAGE DETAILS)



DRAINAGE SYSTEM C1

(a) 600 mm ALTERNATIVE FLARED END SECTION

(b) 600 mm × 43.4 APC

(c) G2 INLET (H=1.594) WITH 600-12X GRATE AND TYPE 3 PCC APRON (SEE DRAINAGE DETAILS)

ALL DIMENSIONS ARE IN METERS UNLESS OTHERWISE SHOWN

AS BUILT
(NO CORRECTIONS ON THIS SHEET)
CONTRACT No. 11-288804
C.C.A. DATE 10-04-13
R.E. NAME M. DEYOE

PHASE 2 PLAN

C1 C2 C3

DRAINAGE PROFILES

SCALE Vert 1:100
Horiz 1:100

DP-75

STATE OF CALIFORNIA - DEPARTMENT OF TRANSPORTATION
Caltrans PROJECT DEVELOPMENT

FUNCTIONAL SUPERVISOR: E. HAJJ
CALCULATED-DESIGNED BY: T. GUERRINI
CHECKED BY: F. BEHBOODY
REVISED BY / DATE REVISED

Station	
m³	Exc
	Emb

LAST REVISION DATE PLOTTED => 05-NOV-2015
07-14-09 TIME PLOTTED => 07:10

BORDER LAST REVISED 3/1/2007

RELATIVE BORDER SCALE IS IN MILLIMETERS 0 20 40 60 80

USERNAME => s130912
DGN FILE => b28880ib075_p2_ab.dgn

CU 11223

EA 288801

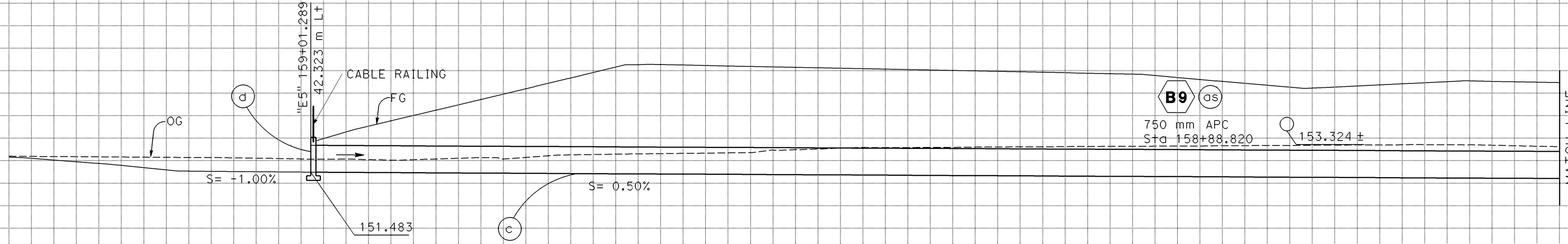
Dist	COUNTY	ROUTE	KILOMETER POST TOTAL PROJECT	SHEET No.	TOTAL SHEETS
11	SD	905	R9.5/R15.0	330	857

06-30-09
REGISTERED CIVIL ENGINEER DATE

F. BEHBOODY No. C 61478 Exp. 06-30-11 CIVIL — REGISTERED PROFESSIONAL ENGINEER — STATE OF CALIFORNIA

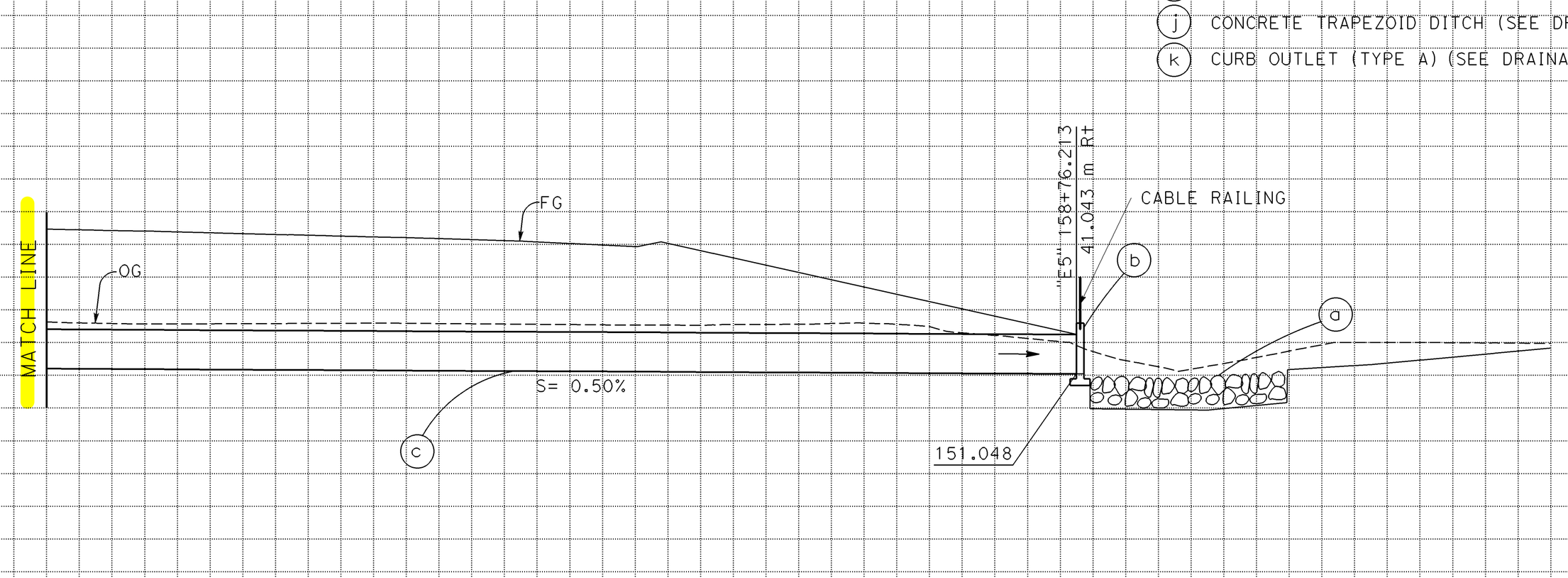
10-20-08
PLANS APPROVAL DATE

THE STATE OF CALIFORNIA OR ITS OFFICERS OR AGENTS SHALL NOT BE RESPONSIBLE FOR THE ACCURACY OR COMPLETENESS OF ELECTRONIC COPIES OF THIS PLAN SHEET.



DRAINAGE SYSTEM B12

- (a) CURVED RSP, FACING METHOD B (SEE DRAINAGE DETAILS)
- (b) "L" HEADWALL (H=1.71) w/CABLE RAILING (SEE DRAINAGE DETAILS)
- (c) 1200 mm x 87.1 APC
- (d) HEADWALL (H=1.71) w/CABLE RAILING
- (e) RSP, FACING METHOD B, 6 x 1.8 x 1
- (f) CONCRETE TRAPEZOID DITCH (SEE DRAINAGE DETAILS)
- (g) CONCRETE TRAPEZOID DITCH (SEE DRAINAGE DETAILS)
- (h) CURB OUTLET (TYPE A) (SEE DRAINAGE DETAILS)
- (j) CONCRETE TRAPEZOID DITCH (SEE DRAINAGE DETAILS)
- (k) CURB OUTLET (TYPE A) (SEE DRAINAGE DETAILS)



ALL DIMENSIONS ARE IN METERS UNLESS OTHERWISE SHOWN

AS BUILT
(NO CORRECTIONS ON THIS SHEET)
CONTRACT No. *11-288804*
C.C.A. DATE *10-04-13*
R.E. NAME *M. DEYOE*

PHASE 2 PLAN

B12

DRAINAGE PROFILES

SCALE Vert 1:100
Horiz 1:100

DP-70

F. BEHBOODY — DESIGNED BY
M. OREIRO — CALCULATED-
CHECKED BY
E. HAJJ — FUNCTIONAL SUPERVISOR
REVISED BY — DATE REVISED

STATE OF CALIFORNIA - DEPARTMENT OF TRANSPORTATION
Caltrans PROJECT DEVELOPMENT

Station
m³ Exc
Emb

LAST REVISION DATE PLOTTED => 05-NOV-2015
07-14-09 TIME PLOTTED => 06:50

BORDER LAST REVISED 3/1/2007

RELATIVE BORDER SCALE IS IN MILLIMETERS 0 20 40 60 80

USERNAME => s130912
DGN FILE => b28880ib070_p2_ab.dgn

CU 11223

EA 288801

AIRWAY ROAD PIPE CROSSING

Dist	COUNTY	ROUTE	KILOMETER POST TOTAL PROJECT	SHEET No.	TOTAL SHEETS
11	SD	905	R9.5/R15.0	258	857

Thomas M. Guerrini 06-30-09
REGISTERED CIVIL ENGINEER DATE

10-20-08
PLANS APPROVAL DATE

T M GUERRINI No. C 65539 Exp. 9-30-09 CIVIL
REGISTERED PROFESSIONAL ENGINEER — STATE OF CALIFORNIA

THE STATE OF CALIFORNIA OR ITS OFFICERS OR AGENTS SHALL NOT BE RESPONSIBLE FOR THE ACCURACY OR COMPLETENESS OF ELECTRONIC COPIES OF THIS PLAN SHEET.

NOTES:

1. FOR COMPLETE RIGHT OF WAY AND ACCURATE ACCESS DATA, SEE RIGHT OF WAY RECORD MAPS AT DISTRICT OFFICE.

Caltrans Metric

PROJECT SITE

SAN DIEGO

"CAC" LINE
CACTUS ROAD

PARCEL No. 33278

RW

4.783 Rt "CAC" 95+54.215
Elev 154.940

SLOPE Ease

CF

450 mm x 17.6 APC

"AIR" LINE
AIRWAY RD

Exist 450mm CMP

C5

CALTRANS PIPE

FTC

PARCEL No. 33086

3.823 Rt "CAC" 94+42.745
Elev 156.294

MATCH LINE STATION "AIR" 102+80 SEE SHEET D-22

AS BUILT
CONTRACT No. *11-288804*
C.C.A. DATE *10-04-13*
R.E. NAME *M. DEYOE*

PHASE 2 PLAN

C5

DRAINAGE PLAN
SCALE 1:500 **D-21**

THIS PLAN ACCURATE FOR DRAINAGE WORK ONLY

ALL DIMENSIONS ARE IN METERS UNLESS OTHERWISE SHOWN

CALCULATED-DESIGNED BY	CHECKED BY	REVISED BY	DATE REVISED
P. SASINOUAN	T. GUERRINI		

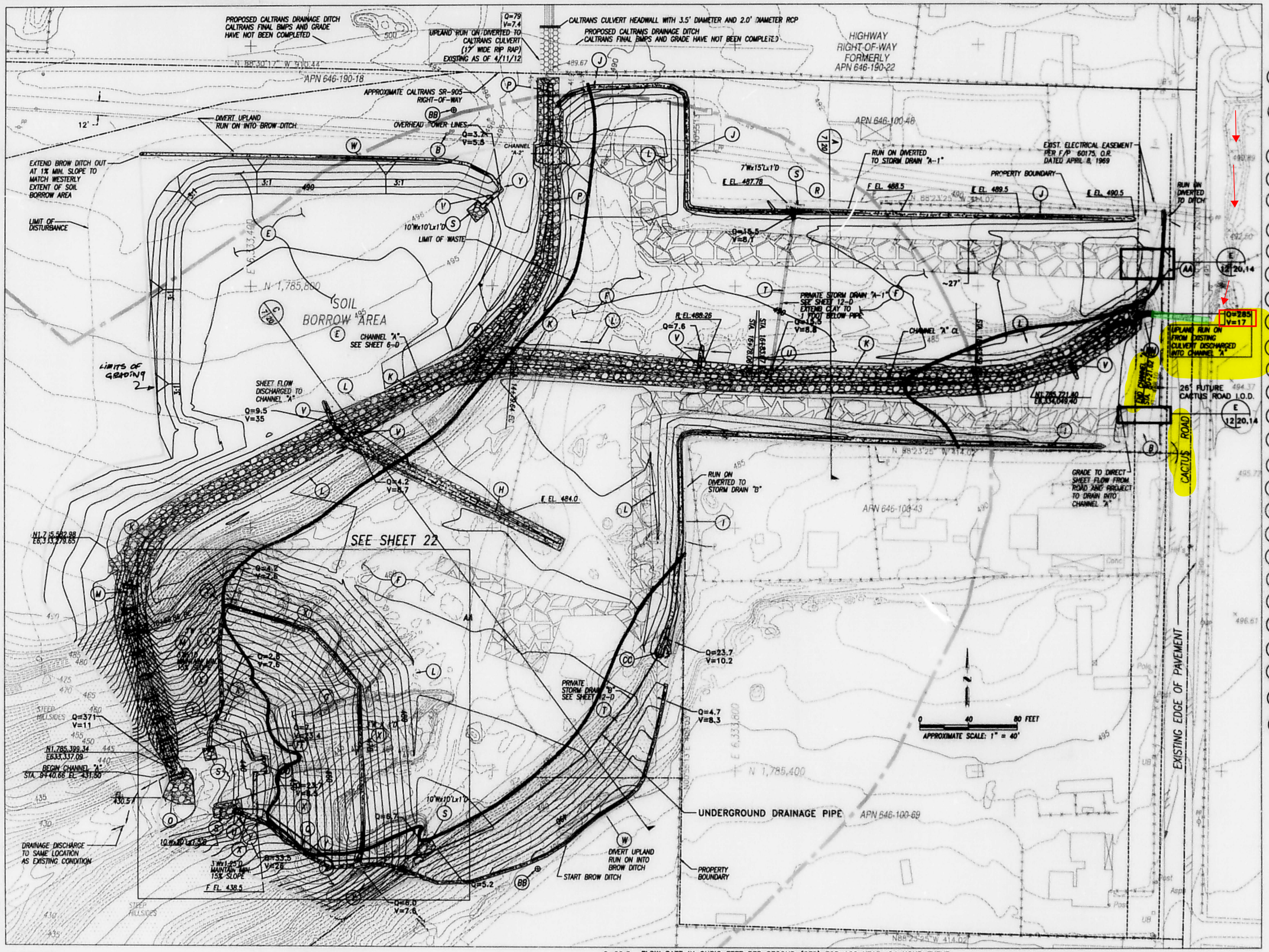
FUNCTIONAL SUPERVISOR: E. HAJJ

STATE OF CALIFORNIA - DEPARTMENT OF TRANSPORTATION
Caltrans PROJECT DEVELOPMENT

LAST REVISION DATE PLOTTED => 27-OCT-2015
TIME PLOTTED => 08:17
07-07-09

BORDER LAST REVISED 3/1/2007 | RELATIVE BORDER SCALE IS IN MILLIMETERS 0 20 40 60 80 | USERNAME => s130912 DGN FILE => b28880ja021_p2_ab.dgn | CU 11223 | EA 288801

EXISTING 48"
STORM DRAIN



CONSTRUCTION NOTES:

- (E) GRADE BORROW AREA TO THE GENERAL LINES AND GRADES FOR SIDE SLOPES AND LEAVE BOTTOM OF EXCAVATION TO DRAIN. ADJUST FINAL SLOPE LOCATIONS AND BOTTOM OF EXCAVATION AS DIRECTED BY THE ENGINEER.
- (F) CONSTRUCT FINAL COVER PER A 9 20
  EXTEND CLAY COVER TO 5 FT BEYOND LIMITS OF WASTE AND AS SHOWN ON B 7 20 ALSO SEE SPECIAL NOTE 8
- (G) CONSTRUCT FINAL COVER FOR FRONT SLOPE PER D 9 20
- (H) CONSTRUCT CONCRETE SWALE PER B 9 20
- (I) CONSTRUCT TOE OF SLOPE KEY AND 4' WIDE PERIMETER V-DITCH PER E 9 20
- (J) CONSTRUCT TOE OF SLOPE KEY AND 4' WIDE ELLIPTICAL-DITCH PER F 9 20
- (K) CONSTRUCT MIN.3.5' HIGH BY 4' WIDE TRAPEZOIDAL CHANNEL "A" PER A 10 20,21
- (L) CONSTRUCT 1.5' HIGH EARTH BERM PER C 9 20
- (M) CONSTRUCT 4' WIDE BOTTOM X VARIABLE DEPTH TRAPEZOIDAL CONCRETE CHANNEL WITH ENERGY DISSIPATORS PER A 11 20,21 B 11 20,21
- (O) CONSTRUCT STILLING BASIN PER E 10 20,21
- (P) CONSTRUCT 2.5' HIGH BY 4' WIDE TRAPEZOIDAL CHANNEL "A-2" PER A 24 20 B 10 20
- (Q) CONSTRUCT 30" DIA PRIVATE HDPE STORM DRAIN LINE "B" PER A 23 20
- (R) CONSTRUCT WINGED HEADWALL - PER SAN DIEGO STD. DWG. D-34
- (S) CONSTRUCT RIP-RAP PAD PER DETAIL AND PER DIMENSIONS SHOWN ON PLANS D 23 20
- (T) INSTALL 18" PRIVATE HDPE STORM DRAIN PER B 23 20
- (U) CONSTRUCT EARTH CHANNEL ENTRY PER C 10 20
- (V) CONSTRUCT CONCRETE DOWNDRAIN PER SAN DIEGO STD. DWG.D-22
- (W) CONSTRUCT BROW DITCH - TYPE A PER SAN DIEGO STD. DWG. D-75
- (X) CONSTRUCT DITCH - TYPE D PER SAN DIEGO STD. DWG. D-75
- (Y) CONSTRUCT 16" HIGH MASONRY CONCRETE UNIT SPLASH WALL 5 15 20
- (Z) ABANDON MONITORING WELLS IN PLACE
- (AA) INSTALL 6' HIGH CHAIN-LINK FENCE WITH 12' AND 24' GATES PER SAN DIEGO STD. DWGS. M-5, M-6 AND M-20
- (BB) INSTALL SETTLEMENT SURVEY MONUMENT PER G 9 20
- (CC) CONSTRUCT STORMDRAIN INLET APRON PER SAN DIEGO STD. DWG. D-39
- (DD) CONSTRUCT RISER PIPE SURFACE COMPLETION PER A 12 20,22
- (FF) EXTEND DRAINAGE ROCK/GEOTEXTILE BLANKET TO ELEVATION 440 IN ALL AREAS UP-CANYON OF CENTERLINE AND BELOW BASE OF FOUNDATION LAYER - SEE SHEET 8
- (HH) INSTALL 48" DIA. R.C.P. SAN DIEGO STD. DWGS. D-60, D-61, AND D-62 WITH RADIAL BEND AS SHOWN 6 15 20,21

ENVIRONMENTAL SENSITIVE AREAS

WATER QUALITY SENSITIVE AREAS

LEGEND:

- GRAVEL (ACCESS ROAD)
- RIP-RAP (DRAINAGE CHANNEL)
- "ONCRETE
- LIMIT OF WASTE WITHIN PROPERTY BOUNDARY
- 505 EXISTING 10-FT CONTOUR
- EXISTING 2-FT CONTOUR
- 450 AS-BUILT 10-FT CONTOUR
- AS-BUILT 2-FT CONTOUR
- FLOW LINE

Q=28.3 FLOW RATE IN CUBIC FEET PER SECOND (CFS) FOR 100 YEAR, 24 HOUR EVENT
V=1.7 FLOW VELOCITY IN FEET PER SECOND (FPS) FOR 100 YEAR, 24 HOUR EVENT

Geo-Logic ASSOCIATES
11415 WEST BERNARDO COURT
SUITE 200
SAN DIEGO, CA 92127
858-451-1136

JOHN HOWER C.E.G. NO. 2142 EXP. 08-31-17 — 01/05/16 DATE

JOSEPH FRANZONE R.C.E. NO. 039552 EXP. 12-31-17 — 01/05/16 DATE

REGISTERED PROFESSIONAL ENGINEER JOSEPH M. G. FRANZONE No. GE 2189 Exp. 12-31-17 PROFESSIONAL STATE OF CALIFORNIA

PROFESSIONAL GEOLOGIST JOHN M HOWER No. EG 2142 CERTIFIED ENGINEERING GEOLOGIST STATE OF CALIFORNIA

PRIVATE CONTRACT

GRADING AND IMPROVEMENT PLANS FOR:
SESI PROPERTY CLOSURE PROJECT

CITY OF SAN DIEGO, CALIFORNIA
DEVELOPMENT SERVICES DEPARTMENT
SHEET 20 OF 24 SHEETS

I.O. NO. 24002703
PROJECT NO. 275220
V.T.M.

FOR CITY ENGINEER — DATE 12/5/16

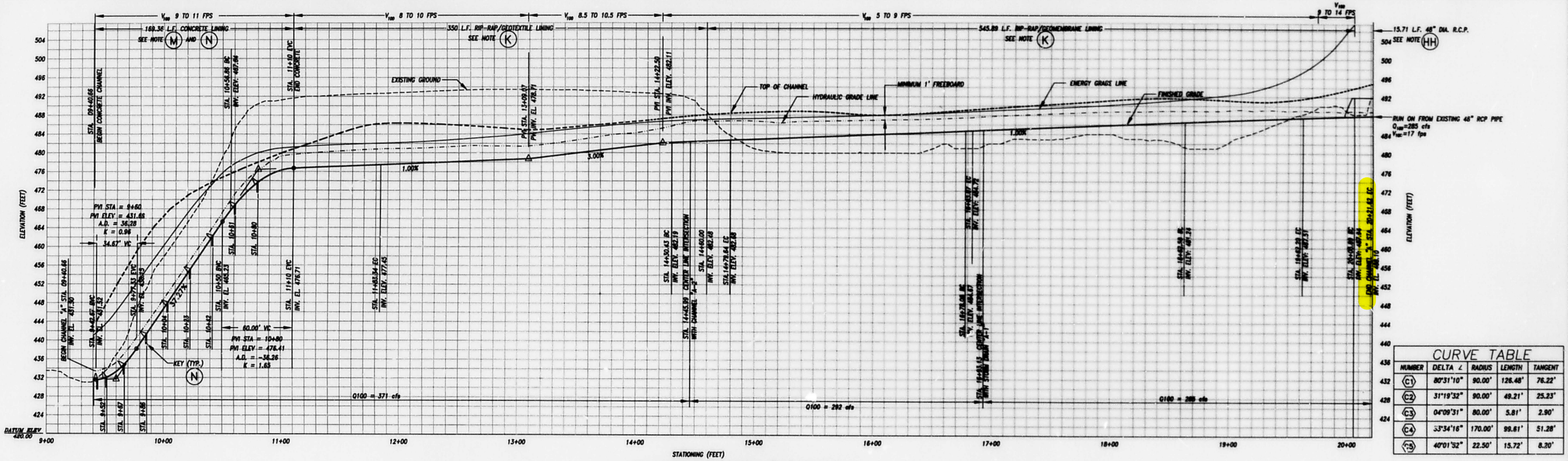
DESCRIPTION	BY	APPROVED	DATE	FILMED
ORIGINAL	GLA			5-01-17
AS-BUILTS	GLA	[illegible]	[illegible]	

1784-6331 NAD83 COORDINATES
144-1771 LAMBERT COORDINATES

CONTRACTOR SUKUT DATE STARTED 9-26-12
INSPECTOR Nick Mangarella DATE COMPLETED 2-27-17

37010-20-D

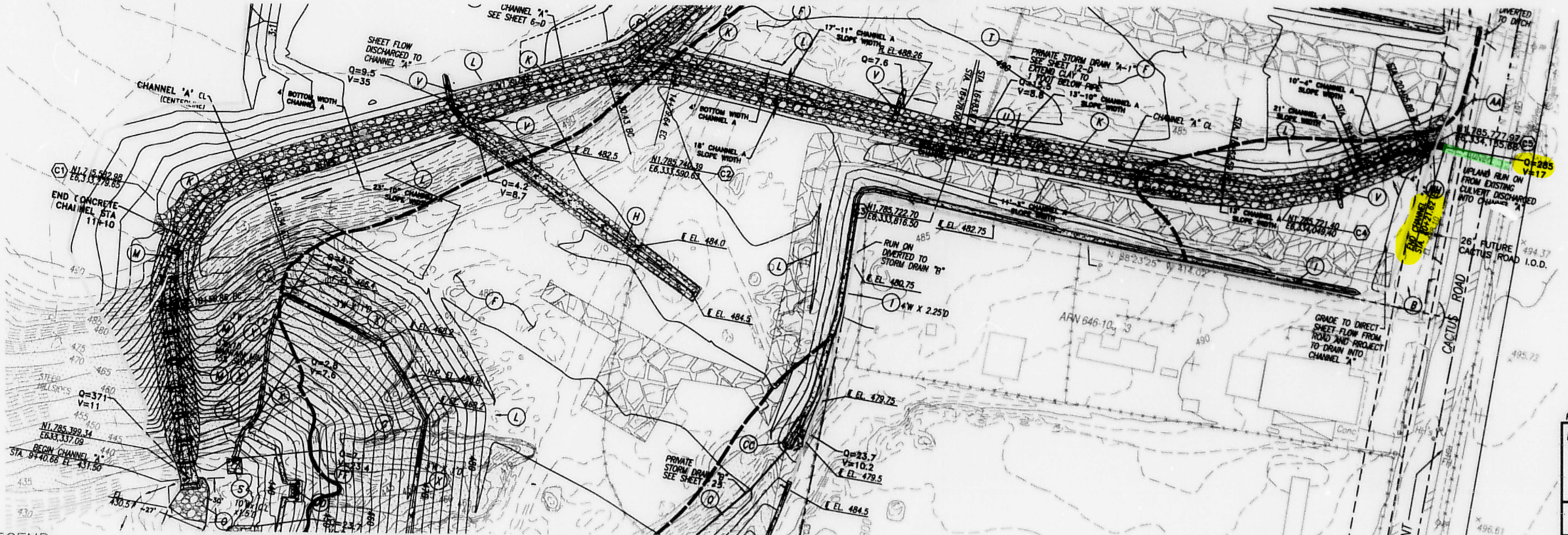
AS BUILT NEW SHEET



CURVE TABLE				
NUMBER	DELTA ∠	RADIUS	LENGTH	TANGENT
C1	80°31'10"	90.00'	126.48'	76.22'
C2	31°19'32"	90.00'	49.21'	25.23'
C3	04°09'31"	80.00'	5.81'	2.90'
C4	33°34'16"	170.00'	99.61'	51.28'
C5	40°01'32"	22.50'	15.72'	8.20'

PRIVATE CHANNEL "A" PROFILE

SCALE: HORIZONTAL 1"=40' & VERTICAL 1"=10'



PLAN VIEW

SCALE: 1"=40'

CONSTRUCTION NOTES:

(K) CONSTRUCT MIN.3.5' HIGH BY 4' WIDE TRAPEZOIDAL CHANNEL "A" PER A 10 20,21

(M) CONSTRUCT 4' WIDE BOTTOM X VARIABLE DEPTH CONCRETE CHANNEL WITH ENERGY DISSIPATOR PER A 11 20,21 B 11 20,21

(N) CONSTRUCT 12" THICK 2.0' DEEP KEY AT CHANNEL ENDS AND EVERY UPSTREAM END OF DISSIPATOR PER A 11 21, B 11 21, E 11 21, F 11 21

(HH) INSTALL 48" DIA R.C.P. SAN DIEGO STD. DWGS. D-60, D-61 AND D-62 WITH RADIAL BEND AS SHOWN PROVIDE 4 - 5' BEVEL OF 48" AT ONE END 6 15 20,21

0 40 80 FEET
SCALE: 1" = 40'

LEGEND:

- GRAVEL (ACCESS ROAD)
- RIP-RAP (DRAINAGE CHANNEL)
- CONCRETE
- LIMIT OF WASTE WITHIN PROPERTY BOUNDARY
- 505 EXISTING 10-FT CONTOUR
- EXISTING 2-FT CONTOUR
- 450 AS-BUILT 10-FT CONTOUR
- AS-BUILT 2-FT CONTOUR
- FLOW LINE

Geo-Logic ASSOCIATES
11415 WEST BERNARDO COURT
SUITE 200
SAN DIEGO, CA 92127
858-451-1136

JOHN HOWER C.E.G. NO. 2142 EXP. 08-31-17 — 01/05/16 DATE

JOSEPH FRANZONE R.C.E. NO. 039552 EXP. 12-31-17 — 01/05/16 DATE

REGISTERED PROFESSIONAL ENGINEER JOSEPH C. FRANZONE No. GE 2189 Exp. 12-31-17 GEOTECHNICAL STATE OF CALIFORNIA

PROFESSIONAL GEOLOGIST JOHN HOWER No. EG 2142 CERTIFIED ENGINEERING GEOLOGIST STATE OF CALIFORNIA

PRIVATE CONTRACT

DRAINAGE CHANNEL "A" PLAN AND PROFILE
SESI PROPERTY CLOSURE PROJECT

CITY OF SAN DIEGO, CALIFORNIA
DEVELOPMENT SERVICES DEPARTMENT
SHEET 21 OF 24 SHEETS

I.O. NO. 24002703
PROJECT NO. 275220

FOR CITY ENGINEER — DATE 12/5/16 — V.T.M.

DESCRIPTION	BY	APPROVED	DATE	FILMED
ORIGINAL	GLA			5-01-17
AS-BUILTS	GLA	Nick Mananisala	2/27/17	3/16/17

1784-6331 NAD83 COORDINATES

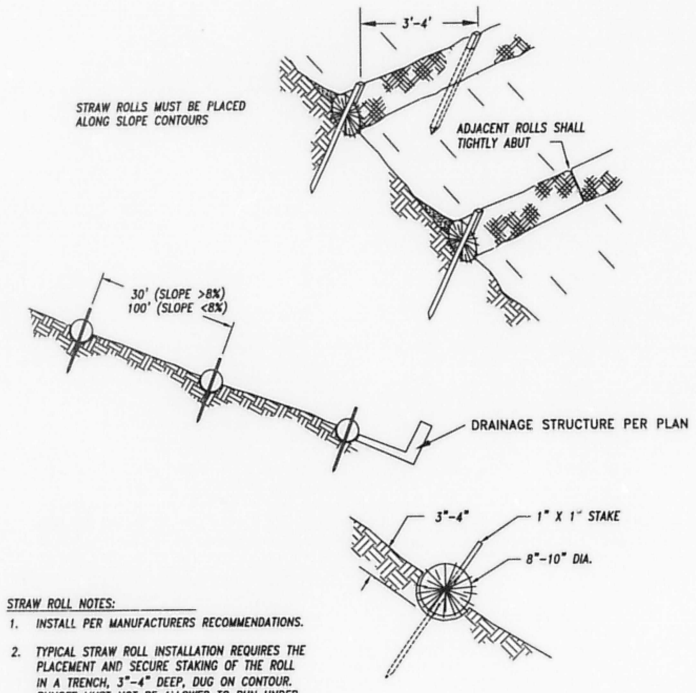
144-1771 LAMBERT COORDINATES

CONTRACTOR SUKUT DATE STARTED 9-21-16
INSPECTOR Nick Mananisala DATE COMPLETED 2-27-17

37010-21-D

AS BUILT NEW SHEET

FILMED FROM THE ORIGINAL. BEST QUALITY

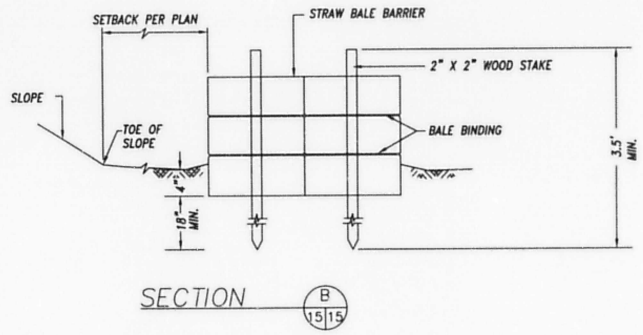


STRAW ROLL NOTES:

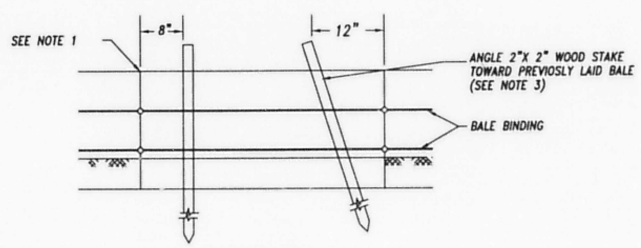
1. INSTALL PER MANUFACTURERS RECOMMENDATIONS.
2. TYPICAL STRAW ROLL INSTALLATION REQUIRES THE PLACEMENT AND SECURE STAKING OF THE ROLL IN A TRENCH, 3"-4" DEEP, DUG ON CONTOUR. RUNOFF MUST NOT BE ALLOWED TO RUN UNDER OR AROUND ROLL.

SLOPE TABLE			
FEATURE	SLOPE	MBP	SPACING
CHANNELS	40% (2.5:1)	FIBER ROLL	<=15 FT
TOP SLOPE	33.3% (3:1)	FIBER ROLL	<=30 FT
LANDFILL DECK	3%	FIBER ROLL	<=100 FT

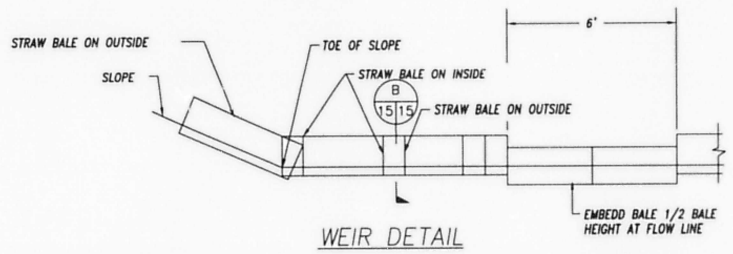
STRAW ROLL DETAILS — NOT TO SCALE — 15|14 #1



SECTION — B 15|15



PROFILE

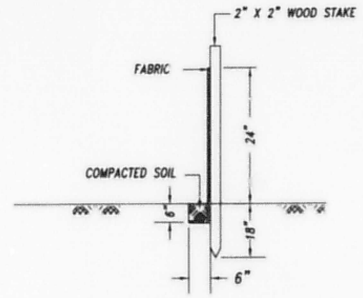


WEIR DETAIL

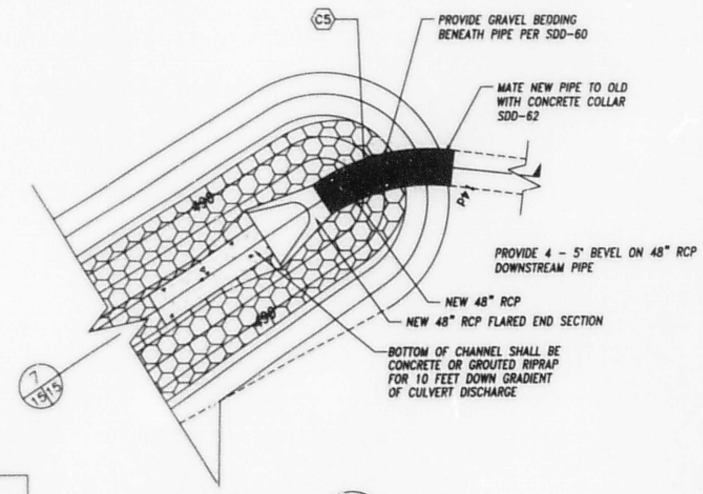
NOTES:

1. PLACE STRAW BALES TIGHTLY TOGETHER
2. TAMP EMBEDMENT SPOILS AGAINST SIDES OF INSTALLED BALES.
3. DRIVE ANGLED WOOD STAKE BEFORE VERTICAL STAKE TO ENSURE TIGHT ABUTMENT TO ADJACENT BAKE.
4. SANDBAG ROWS AND LAYERS SHALL BE OFFSET TO ELIMINATE GAPS.

STRAW BALE DETAIL — NOT TO SCALE — 15|14 #3

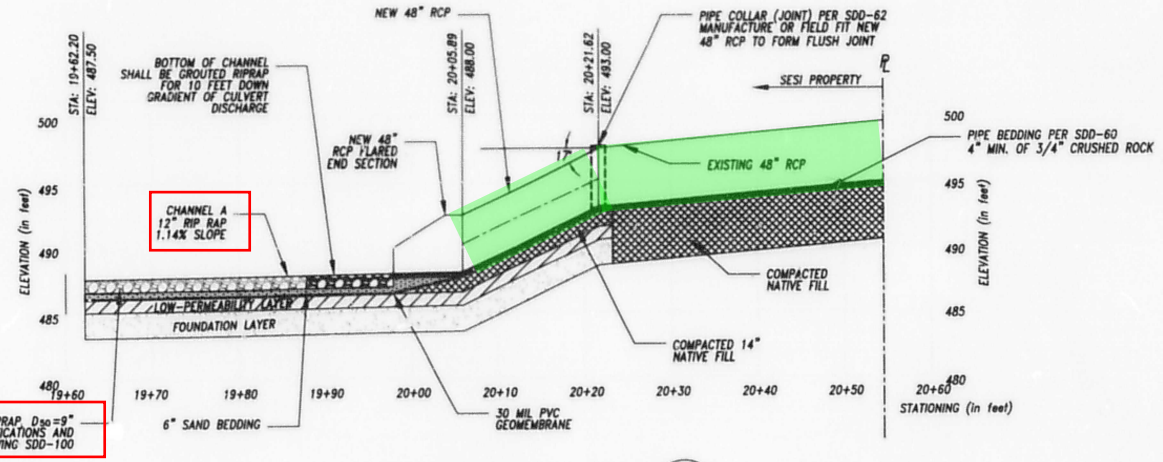


SILT FENCE DETAIL — NOT TO SCALE — 15|14 #4

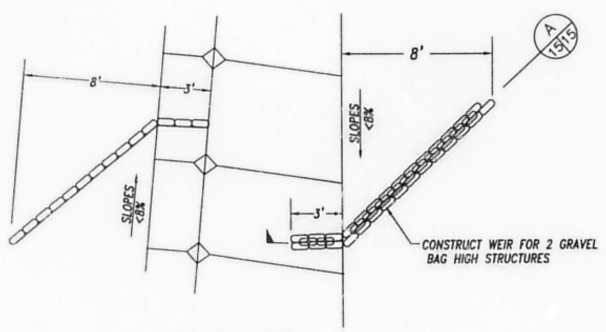


CURVE TABLE				
NUMBER	DELTA ∠	RADIUS	LENGTH	TANGENT
C5	40°01'52"	22.50'	15.72'	8.20'

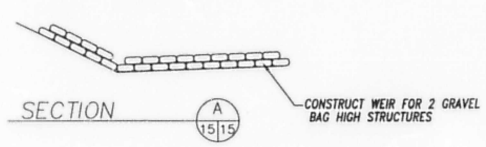
RCP DETAIL — NOT TO SCALE — 15|20.2 #6 B



RCP PROFILE VIEW — NOT TO SCALE — 15|15 #7

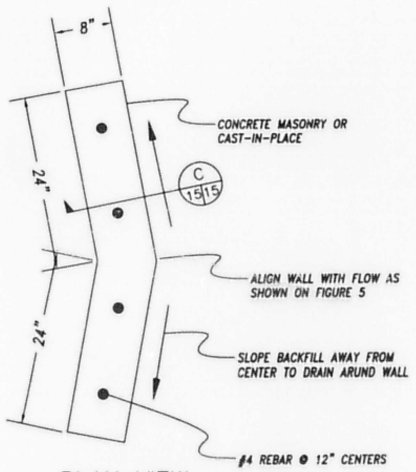


PLAN VIEW

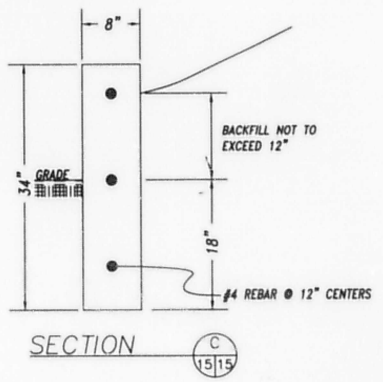


SECTION — A 15|15

GRAVEL BAG CHEVRON DETAIL — NOT TO SCALE — 15|14 #2



PLAN VIEW



SECTION — C 15|15

SPLASH WALL DETAIL — NOT TO SCALE — 15|20 #5 A B

OTIE
Oneida Total Integrated Enterprises
2247 San Diego Ave
SUITE 238
SAN DIEGO, CA 92110
619-230-1712

JOHN O. WINGATE R.C.E. EXP. 09-30-13 — 9/6/12 DATE

JOHN M. HOWER No. EG 2142 CERTIFIED ENGINEERING GEOLOGIST STATE OF CALIFORNIA

JOSEPH G. FRANZONE C 39552 EXP 6-30-15 CIVIL STATE OF CALIFORNIA

Geo-Logic Associates 11-4-2014 DATE
1144 GLENNEYRE ST. SUITE 'C' SAN DIEGO, CA 92037 (858) 459-1260 SIGNATURE REQUEST EXP 6/30/15 DATE

PRIVATE CONTRACT

EROSION AND SEDIMENT CONTROL DETAILS
SESI PROPERTY CLOSURE PROJECT

CITY OF SAN DIEGO, CALIFORNIA
DEVELOPMENT SERVICES DEPARTMENT
SHEET 15 OF 24 SHEETS

VFOR CITY ENGINEER — DATE 9/21/12

I.O. NO. 24002703
PROJECT NO. 275220
V.T.M.

DESCRIPTION	BY	APPROVED	DATE	FILMED
ORIGINAL	OTIE			11-28-12
A	GLA		12/18/13	1-06-14
B	GLA		12/5/16	5-01-17
AS-BUILTS	GLA		6/10/13	11/30/17

CONTRACTOR SOLAR DATE STARTED 9-25-12
INSPECTOR Vic Hernandez DATE COMPLETED 2-27-13

1784-6331 NAD83 COORDINATES
144-1771 LAMBERT COORDINATES
37010-15-D

A MODIFIED DECLARATION OF RESPONSIBLE CHARGE FOR NEW ENGINEER OF WORK. REVISED NUMBER OF SHEETS FROM 17 TO 18.

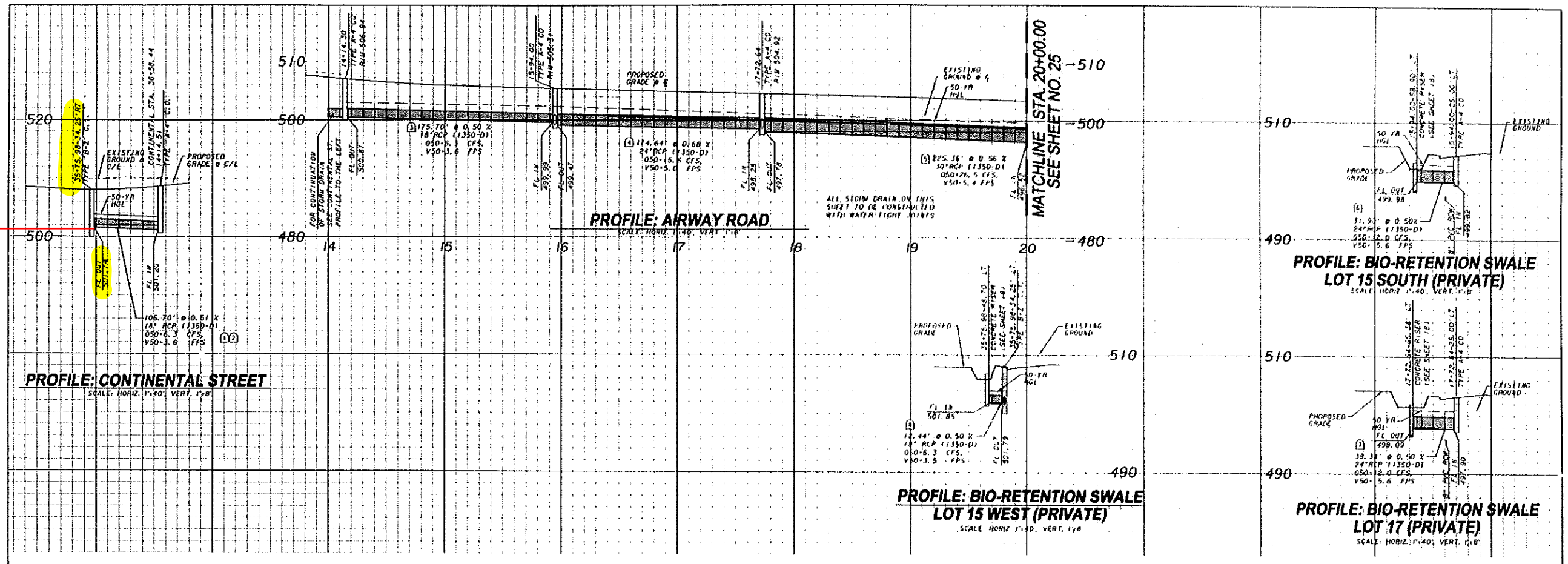
AS BUILT

B REVISED DETAIL REFERENCE SHEET NUMBER. REVISED TOTAL NUMBER OF SHEETS FROM 18 TO 24.

FILMED FROM THE ORIGINAL. BEST QUALITY

CONNECTION TO AIRWAY GARDENS

~500.74 IE



CENTERLINE DATA				
NO.	DELTA OR BRG.	RADIUS	LENGTH	REMARKS
①	N89°56'49"E		667.72'	

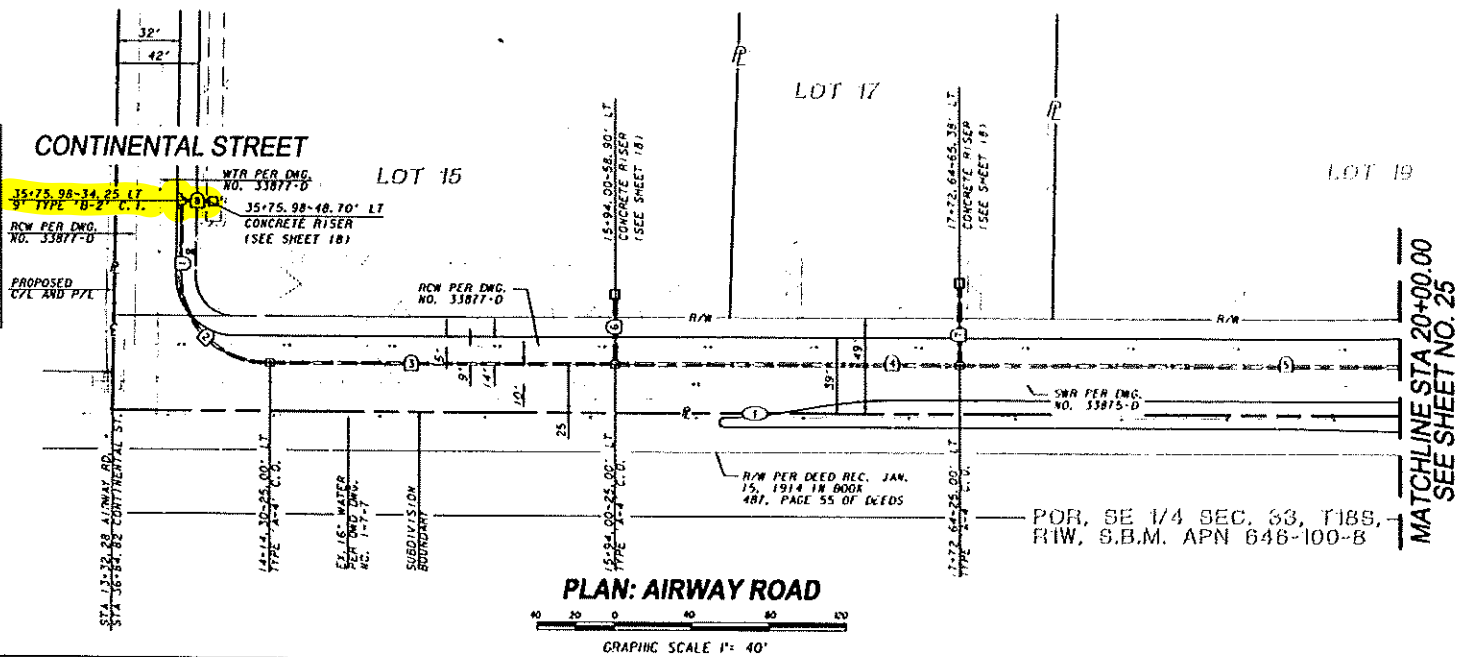
STORM DRAIN DATA					
NO.	DELTA OR BRG.	RADIUS	LENGTH	REMARKS	
①	N0°03'11"W		36.00'	18" RCP	PUB.
②	Δ=91°01'36"	44.50'	70.70'	18" RCP *	PUB.
③	N89°56'49"E		175.70'	18" RCP	PUB.
④	N89°56'49"E		174.64'	24" RCP	PUB.
⑤	N89°56'49"E		225.36'	30" RCP	PUB.
⑥	N0°03'11"W		31.90'	24" RCP	PVT.
⑦	N0°03'11"W		38.38'	24" RCP	PVT.
⑧	N89°01'56"W		12.44'	18" RCP	PVT.

* 4' LENGTHS 5° BEVEL ONE END AS NEEDED TO CONSTRUCT RADIUS

NOTE: ALL STORM DRAIN SEGMENTS SHOWN ON THIS SHEET SHALL BE CONSTRUCTED WITH WATER TIGHT JOINTS

FOR PRIVATE STORM DRAINS IN PUBLIC RIGHT OF WAY, PUBLIC EASEMENTS, AND FLOOD WATER STORAGE EASEMENT SEE EMRA NO. 603904

KARN ENGINEERING & SURVEYING, INC.
129 W. FIG STREET, FALLBROOK, CA 92028
(760) 728-1134



CAUTION!! LOCATION OF EXISTING UTILITIES ON THESE PLANS ARE APPROXIMATE AND SHALL BE VERIFIED BY CONTRACTOR PRIOR TO CONSTRUCTION.

BENCH MARK

THE NORTHEAST BRASS PLUG LOCATED IN THE TOP OF CURB AT THE INTERSECTION OF AIRWAY ROAD AND BRITANNIA BOULEVARD ELEVATION = 498.428 DATUM: NGVD 29 FEET

ENGINEER OF WORK

SCOTT HARRY R.C.E. 63792 DATE 4-14-14

REGISTERED PROFESSIONAL ENGINEER SCOTT R. HARRY NO. 63792 EXP 9-30-14 CIVIL STATE OF CALIFORNIA

PRIVATE CONTRACT J-095152006

STORM DRAIN PLANS FOR:

BROWN FIELD TECH PARK - UNIT 2

AIRWAY ROAD

CITY OF SAN DIEGO, CALIFORNIA
DEVELOPMENT SERVICES DEPARTMENT
SHEET 24 OF 26 SHEETS

4/3/14

DESCRIPTION	BY	APPROVED	DATE	ITEMS
ORIGINAL	KARN		4/14/14	3014

I.D. NO. 23425574
P.T.S. NO. 88430
I.M. 91-0395
1784-6333
144-1773
33876-24-D

BROWN FIELD TECH PARK - UNIT 2

NEW SHEET

PRINTED FROM THE ORIGINAL. BEST QUALITY OBTAINABLE. EXCESSIVE GRAY BACKGROUND

APPENDIX 8

Epoca and Airway Gardens Proposed Drainage Maps
(For Reference Only)

SCALE 1' = 80'

SYSTEM 5000
TOTAL Q100 = 7.3 CFS
TOTAL AREA = 2.0 AC

SYSTEM 4000
TOTAL Q100(UNDET) = 104.8 CFS
TOTAL AREA = 33.8 AC

SYSTEM 3000
TOTAL Q100 = 3.9 CFS
TOTAL AREA = 0.9 AC

SYSTEM 2000
TOTAL Q100 = 4.9 CFS
TOTAL AREA = 3.6 AC

SYSTEM 1000
TOTAL Q100(UNDET) = 156.5 CFS
TOTAL AREA = 67.0 AC

FOR REFERENCE ONLY:

EPOCA PHASE 1 STORM WATER QUALITY MANAGEMENT REPORT DATED 11/20/2020 AND ANY SUBSEQUENT AMENDMENTS PER PTS#658080

AND

EPOCA PHASE 1 DRAINAGE REPORT DATED 01/18/2021 AND ANY SUBSEQUENT AMENDMENTS PER PTS#658080

BASIN 4

BASIN 1

AIRWAY ROAD

FUTURE AIRWAY ROAD (N.A.P.)

ULTIMATE CONDITION ROW

N.A.P.

VILLAGE WAY

CACTUS ROAD

CENTRAL MAIN STREET

STREET C

SIEMPRE VIVA ROAD

EX SD PER DWG 23871-21-D

11.58 AC
0.20 AC
0.1 AC
0.45 AC
1.21 AC
0.17 AC
0.24 AC
0.22 AC
0.77 AC
0.55 AC
0.62 AC
0.65 AC
0.84 AC
1.11 AC
1.72 AC
0.30 AC
0.64 AC
0.44 AC
0.48 AC
0.26 AC
0.38 AC
3.98 AC
5.15 AC
5.48 AC
0.50 AC
0.36 AC
0.59 AC
0.19 AC
5.75 AC
3.23 AC
3.25 AC
0.99 AC
1.01 AC
0.55 AC
0.72 AC
0.47 AC
0.54 AC
0.35 AC
3.32 AC
0.25 AC
0.24 AC
9.12 AC
0.45 AC
0.43 AC
0.35 AC
0.37 AC
0.72 AC
2.26 AC
1.43 AC
4.23 AC
4.68 AC
0.68 AC
0.17 AC
0.30 AC
0.13 AC
0.28 AC
0.54 AC
0.13 AC
0.20 AC
0.35 AC
1.68 AC
0.71 AC
10.47 AC
2.86 AC
0.66 AC
0.40 AC
2.14 AC

LEGEND

- PROPERTY BOUNDARY
- DRAINAGE SUBAREA
- FLOW DIRECTION
- OVERALL DRAINAGE SYSTEM BOUNDARY
- HYDROLOGY NODE
- AREA FROM UPSTREAM TO DOWNSTREAM NODE (X.XX AC)

NOTE: SUPPLEMENTAL TOPOGRAPY IS 2-FT CONTOURS FROM SANGIS (1997, BEFORE SR 905 WAS BUILT)

SCALE: 1"=80'
JOB #: 2357.80
CREATED: 10/15/19

PREPARED BY:

PROJECT DESIGN CONSULTANTS
Planning | Landscape Architecture | Engineering | Survey
701 B Street, Suite 800
San Diego, CA 92101
619.235.6471 Tel
619.234.0349 Fax

CITY OF SAN DIEGO

LUMINA-OTAY CANYON RANCH

DRAINAGE MAP
PROPOSED CONDITIONS
EXHIBIT B

LEGEND

- DRAINAGE SUBAREA (FROM UPSTREAM TO DOWNSTREAM NODE)
- DRAINAGE SYSTEM BOUNDARY
- DRAINAGE AREA FROM UPSTREAM TO DOWNSTREAM NODE — X.XX AC
- FLOW DIRECTION
- DRAINAGE NODE — XX
- FLOW PATH

N

40 20 0 40 80 120

SCALE: 1"=40'

FOR REFERENCE ONLY:

AIRWAY GARDENS STORM WATER QUALITY MANAGEMENT REPORT DATED 11/24/2020 AND ANY SUBSEQUENT AMENDMENTS PER PTS#669201
AND
AIRWAY GARDENS DRAINAGE REPORT DATED 11/11/2020 AND ANY SUBSEQUENT AMENDMENTS PER PTS#669201

OTAY MESA FREEWAY OFFRAMP

PROJECT BOUNDARY

SYSTEM 1000A

SYSTEM 1000B

SYSTEM 1000C

SYSTEM 1000D

SYSTEM 1000E

SYSTEM 1000F

SYSTEM 1000G

BASIN BR11

BASIN BR12

BASIN BR13

BASIN BR14–15

BASIN BR16–17

BASIN BR18–19

BASIN BR20

BASIN BR RD1

BASIN BR RD2

SOUTH BASIN

COLCHESTER COURT

CONTINENTAL STREET

BRITANNIA BLVD

AIRWAY ROAD

THIS AREA NOT INCLUDED IN PROPOSED CONDITION AS IT IS CURRENTLY BEING PROPOSED FOR DEVELOPMENT UNDER ANOTHER FUTURE PROJECT (PAEZ PROPERTY) AND WILL NOT FLOW INTO PROJECT SITE ONCE DEVELOPED.

FUTURE WIDENINGS ON CONTINENTAL STREET AND AIRWAY ROAD STILL ASSUMED TO FLOW TO SOUTH DETENTION BASIN UPON SEPARATE FUTURE PROJECT COMPLETION.

SYSTEM 1000
AREA=32.3 AC
Q(50)=54.9 CFS
Q(50)det=22.8 CFS

SCALE:	1"=40'	PREPARED BY:	CITY OF SAN DIEGO
JOB #:	4422.00	PROJECT DESIGN CONSULTANTS Planning | Landscape Architecture | Engineering | Survey	AIRWAY GARDENS
CREATED:	5/22/20	701 B Street, Suite 800 San Diego, CA 92101 619.235.6471 Tel 619.234.0349 Fax	DRAINAGE MAP PROPOSED CONDITIONS EXHIBIT C

P:\4422.00\Engr\Reports\Drainage\DWG\4422.00 DR PROP.dwg 11/12/2020 11:27:22 AM

APPENDIX 9

Drainage Study for the Otay Mesa Community Plan Update Report and was prepared by Kimley-Horn and Associates in April 2007 (FOR REFERENCE ONLY)

Drainage Study for the Otay Mesa Community Plan Update

April, 2007

Prepared for:
MNA Consulting
427 C Street, Suite 308
San Diego CA 92101

Prepared by:
Kimley-Horn and Associates, Inc.
517 Fourth Avenue, Suite 301
San Diego CA 92101

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Drainage Study For The Otay Mesa Community Plan Update

April, 2007

Chuck Spinks Exp. Date 03/31/08

R.C.E. 30894

TABLE OF CONTENTS

I. BACKGROUND 1

II. EXISTING DRAINAGE FACILITIES 3

III. HYDROLOGIC ANALYSIS 5

IV. HYDRAULIC ANALYSIS 9

V. PROPOSED DRAINAGE FACILITIES 12

VI. PROPOSED DRAINAGE ALTERNATIVES 14

VII. RECOMMENDED DRAINAGE DESIGN CRITERIA 20

VIII. STORM WATER QUALITY REQUIREMENTS 21

LIST OF EXHIBITS

EXISTING DRAINAGE FACILITIES MAP 4

WATERSHED MAP 7

AES SUMMARY TABLE 8

HEC-RAS MODEL 10

PROPOSED DRAINAGE FACILITIES MAP 13

COST ESTIMATE 16

PRELIMINARY DESIGN PLAN: LA MEDIA CHANNEL AND BORDER DETENTION BASIN 17

PRELIMINARY DESIGN: CHANNEL CROSS SECTION 18

PROPERTY OWNERSHIP MAP 19

RECOMMENDED STORM WATER POLICIES 23

EXAMPLE OF PERMANENT STORM WATER BEST MANAGEMENT PRACTICES 24

STORM WATER REQUIREMENTS CHECKLIST 25

APPENDICES

APPENDIX A AES HYDROLOGY CALCULATIONS

APPENDIX B HEC-1 MODEL

I. BACKGROUND

This report has been prepared as an appendix to the Otay Mesa Community Plan update EIR. Its purpose is to provide a summary of the existing drainage situation and facilities and proposed future facilities, including alternatives for draining the large central watershed. In addition, this report presents recommendations for drainage design criteria and storm water quality requirements for each of the watersheds on the Mesa. A detailed pre-design report to be approved by the City of San Diego will be required before initiating the design.

For most of its early history, Otay Mesa was used for agriculture and farming was the primary land use. As industrial and commercial development started taking place in the 1960s, the City of San Diego recognized the need for a comprehensive drainage Master Plan for the Mesa. Because most of the Mesa drains to the South into Mexico, there was concern that the new development would increase the runoff crossing the border. The City needed to establish criteria for the new development such that there was no increase in runoff as a result of the new construction.

In May of 1987, the City Council approved a contract to prepare the Otay Mesa Drainage Master Plan. In August of 1987, the City published a Notice to "All Private Engineers" that established "Drainage Requirements for Development in Otay Mesa" (attached). The Master Plan was published in January, 1988, and included a proposed concrete Channel from Airway Road to Siempre Viva Road that followed the existing drainage channel.

The Master Plan was updated with the "Otay Mesa Drainage Study" published in August, 1999. The most significant recommendation change was moving the proposed new channel from the creek alignment to a new location directly adjacent to La Media Road and Siempre Viva Road. This report utilizes the hydrologic models and analyses prepared for the 1999 Master Plan.

Reproduction of 1987 NOTICE from Engineering and Development Department

NOTICE

Date: August 7, 1987

To: All Private Engineers

From: Subdivision Engineer

Subject: Drainage requirements for development in Otay Mesa

In order to minimize the effects of increased storm water runoff in Mexico, due to development of property in Otay Mesa, all property in Otay Mesa that is within the water shed that drains into Mexico, shall be developed with the following requirements:

1. Each property owner shall provide storm water detention facilities so that there will be no increase in the rate of runoff due to development of the property.

2. The detention facilities shall be designed so that the rate of runoff from the property will not be greater after development than it was before development for a 5 year, 10 year, 25 year and 50 year storm.

3. All drainage facilities crossing four-lane major or higher classification streets shall be designed for a Q100 (existing). Other facilities, except the major channel referred to in paragraph 5, may be designed for Q50 (existing).

4. The Drainage Design Manual shall be used as guidelines for design of drainage facilities and computing design discharges.

5. The City Engineer's Office, Flood Control Section, is preparing a preliminary plan for the main north-south channel from Otay Mesa Road near La Media to the Mexican Border. The preliminary design will include the design "Q" (Q100 existing), the invert grade, and the water surface elevation at the major road crossings.

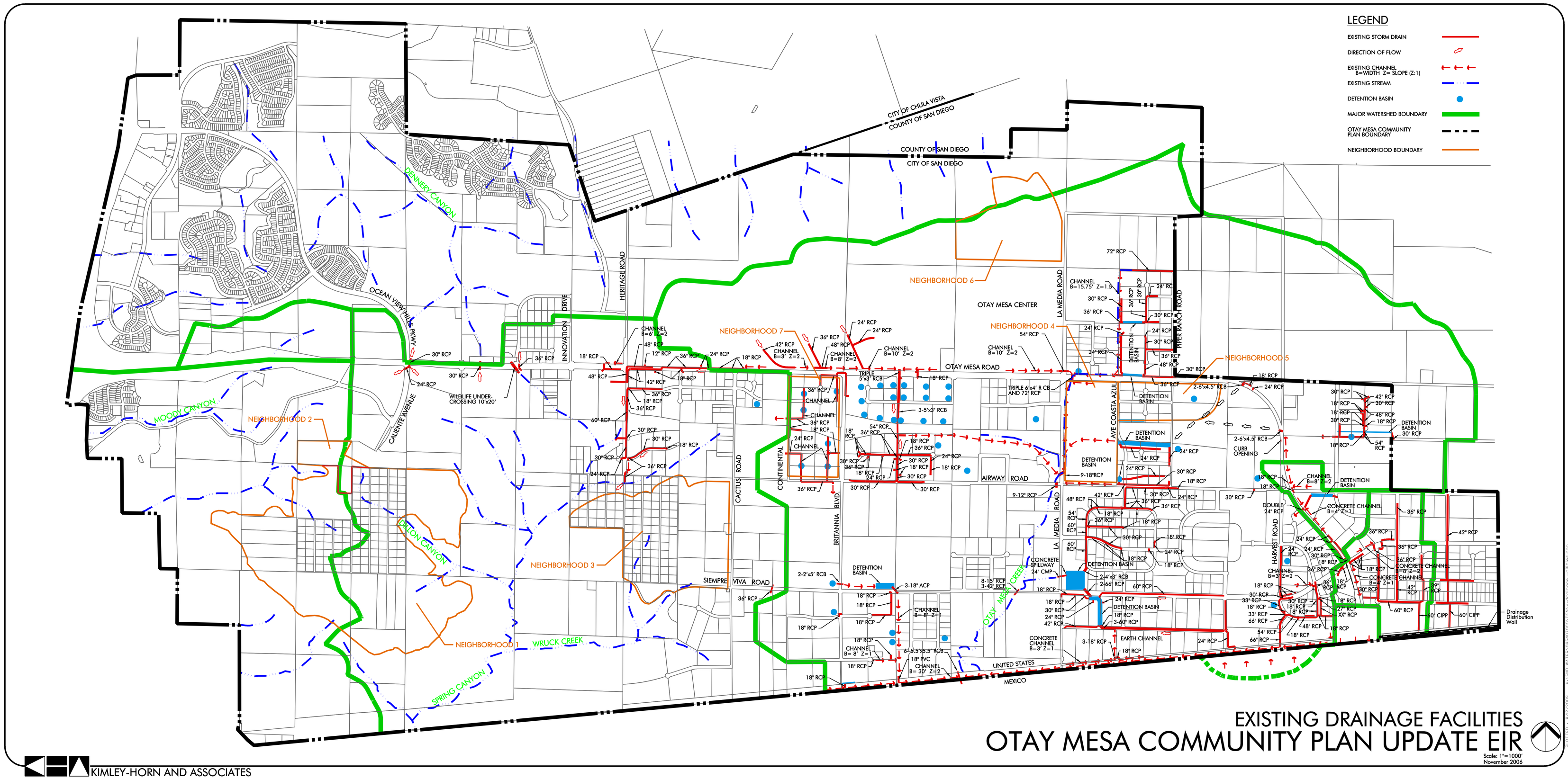
C.R. Lockhead
Subdivision Engineer

II. EXISTING DRAINAGE FACILITIES

Information was collected for existing drainage and flood control facilities on Otay Mesa through as-built plans, SanGIS maps, and site visits. Most of the existing drainage facilities were constructed as part of the private development that is taking place on the Mesa. Many of these facilities are not continuous because of the piecemeal nature of the development. This creates challenges for the subsequent developers that need to tie into the existing facilities. Many of the existing facilities are temporary. We were not able to obtain details on the drainage facilities in Mexico that receive most of the runoff.

Most of the development to-date has occurred in the East Watershed, which therefore includes most of the existing drainage facilities on the Mesa. The existing system is a combination of storm drains, improved channels, and detention basins, which in many areas discharge to natural drainage paths that do not have adequate hydraulic capacity.

The "Existing Drainage Facilities" drawing shows the facilities as-of the date of this report. The area is developing rapidly, and therefore new facilities are continuously being constructed. There are currently no dedicated drainage rights-of-way on the Mesa. Many of the projects, as they were mapped and constructed, dedicated portions of the properties to the city as drainage easements or flood water storage easements. Eventually, the systems and their easements will be continuous.



EXISTING DRAINAGE FACILITIES
OTAY MESA COMMUNITY PLAN UPDATE EIR

Scale: 1"=1000'
November 2006

KIMLEY-HORN AND ASSOCIATES

III. HYDROLOGIC ANALYSIS

The Otay Mesa Study area is shown on the Watershed Map, and includes all of the Mesa area within the City of San Diego divided into five watersheds (with the exception of the far northwest arm of the Mesa, which is fully developed).

Watersheds	Acres	mi^2
West Perimeter Watershed	258	0.40
West Watershed	2,190	3.42
North Perimeter Watershed	590	0.92
East Watershed	3,864	6.04
Border Crossing Watershed	223	0.35
TOTAL	7,125	11.13

Most of the Mesa slopes from North to South, with the flow entering Mexico at several points. The northern and western perimeters of the Mesa flow into the adjacent Canyons. These perimeter watersheds are divided into several independent smaller watersheds. The watershed boundaries on the Mesa are not well defined because the Mesa is so flat. There are very few defined natural drainage paths, with much of the runoff sheet-flowing across the Mesa. The watershed boundaries shown are based on field investigations and best available mapping, but the actual drainage boundaries may be very different.

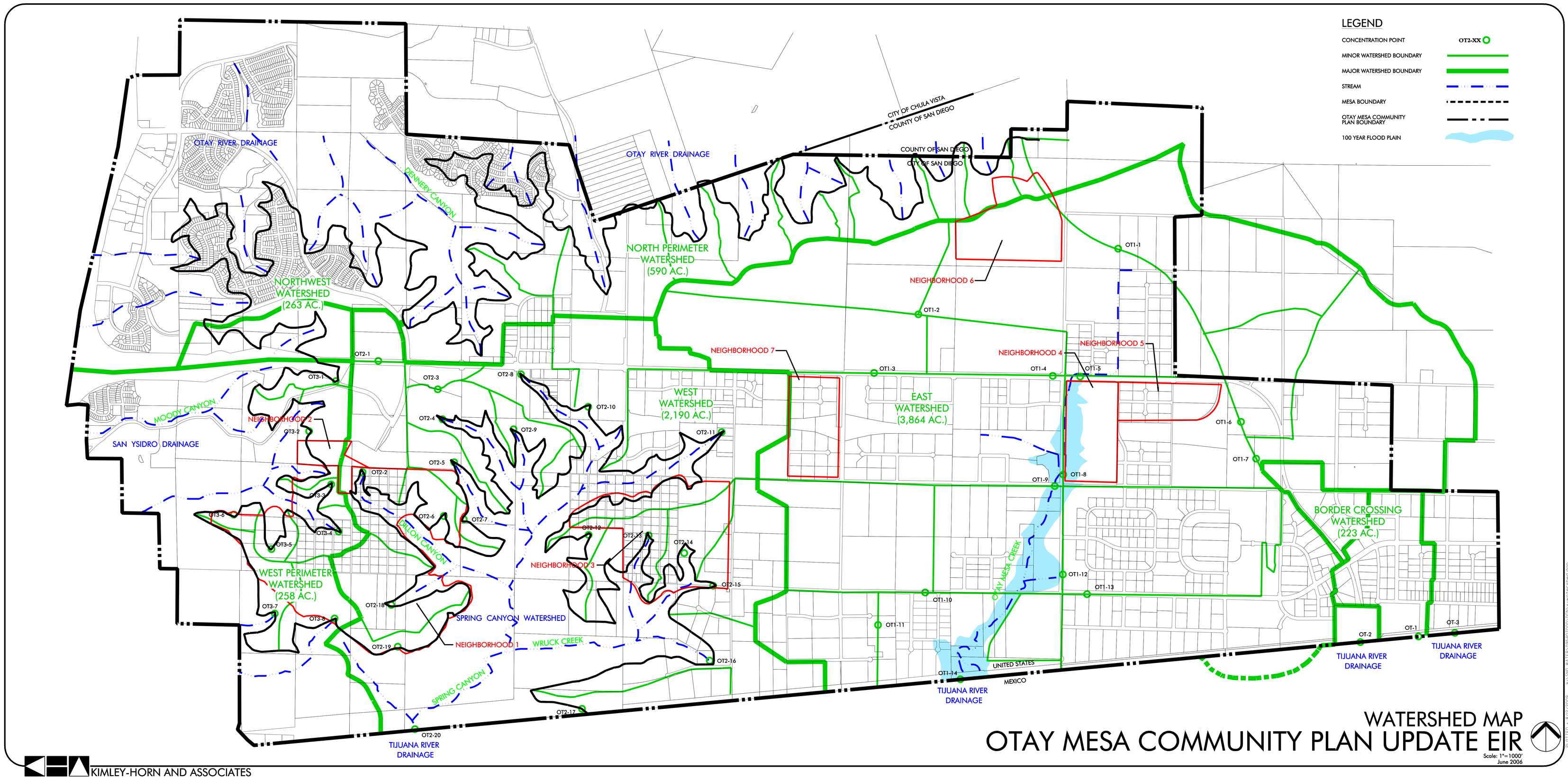
The only watershed that has been studied significantly from a drainage perspective is the East Watershed. Hydrologic models have been prepared for both of the previous drainage studies. The peak flows calculated in the two studies are different, primarily because of different assumptions relative to developed area, proposed drainage facilities, and watershed areas. The East Watershed includes a large area of unincorporated County property. The hydrologic model assumed the same industrial development for the unincorporated area. If land uses change in the County area, it may change the runoff rates. The differences for the concentration point at the border are shown below.

Q100 at Border East Watershed		
	Area (mi^2)	Q100(cfs)
1988 Study	5.72	5,050
1999 Study	6.63	3,529
2004 CPU	6.78	3,673

As part of this study, new hydrologic models have been prepared for the main watersheds which flow into the Tijuana River. For the East Watershed, HEC-1 has been used, since both previous studies used this model. For the other watersheds, the standard City of San Diego Modified Rational Method (AES) has been used. The results of these analyses are shown in the table below.

Hydrologic Analysis Summary			
	Area (mi^2)	Q50(cfs)	Q100(cfs)
West Perimeter Watershed	0.40	170	444
West Watershed	3.42	672	1,676
East Watershed	6.78	1,280	3,673
	10.60	2,122	5,793

In addition to the above flows, the Spring Canyon open space area contributes 109 cfs (Q50) and 257 cfs (Q100) from 1.2 mi^2. Since the Tijuana River Watershed is a water-quality impacted watershed, the quality and quantity of flow will need to be addressed before additional development takes place.



KIMLEY-HORN AND ASSOCIATES

WATERSHED MAP
OTAY MESA COMMUNITY PLAN UPDATE EIR

Scale: 1"=1000'
June 2006

PLOTTED: 3/07/2008 9:43:50 AM BY: DSPENCER N:\SDD_JOBS\069670\GRAPHICS\EIR\WATERSHED.dgn

WATERSHED	CONCENTRATION POINT	AREA (ACRES)	Q_{50}	Q_{100}
WEST PERIMITER	OT3-1	19.4	18.3	51.4
	OT3-1A	14.8	12.0	32.1
	OT3-2	47.1	26.7	67.3
	OT3-3	11.8	10.6	29.3
	OT3-4	35.0	22.4	57.5
	OT3-5	16.5	13.3	35.8
	OT3-6	12.2	10.9	30.3
	OT3-7	46.1	27.7	70.4
	OT3-8	51.4	27.7	69.4
		254.3	**169.5**	**443.5**
WEST	OT2-1	33.3	17.1	42.6
	OT2-2	126.2	41.4	99.5
	OT2-18	97.1	47.7	118.2
	OT2-19	27.7	22.3	60.1
	OT2-3	20.1	14.6	38.4
	OT2-4	67.8	38.5	96.9
	OT2-5	40.8	20.1	49.7
	OT2-6	34.8	17.1	42.4
	OT2-7	14.9	17.9	43.2
	OT2-8	81.3	43.0	108.7
	OT2-9	36.9	23.6	60.6
	OT2-9A	12.9	11.5	31.8
	OT2-10	128.4	43.1	103.8
	OT2-11	275.6	112.2	279.9
	OT2-12	23.6	17.5	46.0
	OT2-13	61.5	42.1	109.3
	OT2-14	48.4	26.1	65.3
	OT2-15	153.8	57.2	138.8
	OT2-16	121.7	40.8	98.4
	OT2-17	60.3	17.8	42.5
		1467.1	**671.6**	**1676.1**
MEXICO	Canyon Area	**774.8**	**109.3**	**257:0**

May 23, 2005

IV. HYDRAULIC ANALYSIS

Most of the Mesa is very flat, resulting in local flooding during storms at the low points and along some drainage ditches. The only significant creek on the Mesa is the main channel in the East Watershed, Otay Mesa Creek, which flows from North to South along La Media Road and crosses the border into Mexico just north of the Tijuana Airport.

A HEC-RAS hydraulic model was prepared for this channel from the border north to Otay Mesa Road. The purpose of this model was to identify the 100-year floodplain for this reach for present conditions. The proposed future drainage project along this alignment will be designed to contain the 100-year flow, reducing or eliminating flooding impacts to adjacent properties.

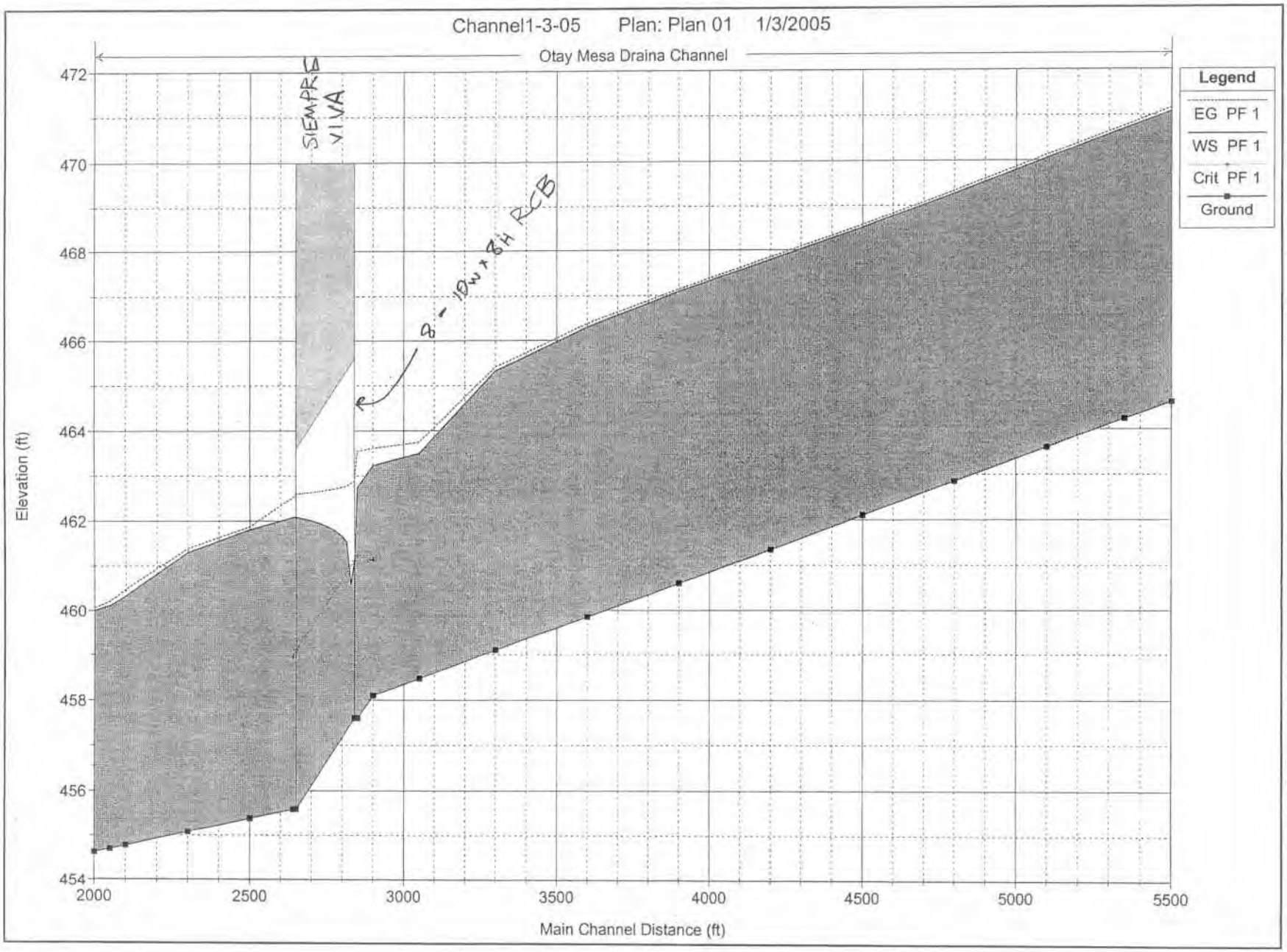
The HEC-RAS model was also used to size the proposed new channel from Airway Road to just south of Siempre Viva Road. Several alternative cross-sections were modeled to reflect input on the environmental aspects of the channel.

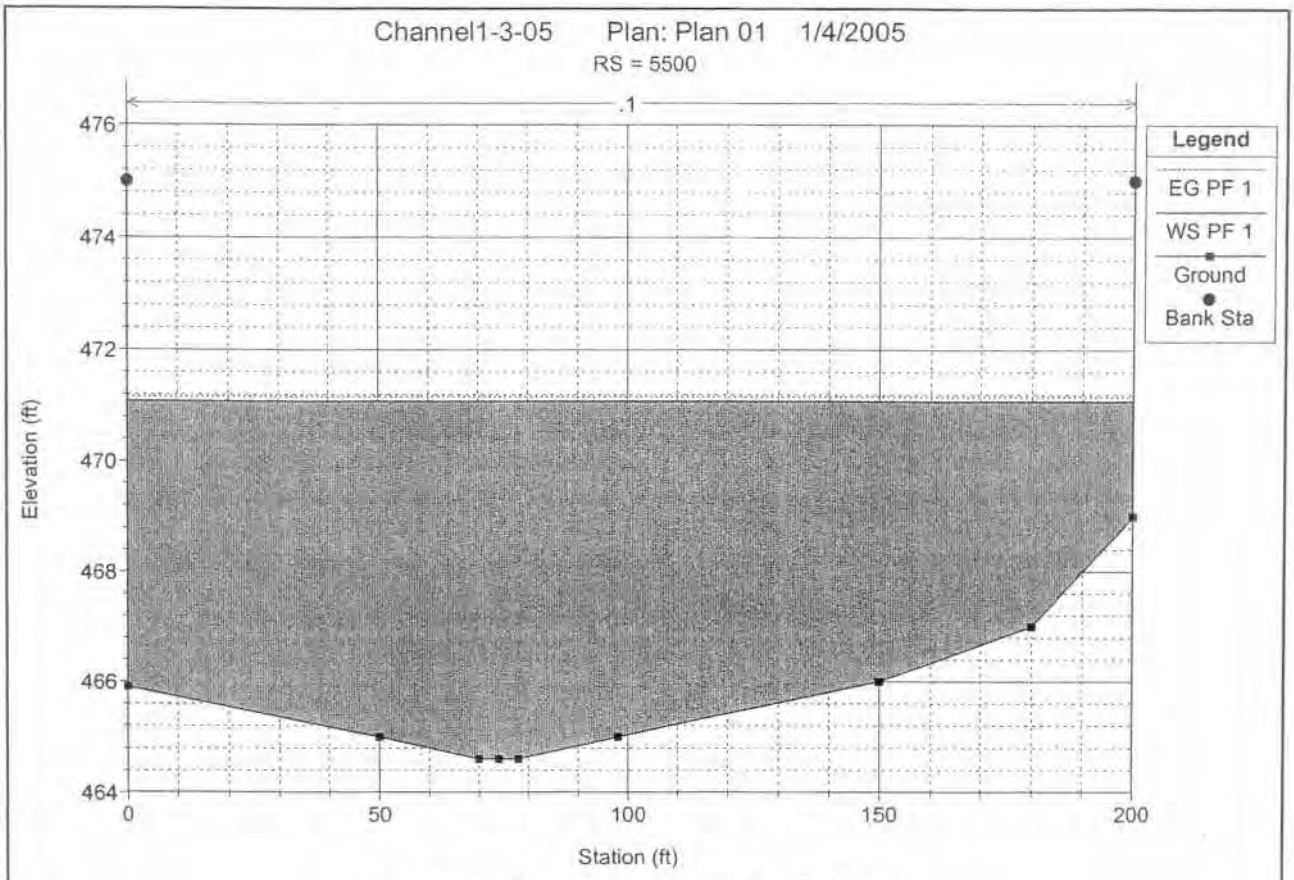
A significant tributary to the main channel enters just upstream of the Siempre Viva Road crossing. This tributary conveys flow from the De La Fuente Business Park and the Siempre Viva Business Park. The existing channel from La Media Road to the proposed main channel is approximately 15 feet wide and 4 feet deep, with a hydraulic capacity of approximately 120 cfs. The 100 year flow in this channel is 1116 cfs. A proposed new channel has a 50 ft bottom width with 1.5:1.0 side slopes and will convey the 100 year flow. A double 10' x 4.5' RCB will also be required for the flow under La Media Road. The cost estimate does not include these facilities.

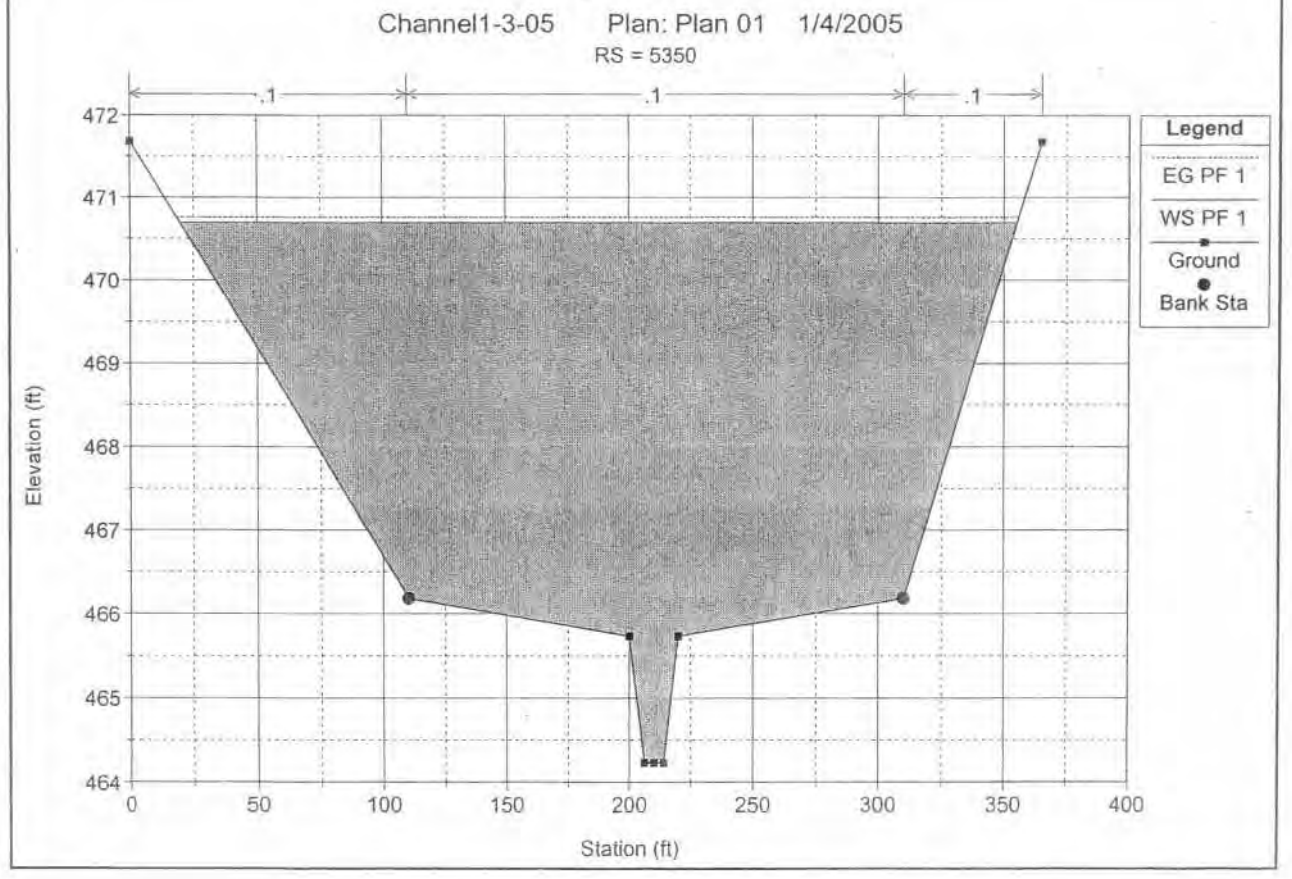
OTAY MESA CPU 1-405

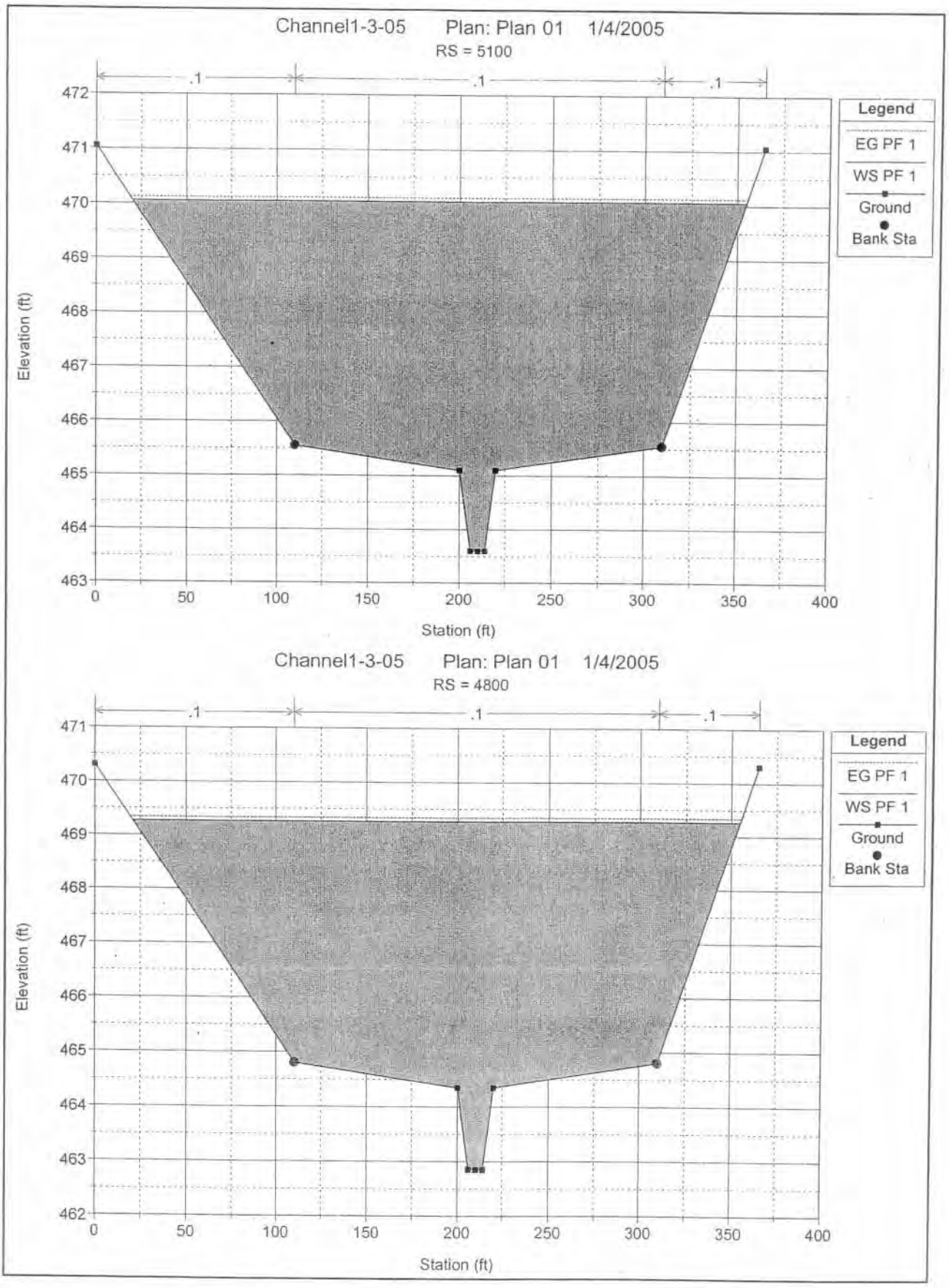
HEC-RAS Plan: Plan 01 River: Otay Mesa Draina Reach: Channel Profile: PF 1

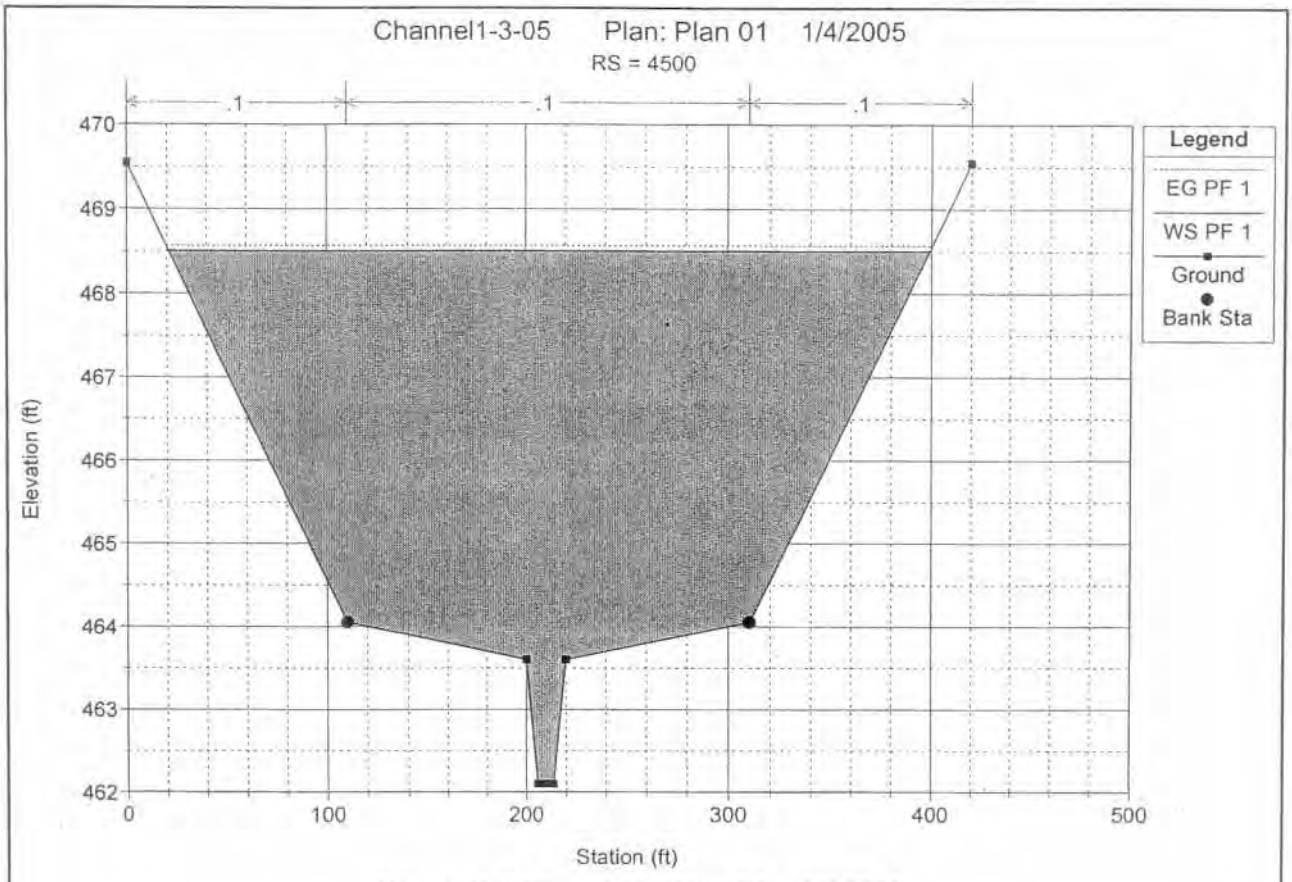
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Channel	5500	PF 1	2500.00	464.60	471.08		471.16	0.002743	2.33	1073.59	200.00	0.18
Channel	5350	PF 1	2500.00	464.23	470.69		470.76	0.002572	2.16	1279.19	335.44	0.17
Channel	5100	PF 1	2500.00	463.60	470.06		470.12	0.002591	2.17	1275.99	335.16	0.17
Channel	4800	PF 1	2500.00	462.85	469.27		469.33	0.002666	2.19	1263.56	334.04	0.18
Channel	4500	PF 1	2500.00	462.10	468.51		468.56	0.002430	2.08	1358.84	378.24	0.17
Channel	4200	PF 1	2500.00	461.35	467.79		467.85	0.002365	2.07	1371.79	379.61	0.17
Channel	3900	PF 1	2500.00	460.60	467.09		467.15	0.002266	2.04	1392.50	381.79	0.16
Channel	3600	PF 1	2500.00	459.85	466.30		466.37	0.002969	2.32	1153.04	281.59	0.19
Channel	3300	PF 1	2500.00	459.10	465.33		465.42	0.003423	2.41	1109.99	285.62	0.20
Channel	3050	PF 1	3000.00	458.48	463.50		463.74	0.014532	4.06	777.90	261.33	0.39
Channel	2900	PF 1	3000.00	458.10	463.23	461.14	463.61	0.000245	4.97	603.31	222.92	0.41
Channel	2850	PF 1	3000.00	457.60	462.74	461.24	463.55	0.000521	7.22	415.32	168.05	0.58
Channel	2750		Culvert									
Channel	2640	PF 1	3000.00	455.59	462.07	458.95	462.52	0.011957	5.38	557.46	183.64	0.37
Channel	2500	PF 1	3000.00	455.38	461.81		461.87	0.001846	2.07	1492.22	277.64	0.15
Channel	2300	PF 1	3000.00	455.08	461.31		461.40	0.003272	2.45	1261.91	277.98	0.19
Channel	2100	PF 1	3000.00	454.78	460.34		460.48	0.006864	3.05	1006.36	275.43	0.27
Channel	2050	PF 1	3000.00	454.70	460.11		460.21	0.003838	2.56	1191.75	275.37	0.21
Channel	2000	PF 1	3000.00	454.63	460.00	456.55	460.06	0.002196	2.06	1582.39	378.00	0.16


Channel1-3-05 Plan: Plan 01 1/3/2005
Otay Mesa Draina Channel
Legend
EG PF 1
WS PF 1
Crit PF 1
Ground
SIEMPRE VIVA
Qb = 18W x 8H RCB
Elevation (ft)
Main Channel Distance (ft)
472
470
468
466
464
462
460
458
456
454
2000
2500
3000
3500
4000
4500
5000
5500


Channel1-3-05 Plan: Plan 01 1/4/2005
RS = 5500
.1
Legend
EG PF 1
WS PF 1
Ground
Bank Sta
Elevation (ft)
476
474
472
470
468
466
464
0
50
100
150
200
Station (ft)


Channel1-3-05 Plan: Plan 01 1/4/2005
RS = 5350
.1
.1
.1
Legend
EG PF 1
WS PF 1
Ground
Bank Sta
Elevation (ft)
472
471
470
469
468
467
466
465
464
0
50
100
150
200
250
300
350
400
Station (ft)


Channel1-3-05 Plan: Plan 01 1/4/2005
RS = 5100
.1
.1
.1
Legend
EG PF 1
WS PF 1
Ground
Bank Sta
Elevation (ft)
472
471
470
469
468
467
466
465
464
463
0
50
100
150
200
250
300
350
400
Station (ft)
Channel1-3-05 Plan: Plan 01 1/4/2005
RS = 4800
.1
.1
.1
Legend
EG PF 1
WS PF 1
Ground
Bank Sta
Elevation (ft)
471
470
469
468
467
466
465
464
463
462
0
50
100
150
200
250
300
350
400
Station (ft)


Channel1-3-05 Plan: Plan 01 1/4/2005
RS = 4500
.1
.1
.1
Legend
EG PF 1
WS PF 1
Ground
Bank Sta
Elevation (ft)
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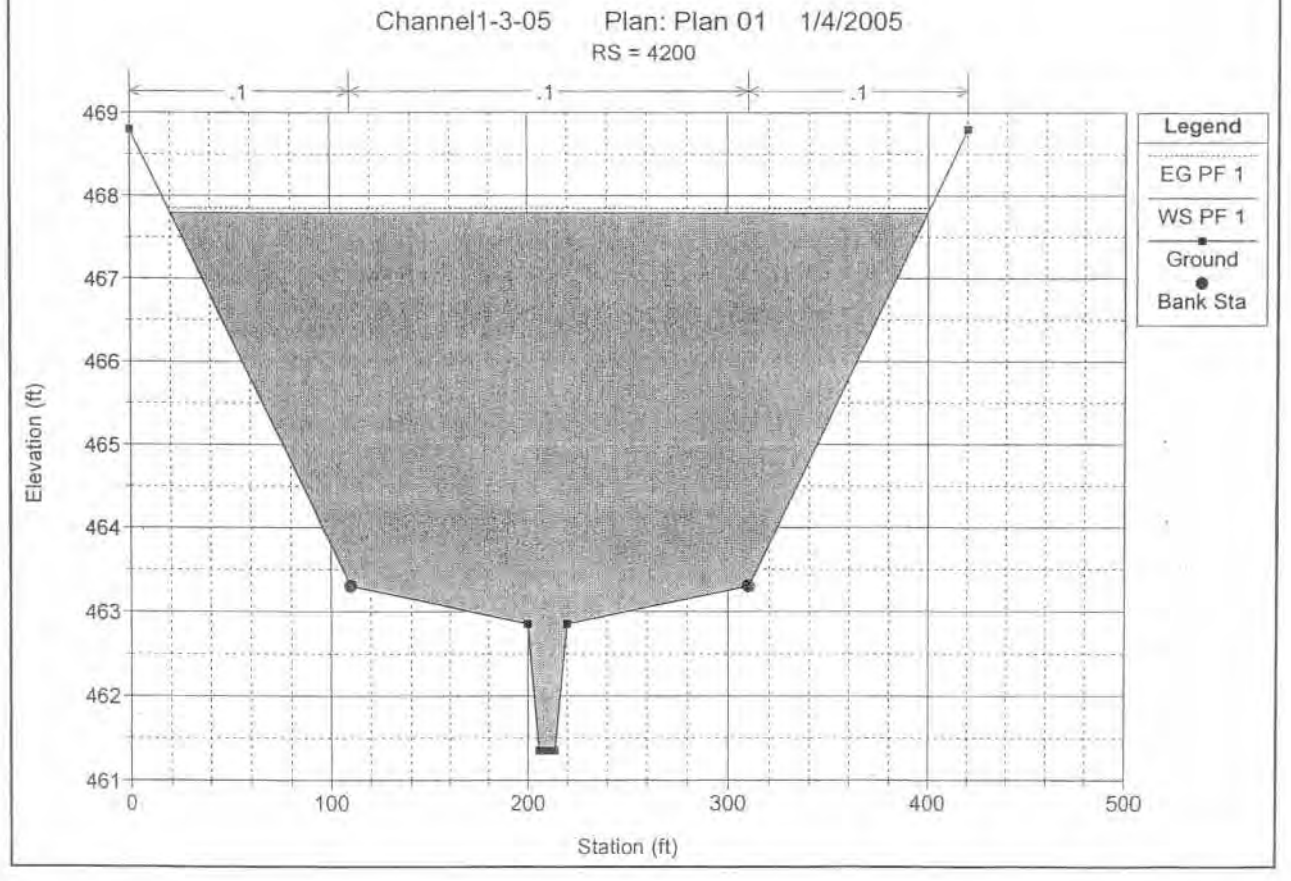
469
468
467
466
465
464
463
462
0
100
200
300
400
500
Station (ft)


Channel1-3-05 Plan: Plan 01 1/4/2005
RS = 4200
.1
.1
.1
Legend
EG PF 1
WS PF 1
Ground
Bank Sta
Elevation (ft)
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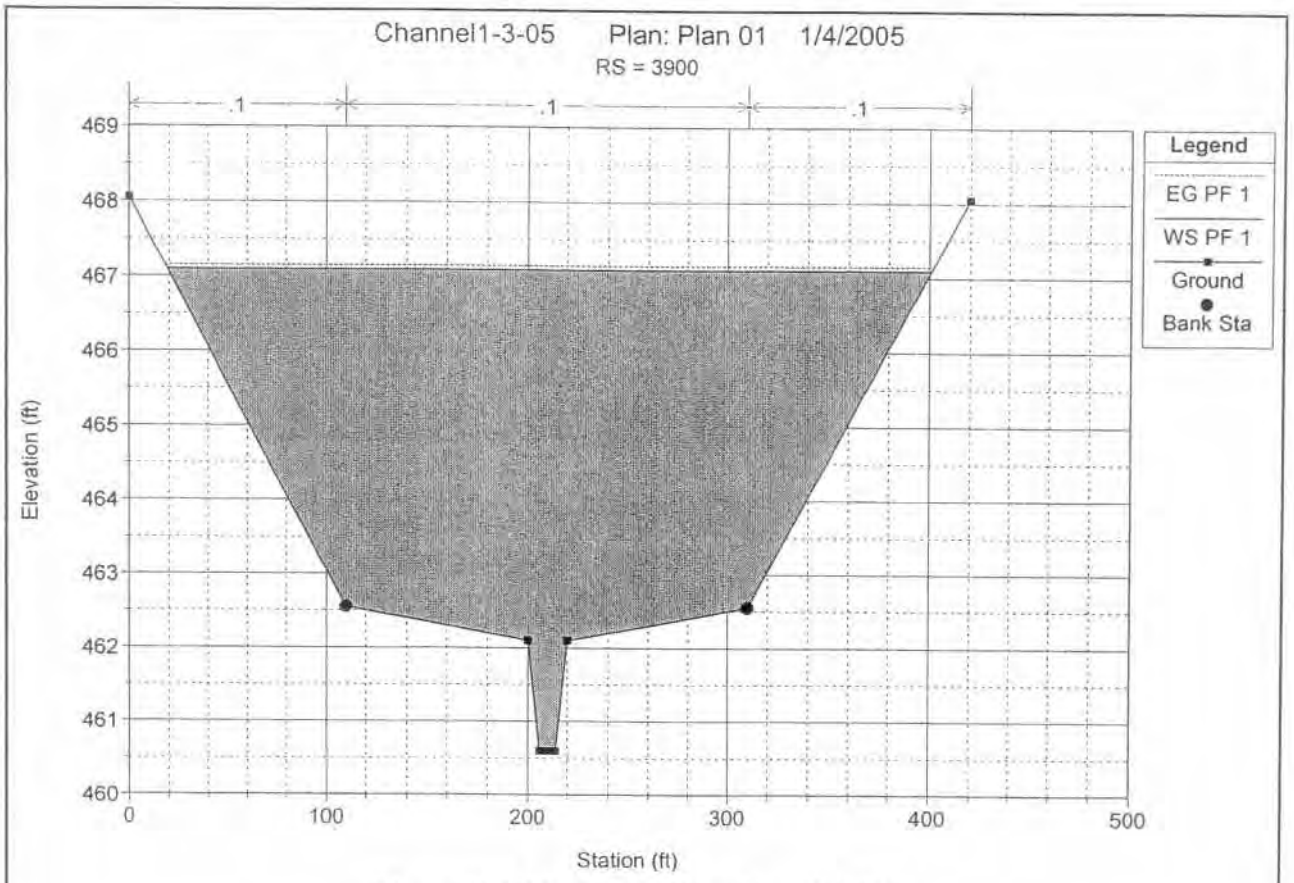
468
467
466
465
464
463
462
461
0
100
200
300
400
500
Station (ft)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RS = 3900
.1
.1
.1
Legend
EG PF 1
WS PF 1
Ground
Bank Sta
Elevation (ft)
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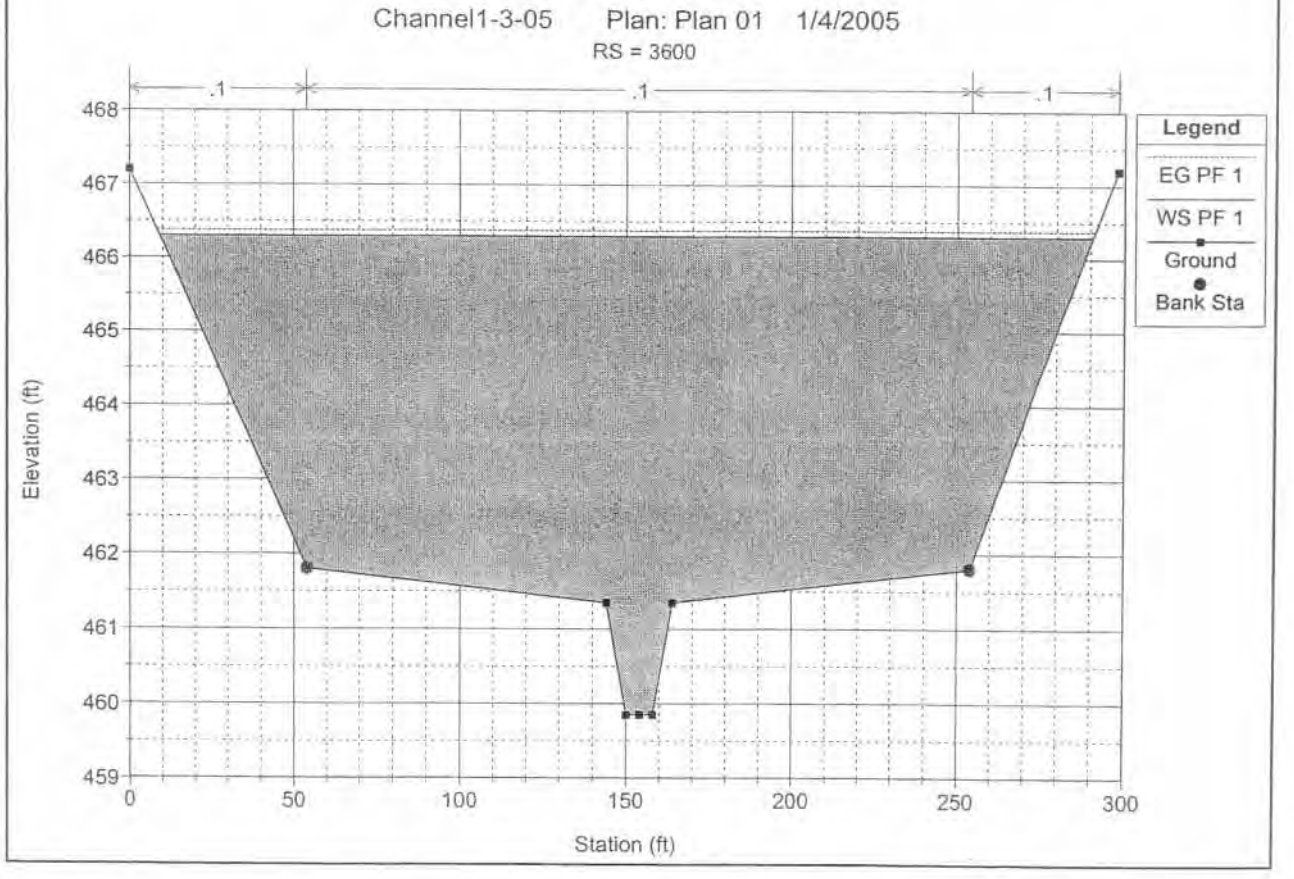
468
467
466
465
464
463
462
461
460
0
100
200
300
400
500
Station (ft)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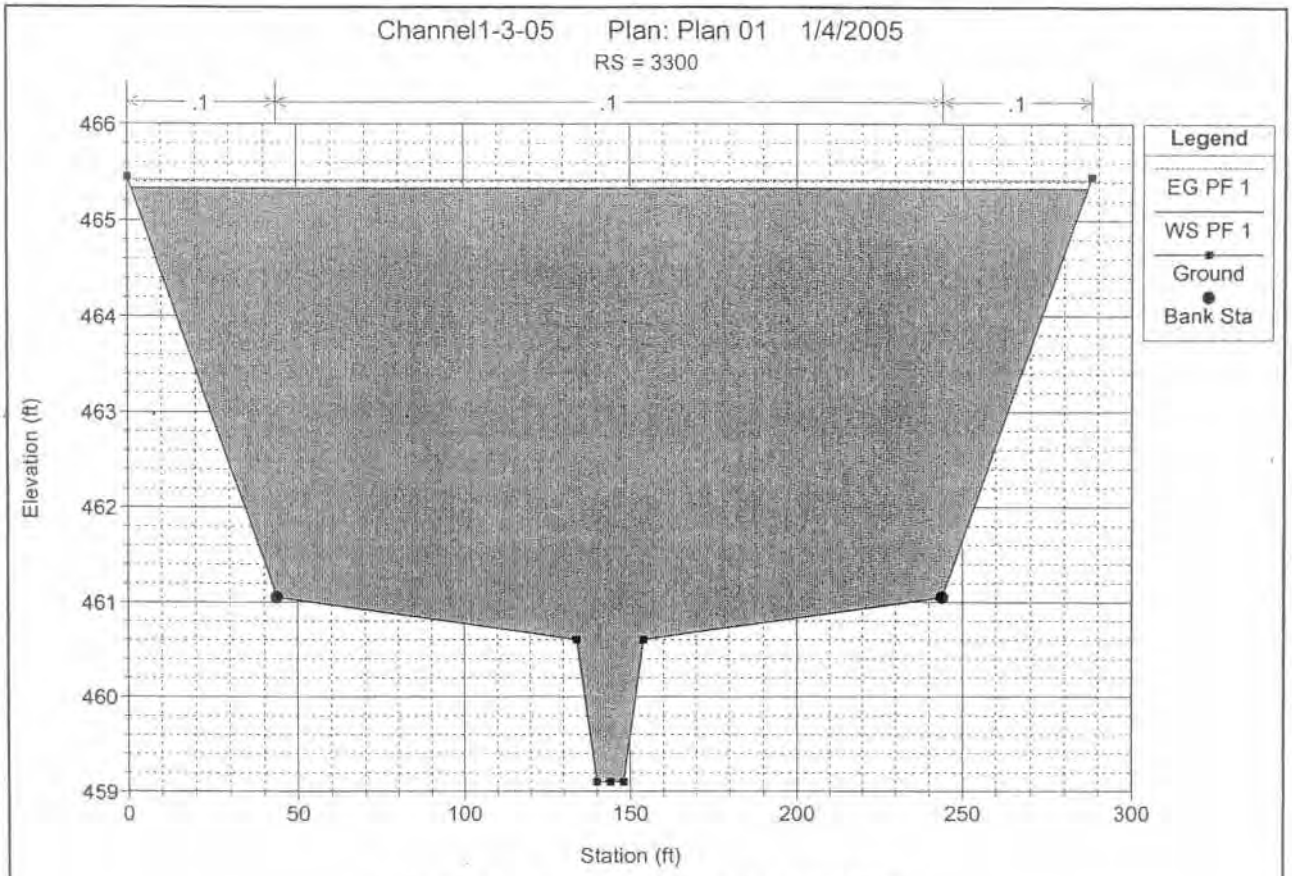
RS = 3600
.1
.1
.1
Legend
EG PF 1
WS PF 1
Ground
Bank Sta
Elevation (ft)
468
467
466
465
464
463
462
461
460
459
0
50
100
150
200
250
300
Station (ft)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RS = 3300
.1
.1
.1
466
465
464
463
462
461
460
459
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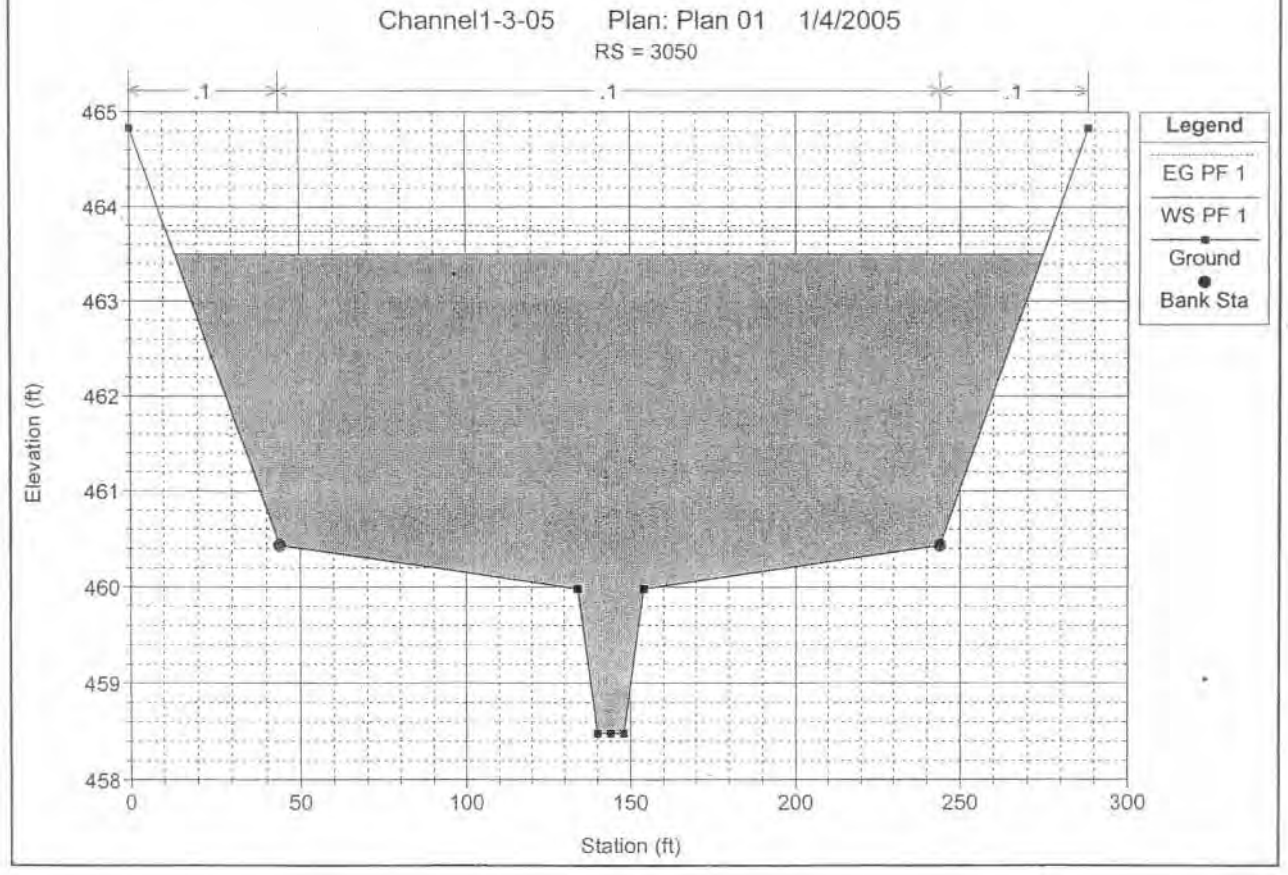
100
150
200
250
300
Elevation (ft)
Station (ft)
Legend
EG PF 1
WS PF 1
Ground
Bank Sta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RS = 3050
.1
.1
.1
465
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463
462
461
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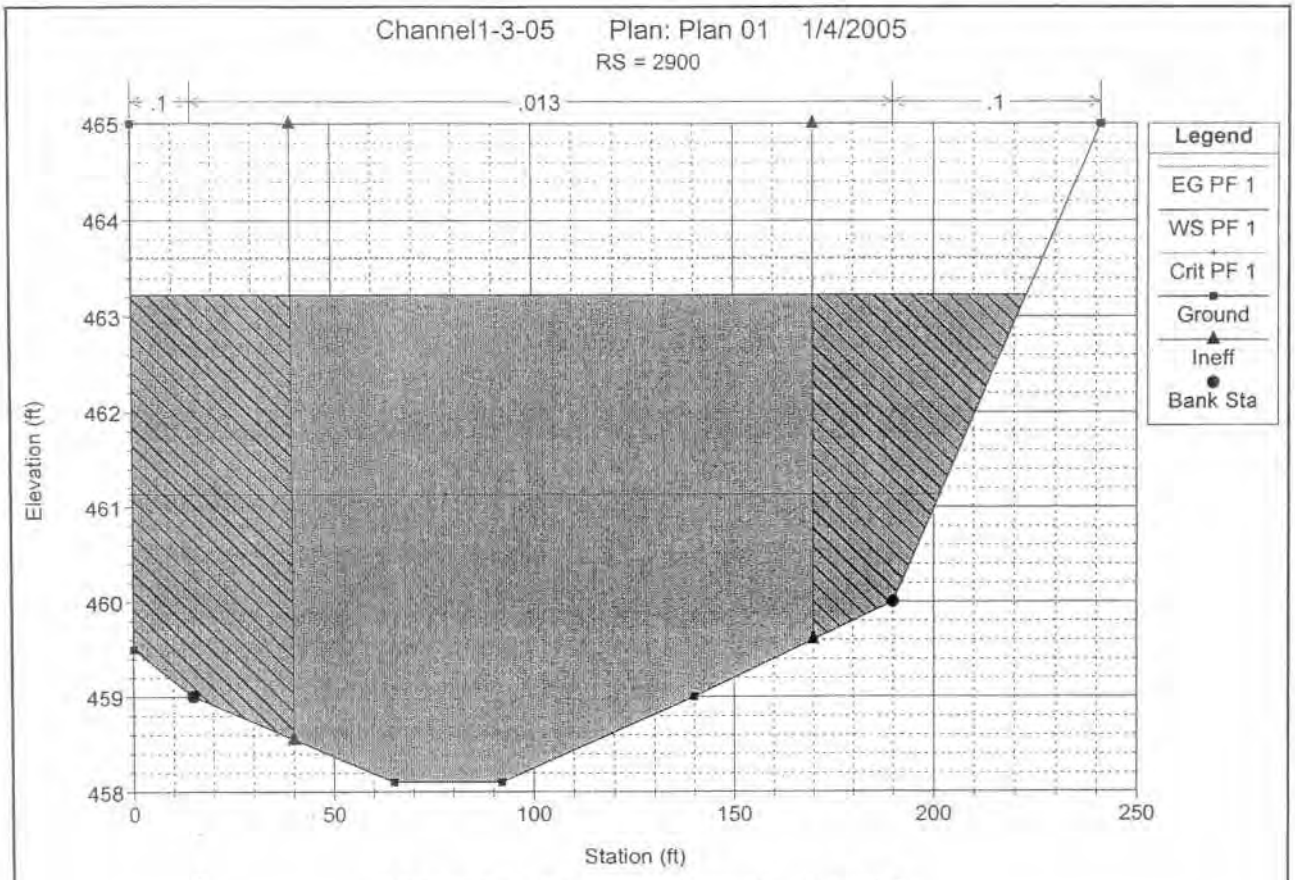
150
200
250
300
Elevation (ft)
Station (ft)
Legend
EG PF 1
WS PF 1
Ground
Bank Sta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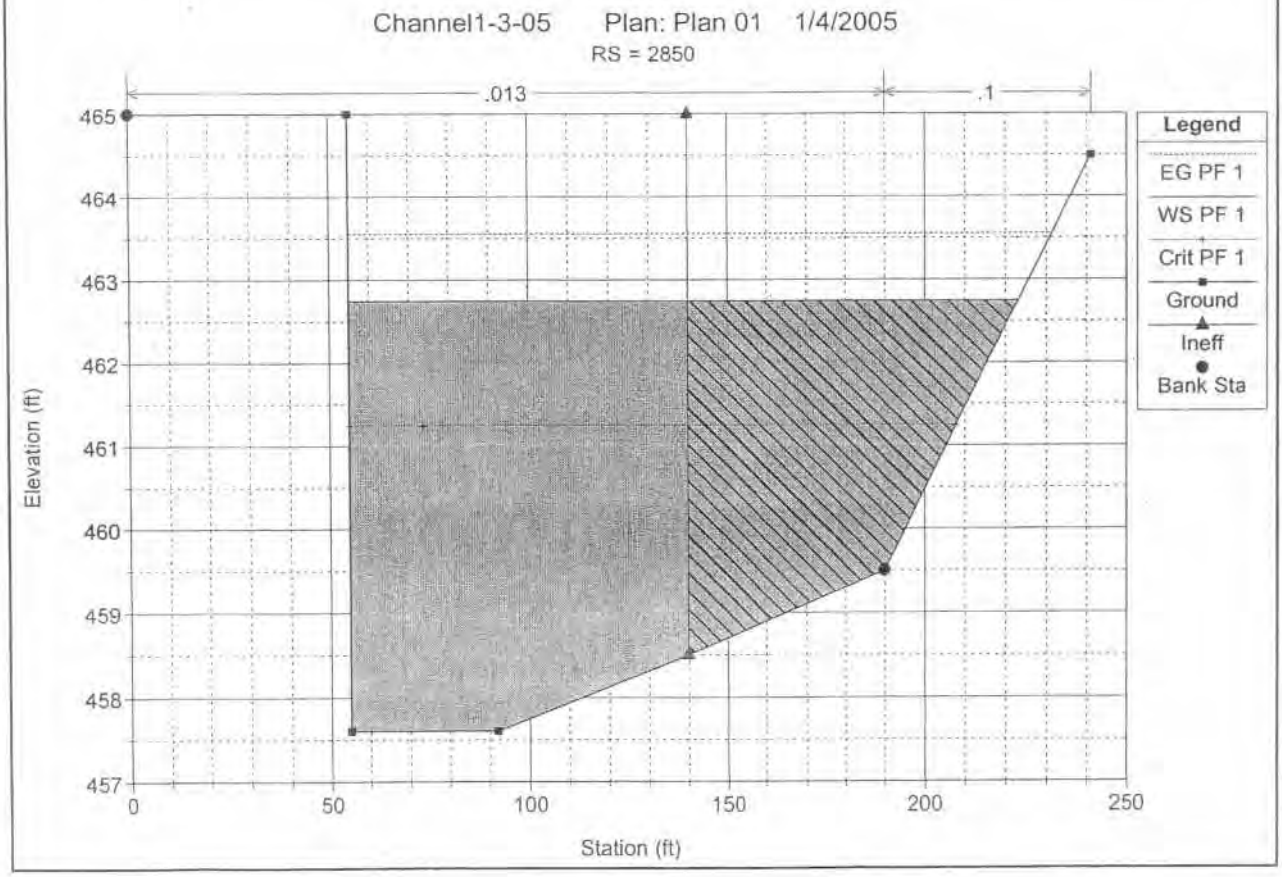
RS = 2900
.1
.013
.1
Legend
EG PF 1
WS PF 1
Crit PF 1
Ground
Ineff
Bank Sta
Elevation (ft)
465
464
463
462
461
460
459
458
0
50
100
150
200
250
Station (ft)


Channel1-3-05 Plan: Plan 01 1/4/2005
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Legend
EG PF 1
WS PF 1
Crit PF 1
Ground
Ineff
Bank Sta
Elevation (ft)
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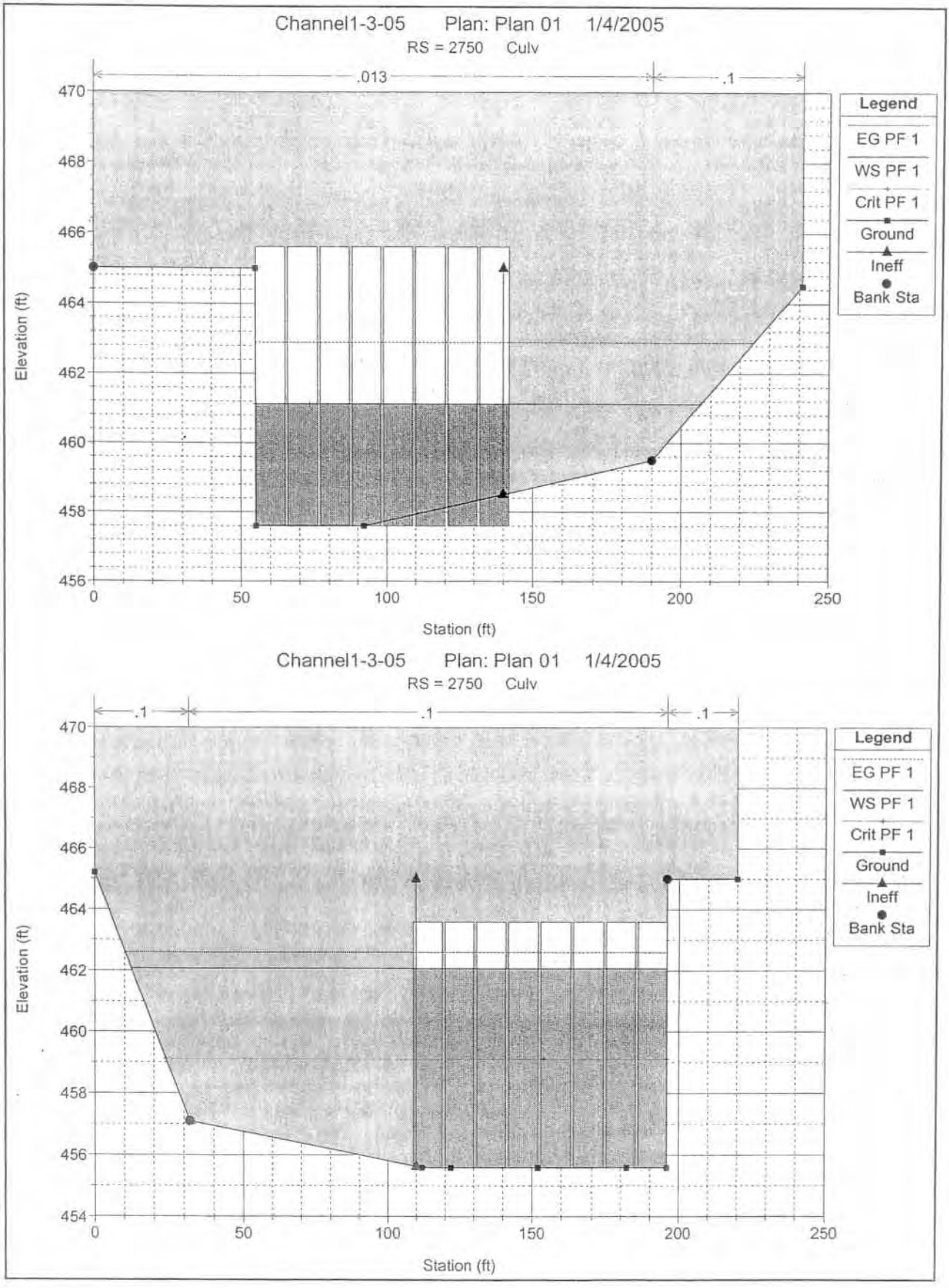
464
463
462
461
460
459
458
457
0
50
100
150
200
250
Station (ft)


Channel1-3-05 Plan: Plan 01 1/4/2005
RS = 2750 Culv
.013
.1
Legend
EG PF 1
WS PF 1
Crit PF 1
Ground
Ineff
Bank Sta
Elevation (ft)
Station (ft)
470
468
466
464
462
460
458
456
0
50
100
150
200
250
Channel1-3-05 Plan: Plan 01 1/4/2005
RS = 2750 Culv
.1
.1
.1
Legend
EG PF 1
WS PF 1
Crit PF 1
Ground
Ineff
Bank Sta
Elevation (ft)
Station (ft)
470
468
466
464
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0
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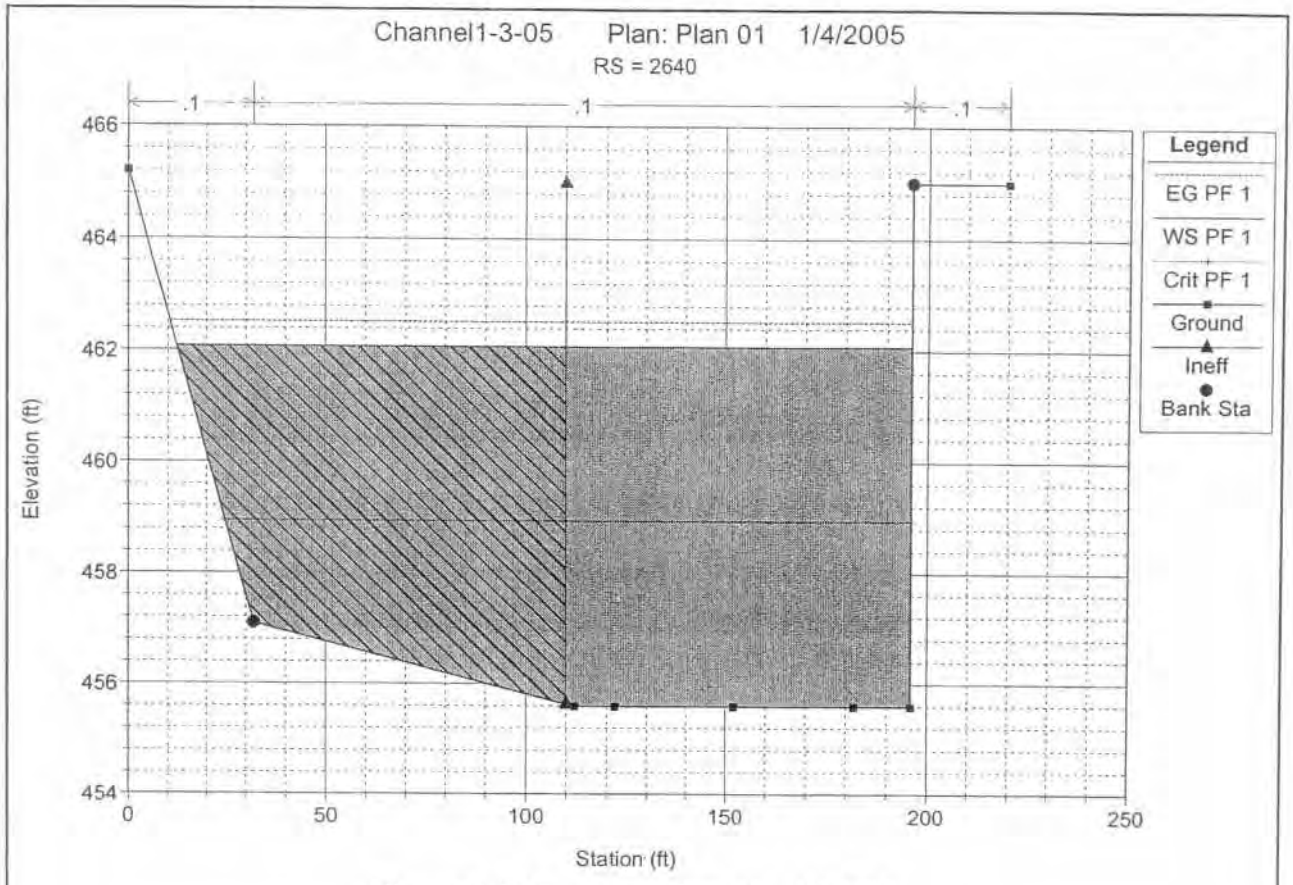
100
150
200
250


Channel1-3-05 Plan: Plan 01 1/4/2005
RS = 2640
.1
.1
.1
466
464
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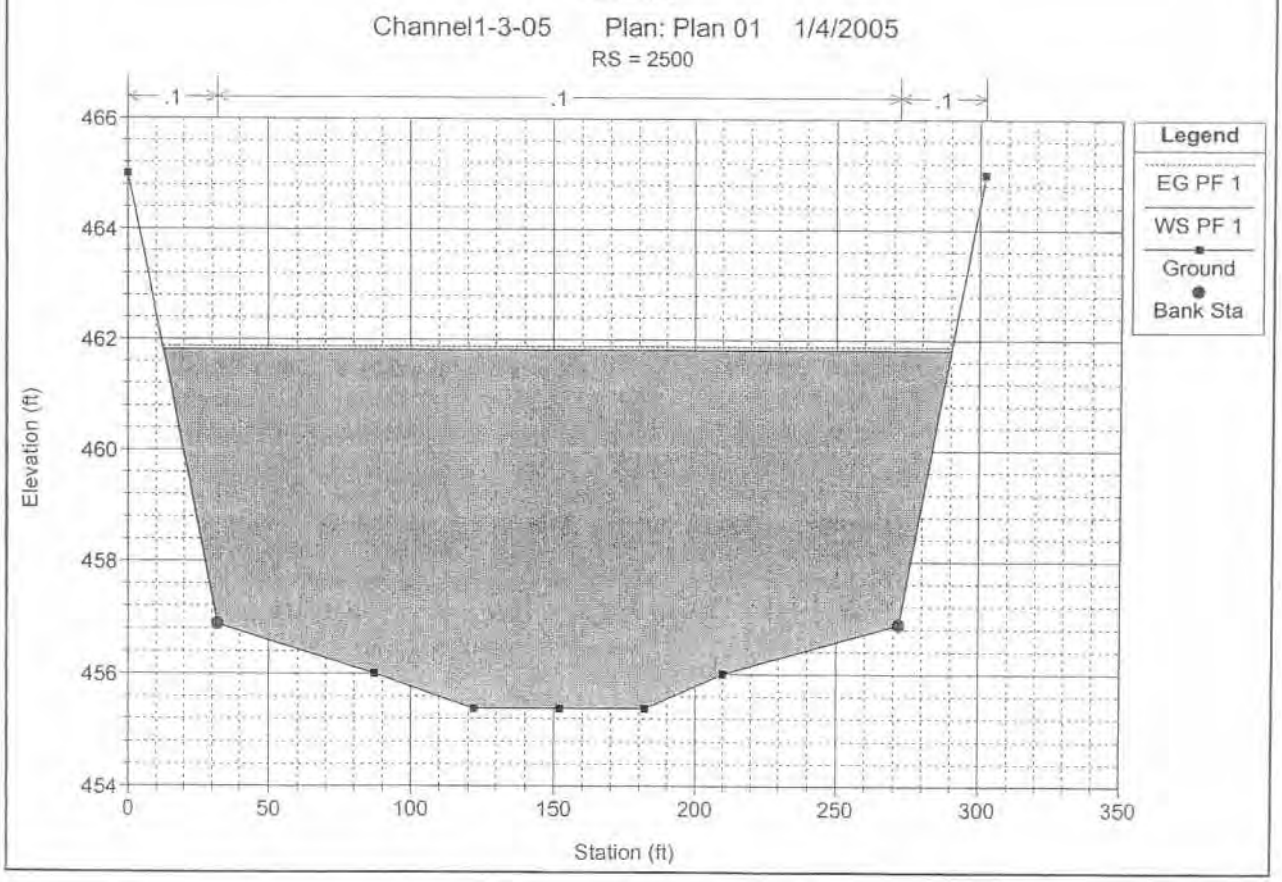
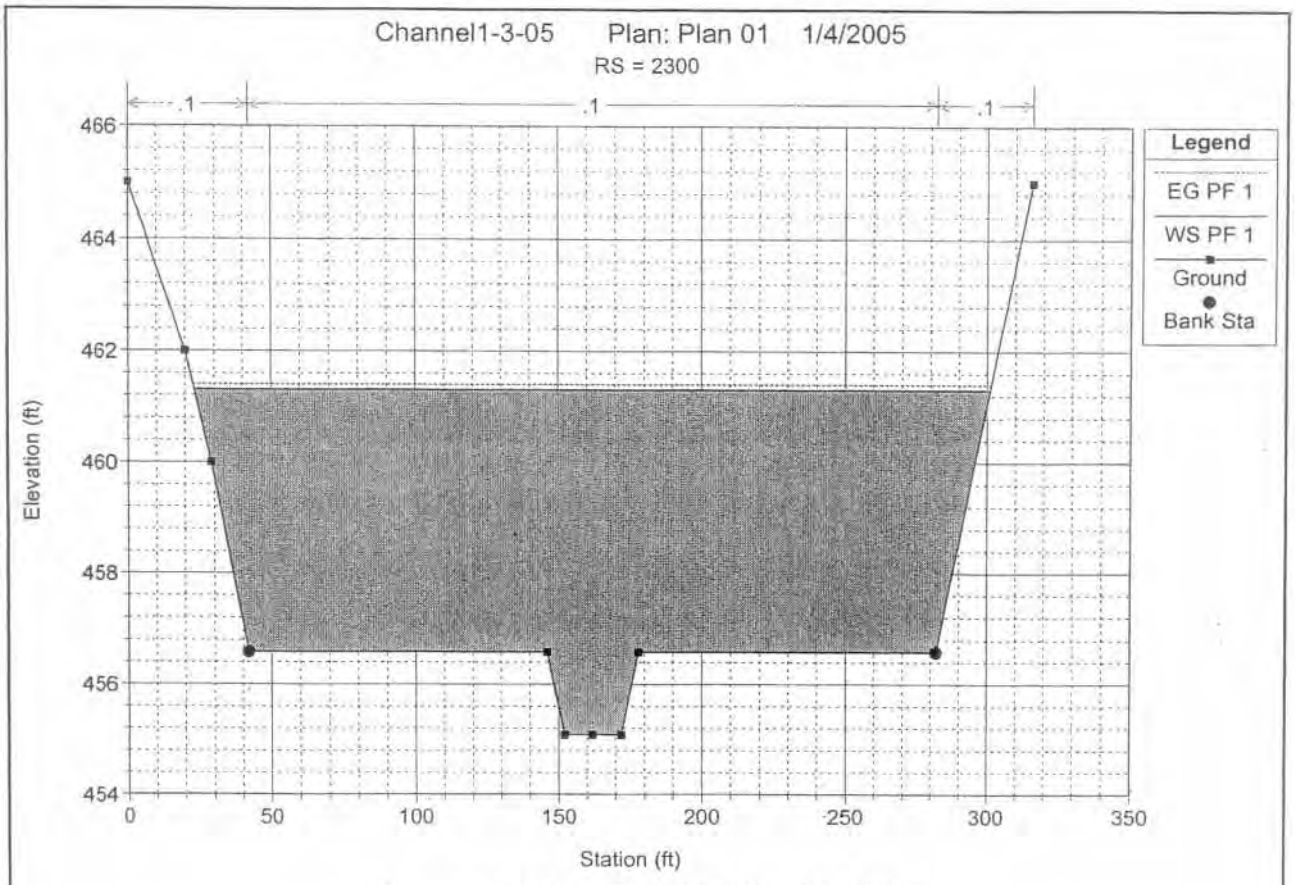
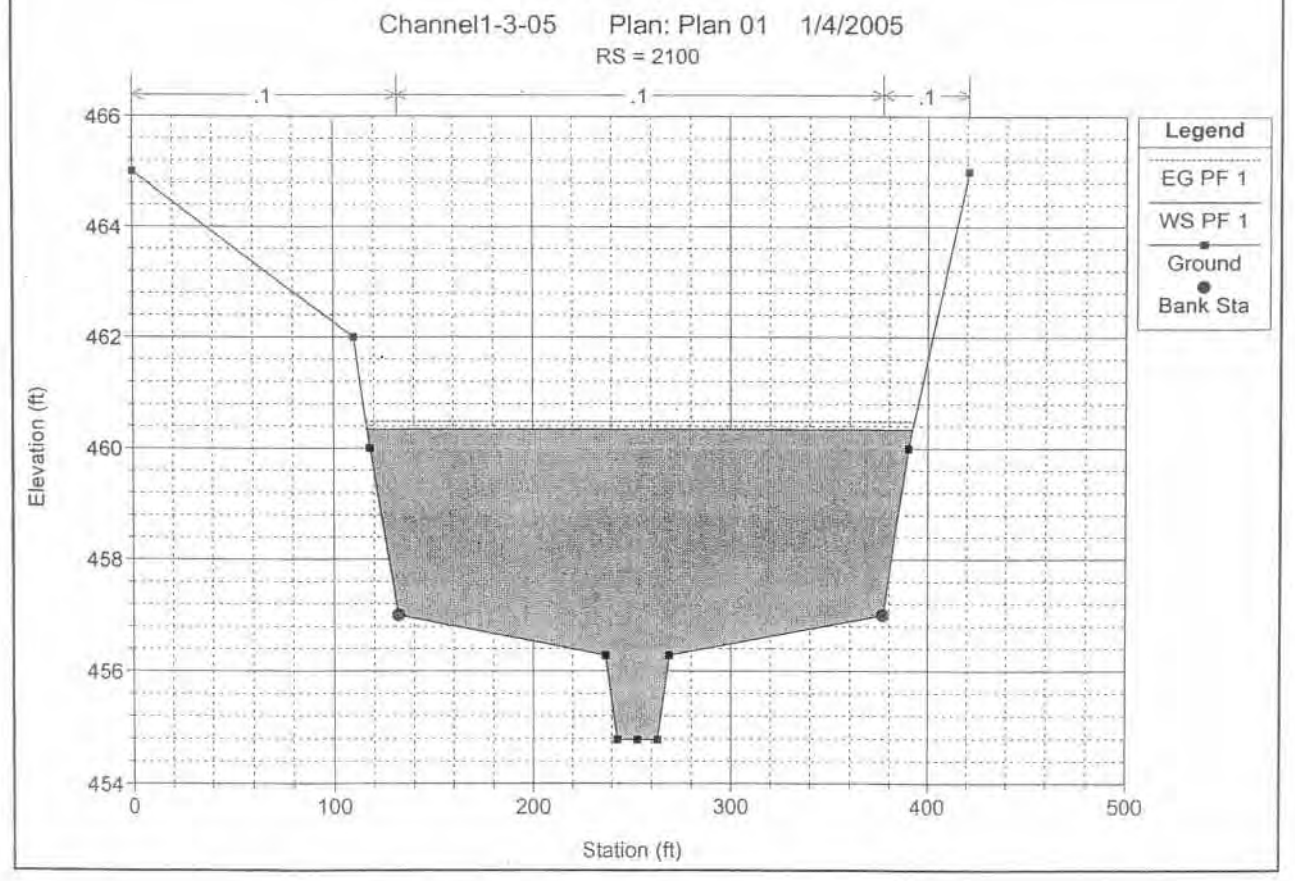
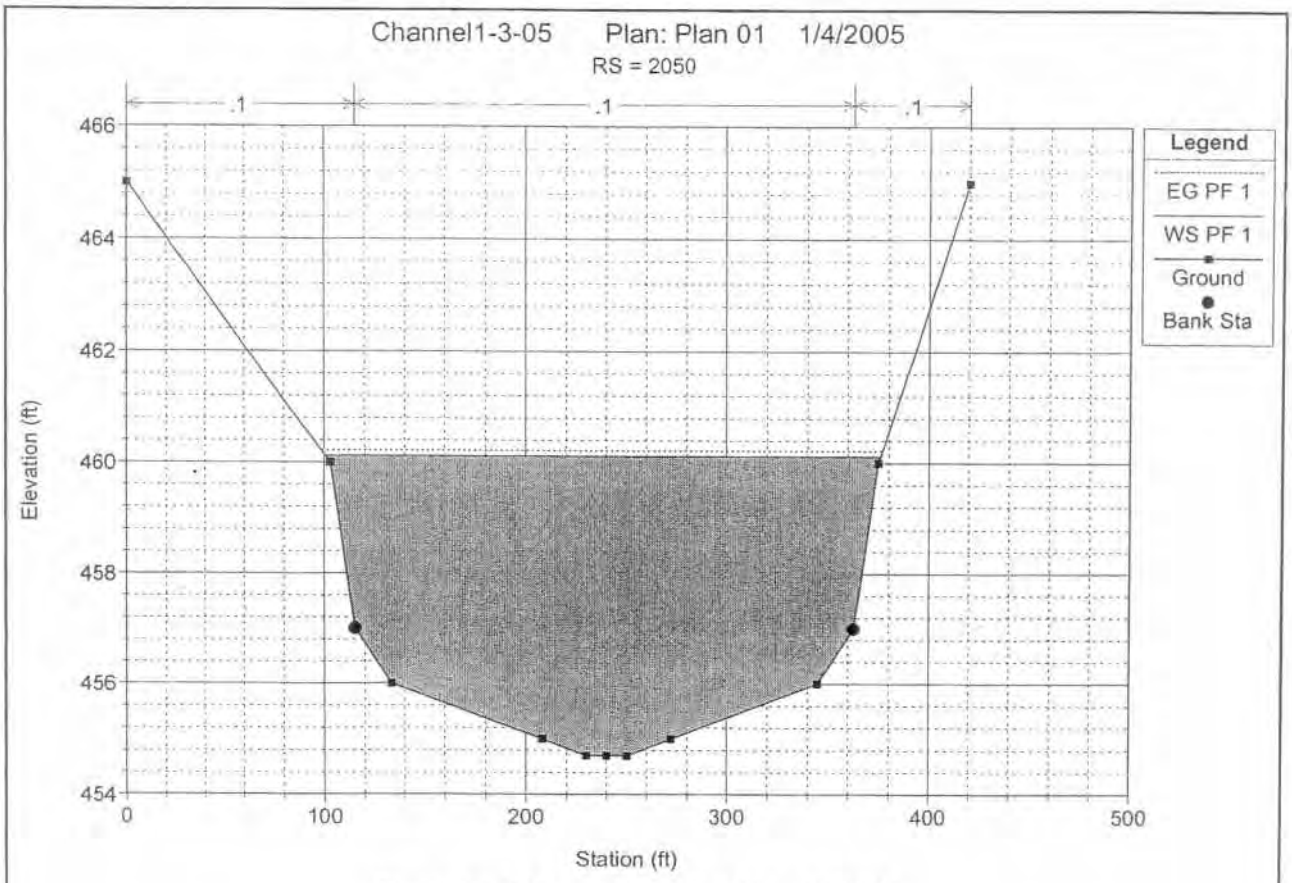
454
0
50
100
150
200
250
Elevation (ft)
Station (ft)
Legend
EG PF 1
WS PF 1
Crit PF 1
Ground
Ineff
Bank Sta


Channel1-3-05 Plan: Plan 01 1/4/2005
RS = 2500
.1
.1
.1
466
464
462
460
458
456
454
0
50
100
150
200
250
300
350
Elevation (ft)
Station (ft)
Legend
EG PF 1
WS PF 1
Ground
Bank Sta


Channel1-3-05 Plan: Plan 01 1/4/2005
RS = 2300
.1
.1
.1
Legend
EG PF 1
WS PF 1
Ground
Bank Sta
Elevation (ft)
466
464
462
460
458
456
454
0
50
100
150
200
250
300
350
Station (ft)


Channel1-3-05 Plan: Plan 01 1/4/2005
RS = 2100
.1
.1
.1
Legend
EG PF 1
WS PF 1
Ground
Bank Sta
Elevation (ft)
466
464
462
460
458
456
454
0
100
200
300
400
500
Station (ft)


Channel1-3-05 Plan: Plan 01 1/4/2005
RS = 2050
.1
.1
.1
466
464
462
460
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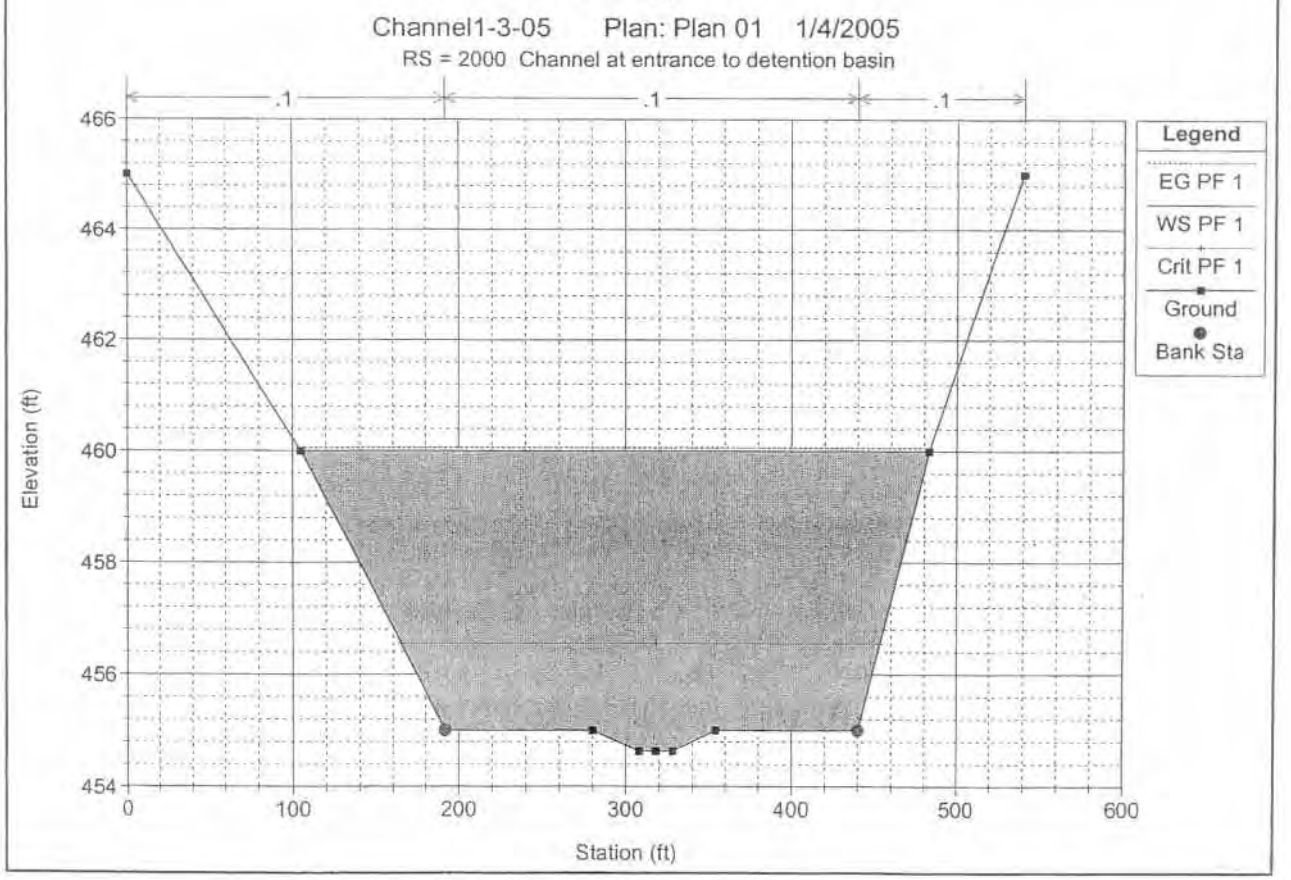
454
0
100
200
300
400
500
Elevation (ft)
Station (ft)
Legend
EG PF 1
WS PF 1
Ground
Bank Sta


Channel1-3-05 Plan: Plan 01 1/4/2005
RS = 2000 Channel at entrance to detention basin
.1
.1
.1
466
464
462
460
458
456
454
0
100
200
300
400
500
600
Elevation (ft)
Station (ft)
Legend
EG PF 1
WS PF 1
Crit PF 1
Ground
Bank Sta

Worksheet
Worksheet for Trapezoidal Channel

Project Description	
Worksheet	Trapezoidal Channel - 1
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Discharge

Input Data		
Mannings Coefficient	0.045	
Slope	0.006150	ft/ft
Depth	4.00	ft
Left Side Slope	1.50	H : V
Right Side Slope	1.50	H : V
Bottom Width	50.00	ft

Results		
Discharge	1,331.30	cfs
Flow Area	224.0	ft²
Wetted Perimeter	64.42	ft
Top Width	62.00	ft
Critical Depth	2.73	ft
Critical Slope	0.022466	ft/ft
Velocity	5.94	ft/s
Velocity Head	0.55	ft
Specific Energy	4.55	ft
Froude Number	0.55	
Flow Type	Subcritical	

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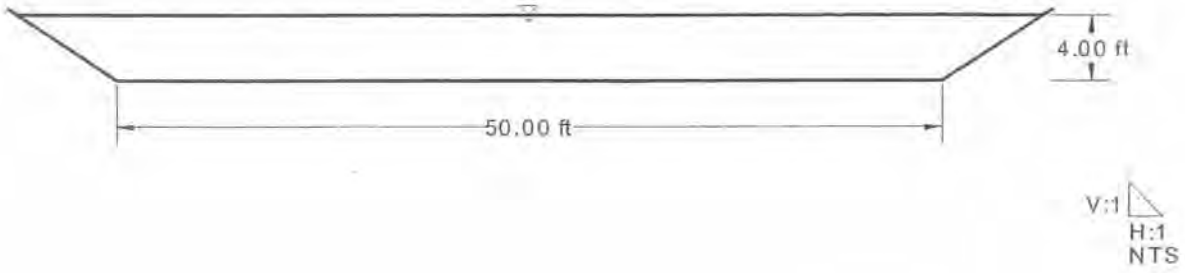
Kimley-Horn and Associates
37 Brookside Road Waterbury, CT 06708 USA (203) 755-1666

Cross Section
Cross Section for Trapezoidal Channel

Project Description	
Worksheet	Trapezoidal Channel - 1
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Discharge

Section Data		
Mannings Coefficient	0.045	
Slope	0.006150	ft/ft
Depth	4.00	ft
Left Side Slope	1.50	H : V
Right Side Slope	1.50	H : V
Bottom Width	50.00	ft
Discharge	1,331.30	cfs



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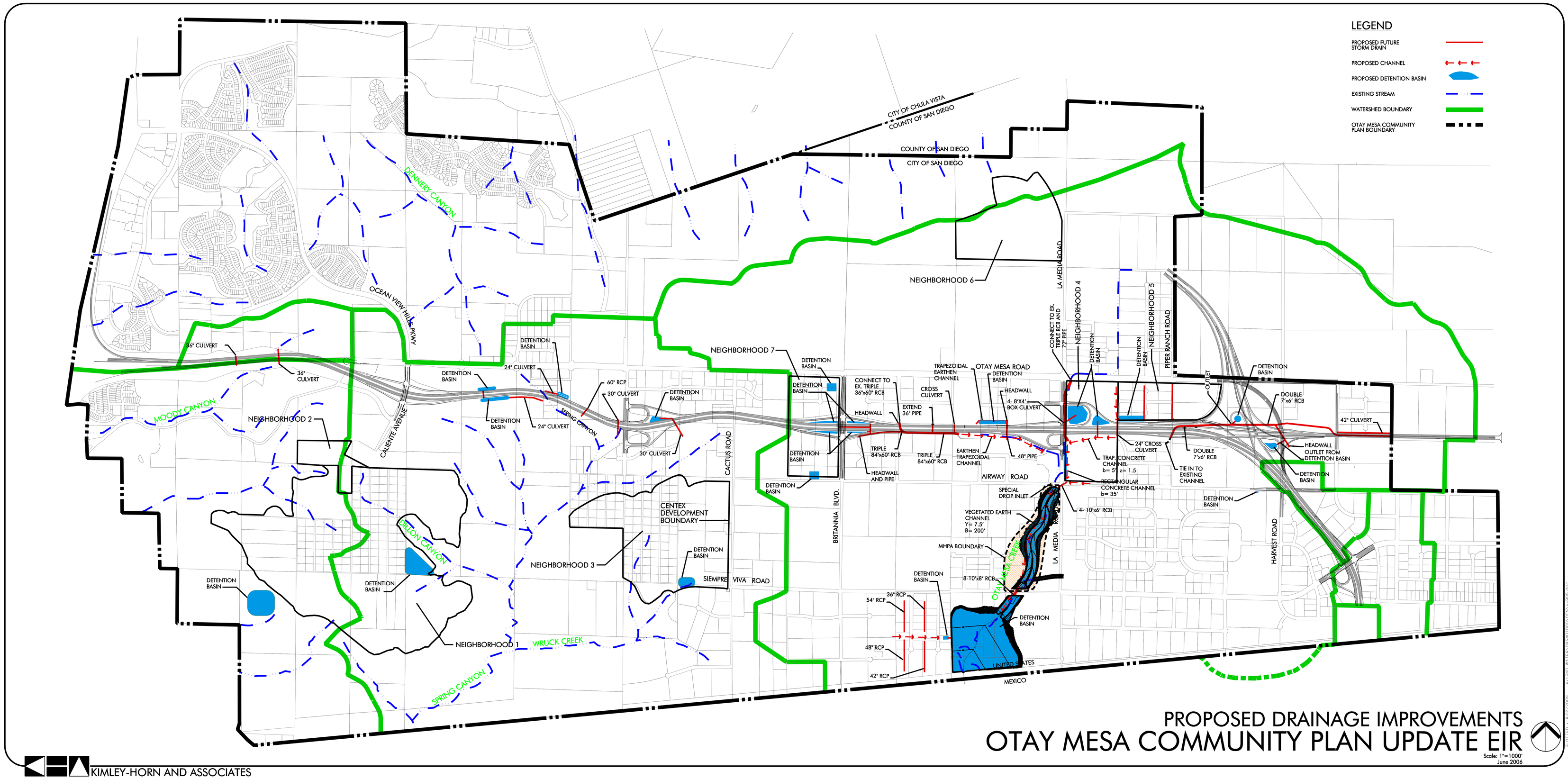
Kimley-Horn and Associates
37 Brookside Road Waterbury, CT 06708 USA (203) 755-1666
Project Engineer: Michael Knapton

V. PROPOSED DRAINAGE FACILITIES

For most of the Mesa, drainage facilities are constructed as part of development or road projects, and include only facilities in the immediate vicinity of the projects. For the proposed future private development, no designs are available to show these future facilities. Caltrans has prepared plans for their SR-905 project, and those facilities are shown on the attached map.

The only Master Planned facility which needs to be constructed before development takes place is the Main Channel and Detention basin in the East Watershed. Details of this system are presented in Section VI.



PROPOSED DRAINAGE IMPROVEMENTS
OTAY MESA COMMUNITY PLAN UPDATE EIR

Scale: 1"=1000'
June 2006

KIMLEY-HORN AND ASSOCIATES

VI. PROPOSED DRAINAGE ALTERNATIVES

The historical drainage on the Mesa, with its flat terrain and shallow swales for drainage paths, did not become a problem until development started taking place in the 1960s. This development started concentrating flows in culverts under roads and redefined some of the historical drainage paths. Some of the development solved problems in some areas, but impacted other areas by moving the problem downstream. One of these areas is the existing creek that parallels La Media Road and eventually crosses the border into Mexico. The frequent flooding along portions of this channel is a constraint to future development for some of the areas along the creek.

1. NO PROJECT

The alternative of doing nothing to improve the drainage along the main creek channel would prevent future development from taking place along portions of La Media Road. The existing creek is not deep enough to allow the adjacent properties to drain effectively. To provide continued access along the truck route during storms, if the channel is not constructed, the roads will need to be raised or alternative routes identified. The existing intersection of Airway Road and La Media Road floods after any significant precipitation. The adjacent roads are too low to allow significant flows to pass under them, so they flood frequently. If the roads are raised to allow more flow to pass under them, they will impact the already-developed adjacent property, parts of which would now be lower than the roads, creating even more difficult drainage issues for the properties.

2. CONCRETE CHANNEL

The 1999 Otay Mesa Drainage Study recommended a concrete channel from Otay Mesa Road to the Border Detention Basin. The recommended plan was a concrete channel along the east side of La Media Road until reaching Siempre Viva Road, where it crossed under La Media and followed on the north side of Siempre Viva to box culverts under Siempre Viva that connected to the Border Detention Basin. All of the concrete channel alternatives assumed that the existing creek with its habitat would continue to carry low flows. The 1999 cost for this alternative was $10.6 million, which would be approximately $14.9 million in 2005 dollars without land acquisition.

3. LA MEDIA CHANNEL AND BORDER DETENTION BASIN

The largest watershed on the Mesa is the East Watershed, which covers an area at 6.78 square miles (4,340 Acres). All of the flow from this watershed collects at a concentration point at a large culvert where it crosses the border with Mexico and flows under the airport access road and airport runway before flowing into the Tijuana River.

This portion at the Mesa is extremely flat, and the adjacent properties can not effectively drain into the existing small creek channel without raising the elevations of the roads and developments near the creek. To allow for future development and to accommodate runoff from proposed future projects, a new channel is required with inverts from 3 to 5 feet below the existing creek channel.

The proposed channel has a bottom width that varies from 240 feet at the new border detention basin to 200 feet from north of Siempre Viva Road to the Airway Road/La Media Road intersection. The side slopes will vary between 4:1 to 10:1. Heavy riparian vegetation will be allowed to grow in the channel and no annual maintenance will be required. Once the vegetation has matured, maintenance of dead or fallen trees may be required every few years. There will be a 12 foot wide access road on each bank. The Channel will contain the 100 year flood flow with mature vegetation growth.

From the Airway Road/La Media Road intersection, a 35 foot wide concrete channel along the east side of La Media Road will connect with the proposed Caltrans culverts which will be constructed with SR 905. The RCB culverts under the intersection will need to accommodate existing utilities in both roads, which may impact the intersection and the utilities.

The Border Detention Basin will be designed to attenuate the peak post-development flows down to their pre-development levels for flows from 5 year through 100 year storms. The outlet structure will be less than six feet high, and will not be under the jurisdiction of the State of California DSOD. The design of the outlet structure will be prepared with final plans for the project. The Detention Basin will be approximately 1700' by 1500' and cover an area of approximately 58 acres.

Border Detention Basin

Area:	58 Acres
Max. Water Depth:	6.0 Feet
Max. Storage Volume:	308 AF

The basin will be graded to appear natural. Natural vegetation will be allowed to grow in the basin and no annual maintenance will be required. A low-flow stream will be created through the basin. A Maintenance Assessment District may be created for maintaining the channel and detention basin.

The basin and channel will require the removal of approximately 915,000 CY of soil. It is assumed that this export will be used on adjacent properties to raise the building pad grades thereby limiting the haul distance. A preliminary cost estimate was prepared which reflects both the construction costs and the land acquisition costs. A Property Ownership Map which shows the ownership within the East Watershed is attached.

La Media Channel and Border Detention Basin

Preliminary Opinion of Probable Construction Cost

2/8/2005

Kimley-Horn and Associates

Construction Items

Item No.	Description	Quantity	Units	Unit Price	Cost
1	Excavation	822,500	CY	$2	$1,645,000
2	Airway Road culvert (6~5'wx5'h)	300	CY	$1,500	$450,000
3	La Media/Airway Road intersection culvert (6~10'wx6'h)	1,500	CY	$1,500	$2,250,000
4	Siempre Viva Road culvert (8~10'wx8'h)	1,490	CY	$1,500	$2,235,000
5	Detention Basin Outlet Structure	1	LS	$100,000	$100,000
6	Traffic Control	1	LS	$100,000	$100,000
7	Utility Relocation	1	LS	$150,000	$150,000
8	Street Repair	1	LS	$50,000	$50,000
9	Erosion Control	1	LS	$50,000	$50,000
10	Revegetation	1	LS	$600,000	$600,000
		Subtotal			$7,630,000
		Contingency	20%		$1,526,000
		Total			$9,156,000

Land Acquisition

1	Land Acquisition (outside MHPA)*	2,610,000	SF	$4	$10,440,000
2	Land Acquisition (inside MHPA)**	1,820,000	SF	$1	$1,820,000
		Subtotal			$12,260,000
		Contingency	20%		$2,452,000
		Total			$14,712,000

Total Cost (Construction and Land Acquisition) $23,868,000

Notes: * Includes area of detention basin and channel south of Siempre Viva

** Includes entire area within MHPA boundary

*** Estimate does not include engineering, environmental, geotechnical, surveying, etc.

K:\095407000\Excel\[cost estimate.xls]Sheet1

OTAY MESA CPU

Earthwork Quantities

Cut: 822,500 CY

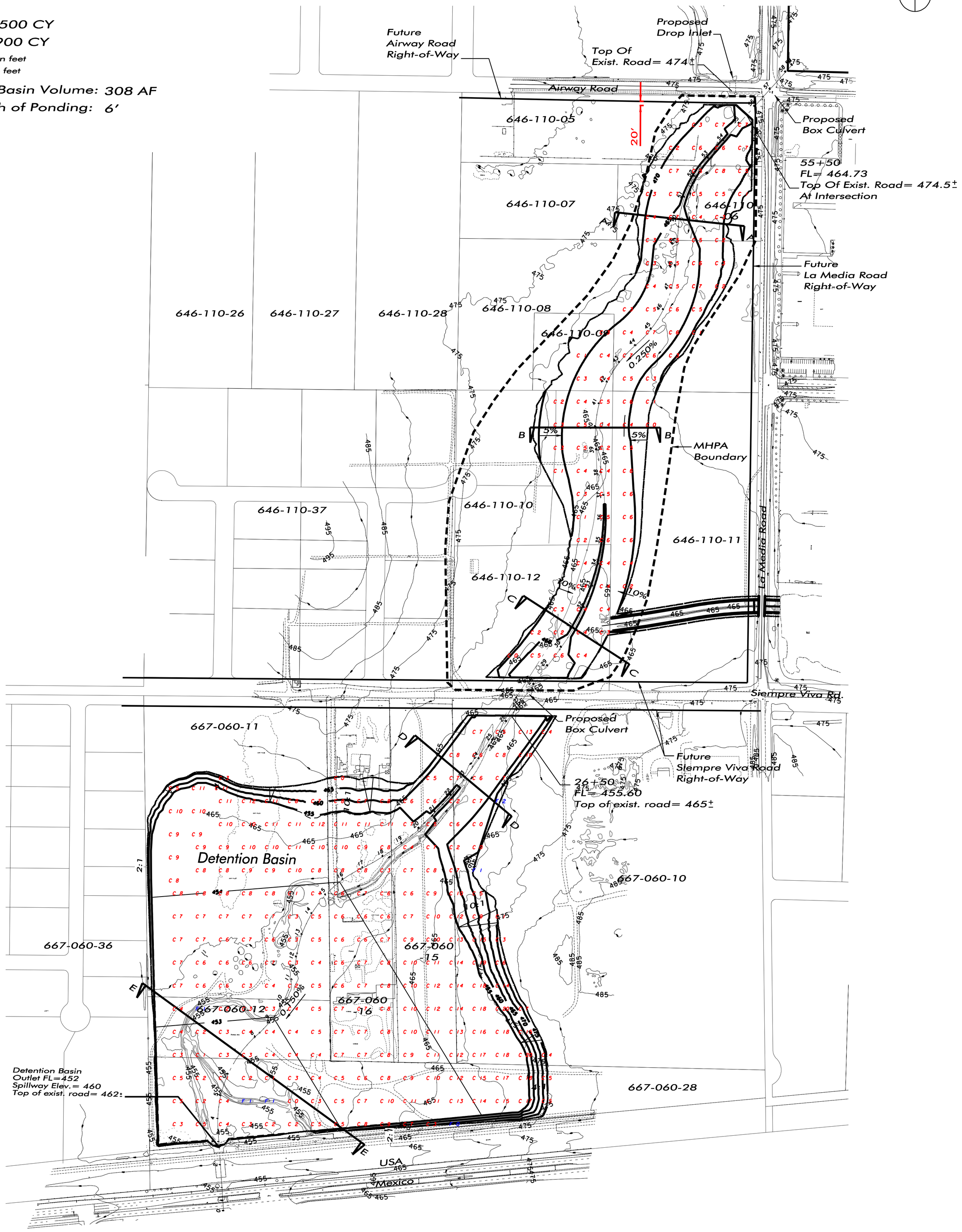
Fill: 900 CY

C = Cut depth in feet

F = Fill depth in feet

Detention Basin Volume: 308 AF

Max. Depth of Ponding: 6'



0 100 200 400

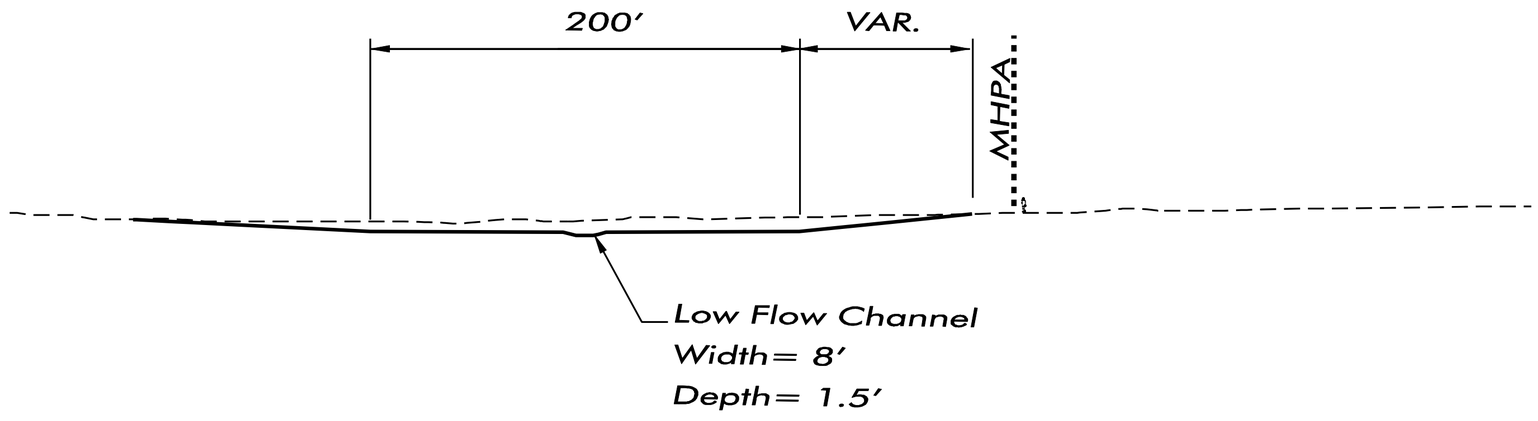
SCALE: 1" = 200'

KIMLEY-HORN and ASSOCIATES

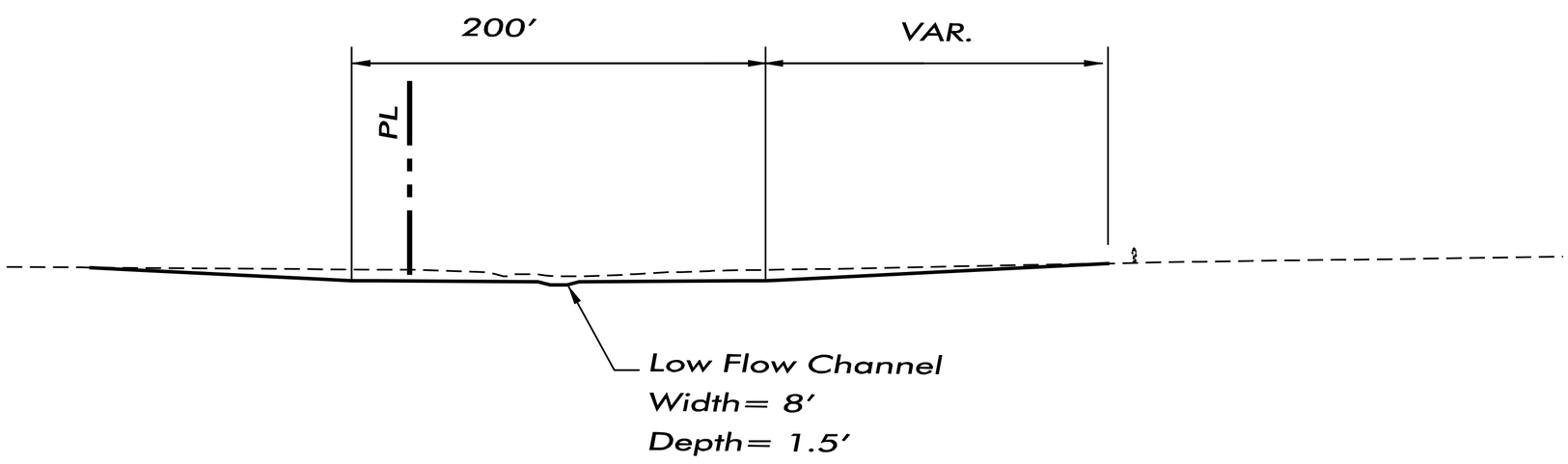
JUNE 2006

CONCEPTUAL CHANNEL/DETENTION BASIN GRADING

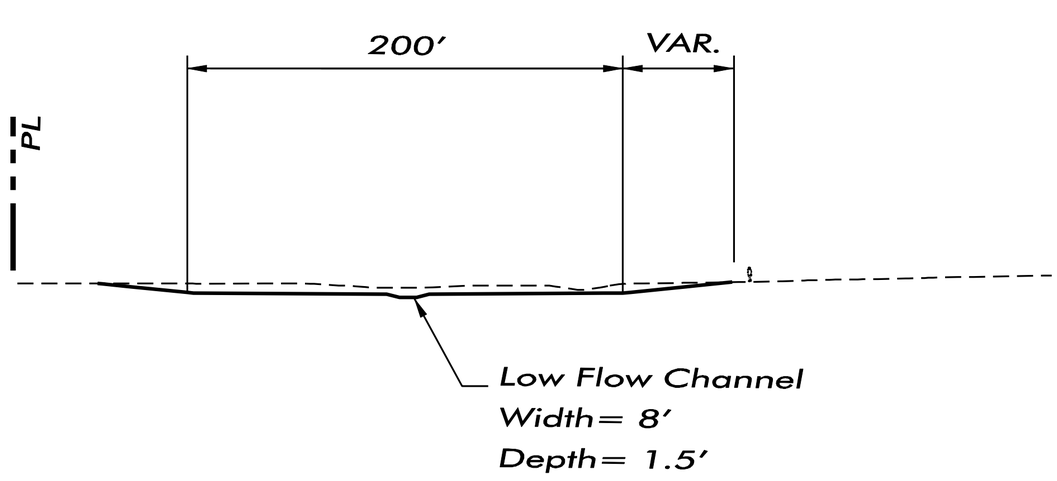
OTAY MESA CPU



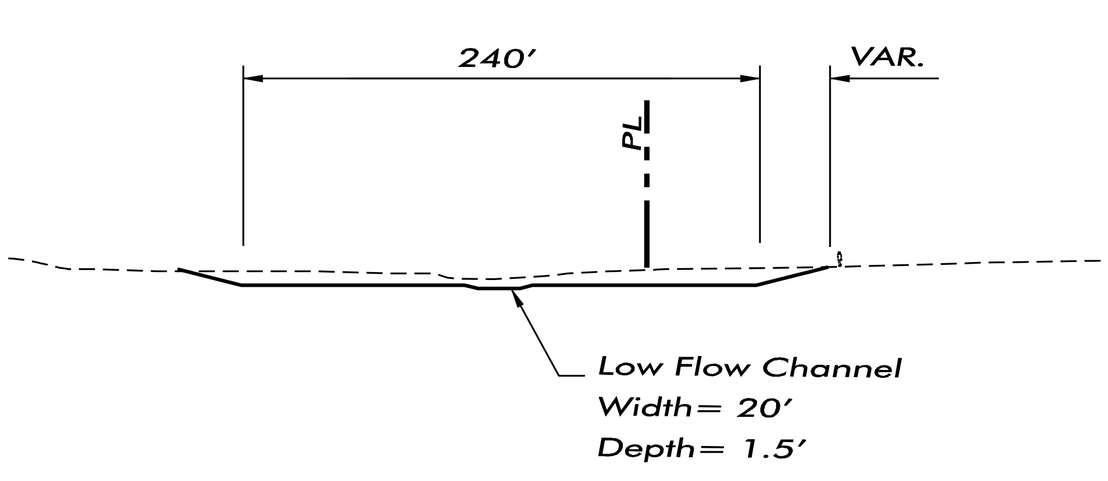
SECTION A-A



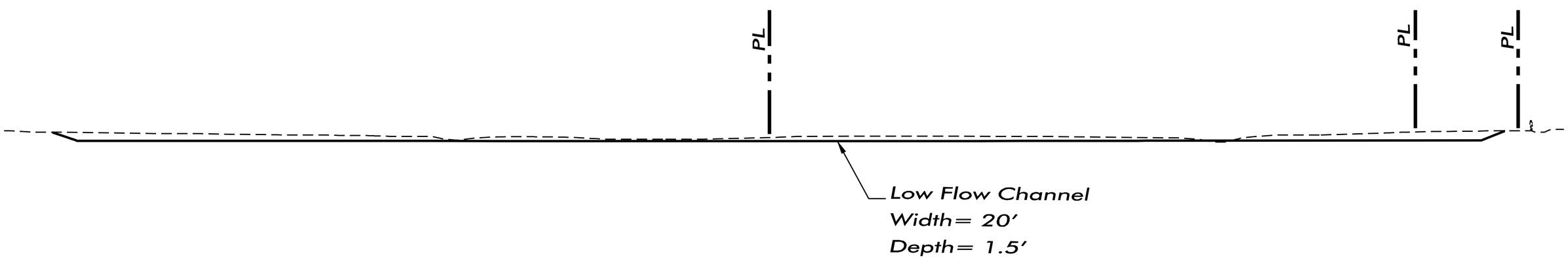
SECTION B-B



SECTION C-C



SECTION D-D



SECTION E-E

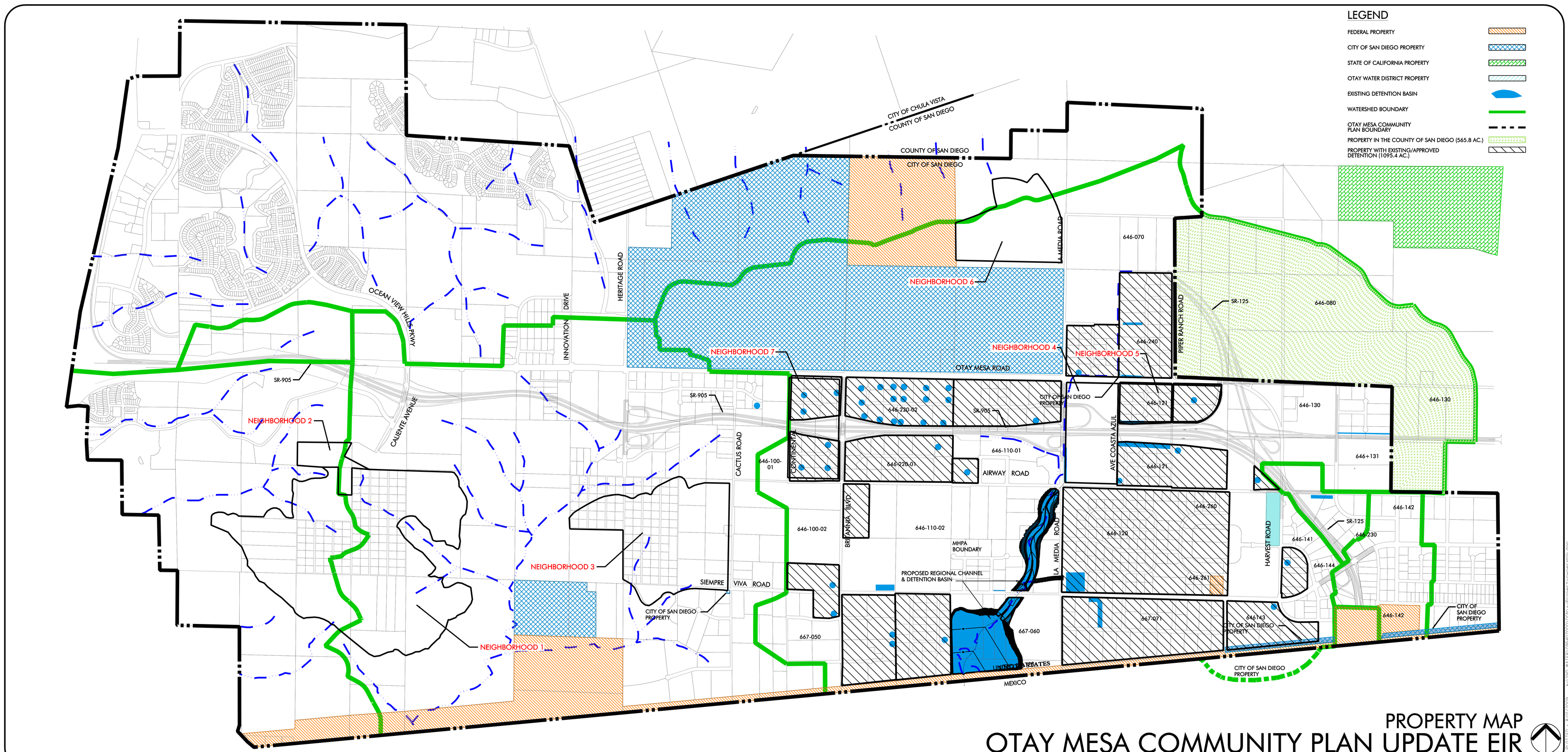
Note: No Vertical Exaggeration On Sections

0 25 50 100
SCALE: 1" = 50'

JUNE 2006

KIMLEY-HORN and ASSOCIATES

EARTHWORK CROSS SECTIONS



PROPERTY MAP

OTAY MESA COMMUNITY PLAN UPDATE EIR

Scale: 1"=1000'
JUNE 2006

KIMLEY-HORN AND ASSOCIATES

PLOTTED: 8/7/2008 9:43:50 AM BY DSMITH N:\SDI_JOBS\065700\000\X-SP-Land Plan.dgn

VII. RECOMMENDED DRAINAGE DESIGN CRITERIA

Since the five watershed areas on the Mesa flow in every direction except east, they flow into different watersheds with different constraints and impacts. The runoff from the five watersheds will have different criteria for design of drainage facilities.

West Perimeter Watershed

This watershed consists of smaller Mesa-top watersheds with a total area of approximately 254 acres that drain to the west to three separate creeks in canyons and gullies. These creeks are carried under the SD&AE and Trolley tracks and through San Ysidro in buried storm drain systems. The storm drains under the tracks have hydraulic capacities of 30 cfs (18" RCP) and 125 cfs (36" RCP) based on the San Ysidro Boulevard Area Master Drainage plan prepared by BSI Consultants, February 15, 1996. Sub-basins OT3-7 and OT3-8 combine downstream into a single creek that flows to the 36" RCP. The current study estimates 140 cfs (Q100) will flow off of the Mesa into this sub-basin. This study does not address the capacity of the downstream system or include the hydrologic analysis for areas to the west of the Mesa, but clearly the 125 cfs capacity of the existing system will be exceeded. This area will need to be addressed in more detail during design of the upstream tributary development. Detention Basins are recommended which will reduce peak flows in the sub-basin to minimize impacts on the downstream system. These detention basins will reduce the peak, 50-year, and 100-year flow to predevelopment levels. Because of the unstable soils in this area, care should be taken that the proposed detention basins and relocated drainage facilities do not contribute to an increase in the risk of slides through increased saturation of the soil.

West Watershed

The West Watershed consists of smaller Mesa-top watersheds that drain into the tributary canyons of Spring Canyon. All of the flow from the watershed flows into Mexico at the Spring Canyon concentration point. Detention basins will be required to reduce the post-development peak flows to predevelopment levels for the 50-year and 100-year storm. If the detention basins concentrate flows at the upper edge of canyons, care must be taken to ensure that erosion potential is not increased downstream.

East Watershed

The East Watershed flows to Mexico at a single concentration point between Britannia and La Media roads. Requirements for the control of peak runoff from development in this watershed already exist. The "Notice" dated August 7, 1987 (page 2), sets criteria for detention basins and for storm drain sizing. As part of the future storm drain project in this watershed, a single detention basin will be constructed at the border. The construction of this basin will eliminate the need for individual on-site detention basins for subsequent development.

North Perimeter Watershed

These small watersheds along the northern edge of the Mesa flow into small canyons that flow into the Otay River. There are no peak flow attenuation requirements for flows from these watersheds. There may be water quality issues with the Otay River, and there may be erosion issues from storm drains on the Mesa. Only approximately 14 acres of Neighborhood 6 are in this watershed.

VIII. STORM WATER QUALITY REQUIREMENTS

Because of problems related to the poor water quality of storm water runoff from urban conveyance systems, the City requires that storm water Best Management Practices (BMPs) be constructed for all new projects. The storm water discharge contains pollution such as chemicals, trash, sediment, bacteria, metals, oil and grease. Construction projects which add impervious areas and change drainage patterns increase the discharge of these pollutants.

The Municipal Storm Water National Pollutant Discharge Elimination System Permit (NPDES Municipal Permit), approved February 21, 2001 by the San Diego Regional Water Quality Control Board (RWQCB), requires the City to implement regulations for constructing storm water BMPs for development projects.

In 2003, as part of the San Diego Municipal Code, the City published "Storm Water Standards – A Manual for Construction & Permanent Storm Water Best Management Practices Requirements." This manual is the reference document for all of the storm water issues encountered in development, including BMPs. Included in this report are Appendix C – Example Permanent Storm Water Best Management Practices, and the Storm Water Requirements Applicability Checklist from the City's Manual. Before preparing a drainage study, the "Storm Water Requirements Applicability Checklist" is completed. This checklist is used to determine the priority level of the project. Most of the projects on the Mesa will require Priority Project Permanent Storm Water BMPs and High Priority Construction Storm Water BMPs.

All projects subject to the priority permanent BMP requirements must include a "Water Quality Technical Report." From the manual, the report will include:

1. A drainage study report prepared by a civil engineer, hydrologist, or hydrogeologist registered in the State of California, with experience in the science of stream and river generated surface features (i.e., fluvial geomorphology) and water resources management, satisfactory to the City Engineer. The report shall consider the project area's location (from the larger watershed perspective), topography, soil and vegetation conditions, percent impervious area, natural and infrastructure drainage features, and any other relevant hydrologic and environmental factors to be protected specific to the project area's watershed.
2. A field reconnaissance to observe and report on downstream conditions, including undercutting erosion, slope stability, vegetative stress (due to flooding, erosion, water quality degradation, or loss of water supplies) and the area's susceptibility to erosion or habitat alteration as a result of any future upstream development.
3. A hydrologic analysis to include rainfall runoff characteristics from the project area including at a minimum, peak runoff, time of concentration, and detention volume (if appropriate). These characteristics shall be developed for the two-year and ten-year frequency, six-hour or 24-hour, type B storm for the coastal areas of San Diego County. The largest peak flow should be included in the report. The report shall also report the project's conditions of concern based on the hydrologic and downstream conditions discussed above. Where downstream conditions of concern have been identified, the drainage study shall establish that pre-project hydrologic conditions that minimize impacts on those downstream conditions of concern would be either improved or maintained by the proposed project, satisfactory to the City Engineer, by incorporating the permanent BMP requirements.

Appendix D of the Manual includes detailed guidelines for the Water Quality Technical Report.

There are numerous alternative permanent BMPs that can be used for each project. The alternatives include Site Design BMPs, Source Control BMPs, and Treatment Control BMPs. The Site Design BMPs are primary ways to reduce storm water runoff through means such as increased pervious areas, increased infiltration, use of natural channels, and appropriate landscaping. All of these except dry wells are applicable to the Mesa. Source Control BMPs are meant to control pollutants at their source before they enter storm water, and are all applicable to the Mesa. Treatment Control BMPs treat the storm water before it leaves the property, and include natural methods such as biofilters, detention basins, wetlands, and porous pavement, and mechanical methods such as filters and separators. The one Treatment Control BMP that is not applicable to the Mesa is infiltration, which is not very effective on the Mesa because of the clay soils.

Most of Otay Mesa drains to the south across the border with Mexico and eventually into the Tijuana River. A small portion flows north into the Otay River, and the far western part of the Mesa flows to the west through San Ysidro and then into the Tijuana River. The Tijuana River has been identified by the 2002 Clean Water Act as a "Section 303(d) Water Quality Limited" river. The pollutants of concern which are included in the attached pages from the USEPA, need to be listed, and the new development project's potential impacts on these pollutants need to be included in the project's drainage report.

Recommended Storm Water Policies

1. **Apply water quality protection measures to land development projects during project design, permitting, construction, and operations in order to minimize the quantity of runoff generated on-site, the disruption of natural water flows and the contamination of storm water runoff.**

    a. Increase on-site infiltration, and preserve, restore or incorporate natural drainage systems into site design
    b. Reduce the amount of impervious surfaces through selection of materials, site planning, and narrowing street widths where possible.
    c. Increase the use of natural vegetation and landscaping in drainage design.
    d. Avoid conversion of areas particularly susceptible to erosion and sediment loss (e.g.: steep slopes), and where unavoidable, enforce regulations that minimize these impacts.
    e. Avoid land use, site development, and zoning regulations that limit impacts on, and protect the natural integrity of topography, drainage systems, and water bodies.
    f. Maintain landscape design standards that minimize the use of pesticides and herbicides.
    g. Enforce maintenance requirements in development permit conditions.

2. **Require construction contractors to comply with accepted storm water pollution prevention planning practices for all projects.**

    a. Minimize the amount of graded land surface exposed to erosion and enforce control ordinances
    b. Continue routine inspection practices to check for proper erosion control methods and housekeeping practices during construction.
    c. Ensure that contractors are aware of and implement urban runoff control programs.

3. **Encourage measures to promote the proper collection and disposal of pollutants at the source, rather than allowing them to enter the storm drain system.**

    a. Promote the provision of used oil recycling and/or hazardous waste recycling facilities and drop-off locations.
    b. Follow up on complaints of illegal discharges and accidental spills to storm drains, waterways, and canyons.

APPENDIX C

EXAMPLE PERMANENT STORM WATER BEST MANAGEMENT PRACTICES

The following are a list of BMPs may be used to minimize the introduction of pollutants of concern that may result in significant impacts to receiving waters. Other BMPs approved by the Development Services Department as being equal or more effective in pollutant reduction than comparable BMPs identified below are acceptable. All BMPs must comply with local zoning and building codes and other applicable regulations.

Site Design BMPs

Minimizing Impervious Areas

- Reduce sidewalk widths
- Incorporate landscaped buffer areas between sidewalks and streets.
- Design residential streets for the minimum required pavement widths
- Minimize the number of residential street cul-de-sacs and incorporate landscaped areas to reduce their impervious cover.
- Use open space development that incorporates smaller lot sizes
- Increase building density while decreasing the building footprint
- Reduce overall lot imperviousness by promoting alternative driveway surfaces and shared driveways that connect two or more homes together
- Reduce overall imperviousness associated with parking lots by providing compact car spaces, minimizing stall dimensions, incorporating efficient parking lanes, and using pervious materials in spillover parking areas

Increase Rainfall Infiltration

- Use permeable materials for private sidewalks, driveways, parking lots, and interior roadway surfaces (examples: hybrid lots, parking groves, permeable overflow parking, etc.)
- Direct rooftop runoff to pervious areas such as yards, open channels, or vegetated areas, and avoid routing rooftop runoff to the roadway or the urban runoff conveyance system

Maximize Rainfall Interception

- Maximizing canopy interception and water conservation by preserving existing native trees and shrubs, and planting Additional native or drought tolerant trees and large shrubs.

Minimize Directly Connected Impervious Areas (DCIAs)

- Draining rooftops into adjacent landscaping prior to discharging to the storm water conveyance system

- Draining parking lots into landscape areas co-designed as biofiltration areas
- Draining roads, sidewalks, and impervious trails into adjacent landscaping

Slope and Channel Protection

Use of natural drainage systems to the maximum extent practicable

- Stabilized permanent channel crossings
- Planting native or drought tolerant vegetation on slopes
- Energy dissipaters, such as riprap, at the outlets of new storm drains, culverts, conduits, or channels that enter unlined Channels

Maximize Rainfall Interception

- Cisterns
- Foundation planting

Increase Rainfall Infiltration

- Dry wells

Source Control BMPs

- Storm water conveyance system stenciling and signage
- Outdoor material and trash storage area designed to reduce or control rainfall runoff
- Efficient irrigation system

Treatment Control BMPs

Biofilters

- Grass swale
- Grass strip
- Wetland vegetation swale
- Bioretention

Detention Basins

- Extended/dry detention basin with grass lining
- Extended/dry detention basin with impervious lining

Infiltration

- Infiltration basin
- Infiltration trench

Pervious Paving
- Porous asphalt
- Porous concrete
- Porous modular concrete block

Wet Ponds and Wetlands
- Wet pond (permanent pool)
- Constructed wetland

Drainage Inserts
- Catch basin/storm drain inserts
- Catch basin screens

Filtration Systems
- Media filtration
- Sand filtration

Hydrodynamic Separation Systems
- Swirl concentrator
- Cyclone separator
- Baffle boxes

City of San Diego
Development Services
1222 First Ave., MS-302
San Diego, CA 92101
(619) 446-5000 for information

THE CITY OF SAN DIEGO

Storm Water Requirements Applicability Checklist

Project Address:	Assessor Parcel Number(s):	Project Number *(for City Use Only)*

Complete Sections 1 and 2 of the following checklist to determine your project's permanent and construction storm water best management practices requirements. This form must be completed and submitted with your permit application.

Section 1 - Permanent Storm Water BMP Requirements:

If any answers to Part A are answered "Yes," your project is subject to the "Priority Project Permanent Storm Water BMP Requirements," and "Standard Permanent Storm Water BMP Requirements" of the Storm Water Standards Manual, Section III, "Permanent Storm Water BMP Selection Procedure." If all answers to Part A are "No," and any answers to Part B are "Yes," your project is only subject to the Standard Permanent Storm Water BMP Requirements. If every question in Part A and B is answered "No," your project is exempt from permanent storm water requirements.

Part A: Determine Priority Project Permanent Storm Water BMP Requirements.

Does the project meet the definition of one or more of the priority project categories?*

1.	Detached residential development of 10 or more units	Yes	No
2.	Attached residential development of 10 or more units	Yes	No
3.	Commercial development greater than 100,000 square feet	Yes	No
4.	Automotive repair shop	Yes	No
5.	Restaurant	Yes	No
6.	Steep hillside development greater than 5,000 square feet	Yes	No
7.	Project discharging to receiving waters within Water Quality Sensitive Areas	Yes	No
8.	Parking lots greater than or equal to 5,000 square feet or with at least 15 parking spaces, and potentially exposed to urban runoff	Yes	No
9.	Streets, roads, highways, and freeways which would create a new paved surface that is 5,000 square feet or greater	Yes	No
10.	Significant redevelopment over 5,000 square feet	Yes	No

** Refer to the definitions section in the* Storm Water Standards *for expanded definitions of the priority project categories.*

Limited Exclusion: *Trenching and resurfacing work associated with utility projects are not considered priority projects. Parking lots, buildings and other structures associated with utility projects are priority projects if one or more of the criteria in Part A is met. If all answers to Part A are "No", continue to Part B.*

Part B: Determine Standard Permanent Storm Water Requirements.

Does the project propose:

1.	New impervious areas, such as rooftops, roads, parking lots, driveways, paths and sidewalks?	Yes	No
2.	New pervious landscape areas and irrigation systems?	Yes	No
3.	Permanent structures within 100 feet of any natural water body?	Yes	No
4.	Trash storage areas?	Yes	No
5.	Liquid or solid material loading and unloading areas?	Yes	No
6.	Vehicle or equipment fueling, washing, or maintenance areas?	Yes	No
7.	Require a General NPDES Permit for Storm Water Discharges Associated with Industrial Activities (Except construction)?*	Yes	No
8.	Commercial or industrial waste handling or storage, excluding typical office or household waste?	Yes	No
9.	Any grading or ground disturbance during construction?	Yes	No
10.	Any new storm drains, or alteration to existing storm drains?	Yes	No

*To find out if your project is required to obtain an Individual General NPDES Permit for Storm Water Discharges Associated with Industrial Activities, visit the State Water Resources Control Board web site at, www.swrcb.ca.gov/stormwtr/industrial.html

OVER

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To request this document in alternative format, call (619) 446-5446 or (800) 735-2929 (TT).
Be sure to see us on the WorldWide Web at www.sandiego.gov/development-services

Section 2. Construction Storm Water BMP Requirements:

If the answer to question 1 of Part C is answered "Yes," your project is subject to Section IV of the Storm Water Standards Manual, "Construction Storm Water BMP Performance Standards," and must prepare a Storm Water Pollution Prevention Plan (SWPPP). If the answer to question 1of Part C is "No," but the answer to any of the remaining questions is "Yes," your project is subject to Section IV of the Storm Water Standards Manual, "Construction Storm Water BMP Performance Standards," and must prepare a Water Pollution Control Plan (WPCP). If every question in Part C is answered "No," your project is exempt from any construction storm water BMP requirements. If any of the answers to the questions in Part C are "Yes," complete the construction site prioritization in Part D below.

Part C: Determine Construction Phase Storm Water Requirements.

Would the project meet any of these criteria during construction?

1. Is the project subject to California's statewide General NPDES Permit for Storm Water Discharges Associated With Construction Activities? ..... Yes No
2. Does the project propose grading or soil disturbance? ..... Yes No
3. Would storm water or urban runoff have the potential to contact any portion of the construction area, including washing and staging areas? ..... Yes No
4. Would the project use any construction materials that could negatively affect water quality if discharged from the site (such as, paints, solvents, concrete, and stucco)? ..... Yes No

Part D: Determine Construction Site Priority

In accordance with the Municipal Permit, each construction site with construction storm water BMP requirements must be designated with a priority: high, medium or low. This prioritization must be completed with this form, noted on the plans, and included in the SWPPP or WPCP. Indicate the project's priority in one of the check boxes using the criteria below, and existing and surrounding conditions of the project, the type of activities necessary to complete the construction and any other extenuating circumstances that may pose a threat to water quality. The City reserves the right to adjust the priority of the projects both before and during construction. [Note: The construction priority does NOT change construction BMP requirements that apply to projects; all construction BMP requirements must be identified on a case-by-case basis. The construction priority does affect the frequency of inspections that will be conducted by City staff. See Section IV.1 for more details on construction BMP requirements.]

☐ 1) High Priority

a) Projects where the site is 50 acres or more and grading will occur during the wet season

b) Projects 5 acres or more and tributary to an impaired water body for sediment (e.g., Peñasquitos watershed)

c) Projects 5 acres or more within or directly adjacent to or discharging directly to a coastal lagoon or other receiving water within an environmentally sensitive area

d) Projects, active or inactive, adjacent or tributary to sensitive water bodies

☐ 2) Medium Priority

a) Capital Improvement Projects where grading occurs, however a Storm Water Pollution Prevention Plan (SWPPP) is not required under the State General Construction Permit (i.e., water and sewer replacement projects, intersection and street re-alignments, widening, comfort stations, etc.)

b) Permit projects in the public right-of-way where grading occurs, however SWPPPs are not required, such as installation of sidewalk, substantial retaining walls, curb and gutter for an entire street frontage, etc.

c) Permit projects on private property where grading permits are required (i.e., cuts over 5 feet, fills over 3 feet), however, Notice Of Intents (NOIs) and SWPPPs are not required.

☐ 3) Low Priority

a) Capital Projects where minimal to no grading occurs, such as signal light and loop installations, street light installations, etc.

b) Permit projects in the public right-of-way where minimal to no grading occurs, such as pedestrian ramps, driveway additions, small retaining walls, etc.

c) Permit projects on private property where grading permits are not required, such as small retaining walls, single-family homes, small tenant improvements, etc.

Name of Owner or Agent *(Please Print)*:	Title:
Signature:	Date:

APPENDICES

Appendix A

- AES Hydrology Calculations

```
**************************************************************************

          RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
          Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT
                       2003,1985,1981 HYDROLOGY MANUAL
        (c) Copyright 1982-2003 Advanced Engineering Software (aes)
            Ver. 1.5A Release Date: 01/01/2003  License ID 1499

                            Analysis prepared by:

                        Kimley-Horn and Associates San Diego
                             517 4th Avenue Suite 301
                            San Diego, California 92101
                          (619) 234-9411 Fax (619) 234-9433

 ************************** DESCRIPTION OF STUDY **************************
* Otay Mesa Watershed Analysis                                            *
* 50 Year Storm Event P=1.70                                              *
* 5/12/05 AMC                                                             *
 **************************************************************************

  FILE NAME: C:\Drainage\407000\OT3-1.DAT
  TIME/DATE OF STUDY: 08:03 05/12/2005
--------------------------------------------------------------------------
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
--------------------------------------------------------------------------
  1985 SAN DIEGO MANUAL CRITERIA

  USER SPECIFIED STORM EVENT(YEAR) =  50.00
  6-HOUR DURATION PRECIPITATION (INCHES) =   1.700
  SPECIFIED MINIMUM PIPE SIZE(INCH) =  18.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 1.00
  SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
  NOTE: ONLY PEAK CONFLUENCE VALUES CONSIDERED
  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-   CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH   CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)      (FT)     SIDE / SIDE/ WAY    (FT)    (FT)  (FT)  (FT)    (n)
===  =====  =========  =================  ======  =====  ====  =====  =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0312 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

**************************************************************************
  FLOW PROCESS FROM NODE   3100.00 TO NODE   3101.00 IS CODE =  21
--------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
==========================================================================
  GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
  SOIL CLASSIFICATION IS "D"
  S.C.S. CURVE NUMBER (AMC II) =  84
```

```
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.86(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    106.00
 DOWNSTREAM ELEVATION(FEET) =    104.32
 ELEVATION DIFFERENCE(FEET) =      1.68
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.86
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.715
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
 FLOW PROCESS FROM NODE   3101.00 TO NODE   3102.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   180.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0240
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.55   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =   5.41   Tc(MIN.) =  16.27
 LONGEST FLOWPATH FROM NODE   3100.00 TO NODE   3102.00 =   250.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   3102.00 TO NODE   3103.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.092
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =   19.30   SUBAREA RUNOFF(CFS) =   18.17
 TOTAL AREA(ACRES) =   19.40   TOTAL RUNOFF(CFS) =   18.29
 TC(MIN.) =  16.27

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   3110.00 TO NODE   3111.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.85(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    110.00
```

```
 DOWNSTREAM ELEVATION(FEET) =    108.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.85
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.717
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
 FLOW PROCESS FROM NODE   3111.00 TO NODE   3112.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   330.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.55   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =   9.91   Tc(MIN.) =  20.76
 LONGEST FLOWPATH FROM NODE   3110.00 TO NODE   3112.00 =   400.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   3112.00 TO NODE   3113.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.788
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =   14.70   SUBAREA RUNOFF(CFS) =   11.83
 TOTAL AREA(ACRES) =     14.80   TOTAL RUNOFF(CFS) =   11.95
 TC(MIN.) =  20.76

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   3200.00 TO NODE   3201.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.86(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    122.00
 DOWNSTREAM ELEVATION(FEET) =    120.29
 ELEVATION DIFFERENCE(FEET) =      1.71
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.86
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.716
```

```
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
 FLOW PROCESS FROM NODE   3201.00 TO NODE   3202.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   830.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0240
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.55   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =  24.94   Tc(MIN.) =  35.80
 LONGEST FLOWPATH FROM NODE   3200.00 TO NODE   3202.00 =   900.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   3202.00 TO NODE   3203.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.258
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =   47.00   SUBAREA RUNOFF(CFS) =   26.61
 TOTAL AREA(ACRES) =     47.10   TOTAL RUNOFF(CFS) =   26.74
 TC(MIN.) =  35.80

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   3300.00 TO NODE   3301.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.83(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    108.00
 DOWNSTREAM ELEVATION(FEET) =    106.13
 ELEVATION DIFFERENCE(FEET) =      1.87
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.83
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.721
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
```

```
 FLOW PROCESS FROM NODE   3201.00 TO NODE   3202.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   230.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0267
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.56   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =   6.90   Tc(MIN.) =  17.73
 LONGEST FLOWPATH FROM NODE   3300.00 TO NODE   3202.00 =   300.00 FEET.
****************************************************************************
 FLOW PROCESS FROM NODE   3302.00 TO NODE   3303.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.980
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =   11.70   SUBAREA RUNOFF(CFS) =   10.42
 TOTAL AREA(ACRES) =     11.80   TOTAL RUNOFF(CFS) =   10.55
 TC(MIN.) =  17.73
****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   3400.00 TO NODE   3401.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.84(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    118.00
 DOWNSTREAM ELEVATION(FEET) =    116.20
 ELEVATION DIFFERENCE(FEET) =      1.80
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.84
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.719
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12
****************************************************************************
 FLOW PROCESS FROM NODE   3401.00 TO NODE   3402.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
```

```
==========================================================================
  CHANNEL LENGTH THRU SUBAREA(FEET) =   630.00
  REPRESENTATIVE CHANNEL SLOPE =  0.0257
  CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
  MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
  CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
  FLOW VELOCITY(FEET/SEC.) =   0.56   FLOW DEPTH(FEET) =   0.02
  TRAVEL TIME(MIN.) =  18.91   Tc(MIN.) =  29.75
  LONGEST FLOWPATH FROM NODE   3400.00 TO NODE   3402.00 =   700.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE   3402.00 TO NODE   3403.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
    50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.418
  GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
  SOIL CLASSIFICATION IS "D"
  S.C.S. CURVE NUMBER (AMC II) =  84
  SUBAREA AREA(ACRES) =   34.90   SUBAREA RUNOFF(CFS) =   22.27
  TOTAL AREA(ACRES) =     35.00   TOTAL RUNOFF(CFS) =   22.39
  TC(MIN.) =  29.75

****************************************************************************
  FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
  >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
  FLOW PROCESS FROM NODE   3500.00 TO NODE   3501.00 IS CODE =  21
----------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
  GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
  SOIL CLASSIFICATION IS "D"
  S.C.S. CURVE NUMBER (AMC II) =  84
  NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
  WITH 10-MIN. ADDED =  10.85(MIN.)
  INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
  UPSTREAM ELEVATION(FEET) =    110.00
  DOWNSTREAM ELEVATION(FEET) =    108.25
  ELEVATION DIFFERENCE(FEET) =      1.75
  NATURAL WATERSHED TIME OF CONCENTRATION =  10.85
    50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.717
  SUBAREA RUNOFF(CFS) =      0.12
  TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
  FLOW PROCESS FROM NODE   3501.00 TO NODE   3502.00 IS CODE =  51
----------------------------------------------------------------------------
  >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
  >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
  CHANNEL LENGTH THRU SUBAREA(FEET) =   330.00
  REPRESENTATIVE CHANNEL SLOPE =  0.0250
  CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
```

```
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.55   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =   9.91   Tc(MIN.) =  20.76
 LONGEST FLOWPATH FROM NODE   3500.00 TO NODE   3502.00 =   400.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   3502.00 TO NODE   3503.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.788
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =   16.40   SUBAREA RUNOFF(CFS) =   13.20
 TOTAL AREA(ACRES) =     16.50   TOTAL RUNOFF(CFS) =   13.32
 TC(MIN.) =  20.76

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   3600.00 TO NODE   3601.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.83(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    108.00
 DOWNSTREAM ELEVATION(FEET) =    106.13
 ELEVATION DIFFERENCE(FEET) =      1.87
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.83
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.721
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
 FLOW PROCESS FROM NODE   3601.00 TO NODE   3602.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   230.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0267
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.56   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =   6.90   Tc(MIN.) =  17.73
```

```
 LONGEST FLOWPATH FROM NODE   3600.00 TO NODE   3602.00 =   300.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   3602.00 TO NODE   3603.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.980
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =   12.10   SUBAREA RUNOFF(CFS) =   10.78
 TOTAL AREA(ACRES) =     12.20   TOTAL RUNOFF(CFS) =   10.90
 TC(MIN.) =  17.73

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   3700.00 TO NODE   3701.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.85(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    120.00
 DOWNSTREAM ELEVATION(FEET) =    118.25
 ELEVATION DIFFERENCE(FEET) =     1.75
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.85
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.717
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
 FLOW PROCESS FROM NODE   3701.00 TO NODE   3702.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   730.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.55   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =  21.92   Tc(MIN.) =  32.77
 LONGEST FLOWPATH FROM NODE   3700.00 TO NODE   3702.00 =   800.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   3702.00 TO NODE   3703.00 IS CODE =  81
```

```
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
    50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.332
  GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
  SOIL CLASSIFICATION IS "D"
  S.C.S. CURVE NUMBER (AMC II) =  84
  SUBAREA AREA(ACRES) =   46.00   SUBAREA RUNOFF(CFS) =   27.57
  TOTAL AREA(ACRES) =     46.10   TOTAL RUNOFF(CFS) =   27.69
  TC(MIN.) =  32.77

****************************************************************************
  FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
  >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
  FLOW PROCESS FROM NODE   3800.00 TO NODE   3801.00 IS CODE =  21
----------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
  GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
  SOIL CLASSIFICATION IS "D"
  S.C.S. CURVE NUMBER (AMC II) =  84
  NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
  WITH 10-MIN. ADDED =  10.85(MIN.)
  INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
  UPSTREAM ELEVATION(FEET) =    125.00
  DOWNSTREAM ELEVATION(FEET) =    123.25
  ELEVATION DIFFERENCE(FEET) =      1.75
  NATURAL WATERSHED TIME OF CONCENTRATION =  10.85
    50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.717
  SUBAREA RUNOFF(CFS) =      0.12
  TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
  FLOW PROCESS FROM NODE   3801.00 TO NODE   3802.00 IS CODE =  51
----------------------------------------------------------------------------
  >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
  >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
  CHANNEL LENGTH THRU SUBAREA(FEET) =   930.00
  REPRESENTATIVE CHANNEL SLOPE =  0.0250
  CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
  MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
  CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
  FLOW VELOCITY(FEET/SEC.) =   0.55   FLOW DEPTH(FEET) =   0.02
  TRAVEL TIME(MIN.) =  27.93   Tc(MIN.) =  38.78
  LONGEST FLOWPATH FROM NODE   3800.00 TO NODE   3802.00 =  1000.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE   3802.00 TO NODE   3803.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
    50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.195
```

```
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =   51.30   SUBAREA RUNOFF(CFS) =   27.59
 TOTAL AREA(ACRES) =     51.40   TOTAL RUNOFF(CFS) =   27.71
 TC(MIN.) =  38.78

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2100.00 TO NODE   2101.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.85(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    128.00
 DOWNSTREAM ELEVATION(FEET) =    126.22
 ELEVATION DIFFERENCE(FEET) =      1.78
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.85
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.718
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
 FLOW PROCESS FROM NODE   2101.00 TO NODE   2102.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =  1030.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0255
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.56   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =  30.92   Tc(MIN.) =  41.77
 LONGEST FLOWPATH FROM NODE   2100.00 TO NODE   2102.00 =  1100.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2102.00 TO NODE   2103.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.139
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =   33.20   SUBAREA RUNOFF(CFS) =   17.02
```

```
 TOTAL AREA(ACRES) =     33.30   TOTAL RUNOFF(CFS) =   17.14
 TC(MIN.) =  41.77

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2200.00 TO NODE   2201.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.85(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    163.00
 DOWNSTREAM ELEVATION(FEET) =    161.24
 ELEVATION DIFFERENCE(FEET) =      1.76
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.85
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.718
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
 FLOW PROCESS FROM NODE   2201.00 TO NODE   2202.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =  2430.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0252
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.56   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =  72.97   Tc(MIN.) =  83.82
 LONGEST FLOWPATH FROM NODE   2200.00 TO NODE   2202.00 =  2500.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2202.00 TO NODE   2203.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  0.727
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =  126.10   SUBAREA RUNOFF(CFS) =   41.25
 TOTAL AREA(ACRES) =    126.20   TOTAL RUNOFF(CFS) =   41.37
 TC(MIN.) =  83.82

****************************************************************************
```

```
 FLOW PROCESS FROM NODE       0.00 TO NODE       0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE    2180.00 TO NODE    2181.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED = 10.85(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    130.00
 DOWNSTREAM ELEVATION(FEET) =    128.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.85
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.717
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =    0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
 FLOW PROCESS FROM NODE    2181.00 TO NODE    2182.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =  1130.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =  10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.55   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =  33.94   Tc(MIN.) =  44.79
 LONGEST FLOWPATH FROM NODE    2180.00 TO NODE    2182.00 =  1200.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE    2182.00 TO NODE    2183.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.089
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =   97.00   SUBAREA RUNOFF(CFS) =   47.54
 TOTAL AREA(ACRES) =    97.10   TOTAL RUNOFF(CFS) =   47.66
 TC(MIN.) =  44.79

****************************************************************************
 FLOW PROCESS FROM NODE       0.00 TO NODE       0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================
```

```
 S.C.S. CURVE NUMBER (AMC II) =  84
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.86(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    122.00
 DOWNSTREAM ELEVATION(FEET) =    120.29
 ELEVATION DIFFERENCE(FEET) =      1.71
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.86
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.716
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
 FLOW PROCESS FROM NODE   2401.00 TO NODE   2402.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   830.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0244
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.55   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =  24.94   Tc(MIN.) =  35.80
 LONGEST FLOWPATH FROM NODE   2400.00 TO NODE   2402.00 =   900.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2402.00 TO NODE   2403.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.258
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =   67.70   SUBAREA RUNOFF(CFS) =   38.34
 TOTAL AREA(ACRES) =     67.80   TOTAL RUNOFF(CFS) =   38.46
 TC(MIN.) =  35.80

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2500.00 TO NODE   2501.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.85(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
```

```
 UPSTREAM ELEVATION(FEET) =    130.00
 DOWNSTREAM ELEVATION(FEET) =    128.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.85
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.717
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
 FLOW PROCESS FROM NODE   2501.00 TO NODE   2502.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =  1130.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.55   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =  33.94   Tc(MIN.) =  44.79
 LONGEST FLOWPATH FROM NODE   2500.00 TO NODE   2502.00 =  1200.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2502.00 TO NODE   2503.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.089
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =   40.70   SUBAREA RUNOFF(CFS) =   19.95
 TOTAL AREA(ACRES) =   40.80   TOTAL RUNOFF(CFS) =   20.07
 TC(MIN.) =  44.79

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2600.00 TO NODE   2601.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.85(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    130.00
 DOWNSTREAM ELEVATION(FEET) =    128.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.85
```

```
  50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.717
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
 FLOW PROCESS FROM NODE   2601.00 TO NODE   2602.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =  1130.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.55   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =  33.94   Tc(MIN.) =  44.79
 LONGEST FLOWPATH FROM NODE   2600.00 TO NODE   2602.00 =  1200.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2602.00 TO NODE   2603.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.089
 GRASS FAIR COVER RUNOFF COEFFICIENT =.4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =   34.70   SUBAREA RUNOFF(CFS) =   17.00
 TOTAL AREA(ACRES) =     34.80   TOTAL RUNOFF(CFS) =   17.13
 TC(MIN.) =  44.79

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2700.00 TO NODE   2701.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    105.00
 DOWNSTREAM ELEVATION(FEET) =    103.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) =    7.213
  50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.536
 SUBAREA RUNOFF(CFS) =      0.16
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.16

****************************************************************************
 FLOW PROCESS FROM NODE   2701.00 TO NODE   2702.00 IS CODE =  51
```

```
------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
========================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   130.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.16
 FLOW VELOCITY(FEET/SEC.) =   0.55   FLOW DEPTH(FEET) =   0.03
 TRAVEL TIME(MIN.) =   3.96   Tc(MIN.) =  11.17
 LONGEST FLOWPATH FROM NODE   2700.00 TO NODE   2702.00 =   200.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2702.00 TO NODE   2703.00 IS CODE =  81
------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
========================================================================
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.667
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =   14.80   SUBAREA RUNOFF(CFS) =   17.76
 TOTAL AREA(ACRES) =     14.90   TOTAL RUNOFF(CFS) =   17.92
 TC(MIN.) =  11.17

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
========================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2800.00 TO NODE   2801.00 IS CODE =  21
------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
========================================================================
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.18(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    128.00
 DOWNSTREAM ELEVATION(FEET) =     26.22
 ELEVATION DIFFERENCE(FEET) =    101.78
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.18
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.832
 SUBAREA RUNOFF(CFS) =      0.13
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.13

****************************************************************************
 FLOW PROCESS FROM NODE   2801.00 TO NODE   2802.00 IS CODE =  51
------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
========================================================================
```

```
 CHANNEL LENGTH THRU SUBAREA(FEET) =  1030.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.13
 FLOW VELOCITY(FEET/SEC.) =   0.58   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =  29.68   Tc(MIN.) =  39.86
 LONGEST FLOWPATH FROM NODE   2800.00 TO NODE   2802.00 =  1100.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2802.00 TO NODE   2803.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.174
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =   81.20   SUBAREA RUNOFF(CFS) =   42.90
 TOTAL AREA(ACRES) =     81.30   TOTAL RUNOFF(CFS) =   43.03
 TC(MIN.) =  39.86

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2900.00 TO NODE   2901.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.84(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    118.00
 DOWNSTREAM ELEVATION(FEET) =    116.20
 ELEVATION DIFFERENCE(FEET) =      1.80
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.84
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.719
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
 FLOW PROCESS FROM NODE   2901.00 TO NODE   2902.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   630.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
```

```
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.56   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =  18.91   Tc(MIN.) =  29.75
 LONGEST FLOWPATH FROM NODE   2900.00 TO NODE   2902.00 =   700.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2902.00 TO NODE   2903.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.418
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =   36.80   SUBAREA RUNOFF(CFS) =   23.48
 TOTAL AREA(ACRES) =     36.90   TOTAL RUNOFF(CFS) =   23.60
 TC(MIN.) =  29.75

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2910.00 TO NODE   2911.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.85(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    108.00
 DOWNSTREAM ELEVATION(FEET) =    106.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.85
  50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.717
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
 FLOW PROCESS FROM NODE   2911.00 TO NODE   2912.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   230.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.55   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =   6.91   Tc(MIN.) =  17.76
 LONGEST FLOWPATH FROM NODE   2910.00 TO NODE   2912.00 =   300.00 FEET.
```

```
****************************************************************************
  FLOW PROCESS FROM NODE   2912.00 TO NODE   2913.00 IS CODE =  81
----------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
    50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.978
  GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
  SOIL CLASSIFICATION IS "D"
  S.C.S. CURVE NUMBER (AMC II) =  84
  SUBAREA AREA(ACRES) =   12.80   SUBAREA RUNOFF(CFS) =   11.39
  TOTAL AREA(ACRES) =     12.90   TOTAL RUNOFF(CFS) =   11.51
  TC(MIN.) =  17.76

****************************************************************************
  FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
  >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
  FLOW PROCESS FROM NODE   2100.00 TO NODE   2101.00 IS CODE =  21
----------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
  GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
  SOIL CLASSIFICATION IS "D"
  S.C.S. CURVE NUMBER (AMC II) =  84
  NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
  WITH 10-MIN. ADDED =  10.85(MIN.)
  INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
  UPSTREAM ELEVATION(FEET) =    160.00
  DOWNSTREAM ELEVATION(FEET) =    158.25
  ELEVATION DIFFERENCE(FEET) =      1.75
  NATURAL WATERSHED TIME OF CONCENTRATION =  10.85
    50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.717
  SUBAREA RUNOFF(CFS) =      0.12
  TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
  FLOW PROCESS FROM NODE   2101.00 TO NODE   2102.00 IS CODE =  51
----------------------------------------------------------------------------
  >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
  >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
  CHANNEL LENGTH THRU SUBAREA(FEET) =  2330.00
  REPRESENTATIVE CHANNEL SLOPE =  0.0250
  CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
  MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
  CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
  FLOW VELOCITY(FEET/SEC.) =   0.55   FLOW DEPTH(FEET) =   0.02
  TRAVEL TIME(MIN.) =  69.97   Tc(MIN.) =  80.82
  LONGEST FLOWPATH FROM NODE   2100.00 TO NODE   2102.00 =  2400.00 FEET.

****************************************************************************
  FLOW PROCESS FROM NODE   2102.00 TO NODE   2103.00 IS CODE =  81
----------------------------------------------------------------------------
```

```
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
================================================================================
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  0.744
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =  128.30   SUBAREA RUNOFF(CFS) =   42.96
 TOTAL AREA(ACRES) =    128.40   TOTAL RUNOFF(CFS) =   43.09
 TC(MIN.) =  80.82

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
================================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2110.00 TO NODE   2111.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
================================================================================
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.85(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    143.00
 DOWNSTREAM ELEVATION(FEET) =    141.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.85
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.717
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
 FLOW PROCESS FROM NODE   2111.00 TO NODE   2112.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
================================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =  1630.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.55   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =  48.95   Tc(MIN.) =  59.80
 LONGEST FLOWPATH FROM NODE   2110.00 TO NODE   2112.00 =  1700.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2112.00 TO NODE   2113.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
================================================================================
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  0.904
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
```

```
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =  275.50   SUBAREA RUNOFF(CFS) =  112.04
 TOTAL AREA(ACRES) =    275.60   TOTAL RUNOFF(CFS) =  112.16
 TC(MIN.) =  59.80

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2120.00 TO NODE   2121.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.85(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    113.00
 DOWNSTREAM ELEVATION(FEET) =    111.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.85
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.717
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
 FLOW PROCESS FROM NODE   2121.00 TO NODE   2122.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   430.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.55   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =  12.91   Tc(MIN.) =  23.76
 LONGEST FLOWPATH FROM NODE   2120.00 TO NODE   2122.00 =   500.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2122.00 TO NODE   2123.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.639
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =   23.50   SUBAREA RUNOFF(CFS) =   17.33
 TOTAL AREA(ACRES) =     23.60   TOTAL RUNOFF(CFS) =   17.45
```

```
 TC(MIN.) =  23.76

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2130.00 TO NODE   2131.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.85(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    115.00
 DOWNSTREAM ELEVATION(FEET) =    113.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.85
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.717
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
 FLOW PROCESS FROM NODE   2131.00 TO NODE   2132.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   530.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.55   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =  15.92   Tc(MIN.) =  26.77
 LONGEST FLOWPATH FROM NODE   2130.00 TO NODE   2132.00 =   600.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2132.00 TO NODE   2133.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.518
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =   61.40   SUBAREA RUNOFF(CFS) =   41.94
 TOTAL AREA(ACRES) =     61.50   TOTAL RUNOFF(CFS) =   42.06
 TC(MIN.) =  26.77

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
```

```
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2140.00 TO NODE   2141.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.85(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    125.00
 DOWNSTREAM ELEVATION(FEET) =    123.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.85
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.717
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
 FLOW PROCESS FROM NODE   2141.00 TO NODE   2142.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   930.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.55   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =  27.93   Tc(MIN.) =  38.78
 LONGEST FLOWPATH FROM NODE   2140.00 TO NODE   2142.00 =  1000.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2142.00 TO NODE   2143.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.195
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =   48.30   SUBAREA RUNOFF(CFS) =   25.97
 TOTAL AREA(ACRES) =   48.40   TOTAL RUNOFF(CFS) =   26.10
 TC(MIN.) =  38.78

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================
```

```
****************************************************************************
 FLOW PROCESS FROM NODE   2150.00 TO NODE   2151.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.85(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    150.00
 DOWNSTREAM ELEVATION(FEET) =    148.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.85
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.717
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
 FLOW PROCESS FROM NODE   2151.00 TO NODE   2152.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =  1930.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.55   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =  57.96   Tc(MIN.) =  68.81
 LONGEST FLOWPATH FROM NODE   2150.00 TO NODE   2152.00 =  2000.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2152.00 TO NODE   2153.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  0.826
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =  153.70   SUBAREA RUNOFF(CFS) =   57.10
 TOTAL AREA(ACRES) =   153.80   TOTAL RUNOFF(CFS) =   57.22
 TC(MIN.) =  68.81

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2160.00 TO NODE   2161.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
```

```
================================================================================
  GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
  SOIL CLASSIFICATION IS "D"
  S.C.S. CURVE NUMBER (AMC II) =  84
  NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
  WITH 10-MIN. ADDED =  10.85(MIN.)
  INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
  UPSTREAM ELEVATION(FEET) =    160.00
  DOWNSTREAM ELEVATION(FEET) =    158.25
  ELEVATION DIFFERENCE(FEET) =      1.75
  NATURAL WATERSHED TIME OF CONCENTRATION =  10.85
    50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.717
  SUBAREA RUNOFF(CFS) =      0.12
  TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

********************************************************************************
  FLOW PROCESS FROM NODE   2161.00 TO NODE   2162.00 IS CODE =  51
--------------------------------------------------------------------------------
  >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
  >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
================================================================================
  CHANNEL LENGTH THRU SUBAREA(FEET) =  2330.00
  REPRESENTATIVE CHANNEL SLOPE =  0.0250
  CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
  MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
  CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
  FLOW VELOCITY(FEET/SEC.) =   0.55   FLOW DEPTH(FEET) =   0.02
  TRAVEL TIME(MIN.) =  69.97   Tc(MIN.) =  80.82
  LONGEST FLOWPATH FROM NODE   2160.00 TO NODE   2162.00 =  2400.00 FEET.

********************************************************************************
  FLOW PROCESS FROM NODE   2162.00 TO NODE   2163.00 IS CODE =  81
--------------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
================================================================================
    50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  0.744
  GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
  SOIL CLASSIFICATION IS "D"
  S.C.S. CURVE NUMBER (AMC II) =  84
  SUBAREA AREA(ACRES) =  121.60   SUBAREA RUNOFF(CFS) =   40.72
  TOTAL AREA(ACRES) =    121.70   TOTAL RUNOFF(CFS) =   40.84
  TC(MIN.) =  80.82

********************************************************************************
  FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
--------------------------------------------------------------------------------
  >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
================================================================================

********************************************************************************
  FLOW PROCESS FROM NODE   2170.00 TO NODE   2171.00 IS CODE =  21
--------------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
================================================================================
  GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
  SOIL CLASSIFICATION IS "D"
  S.C.S. CURVE NUMBER (AMC II) =  84
```

```
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.85(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    175.00
 DOWNSTREAM ELEVATION(FEET) =    173.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.85
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.717
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
 FLOW PROCESS FROM NODE   2171.00 TO NODE   2172.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =  2930.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.55   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) =  87.99   Tc(MIN.) =  98.84
 LONGEST FLOWPATH FROM NODE   2170.00 TO NODE   2172.00 =  3000.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2172.00 TO NODE   2173.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  0.654
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =   60.20   SUBAREA RUNOFF(CFS) =   17.70
 TOTAL AREA(ACRES) =     60.30   TOTAL RUNOFF(CFS) =   17.83
 TC(MIN.) =  98.84

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   9990.00 TO NODE   9991.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 NATURAL WATERSHED NOMOGRAPH TIME OF CONCENTRATION (APPENDIX X-A)
 WITH 10-MIN. ADDED =  10.85(MIN.)
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =   1300.00
```

```
 DOWNSTREAM ELEVATION(FEET) =   1298.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 NATURAL WATERSHED TIME OF CONCENTRATION =  10.85
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.717
 SUBAREA RUNOFF(CFS) =      0.12
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.12

****************************************************************************
 FLOW PROCESS FROM NODE   9991.00 TO NODE   9992.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =  9930.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0300
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.12
 FLOW VELOCITY(FEET/SEC.) =   0.55   FLOW DEPTH(FEET) =   0.02
 TRAVEL TIME(MIN.) = 298.21   Tc(MIN.) = 309.06
 LONGEST FLOWPATH FROM NODE   9990.00 TO NODE   9992.00 = 10000.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   9992.00 TO NODE   9993.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
   50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  0.313
 GRASS FAIR COVER RUNOFF COEFFICIENT = .4500
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  84
 SUBAREA AREA(ACRES) =  774.70   SUBAREA RUNOFF(CFS) =  109.22
 TOTAL AREA(ACRES) =    774.80   TOTAL RUNOFF(CFS) =  109.34
 TC(MIN.) = 309.06
============================================================================
 END OF STUDY SUMMARY:
 TOTAL AREA(ACRES)      =    774.80  TC(MIN.) =    309.06
 PEAK FLOW RATE(CFS)    =    109.34
============================================================================
============================================================================
 END OF RATIONAL METHOD ANALYSIS
```

Q100

```
**************************************************************************

          RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
          Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT
                       2003,1985,1981 HYDROLOGY MANUAL
        (c) Copyright 1982-2003 Advanced Engineering Software (aes)
            Ver. 1.5A Release Date: 01/01/2003  License ID 1499

                          Analysis prepared by:

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 ************************** DESCRIPTION OF STUDY **************************
* Otay Mesa Watershed Analysis                                            *
* 100 Year Storm Event P=1.90                                             *
* 5/20/05 AMC                                                             *
 **************************************************************************

  FILE NAME: C:\Drainage\407000\CPU100yr.DAT
  TIME/DATE OF STUDY: 11:16 05/20/2005
--------------------------------------------------------------------------
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
--------------------------------------------------------------------------
  2003 SAN DIEGO MANUAL CRITERIA

  USER SPECIFIED STORM EVENT(YEAR) = 100.00
  6-HOUR DURATION PRECIPITATION (INCHES) =   1.900
  SPECIFIED MINIMUM PIPE SIZE(INCH) =  18.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 1.00
  SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
  NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS
  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-   CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH  CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)     (FT)    SIDE / SIDE/ WAY    (FT)    (FT)  (FT)  (FT)    (n)
===  =====  =========  ==================  ======  ===== ====== ===== =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0312 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

**************************************************************************
  FLOW PROCESS FROM NODE   3100.00 TO NODE   3101.00 IS CODE =  21
--------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
==========================================================================
  STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
  SOIL CLASSIFICATION IS "D"
  S.C.S. CURVE NUMBER (AMC II) =  93
```

```
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    106.00
 DOWNSTREAM ELEVATION(FEET) =    104.32
 ELEVATION DIFFERENCE(FEET) =      1.68
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.387
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   3101.00 TO NODE   3102.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   180.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0240
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =   3.50   Tc(MIN.) =   7.89
 LONGEST FLOWPATH FROM NODE   3100.00 TO NODE   3102.00 =  250.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   3102.00 TO NODE   3103.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.730
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   19.30   SUBAREA RUNOFF(CFS) =   51.11
 TOTAL AREA(ACRES) =   19.40   TOTAL RUNOFF(CFS) =   51.37
 TC(MIN.) =   7.89

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   3110.00 TO NODE   3111.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    110.00
 DOWNSTREAM ELEVATION(FEET) =    108.25
 ELEVATION DIFFERENCE(FEET) =      1.75
```

```
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.328
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   3111.00 TO NODE   3112.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   330.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =   6.42   Tc(MIN.) =  10.75
 LONGEST FLOWPATH FROM NODE   3110.00 TO NODE   3112.00 =   400.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   3112.00 TO NODE   3113.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.055
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   14.70   SUBAREA RUNOFF(CFS) =   31.89
 TOTAL AREA(ACRES) =     14.80   TOTAL RUNOFF(CFS) =   32.10
 TC(MIN.) =  10.75

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   3200.00 TO NODE   3201.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    122.00
 DOWNSTREAM ELEVATION(FEET) =    120.29
 ELEVATION DIFFERENCE(FEET) =      1.71
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.361
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
```

```
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   3201.00 TO NODE   3202.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   830.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0240
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =  16.16   Tc(MIN.) =  20.52
 LONGEST FLOWPATH FROM NODE   3200.00 TO NODE   3202.00 =   900.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   3202.00 TO NODE   3203.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.014
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   47.00   SUBAREA RUNOFF(CFS) =   67.20
 TOTAL AREA(ACRES) =     47.10   TOTAL RUNOFF(CFS) =   67.34
 TC(MIN.) =  20.52

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   3300.00 TO NODE   3301.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    108.00
 DOWNSTREAM ELEVATION(FEET) =    106.13
 ELEVATION DIFFERENCE(FEET) =      1.87
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.233
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   3201.00 TO NODE   3202.00 IS CODE =  51
```

```
------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
========================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   230.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0267
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =  4.48   Tc(MIN.) =   8.71
 LONGEST FLOWPATH FROM NODE   3300.00 TO NODE   3202.00 =   300.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   3302.00 TO NODE   3303.00 IS CODE =  81
------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
========================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.500
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   11.70   SUBAREA RUNOFF(CFS) =   29.07
 TOTAL AREA(ACRES) =     11.80   TOTAL RUNOFF(CFS) =   29.32
 TC(MIN.) =   8.71

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
========================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   3400.00 TO NODE   3401.00 IS CODE =  21
------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
========================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    118.00
 DOWNSTREAM ELEVATION(FEET) =    116.20
 ELEVATION DIFFERENCE(FEET) =      1.80
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.287
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =     0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   3401.00 TO NODE   3402.00 IS CODE =  51
------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
========================================================================
```

```
 CHANNEL LENGTH THRU SUBAREA(FEET) =   630.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0257
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =  12.26   Tc(MIN.) =  16.55
 LONGEST FLOWPATH FROM NODE   3400.00 TO NODE   3402.00 =   700.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   3402.00 TO NODE   3403.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.313
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   34.90   SUBAREA RUNOFF(CFS) =   57.32
 TOTAL AREA(ACRES) =     35.00   TOTAL RUNOFF(CFS) =   57.48
 TC(MIN.) =  16.55

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   3500.00 TO NODE   3501.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    110.00
 DOWNSTREAM ELEVATION(FEET) =    108.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.328
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   3501.00 TO NODE   3502.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   330.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
```

```
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =   6.42   Tc(MIN.) =  10.75
 LONGEST FLOWPATH FROM NODE   3500.00 TO NODE   3502.00 =   400.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   3502.00 TO NODE   3503.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.055
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   16.40   SUBAREA RUNOFF(CFS) =   35.57
 TOTAL AREA(ACRES) =     16.50   TOTAL RUNOFF(CFS) =   35.79
 TC(MIN.) =  10.75

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   3600.00 TO NODE   3601.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    108.00
 DOWNSTREAM ELEVATION(FEET) =    106.13
 ELEVATION DIFFERENCE(FEET) =      1.87
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.233
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   3601.00 TO NODE   3602.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =  230.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0267
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =   4.48   Tc(MIN.) =   8.71
 LONGEST FLOWPATH FROM NODE   3600.00 TO NODE   3602.00 =   300.00 FEET.
```

```
****************************************************************************
 FLOW PROCESS FROM NODE   3602.00 TO NODE   3603.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.500
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   12.10   SUBAREA RUNOFF(CFS) =   30.06
 TOTAL AREA(ACRES) =     12.20   TOTAL RUNOFF(CFS) =   30.31
 TC(MIN.) =   8.71

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   3700.00 TO NODE   3701.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    120.00
 DOWNSTREAM ELEVATION(FEET) =    118.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.328
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   3701.00 TO NODE   3702.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   730.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =  14.21   Tc(MIN.) =  18.54
 LONGEST FLOWPATH FROM NODE   3700.00 TO NODE   3702.00 =   800.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   3702.00 TO NODE   3703.00 IS CODE =  81
----------------------------------------------------------------------------
```

```
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
================================================================================
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.150
  STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
  SOIL CLASSIFICATION IS "D"
  S.C.S. CURVE NUMBER (AMC II) =  93
  AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
  SUBAREA AREA(ACRES) =    46.00   SUBAREA RUNOFF(CFS) =   70.22
  TOTAL AREA(ACRES) =      46.10   TOTAL RUNOFF(CFS) =   70.37
  TC(MIN.) =  18.54

********************************************************************************
  FLOW PROCESS FROM NODE       0.00 TO NODE       0.00 IS CODE =  13
--------------------------------------------------------------------------------
  >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
================================================================================

********************************************************************************
  FLOW PROCESS FROM NODE    3800.00 TO NODE    3801.00 IS CODE =  21
--------------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
================================================================================
  STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
  SOIL CLASSIFICATION IS "D"
  S.C.S. CURVE NUMBER (AMC II) =  93
  INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
  UPSTREAM ELEVATION(FEET) =    125.00
  DOWNSTREAM ELEVATION(FEET) =    123.25
  ELEVATION DIFFERENCE(FEET) =      1.75
  SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.328
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
  NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
  SUBAREA RUNOFF(CFS) =      0.36
  TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

********************************************************************************
  FLOW PROCESS FROM NODE    3801.00 TO NODE    3802.00 IS CODE =  51
--------------------------------------------------------------------------------
  >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
  >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
================================================================================
  CHANNEL LENGTH THRU SUBAREA(FEET) =   930.00
  REPRESENTATIVE CHANNEL SLOPE =  0.0250
  CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
  MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
  CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
  FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
  TRAVEL TIME(MIN.) =  18.10   Tc(MIN.) =  22.43
  LONGEST FLOWPATH FROM NODE    3800.00 TO NODE    3802.00 =  1000.00 FEET.

********************************************************************************
  FLOW PROCESS FROM NODE    3802.00 TO NODE    3803.00 IS CODE =  81
--------------------------------------------------------------------------------
  >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
================================================================================
   100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.901
  STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
```

```
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   51.30   SUBAREA RUNOFF(CFS) =   69.25
 TOTAL AREA(ACRES) =     51.40   TOTAL RUNOFF(CFS) =   69.38
 TC(MIN.) =  22.43

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2100.00 TO NODE   2101.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =   70.00
 UPSTREAM ELEVATION(FEET) =    128.00
 DOWNSTREAM ELEVATION(FEET) =    126.22
 ELEVATION DIFFERENCE(FEET) =      1.78
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.303
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   2101.00 TO NODE   2102.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =  1030.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0255
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =     0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =  20.05   Tc(MIN.) =  24.35
 LONGEST FLOWPATH FROM NODE   2100.00 TO NODE   2102.00 =  1100.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2102.00 TO NODE   2103.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.803
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   33.20   SUBAREA RUNOFF(CFS) =   42.50
```

```
 TOTAL AREA(ACRES) =     33.30   TOTAL RUNOFF(CFS) =   42.63
 TC(MIN.) =  24.35

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2200.00 TO NODE   2201.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    163.00
 DOWNSTREAM ELEVATION(FEET) =    161.24
 ELEVATION DIFFERENCE(FEET) =      1.76
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.319
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   2201.00 TO NODE   2202.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =  2430.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0252
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =  47.30   Tc(MIN.) =  51.62
 LONGEST FLOWPATH FROM NODE   2200.00 TO NODE   2202.00 =  2500.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2202.00 TO NODE   2203.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.111
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =  126.10   SUBAREA RUNOFF(CFS) =   99.43
 TOTAL AREA(ACRES) =    126.20   TOTAL RUNOFF(CFS) =   99.51
 TC(MIN.) =  51.62

****************************************************************************
```

```
 FLOW PROCESS FROM NODE       0.00 TO NODE       0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE    2180.00 TO NODE    2181.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    130.00
 DOWNSTREAM ELEVATION(FEET) =    128.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.328
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE    2181.00 TO NODE    2182.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =  1130.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =  22.00   Tc(MIN.) =  26.32
 LONGEST FLOWPATH FROM NODE   2180.00 TO NODE   2182.00 =  1200.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE    2182.00 TO NODE    2183.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.715
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   97.00   SUBAREA RUNOFF(CFS) =  118.10
 TOTAL AREA(ACRES) =    97.10   TOTAL RUNOFF(CFS) =  118.22
 TC(MIN.) =  26.32

****************************************************************************
 FLOW PROCESS FROM NODE       0.00 TO NODE       0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================
```

```
****************************************************************************
 FLOW PROCESS FROM NODE   2190.00 TO NODE   2191.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    110.00
 DOWNSTREAM ELEVATION(FEET) =    108.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.328
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   2191.00 TO NODE   2192.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   330.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =   6.42   Tc(MIN.) =  10.75
 LONGEST FLOWPATH FROM NODE   2190.00 TO NODE   2192.00 =   400.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2192.00 TO NODE   2193.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.055
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   27.60   SUBAREA RUNOFF(CFS) =   59.87
 TOTAL AREA(ACRES) =     27.70   TOTAL RUNOFF(CFS) =   60.09
 TC(MIN.) =  10.75

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2300.00 TO NODE   2301.00 IS CODE =  21
----------------------------------------------------------------------------
```

```
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
================================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    113.00
 DOWNSTREAM ELEVATION(FEET) =    111.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.328
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

********************************************************************************
 FLOW PROCESS FROM NODE   2301.00 TO NODE   2302.00 IS CODE =  51
--------------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
================================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   450.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =   8.76   Tc(MIN.) =  13.09
 LONGEST FLOWPATH FROM NODE   2300.00 TO NODE   2302.00 =   520.00 FEET.

********************************************************************************
 FLOW PROCESS FROM NODE   2302.00 TO NODE   2303.00 IS CODE =  81
--------------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
================================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.691
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   20.00   SUBAREA RUNOFF(CFS) =   38.22
 TOTAL AREA(ACRES) =   20.10   TOTAL RUNOFF(CFS) =   38.41
 TC(MIN.) =  13.09

********************************************************************************
 FLOW PROCESS FROM NODE    0.00 TO NODE      0.00 IS CODE =  13
--------------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
================================================================================

********************************************************************************
 FLOW PROCESS FROM NODE   2400.00 TO NODE   2401.00 IS CODE =  21
--------------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
================================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
```

```
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    122.00
 DOWNSTREAM ELEVATION(FEET) =    120.29
 ELEVATION DIFFERENCE(FEET) =      1.71
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.361
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   2401.00 TO NODE   2402.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   830.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0244
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =  16.16   Tc(MIN.) =  20.52
 LONGEST FLOWPATH FROM NODE   2400.00 TO NODE   2402.00 =   900.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2402.00 TO NODE   2403.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.014
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   67.70   SUBAREA RUNOFF(CFS) =   96.79
 TOTAL AREA(ACRES) =   67.80   TOTAL RUNOFF(CFS) =   96.94
 TC(MIN.) =  20.52

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2500.00 TO NODE   2501.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    130.00
 DOWNSTREAM ELEVATION(FEET) =    128.25
```

```
 ELEVATION DIFFERENCE(FEET) =      1.75
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.328
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   2501.00 TO NODE   2502.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =  1130.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =  22.00   Tc(MIN.) =  26.32
 LONGEST FLOWPATH FROM NODE   2500.00 TO NODE   2502.00 =  1200.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2502.00 TO NODE   2503.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.715
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   40.70   SUBAREA RUNOFF(CFS) =   49.55
 TOTAL AREA(ACRES) =     40.80   TOTAL RUNOFF(CFS) =   49.67
 TC(MIN.) =  26.32

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2600.00 TO NODE   2601.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    130.00
 DOWNSTREAM ELEVATION(FEET) =    128.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.328
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
```

```
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   2601.00 TO NODE   2602.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =  1130.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =  22.00   Tc(MIN.) =  26.32
 LONGEST FLOWPATH FROM NODE   2600.00 TO NODE   2602.00 =  1200.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2602.00 TO NODE   2603.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.715
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   34.70   SUBAREA RUNOFF(CFS) =   42.25
 TOTAL AREA(ACRES) =     34.80   TOTAL RUNOFF(CFS) =   42.37
 TC(MIN.) =  26.32

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2700.00 TO NODE   2701.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    105.00
 DOWNSTREAM ELEVATION(FEET) =    103.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.328
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
```

```
 FLOW PROCESS FROM NODE   2701.00 TO NODE   2702.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   130.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =   2.53   Tc(MIN.) =   6.86
 LONGEST FLOWPATH FROM NODE   2700.00 TO NODE   2702.00 =   200.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2702.00 TO NODE   2703.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.083
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   14.80   SUBAREA RUNOFF(CFS) =   42.90
 TOTAL AREA(ACRES) =     14.90   TOTAL RUNOFF(CFS) =   43.19
 TC(MIN.) =   6.86

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2800.00 TO NODE   2801.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    128.00
 DOWNSTREAM ELEVATION(FEET) =     26.22
 ELEVATION DIFFERENCE(FEET) =    101.78
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    2.726
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   2801.00 TO NODE   2802.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
```

```
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
================================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =  1030.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =  20.05   Tc(MIN.) =  22.78
 LONGEST FLOWPATH FROM NODE   2800.00 TO NODE   2802.00 =  1100.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2802.00 TO NODE   2803.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
================================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.883
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   81.20   SUBAREA RUNOFF(CFS) =  108.53
 TOTAL AREA(ACRES) =     81.30   TOTAL RUNOFF(CFS) =  108.67
 TC(MIN.) =  22.78

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
================================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2900.00 TO NODE   2901.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
================================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    118.00
 DOWNSTREAM ELEVATION(FEET) =    116.20
 ELEVATION DIFFERENCE(FEET) =      1.80
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.287
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   2901.00 TO NODE   2902.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
================================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   630.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
```

```
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =  12.26   Tc(MIN.) =  16.55
 LONGEST FLOWPATH FROM NODE   2900.00 TO NODE   2902.00 =   700.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2902.00 TO NODE   2903.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.313
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   36.80   SUBAREA RUNOFF(CFS) =   60.44
 TOTAL AREA(ACRES) =     36.90   TOTAL RUNOFF(CFS) =   60.60
 TC(MIN.) =  16.55

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2910.00 TO NODE   2911.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    108.00
 DOWNSTREAM ELEVATION(FEET) =    106.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.328
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   2911.00 TO NODE   2912.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   230.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
```

```
 TRAVEL TIME(MIN.) =   4.48   Tc(MIN.) =   8.80
 LONGEST FLOWPATH FROM NODE   2910.00 TO NODE   2912.00 =   300.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2912.00 TO NODE   2913.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.475
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   12.80   SUBAREA RUNOFF(CFS) =   31.58
 TOTAL AREA(ACRES) =     12.90   TOTAL RUNOFF(CFS) =   31.83
 TC(MIN.) =   8.80

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2100.00 TO NODE   2101.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    160.00
 DOWNSTREAM ELEVATION(FEET) =    158.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.328
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   2101.00 TO NODE   2102.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =  2330.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =  45.35   Tc(MIN.) =  49.68
 LONGEST FLOWPATH FROM NODE   2100.00 TO NODE   2102.00 =  2400.00 FEET.

****************************************************************************
```

```
 FLOW PROCESS FROM NODE   2102.00 TO NODE   2103.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.138
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =  128.30   SUBAREA RUNOFF(CFS) =  103.70
 TOTAL AREA(ACRES) =    128.40   TOTAL RUNOFF(CFS) =  103.78
 TC(MIN.) =  49.68

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2110.00 TO NODE   2111.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    143.00
 DOWNSTREAM ELEVATION(FEET) =    141.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.328
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   2111.00 TO NODE   2112.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =  1630.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =  31.73   Tc(MIN.) =  36.06
 LONGEST FLOWPATH FROM NODE   2110.00 TO NODE   2112.00 =  1700.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2112.00 TO NODE   2113.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
```

```
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.400
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =  275.50   SUBAREA RUNOFF(CFS) =  273.81
 TOTAL AREA(ACRES) =    275.60   TOTAL RUNOFF(CFS) =  273.91
 TC(MIN.) =  36.06

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2120.00 TO NODE   2121.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    113.00
 DOWNSTREAM ELEVATION(FEET) =  111.25
 ELEVATION DIFFERENCE(FEET) =    1.75
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =   4.328
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   2121.00 TO NODE   2122.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   430.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00  "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =   8.37   Tc(MIN.) =  12.70
 LONGEST FLOWPATH FROM NODE   2120.00 TO NODE   2122.00 =   500.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2122.00 TO NODE   2123.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.744
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
```

```
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   23.50   SUBAREA RUNOFF(CFS) =   45.79
 TOTAL AREA(ACRES) =     23.60   TOTAL RUNOFF(CFS) =   45.98
 TC(MIN.) =  12.70

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2130.00 TO NODE   2131.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    115.00
 DOWNSTREAM ELEVATION(FEET) =    113.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.328
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   2131.00 TO NODE   2132.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   530.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =  10.32   Tc(MIN.) =  14.64
 LONGEST FLOWPATH FROM NODE   2130.00 TO NODE   2132.00 =   600.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2132.00 TO NODE   2133.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  2.503
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   61.40   SUBAREA RUNOFF(CFS) =  109.12
 TOTAL AREA(ACRES) =     61.50   TOTAL RUNOFF(CFS) =  109.30
 TC(MIN.) =  14.64
```

```
****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2140.00 TO NODE   2141.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    125.00
 DOWNSTREAM ELEVATION(FEET) =    123.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.328
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   2141.00 TO NODE   2142.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =   930.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =  18.10   Tc(MIN.) =  22.43
 LONGEST FLOWPATH FROM NODE   2140.00 TO NODE   2142.00 =  1000.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2142.00 TO NODE   2143.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.901
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   48.30   SUBAREA RUNOFF(CFS) =   65.20
 TOTAL AREA(ACRES) =    48.40   TOTAL RUNOFF(CFS) =   65.33
 TC(MIN.) =  22.43

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
```

```
 FLOW PROCESS FROM NODE   2160.00 TO NODE   2161.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    160.00
 DOWNSTREAM ELEVATION(FEET) =    158.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.328
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   2161.00 TO NODE   2162.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =  2330.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET):=   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR =0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =  45.35   Tc(MIN.) =  49.68
 LONGEST FLOWPATH FROM NODE   2160.00 TO NODE   2162.00 =  2400.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2162.00 TO NODE   2163.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  1.138
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =  121.60   SUBAREA RUNOFF(CFS) =   98.28
 TOTAL AREA(ACRES) =   121.70   TOTAL RUNOFF(CFS) =   98.36
 TC(MIN.) =  49.68

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   2170.00 TO NODE   2171.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
```

```
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
 UPSTREAM ELEVATION(FEET) =    175.00
 DOWNSTREAM ELEVATION(FEET) =    173.25
 ELEVATION DIFFERENCE(FEET) =      1.75
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.328
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =      0.36
 TOTAL AREA(ACRES) =      0.10   TOTAL RUNOFF(CFS) =      0.36

****************************************************************************
 FLOW PROCESS FROM NODE   2171.00 TO NODE   2172.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =  2930.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0250
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =      0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) =  57.03   Tc(MIN.) =  61.36
 LONGEST FLOWPATH FROM NODE   2170.00 TO NODE   2172.00 =  3000.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE   2172.00 TO NODE   2173.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  0.993
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =   60.20   SUBAREA RUNOFF(CFS) =   42.46
 TOTAL AREA(ACRES) =     60.30   TOTAL RUNOFF(CFS) =   42.53
 TC(MIN.) =  61.36

****************************************************************************
 FLOW PROCESS FROM NODE      0.00 TO NODE      0.00 IS CODE =  13
----------------------------------------------------------------------------
 >>>>>CLEAR THE MAIN-STREAM MEMORY<<<<<
============================================================================

****************************************************************************
 FLOW PROCESS FROM NODE   9990.00 TO NODE   9991.00 IS CODE =  21
----------------------------------------------------------------------------
 >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
============================================================================
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 INITIAL SUBAREA FLOW-LENGTH(FEET) =    70.00
```

```
 UPSTREAM ELEVATION(FEET) =    1300.00
 DOWNSTREAM ELEVATION(FEET) =    1298.25
 ELEVATION DIFFERENCE(FEET) =       1.75
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =     4.328
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.006
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
 SUBAREA RUNOFF(CFS) =       0.36
 TOTAL AREA(ACRES) =       0.10   TOTAL RUNOFF(CFS) =       0.36

****************************************************************************
 FLOW PROCESS FROM NODE    9991.00 TO NODE    9992.00 IS CODE =  51
----------------------------------------------------------------------------
 >>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
============================================================================
 CHANNEL LENGTH THRU SUBAREA(FEET) =  9930.00
 REPRESENTATIVE CHANNEL SLOPE =  0.0300
 CHANNEL BASE(FEET) =   10.00   "Z" FACTOR =  50.000
 MANNING'S FACTOR = 0.030   MAXIMUM DEPTH(FEET) =   2.00
 CHANNEL FLOW THRU SUBAREA(CFS) =       0.36
 FLOW VELOCITY(FEET/SEC.) =   0.86   FLOW DEPTH(FEET) =   0.04
 TRAVEL TIME(MIN.) = 193.29   Tc(MIN.) = 197.62
 LONGEST FLOWPATH FROM NODE    9990.00 TO NODE    9992.00 = 10000.00 FEET.

****************************************************************************
 FLOW PROCESS FROM NODE    9992.00 TO NODE    9993.00 IS CODE =  81
----------------------------------------------------------------------------
 >>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
============================================================================
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  0.467
 STREETS & ROADS (DITCHES) RUNOFF COEFFICIENT = .7100
 SOIL CLASSIFICATION IS "D"
 S.C.S. CURVE NUMBER (AMC II) =  93
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7100
 SUBAREA AREA(ACRES) =  774.70   SUBAREA RUNOFF(CFS) =  256.98
 TOTAL AREA(ACRES) =    774.80   TOTAL RUNOFF(CFS) =  257.02
 TC(MIN.) = 197.62
============================================================================
 END OF STUDY SUMMARY:
 TOTAL AREA(ACRES)      =    774.80  TC(MIN.) =    197.62
 PEAK FLOW RATE(CFS)    =    257.02
============================================================================
============================================================================
 END OF RATIONAL METHOD ANALYSIS
```

Appendix B

- HEC-1 Model

OTAY CPU HEC-1 12-21-04

```
*****************************************
*****************************************
*                                       *
*                                       *
*   FLOOD HYDROGRAPH PACKAGE  (HEC-1)   *
*         JUN  1998                     *
*       VERSION 4.1                     *
*                                       *
*  RUN DATE  21DEC04  TIME  07:23:00    *
*                                       *
*                                       *
*****************************************
*****************************************
```

U.S. ARMY CORPS OF ENGINEERS
HYDROLOGIC ENGINEERING CENTER
609 SECOND STREET
DAVIS, CALIFORNIA 95616
(916) 756-1104

```
X     X  XXXXXXX   XXXXX          X
X     X  X       X     X        XX
X     X  X       X              X
XXXXXXX  XXXX    X        XXXXX X
X     X  X       X              X
X     X  X       X     X        X
X     X  XXXXXXX   XXXXX        XXX
```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT PAGE 1

```
LINE          ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

              *DIAGRAM
   1          ID  .....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
   2          ID
   3          ID       ****************************************************************
   4          ID       OTAY MESA HYDROLOGY
   5          ID       ****************************************************************
   6          ID
   7          ID       KIMLEY-HORN AND ASSOCIATES, INC.
   8          ID       100 YEAR, 6 HOUR STORM EVENT
   9          ID       FILE: IN"9300WDB-SD-IN2.TXT OUT 9300WDB-015
  10          ID       LSM 8-31-98, MODIFIED 7-27-99 BY SLM
  11          ID
  12          IT       2                    300
  13          IO       0

  14          KK       A1  RUNOFF HYDROGRAPH
  15          BA    0.075
  16          PB     2.95
  17          PI  0.0024  0.0024  0.0024  0.0024  0.0024  0.0024  0.0024  0.0024  0.0024  0.0024
  18          PI  0.0024  0.0024  0.0024  0.0024  0.0024  0.0031  0.0031  0.0031  0.0031  0.0031
  19          PI  0.0031  0.0031  0.0031  0.0031  0.0031  0.0031  0.0031  0.0031  0.0031  0.0031
  20          PI  0.0037  0.0037  0.0037  0.0037  0.0037  0.0037  0.0037  0.0037  0.0037  0.0037
  21          PI  0.0037  0.0037  0.0037  0.0037  0.0037  0.0047  0.0047  0.0047  0.0053  0.0053
  22          PI  0.0053  0.0057  0.0057  0.0057  0.0067  0.0067  0.0067  0.0083  0.0083  0.0083
  23          PI  0.0150  0.0180  0.0270  0.0380  0.0440  0.0420  0.0360  0.0280  0.0220  0.0220
  24          PI  0.0200  0.0180  0.0160  0.0140  0.0110  0.0083  0.0083  0.0083  0.0077  0.0077
  25          PI  0.0077  0.0073  0.0073  0.0073  0.0067  0.0067  0.0067  0.0053  0.0053  0.0053
  26          PI  0.0048  0.0048  0.0048  0.0048  0.0048  0.0048  0.0048  0.0048  0.0048  0.0048
  27          PI  0.0048  0.0048  0.0048  0.0048  0.0048  0.0038  0.0038  0.0038  0.0038  0.0038
  28          PI  0.0038  0.0038  0.0038  0.0038  0.0038  0.0038  0.0038  0.0038  0.0038  0.0038
  29          PI  0.0032  0.0032  0.0032  0.0032  0.0032  0.0032  0.0032  0.0032  0.0032  0.0032
  30          PI  0.0032  0.0032  0.0032  0.0032  0.0032  0.0028  0.0028  0.0028  0.0028  0.0028
  31          PI  0.0028  0.0028  0.0028  0.0028  0.0028  0.0028  0.0028  0.0028  0.0028  0.0028
  32          PI  0.0025  0.0025  0.0025  0.0025  0.0025  0.0025  0.0025  0.0025  0.0025  0.0025
  33          PI  0.0025  0.0025  0.0025  0.0025  0.0025  0.0025  0.0025  0.0025  0.0025  0.0025
  34          PI  0.0024  0.0024  0.0024  0.0024  0.0024  0.0024  0.0024  0.0024  0.0024  0.0024
  35          LS            83.9
  36          UD    0.140

  37          KK       A7  RUNOFF HYDROGRAPH
  38          BA    0.033
  39          PB     2.90
  40          LS            88.8
  41          UD    0.062

  42          KK       01  RUNOFF HYDROPGRAPH
  43          BA    0.228
  44          PB     2.90
  45          LS            83.5
  46          UD    0.262
```

HEC-1 INPUT PAGE 2

```
LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

  47      KK   CP-01  COMBINE HYDROPGRAPHS FROM A1, A7, AND 01
  48      HC      3

  49      KK  CP-A15  ROUTE FROM CP 01
  50      RK    1800   0.009    0.20            TRAP     100      20

  51      KK      A5  RUNOFF HYDROGRAPH
  52      BA   0.062
  53      PB    3.00
  54      LS            83.9
  55      UD   0.062

  56      KK  CP-A10  ROUTE FROM A5
  57      RK    1320   0.003   0.013            TRAP      35       0

  58      KK     A10  RUNOFF HYDROGRAPH
  59      BA   0.082
  60      PB    2.90
  61      LS            88.8
  62      UD   0.042

  63      KK  CP-A10  COMBINE HYDROGRAPHS FROM A5 AND A10
  64      HC      2

  65      KK  CP-A15  ROUTE FROM CP A10
  66      RK    1320   0.011   0.017            TRAP      50      20

  67      KK     A15  RUNOFF HYDROGRAPH
  68      BA   0.098
  69      PB    2.80
  70      LS            89.9
  71      UD   0.087

  72      KK  CP-A15  COMBINE HYDROGRAPHS FROM CP-01, CP-A10, AND A15
  73      HC      3

  74      KK  CP-A20  ROUTE FROM CP-A15
  75      RK    3400   0.006   0.020            TRAP     200      20

  76      KK      05  RUNOFF HYDROGRAPH FROM 05
  77      BA   0.097
  78      PB    2.75
  79      LS            83.9
  80      UD   0.080

  81      KK  CP-A20  ROUTE FROM 05
  82      RK    3500  0.006    0.020            TRAP     200      20

  83      KK     A20  RUNOFF HYDROGRAPH
  84      BA   0.254
  85      PB    2.75
  86      LS            88.4
  87      UD   0.184
```



```
LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

  88      KK     A25  RUNOFF FROM A25
  89      BA   0.030
  90      PB    2.60
  91      LS            88.4
  92      UD   0.076

  93      KK     A27  RUNOFF HYDROGRAPH
  94      BA   0.021
  95      PB    2.60
  96      LS            93.8
  97      UD   0.041

  98      KK  CP-A20  COMBINE HYDROGRAPHS FROM CP-A15, 05, A25, A27, AND A20
  99      HC      5

 100      KK  CP-A25 ROUTE FROM CP-A20
 101      RK    1200   0.005    0.02            TRAP      20       2

 102      KK     A23  RUNOFF HYDROGRAPH FROM A23
 103      BA   0.051
 104      PB    2.60
 105      LS            93.8
 106      UD   0.058

 107      KK  CP-A25  ROUTE FROM A23
 108      RK     525   0.005   0.013            CIRC     3.5

 109      KK  CP-A25 COMBINE HYDROGRAPHS FROM A23, CP-A20
 110      HC      2

 111      KK  CP-A30 ROUTE FROM CP-A25
 112      RK    1100   0.005   0.020            TRAP      20

 113      KK     O25  RUNOFF HYDROGRAPH
 114      BA   0.134
 115      PB    2.60
 116      LS            83.9
 117      UD   0.228

 118      KK     O20  RUNOFF HYDROGRAPH
```

```
119          BA   0.263
120          PB    2.70
121          LS              83.9
122          UD   0.294

123          KK  CP-030  ROUTE FROM 020
124          RK     900   0.001   0.020            TRAP     200      20

125          KK     030  RUNOFF HYDROGRAPH
126          BA   0.129
127          PB    2.50
128          LS              83.9
129          UD   0.258
```



```
LINE         ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

130          KK  CP-030  COMBINE HYDROGRAPHS FROM 025, 020 AND 030
131          HC       3

132          KK  CP-045 ROUTE FROM 030
133          RK     600   0.007   0.030            TRAP      70       0

134          KK     045  RUNOFF HYDROGRAPH
135          BA   0.079
136          PB    2.50
137          LS              93.8
138          UD   0.137

139          KK  CP-045  COMBINE HYDROGRAPHS FROM 045, CP-030
140          HC       2

141          KK  CP-050 ROUTE FROM CP-045
142          RK    2100   0.007   0.015            TRAP      70       0

143          KK     057  RUNOFF HYDROGRAPH
144          BA   0.527
145          PB    2.45
146          LS              93.8
147          UD   0.171

148          KK  CP-050
149          RK    5900   0.007   0.015            TRAP      70       0

150          KK     050  RUNOFF HYDROGRAPH
151          BA   0.463
152          PB    2.45
153          LS              93.8
154          UD   0.185

155          KK  CP-050  COMBINE HYDROGRAPHS FROM  CP-045, 057, 050
156          HC       3

157          KK  CP-010  ROUTE FROM CP-050
158          RK    1000   0.007   0.015

159          KK     010  RUNOFF HYDROGRAPH
160          BA   0.081
161          PB    2.75
162          LS              83.9
163          UD   0.087

164          KK  CP-010  COMBINE HYDROGRAPHS FROM 010,CP-050
165          HC              83.9

166          KK  CP-036  ROUTE FROM CP-010
167          RK    2100   0.007   0.015            TRAP      70       0
```



```
LINE         ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

168          KK     036  RUNOFF HYDROGRAPH
169          BA   0.116
170          PB    2.60
171          LS              93.8
172          UD   0.088

173          KK     060
174          BA   0.146
175          PB    2.40
176          LS              84.2
177          UD   0.086

178          KK  CP-036 ROUTE FROM CP-060
179          RK     500   0.007   0.015            TRAP      30       0

180          KK  CP-036  COMBINE HYDROGRAPHS FROM 060, 036, CP-010
181          HC       3

182          KK  CP-A30  ROUTE FROM CP-036
183          RK    1700   0.002   0.002   0.040    TRAP      30       0

184          KK     A30  RUNOFF HYDROGRAPH
185          BA   0.070
186          PB    2.50
187          LS              90.5
188          UD   0.083

189          KK  CP-A30  COMBINE HYDROGRAPHS FROM A30, CP-036, CP-A25
```

```
190          HC       3

191          KK  CP-A31  ROUTE FROM CP-A30
192          RK    1000   0.002   0.040            TRAP      30       0

193          KK     A28  RUNOFF HYDROGRAPH
194          BA   0.021
195          PB    2.60
196          LS            93.8
197          UD   0.041

198          KK  CP-A31  RUNOFF HYDROGRAPH
199          RK    1200   0.005    0.02            TRAP      10       2

200          KK     A31  RUNOFF HYDROGRAPH
201          BA   0.047
202          PB    2.60
203          LS            93.8
204          UD   0.063

205          KK  CP-A31  COMBINE HYDROGRAPHS FROM CP-A30, A28, A31
206          HC       3
1                                        HEC-1 INPUT                                                    PAGE  6

LINE         ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

207          KK  CP-S1A  ROUTE FROM CP-A31
208          RK    2600   0.002   0.040            TRAP      30       2

209          KK     B10
210          KM            BASIN 10
211          BA   .0067
212          PB     2.0
213          LS       0      91      61
214          UD    .004

215          KK     B20
216          KM            BASIN 20
217          BA   .0055
218          LS       0      89      52
219          UD    .007

220          KK     C12        COMBINE B10 & B20
221          HC       2

222          KK      C2        ROUTE CHANNEL NUMBER 2
223          UK     150    .020     .08      100
224          RK     620    .005    .035            TRAP      30       4

225          KK     B30
226          KM            BASIN 30
227          BA   .0052
228          LS       0      89      43
229          UD    .005

230          KK     C23        COMBINE B20 OUT & B30
231          HC       2

232          KK      C3        ROUTE CHANNEL NUMBER 3
233          RK    1100    .005    .035            TRAP      30       4

234          KK     B40
235          KP       1
236          KM            BASIN 40
237          BA   .0942
238          LS       0      91      60
239          UD    .024

240          KK    SD43        ROUTE B40 THROUGH B30: STORM DRAIN
241          UK    1050    .020     .08      100
242          RK     800    .015    .015            CIRC     5.5

243          KK     B50
244          KP       1
245          KM            BASIN 50
246          BA   .0781
247          LS       0      90      60
248          UD    .019
1                                        HEC-1 INPUT                                                    PAGE  7

LINE         ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

249          KK     C45         COMBINE B40 & B50 @ B30
250          HC       2

251          KK     CP4
252          BA    .032
253          UK     250    .012     .08      100
254          RK    1320    .015    .015            CIRC       6            YES

255          KK    CCP4
256          KM         COMBINE AT  CONC. PT. 4
257          HC       2

258          KK     CP3
259          KM          ROUTE TO CONC. PT. 3
260          BA    .040
261          UK     650    .011     .08      100
262          RK    1320    .015    .015            CIRC       6            YES
```

```
263          KK    CCP3
264          KM        COMBINE AT CONC. PT. 3
265          HC       2

266          KK     MX1
267          KM        MEXICO BASIN 1
268          BA   .0316
269          LS        0       90       60
270          UD    .007

271          KK     MX2
272          KM        MEXICO BASIN 2
273          BA   .0781
274          LS        0       89       50
275          UD    .019

276          KK    MX12
277          KM        COMBINE MEXICO AND BORDER AREA
278          HC       2

279          KK   MX123
280          KM        ROUTE TO CP3A
281          RK     600    .015    .015            CIRC       5

282          KK     MX3
283          KM        BORDER CORRIDOR
284          BA   .0215
285          LS        0       88       30
286          UD    .005

287          KK    CP3A
288          KM        COMBINE AT CONC. PT. 3A
289          HC       2
1                                        HEC-1 INPUT                                                    PAGE  8

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9.......10

290          KK    RCP3
291          KM        ROUTE TO CONC. PT. 3A
292          RK     750    .015    .015            CIRC       5

293          KK    CCP3
294          KM        COMBINE AT CONC. PT. 3
295          HC       2

296          KK    RCP2
297          KM        ROUTE TO CONC. PT. 2
298          RK     400    .015    .015            CIRC       7

299          KK     RP2
300          KM        RUNOFF TO CONC. PT. 2
301          BA   .0473
302          UK     550    .012     .08     100
303          RK    1200    .015    .015            CIRC       4

304          KK    CCP2
305          KM        COMBINEAT CONC. PT. 2
306          HC       2

307          KK    SVRW
308          KM        SIEMPRE VIVA RD WATESHED
309          BA   .0646
310          UK     450    .015     .08     100
311          RK    3000    .015    .015            CIRC       5

312          KK      EB
313          KM        WATESHED EAST OF PREVIOUS DET. BASIN
314          BA   .0102
315          UK     250    .010     .08     100
316          RK     100    .015    .015            CIRC       2

317          KK      WB
318          KM        WATERSHED WEST OF PREVIOUS DET. BASIN
319          BA   .0158
320          UK     400    .010     .08     100
321          RK     100    .015    .015            CIRC       2

322          KK    WSVR
323          KM        WEST SIEMPRE VIVA RD.
324          BA   .0108
325          UK     350    .012     .08     100
326          RK     600    .015    .015            CIRC       4

327          KK     CP1
328          HC       5
1                                        HEC-1 INPUT                                                    PAGE  9

LINE         ID.......1.......2.......3.......4.......5.......6.......7.......8.......9.......10

329          KK      S1  RUNOFF HYDROGRAPH
330          BA   0.516
331          PB    2.70
332          LS            93.8
333          UD   0.143

334          KK   CP-S1  COMBINE HYDROGRAPHS FROM B10, CP1 AND S1
335          HC       3
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336          KK  CP-S1A  COMBINE HYDROGRAPHS FROM CP-S1, CP-A31
337          HC       2
338          KK  CP-S10  ROUTE FROM CP-S1A
339          RK    1300   0.004   0.004            TRAP      30       0
340          KK     A60  RUNOFF HYDROGRAPH
341          BA   0.033
342          PB    2.30
343          LS            93.8
344          UD   0.039
345          KK  CP-A50  ROUTE FROM A60
346          RK    3000   0.005   0.013            CIRC       2
347          KK     055  RUNOFF HYDROGRAPH
348          BA   0.482
349          PB    2.35
350          LS            91.7
351          UD   0.140
352          KK  CP-A50  ROUTE FROM 055
353          RK    2900   0.004   0.013            TRAP      15       0
354          KK     A50  RUNOFF HYDROGRAPH
355          BA   0.250
356          PB    2.35
357          LS            93.8
358          UD   0.121
359          KK  CP-A50  COMBINE HYDROGRAPHS FROM A60, 055, AND A50
360          HC       3
361          KK     A50
362          DT     A50
363          DI       0     615    1000
364          DQ       0    0.01     385
365          KK     A42  RUNOFF HYDROGRAPH
366          BA   0.032
367          PB    2.40
368          LS            93.8
369          UD   0.046
1                                        HEC-1 INPUT                                                    PAGE 10
LINE         ID.......1.....2.....3.....4.....5.....6.....7.....8.....9.....10
370          KK  CP-A50  COMBINE HYDROGRAPHS FROM A50 AND A42
371          HC       2
372          KK  CP-A45  ROUTE FROM CP-A50
373          RK    3000   0.002   0.040            TRAP      40       1
374          KK     A40  RUNOFF HYDROGRAPH
375          BA   0.032
376          PB    2.40
377          LS            93.8
378          UD   0.057
379          KK  CP-A45  ROUTE FROM A40
380          RK    2380   0.006   0.040            TRAP      40       1
381          KK     A35  RUNOFF HYDROGRAPH
382          BA   0.065
383          PB    2.50
384          LS            93.8
385          UD   0.076
386          KK  CP-A45  ROUTE FROM A35
387          RK    2000   0.001   0.040            TRAP       5       1
388          KK     A45  RUNOFF HYDROGRAPH
389          BA   0.122
390          PB    2.45
391          LS            94.0
392          UD   0.112
393          KK  CP-A45  COMBINE HYDROGRAPHS FROM CP-A50, A40 AND A45
394          HC       4
395          KK     A45
396          DT     A45
397          DI       0      60    1000
398          DQ       0    0.01     940
399          KK  CP-S10  ROUTE FROM CP-A45
400          RK    2900   0.003   0.040            TRAP      25     0.8
401          KK     S10  RUNOFF FROM HYDROGRAPH
402          BA   0.263
403          PB    2.50
404          LS            94.4
405          UD   0.235
406          KK  CP-S10  COMBINE HYDROGRAPHS FROM S1-DET, CP-A45, AND S10
407          HC       3
1                                        HEC-1 INPUT                                                    PAGE 11
LINE         ID.......1.....2.....3.....4.....5.....6.....7.....8.....9.....10
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408          KK  CP-B30  ROUTE FROM CP-S10
409          RD    2400   0.004   0.040            TRAP      50      0.8

410          KK     A65  RUNOFF HYDROGRAPH FROM A65
411          BA   0.055
412          PB    2.30
413          LS              93.8
414          UD   0.037

415          KK  CP-S25 ROUTE FROM A65
416          RK    2910   0.010   0.040            TRAP     200      20

417          KK     S25  RUNOFF HYDROGRAPH
418          BA   0.082
419          PB    2.30
420          LS              83.9
421          UD   0.202

422          KK  CP-S25  COMBINE HYDROGRAPHS FROM A65 AND S25
423          HC       2

424          KK  CP-S20  ROUTE FROM CP-S25
425          RK    1460   0.004   0.020            TRAP      15      1

426          KK     S20  RUNOFF HYDROGRAPH
427          BA   0.136
428          PB    2.30
429          LS              83.9
430          UD   0.176

431          KK  CP-S20  COMBINE HYDROGRAPHS FROM CP-S25, AND S20
432          HC       2

433          KK  CP-B30  ROUTE FROM CP-S20
434          RK    3500   0.004   0.040            TRAP      15      1

435          KK     S15  RUNOFF HYDROGRAPH
436          BA   0.128
437          PB    2.40
438          LS              93.8
439          UD   0.083

440          KK  CP-B30  ROUTE FROM S15
441          RK    2800   0.004   0.040            TRAP      15      1

442          KK     B20  RUNOFF HYDROGRAPH
443          BA   0.040
444          PB    2.30
445          LS              93.8
446          UD   0.051

1                                        HEC-1 INPUT                                                    PAGE 12

LINE         ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

447          KK  CP-B25  ROUTE FROM B20
448          RK    1320   0.002   0.020            TRAP       8      .3

449          KK     B25  RUNOFF HYDROGRAPH
450          BA   0.127
451          PB    2.30
452          LS              93.8
453          UD   0.070

454          KK  CP-B25  COMBINE HYDROGRAPHS FROM B20 AND B25
455          HC       2

456          KK  CP-B25  ROUTE FROM CP-B25
457          RK    2700   0.001   0.040            TRAP      15      1

458          KK     B15  RUNOFF HYDROGRAPH
459          BA   0.074
460          PB    2.50
461          LS              94.5
462          UD   0.078

463          KK  CP-B30
464          RK    1000   0.015   0.040            TRAP      15      1

465          KK     B30  RUNOFF HYDROGRAPH
466          BA   0.228
467          PB    2.45
468          LS              84.8
469          UD   0.465

470          KK  CP-B30  COMBINE HYDROGRAPHS FROM CP-S10, CP-S20, S15, CP-B25, B15 AND B30
471          KO       1
472          HC       6

473          KK  DB-030  DETENTION BASIN AT BORDER
474          RS       1    STOR
475          SV       0      11      71     166     268     319
476          SE       0       2       4       6       8       9
477          SQ       0      20     150     350    1000    2200
478          ZZ

1
          SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT
 LINE     (V) ROUTING          |--->| DIVERSION OR PUMP FLOW
```
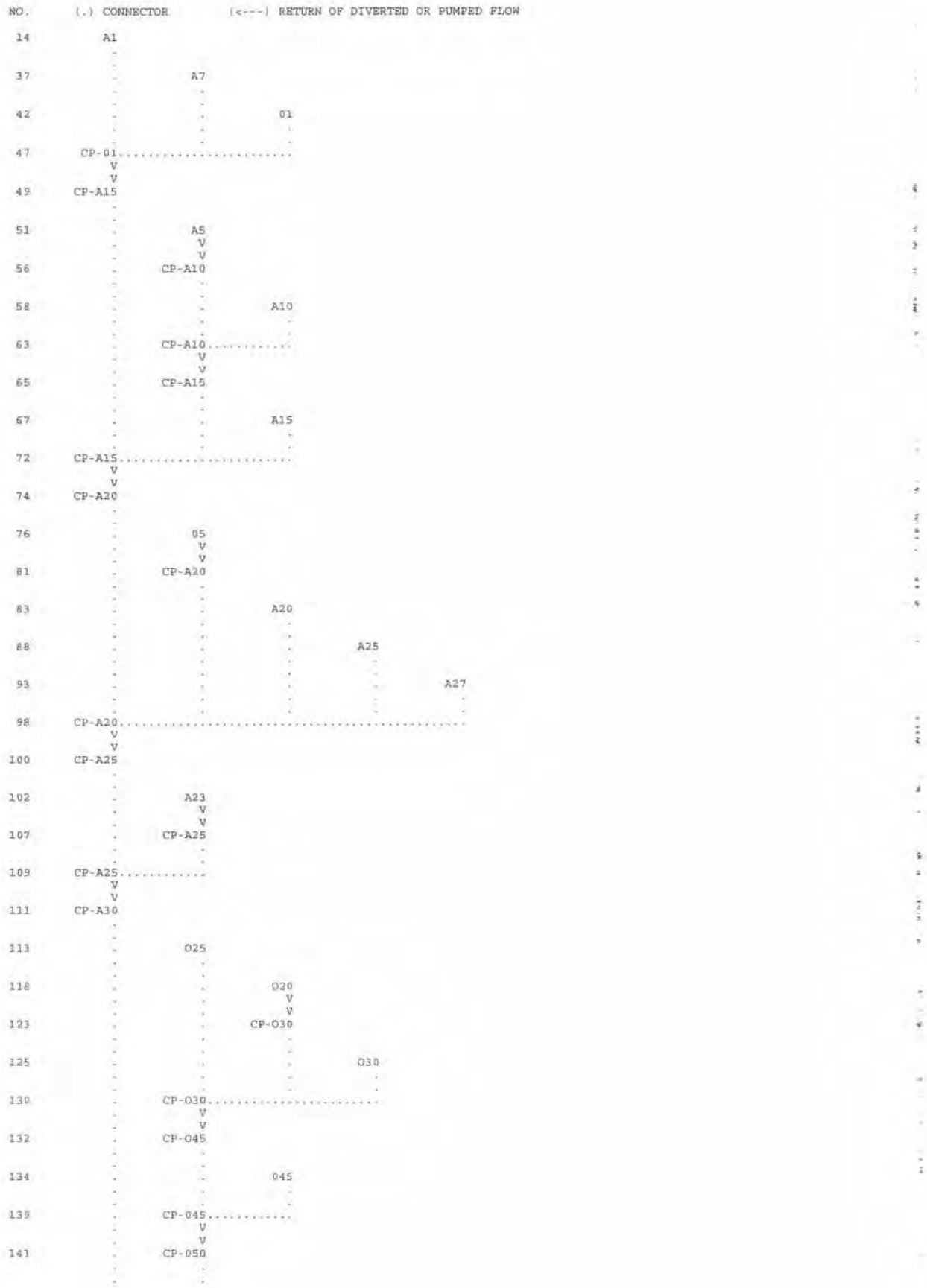
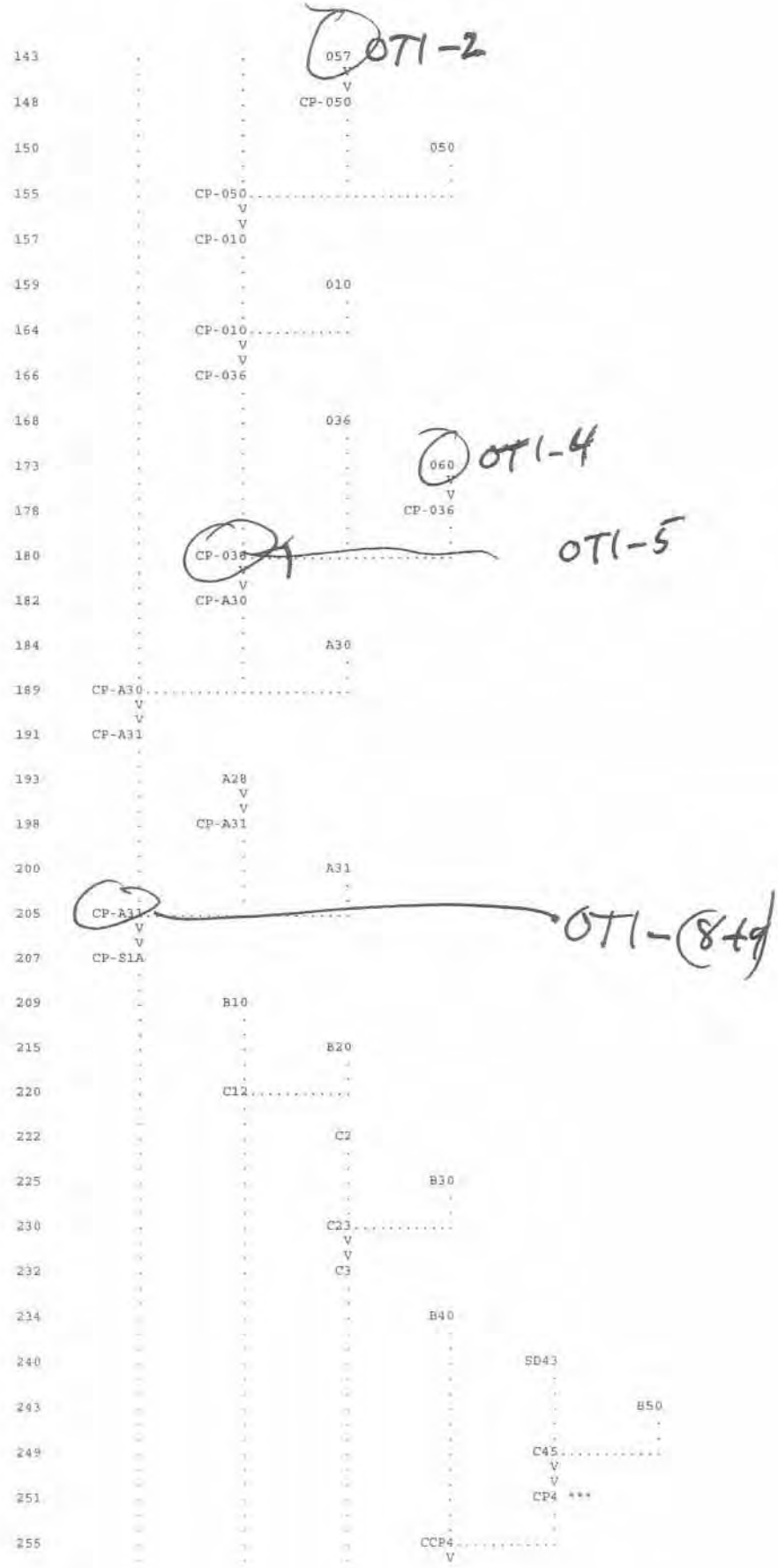


NO.
(.) CONNECTOR
(<---) RETURN OF DIVERTED OR PUMPED FLOW
14
A1
37
A7
42
01
47
CP-01
49
CP-A15
51
A5
56
CP-A10
58
A10
63
CP-A10
65
CP-A15
67
A15
72
CP-A15
74
CP-A20
76
05
81
CP-A20
83
A20
88
A25
93
A27
98
CP-A20
100
CP-A25
102
A23
107
CP-A25
109
CP-A25
111
CP-A30
113
025
118
020
123
CP-030
125
030
130
CP-030
132
CP-045
134
045
139
CP-045
141
CP-050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148
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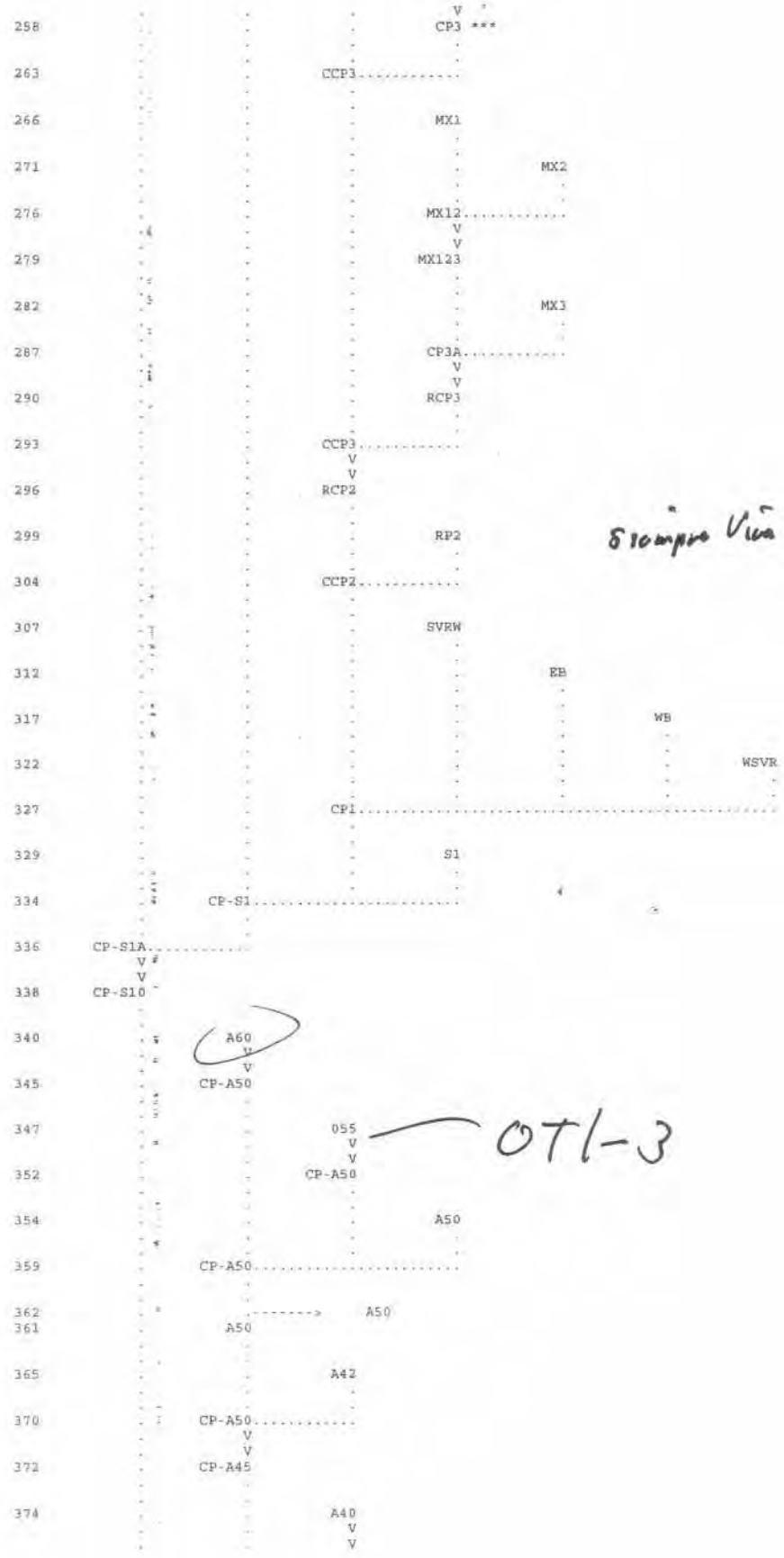
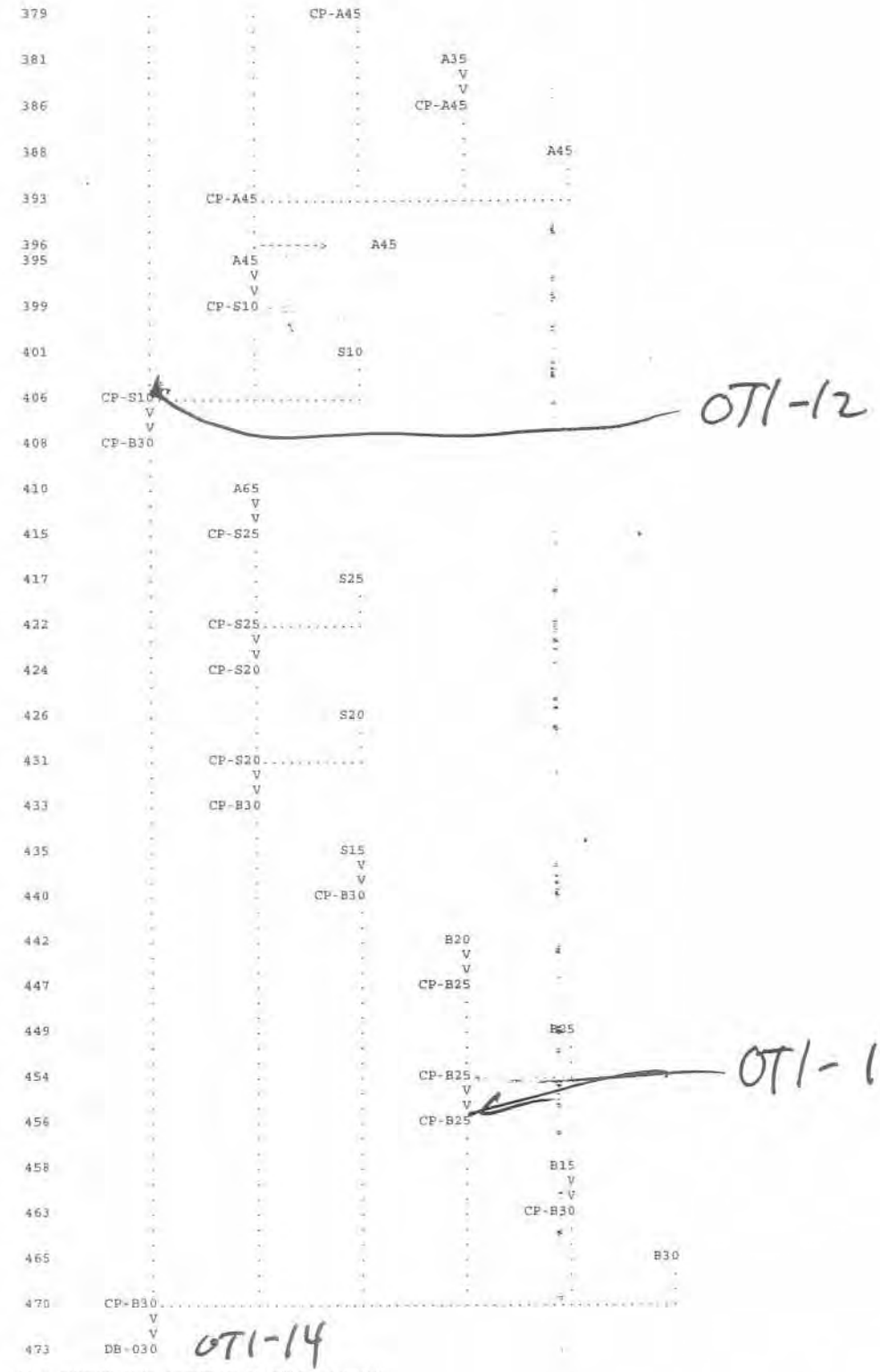
225
230
232
234
240
243
249
251
255
057
CP-050
050
CP-050
CP-010
010
CP-010
CP-036
036
060
CP-036
CP-038
CP-A30
A30
CP-A30
CP-A31
A28
CP-A31
A31
CP-A31
CP-S1A
B10
B20
C12
C2
B30
C23
C3
B40
SD43
B50
C45
CP4 ***
CCP4
OT1-2
OT1-4
OT1-5
OT1-(8+9)



Siempre Vía BP

OTI-3



(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

***

```
*                                   *                                   *       DAVIS, CALIFORNIA
95616       *
*  RUN DATE   21DEC04  TIME  07:23:00   *                               *           (916) 756-1104
*
*                                   *                                   *
*
 ****************************************
****************************************


                        ....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
                             ****************************************************************
                             OTAY MESA HYDROLOGY
                             ****************************************************************

                             KIMLEY-HORN AND ASSOCIATES, INC.
                             100 YEAR, 6 HOUR STORM EVENT
                             FILE: IN"9300WDB-SD-IN2.TXT OUT 9300WDB-015
                             LSM 8-31-98, MODIFIED 7-27-99 BY SLM

  13 IO          OUTPUT CONTROL VARIABLES
                      IPRNT           0  PRINT CONTROL
                      IPLOT           0  PLOT CONTROL
                      QSCAL          0.  HYDROGRAPH PLOT SCALE

     IT          HYDROGRAPH TIME DATA
                      NMIN           2  MINUTES IN COMPUTATION INTERVAL
                     IDATE       1    0  STARTING DATE
                     ITIME        0000  STARTING TIME
                        NQ         300  NUMBER OF HYDROGRAPH ORDINATES
                    NDDATE       1    0  ENDING DATE
                    NDTIME        0958  ENDING TIME
                     ICENT          19  CENTURY MARK

                COMPUTATION INTERVAL      .03 HOURS
                   TOTAL TIME BASE     9.97 HOURS

          ENGLISH UNITS
               DRAINAGE AREA          SQUARE MILES
               PRECIPITATION DEPTH    INCHES
               LENGTH, ELEVATION      FEET
               FLOW                   CUBIC FEET PER SECOND
               STORAGE VOLUME         ACRE-FEET
               SURFACE AREA           ACRES
               TEMPERATURE            DEGREES FAHRENHEIT

*** *** *** *
```

215.7	7.0											
1	0010	6	0.	.0	.0 * 1	0330 106	732.	225.9	7.2 * 1	0650 206	659.	
214.5	7.0											
1	0012	7	0.	.0	.0 * 1	0332 107	742.	227.5	7.2 * 1	0652 207	652.	
213.3	6.9											
1	0014	8	0.	.0	.0 * 1	0334 108	752.	229.1	7.2 * 1	0654 208	644.	
212.1	6.9											
1	0016	9	0.	.0	.0 * 1	0336 109	761.	230.5	7.3 * 1	0656 209	636.	
210.9	6.9											
1	0018	10	0.	.1	.0 * 1	0338 110	770.	231.9	7.3 * 1	0658 210	628.	
209.7	6.9											
1	0020	11	0.	.1	.0 * 1	0340 111	778.	233.2	7.3 * 1	0700 211	620.	
208.4	6.8											
1	0022	12	0.	.1	.0 * 1	0342 112	786.	234.4	7.3 * 1	0702 212	612.	
207.2	6.8											
1	0024	13	0.	.2	.0 * 1	0344 113	793.	235.5	7.4 * 1	0704 213	604.	
205.9	6.8											
1	0026	14	0.	.2	.0 * 1	0346 114	799.	236.5	7.4 * 1	0706 214	596.	
204.7	6.8											
1	0028	15	0.	.3	.0 * 1	0348 115	805.	237.5	7.4 * 1	0708 215	588.	
203.4	6.7											
1	0030	16	1.	.3	.1 * 1	0350 116	811.	238.4	7.4 * 1	0710 216	580.	
202.1	6.7											
1	0032	17	1.	.4	.1 * 1	0352 117	816.	239.2	7.4 * 1	0712 217	572.	
200.9	6.7											
1	0034	18	1.	.4	.1 * 1	0354 118	821.	239.9	7.4 * 1	0714 218	564.	
199.6	6.7											
1	0036	19	1.	.4	.1 * 1	0356 119	826.	240.6	7.5 * 1	0716 219	557.	
198.4	6.6											
1	0038	20	1.	.5	.1 * 1	0358 120	830.	241.3	7.5 * 1	0718 220	549.	
197.2	6.6											
1	0040	21	1.	.5	.1 * 1	0400 121	834.	241.9	7.5 * 1	0720 221	541.	
195.9	6.6											
1	0042	22	1.	.6	.1 * 1	0402 122	837.	242.4	7.5 * 1	0722 222	533.	
194.7	6.6											
1	0044	23	1.	.6	.1 * 1	0404 123	840.	242.9	7.5 * 1	0724 223	525.	
193.5	6.5											
1	0046	24	1.	.7	.1 * 1	0406 124	843.	243.4	7.5 * 1	0726 224	518.	
192.3	6.5											
1	0048	25	1.	.8	.1 * 1	0408 125	846.	243.8	7.5 * 1	0728 225	510.	
191.1	6.5											
1	0050	26	1.	.8	.1 * 1	0410 126	848.	244.2	7.5 * 1	0730 226	503.	
190.0	6.5											
1	0052	27	2.	.9	.2 * 1	0412 127	850.	244.5	7.5 * 1	0732 227	495.	
188.8	6.4											
1	0054	28	2.	.9	.2 * 1	0414 128	852.	244.8	7.5 * 1	0734 228	488.	
187.7	6.4											
1	0056	29	2.	1.0	.2 * 1	0416 129	854.	245.0	7.5 * 1	0736 229	481.	
186.5	6.4											
1	0058	30	2.	1.1	.2 * 1	0418 130	855.	245.2	7.6 * 1	0738 230	474.	
185.4	6.4											
1	0100	31	2.	1.2	.2 * 1	0420 131	856.	245.4	7.6 * 1	0740 231	466.	
184.3	6.4											
1	0102	32	2.	1.2	.2 * 1	0422 132	857.	245.5	7.6 * 1	0742 232	459.	
183.2	6.3											
1	0104	33	2.	1.3	.2 * 1	0424 133	858.	245.7	7.6 * 1	0744 233	452.	
182.1	6.3											
1	0106	34	3.	1.4	.3 * 1	0426 134	858.	245.7	7.6 * 1	0746 234	446.	
181.0	6.3											
1	0108	35	3.	1.5	.3 * 1	0428 135	859.	245.8	7.6 * 1	0748 235	439.	
179.9	6.3											
1	0110	36	3.	1.6	.3 * 1	0430 136	859.	245.8	7.6 * 1	0750 236	432.	
178.9	6.3											
1	0112	37	3.	1.8	.3 * 1	0432 137	859.	245.9	7.6 * 1	0752 237	425.	
177.8	6.2											
1	0114	38	3.	1.9	.3 * 1	0434 138	859.	245.8	7.6 * 1	0754 238	419.	
176.8	6.2											
1	0116	39	4.	2.0	.4 * 1	0436 139	859.	245.8	7.6 * 1	0756 239	412.	
175.8	6.2											
1	0118	40	4.	2.2	.4 * 1	0438 140	858.	245.8	7.6 * 1	0758 240	406.	
174.7	6.2											
1	0120	41	4.	2.4	.4 * 1	0440 141	858.	245.7	7.6 * 1	0800 241	399.	
173.7	6.2											
1	0122	42	5.	2.5	.5 * 1	0442 142	857.	245.6	7.6 * 1	0802 242	393.	
172.8	6.1											
1	0124	43	5.	2.7	.5 * 1	0444 143	857.	245.5	7.6 * 1	0804 243	387.	
171.8	6.1											
1	0126	44	5.	2.9	.5 * 1	0446 144	856.	245.4	7.6 * 1	0806 244	381.	
170.8	6.1											
1	0128	45	6.	3.1	.6 * 1	0448 145	855.	245.2	7.6 * 1	0808 245	375.	
169.9	6.1											
1	0130	46	6.	3.4	.6 * 1	0450 146	854.	245.1	7.6 * 1	0810 246	369.	
169.0	6.1											
1	0132	47	7.	3.6	.7 * 1	0452 147	853.	244.9	7.5 * 1	0812 247	363.	
168.0	6.0											
1	0134	48	7.	3.8	.7 * 1	0454 148	851.	244.7	7.5 * 1	0814 248	357.	
167.1	6.0											
1	0136	49	7.	4.1	.7 * 1	0456 149	850.	244.5	7.5 * 1	0816 249	351.	
166.2	6.0											
1	0138	50	8.	4.4	.8 * 1	0458 150	849.	244.2	7.5 * 1	0818 250	349.	
165.3	6.0											
1	0140	51	8.	4.6	.8 * 1	0500 151	847.	244.0	7.5 * 1	0820 251	347.	
164.5	6.0											
1	0142	52	9.	4.9	.9 * 1	0502 152	846.	243.8	7.5 * 1	0822 252	345.	
163.6	5.9											
1	0144	53	10.	5.2	1.0 * 1	0504 153	844.	243.5	7.5 * 1	0824 253	343.	
162.7	5.9											
1	0146	54	10.	5.6	1.0 * 1	0506 154	842.	243.2	7.5 * 1	0826 254	341.	
161.8	5.9											
1	0148	55	11.	6.0	1.1 * 1	0508 155	840.	243.0	7.5 * 1	0828 255	339.	
161.0	5.9											

1	0150	56	12.	6.4	1.2	* 1	0510	156	839.	242.7	7.5	* 1	0830	256	338.
160.1	5.9														
1	0152	57	12.	6.8	1.2	* 1	0512	157	837.	242.4	7.5	* 1	0832	257	336.
159.2	5.9														
1	0154	58	13.	7.3	1.3	* 1	0514	158	835.	242.1	7.5	* 1	0834	258	334.
158.3	5.8														
1	0156	59	14.	7.8	1.4	* 1	0516	159	833.	241.8	7.5	* 1	0836	259	332.
157.5	5.8														
1	0158	60	15.	8.4	1.5	* 1	0518	160	831.	241.4	7.5	* 1	0838	260	330.
156.6	5.8														
1	0200	61	17.	9.1	1.7	* 1	0520	161	829.	241.1	7.5	* 1	0840	261	328.
155.8	5.8														
1	0202	62	18.	9.9	1.8	* 1	0522	162	826.	240.8	7.5	* 1	0842	262	327.
154.9	5.8														
1	0204	63	19.	10.7	1.9	* 1	0524	163	824.	240.4	7.5	* 1	0844	263	325.
154.1	5.7														
1	0206	64	21.	11.7	2.0	* 1	0526	164	822.	240.1	7.5	* 1	0846	264	323.
153.2	5.7														
1	0208	65	24.	12.8	2.1	* 1	0528	165	820.	239.7	7.4	* 1	0848	265	321.
152.4	5.7														
1	0210	66	27.	14.2	2.1	* 1	0530	166	817.	239.3	7.4	* 1	0850	266	320.
151.5	5.7														
1	0212	67	31.	16.0	2.2	* 1	0532	167	815.	238.9	7.4	* 1	0852	267	318.
150.7	5.7														
1	0214	68	36.	18.5	2.2	* 1	0534	168	812.	238.6	7.4	* 1	0854	268	316.
149.9	5.7														
1	0216	69	43.	21.7	2.4	* 1	0536	169	810.	238.2	7.4	* 1	0856	269	314.
149.0	5.6														
1	0218	70	52.	25.8	2.5	* 1	0538	170	808.	237.8	7.4	* 1	0858	270	313.
148.2	5.6														
1	0220	71	63.	30.8	2.7	* 1	0540	171	805.	237.4	7.4	* 1	0900	271	311.
147.4	5.6														
1	0222	72	76.	36.8	2.9	* 1	0542	172	803.	237.0	7.4	* 1	0902	272	309.
146.6	5.6														
1	0224	73	91.	43.7	3.1	* 1	0544	173	800.	236.7	7.4	* 1	0904	273	307.
145.8	5.6														
1	0226	74	108.	51.5	3.3	* 1	0546	174	798.	236.3	7.4	* 1	0906	274	306.
145.0	5.6														
1	0228	75	126.	59.9	3.6	* 1	0548	175	795.	235.9	7.4	* 1	0908	275	304.
144.1	5.5														
1	0230	76	145.	68.7	3.9	* 1	0550	176	793.	235.5	7.4	* 1	0910	276	302.
143.3	5.5														
1	0232	77	165.	77.9	4.1	* 1	0552	177	790.	235.1	7.4	* 1	0912	277	301.
142.5	5.5														
1	0234	78	185.	87.4	4.3	* 1	0554	178	788.	234.7	7.3	* 1	0914	278	299.
141.7	5.5														
1	0236	79	205.	97.0	4.5	* 1	0556	179	786.	234.3	7.3	* 1	0916	279	297.
141.0	5.5														
1	0238	80	225.	106.4	4.7	* 1	0558	180	783.	234.0	7.3	* 1	0918	280	296.
140.2	5.5														
1	0240	81	244.	115.6	4.9	* 1	0600	181	781.	233.6	7.3	* 1	0920	281	294.
139.4	5.4														
1	0242	82	262.	124.3	5.1	* 1	0602	182	778.	233.2	7.3	* 1	0922	282	292.
138.6	5.4														
1	0244	83	280.	132.7	5.3	* 1	0604	183	776.	232.8	7.3	* 1	0924	283	291.
137.8	5.4														
1	0246	84	296.	140.5	5.5	* 1	0606	184	773.	232.4	7.3	* 1	0926	284	289.
137.0	5.4														
1	0248	85	312.	147.8	5.6	* 1	0608	185	771.	232.1	7.3	* 1	0928	285	287.
136.3	5.4														
1	0250	86	326.	154.5	5.8	* 1	0610	186	768.	231.6	7.3	* 1	0930	286	286.
135.5	5.4														
1	0252	87	339.	160.9	5.9	* 1	0612	187	765.	231.2	7.3	* 1	0932	287	284.
134.8	5.3														
1	0254	88	355.	166.7	6.0	* 1	0614	188	762.	230.7	7.3	* 1	0934	288	283.
134.0	5.3														
1	0256	89	389.	172.2	6.1	* 1	0616	189	759.	230.1	7.3	* 1	0936	289	281.
133.2	5.3														
1	0258	90	421.	177.2	6.2	* 1	0618	190	755.	229.6	7.2	* 1	0938	290	279.
132.5	5.3														
1	0300	91	451.	181.8	6.3	* 1	0620	191	751.	228.9	7.2	* 1	0940	291	278.
131.7	5.3														
1	0302	92	478.	186.1	6.4	* 1	0622	192	747.	228.2	7.2	* 1	0942	292	276.
131.0	5.3														
1	0304	93	504.	190.2	6.5	* 1	0624	193	742.	227.5	7.2	* 1	0944	293	275.
130.3	5.2														
1	0306	94	529.	194.1	6.6	* 1	0626	194	737.	226.7	7.2	* 1	0946	294	273.
129.5	5.2														
1	0308	95	552.	197.8	6.6	* 1	0628	195	732.	225.9	7.2	* 1	0948	295	272.
128.8	5.2														
1	0310	96	575.	201.3	6.7	* 1	0630	196	726.	225.0	7.2	* 1	0950	296	270.
128.1	5.2														
1	0312	97	596.	204.6	6.8	* 1	0632	197	720.	224.1	7.1	* 1	0952	297	269.
127.3	5.2														
1	0314	98	615.	207.7	6.8	* 1	0634	198	714.	223.1	7.1	* 1	0954	298	267.
126.6	5.2														
1	0316	99	634.	210.5	6.9	* 1	0636	199	708.	222.1	7.1	* 1	0956	299	266.
125.9	5.2														
1	0318	100	651.	213.2	6.9	* 1	0638	200	701.	221.1	7.1	* 1	0958	300	264.
125.2	5.1					*						*			

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PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	9.97-HR
(CFS)	(HR)					
		(CFS)				
859.	4.53		658.	441.	441.	441.
		(INCHES)	.954	1.061	1.061	1.061

	(AC-FT)	326.	363.	363.	363.	

PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	9.97-HR
(AC-FT)	(HR)				
246.	4.53	214.	150.	150.	150.

PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	9.97-HR
(FEET)	(HR)				
7.57	4.53	6.94	5.16	5.16	5.16

CUMULATIVE AREA = 6.41 SQ MI

RUNOFF SUMMARY
FLOW IN CUBIC FEET PER SECOND
TIME IN HOURS, AREA IN SQUARE MILES

			PEAK	TIME OF	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN	MAXIMUM	
TIME OF	OPERATION	STATION	FLOW	PEAK				AREA	STAGE	MAX
STAGE					6-HOUR	24-HOUR	72-HOUR			
	HYDROGRAPH AT	A1	64.	2.37	12.	7.	7.	.08		
	HYDROGRAPH AT	A7	44.	2.27	6.	4.	4.	.03		
	HYDROGRAPH AT	01	153.	2.53	35.	21.	21.	.23		
	3 COMBINED AT	CP-01	229.	2.47	53.	32.	32.	.34		
	ROUTED TO	CP-A15	227.	2.83	54.	33.	33.	.34		
	HYDROGRAPH AT	A5	66.	2.27	10.	6.	6.	.06		
	ROUTED TO	CP-A10	65.	2.30	10.	6.	6.	.06		
	HYDROGRAPH AT	A10	117.	2.23	16.	10.	10.	.08		
	2 COMBINED AT	CP-A10	170.	2.27	26.	16.	16.	.14		
	ROUTED TO	CP-A15	170.	2.30	26.	16.	16.	.14		
	HYDROGRAPH AT	A15	124.	2.30	19.	11.	11.	.10		
	3 COMBINED AT	CP-A15	307.	2.83	98.	60.	60.	.58		
	ROUTED TO	CP-A20	306.	3.00	99.	60.	60.	.58		
	HYDROGRAPH AT	05	82.	2.30	14.	8.	8.	.10		
	ROUTED TO	CP-A20	81.	2.57	14.	9.	9.	.10		
	HYDROGRAPH AT	A20	232.	2.40	44.	27.	27.	.25		
	HYDROGRAPH AT	A25	32.	2.27	5.	3.	3.	.03		
	HYDROGRAPH AT	A27	34.	2.23	4.	3.	3.	.02		
	5 COMBINED AT	CP-A20	569.	2.50	165.	101.	101.	.98		
	ROUTED TO	CP-A25	567.	2.53	165.	101.	101.	.98		
	HYDROGRAPH AT	A23	79.	2.23	11.	6.	6.	.05		
	ROUTED TO	CP-A25	78.	2.27	11.	6.	6.	.05		
	2 COMBINED AT	CP-A25	599.	2.53	176.	107.	107.	1.03		
	ROUTED TO	CP-A30	598.	2.53	176.	107.	107.	1.03		
	HYDROGRAPH AT	O25	77.	2.50	17.	10.	10.	.13		
	HYDROGRAPH AT									

+		O20	147.	2.57	36.	22.	22.	.26
+	ROUTED TO	CP-O30	146.	2.67	36.	22.	22.	.26
+	HYDROGRAPH AT	O30	65.	2.53	15.	9.	9.	.13
+	3 COMBINED AT	CP-O30	276.	2.60	68.	41.	41.	.53
+	ROUTED TO	CP-O45	275.	2.60	68.	41.	41.	.53
+	HYDROGRAPH AT	045	95.	2.33	16.	9.	9.	.08
+	2 COMBINED AT	CP-045	329.	2.57	84.	51.	51.	.61
+	ROUTED TO	CP-050	328.	2.60	84.	51.	51.	.61
+	HYDROGRAPH AT	057	575.	2.37	102.	62.	62.	.53
+	ROUTED TO	CP-050	570.	2.47	102.	62.	62.	.53
+	HYDROGRAPH AT	050	493.	2.40	90.	54.	54.	.46
+	3 COMBINED AT	CP-050	1201.	2.47	275.	166.	166.	1.60
+	ROUTED TO	CP-010	1299.	2.50	275.	166.	166.	1.60
+	HYDROGRAPH AT	010	68.	2.30	11.	7.	7.	.08
+	2 COMBINED AT	CP-010	1346.	2.50	286.	173.	173.	1.68
+	ROUTED TO	CP-036	1345.	2.50	287.	173.	173.	1.68
+	HYDROGRAPH AT	036	166.	2.27	24.	15.	15.	.12
+	HYDROGRAPH AT	060	95.	2.30	17.	10.	10.	.15
+	ROUTED TO	CP-036	94.	2.30	17.	10.	10.	.15
+	3 COMBINED AT	CP-036	1508.	2.50	327.	198.	198.	1.94
+	ROUTED TO	CP-A30	1507.	2.50	327.	198.	198.	1.94
+	HYDROGRAPH AT	A30	78.	2.27	12.	7.	7.	.07
+	3 COMBINED AT	CP-A30	2150.	2.50	514.	312.	312.	3.04
+	ROUTED TO	CP-A31	2145.	2.50	514.	312.	312.	3.04
+	HYDROGRAPH AT	A28	34.	2.23	4.	3.	3.	.02
+	ROUTED TO	CP-A31	33.	2.27	4.	3.	3.	.02
+	HYDROGRAPH AT	A31	71.	2.27	10.	6.	6.	.05
+	3 COMBINED AT	CP-A31	2196.	2.50	528.	321.	321.	3.11
+	ROUTED TO	CP-S1A	2184.	2.57	527.	320.	320.	3.11
+	HYDROGRAPH AT	B10	3.	2.20	1.	1.	1.	.01
+	HYDROGRAPH AT	B20	7.	2.20	1.	1.	1.	.01
+	2 COMBINED AT	C12	16.	2.20	2.	1.	1.	.01
+	HYDROGRAPH AT	C2	5.	2.33	1.	1.	1.	.01
+	HYDROGRAPH AT	B30	6.	2.20	1	0.	0.	.01

+	2 COMBINED AT	C23	9.	2.27	2.	1.	1.	.01
+	ROUTED TO	C3	9.	2.40	2.	1.	1.	.01
+	HYDROGRAPH AT	B40	127.	2.20	17.	10.	10.	.09
+	HYDROGRAPH AT	SD43	64.	2.47	16.	10.	10.	.09
+	HYDROGRAPH AT	B50	104.	2.20	14.	8.	8.	.08
+	2 COMBINED AT	C45	139.	2.20	29.	18.	18.	.17
+	HYDROGRAPH AT	CP4	163.	2.23	35.	22.	22.	.20
+	2 COMBINED AT	CCP4	283.	2.20	52.	32.	32.	.30
+	HYDROGRAPH AT	CP3	302.	2.23	58.	36.	36.	.34
+	2 COMBINED AT	CCP3	304.	2.23	60.	37.	37.	.35
+	HYDROGRAPH AT	MX1	42.	2.20	6.	3.	3.	.03
+	HYDROGRAPH AT	MX2	95.	2.20	13.	8.	8.	.08
+	2 COMBINED AT	MX12	137.	2.20	18.	11.	11.	.11
+	ROUTED TO	MX123	136.	2.20	18.	11.	11.	.11
+	HYDROGRAPH AT	MX3	22.	2.20	3.	2.	2.	.02
+	2 COMBINED AT	CP3A	158.	2.20	21.	13.	13.	.13
+	ROUTED TO	RCP3	155.	2.20	21.	13.	13.	.13
+	3 COMBINED AT	CCP3	455.	2.23	81.	50.	50.	.48
+	ROUTED TO	RCP2	454.	2.23	81.	50.	50.	.48
+	HYDROGRAPH AT	RP2	26.	2.50	6.	4.	4.	.05
+	2 COMBINED AT	CCP2	468.	2.23	87.	54.	54.	.53
+	HYDROGRAPH AT	SVRW	40.	2.47	9.	5.	5.	.06
+	HYDROGRAPH AT	EB	7.	2.37	1.	1.	1.	.01
+	HYDROGRAPH AT	WB	10.	2.47	2.	1.	1.	.02
+	HYDROGRAPH AT	WSVR	7.	2.40	1.	1.	1.	.01
+	5 COMBINED AT	CP1	503.	2.23	100.	62.	62.	.63
+	HYDROGRAPH AT	S1	679.	2.33	113.	68.	68.	.52
+	3 COMBINED AT	CP-S1	1116.	2.33	216.	132.	132.	1.16
+	2 COMBINED AT	CP-S1A	2955.	2.53	736.	452.	452.	4.26
+	ROUTED TO	CP-S10	2950.	2.53	736.	452.	452.	4.26
+	HYDROGRAPH AT	A60	45.	2.23	6.	4.	4.	.03
+	ROUTED TO	CP-A50	44.	2.30	6.	4.	4.	.03
+	HYDROGRAPH AT	055	463.	2.33	79.	48.	48.	.48
+	ROUTED TO	CP-A50	462.	2.37	79.	48.	48.	.48

@ La Media

+	HYDROGRAPH AT	A50	287.	2.33	46.	28.	28.	.25
+	3 COMBINED AT	CP-A50	771.	2.33	131.	79.	79.	.76
+	DIVERSION TO	A50	156.	2.33	4.	2.	2.	.76
+	HYDROGRAPH AT	A50	615.	2.33	127.	77.	77.	.76
+	HYDROGRAPH AT	A42	46.	2.23	6.	4.	4.	.03
+	2 COMBINED AT	CP-A50	658.	2.27	133.	80.	80.	.80
+	ROUTED TO	CP-A45	653.	2.40	133.	80.	80.	.80
+	HYDROGRAPH AT	A40	45.	2.23	6.	4.	4.	.03
+	ROUTED TO	CP-A45	44.	2.43	6.	4.	4.	.03
+	HYDROGRAPH AT	A35	92.	2.27	13.	8.	8.	.06
+	ROUTED TO	CP-A45	90.	2.43	13.	8.	8.	.06
+	HYDROGRAPH AT	A45	154.	2.30	24.	14.	14.	.12
+	4 COMBINED AT	CP-A45	915.	2.40	176.	106.	106.	1.02
+	DIVERSION TO	A45	855.	2.37	126.	76.	76.	1.02
+	HYDROGRAPH AT	A45	60.	2.37	50.	31.	31.	1.02
+	ROUTED TO	CP-S10	60.	2.60	50.	30.	30.	1.02
+	HYDROGRAPH AT	S10	273.	2.47	54.	32.	32.	.26
+	3 COMBINED AT	CP-S10	3270.	2.53	839.	515.	515.	5.54
+	ROUTED TO	CP-B30	3217.	2.60	838.	514.	514.	5.54
+	HYDROGRAPH AT	A65	76.	2.23	10.	6.	6.	.05
+	ROUTED TO	CP-S25	74.	2.53	10.	6.	6.	.05
+	HYDROGRAPH AT	S25	38.	2.47	8.	5.	5.	.08
+	2 COMBINED AT	CP-S25	111.	2.53	19.	11.	11.	.14
+	ROUTED TO	CP-S20	108.	2.57	19.	11.	11.	.14
+	HYDROGRAPH AT	S20	66.	2.43	14.	8.	8.	.14
+	2 COMBINED AT	CP-S20	166.	2.57	33.	20.	20.	.27
+	ROUTED TO	CP-B30	162.	2.73	32.	20.	20.	.27
+	HYDROGRAPH AT	S15	167.	2.27	24.	15.	15.	.13
+	ROUTED TO	CP-B30	163.	2.37	24.	15.	15.	.13
+	HYDROGRAPH AT	B30	54.	2.23	7.	4.	4.	.04
+	ROUTED TO	CP-B25	52.	2.30	7.	4.	4.	.04
+	HYDROGRAPH AT	B25	162.	2.27	23.	14.	14.	.13
+	2 COMBINED AT	CP-B25	212.	2.27	30.	18.	18.	.17
	ROUTED TO							

	CP-B25	209.	2.43	30.	18.	18.	.17
HYDROGRAPH AT	B15	108.	2.27	15.	9.	9.	.07
ROUTED TO	CP-B30	107.	2.30	15.	9.	9.	.07
HYDROGRAPH AT	B30	90.	2.80	28.	17.	17.	.23
6 COMBINED AT	CP-B30	3673.	2.60	967.	593.	593.	6.41
ROUTED TO	DB-030	859.	4.53	658.	441.	441.	6.41

4.53
1

7.57

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING

6.78 mi 2

APPENDIX G-2

Review of Otay Mesa Drainage Studies

TETRA TECH

Review of Otay Mesa Drainage Studies

Contract H084445

Task Order No. 16

Review of Otay Mesa Drainage Studies

Contract H084445

Task Order No. 16

Table of Contents

I. Introduction 4
II. Review of Completed and Draft Planning and Engineering Reports 5
A. Introduction 5
B. Review of Pertinent Notices and Planning Reports 5
C. Impetus of Drainage Studies 11
III. Data Compilation and Review 12
A. Data Compilation 12
B. Drainage Areas 12
C. Zoning Status 13
D. Land Uses 14
E. Soils 15
F. Vegetation 17
IV. Environmentally Sensitive Lands 18
A. Vernal Pool Background 18
B. Otay Mesa Vernal Pools 18
V. Review of Stormwater Regulations 20
A. Federal Regulations and Permits 20
B. State Regulations and Permits 23
C. Local Regulations and Permits 25
D. County Regulations and Permits 31
E. International Regulations and Permits 31
VI. Drainage Requirements, Considerations, and Opportunities 31
A. Consideration 1: Drainage and Runoff Management Responsibilities 32
B. Consideration 2: Potential for BMPs 33
C. Consideration 3: Estimated Annualized Costs for Planning, Permitting, Land Acquisition, Design, Construction, and Maintenance of Stormwater and Drainage Infrastructure 36
D. Consideration 4: Risk-Based Analyses 38
E. Consideration 5: Border Issues 39
VII. Conclusions 41
VIII. References 42

List of Tables

Table 1. Drainage Area Sizes 13
Table 2. Zoning Status for Drainage Areas 14
Table 3. Land uses for Drainage Areas 15
Table 4. Soils for Drainage Areas 16
Table 5. Vegetation Coverage for Drainage Areas 17
Table 6. Summary of biological survey requirements 29
Table 7: Per Unit Cost Estimates for Construction Components 37

List of Figures

Figure 1. Location of Otay Mesa 4
Figure 2. Defined Drainage Areas 13
Figure 3. Zoning Status 14
Figure 4. Land Uses 15
Figure 5. Soils 16
Figure 6. Vegetation of Otay Mesa 17
Figure 7. Location of vernal pools at the J28 East site (blue areas; blue hashed area depicts the MHPA) 30
Figure 8. Location of vernal pools at the J21 site (blue areas; blue hashed area depicts the MHPA) 30
Figure 9. 100-year Floodplain in the Water Tanks (East) drainage area (Kimley-Horn and Associate, 2007). 33
Figure 10. Suitable Areas for Vernal Pools with 9% or less Slope and 0.06 inches/hour or less Permeability 35
Figure 11. Potential Areas for Vernal Pools within the Water Tanks (East) drainage area 35
Figure 12. Risk-Based Design Costs Analyses Concepts 39

I. Introduction

Otay Mesa is a community located within the City of San Diego. Originally developed as an industrial area in 1985 in response to the creation of a U.S./Mexico border crossing, Otay Mesa now includes residential areas, an airport, and more than 1200 companies which sell and ship directly to Mexico or utilize the labor pool that commutes from Tijuana. Current development projects in the area include a major transportation project, State Route 905, to improve traffic in the region, with completion anticipated by 2013. With this, continued industrial and residential growth is anticipated. See Figure 1 for a map of Otay Mesa's location.

Figure 1. Location of Otay Mesa

Prior to development, the region was primarily an agricultural community. Effects of increased development were identified soon after it began. Because most of the Mesa drains south towards Mexico, concern arose over increased stormwater runoff crossing the border. In 1987, the City Council approved a contract to prepare the Otay Mesa Master Drainage Plan and published a Notice to "All Private Engineers" that established drainage requirements for development in Otay Mesa. The Notice required no increase in the rate of stormwater runoff from the property after development than it was before development, by the construction of stormwater detention basins on-site. The Notice also

indicated the plans of the City's Engineer Office, Flood Control Section, to prepare a plan for a main north–south channel from Otay Mesa Road to the Mexican border. The *Otay Mesa Drainage Master Plan- Preliminary Channel Design* was published in January 1988, and was updated in August 1999 (*Otay Mesa Drainage Study*), May 2005 (*Otay Mesa Community Plan Update*), and April 2007 (*Drainage Study for the Otay Mesa Community Plan Update*.)

Most existing drainage facilities were constructed as part of private development. These facilities are discontinuous because of the nature of individual development projects, which creates difficulties for subsequent developers that need to connect to private drainage facilities. Most development has occurred in the East Watershed of the Mesa, where most existing drainage facilities are located. These facilities consist of a system of storm drains, improved channels, and detention basins. Many of the detention basins discharge to natural drainages, which do not have adequate hydraulic capacity. Flooding therefore occurs occasionally in the area.

Because of continuing development in the area, recommendations and guidance provided in the previous drainage reports quickly become outdated. This document provides a review of the previous reports and summarizes report recommendations. Current land use and drainage patterns, as well as regulations regarding stormwater are also reviewed to provide up-to-date considerations and recommendations for the placement of storm water management facilities and to shed light on potential restoration projects that may be required to mitigate impacts to sensitive areas (e.g., vernal pools).

II. Review of Completed and Draft Planning and Engineering Reports

A. Introduction

The purpose of this report is to provide a summary of the engineering reports to gain a better understanding on the motivation behind the reports and to highlight considerations that may require additional thought weighed if progress were to be made in implementing the projects contained within the engineering reports.

B. Review of Pertinent Notices and Planning Reports

The following sections are a summary of four engineering reports for the Otay Mesa that were supplied to Tetra Tech by the City of San Diego.

August 7, 1987. Notice to All Private Engineers

The notice required all property in Otay Mesa that is within the watershed that drains to Mexico to be developed with the following requirements:

- Each property owner shall provide stormwater detention facilities so that there will be no increase in the rate of runoff due to development of the property.
- The detention facility shall be designed so that the rate of runoff from the property will be no greater after development than it was before development for a 5-year, 10-year, 25-year, and 50-year storm.
- All drainage facilities crossing four-lane major or higher classification streets shall be designed for a Q100 (existing). Other facilities, except the major channel described below, may be designed for Q50 (existing).

- The Drainage Design Manual shall be used as guidelines for design of drainage facilities, and computing design discharges.
- The City's Engineer Office, Flood Control Section, is preparing a preliminary plan for the main north-south channel from Otay Mesa Road near La Media to the Mexican border. The preliminary design will include the design Q (Q100 existing), the invert grade and the water surface elevation at the major road crossings.

January 1988. Otay Mesa Drainage Master Plan – Preliminary Channel Design

This document provided the initial preliminary design for the main channel indicated in the Notice, above.

Introduction: To prevent flooding problems, the City has required individual developments to regulated runoff from their property. The Mesa is zoned for industrial and commercial use. To allow for the planning and development of the area, an area-wide drainage collection and conveyance system is needed to serve the many individual properties. The report presented a preliminary channel design for a main channel to give Otay Mesa developers a basis for the design of the individual property storm drains.

Hydrologic Analyses: The hydrologic analysis was conducted using the US Army Corp of Engineers (US ACE) HEC-1 flood hydrograph computer model. The watershed was divided into 53 subareas, and the design storm was a 100-year, 6-hour event. The precipitation for the design event was estimated for the 53 subareas from the NOAA isopluvial map for San Diego. Other inputs for the program included the percent of impervious area in the subarea, the Soil Conservation Service (SCS) curve number, which was estimated from SCS soil maps and existing land uses, and the basin lag time. The HEC-1 model calculated peak discharges at 5 flow concentration points along the proposed channel route.

Hydraulic Analyses: The hydraulic analysis was conducted using the US ACE HEC-2 water surface profile computer program. The design discharges for various segments of the channel were those calculated using the HEC-1 model. A minimum of 1 foot of free board was assumed, and the top of road, top of bank, and channel invert elevations needed to develop cross-sectional input data was determined from maps, surveying notes, and road grading plans for the area. Other input parameters for the HEC-2 program were estimated, using the guidelines in the HEC-2 user's manual and independent hydraulic calculations, and included the Manning's "n" roughness coefficient and flow expansion and contraction coefficients. The analysis also assumed that there would be reinforced concrete box culverts placed at the road crossings and that the design would include a spreading basin at the terminus of the proposed channel. The purpose of the proposed spreading basin in the design was to reduce flow velocities, to spread flows such that the discharge to Mexico would occur in approximately the same area, to provide area for potential wetland mitigation, and to lessen the adverse aesthetic of a concrete channel. The results of the hydraulic analysis provided the optimal design of the main channel. The channel was designed as a concrete trapezoidal channel with a 2:1 slope.

Conclusions: The proposed channel would start at the south end of reinforced box concrete culverts under Otay Mesa Road just east of La Media Road, and then end with the spreading basin prior to discharge to Mexico. The proposed channel is approximately 7,570 feet (ft) long, with a width of 56 –

150 ft. The final 515 ft length of the channel would encompass the spreading basin, which would be approximately 600 ft wide. The spreading basin would be planted with natural riparian vegetation and would have a low-flow channel connecting the upstream concrete channel to the existing channel in Mexico.

August 9, 1999. Otay Mesa Drainage Study

This document provided an update to the 1988 Master Plan and identified a project that was compatible with new development plans for Otay Mesa and considered environmental constraints and alternative analyses.

Introduction: The goal of the document was to provide a primary drainage channel from Otay Mesa Road to the border with Mexico to accommodate runoff from existing and future development. Since the 1988 study, new channels, roads, development and detention basins had been constructed. The original project predicted construction of the channel described by 2005. The funding for the project was proposed to be collected from fees collected at the Final Map/ Building Permit approval for new developments.

Hydrologic Analysis: The new hydrologic analysis using the United States Army Corps of Engineers (US ACE) Hydraulic Engineering Center – HEC-1 model reflected runoff expected with new developments. The US ACE HEC-1 model was used, and the SCS method of analysis was used to estimate the rainfall on subareas with the study area. Guidance from the San Diego County Hydrology manual was used in providing required input for the program. The analysis derived subareas and flow concentration points based on existing drainage facilities, and where available, improvement plans for proposed facilities. If no improvement plan was available, the hydrologic criteria and drainage paths were based on assumptions of further development from master plans for the Mesa. The analysis included the proposed SR 905 and SR 125 freeways, and the proposed San Diego Air Commerce Center.

Hydraulic Analysis: Water surface profiles for the proposed channel were generated using the US ACE Hydraulic Engineering Center – River Analysis System (HECRAS), Version 1.2, a US ACE computer program. The HECRAS program determined steady state flow conditions based on user supplied cross section geometry and flow rates.

The slope of the proposed channel would be controlled by the gradual slope of the Mesa, the existing drainage facility located under Otay Mesa Road, and the channel elevation at the border. To convey the 100-year flood flow, the proposed channel would have to be very wide. A rectangular channel was recommended, as the rectangular shape carries the most flow per unit of area. The proposed rectangular channel would have a width of 40 ft across the inside bottom, plus wall width and channel access, such that the total width would be 55 ft. Any channel narrower and deeper than that proposed would possibly affect the ability of adjacent properties to properly drain. Existing sewer lines also constrained the depth of the proposed channel.

Environmental Constraints

Hydrologic: The future design of the Otay Mesa Master Drainage Plan would need to include future projects, including SR 905, SR 125, the Otay Mesa Road future realignment, and the Brown Field Airport. The project must meet the purpose and interest of the San Diego Environmentally Sensitive

Lands Ordinance. The channel design must also consider the effects of other planned projects in the vicinity and the concerns of the International Boundary and Water Commission (IBWC) regarding stormwater runoff rates. Permit requirements for the project would also likely include the use of soft bottom for the channel and incorporation of natural vegetation as much as possible, and demonstration that the project minimizes impacts to regional wildlife habitat.

Biological Resources: The Empire Center Mitigation Site, constructed in 1997 as part of a City, State and federal permitting action for an earlier project, included 5 acres of land in an area north of Airway Road and west of La Media Road and included over 12 created and naturally occurring vernal pools and habitat for San Diego button celery, a federally listed species. At least 14 vernal pools, encompassing approximately 25,756 ft^2, are located outside of the mitigation area. A patch of freshwater marsh was identified in the vernal pool restoration area. Mitigation at a probable ratio of 2:1 would be required to ameliorate any impacts to vernal pools and the freshwater marsh. Indirect effects to wetlands through changes in drainage patterns that could significantly affect their functionality would also possibly require mitigation.

Recommended actions for the Master Drainage Plan in reference to biological resources constraints included:

- Avoiding impacts to the Empire Centre Mitigation Site;
- Accurately mapping vernal pools with a survey crew in the spring;
- Avoiding impact to the vernal pools or concurrently mitigating impacts to the pools outside of the project site;
- Avoiding impacts to federally listed and narrow endemic plant species (i.e., San Diego celery-button, Otay tarplant, and variegated dudleya;
- Avoiding impacts to the San Diego Multi-Habitat Planning Area (MHPA);
- Including plans in the Master Drainage Plan to maintain low flow drainage patterns to avoid indirect effects on wetland habitats;
- Conduct surveys for burrowing owl burrows prior to development and impacts should be avoided or mitigated;
- Conduct protocol surveys for other potential federally listed species on the site;
- Mitigation of nonnative grassland at a ratio of 0.5:1.

Cultural Resources: Completion of a literature review and record searches at San Diego University and the San Diego Museum of Man was recommended for previously conducted archeological surveys.

Alternative Analyses

The objective of the alternatives analysis was to identify an alignment for the drainage channel that will efficiently convey the flows from an existing rectangular concrete box culvert under Otay Mesa Road to the U.S.-Mexico Border while minimizing impacts on environmentally sensitive areas and adjacent properties. The preferred alternative placed the channel along the east side of La Media to a box culvert crossing from the northeast corner to the northwest corner of the intersection of La Media with Siempre Viva Road. The channel continued along the north side of Siempre Viva from the box culvert outlet at La Media to a box culvert crossing to the south side of Siempre Viva to connect to the existing stream channel. This alternative was chosen as the preferred alternative because an existing drainage ditch is on the east side of La Media Road; the channel would intercept flows from

the east without potential conflicts from utilities in La Media Road; and flows from the west would continue to flow in the old drainage path. Additionally, the alternative minimizes impact on properties by following the property line and minimizes potential utilities conflicts in Siempre Viva Road by crossing under it through a box culvert at the existing stream location.

Possible funding mechanisms identified for funding the project included general obligation bonds, Mello-Roos Community Facilities Districts tax, special assessment bonds, and certificates of participation.

May 2005. Drainage Study for Otay Mesa Community Plan Update

The report was prepared as an appendix to the Otay Mesa Community Plan update EIR to provide a summary of existing drainage facilities and to provide alternatives for draining the Mesa. Most existing drainage facilities are located within East Watershed. The system existing at the time of the report was a combination of storm drains, improved channels, and detention basins, which discharge in many areas to natural drainage paths that do not have adequate hydraulic capacity. As many of the projects have been developed, portions of the properties have been dedicated to the city as drainage easements or flood water storage easements. These were presumably recorded as easements, however, this part of the Study was not verified.

Hydrologic Analysis: The Otay Mesa Drainage Study area included all of the Mesa area within the City of San Diego, divided into 5 watersheds (West Perimeter, West, North Perimeter, East, and Border Crossing), excluding the far northwest arm of the Mesa which had been fully developed. Most of Otay Mesa slopes from north to south with flow entering Mexico at several points. The perimeter of the Mesa drains into the adjacent canyons. The watershed boundaries on the Mesa are not well defined because the Mesa is flat, with stormwater run-off mostly sheet-flowing across the Mesa. Previous drainage study reports (1988, 1999) prepared hydrologic analyses for the East watershed. In the current report, new hydrologic models were developed using the HEC-1 model for the East watershed, since that was the hydrologic model previously used in analysis of the watershed. For the other main watersheds, West Perimeter and West, the AES-developed standard City of San Diego Modified Rational Method was used. The hydrologic analyses calculated that the total flow from these watersheds at the concentration point at the border for the 100-year flow was 5,793 cubic feet per second (cfs). The Spring Canyon open space in the West Watershed was calculated to contribute an additional 257 cfs.

Hydraulic Analysis: The HEC-RAS model was used to size the 100-year floodplain of Otay Mesa Creek based on current conditions. The model was also used to size the proposed new channel to contain the 100-year flow which would reduce or eliminate flooding impacts to nearby facilities. An existing channel that is tributary to the proposed main channel and located just upstream of the Siempre Viva Road Crossing is approximately 15 ft wide and 4 ft deep, with a hydraulic capacity of approximately 120 cfs. The 100-year flow in this channel however would be 1116 cfs. A new channel proposed for this tributary by this report is sized 50 ft wide with 1.5:1 side slopes to convey the 100 year flow. The cost estimate proposed by this report does not include this tributary channel.

Proposed Drainage Facilities: Caltrans had completed their plans for the SR-905 project. For proposed private development, the only Master Planned facility which would need to be constructed prior to

continued development is the Main Channel and the Detention Basin in the East Watershed. The Main Channel proposed by this report would have a bottom width of 240 ft at the Detention Basin to 200 ft from just north of Siempre Viva Road to the intersection of Airway Road and La Media Road. The side slopes would be 4:1 to 10:1 and heavy riparian vegetation would be allowed to grow in the channel. Hiking trails and access roads with a width of 12 feet would line each bank of the channel. At the Airway Road and La Media intersection, a 35 ft wide concrete channel would connect the channel with the proposed Caltrans culverts which would be constructed concurrently with SR 905.

The proposed Detention Basin was designed to attenuate peak flows from 5 year to 100 year storms, with dimensions of approximately 1700 ft by 1500 ft. The basin would encompass 58 acres with a maximum storage depth of 6.0 ft and a maximum storage volume of 308 acre-ft. The basin would be graded and vegetated to appear natural and to create a low flow stream. The basin and channel would require removal of 915,000 cubic yards of soil. It was assumed this soil would be used on adjacent properties to raise building pad grades.

A preliminary cost estimate was $23,868,000 to complete the proposed project.

Recommended Drainage Design Criteria: The current study estimated that approximately 140 cfs will flow off of Otay Mesa into the West Perimeter Watershed. Detention basins were recommended for this watershed to reduce peak flows to predevelopment levels. Because of unstable soils in the area, placement of these detention basins and relocation of drainage facilities should be planned carefully to avoid an increase in soil instability and slope failure.

The West Watershed consists of smaller mesa-top watersheds that drain into the tributary canyons of Spring Canyon, which then flow into Mexico via the Spring Canyon concentration point. Detention basins were recommended in this watershed to reduce post-development peak flows to predevelopment levels. Care must be taken if detention basins concentrate flows at the upper edge of canyons so that erosion potential is not increased downstream.

Requirements have already been implemented in the East Watershed for control of peak runoff from development. The August 7, 1987 Notice provided requirements for individual developments to regulate stormwater such that runoff from developed properties did not increase above the runoff rate prior to development. The proposed single Detention Basin at the border would eliminate the need for individual on-site detention basins for subsequent development.

In the North Perimeter watershed, there were no identified peak flow attenuation requirements for the small watersheds that flow into small canyons that flow into the Otay River.

Stormwater Quality Requirements: The City requires Best Management Practices (BMPs) be constructed for all new projects. In 2003, the City published “Storm Water Standards – A Manual for Construction & Permanent Storm Water Best Management Practices Requirements”, a reference document for all stormwater issues encountered in development. Most projects on Otay Mesa will require Priority Project Permanent Storm Water BMPs and High Priority Construction Storm Water BMPs. The manual requires the submission of a “Water Quality Technical Report” for all projects subject to priority permanent BMP requirements.

Most of Otay Mesa drains to the south across the U.S./Mexico border to the Tijuana River, which has been identified as an impaired water body pursuant to section 303(d) of the Clean Water Act. A small portion of the drainage flows north into the Otay River and the far western part of the Mesa flows to the west through San Ysidiro and then into the Tijuana River.

April 2007. Drainage Study for the Otay Mesa Community Plan Update

The 2007 report was identical to the 2005 report, except for the addition of a section regarding the proposed drainage alternatives. This additional section is summarized below.

No Project Alternative: The alternative of doing nothing to improve drainage along the main creek channel would prevent future development from taking place along portions of La Media Road. The intersection of Airway Road and La Media Road floods during significant precipitation. The existing creek would not be deep enough to allow adjacent properties to drain effectively. To provide continued access along the truck route during storms the roads would need to be raised to allow flow to pass under them, or an alternative route would need to be identified.

Concrete Channel: The 1999 Otay Mesa Drainage Study identified a concrete channel as a recommended plan from Otay Mesa Road to the Border Detention Basin. The concrete channel would follow the east side of La Media Road until intersecting at Siempre Viva Road, where it crossed under La Media and followed on the north side of Siempre Viva to box culverts under Siempre Viva that connected to the Border Detention Basin. The concrete channel plan assumed that the existing creek with its habitat would continue to carry low flows. The 1999 cost for this project was $10.6 million dollars, without including land acquisition costs, which corresponds to a 2005 cost of $14.9 million.

La Media Channel and Border Detention Basin: The East Watershed is the largest watershed on the Mesa. All flows from the watershed collect at a concentration point at a large culvert where flows cross the U.S./Mexico border. The surrounding area is very flat and adjacent properties cannot drain effectively into the existing creek. To allow for future development, and to accommodate runoff from proposed future projects, a new channel would be required that has an invert of 3 to 5 feet below that of the existing creek channel. The proposed La Media Channel and Border Detention Basin would be built as described in the 2005 report.

C. Impetus of Drainage Studies

Tetra Tech was asked to provide as much detail as possible into the funding and motivation behind the drainage studies completed for Otay Mesa. It is well understood that the first report in 1988 was intended to provide drainage opportunities in the developing Otay Mesa area. The 1999, 2005, and 2007 reports all indicate the need for drainage planning in the rapidly developing Mesa area but also point to the need for water quality considerations and regulations, as well. Meeting regulatory requirements for flood and drainage control (1988) as well as water quality and environmental considerations (1999, 2005, and 2007) seem to be the initial motivation behind the reports.

The drainage reports provided little insight into the funding mechanisms supporting these studies. There were suggestions in several of the studies for funding mechanisms to implement the recommendations

within the studies including general obligation bonds, Mello-Roos Community Facilities Districts tax, special assessment bonds, and certificates of participation. Based on the direction of recommendations, the development community might have initiated the request for drainage control and improved drainage within the public right of way to accommodate drainage from developing areas. However, it is also quite possible that the motivation was also a part of a plan to design the public portion of the drainage system to fully accommodate a built out Otay Mesa that would provide the necessary public safety and flood control needs that a future fully developed scenario might require.

III. Data Compilation and Review

Plans and data including GIS data relevant to Otay Mesa study have been compiled for this report. Relevant drainage requirements and existing drainage plans for Otay Mesa area are summarized in the previous section. Using GIS data, drainage areas for the project site were defined and relevant spatial analyses have been conducted for each drainage area. Potential areas for restoring or improving vernal pools were identified using soil suitability, land uses, and site availability.

A. Data Compilation

The following data were compiled for this Otay Mesa study. Most of the data were downloaded from two websites, SanGIS (http://files.sangis.org/) and SANDAG (http://www.sandag.org/). Vernal pools data were supplied directly from the City.

- Otay Mesa community boundary (SanGIS)
- Zoning (SanGIS)
- Land use (SANDAG)
- Soils (SanGIS)
- Topography: 20-m DEM and 2-ft contours (SanGIS)
- Streams (SanGIS)
- Roads / Streets (SanGIS)
- Parcel boundaries (SanGIS)
- Watershed / Subwatershed boundaries (SanGIS)
- Vegetation (SanGIS)
- Existing vernal pools (City)

B. Drainage Areas

From the existing watershed/subwatershed data, three drainage areas were found in the Otay Mesa study area, which are Otay Valley, San Ysidro, and Water Tanks. Otay Valley covers north of Otay Mesa around the Otay River, San Ysidro covers west, and Water Tanks covers south of Otay Mesa. Otay Valley and Water Tanks were sub-divided into east and west areas respectively. As a result, the Otay Mesa area was divided into five drainages as shown in Figure 2. The sizes of drainage areas are presented in Table 1.

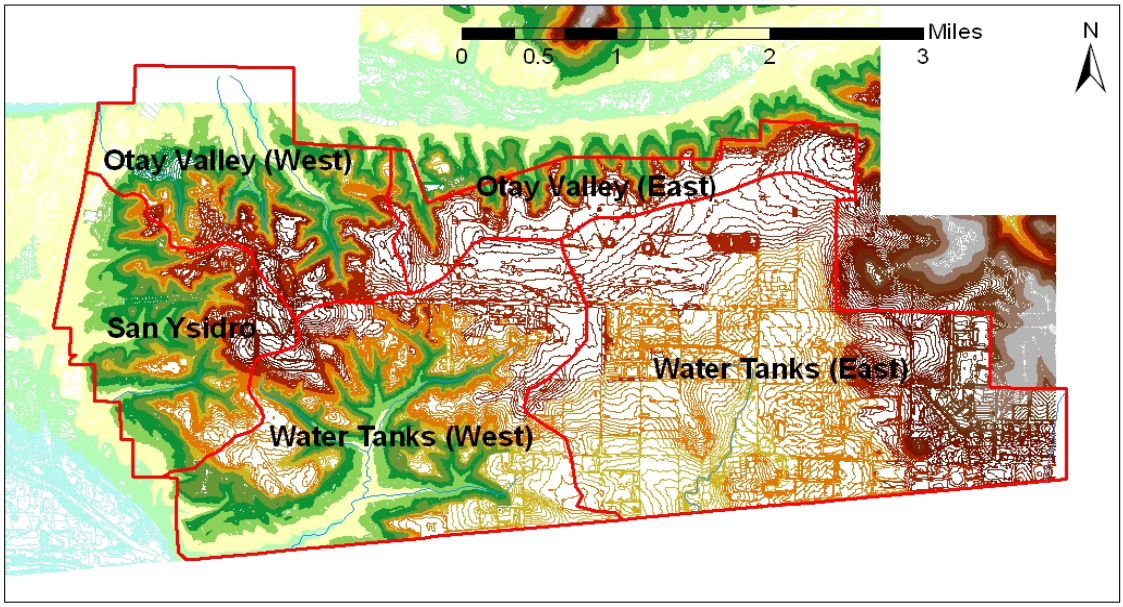

Figure 2. Defined Drainage Areas

Table 1. Drainage Area Sizes

Drainage Areas	Acres
Otay Valley (East)	827.5
Otay Valley (West)	1,378.4
San Ysidro	1,226.1
Water Tanks (East)	3,380.2
Water Tanks (West)	2,488.0
Total	9,300.2

C. Zoning Status

Existing zoning for the Otay Mesa is presented in Figure 3. Otay Mesa zoning consists of Industrial (41.2%), Agricultural (25.4%), Residential (12.2%), Commercial (4.8%), Open Space (0.2%), Other (4.8%), and Unzoned (11.4%) areas. The individual drainage area of each zone and total area is summarized in Table 2.

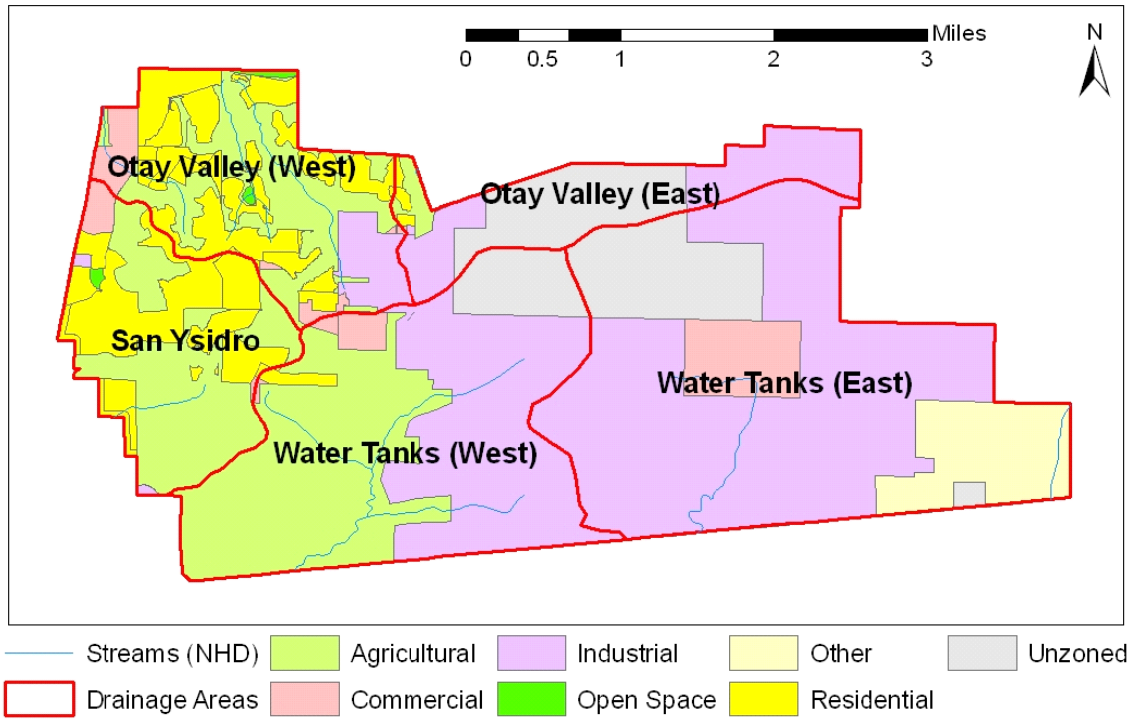

Figure 3. Zoning Status

Table 2. Zoning Status for Drainage Areas

Zoning	Drainage Areas					
	Otay Valley (East)	Otay Valley (West)	San Ysidro	Water Tanks (East)	Water Tanks (West)	Total
Agricultural	46.3	543.2	643.0	0.0	1,127.3	2,359.8
Commercial	0.7	100.2	43.2	241.5	61.5	447.0
Industrial	378.4	149.3	10.6	2,227.9	1,062.6	3,828.7
Open Space	0.0	15.1	5.9	0.0	0.0	21.0
Other	0.0	0.0	0.0	445.3	0.0	445.3
Residential	18.8	570.7	523.3	0.0	25.8	1,138.6
Unzoned	383.3	0.0	0.0	465.7	210.8	1,059.8
Total	827.5	1,378.4	1,226.1	3,380.3	2,488.0	9,300.2

D. Land Uses

Land use status for Otay Mesa is presented in Figure 4 using the 2009 SANDAG land use data set. The detailed land use status for each drainage area is summarized in Table 3. The Otay Mesa land uses consist of Open Space (28.8%), Undeveloped (25.4%), Transportation (21.5%), Industrial (12.1%), Residential (5.6%), Agricultural (3.3%), Commercial (2.1%), Education (1.0%), and Park (0.1%). Land use status appears quite different from the Otay Mesa zoning status. This might be because some areas within a particular zone are not fully developed or because the land use data have more detailed spatial descriptions, which consider topography that can impact land use, than the zoning data.

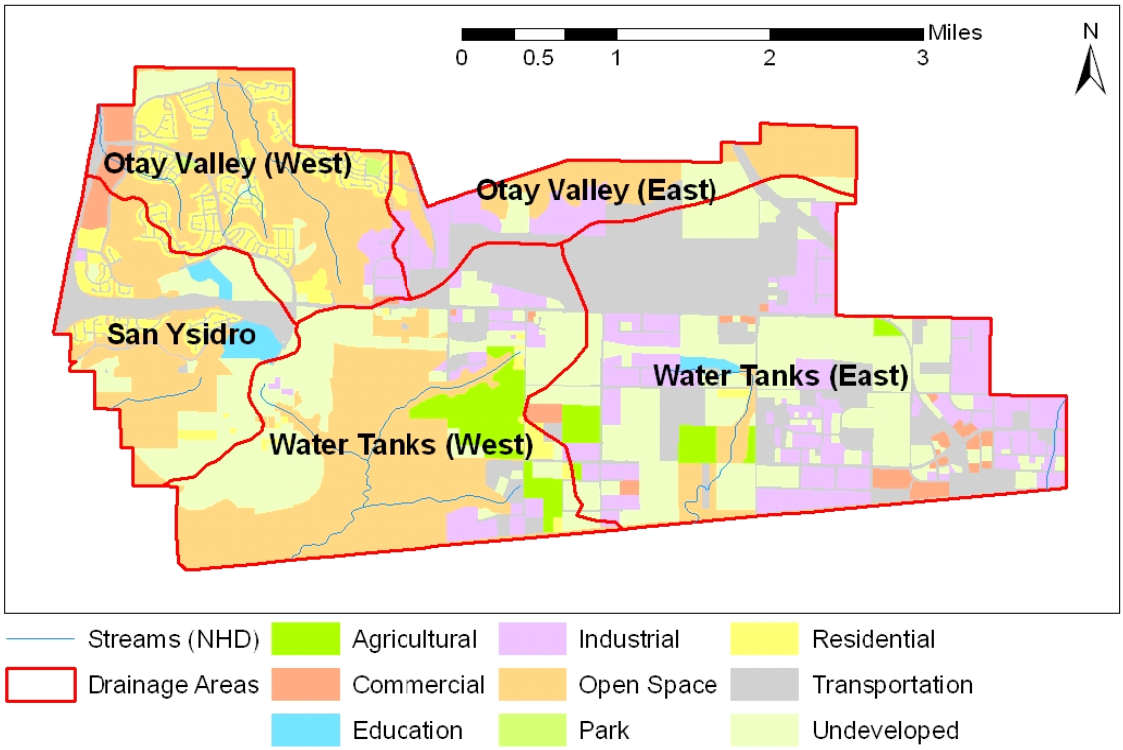

Figure 4. Land Uses

Table 3. Land uses for Drainage Areas

Land Use	Drainage Areas					
	Otay Valley (East)	Otay Valley (West)	San Ysidro	Water Tanks (East)	Water Tanks (West)	Total
Agricultural	0.0	0.0	0.0	101.6	204.3	305.9
Commercial	0.0	60.7	30.6	101.3	5.4	197.9
Education	0.0	0.0	70.1	17.6	0.7	88.4
Industrial	181.6	59.8	2.9	740.5	137.6	1,122.6
Open Space	377.3	629.0	461.2	133.1	1,081.3	2,681.9
Park	0.0	12.9	0.0	0.0	0.0	12.9
Residential	10.7	316.8	136.0	9.9	49.7	523.1
Transportation	146.5	190.0	227.0	1,148.0	290.1	2,001.7
Undeveloped	111.4	109.2	298.1	1,128.2	719.0	2,366.0
Total	827.5	1,378.4	1,226.1	3,380.2	2,488.0	9,300.2

E. Soils

Soil properties for the Otay Mesa are presented in Figure 5. Soil coverage for each drainage area is summarized in Table 4. Otay Mesa is covered mainly by loam (81.2%) and clay (18.0%) type soils.

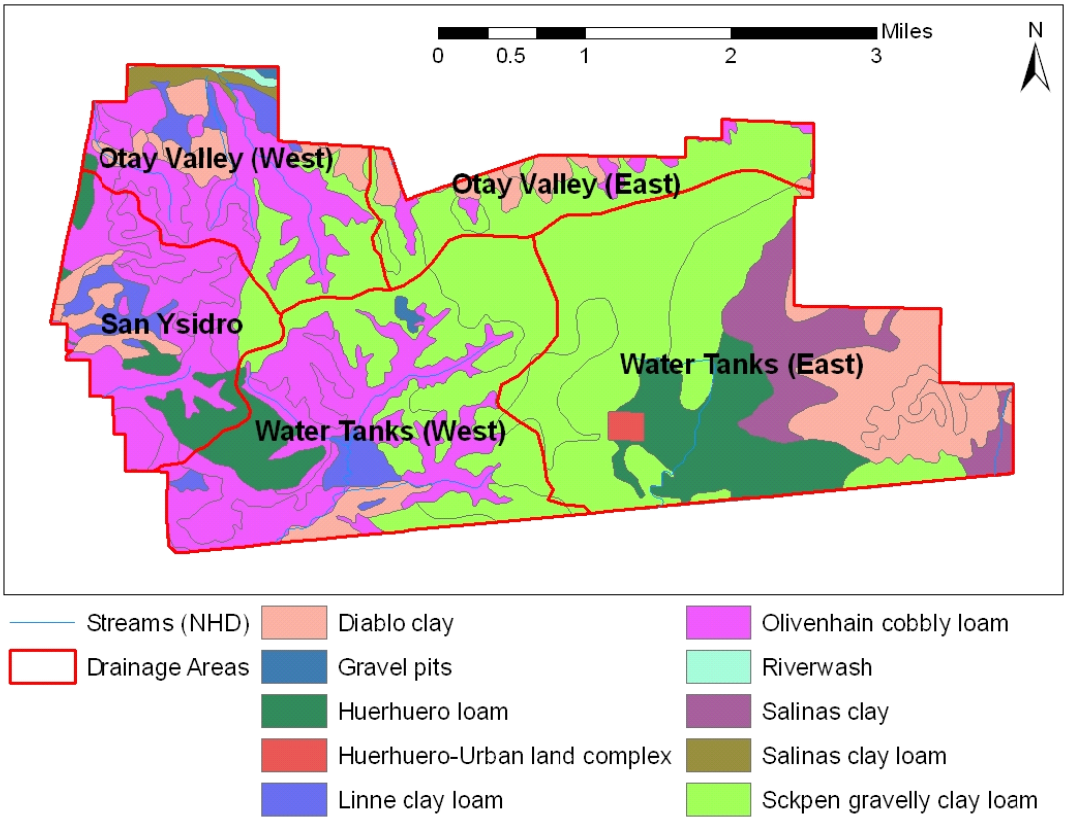

Figure 5. Soils

Table 4. Soils for Drainage Areas

Soils	Drainage Areas					
	Otay Valley (East)	Otay Valley (West)	San Ysidro	Water Tanks (East)	Water Tanks (West)	Total
Diablo clay	149.8	196.0	121.3	635.1	98.0	1,200.1
Gravel pits	0.0	8.6	0.0	0.0	15.7	24.3
Huerhuero loam	0.0	6.9	174.7	606.4	182.4	970.4
Huerhuero-Urban land complex	0.0	0.0	0.0	31.4	0.0	31.4
Linne clay loam	1.5	93.2	111.1	0.0	105.9	311.7
Olivenhain cobbly loam	83.0	714.0	742.3	0.0	989.7	2,529.1
Riverwash	0.0	17.8	0.0	0.0	0.0	17.8
Salinas clay	0.0	0.0	0.0	474.1	0.0	474.1
Salinas clay loam	0.0	71.3	0.0	0.0	0.0	71.3
Stockpen gravelly clay loam	593.1	270.7	76.7	1,633.2	1,096.2	3,670.1
Total	827.5	1,378.4	1,226.1	3,380.2	2,488.0	9,300.2

F. Vegetation

Vegetation coverage for Otay Mesa is presented in Figure 6. The size of vegetation coverage for each drainage area is summarized in Table 5. Otay Mesa vegetation consists mostly of non-native vegetation or developed/unvegetated areas (70.6%), scrub and chaparral (18.9%), grasslands and meadows (10.2%), and other areas (0.4%).

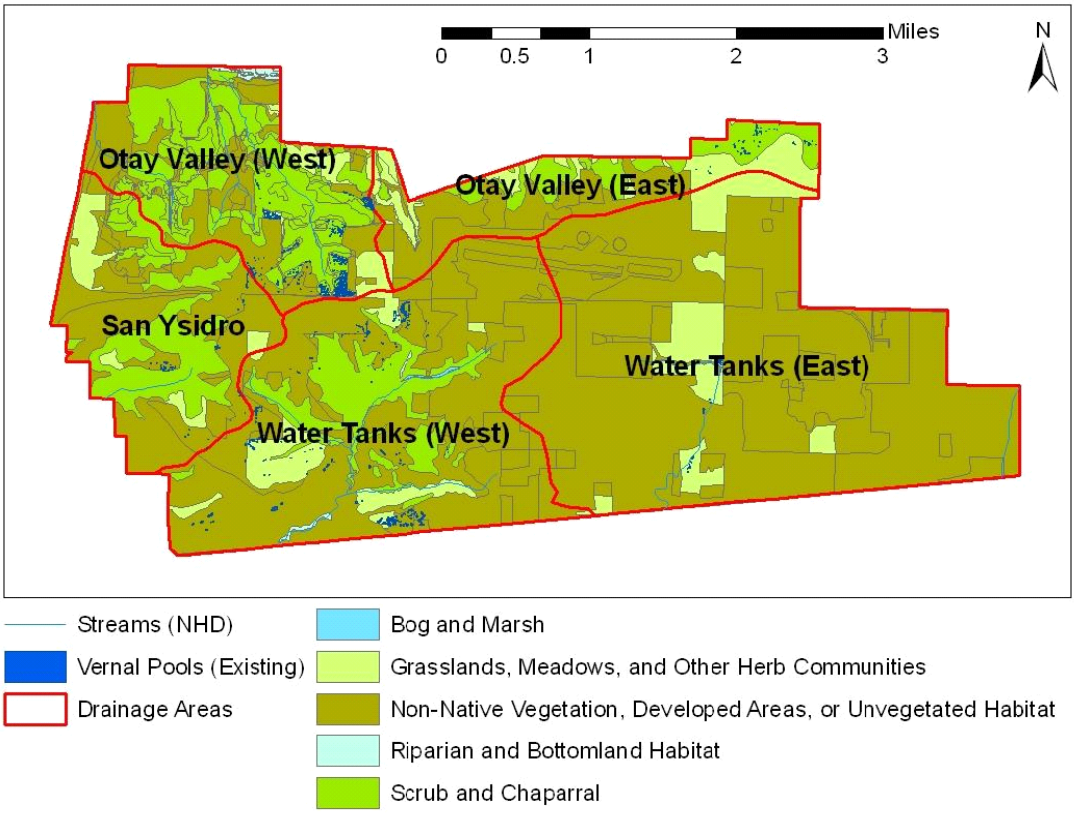

Figure 6. Vegetation of Otay Mesa

Table 5. Vegetation Coverage for Drainage Areas

Vegetation	Drainage Areas					
	Otay Valley (East)	Otay Valley (West)	San Ysidro	Water Tanks (East)	Water Tanks (West)	Total
Bog and Marsh	0.0	0.8	0.0	0.0	4.0	4.8
Grasslands, Meadows, and Other Herb Communities	205.1	88.6	112.0	341.0	201.8	948.5
Non-Native Vegetation, Developed Areas, or Unvegetated Habitat	394.2	528.9	720.2	3,039.2	1,883.4	6,565.9
Riparian and Bottomland Habitat	0.0	17.6	0.2	0.0	8.6	26.4
Scrub and Chaparral	228.2	742.5	393.7	0.0	390.2	1,754.7
Total	827.5	1,378.4	1,226.1	3,380.2	2,488.0	9,300.2

IV. Environmentally Sensitive Lands

A. Vernal Pool Background

Vernal pools are unique seasonal and ephemeral wetlands that result from specific depression-type geomorphic regions. (City of San Diego Vernal Pool Inventory, 2004) Vernal pools form when small, shallow depressions collect precipitation, and by nature are dry basins in the dry months followed by variable lengths of saturation and inundation. [Draft City of San Diego Multiple Species Conservation Program (MSCP) Vernal Pool Management Plan, 2008] The variability in moisture conditions separates these pools from other wetland ecosystems, which is a characteristic of the Mediterranean –type climate that exists in southern California.

Within the City of San Diego, groups or series of vernal pools are found in Del Mar Mesa, Mire Mesa, Carmel Mountain, Kearny Mesa, Mission Trails Regional Park, Otay Mesa, Otay Lakes, and Marron Valley. The pools are often associated with small hills known as Mima mounds, and form in the inter-mound swales. The vernal pools located in these areas have been found to be associated with the particular soil types in these areas. (Bauder and McMillan, 1998) In Otay Mesa, Stockpen, a gravelly clay, is the dominant type of pool-supporting soil, as identified from the county's 1973 Soil Survey maps, with the type of vernal pools associated with this soil called Coastal Mesa pools. Coastal mesa pools are found almost exclusively on the mesas but sustain different flora and fauna depending on the dominant soil series.

Vernal pools support a specific biological ecosystem. Research has found that 47 plant species from 20 families are restricted to vernal pool habitat. (Draft San Diego MSCP Vernal Pool Management Plan, 2008) Vernal pool habitat also supports animals from insect larvae to amphibians, birds, and mammals. San Diego vernal pools provide habitat for two federally listed endangered invertebrates, San Diego and Riverside fairy shrimp; five federally listed endangered plants, spreading navarretia, San Diego and Otay mesa mint, San Diego button celery, and California Orcutt grass; and an unprotected, although rare, plant, little mousetail. *Pogogyne nudiuscula* is a mesa mint species endemic to the coastal mesa pool type of Otay Mesa.

Ecological processes that occur within vernal pools are complex, and not fully understood. Local processes are affected by the relatively short period of wet conditions and relatively small affected area (Leidy and White, 1998). The ecology of the vernal pool is also influenced by larger-scale effects of the watershed including landscape processes of stormwater run-off and native and invasive vegetation. Vernal pools and their associated wetland functions may be indirectly impacted by changes in the watershed, especially changes in hydrologic conditions which need to be considered when development or other landscape changes occur.

B. Otay Mesa Vernal Pools

Within Otay Mesa, the number and quality of vernal pools has been impacted historically by farming and grazing, and more recently, by rapid development in the area. Vernal pool surveys in the San Diego area have been conducted since the late 1970s. In 1988, the California Department of Parks and Recreation estimated that approximately 905 of the Otay Mesa vernal pools had been lost to urban development, agriculture and mining (Leidy and White, 1998). The most recent survey was conducted by the City of San Diego in 2002 – 2003 (City of San Diego Vernal Pool Inventory 2002 – 2003, 2004). This survey identified 29 series, or clusters, of vernal pool basins within the Otay Mesa area, and a total of 983

basins. The survey also identified a total of 12.89 acres of pools that were under creation, enhancement or restoration activities.

The Draft San Diego MSCP Vernal Pool Management Plan identified several factors that should be considered in management and preservation of vernal pools, with urban development identified as the primary threat to these ecosystems. Border Patrol activities along the U.S./Mexico border have caused impacts to Otay Mesa vernal pools because of foot traffic of illegal immigrants and Border Patrol agents. Recreational off-road vehicle users, illegal dumping and littering have also lead to vernal pool impacts. Disturbance and fragmentation of native habitat have resulted in vernal pool ecosystem impacts.

Recommendations for management of vernal pool resources have been implemented at the City and federal level. The 2008 draft San Diego MSCP Vernal Pool Management Plan includes site-specific management requirements and general recommendations for multiple vernal pool complex locations in Otay Mesa. These recommendations include conservation, enhancement or restoration of degraded basins through government implementation, project mitigation requirements, and/or interested non-governmental organizations. The document also recommended research on vernal pool plant genetics, native pollination and dispersal mechanisms to better understanding of vernal pool functions. Also, public education efforts are recommended to increase awareness of vernal pools. The City prioritized the following recommendations:

1. Conservation of land comprising the vernal pool site(s) through government or private land trust acquisition, dedication in fee title, conservation easement, or covenant of easement.
2. Adequate protection of conserved vernal pools from illegal and inadvertent impacts by fencing the site, placing signs, and providing education and/or law enforcement patrol of the sites.
3. Enhancement or restoration of vernal pools to reinstate historic ecosystem functions and values.
4. Solicit and fund, if possible, research on vernal pool ecosystems.

The recommendations provided by the Vernal Pool Management Plan may be enforceable by regulatory agencies through permit conditions, approved mitigation, monitoring and reporting programs, a Biological Opinion resulting from a Section 7 consultation with the U.S. Fish and Wildlife Service (FWS), and development agreement(s).

The U.S. FWS first provided a vernal pool recovery plan for southern California in 1998, and again in 2005. The more recent plan addressed 33 species of plants and animals that occur exclusively or primarily within a vernal pool ecosystem in California, with the ultimate goal of achieving and protecting self-sustaining populations of each species, through stabilizing and protecting populations to prevent further decline. (U.S. FWS, 2005) The key elements included in the plan for achieving these goals were habitat protection; adaptive management, restoration and monitoring; status surveys; and research.

U.S. EPA has also provided recommendations for vernal pool compensation and conservation (Leidy and White, 1998). In light of the complex system of processes that occur within vernal pool ecosystems, and the relationship of these niches to the larger watershed, U.S. EPA recommended using an ecosystem approach in assessing vernal pool compensation. The ecosystem approach would base compensation on preservation of vernal pool complexes within *an ecosystem* rather than the current approach of creating or restoring isolated pools. A hydrogeomorphic approach to assessing wetland function was

recommended to provide the most efficient method to determine mitigation requirements for impacted vernal pools (Leidy and White, 1998).

V. Review of Stormwater Regulations

A. Federal Regulations and Permits

CWA Section 404 Permits

Most projects conducted in or adjacent to streams or wetlands will require a U.S. Army Corp of Engineers (US ACE) Clean Water Act (CWA) Section 404 Permit. A Section 404 Permit is required if materials, including dirt, rocks, geotextiles, concrete, or culverts, are moved or placed into or within US ACE jurisdictional areas. Permit coverage may be granted if the following are performed: (1) actions are taken to avoid wetland impacts, (2) potential impacts are minimized, and (3) compensation for any unavoidable impacts is provided.

Proposed activities are regulated through a permit review process. An individual permit is required for potentially significant impacts. Individual permits are reviewed by the US ACE and evaluated under a public interest review, as well as the environmental criteria set forth in the CWA Section 404(b)(1) Guidelines. However, for most discharges that will have only minimal adverse effects, a general permit may be suitable. The Section 404 general permit process is more streamlined than the individual permit process due to the elimination of the individual review, provided that the general or specific conditions for general permit coverage are met. General permits are issued on a nationwide, state, or regional basis for particular categories of activities.

- Regional General Permits (RGPs) are issued for common maintenance-type activities with minimal impact to the environment and often include pre-approval from the RWQCB Section 401 Certification and/or from the U.S. Fish and Wildlife Service (FWS) and NOAA Fisheries Service for Endangered Species Act consultations. Permit coverage takes approximately one to six months for existing activity categories or six months to one year for new and unique activity categories.
- Nationwide Permits (NWPs) are written for categories of projects that occur nationwide, such as road crossings, bank stabilization, repairs to existing structures, flood control maintenance, and wetland restoration for wildlife habitat. Permit coverage takes from three to nine months.
- An Individual Permit (IP) may be required if over one-half acre of permanent impacts may occur. Public review is required for an IP, which lengthens the amount of time between permit application and permit coverage (six months to a year under the best circumstances, but can be multiple years).

The 404 Permit process should begin with a consultation with US ACE. Prior to application for a Section 404 Permit, a wetland delineation and estimation of US ACE jurisdictional area should be performed. RWQCB 401 Water Quality Certification must also be obtained when applying for a NWP or IP. After any pre-application steps are completed, the US ACE “Application for Department of the Army Permit” should be prepared and submitted.

The US ACE Section 404 permit also requires that a Section 106 Review be conducted as part of the permit application. Section 106 is a document review of the project site for historical significance. Based on the results, additional studies may be required, such as an additional Historical/Archaeological Report or mitigation to protect the historical significance of the site. The review search and approval duration varies on the project scope.

Endangered Species Act

Impacts to endangered or threatened species are regulated under both the California Endangered Species Act (CESA) administered by CA Department of Fish and Game (DFG) and the federal Endangered Species Act (ESA) administered by US Fish and Wildlife Service (FWS). Species that are protected under these laws are designated on the state and federal endangered and threatened species lists. The term "take" is used to describe the impact to a species. Under Section 2081 of the DFG code, a development project that coincides with the occurrence of a listed species must have an incidental take permit. To obtain this permit, the applicant must meet the following criteria (California Department of Fish and Game, 2009):

1. The authorized take is incidental to an otherwise lawful activity
2. The impacts of the authorized take are minimized and fully mitigated
3. The measures required to minimize and fully mitigate the impacts of the authorized take are roughly proportional in extent to the impact of the taking on the species, maintain the applicant's objectives to the greatest extent possible, and are capable of successful implementation.
4. Adequate funding is provided to implement the required minimization and mitigation measures and to monitor compliance with and the effectiveness of the measures
5. Issuance of the permit will not jeopardize the continued existence of a State-listed species.

A mitigation plan is attached to a permit that outlines how these criteria will be met. Measures for meeting the criteria vary and may include avoidance measures or acquisition and transfer of habitat management lands (including funds for protecting and maintaining land in perpetuity). Applicants must avoid all take for "fully protected" species and "specified birds" as defined in Fish and Game Code Sections 3505, 3511, 4700, 5050, 5515, and 5517 (http://www.leginfo.ca.gov/cgi-bin/calawquery?codesection=fgc&codebody=&hits=20). All take of bird species protected under the Migratory Bird Treaty Act must also be avoided, as stated in Section 3515 of the DFG code.

An applicant determines whether an incidental take permit and a Habitat Conservation Plan (HCP) are required by contacting the nearest DFG. The potential need for a permit can be assessed by using the DFG's online mapping resources. If a listed species is present on the property and the project will result in a take of that species, then a permit is required. Permit processing is likely to take between 3 and 12 months or longer depending on the project circumstances and whether a federal permit is required.

To meet federal ESA requirements for a take of federally listed species, an incidental take permit (http://www.dfg.ca.gov/habcon/cesa/incidental/CodeRegT14_783.pdf) must also be obtained by developing a HCP that outlines plans to offset impacts to the species listed as threatened or endangered (http://www.fws.gov/Endangered/wildlife.html). HCP must meet the following criteria:

1. Taking will be incidental
2. The applicant will, to the maximum extent practicable, minimize and mitigate the impacts of the taking
3. The applicant will ensure that adequate funding for the plan will be provided
4. Taking will not appreciably reduce the likelihood of the survival and recovery of the species in the wild
5. Other measures, as required by the Secretary, will be met.

Mitigation measures for ESA, like measures for CESA, vary by the project and may include the following:

- Payment into an established conservation fund or bank
- Preservation (via acquisition or conservation easement) of existing habitat
- Enhancement or restoration of degraded or a former habitat
- Establishment of buffer areas around existing habitats
- Modifications of land use practices and restrictions on access.

An applicant determines whether an incidental take permit and HCP are required by contacting the nearest DFG or FWS office. If a listed species is present on the property and the project will result in a take of that species, then a permit is required.

Under ESA, an incidental take permit is not required for plant species. However, if a permit is required for other endangered or threatened species and an HCP must be prepared, then the HCP must analyze the effects of the action on any endangered or threatened plant species. Accordingly, if a plant is on the California threatened or endangered list, then a permit must be obtained through DFG.

The timeline for federal incidental permit processing varies by project complexity and whether FWS must require National Environmental Policy Act (NEPA) documentation. Minor, or "Low Effect," HCPs do not require FWS to prepare NEPA documentation, and the target processing time for these HCPs is three months. HCPs that require an Environmental Assessment (EA) under NEPA have a target processing time of four to six months, and for HCPs requiring an Environmental Impact Statement (EIS), processing may take up to 12 months or longer (U.S. Fish and Wildlife Service, 2005).

A Section 7 Consultation may also be required under the ESA if the project has a "federal nexus," usually in the form of another federal permit or federal funding, at some stage of the project and with any federal agency. The type of consultation will be either informal or formal, depending on whether the project affects listed or protected species. If the project has a federal nexus, it will also require NEPA documentation, which is described under the federal requirements section of this report.

Data on endangered and threatened species observations are available from the California Natural Diversity Database, which is developed by the Biogeographic Data Branch of DFG, and these data estimate the approximate spatial range of the species.

B. State Regulations and Permits

California Endangered Species Act (CESA)

CESA states that all native species of fishes, amphibians, reptiles, birds, mammals, invertebrates, and plants, and their habitats, threatened with extinction and those experiencing a significant decline which, if not halted, would lead to a threatened or endangered designation, will be protected or preserved (California Department of Fish and Game, no date). Sections 2081(b) and (c) of CESA allow the California DFG to issue an incidental take permit for a State listed threatened and endangered species only if specific criteria are met. These criteria are as follows:

- The authorized take is incidental to an otherwise lawful activity;
- The impacts of the authorized take are minimized and fully mitigated;
- The measures required to minimize and fully mitigate the impacts of the authorized take are roughly proportional in extent to the impact of the taking on the species, maintain the applicant's objectives to the greatest extent possible, and are capable of successful implementation;
- Adequate funding is provided to implement the required minimization and mitigation measures and to monitor compliance with and the effectiveness of the measures; and
- Issuance of the permit will not jeopardize the continued existence of a State-listed species.

Measures to minimize the take of species covered by the permit and to mitigate the impacts caused by the take will be set forth in one or more attachments to the permit. Incidental Take Permit Applications include the following (California Department of Fish and Game, 2008):

1. Applicant's full name, mailing address, and telephone number(s).
2. The common and scientific names of the species to be covered by the permit and the species' status under CESA, including whether the species is the subject of rules and guidelines pursuant to Section 2112 and Section 2114 of the Fish and Game Code.
3. A complete description of the project or activity for which the permit is sought.
4. The location where the project or activity is to occur or to be conducted.
5. An analysis of whether and to what extent the project or activity for which the permit is sought could result in the taking of species to be covered by the permit.
6. An analysis of the impacts of the proposed taking on the species.
7. An analysis of whether issuance of the Incidental Take Permit would jeopardize the continued existence of a species. This analysis includes consideration of the species' capability to survive and reproduce, and any adverse impacts of the taking on those abilities in light of (a) known population trends; (b) known threats to the species; and (c) reasonably foreseeable impacts on the species from other related projects and activities.
8. Proposed measures to minimize and fully mitigate the impacts of the proposed taking.
9. A proposed plan to monitor compliance with the minimization and mitigation measures and the effectiveness of the measures.
10. A description of the funding source and the level of funding available for implementation of the minimization and mitigation measures.
11. Certification of accuracy.

California Environmental Quality Act (CEQA)

CEQA requires environmental impact assessment and mitigation for non-exempt projects occurring within the State of California. As unique ecosystems associated with endangered and threatened species, vernal pools are considered rare biological resources in CEQA review. CEQA applies to projects proposed to be undertaken or requiring approval by State and local government agencies. The lead agency is responsible for completing an environmental review process defined by CEQA. The review process includes

1. Determining if the activity is a project subject to CEQA,
2. Determining if the project is exempt from CEQA, and
3. Performing an Initial Study to identify the environmental impacts of the project and determine whether the identified impacts are "significant." Based on the findings of significance, one of the following documents must be prepared:

    - Negative Declaration if the review finds no "significant" impacts;
    - Mitigated Negative Declaration if the review finds "significant" impacts but the project can be altered to avoid or mitigate those significant impacts;
    - Environmental Impact Report (EIR) if the review finds "significant" impacts.

Some projects may be determined to be exempt from CEQA by law because the project may fall under a category of projects that have already been determined to generally not have significant environmental impacts. Examples include resource and environmental protection actions by regulatory agencies, wildlife habitat acquisition, habitat restoration on five acres of less, maintenance activities, or emergencies. Retrofits to existing structures may be considered an exception. Articles 18 (http://ceres.ca.gov/ceqa/guidelines/art18.html) and Article 19 (http://ceres.ca.gov/ceqa/guidelines/art19.html) of the Act contain details on exemptions and exceptions to CEQA.

This project may require consideration of cultural resources as part of CEQA documentation. The purpose of a cultural resources study is to identify significant impacts and potentially significant impacts of a proposed project to cultural resources, and to provide mitigation measures to reduce impacts to a level less than significant.

401 Certification

Under CWA Section 401, every applicant for a federal permit or license for any activity which may result in a discharge to a water body must obtain State Water Quality Certification (401 Certification) to ensure the proposed activity will comply with state water quality standards. In general, a 401 Certification is required for all projects in which a US ACE CWA Section 404 Permit (described above) is obtained or that will discharge dredged or fill material to waters of the U.S., including removing vegetation or channel materials for flood control, constructing levees, and filling wetlands. If the Regional Water Quality Control Board (RWQCB) deems a project exempt from the provisions of Section 401, it may regulate the dredge and fill activity under State authority in the form of Waste Discharge Requirements or Certification of Waste Discharge Requirements.

To initiate the 401 Certification process, a Biological Assessment is typically performed in which any potential impact to waters of the U.S., adjacent wetlands, and receiving waters is determined. Coordination between the City and the RWQCB is recommended before the application is submitted. A *Section 401 Water Quality Certification Application Form* should then be prepared and submitted to the RWQCB. On average, the 401 Certification application process takes three to four months to complete from the time of application to the time of approval.

C. Local Regulations and Permits

Post-Construction Stormwater Management

For typical development projects, the City requires project proponents to use a checklist to determine whether standard stormwater requirements (low impact development and source controls) or priority stormwater requirements (for development that meets certain size or land use thresholds or that might impact sensitive areas) are applicable. The Stormwater Standards Manual describes the steps that then need to be taken (i.e., Best Management Practices, or BMPs) to meet the applicable requirements. These stormwater requirements are not likely to apply to a drainage project.

Project proponents are required to submit Urban Stormwater Mitigation Plans consistent with the region's Standard Urban Stormwater Mitigation Plan (http://www.sdcounty.ca.gov/dpw/watersheds/susmp/susmp.html) to meet the following objectives:

- Reduce Priority Development Project discharges of pollutants from the MS4 to the maximum extent practicable
- Prevent Priority Development Project runoff discharges from the MS4 from causing or contributing to a violation of water quality standards
- Manage increases in runoff discharge rates and durations from Priority Development Projects that are likely to cause increased erosion of stream beds and banks, silt pollutant generation, or other impacts to beneficial uses and stream habitat due to increased erosive force.

Some areas within Otay Mesa could be considered a Priority Development Project Areas if they were to discharge runoff from any development or redevelopment directly into or directly adjacent to receiving waters within an Environmentally Sensitive Area (ESA; includes vernal pools). Other conditions that would trigger the application of a priority development project area include either the creation of 2,500 square feet of impervious surface on a proposed project site or an increase in the area of imperviousness of a proposed project site to 10 percent or more of its naturally occurring condition (San Diego Regional Water Board Order R9-2007-0001 (Section D.1.d.(2)(g)). Within these definitions, "directly adjacent" is defined as project sites situated within 200 feet of the ESA. "Discharging directly to" is defined as outflow from a drainage conveyance system that is composed entirely of flows from the subject development or redevelopment site, and not commingled with flows from adjacent lands.

Provision D.1.g of San Diego Regional Water Board Order R9-2007-0001 requires the San Diego Stormwater Copermittees to implement a Hydromodification Management Plan (HMP) "…to manage increases in runoff discharge rates and durations from all Priority Development Projects, where such increased rates and durations are likely to cause increased erosion of channel beds and banks, sediment pollutant generation, or other impacts to beneficial uses and stream habitat due to

increased erosive force." To comply with this requirement, the San Diego Copermittees developed an HMP (http://www.projectcleanwater.org/pdf/susmp/hmp_final_12-29-09_clean.pdf, December 29, 2009), which is subject to Regional Water Quality Control Board approval. The HMP specifies that Priority Development Projects are required to implement hydromodification mitigation measures so that post-project runoff flow rates and durations do not exceed pre-project flow rates and durations where such increases would result in an increased potential for erosion or significant impacts to beneficial uses. Hydromodification mitigation can be provided as follows:

- Demonstrate no post-project increase in impervious area and resultant peak flow rates as compared to pre-project conditions
- Installation of LID BMPs, such as bioretention facilities, to control runoff flows and durations from new impervious areas
- Mitigation of flow and durations through implementation of extended detention flow duration control basins
- Preparation of continuous simulation hydrologic models and comparison of the pre-project and mitigated post-project runoff peaks and durations (with hydromodification flow controls) until compliance is achieved
- Implementation of in-stream rehabilitation controls to demonstrate that projected increases in runoff peaks and/or durations would not accelerate erosion to the rehabilitated receiving stream reach.

Chapter 6 of the HMP Guidance provides guidance on applicability, hydromodification mitigation criteria and implementation options, and a framework for in-stream rehabilitation options.

Construction Stormwater Management

In California, discharges from construction sites one acre or larger are regulated under the State-wide General Permit for Waste Discharge Requirements for Discharges of Storm Water Associated with Construction Activity (NPDES General Permit CAS000002) Water Quality Order 98-08-DWQ (General Permit). The General Permit requires a Storm Water Pollution Prevention Plan (SWPPP) that describes BMPs to prevent pollutant and sediment discharges from the construction site, as well as an inspection and monitoring program. A Notice of Intent (Attachment 2 of the General Permit) is to be submitted to the State Water Resources Control Board (SWRCB) along with a project site map and fee at least two weeks prior to construction initiation.

The SWPPP must remain onsite at all times and regular self-inspections must be performed to assess the effectiveness of the BMPs. Stormwater samples must be collected if there is reason to suspect that non-visible pollutants have come into contact with stormwater or the site discharges to a water body listed on the 2006 CWA Section 303(d) List of Water Quality Limited Segments Requiring TMDLs. If permit coverage is not terminated within a year, an annual report must be completed and submitted to the LARWQCB. To terminate permit coverage, a Notice of Termination is to be completed and submitted to the SWRCB. The Construction Storm Water General Permit is currently under revision and is available online at: http://www.waterboards.ca.gov/water_issues/programs/stormwater/constpermits.shtml.

Biological Resources

Multi-Species Conservation Program

The Multi-Species Conservation Program (MSCP) applies to the Otay Mesa area. The MSCP is designed to preserve native habitat for multiple species by identifying areas for directed development and areas to be conserved in perpetuity (referred to as Multi-Habitat Planning Area or MHPA) to achieve a workable balance between smart growth and species protection. The project area falls within portions of the City's MHPA and includes areas directly adjacent to the MHPA. These two categories have different requirements as follows:

- For **premises that are located within or adjacent the City's MHPA**, the project must demonstrate compliance with the MHPA land use adjacency guidelines (see the City's MSCP Subarea Plan, March 1997, http://www.sandiego.gov/planning/mscp/pdf/subarea.pdf) to address potential indirect effects to the MHPA through features incorporated into the project and/or permit conditions. The following issue areas are addressed:

    1. Drainage;
    2. Toxics;
    3. Lighting;
    4. Noise;
    5. Barriers;
    6. Invasive species;
    7. Brush management; and,
    8. Grading/land development.

- For **sites partially within the MHPA**, the allowable development area under the MSCP includes all the land outside the MHPA. If less than 25 percent is outside the MHPA, the project would be allowed the required area to achieve a 25 percent development area. In defining the 25 percent developable area, the least sensitive portion of the site must be used and would include avoidance/minimization of wetlands and MSCP narrow endemics.

The MHPA can be altered on a site to accommodate a project, subject to approval by the City and wildlife agencies in accordance with meeting the six MHPA boundary line adjustment functional criteria (see Section 5.4.2 of the Regional MSCP Plan, August 1998, http://www.co.san-diego.ca.us/dplu/mscp/docs/SCMSCP/FinalMSCPProgramPlan.pdf). These criteria include:

- Effects on significantly and sufficiently conserved habitats;
- Effects to covered species;
- Effects on habitat linkages and function of preserve areas;
- Effects on preserve configuration and management;
- Effects on ecotones of other conditions affecting species diversity; and
- Effects to species of concern not on the covered species list.

The analysis for any proposed MHPA adjustment should be included in the project biology report[1] (if required, see below), and include:

1. An exhibit clearly showing the proposed removal and addition areas with the proposed grading;
2. A table showing, by habitat type, area within the existing MHPA, area to be removed, area to be added, and the proposed net change to the preserve; and
3. A written analysis of how the proposed MHPA adjustment meets the six required functional equivalency criteria.

Environmentally Sensitive Lands (ESL) Regulations
The City oversees development that may impact listed species through the ESL Regulations (San Diego Municipal Code, Land Development Code, and Biology Guidelines, currently pending amendment). City public projects do not need a grading permit, however these projects will still be required to obtain all necessary City, State, and Federal permits prior to the preconstruction meeting or any clearing or grading of the project site.

Land Development Code Biology Guidelines (City of San Diego, 2001) lists *Eryngium aristulatum* var. *parishii* (Parish's eryngo, San Diego button celery), *Navarretia fossalis* (spreading navarretia, vernal pool pincushionplant), *Orcuttia californica* (California Orcutt grass), *Pogogyne abramsii* (San Diego mesa mint), and *P. nudiuscula* (Otay Mesa mint) as narrow endemic species. Narrow endemics are included in the definition of Environmentally Sensitive Lands, which requires a discretionary review of the project permit including biological surveys and species specific mitigation requirements. These species are associated with vernal pool habitats, which are found within the project area (see Section Vernal Pool Management Plan, below, for more information about vernal pool management).

A biological survey report is required for all proposed development projects that are subject to the ESL Regulations, and/or where CEQA review has determined that there may be a significant impact on other biological resources considered sensitive under CEQA. Table 6 summarizes survey requirements for various biological resources inside and outside the MHPA. Note that the proposed project site includes areas that are inside, adjacent to, and outside of the MHPA area.

The Biological Survey Report must identify all potential impacts from the development (both on-site impacts and off-site impacts such as roads, water and sewer lines) to sensitive biological resources and to other significant biological resources as determined by the CEQA process. The report should evaluate the significance of these impacts. Impact assessments need to include analysis of direct impacts (e.g. grading, Zone 1 brush management), indirect impacts (e.g. lighting, noise) and cumulative impacts. The City of San Diego (1994) Significance Determination Guidelines under the CEQA should be used as a reference.

The ESL regulations require that impacts to wetlands be avoided, and all unavoidable wetlands impacts (both temporary and permanent) will need to be analyzed and mitigated via wetland creation, restoration, enhancement, and/or acquisition. Acquisition and/or enhancement of existing wetlands

[1] Three full sets of the MHPA adjustment materials will be required for any proposed MHPA adjustment.

may be considered as partial mitigation only. The mitigation ratio for vernal pools ranges from 2:1 when no endangered species are present, up to 4:1 when endangered species with very limited distributions (e.g., *P. abramsii*) are present.

Table 6. Summary of biological survey requirements

Resource	Survey Requirements	
	Inside MHPA	Outside MHPA
Vegetation		
Uplands	Confirm/Revise MSCP mapping	Confirm/Revise MSCP mapping
Wetlands	Delineate wetlands per City definition	Delineate wetlands per City definition
Covered species[1]		
Listed species	Focused survey per protocol	Per MSCP conditions of coverage[2]
Narrow endemic	Focused survey per protocol	Focused survey per protocol
Other	Survey as necessary to comply with requirements as outlined in Section II.A.2 of Biology Guidelines	Per MSCP conditions of coverage[2]
Non-covered species		
Listed species	Focused survey per protocol	Focused survey per protocol
"Other sensitive species" [3]	Case-by-case determination depending on the species	Case-by-case determination depending on the species

1. Based upon the MSCP mapping, site specific surveys, the NDDB records, previous EIRs and biological surveys and/or discussion with the Wildlife Agencies, the potential for listed species, narrow endemic and CEQA sensitive species will be determined. Where there is a reasonable likelihood that one of these species exists, surveys will follow the above requirements.
2. Survey as necessary to conform with to Appendix A of the City of San Diego MSCP Subarea Plan (March 1997).
3. "Other Sensitive Species". Those other species that are not listed by federal and/or state agencies and/or not covered by the MSCP and to which any impacts may be considered significant under CEQA.

Vernal Pool Management Plan

To protect vernal pools, site-specific management recommendations were developed for ten Otay Mesa locations (http://www.sandiego.gov/planning/mscp/vpmp/index.shtml), two of which occur in the project area: "J28 East" and "J21." J 28 East is a 20-acre site located southwest of the intersection of La Media Road and Avenida de la Fuente with five mapped vernal pools that are located within the MHPA. J21 is a 49-acre site located southwest of Siempre Viva Road and La Media Road with seven vernal pools that are located outside of the MHPA. Both sites' vernal pools were identified by the adopted Recovery Plan for Vernal Pools of Southern California (USFWS, 1998) as necessary to stabilize populations of the following endangered and threatened species: *E. aristulatum*, *P. nudiuscula*, *N. fossalis*, *O. californica*, *B. sandiegonensis* and *S. woottoni*.

Both sites are subject to the same threats: development (both sites are privately owned and not conserved); invasive species (particularly grasses); trespass from foot traffic and off-road vehicles; litter, wind-blown debris, and illegal dumping; and fire and fire suppression activities. Both sites are recommended for conservation through public acquisition or private mitigation, and restoration or

enhancement of the vernal pools is appropriate given the high species diversity recorded historically at those sites. Restoration at J28 East should focus on creating stable populations of the aforementioned species, particularly on *E. aristulatum*, *M. minimus*, and *P. nudiuscula*, and restoration at J21 should focus particularly on *E. aristulatum*, *N. fossalis*, *O. californica*, and *P. nudiuscula*.

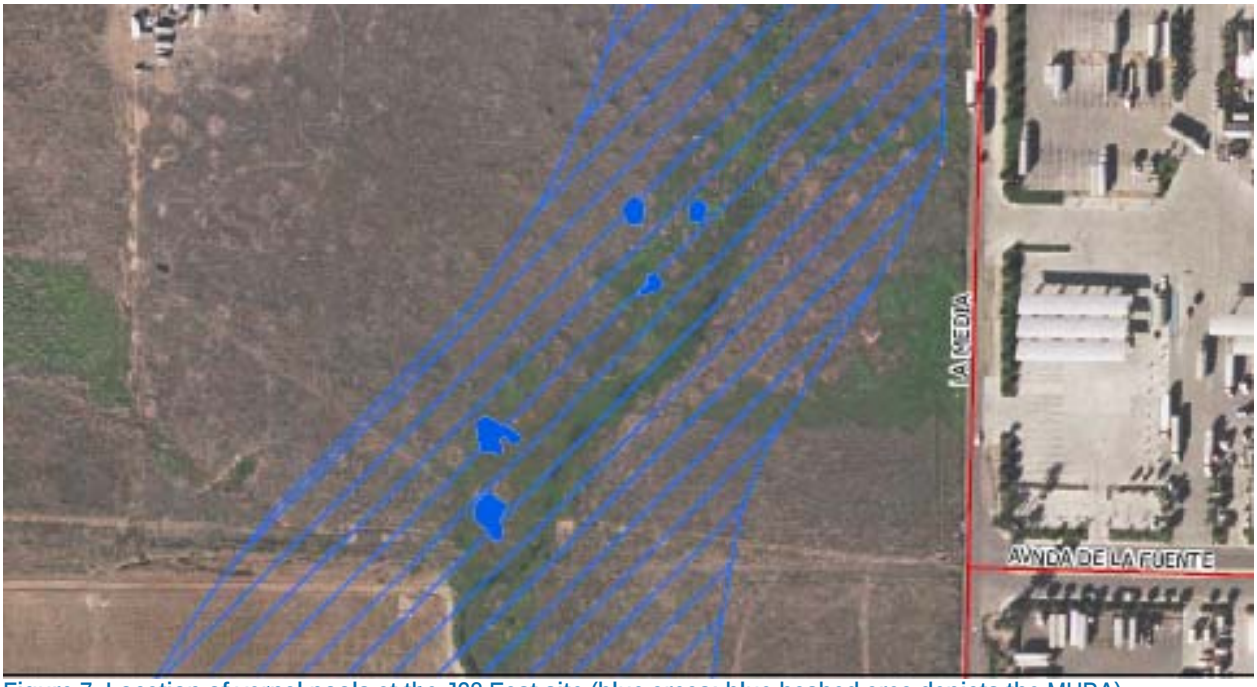

Figure 7. Location of vernal pools at the J28 East site (blue areas; blue hashed area depicts the MHPA).

Figure 8. Location of vernal pools at the J21 site (blue areas; blue hashed area depicts the MHPA).

Geologic Hazards

Unstable slopes, slide-prone geologic formations, faults and liquefaction-prone soils occur in many parts of the City. The relative risk of these geologic hazards has been mapped as part of the City of San Diego Seismic Safety Study (SSS) (City of San Diego Development Services, 2009). The maps indicate where potentially adverse geological conditions may exist, as defined by Geologic Hazard Category (http://www.sandiego.gov/development-services/hazards/hazardsmaps.shtml).

Evaluation of the SSS maps for the project area show the presence of Geologic Hazard Category 53, defined as level or sloping terrain with unfavorable geologic structure, which presents a low to moderate geologic risk.

The proposed project can be categorized as a minor public structure, which can be considered Building Type/Land Use Category IV, defined as "residential (single-family residences, apartments, etc.) and most commercial and *minor public structures*" (emphasis added). Group III, the next more stringent group, specifies places normally attracting large concentrations of people, and this project should not fall into that category.

Based on the presence of Geologic Hazard Category 53 and a Category IV project, a soil investigation and geologic investigation are anticipated. The City of San Diego (2008) *Guidelines for Geotechnical Reports* (http://www.sandiego.gov/development-services/industry/pdf/geoguidelines.pdf) describes these investigations in greater detail.

Grading

Not applicable; public works projects do not require a grading permit.

D. County Regulations and Permits

Because the areas in question are located within the City limits, county permits are not anticipated to be needed unless drainage or other infrastructure will connect to or otherwise affect county-owned infrastructure.

E. International Regulations and Permits

The International Boundary and Water Commission (IBWC) issues licenses and permits for activities in the IBWC right-of-way at the border or on IBWC maintained floodways. The *Criteria for Construction Activities within the Limits of USIBWAC Floodways* specifies that a license or permit is required for any proposed activities crossing or encroaching upon the floodplains of the IBWC flood control projects and right-of-way. This project does not affect the floodplains or right-of-way of any IBWC flood control project. Water quality considerations under IBWC jurisdiction focus on Texas rivers only and do not apply to the Otay Mesa area.

VI. Drainage Requirements, Considerations, and Opportunities

This report provides information primarily on the East and West Water Tanks drainage areas as these are the areas covered by the engineering reports. The West Watershed consists of smaller mesa-top watersheds that drain into the tributary canyons of Spring Canyon, which then flow into Mexico via the

Spring Canyon concentration point. While there is a need for some runoff management in these areas to reduce post-development peak flows to predevelopment levels, this area is of fairly low priority.

The engineering reports completed in the Otay Mesa area and summarized above focus primarily on the industrialized areas of the East Water Tanks drainage areas. This East Watershed is the largest watershed on the Mesa. All flows from the watershed collect at a concentration point at a large culvert where flows cross the U.S./Mexico border. The surrounding area is fairly flat and adjacent properties have difficulty draining effectively into the existing creek during larger storm events. The existing drainage is a combination of storm drains, improved channels, and detention basins, which discharge in many areas to natural drainage paths that do not have adequate hydraulic capacity. As projects have been developed in this area, portions of the private properties have been dedicated to the city as drainage easements or flood water storage easements (not verified as a part of this report).

Collectively, the engineering reports have recommended in one way or another that for this area to accommodate future development, the construction of a drainage channel along the east side of La Media crossing from the northeast corner to the northwest corner of the intersection of La Media with Siempre Viva Road would be required. The proposed channel would continue along the north side of Siempre Viva at La Media to the current culvert crossing along Siempre Viva to connect to the existing stream channel. This plan was selected because an existing drainage ditch located on the east side of La Media Road could be expanded to intercept flows from the east without creating potential conflicts from utilities in La Media Road; and flows from the west would continue to flow in the old drainage path. Additionally, this plan may reduce impacts to properties by following the property boundaries and could minimize potential utilities conflicts along Siempre Viva Road.

In this area, drainage alternatives should be given substantial thought by the City of San Diego. The next section presents several considerations that highlight key practical issues that might impinge on future drainage and development decisions.

A. Consideration 1: Drainage and Runoff Management Responsibilities

One of the first considerations is who has the responsibility to provide drainage the East Water tanks Drainage Area. The City of San Diego is responsible for public land including runoff from public roads and right of ways. However, as has been pointed out several times in this document, private property owners or developers are required to provide adequate storage and conveyance for 50-year flows in areas in the watershed that are above major (four lane) road crossings (City of San Diego Development Services, 2004). This is typical for most developments in the East Water Tanks drainage area. However, below major roadways, the drainage infrastructure must be designed to accommodate 100-year flows. The 100-year floodplain is also significant in that it is a standard used by the National Flood Insurance Program (NFIP) for floodplain management and to determine the need for flood insurance.

Figure 9 shows 100-year floodplain in the Water Tanks (East) drainage area (Kimley-Horn and Associate, 2007).

The interpretation of drainage language is that all public or private properties are required to provide adequate storage and conveyance for up to the 50-year flows, except for those in the natural drainage channel which are exempt. “Major roadways”, that is, those that are four lane or greater and major roadway crossings would require designs that consider conveyance of the 100-year storm either beneath,

along and/or on the roadway as long as not more than one lane of the four is used for conveyance and the conveyance does not encroach onto private property outside of the road right-of-way. None of the areas shown in Figure 9 are considered to be below major roadways.

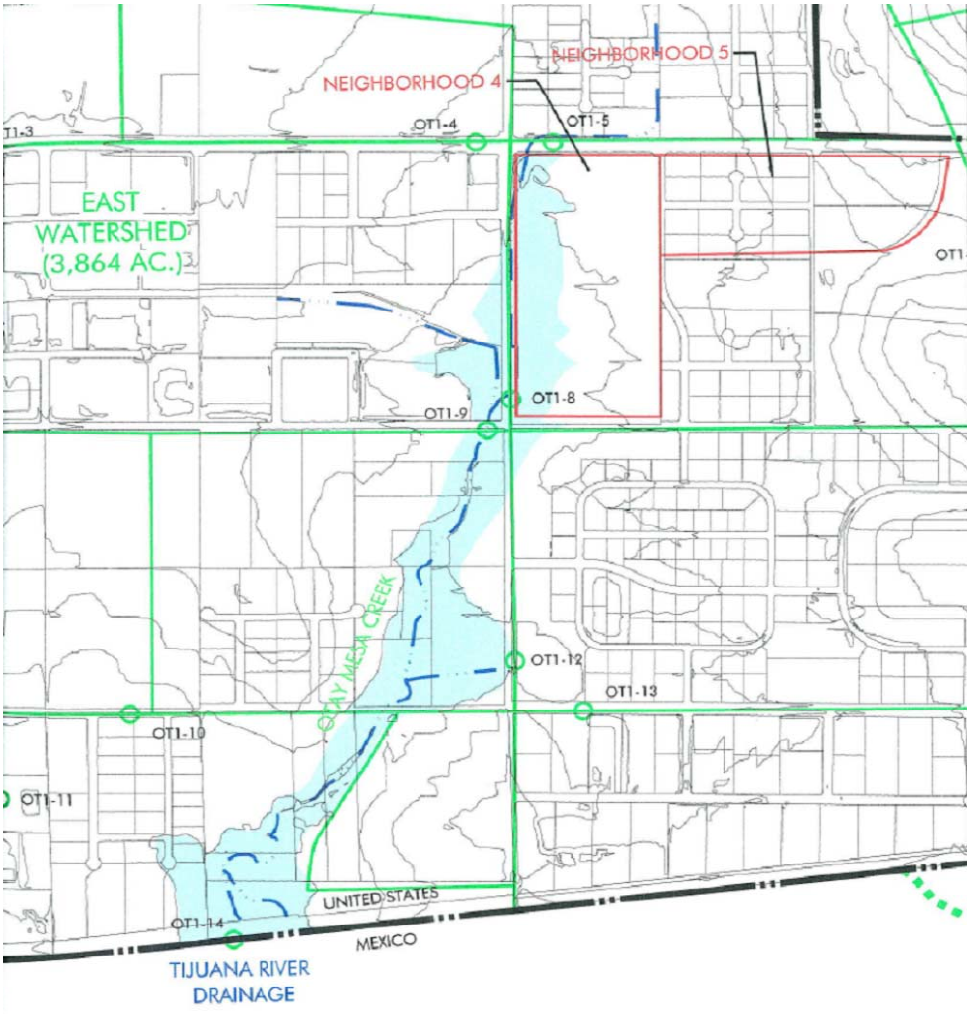

Figure 9. 100-year Floodplain in the Water Tanks (East) drainage area (Kimley-Horn and Associate, 2007).

B. Consideration 2: Potential for BMPs

The potential for stormwater BMPs is another consideration in the decision making process. If, in the future, conveyance along with water quality systems like BMPs are required in the Water Tanks East Drainage, current policies state that all BMPs be constructed for Priority Project Permanent Storm Water BMPs and High Priority Construction Storm Water BMPs. Most projects in the East Water Tanks watershed then would require the submission of a "Water Quality Technical Report" which follows the guidance "Storm Water Standards – A Manual for Construction & Permanent Storm Water Best Management Practices Requirements."

Several factors must be considered when including BMPs in this area. The suitability and types of BMPs that may be selected are highly dependent on the existing conditions, including slope, soils, adequate area, and other natural resource considerations such as destruction of natural vernal pools. However,

this may potentially be an opportunity as well. As has previously been noted, this area is endemic to vernal pools. Projects within this area may provide a very good opportunity to include vernal pool restoration or creation and habitat improvements to support this unique ecosystem natural to Otay Mesa.

Potential Areas for Vernal Pools

Potential areas for restoring and/or improving vernal pools were identified using soil suitability, land use, and site availability. Bauder and McMillan (1998) describe suitable areas for vernal pools with slopes 9% or less and a substance layer with permeability of 0.06 inches/hour or less. Suitable areas using the criteria are shown in Figure 10.

The downstream areas of the Water Tanks (East) drainage area are mainly covered by two types of soils as shown in Figure 5. Major characteristics of the soils are summarized below (Bauder and McMillan 1998).

Huerhuero loam:

- Slopes: 2 to 9 percent
- Impervious sub-surface layer: 12 to 55 inches of clay and clay loam
- Permeability of sub-surface layer: <0.06 inches/hour
- pH: 5.3- for surface and 8.2 for sub-surface

Sckpen (Stockpen) gravelly clay loam:

- Slopes: 0 to 2 percent
- Impervious sub-surface layer: 21 to 60 inches of gravelly clay or clay
- Permeability of sub-surface layer: <0.06 inches/hour
- pH: 6.5 for surface and 8.0 for sub-surface

The characteristics of these soils make them ideal for creating vernal pools.

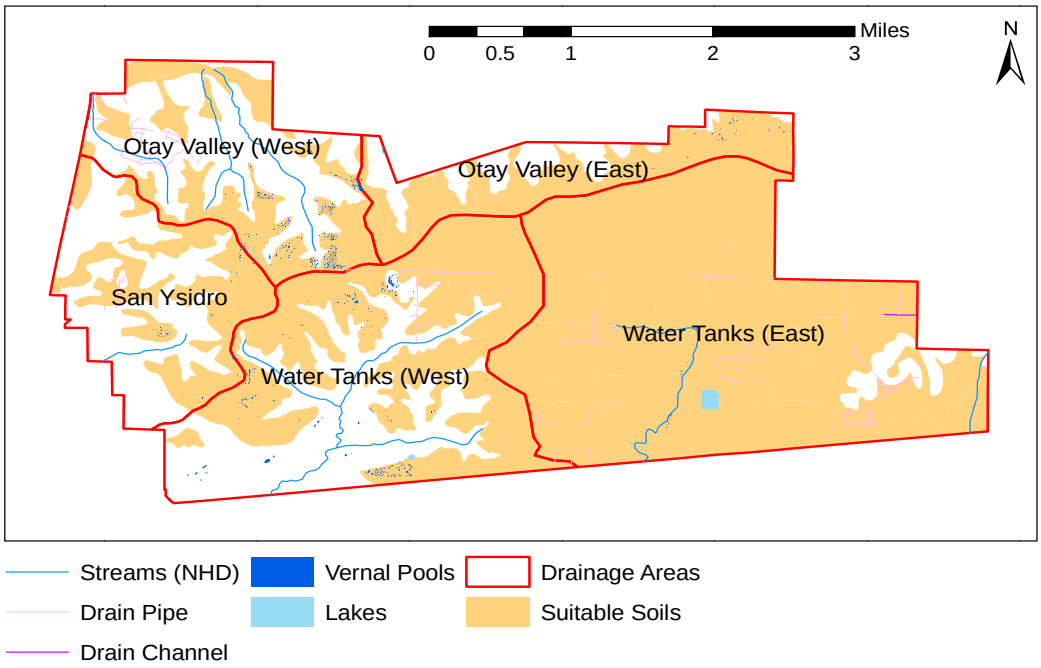

Figure 10. Suitable Areas for Vernal Pools with 9% or less Slope and 0.06 inches/hour or less Permeability

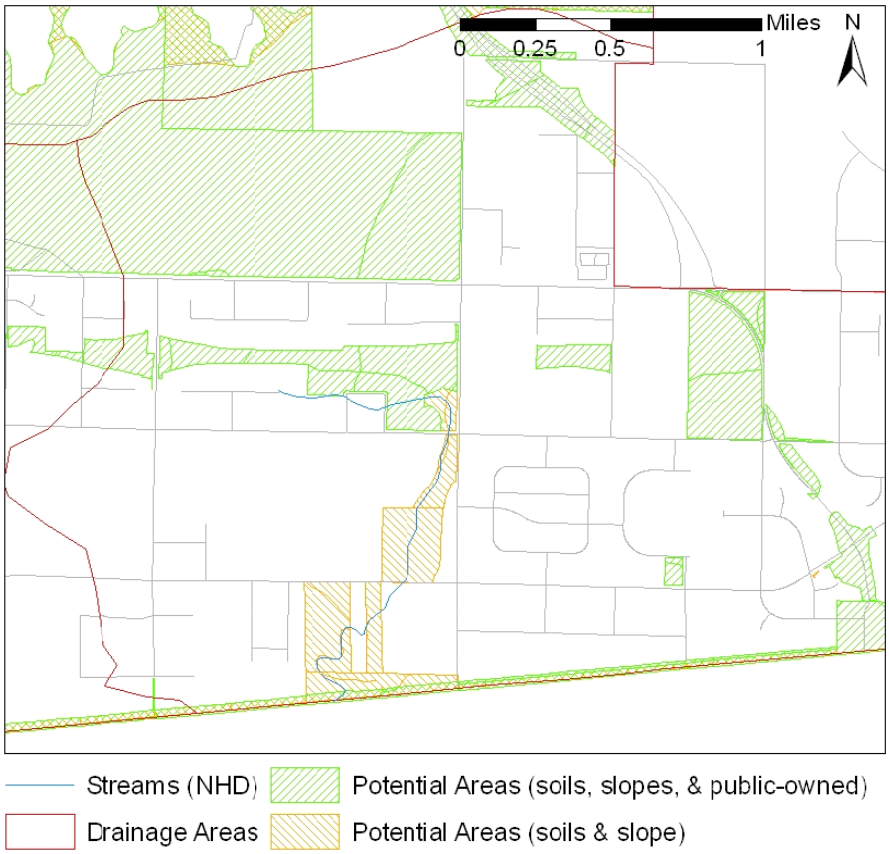

Figure 11. Potential Areas for Vernal Pools within the Water Tanks (East) drainage area

There are a number of parcels that could serve as potential areas for vernal pool creation as supplemental stormwater BMPs beyond the canal and detention system highlighted in the engineering reports.

C. Consideration 3: Estimated Annualized Costs for Planning, Permitting, Land Acquisition, Design, Construction, and Maintenance of Stormwater and Drainage Infrastructure

Another consideration is the cost of future maintenance of stormwater and drainage facilities if these were to be put in place.

Planning

Costs for planning include the effort required to further develop the project concept which, depending on the complexity of the project, could result in preparing a Project Concept Report. Additional administrative costs could be required to administer, manage and coordinate the project's implementation and are included with the planning costs. Administrative costs can vary widely with the complexity of the project, but for purposes of comparison, a value of 5 percent of the capital costs is assumed for planning.

Permitting

Regulatory requirements have to be met and environmental permits are required to implement most BMPs. The applicability of many regulations for a specific project depends on its site or design characteristics. Because the requirements imposed by regulatory agencies often have an effect on the project cost, the associated costs were included in the analysis for centralized BMPs: Because the opportunities identified for distributed structural BMPs are for areas of impervious cover and not applied to vacant or open spaces, the permitting effort anticipated for such projects is minimal, if any. Therefore, no separate costs are identified in the analysis for permitting. It is assumed that any permitting costs associated with the construction phase, such as erosion and sedimentation control, are included in the construction costs.

Land Acquisition

Cost estimates for any acquisition of private lands in Otay Mesa would be generated at the time when the City has determined to move forward with a public drainage facility. The cost estimates would be based on market value at that time, and would include BMP's as necessary.

Design

Designing structural BMPs requires collecting data, analyzing it, and preparing documents that can be used for constructing a project. Data collection could include geotechnical investigations, field investigation of existing utilities (potholing), and a topographic survey for mapping. The design deliverables are project plans and specifications that can be bid by a contractor for construction. Engineering costs can vary widely depending on the complexity of the project. For the purposes of the cost estimates, fixed rates of 5 and 10 percent were applied to the distributed and centralized BMP construction costs, respectively, to estimate the design/engineering cost. A lower percent was used for distributed BMP design costs because these BMPs are expected to have less time-intensive designs compared to centralized BMPs.

Construction

The typical levels of construction cost estimates are:

- Preliminary/Order of Magnitude—provide a range of costs at the planning level for a conceptually defined project
- Budget—cost estimates based on layouts and specific quantities
- Final/Definitive—prepared after the design documents are complete

The estimates for centralized BMPs on public and private property are not site-specific and are in the preliminary/order of magnitude category. To the extent possible, construction costs are based on approximate quantifications of the major components of the BMP.

Mobilization: Mobilization costs are highly variable depending on the magnitude of the project. A mobilization factor of 5% was included.

Excavation and removal: Excavation and removal costs include the cost of excavating the volume of soil required to provide the required storage, hauling the removed dirt offsite, and disposal to an appropriate facility.

Reinforced Concrete Pipe: Costs were derived from R.S. Means (2007) and are included to estimate the costs for constructing a storm drain extension of or to bypass an existing storm drain system.
Landscaping: One of the benefits of distributed BMPs is that they can be integrated into the site plan and often incorporated into the landscaping. Landscaping costs were estimated based on regional data.

Native Landscaping: Native landscaping should be used for any BMP because native landscaping is more adapted to the natural conditions which increase plant survivability.

Contingency: Because some of the project components have not been fully defined at this preliminary stage, a contingency factor of 25 percent should be applied to the construction costs to estimate the total construction costs and capture expected but as yet unidentified additional costs. The costs could arise from site-specific field conditions such as those associated with utility relocations, dewatering, and erosion and sedimentation control. At this stage of project development, the contingency also includes an allowance for such items as field facilities and construction scheduling, which might be required but are not specifically itemized. The contingency factor has **not** been applied to any of the cost functions or component cost estimates itemized in Table 7.

Table 7: Per Unit Cost Estimates for Construction Components

Construction Component	Cost
Mobilization	5% of construction total
Excavation and Removal	$25.00/yd^3
Asphalt/Base Removal	$8.00/yd^3
Site Preparation	$20.00/ft^2
Reinforced Concrete Pipe	$8.00 per diameter (inch) per length (ft)
Landscaping (includes mulch/sod and vegetation)	$5.00/ft^2
Native Landscaping	$25.00/ft^2
Planning	5% of total

Construction Component	Cost
	construction costs
Permits/Studies	Included in design
Design (Centralized)	10% of total construction costs
Design (Distributed)	5% of total construction costs
Contingency for Planning Estimate (Centralized)	25% of total construction costs
Contingency for Planning Estimate (Distributed)	15% of total construction costs

This costing information can be used by the City of San Diego to evaluate costs of planning, permitting, operating and maintaining the proposed drainage facilities and BMPs.

D. Consideration 4: Risk-Based Analyses

On method of assessing the level of service to provide to some drainage areas is to evaluate the risk to private citizens and the economic losses due to flooding. Risk costs are those cost items incurred due to the unexpected failure in the drainage system due to flooding and can broadly be categorized as tangible and intangible costs. Tangible costs are those measured as direct monetary losses including damage to properties and structures, loss of business, cost of repair, etc. Intangible costs include psychological trauma, damage to the environment, and other costs that do not have a direct, agreed upon, or known value.

Economic risks and flood loss costs were considered began to take hold in the early 1960's. One of the early applications was risk based concept to hydraulic design of highway culverts. Pritchett used four actual locations, calculating the investment costs with the expected flood damage costs on an annual basis for several design alternatives. The results indicated that a more economical solution would be reached by selecting smaller culvert sizes compared to the traditional return method typically used.

The basic concept of risk based design is shown schematically in Figure 13. The risk function can account for the potential undesirable consequence associated with the failure of hydraulic structures on the damage and costs related to flooding costs. However, it must be recognized that the risk costs associated with the failure of hydraulic structures cannot be precisely predicted from year to year

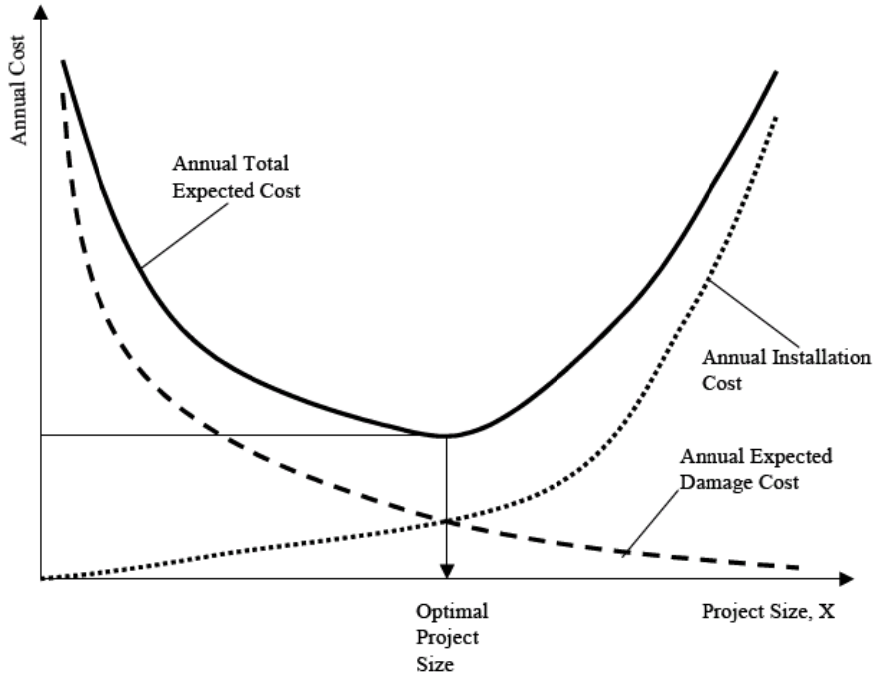

Figure 12. Risk-Based Design Costs Analyses Concepts

The Annual Total Expected Cost is the sum of the annual expected installation and maintenance costs and the annual expected damage and flooding costs. The sum of cost that makes up the intersection between the individual cost curves is the estimated optimal project size. Using this risk-based approach projects can more efficiently determine the estimated costs to inform project design.

For Otay Mesa, the engineering reports summarized potential drainage designs but do not consider the design based on a risk-based approach. These reports use the 100-year return interval for their recommended designs. It should be noted that the land uses where the drainage upgrades are suggested are primarily industrial in nature. This may impact tangible economic costs (e.g., transportation/delivery, vehicle and employee access, etc.), but other intangible costs such as loss of life and threat to personal safety are likely to be minimal because of very little if any residential land uses in this area.

A risk-based approach may be well suited for decision making in the Otay Mesa area. To adequately determine the size of a project to be designed, the annual total expected costs should be evaluated to assist in determining the optimal project size most appropriate for the drainage area. While risk based analyses is not as commonly used by engineers and planners, it is recommended that this task include economists from the City to consider risk-based costs when evaluating engineering designs such as those planned for the Otay Mesa drainage areas.

E. Consideration 5: Border Issues

There are some transboundary considerations beyond what was covered in the regulatory section of this report. The International Boundary and Water Commission (IBWC) is the lead agency for transboundary water management and settlement of bilateral disputes relating to managing shared water resources. An

international pollution abatement board makes recommendations to the EPA administrator for the abatement of international water pollution.

In August 1983, the U.S.-Mexico Border Environment Cooperation Agreement, better known as the La Paz Agreement, initiated a new era of formal multinational consultation and heightened attention to environmental issues within the border region. The La Paz process was strengthened by the 1992-1994 Integrated Border Environmental Program, the 1995-2000 Border XXI Program, and most recently by EPA's Border 2012 Program. These programs broadened the scope of border water management to include pollution prevention, water quality management, a concern for ecological processes, and a concern for advancing sustainable development of water resources along the border. Although these programs acknowledge IBWC's historic treaty role in binational water planning, they favor more regionalized and local workgroups and task forces to de-centralize decision making and to mobilize local resources for local solutions to water issues.

Even with these layers of bureaucracy, it is understood that Governments may be liable when mismanagement of reservoirs or other storage systems result in major flooding of downstream areas. For example, The U.S. Court of Claims [Gasser v United States, 14 Cl. Ct 476 (1988)] has held that the U.S. may be liable for flood damages in Mexico caused by operation of an upstream government reservoir. However, catastrophic natural events do not seem to apply to flood control requirements. Similarly, there is no standard set for the control of flows from the U.S. into Mexico, especially for intermittent or ephemeral streams such as the drainage of the Water Tanks (East) catchment. If a canal and detention system were built in this area, consideration of this area as a "hydrocommons", hydraulically linked basins connected through man-made engineered systems, may be necessary (Michel, 2000). The changing of current drainage patterns and timing of flow across the border in the Water Tanks (East) watershed of Otay Mesa could significantly alter downstream (Mexico) hydrologic functions such as water quality, aquatic habitat, riparian ecosystems, and land use. These issues are weakly addresses with federal, state, and international laws with the implications of constructing the proposed drainage and flood control systems unclear. Further investigation into the legal responsibilities and ramifications should be further reviewed if the drainage and detention projects proceed.

VII. Conclusions

This report has provided a review of previously developed engineering drainage reports with the report recommendations summarized. An inventory of current land use and drainage patterns, as well as regulations regarding storm water were provided as background to support up-to-date considerations for the placement of stormwater management facilities including the possibility of vernal pool restoration. This type of restoration may be required to mitigate impacts to sensitive areas (e.g.,vernal pools) associated with the implementation of the previously recommended drainage reports. The five considerations that were forwarded in this report are:

- Drainage and Runoff Management Responsibilities
- Potential for BMPs
- Estimated Annualized Costs for Planning, Permitting, Land Acquisition, Design, Construction, and Maintenance of Stormwater and Drainage Infrastructure
- Risk-Based Analyses
- Border issues

Through the consideration of these issues, the many regulatory layers, background on environmental sensitive areas of Otay Mesa, data compilation and description, and the summary and evaluation of the engineering reports the City of San Diego will have the necessary information for decision analysis for the Otay Mesa drainage area.

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APPENDIX G-3

Water Quality Technical Report

Water Quality Technical Report

Otay Mesa Community Plan Update

January, 2007

Prepared for:
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and Associates, Inc.

WATER QUALITY TECHNICAL REPORT

Otay Mesa Community Plan

January, 2007

Prepared for:
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427 C Street, Suite 308
San Diego, CA 92101

TABLE OF CONTENTS

Introduction 1
Pollutants That May Effect Storm Water Quality 1
Proposed Control Measures 2
Operation and Maintenance Procedures 5
Operation and Maintenance Responsibility 5
Installation Costs 6
Conclusion 7

APPENDICES

Appendix A Otay Mesa Community Plan Watershed and BMP Exhibit
Appendix B Treatment BMP Specifications
Appendix C Otay Mesa Drainage Study (without attachments)
Appendix D References

1. Introduction

The Otay Mesa Community is quickly developing in the City of San Diego. This area consists of approximately 7,000 acres bounded by the City of Chula Vista and the Otay River Valley on the north, the International Border on the south, Interstate 805 on the west, and the County of San Diego on the east. The far northwest arm of the Mesa is fully developed and all other areas are envisioned for residential, industrial, and commercial development in the Otay Mesa Community Plan.

The Mesa consists of flat terrain and shallow swales for drainage paths. Most of the Mesa slopes north to south resulting in runoff entering Mexico at several points. Increased development has caused concentrated flows in culverts under roads, redefined some of the historical drainage paths, and increased runoff into Mexico. For the most part, the existing drainage facilities have been constructed by private development causing non-continuous facilities and difficulty for subsequent developers to tie into the existing facilities. The Otay Mesa Creek is the only significant creek on the Mesa which lies in the East Watershed (see **Appendix A** for watersheds). The Drainage Study prepared for the Otay Mesa Community Plan Update proposes improvements to the Otay Mesa Creek with the La Media Channel and Border Detention Basin in the East Watershed to be constructed to convey flow and prevent downstream flooding. From the hydraulic analysis in the Drainage Study, Otay Mesa Creek crosses the border into Mexico just north of the Tijuana Airport and eventually to the Tijuana River. The West Perimeter Watershed and West Watershed also flow into the Tijuana River. The Tijuana River Watershed is a water quality impacted watershed; therefore, the water quality must be addressed for additional development. The Tijuana River is included in the 2002 Clean Water Act Section 303(d) List of Water Quality Limited Segments approved by the U.S. Environmental Protection Agency (EPA) and by the State Water Resources Control Board (SWRCB) on February 4, 2003.

The proposed detention basins in the West Perimeter Watershed and West Watershed will be constructed as part of development in the immediate vicinity of future projects. These detention basins are recommended to also function as treatment BMPs for runoff caused by new development. The La Media Channel and Border Detention Basin will be constructed before new development along the creek takes place (see **Appendix A** for locations). These BMPs target sediment, nutrients, trash, metals, oil & grease, and organics from existing and future development prior to crossing the border and into the Tijuana River.

This document complies with the City of San Diego's Standard Urban Storm Water Mitigation Plan and Storm Water Standards Manual.

2. Pollutants that May Affect Storm Water Quality

Future use of the undeveloped land may consist of residential, industrial, and commercial projects. From Table 2 of the City of San Diego's Storm Water Standards Manual, the anticipated and potential pollutants can be identified based on project category. For a residential development, the anticipated pollutants of concern are sediments, nutrients, trash and debris, and pesticides. The potential pollutants of concern include oxygen demanding substances, oil & grease, and bacteria & viruses. The anticipated pollutants for commercial developments include trash & debris and oil & grease. Potential pollutants are sediments, nutrients, organic compounds, oxygen demanding substances, bacteria &

viruses, and pesticides.

The Tijuana River is listed on the 303(d) list for impaired water bodies for bacteria, nutrients, oxygen demanding substances, low dissolved oxygen, pesticides, synthetic organics, and trash. This project proposes the La Media Channel and Border Detention Basin to improve existing drainage. Since residential, industrial, and commercial developments are planned uses of the site, this water quality technical report will not address additional pollutants (associated with the planned uses). Permanent storm water BMPs must be incorporated into future project where necessary to mitigate the impacts of urban runoff as a result of the development. For this project, the proposed channel and detention basin will contribute to filtering of pollutants prior to crossing the border. Heavy riparian vegetation will be allowed to grow in the channel, which traps pollutants. The channel slowly conveys runoff into a detention basin where runoff will be held for some minimum time allowing pollutants to settle prior to discharge.

3. Proposed Control Measures

The Water Quality Technical Report or the Storm Water Management Plan for future projects in the Otay Mesa Community rely on implementation of site design BMPs, source control BMPs, and treatment control BMPs. This project, Otay Mesa Community Plan Update, will only implement treatment control BMPs for the region. Future developers must address site design BMPs, source control BMPs, and additional treatment control BMPs based on anticipated and potential pollutants for the corresponding planned use. The main objective is to ensure that pollutants do not come in contact with storm water by reducing or eliminating the pollutants. These objectives are achieved by implementing the required source, site, priority project and treatment BMPs set forth in the City of San Diego Storm Water Standards.

Site Design

The following Site design BMPs are identified for future development (City Storm Water Standards – Section III.2.A and Appendix C):

1. Minimize impervious footprint. (1) Increase building density (number of stories above or below ground); (2) construct walkways, trails, patios, overflow parking lots and alleys and other low-traffic area with permeable surfaces, such as pervious concrete, porous asphalt, unit pavers, and granular materials; (3) construct streets, sidewalks and parking lot aisles to the minimum widths necessary, provided that public safety and a walkable environment for pedestrians are not compromised; and (4) minimize the use of impervious surfaces, such as decorative concrete, in the landscape design.
2. Conserve natural areas and provide buffer zones between natural water bodies and the project footprint. (1) Concentrate or cluster development on the least environmentally sensitive portions of a site while leaving the remaining land in a natural, undisturbed condition; and (2) use natural drainage systems to the maximum extent practicable (natural drainages and vegetated swales are preferred over using lined channels or underground storm drains.
3. Minimize directly connect impervious areas. (1) Where landscaping is proposed, drain rooftops into adjacent landscaping prior to discharging to the storm water conveyance system; and (2) where landscaping is proposed, drain impervious parking lots, sidewalks, walkways, trails, and patios into adjacent landscaping.

4. Maximize canopy interception and water conservation. (1) Preserve existing native trees and shrubs; and (2) plant additional native or drought tolerant trees and large shrubs in place of non-drought tolerant exotics.
5. Convey runoff safely from the tops of slopes.
6. Vegetate slopes with native or drought tolerant vegetation
7. Stabilize permanent channel crossings.
8. Install energy dissipaters, such as riprap, at the outlets of new storm drains, culverts, conduits, or channels that enter unlined channels in accordance with applicable specifications to minimize erosion. Energy dissipaters shall be installed in such a way as to minimize impacts to receiving waters.

Source Control

The following source control BMPs are identified for future development (City Storm Water Standards – Section III.2.B and Appendix C):

1. Outdoor material storage areas will be designed to reduce pollution introduction. Any hazardous materials with the potential to contaminate urban runoff shall be: (1) placed in an enclosure such as, but not limited to, a cabinet, shed, or similar structure that prevents contact with rain, runoff or spillage to the storm water conveyance system; and (2) protected by secondary containment structures such as berms, dikes or curbs. The storage area shall be pave and sufficiently impervious to contain leaks and spills and have a roof or awning to minimize direct precipitation within the secondary containment area.
2. Trash storage areas shall be: (1) paved with an impervious surface, designed not to allow run-on from adjoining areas, and screened or walled to prevent off-site transport of trash; and, (2) contain attached lids on all trash containers that exclude rain; or (3) contain a roof or awning to minimize direct precipitation.
3. Integrated pest management principles shall be employed including planting pest-resistant or well-adapted varieties such as native plants and using pesticides as a last line of defense. These principles shall be extended through the distribution of IPM educational materials to future site tenants.
4. Efficient irrigation systems and landscape design should employ rain shutoff devices to prevent irrigation during and after precipitation, irrigation design according to specific water requirements, and flow reducers or shutoff valves triggered by a pressure drop to control water loss in the event of broken sprinkler heads or lines.
5. All inlets should contain prohibitive illegal dumping language.

Priority Project

The following Priority Project design BMPs are identified for applicable future developments (City Storm Water Standards – Section III.2.C):

1. The design of private roadways shall use at least one of the following: (1) rural swale system; (2) urban curb/swale system; or (3) dual drainage system.
2. Residential driveways shall have one of the following: (1) shared access; (2) flared entrance; (3) wheelstrips (paving under tires); (4) porous paving; or (5) designed to drain into landscaping prior to discharging to the storm water conveyance system. Uncovered temporary

or guest parking on private residential lots shall be: (1) paved with permeable surface; or (2) designed to drain into landscaping prior to discharging to the storm water conveyance system.

3. Loading/unloading dock areas shall include the following: (1) cover loading dock areas, or design drainage to preclude urban run-on and runoff; and (2) an acceptable method of containment and pollutant removal, such as a shut-ff valve and containment area.
4. Maintenance bays shall include at least one of the following: (1) repair/maintenance bays shall be indoors; or, (2) designed to preclude urban run-on and runoff. Maintenance bays shall include a repair/maintenance bay drainage system to capture all wash water, leaks, and spills.
5. Outdoor areas for vehicle & equipment washing shall be: (1) self-contained to preclude run-on and run-off, covered with a roof or overhang, and equipped with a clarifier or other pre-treatment facility; and (2) properly connected to a sanitary sewer.
6. Outdoor processing areas shall: (1) cover or enclose areas that would be the most significant source of pollutants; or, (2) slope the area toward a dead-end sump; or, (3) discharge to the sanitary sewer system. Grade or berm processing area to prevent run-on from surrounding areas.
7. Where landscaping is proposed in surface parking areas, incorporate landscape areas into the drainage system. Overflow parking may be constructed with permeable paving.
8. Non-Retail fueling areas should be designed with the following: (1) paved with Portland cement concrete or equivalent; (2) designed to extend 6.5 feet from the corner of each fuel dispenser, or the length at which the hose and nozzle assembly may be operated plus 1 foot, whichever is less; (3) sloped to prevent ponding; (4) separated from the rest of the site by a grade break; and (5) designed to drain to the project's treatment control BMP. Must have overhanging roof structure or canopy that is equal to or greater than the area within the fuel dispensing area's grade break and designed not to drain onto or across the fuel dispensing area.
9. Steep hillside areas shall be landscaped with deep-rooted, drought tolerant plant species.

Treatment Control

Treatment control BMPs are designed to filter or treat runoff prior to discharging into an on-site or off-site storm drain system. The largest watershed of the Mesa is the East Watershed encompassing approximately 4,000 acres. This watershed flows into Mexico at a single point between Britannia and La Media roads. The La Media Channel and Border Detention Basin will function as a treatment design BMP (See Exhibit A for locations). Runoff drains to the La Media Channel where runoff is slowly conveyed through heavy riparian vegetation. The channel slopes at 0.25% for approximately 3,500 feet and behaves similar to a vegetated swale. Runoff is then discharged into the Border Detention Basin where storm water flow is slowed in order for pollutants to settle. The basin is approximately 58 acres with a maximum water depth of 6ft. These BMPs were chosen on the basis of site design feasibility and the City Storm Water Standards- Section III.2.D. Additional site treatment control BMPs may be necessary and addressed for future developments.

4. Operation and Maintenance Procedures

Grass Lined Channel

1) Inspect swales at least twice annually for erosion, damage to vegetation, and sediment and debris. See BMP detail TC-30 in **Appendix B** for preferred schedule.
2) Regularly inspect swales for pools of standing water to prevent mosquito breeding.
3) Every few years maintenance of dead or fallen trees may be required.

Detention Basin

An effective maintenance program should include the following key components:

1. Weather-triggered inspections – Inspect after several storm events for bank stability and to determine if the desired residence time has been achieved.
2. Regular inspections – Inspect semi-annually and after significant storm events. Inspect for the issues as described in BMP detail TC-22 in **Appendix B**.
3. Sediment Removal – Remove accumulated sediment when accumulated sediment volume exceeds 10-20% of the basin volume or when accumulation reaches 6 inches or if re-suspension is observed. Significant sediment deposition is not expected after development on The Mesa is completed.
4. Water Removal – Basin will be designed with a "low-flow" outlet; however, if water remains remove standing water by cleaning drainage path within 72 hours after accumulation.
5. General Maintenance Activities – see BMP detail TC-22 in **Appendix B** for maintenance activities and suggested frequency.

5. Operation and Maintenance Responsibility

A Maintenance District will be created for maintaining the channel and regional detention basin. Project detention/water quality basins and BMPs will be maintained by the project owners.

6. Installation Costs

La Media Channel and Border Detention Basin

Preliminary Opinion of Probable Construction Cost
2/8/2005
Kimley-Horn and Associates
Construction Items

Item No.	Description	Quantity	Units	Unit Price	Cost
1	Excavation	822,500	CY	$2	$1,645,000
2	Airway Road culvert (6~5'wx5'h)	300	CY	$1,500	$450,000
3	La Media/Airway Road culvert (6~10'wx6'h)	1,500	CY	$1,500	$2,250,000
4	Siempre Viva Road culvert (8~10'wx8'h)	1,490	CY	$1,500	$2,235,000
5	Detention Basin Outlet Structure	1	LS	$100,000	$100,000
6	Traffic Control	1	LS	$100,000	$100,000
7	Utility Relocation	1	LS	$150,000	$150,000
8	Street Repair	1	LS	$50,000	$50,000
9	Erosion Control	1	LS	$50,000	$50,000
10	Revegetation	1	LS	$600,000	$600,000
		Subtotal			$7,630,000
		Contingency	20%		$1,526,000
		Total			$9,156,000

Land Acquisition

1	Land Acquisition (outside MHPA)*	2,610,000	SF	$4	$10,440,000
2	Land Acquisition (inside MHPA)**	1,820,000	SF	$1	$1,820,000
		Subtotal			$12,260,000
		Contingency	20%		$2,452,000
		Total			$14,712,000

Total Cost (Construction and Land Acquisition) $23,868,000

Notes: * Includes area of detention basin and channel south of Siempre Viva
** Includes entire area within MHPA boundary
*** Estimate does not include engineering, environmental, geotechnical, surveying, etc.

8. Conclusion

The future developments on the Mesa will include source, site, priority project, and treatment control BMPs consistent with the City of San Diego Storm Water Standards. This project consists of treatment control which will be in place before adjacent development is completed. The treatment control consist of a detention basin and a grass lined channel for the watershed to minimize downstream flooding and to treat and filter runoff prior to discharge across border. Use of these control measures complies with the Municipal Storm Water National Pollutant Discharge Elimination System (NPDES) Permit and the City of San Diego's Storm Water Standards.

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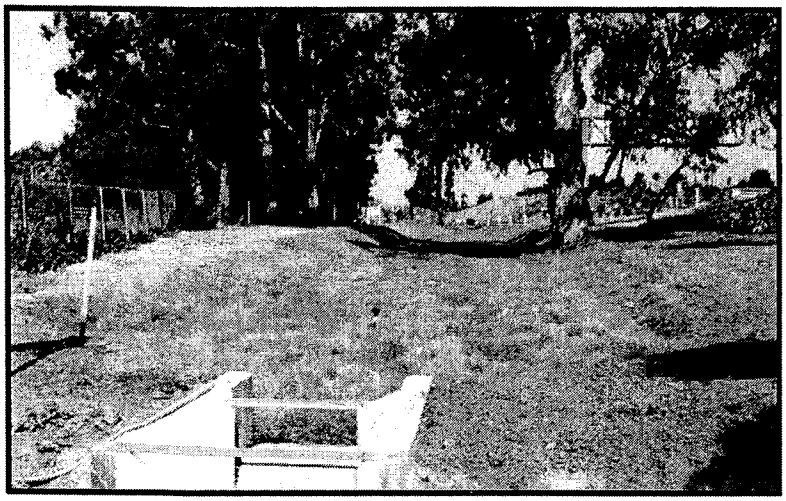
Vegetated Swale TC-30



Design Considerations

- Tributary Area
- Area Required
- Slope
- Water Availability

Description

Vegetated swales are open, shallow channels with vegetation covering the side slopes and bottom that collect and slowly convey runoff flow to downstream discharge points. They are designed to treat runoff through filtering by the vegetation in the channel, filtering through a subsoil matrix, and/or infiltration into the underlying soils. Swales can be natural or manmade. They trap particulate pollutants (suspended solids and trace metals), promote infiltration, and reduce the flow velocity of stormwater runoff. Vegetated swales can serve as part of a stormwater drainage system and can replace curbs, gutters and storm sewer systems.

Targeted Constituents

☑	Sediment	▲
☑	Nutrients	●
☑	Trash	●
☑	Metals	▲
☑	Bacteria	●
☑	Oil and Grease	▲
☑	Organics	▲

Legend *(Removal Effectiveness)*

● Low ■ High

▲ Medium

California Experience

Caltrans constructed and monitored six vegetated swales in southern California. These swales were generally effective in reducing the volume and mass of pollutants in runoff. Even in the areas where the annual rainfall was only about 10 inches/yr, the vegetation did not require additional irrigation. One factor that strongly affected performance was the presence of large numbers of gophers at most of the sites. The gophers created earthen mounds, destroyed vegetation, and generally reduced the effectiveness of the controls for TSS reduction.

Advantages

- If properly designed, vegetated, and operated, swales can serve as an aesthetic, potentially inexpensive urban development or roadway drainage conveyance measure with significant collateral water quality benefits.

- Roadside ditches should be regarded as significant potential swale/buffer strip sites and should be utilized for this purpose whenever possible.

Limitations

- Can be difficult to avoid channelization.
- May not be appropriate for industrial sites or locations where spills may occur
- Grassed swales cannot treat a very large drainage area. Large areas may be divided and treated using multiple swales.
- A thick vegetative cover is needed for these practices to function properly.
- They are impractical in areas with steep topography.
- They are not effective and may even erode when flow velocities are high, if the grass cover is not properly maintained.
- In some places, their use is restricted by law: many local municipalities require curb and gutter systems in residential areas.
- Swales are mores susceptible to failure if not properly maintained than other treatment BMPs.

Design and Sizing Guidelines

- Flow rate based design determined by local requirements or sized so that 85% of the annual runoff volume is discharged at less than the design rainfall intensity.
- Swale should be designed so that the water level does not exceed 2/3rds the height of the grass or 4 inches, which ever is less, at the design treatment rate.
- Longitudinal slopes should not exceed 2.5%
- Trapezoidal channels are normally recommended but other configurations, such as parabolic, can also provide substantial water quality improvement and may be easier to mow than designs with sharp breaks in slope.
- Swales constructed in cut are preferred, or in fill areas that are far enough from an adjacent slope to minimize the potential for gopher damage. Do not use side slopes constructed of fill, which are prone to structural damage by gophers and other burrowing animals.
- A diverse selection of low growing, plants that thrive under the specific site, climatic, and watering conditions should be specified. Vegetation whose growing season corresponds to the wet season are preferred. Drought tolerant vegetation should be considered especially for swales that are not part of a regularly irrigated landscaped area.
- The width of the swale should be determined using Manning's Equation using a value of 0.25 for Manning's n.

Construction/Inspection Considerations

- Include directions in the specifications for use of appropriate fertilizer and soil amendments based on soil properties determined through testing and compared to the needs of the vegetation requirements.
- Install swales at the time of the year when there is a reasonable chance of successful establishment without irrigation; however, it is recognized that rainfall in a given year may not be sufficient and temporary irrigation may be used.
- If sod tiles must be used, they should be placed so that there are no gaps between the tiles; stagger the ends of the tiles to prevent the formation of channels along the swale or strip.
- Use a roller on the sod to ensure that no air pockets form between the sod and the soil.
- Where seeds are used, erosion controls will be necessary to protect seeds for at least 75 days after the first rainfall of the season.

Performance

The literature suggests that vegetated swales represent a practical and potentially effective technique for controlling urban runoff quality. While limited quantitative performance data exists for vegetated swales, it is known that check dams, slight slopes, permeable soils, dense grass cover, increased contact time, and small storm events all contribute to successful pollutant removal by the swale system. Factors decreasing the effectiveness of swales include compacted soils, short runoff contact time, large storm events, frozen ground, short grass heights, steep slopes, and high runoff velocities and discharge rates.

Conventional vegetated swale designs have achieved mixed results in removing particulate pollutants. A study performed by the Nationwide Urban Runoff Program (NURP) monitored three grass swales in the Washington, D.C., area and found no significant improvement in urban runoff quality for the pollutants analyzed. However, the weak performance of these swales was attributed to the high flow velocities in the swales, soil compaction, steep slopes, and short grass height.

Another project in Durham, NC, monitored the performance of a carefully designed artificial swale that received runoff from a commercial parking lot. The project tracked 11 storms and concluded that particulate concentrations of heavy metals (Cu, Pb, Zn, and Cd) were reduced by approximately 50 percent. However, the swale proved largely ineffective for removing soluble nutrients.

The effectiveness of vegetated swales can be enhanced by adding check dams at approximately 17 meter (50 foot) increments along their length (See Figure 1). These dams maximize the retention time within the swale, decrease flow velocities, and promote particulate settling. Finally, the incorporation of vegetated filter strips parallel to the top of the channel banks can help to treat sheet flows entering the swale.

Only 9 studies have been conducted on all grassed channels designed for water quality (Table 1). The data suggest relatively high removal rates for some pollutants, but negative removals for some bacteria, and fair performance for phosphorus.

Table 1 Grassed swale pollutant removal efficiency data							
	Removal Efficiencies (% Removal)						
Study	TSS	TP	TN	NO_3	Metals	Bacteria	Type
Caltrans 2002	77	8	67	66	83-90	-33	dry swales
Goldberg 1993	67.8	4.5	-	31.4	42–62	-100	grassed channel
Seattle Metro and Washington Department of Ecology 1992	60	45	-	-25	2–16	-25	grassed channel
Seattle Metro and Washington Department of Ecology, 1992	83	29	-	-25	46–73	-25	grassed channel
Wang et al., 1981	80	-	-	-	70–80	-	dry swale
Dorman et al., 1989	98	18	-	45	37–81	-	dry swale
Harper, 1988	87	83	84	80	88–90	-	dry swale
Kercher et al., 1983	99	99	99	99	99	-	dry swale
Harper, 1988.	81	17	40	52	37–69	-	wet swale
Koon, 1995	67	39	-	9	-35 to 6	-	wet swale

While it is difficult to distinguish between different designs based on the small amount of available data, grassed channels generally have poorer removal rates than wet and dry swales, although some swales appear to export soluble phosphorus (Harper, 1988; Koon, 1995). It is not clear why swales export bacteria. One explanation is that bacteria thrive in the warm swale soils.

Siting Criteria

The suitability of a swale at a site will depend on land use, size of the area serviced, soil type, slope, imperviousness of the contributing watershed, and dimensions and slope of the swale system (Schueler et al., 1992). In general, swales can be used to serve areas of less than 10 acres, with slopes no greater than 5 %. Use of natural topographic lows is encouraged and natural drainage courses should be regarded as significant local resources to be kept in use (Young et al., 1996).

Selection Criteria (NCTCOG, 1993)

- Comparable performance to wet basins
- Limited to treating a few acres
- Availability of water during dry periods to maintain vegetation
- Sufficient available land area

Research in the Austin area indicates that vegetated controls are effective at removing pollutants even when dormant. Therefore, irrigation is not required to maintain growth during dry periods, but may be necessary only to prevent the vegetation from dying.

The topography of the site should permit the design of a channel with appropriate slope and cross-sectional area. Site topography may also dictate a need for additional structural controls. Recommendations for longitudinal slopes range between 2 and 6 percent. Flatter slopes can be used, if sufficient to provide adequate conveyance. Steep slopes increase flow velocity, decrease detention time, and may require energy dissipating and grade check. Steep slopes also can be managed using a series of check dams to terrace the swale and reduce the slope to within acceptable limits. The use of check dams with swales also promotes infiltration.

Additional Design Guidelines

Most of the design guidelines adopted for swale design specify a minimum hydraulic residence time of 9 minutes. This criterion is based on the results of a single study conducted in Seattle, Washington (Seattle Metro and Washington Department of Ecology, 1992), and is not well supported. Analysis of the data collected in that study indicates that pollutant removal at a residence time of 5 minutes was not significantly different, although there is more variability in that data. Therefore, additional research in the design criteria for swales is needed. Substantial pollutant removal has also been observed for vegetated controls designed solely for conveyance (Barrett et al, 1998); consequently, some flexibility in the design is warranted.

Many design guidelines recommend that grass be frequently mowed to maintain dense coverage near the ground surface. Recent research (Colwell et al., 2000) has shown mowing frequency or grass height has little or no effect on pollutant removal.

Summary of Design Recommendations

1) The swale should have a length that provides a minimum hydraulic residence time of at least 10 minutes. The maximum bottom width should not exceed 10 feet unless a dividing berm is provided. The depth of flow should not exceed 2/3rds the height of the grass at the peak of the water quality design storm intensity. The channel slope should not exceed 2.5%.

2) A design grass height of 6 inches is recommended.

3) Regardless of the recommended detention time, the swale should be not less than 100 feet in length.

4) The width of the swale should be determined using Manning's Equation, at the peak of the design storm, using a Manning's n of 0.25.

5) The swale can be sized as both a treatment facility for the design storm and as a conveyance system to pass the peak hydraulic flows of the 100-year storm if it is located "on-line." The side slopes should be no steeper than 3:1 (H:V).

6) Roadside ditches should be regarded as significant potential swale/buffer strip sites and should be utilized for this purpose whenever possible. If flow is to be introduced through curb cuts, place pavement slightly above the elevation of the vegetated areas. Curb cuts should be at least 12 inches wide to prevent clogging.

7) Swales must be vegetated in order to provide adequate treatment of runoff. It is important to maximize water contact with vegetation and the soil surface. For general purposes, select fine, close-growing, water-resistant grasses. If possible, divert runoff (other than necessary irrigation) during the period of vegetation

establishment. Where runoff diversion is not possible, cover graded and seeded areas with suitable erosion control materials.

Maintenance

The useful life of a vegetated swale system is directly proportional to its maintenance frequency. If properly designed and regularly maintained, vegetated swales can last indefinitely. The maintenance objectives for vegetated swale systems include keeping up the hydraulic and removal efficiency of the channel and maintaining a dense, healthy grass cover.

Maintenance activities should include periodic mowing (with grass never cut shorter than the design flow depth), weed control, watering during drought conditions, reseeding of bare areas, and clearing of debris and blockages. Cuttings should be removed from the channel and disposed in a local composting facility. Accumulated sediment should also be removed manually to avoid concentrated flows in the swale. The application of fertilizers and pesticides should be minimal.

Another aspect of a good maintenance plan is repairing damaged areas within a channel. For example, if the channel develops ruts or holes, it should be repaired utilizing a suitable soil that is properly tamped and seeded. The grass cover should be thick; if it is not, reseed as necessary. Any standing water removed during the maintenance operation must be disposed to a sanitary sewer at an approved discharge location. Residuals (e.g., silt, grass cuttings) must be disposed in accordance with local or State requirements. Maintenance of grassed swales mostly involves maintenance of the grass or wetland plant cover. Typical maintenance activities are summarized below:

- Inspect swales at least twice annually for erosion, damage to vegetation, and sediment and debris accumulation preferably at the end of the wet season to schedule summer maintenance and before major fall runoff to be sure the swale is ready for winter. However, additional inspection after periods of heavy runoff is desirable. The swale should be checked for debris and litter, and areas of sediment accumulation.
- Grass height and mowing frequency may not have a large impact on pollutant removal. Consequently, mowing may only be necessary once or twice a year for safety or aesthetics or to suppress weeds and woody vegetation.
- Trash tends to accumulate in swale areas, particularly along highways. The need for litter removal is determined through periodic inspection, but litter should always be removed prior to mowing.
- Sediment accumulating near culverts and in channels should be removed when it builds up to 75 mm (3 in.) at any spot, or covers vegetation.
- Regularly inspect swales for pools of standing water. Swales can become a nuisance due to mosquito breeding in standing water if obstructions develop (e.g. debris accumulation, invasive vegetation) and/or if proper drainage slopes are not implemented and maintained.

Cost

Construction Cost

Little data is available to estimate the difference in cost between various swale designs. One study (SWRPC, 1991) estimated the construction cost of grassed channels at approximately $0.25 per ft². This price does not include design costs or contingencies. Brown and Schueler (1997) estimate these costs at approximately 32 percent of construction costs for most stormwater management practices. For swales, however, these costs would probably be significantly higher since the construction costs are so low compared with other practices. A more realistic estimate would be a total cost of approximately $0.50 per ft², which compares favorably with other stormwater management practices.

Table 2 Swale Cost Estimate (SEWRPC, 1991)

Component	Unit	Extent	Unit Cost			Total Cost		
			Low	Moderate	High	Low	Moderate	High
Mobilization / Demobilization-Light	Swale	1	$107	$274	$441	$107	$274	$441
Site Preparation								
Clearing[b]	Acre	0.5	$2,200	$3,800	$5,400	$1,100	$1,900	$2,700
Grubbing[c]	Acre	0.25	$3,800	$5,200	$6,600	$950	$1,300	$1,650
General								
Excavation[d]	Yd^3	372	$2.10	$3.70	$5.30	$781	$1,376	$1,972
Level and Till[e]	Yd^2	1,210	$0.20	$0.35	$0.50	$242	$424	$605
Sites Development								
Salvaged Topsoil Seed, and Mulch[f]	Yd^2	1,210	$0.40	$1.00	$1.60	$484	$1,210	$1,936
Sod[g]	Yd^2	1,210	$1.20	$2.40	$3.60	$1,452	$2,904	$4,356
Subtotal	--	--	--	--	--	$5,116	$9,388	$13,660
Contingencies	Swale	1	25%	25%	25%	$1,279	$2,347	$3,415
Total	--	--	--	--	--	$6,395	$11,735	$17,075

Source: (SEWRPC, 1991)

Note: Mobilization/demobilization refers to the organization and planning involved in establishing a vegetative swale.

[a] Swale has a bottom width of 1.0 foot, a top width of 10 feet with 1:3 side slopes, and a 1,000-foot length.

[b] Area cleared = (top width + 10 feet) x swale length.

[c] Area grubbed = (top width x swale length).

[d] Volume excavated = (0.67 x top width x swale depth) x swale length (parabolic cross-section).

[e] Area tilled = $\left(\text{top width} + \frac{8(\text{swale depth}^2)}{3(\text{top width})}\right) \times$ swale length (parabolic cross-section).

[f] Area seeded = area cleared x 0.5.

[g] Area sodded = area cleared x 0.5.

Table 3 Estimated Maintenance Costs (SEWRPC, 1991)

Component	Unit Cost	Swale Size (Depth and Top Width)		Comment
		1.5 Foot Depth, One-Foot Bottom Width, 10-Foot Top Width	3-Foot Depth, 3-Foot Bottom Width, 21-Foot Top Width	
Lawn Mowing	$0.85 / 1,000 ft^2 / mowing	$0.14 / linear foot	$0.21 / linear foot	Lawn maintenance area=(top width + 10 feet) x length. Mow eight times per year
General Lawn Care	$9.00 / 1,000 ft^2 / year	$0.18 / linear foot	$0.28 / linear foot	Lawn maintenance area = (top width + 10 feet) x length
Swale Debris and Litter Removal	$0.10 / linear foot / year	$0.10 / linear foot	$0.10 / linear foot	--
Grass Reseeding with Mulch and Fertilizer	$0.30 / yd^2	$0.01 / linear foot	$0.01 / linear foot	Area revegetated equals 1% of lawn maintenance area per year
Program Administration and Swale Inspection	$0.15 / linear foot / year, plus $25 / inspection	$0.15 / linear foot	$0.15 / linear foot	Inspect four times per year
Total	--	$0.58 / linear foot	$ 0.75 / linear foot	--

Maintenance Cost

Caltrans (2002) estimated the expected annual maintenance cost for a swale with a tributary area of approximately 2 ha at approximately $2,700. Since almost all maintenance consists of mowing, the cost is fundamentally a function of the mowing frequency. Unit costs developed by SEWRPC are shown in Table 3. In many cases vegetated channels would be used to convey runoff and would require periodic mowing as well, so there may be little additional cost for the water quality component. Since essentially all the activities are related to vegetation management, no special training is required for maintenance personnel.

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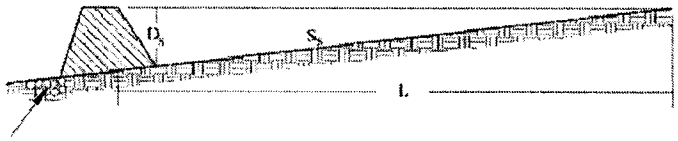
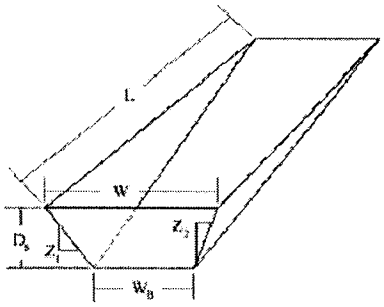


Provide for scour protection.

(a) Cross section of swale with check dam.

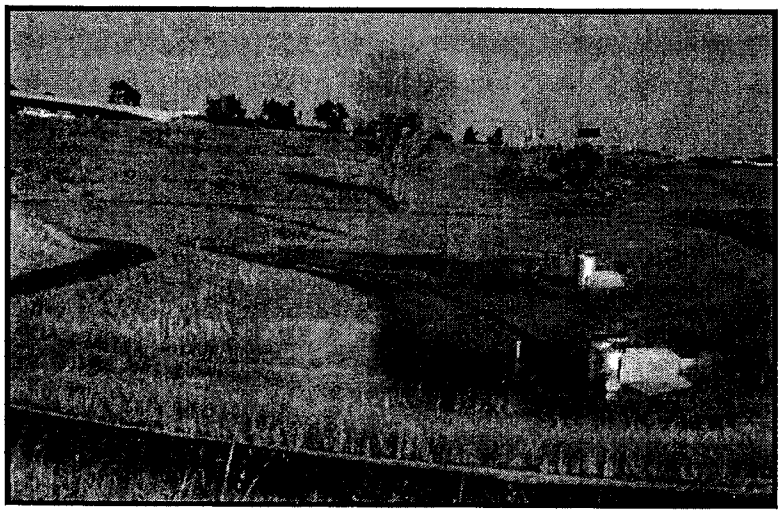


(b) Dimensional view of swale impoundment area.

Notation:

L = Length of swale impoundment area per check dam (ft)
D_s = Depth of check dam (ft)
S_s = Bottom slope of swale (ft/ft)
W = Top width of check dam (ft)
W_B = Bottom width of check dam (ft)
$Z_{1&2}$ = Ratio of horizontal to vertical change in swale side slope (ft/ft)

Extended Detention Basin TC-22



Design Considerations

- Tributary Area
- Area Required
- Hydraulic Head

Description

Dry extended detention ponds (a.k.a. dry ponds, extended detention basins, detention ponds, extended detention ponds) are basins whose outlets have been designed to detain the stormwater runoff from a water quality design storm for some minimum time (e.g., 48 hours) to allow particles and associated pollutants to settle. Unlike wet ponds, these facilities do not have a large permanent pool. They can also be used to provide flood control by including additional flood detention storage.

Targeted Constituents

☑	Sediment	▲
☑	Nutrients	●
☑	Trash	■
☑	Metals	▲
☑	Bacteria	▲
☑	Oil and Grease	▲
☑	Organics	▲

Legend *(Removal Effectiveness)*

● Low ■ High

▲ Medium

California Experience

Caltrans constructed and monitored 5 extended detention basins in southern California with design drain times of 72 hours. Four of the basins were earthen, less costly and had substantially better load reduction because of infiltration that occurred, than the concrete basin. The Caltrans study reaffirmed the flexibility and performance of this conventional technology. The small headloss and few siting constraints suggest that these devices are one of the most applicable technologies for stormwater treatment.

Advantages

- Due to the simplicity of design, extended detention basins are relatively easy and inexpensive to construct and operate.
- Extended detention basins can provide substantial capture of sediment and the toxics fraction associated with particulates.
- Widespread application with sufficient capture volume can provide significant control of channel erosion and enlargement caused by changes to flow frequency

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relationships resulting from the increase of impervious cover in a watershed.

Limitations

- Limitation of the diameter of the orifice may not allow use of extended detention in watersheds of less than 5 acres (would require an orifice with a diameter of less than 0.5 inches that would be prone to clogging).
- Dry extended detention ponds have only moderate pollutant removal when compared to some other structural stormwater practices, and they are relatively ineffective at removing soluble pollutants.
- Although wet ponds can increase property values, dry ponds can actually detract from the value of a home due to the adverse aesthetics of dry, bare areas and inlet and outlet structures.

Design and Sizing Guidelines

- Capture volume determined by local requirements or sized to treat 85% of the annual runoff volume.
- Outlet designed to discharge the capture volume over a period of hours.
- Length to width ratio of at least 1.5:1 where feasible.
- Basin depths optimally range from 2 to 5 feet.
- Include energy dissipation in the inlet design to reduce resuspension of accumulated sediment.
- A maintenance ramp and perimeter access should be included in the design to facilitate access to the basin for maintenance activities and for vector surveillance and control.
- Use a draw down time of 48 hours in most areas of California. Draw down times in excess of 48 hours may result in vector breeding, and should be used only after coordination with local vector control authorities. Draw down times of less than 48 hours should be limited to BMP drainage areas with coarse soils that readily settle and to watersheds where warming may be determined to downstream fisheries.

Construction/Inspection Considerations

- Inspect facility after first large to storm to determine whether the desired residence time has been achieved.
- When constructed with small tributary area, orifice sizing is critical and inspection should verify that flow through additional openings such as bolt holes does not occur.

Performance

One objective of stormwater management practices can be to reduce the flood hazard associated with large storm events by reducing the peak flow associated with these storms. Dry extended detention basins can easily be designed for flood control, and this is actually the primary purpose of most detention ponds.

Dry extended detention basins provide moderate pollutant removal, provided that the recommended design features are incorporated. Although they can be effective at removing some pollutants through settling, they are less effective at removing soluble pollutants because of the absence of a permanent pool. Several studies are available on the effectiveness of dry extended detention ponds including one recently concluded by Caltrans (2002).

The load reduction is greater than the concentration reduction because of the substantial infiltration that occurs. Although the infiltration of stormwater is clearly beneficial to surface receiving waters, there is the potential for groundwater contamination. Previous research on the effects of incidental infiltration on groundwater quality indicated that the risk of contamination is minimal.

There were substantial differences in the amount of infiltration that were observed in the earthen basins during the Caltrans study. On average, approximately 40 percent of the runoff entering the unlined basins infiltrated and was not discharged. The percentage ranged from a high of about 60 percent to a low of only about 8 percent for the different facilities. Climatic conditions and local water table elevation are likely the principal causes of this difference. The least infiltration occurred at a site located on the coast where humidity is higher and the basin invert is within a few meters of sea level. Conversely, the most infiltration occurred at a facility located well inland in Los Angeles County where the climate is much warmer and the humidity is less, resulting in lower soil moisture content in the basin floor at the beginning of storms.

Vegetated detention basins appear to have greater pollutant removal than concrete basins. In the Caltrans study, the concrete basin exported sediment and associated pollutants during a number of storms. Export was not as common in the earthen basins, where the vegetation appeared to help stabilize the retained sediment.

Siting Criteria

Dry extended detention ponds are among the most widely applicable stormwater management practices and are especially useful in retrofit situations where their low hydraulic head requirements allow them to be sited within the constraints of the existing storm drain system. In addition, many communities have detention basins designed for flood control. It is possible to modify these facilities to incorporate features that provide water quality treatment and/or channel protection. Although dry extended detention ponds can be applied rather broadly, designers need to ensure that they are feasible at the site in question. This section provides basic guidelines for siting dry extended detention ponds.

In general, dry extended detention ponds should be used on sites with a minimum area of 5 acres. With this size catchment area, the orifice size can be on the order of 0.5 inches. On smaller sites, it can be challenging to provide channel or water quality control because the orifice diameter at the outlet needed to control relatively small storms becomes very small and thus prone to clogging. In addition, it is generally more cost-effective to control larger drainage areas due to the economies of scale.

Extended detention basins can be used with almost all soils and geology, with minor design adjustments for regions of rapidly percolating soils such as sand. In these areas, extended detention ponds may need an impermeable liner to prevent ground water contamination.

The base of the extended detention facility should not intersect the water table. A permanently wet bottom may become a mosquito breeding ground. Research in Southwest Florida (Santana et al., 1994) demonstrated that intermittently flooded systems, such as dry extended detention ponds, produce more mosquitoes than other pond systems, particularly when the facilities remained wet for more than 3 days following heavy rainfall.

A study in Prince George's County, Maryland, found that stormwater management practices can increase stream temperatures (Galli, 1990). Overall, dry extended detention ponds increased temperature by about 5°F. In cold water streams, dry ponds should be designed to detain stormwater for a relatively short time (i.e., 24 hours) to minimize the amount of warming that occurs in the basin.

Additional Design Guidelines

In order to enhance the effectiveness of extended detention basins, the dimensions of the basin must be sized appropriately. Merely providing the required storage volume will not ensure maximum constituent removal. By effectively configuring the basin, the designer will create a long flow path, promote the establishment of low velocities, and avoid having stagnant areas of the basin. To promote settling and to attain an appealing environment, the design of the basin should consider the length to width ratio, cross-sectional areas, basin slopes and pond configuration, and aesthetics (Young et al., 1996).

Energy dissipation structures should be included for the basin inlet to prevent resuspension of accumulated sediment. The use of stilling basins for this purpose should be avoided because the standing water provides a breeding area for mosquitoes.

Extended detention facilities should be sized to completely capture the water quality volume. A micropool is often recommended for inclusion in the design and one is shown in the schematic diagram. These small permanent pools greatly increase the potential for mosquito breeding and complicate maintenance activities; consequently, they are not recommended for use in California.

A large aspect ratio may improve the performance of detention basins; consequently, the outlets should be placed to maximize the flowpath through the facility. The ratio of flowpath length to width from the inlet to the outlet should be at least 1.5:1 (L:W) where feasible. Basin depths optimally range from 2 to 5 feet.

The facility's drawdown time should be regulated by an orifice or weir. In general, the outflow structure should have a trash rack or other acceptable means of preventing clogging at the entrance to the outflow pipes. The outlet design implemented by Caltrans in the facilities constructed in San Diego County used an outlet riser with orifices

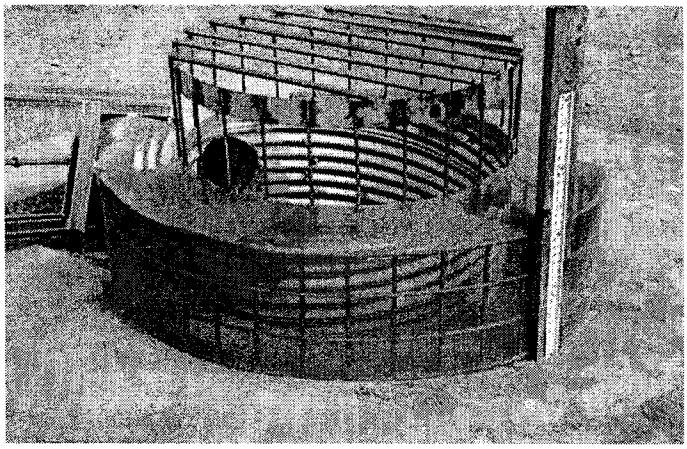

Figure 1
Example of Extended Detention Outlet Structure

sized to discharge the water quality volume, and the riser overflow height was set to the design storm elevation. A stainless steel screen was placed around the outlet riser to ensure that the orifices would not become clogged with debris. Sites either used a separate riser or broad crested weir for overflow of runoff for the 25 and greater year storms. A picture of a typical outlet is presented in Figure 1.

The outflow structure should be sized to allow for complete drawdown of the water quality volume in 72 hours. No more than 50% of the water quality volume should drain from the facility within the first 24 hours. The outflow structure can be fitted with a valve so that discharge from the basin can be halted in case of an accidental spill in the watershed.

Summary of Design Recommendations

(1) Facility Sizing - The required water quality volume is determined by local regulations or the basin should be sized to capture and treat 85% of the annual runoff volume. See Section 5.5.1 of the handbook for a discussion of volume-based design.

Basin Configuration – A high aspect ratio may improve the performance of detention basins; consequently, the outlets should be placed to maximize the flowpath through the facility. The ratio of flowpath length to width from the inlet to the outlet should be at least 1.5:1 (L:W). The flowpath length is defined as the distance from the inlet to the outlet as measured at the surface. The width is defined as the mean width of the basin. Basin depths optimally range from 2 to 5 feet. The basin may include a sediment forebay to provide the opportunity for larger particles to settle out.

A micropool should not be incorporated in the design because of vector concerns. For online facilities, the principal and emergency spillways must be sized to provide 1.0 foot of freeboard during the 25-year event and to safely pass the flow from 100-year storm.

(2) Pond Side Slopes - Side slopes of the pond should be 3:1 (H:V) or flatter for grass stabilized slopes. Slopes steeper than 3:1 (H:V) must be stabilized with an appropriate slope stabilization practice.

(3) Basin Lining – Basins must be constructed to prevent possible contamination of groundwater below the facility.

(4) Basin Inlet – Energy dissipation is required at the basin inlet to reduce resuspension of accumulated sediment and to reduce the tendency for short-circuiting.

(5) Outflow Structure - The facility's drawdown time should be regulated by a gate valve or orifice plate. In general, the outflow structure should have a trash rack or other acceptable means of preventing clogging at the entrance to the outflow pipes.

The outflow structure should be sized to allow for complete drawdown of the water quality volume in 72 hours. No more than 50% of the water quality volume should drain from the facility within the first 24 hours. The outflow structure should be fitted with a valve so that discharge from the basin can be halted in case of an accidental spill in the watershed. This same valve also can be used to regulate the rate of discharge from the basin.

The discharge through a control orifice is calculated from:

$$Q = CA(2g(H-H_o))^{0.5}$$

where: Q = discharge (ft^3/s)
C = orifice coefficient
A = area of the orifice (ft^2)
g = gravitational constant (32.2)
H = water surface elevation (ft)
H_o= orifice elevation (ft)

Recommended values for C are 0.66 for thin materials and 0.80 when the material is thicker than the orifice diameter. This equation can be implemented in spreadsheet form with the pond stage/volume relationship to calculate drain time. To do this, use the initial height of the water above the orifice for the water quality volume. Calculate the discharge and assume that it remains constant for approximately 10 minutes. Based on that discharge, estimate the total discharge during that interval and the new elevation based on the stage volume relationship. Continue to iterate until H is approximately equal to H_o. When using multiple orifices the discharge from each is summed.

(6) Splitter Box - When the pond is designed as an offline facility, a splitter structure is used to isolate the water quality volume. The splitter box, or other flow diverting approach, should be designed to convey the 25-year storm event while providing at least 1.0 foot of freeboard along pond side slopes.

(7) Erosion Protection at the Outfall - For online facilities, special consideration should be given to the facility's outfall location. Flared pipe end sections that discharge at or near the stream invert are preferred. The channel immediately below the pond outfall should be modified to conform to natural dimensions, and lined with large stone riprap placed over filter cloth. Energy dissipation may be required to reduce flow velocities from the primary spillway to non-erosive velocities.

(8) Safety Considerations - Safety is provided either by fencing of the facility or by managing the contours of the pond to eliminate dropoffs and other hazards. Earthen side slopes should not exceed 3:1 (H:V) and should terminate on a flat safety bench area. Landscaping can be used to impede access to the facility. The primary spillway opening must not permit access by small children. Outfall pipes above 48 inches in diameter should be fenced.

Maintenance

Routine maintenance activity is often thought to consist mostly of sediment and trash and debris removal; however, these activities often constitute only a small fraction of the maintenance hours. During a recent study by Caltrans, 72 hours of maintenance was performed annually, but only a little over 7 hours was spent on sediment and trash removal. The largest recurring activity was vegetation management, routine mowing. The largest absolute number of hours was associated with vector control because of mosquito breeding that occurred in the stilling basins (example of standing water to be avoided) installed as energy dissipaters. In most cases, basic housekeeping practices such as removal of debris accumulations and vegetation

management to ensure that the basin dewaters completely in 48-72 hours is sufficient to prevent creating mosquito and other vector habitats.

Consequently, maintenance costs should be estimated based primarily on the mowing frequency and the time required. Mowing should be done at least annually to avoid establishment of woody vegetation, but may need to be performed much more frequently if aesthetics are an important consideration.

Typical activities and frequencies include:

- Schedule semiannual inspection for the beginning and end of the wet season for standing water, slope stability, sediment accumulation, trash and debris, and presence of burrows.
- Remove accumulated trash and debris in the basin and around the riser pipe during the semiannual inspections. The frequency of this activity may be altered to meet specific site conditions.
- Trim vegetation at the beginning and end of the wet season and inspect monthly to prevent establishment of woody vegetation and for aesthetic and vector reasons.
- Remove accumulated sediment and re-grade about every 10 years or when the accumulated sediment volume exceeds 10 percent of the basin volume. Inspect the basin each year for accumulated sediment volume.

Cost

Construction Cost

The construction costs associated with extended detention basins vary considerably. One recent study evaluated the cost of all pond systems (Brown and Schueler, 1997). Adjusting for inflation, the cost of dry extended detention ponds can be estimated with the equation:

$$C = 12.4V^{0.760}$$

where: C = Construction, design, and permitting cost, and
V = Volume (ft^3).

Using this equation, typical construction costs are:

$ 41,600 for a 1 acre-foot pond

$ 239,000 for a 10 acre-foot pond

$ 1,380,000 for a 100 acre-foot pond

Interestingly, these costs are generally slightly higher than the predicted cost of wet ponds (according to Brown and Schueler, 1997) on a cost per total volume basis, which highlights the difficulty of developing reasonably accurate construction estimates. In addition, a typical facility constructed by Caltrans cost about $160,000 with a capture volume of only 0.3 ac-ft.

An economic concern associated with dry ponds is that they might detract slightly from the value of adjacent properties. One study found that dry ponds can actually detract from the

perceived value of homes adjacent to a dry pond by between 3 and 10 percent (Emmerling-Dinovo, 1995).

Maintenance Cost

For ponds, the annual cost of routine maintenance is typically estimated at about 3 to 5 percent of the construction cost (EPA website). Alternatively, a community can estimate the cost of the maintenance activities outlined in the maintenance section. Table 1 presents the maintenance costs estimated by Caltrans based on their experience with five basins located in southern California. Again, it should be emphasized that the vast majority of hours are related to vegetation management (mowing).

Table 1 Estimated Average Annual Maintenance Effort

Activity	Labor Hours	Equipment & Material ($)	Cost
Inspections	4	7	183
Maintenance	49	126	2282
Vector Control	0	0	0
Administration	3	0	132
Materials	-	535	535
Total	**56**	**$668**	**$3,132**

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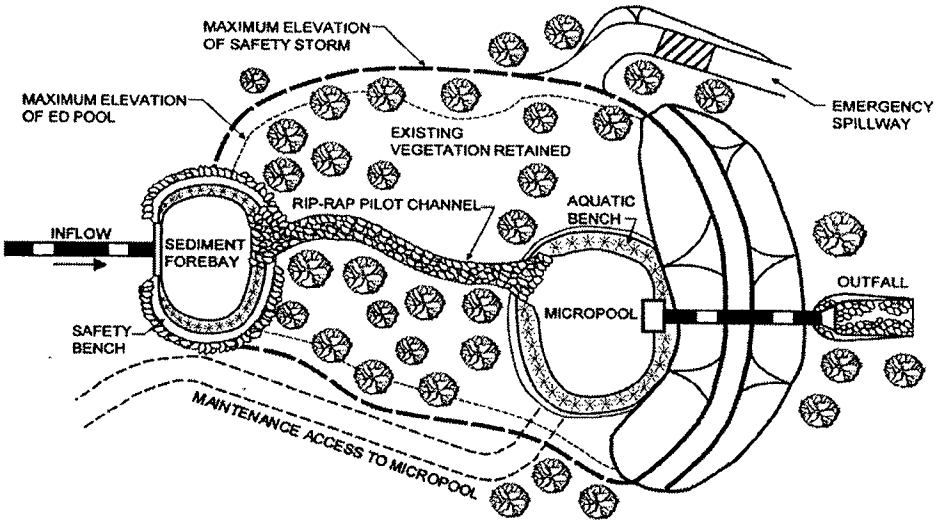
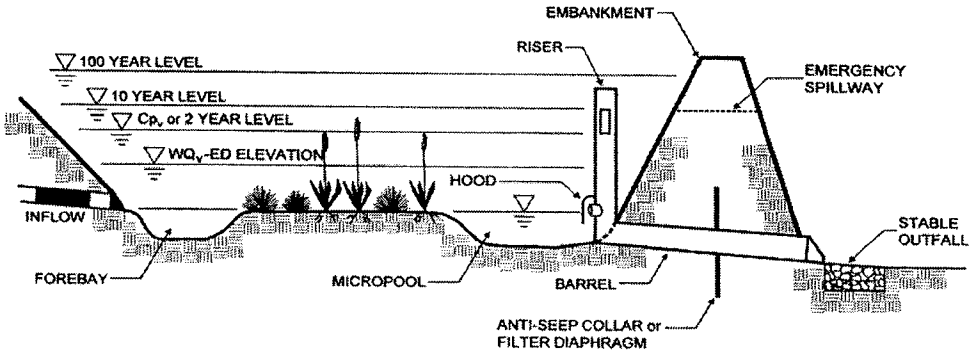


PLAN VIEW



PROFILE

Schematic of an Extended Detention Basin (MDE, 2000)

Drainage Study for the Otay Mesa Community Plan Update

June, 2006

Prepared for:
MNA Consulting
427 C Street, Suite 308
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Prepared by:
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TABLE OF CONTENTS

I. BACKGROUND 1

II. EXISTING DRAINAGE FACILITIES 3

III. HYDROLOGIC ANALYSIS 5

IV. HYDRAULIC ANALYSIS 9

V. PROPOSED DRAINAGE FACILITIES 12

VI. PROPOSED DRAINAGE ALTERNATIVES 14

VII. RECOMMENDED DRAINAGE DESIGN CRITERIA 20

VIII. STORM WATER QUALITY REQUIREMENTS 21

LIST OF EXHIBITS

EXISTING DRAINAGE FACILITIES MAP 4

WATERSHED MAP 7

AES SUMMARY TABLE 8

HEC-RAS MODEL 10

PROPOSED DRAINAGE FACILITIES MAP 13

COST ESTIMATE 16

PRELIMINARY DESIGN PLAN: LA MEDIA CHANNEL AND BORDER DETENTION BASIN 17

PRELIMINARY DESIGN: CHANNEL CROSS SECTION 18

PROPERTY OWNERSHIP MAP 19

RECOMMENDED STORM WATER POLICIES 23

EXAMPLE OF PERMANENT STORM WATER BEST MANAGEMENT PRACTICES 24

STORM WATER REQUIREMENTS CHECKLIST 25

APPENDICES

APPENDIX A AES HYDROLOGY CALCULATIONS

APPENDIX B HEC-1 MODEL

I. BACKGROUND

This report has been prepared as an appendix to the Otay Mesa Community Plan update EIR. Its purpose is to provide a summary of the existing drainage situation and facilities and proposed future facilities, including alternatives for draining the large central watershed. In addition, this report presents recommendations for drainage design criteria and storm water quality requirements for each of the watersheds on the Mesa.

For most of its early history, Otay Mesa was used for agriculture and farming was the primary land use. As industrial and commercial development started taking place in the 1960s, the City of San Diego recognized the need for a comprehensive drainage Master Plan for the Mesa. Because most of the Mesa drains to the South into Mexico, there was concern that the new development would increase the runoff crossing the border. The City needed to establish criteria for the new development such that there was no increase in runoff as a result of the new construction.

In May of 1987, the City Council approved a contract to prepare the Otay Mesa Drainage Master Plan. In August of 1987, the City published a Notice to "All Private Engineers" that established "Drainage Requirements for Development in Otay Mesa" (attached). The Master Plan was published in January, 1988, and included a proposed concrete Channel from Airway Road to Siempre Viva Road that followed the existing drainage channel.

The Master plan was updated with the "Otay Mesa Drainage Study" published in August, 1999. The most significant recommendation change was moving the proposed new channel from the creek alignment to a new location directly adjacent to La Media Road and Siempre Viva Road.

Reproduction of 1987 NOTICE from Engineering and Development Department

NOTICE

Date: August 7, 1987

To: All Private Engineers

From: Subdivision Engineer

Subject: Drainage requirements for development in Otay Mesa

In order to minimize the effects of increased storm water runoff in Mexico, due to development of property in Otay Mesa, all property in Otay Mesa that is within the water shed that drains into Mexico, shall be developed with the following requirements:

1. Each property owner shall provide storm water detention facilities so that there will be no increase in the rate of runoff due to development of the property.

2. The detention facilities shall be designed so that the rate of runoff from the property will not be greater after development than it was before development for a 5 year, 10 year, 25 year and 50 year storm.

3. All drainage facilities crossing four-lane major or higher classification streets shall be designed for a Q100 (existing). Other facilities, except the major channel referred to in paragraph 5, may be designed for Q50 (existing).

4. The Drainage Design Manual shall be used as guidelines for design of drainage facilities and computing design discharges.

5. The City Engineer's Office, Flood Control Section, is preparing a preliminary plan for the main north-south channel from Otay Mesa Road near La Media to the Mexican Border. The preliminary design will include the design "Q" (Q100 existing), the invert grade, and the water surface elevation at the major road crossings.

C.R. Lockhead
Subdivision Engineer

II. EXISTING DRAINAGE FACILITIES

Information was collected for existing drainage and flood control facilities on Otay Mesa through as-built plans, SanGIS maps, and site visits. Most of the existing drainage facilities were constructed as part of the private development that is taking place on the Mesa. Many of these facilities are not continuous because of the piecemeal nature of the development. This creates challenges for the subsequent developers that need to tie into the existing facilities. Many of the existing facilities are temporary.

Most of the development to-date has occurred in the East Watershed, which therefore includes most of the existing drainage facilities on the Mesa. The existing system is a combination of storm drains, improved channels, and detention basins, which in many areas discharge to natural drainage paths that do not have adequate hydraulic capacity.

The "Existing Drainage Facilities" drawing shows the facilities as-of the date of this report. The area is developing rapidly, and therefore new facilities are continuously being constructed. There are currently no dedicated drainage rights-of-way on the Mesa. Many of the projects, as they were mapped and constructed, dedicated portions of the properties to the city as drainage easements or flood water storage easements. Eventually, the systems and their easements will be continuous.

III. HYDROLOGIC ANALYSIS

The Otay Mesa Study area is shown on the Watershed Map, and includes all of the Mesa area within the City of San Diego divided into five watersheds (with the exception of the far northwest arm of the Mesa, which is fully developed).

Watersheds	Acres	mi^2
West Perimeter Watershed	258	0.40
West Watershed	2,190	3.42
North Perimeter Watershed	590	0.92
East Watershed	3,864	6.04
Border Crossing Watershed	223	0.35
TOTAL	7,125	11.13

Most of the Mesa slopes from North to South, with the flow entering Mexico at several points. The northern and western perimeters of the Mesa flow into the adjacent Canyons. These perimeter watersheds are divided into several independent smaller watersheds. The watershed boundaries on the Mesa are not well defined because the Mesa is so flat. There are very few defined natural drainage paths, with much of the runoff sheet-flowing across the Mesa. The watershed boundaries shown are based on field investigations and best available mapping, but the actual drainage boundaries may be very different.

The only watershed that has been studied significantly from a drainage perspective is the East Watershed. Hydrologic models have been prepared for both of the previous drainage studies. The peak flows calculated in the two studies are different, primarily because of different assumptions relative to developed area, proposed drainage facilities, and watershed areas. The East Watershed includes a large area of unincorporated County property. The hydrologic model assumed the same industrial development for the unincorporated area. If land uses change in the County area, it may change the runoff rates. The differences for the concentration point at the border are shown below.

Q100 at Border East Watershed		
	Area (mi^2)	Q100(cfs)
1988 Study	5.72	5,050
1999 Study	6.63	3,529
2004 CPU	6.78	3,673

As part of this study, new hydrologic models have been prepared for the main watersheds which flow into the Tijuana River. For the East Watershed, HEC-1 has been used, since both previous studies used this model. For the other watersheds, the standard City of San Diego Modified Rational Method (AES) has been used. The results of these analyses are shown in the table below.

Hydrologic Analysis Summary			
	Area (mi^2)	Q50(cfs)	Q100(cfs)
West Perimeter Watershed	0.40	170	444
West Watershed	3.42	672	1,676
East Watershed	6.78	1,280	3,673
	10.60	2,122	5,793

In addition to the above flows, the Spring Canyon open space area contributes 109 cfs (Q50) and 257 cfs (Q100) from 1.2 mi^2. Since the Tijuana River Watershed is a water-quality impacted watershed, the quality and quantity of flow will need to be addressed before additional development takes place.

IV. HYDRAULIC ANALYSIS

Most of the Mesa is very flat, resulting in local flooding during storms at the low points and along some drainage ditches. The only significant creek on the Mesa is the main channel in the East Watershed, Otay Mesa Creek, which flows from North to South along La Media Road and crosses the border into Mexico just north of the Tijuana Airport.

A HEC-RAS hydraulic model was prepared for this channel from the border north to Otay Mesa Road. The purpose of this model was to identify the 100-year floodplain for this reach for present conditions. The proposed future drainage project along this alignment will be designed to contain the 100-year flow, reducing or eliminating flooding impacts to adjacent properties.

The HEC-RAS model was also used to size the proposed new channel from Airway Road to just south of Siempre Viva Road. Several alternative cross-sections were modeled to reflect input on the environmental aspects of the channel.

A significant tributary to the main channel enters just upstream of the Siempre Viva Road crossing. This tributary conveys flow from the De La Fuente Business Park and the Siempre Viva Business Park. The existing channel from La Media Road to the proposed main channel is approximately 15 feet wide and 4 feet deep, with a hydraulic capacity of approximately 120 cfs. The 100 year flow in this channel is 1116 cfs. A proposed new channel has a 50 ft bottom width with 1.5:1.0 side slopes and will convey the 100 year flow. A double 10' x 4.5' RCB will also be required for the flow under La Media Road. The cost estimate does not include these facilities.

HEC-RAS Plan: Plan 01 River: Otay Mesa Draina Reach: Channel Profile: PF 1

Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Channel	5500	PF 1	2500.00	464.60	471.08		471.16	0.002743	2.33	1073.59	200.00	0.18
Channel	5350	PF 1	2500.00	464.23	470.69		470.76	0.002572	2.16	1279.19	335.44	0.17
Channel	5100	PF 1	2500.00	463.60	470.06		470.12	0.002591	2.17	1275.99	335.16	0.17
Channel	4800	PF 1	2500.00	462.85	469.27		469.33	0.002666	2.19	1263.56	334.04	0.18
Channel	4500	PF 1	2500.00	462.10	468.51		468.56	0.002430	2.08	1358.84	378.24	0.17
Channel	4200	PF 1	2500.00	461.35	467.79		467.85	0.002365	2.07	1371.79	379.61	0.17
Channel	3900	PF 1	2500.00	460.60	467.09		467.15	0.002266	2.04	1392.50	381.79	0.16
Channel	3600	PF 1	2500.00	459.85	466.30		466.37	0.002969	2.32	1153.04	281.59	0.19
Channel	3300	PF 1	2500.00	459.10	465.33		465.42	0.003423	2.41	1109.99	285.62	0.20
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Channel	2900	PF 1	3000.00	458.10	463.23	461.14	463.61	0.000245	4.97	603.31	222.92	0.41
Channel	2850	PF 1	3000.00	457.60	462.74	461.24	463.55	0.000521	7.22	415.32	168.05	0.58
Channel	2750		Culvert									
Channel	2640	PF 1	3000.00	455.59	462.07	458.95	462.52	0.011957	5.38	557.46	183.64	0.37
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Channel	2100	PF 1	3000.00	454.78	460.34		460.48	0.006864	3.05	1006.36	275.43	0.27
Channel	2050	PF 1	3000.00	454.70	460.11		460.21	0.003838	2.56	1191.75	275.37	0.21
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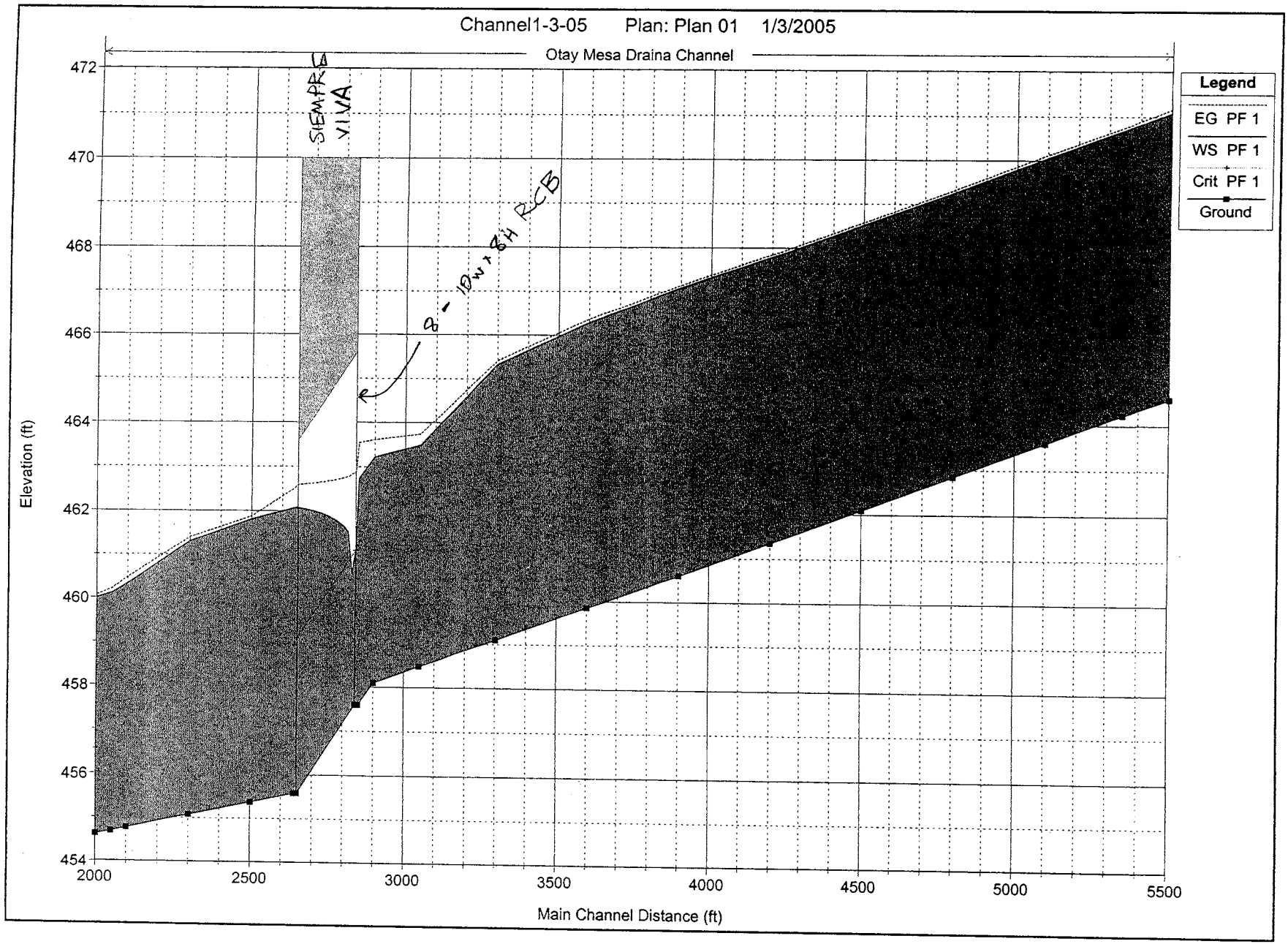
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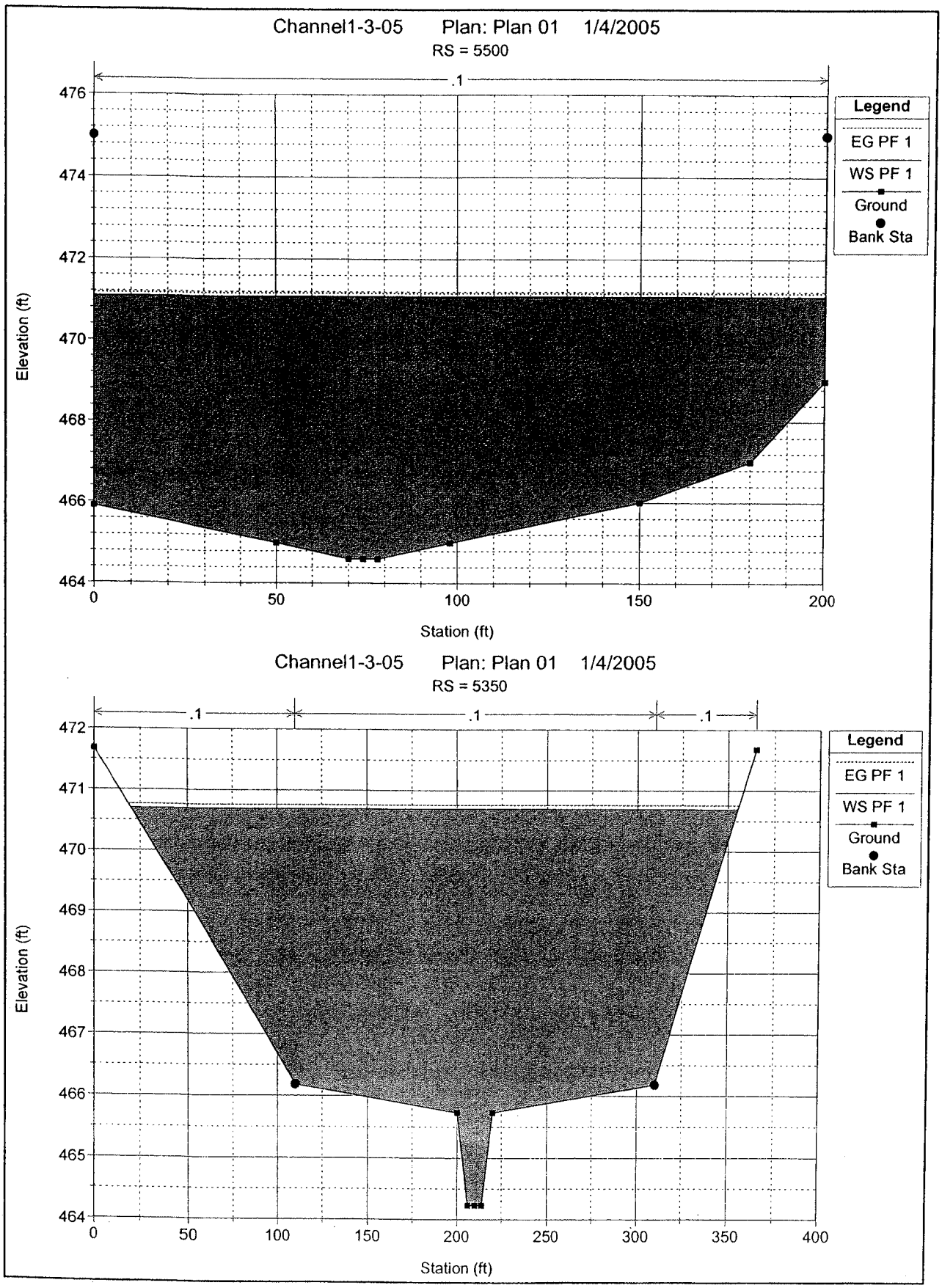
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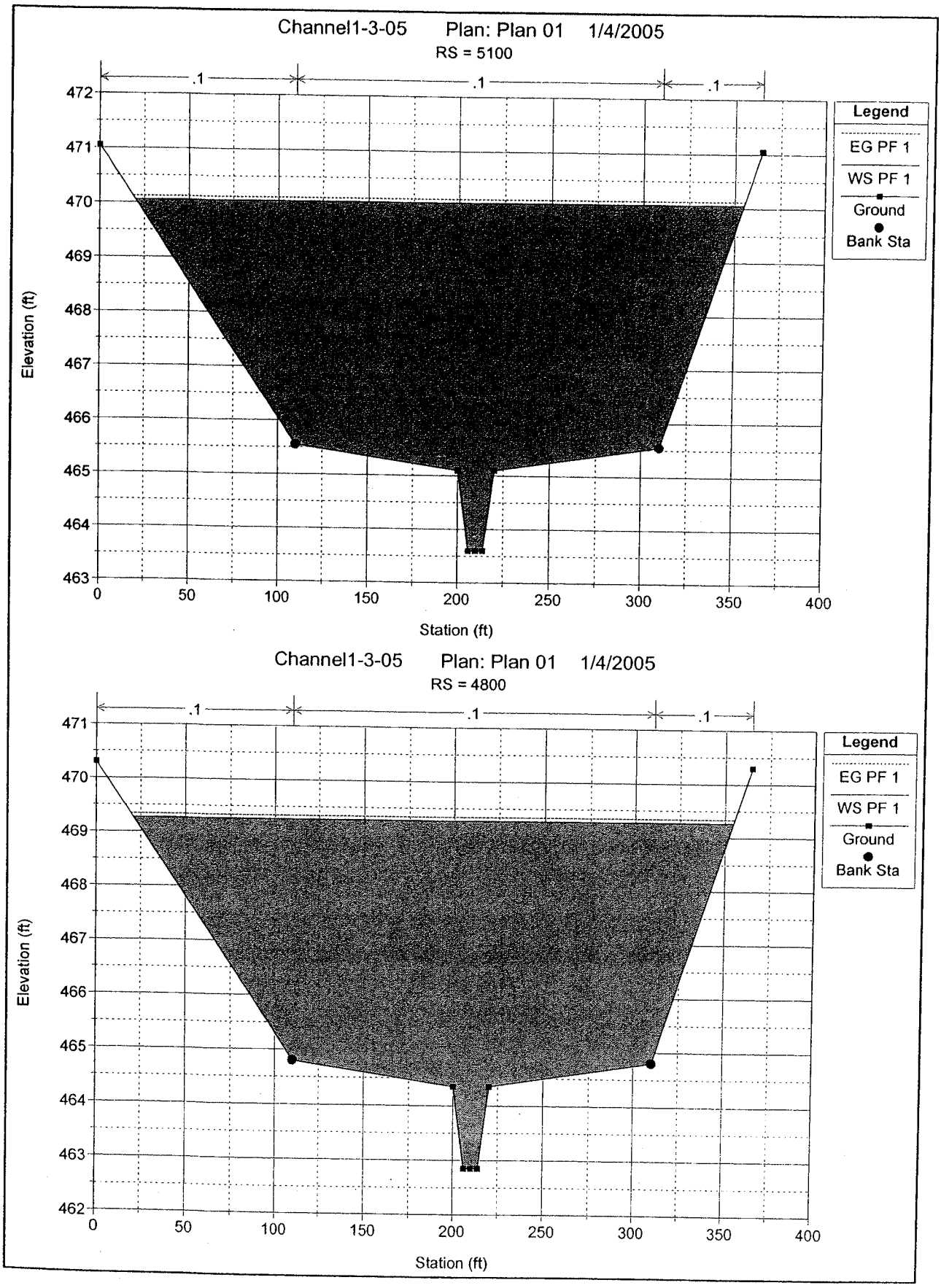
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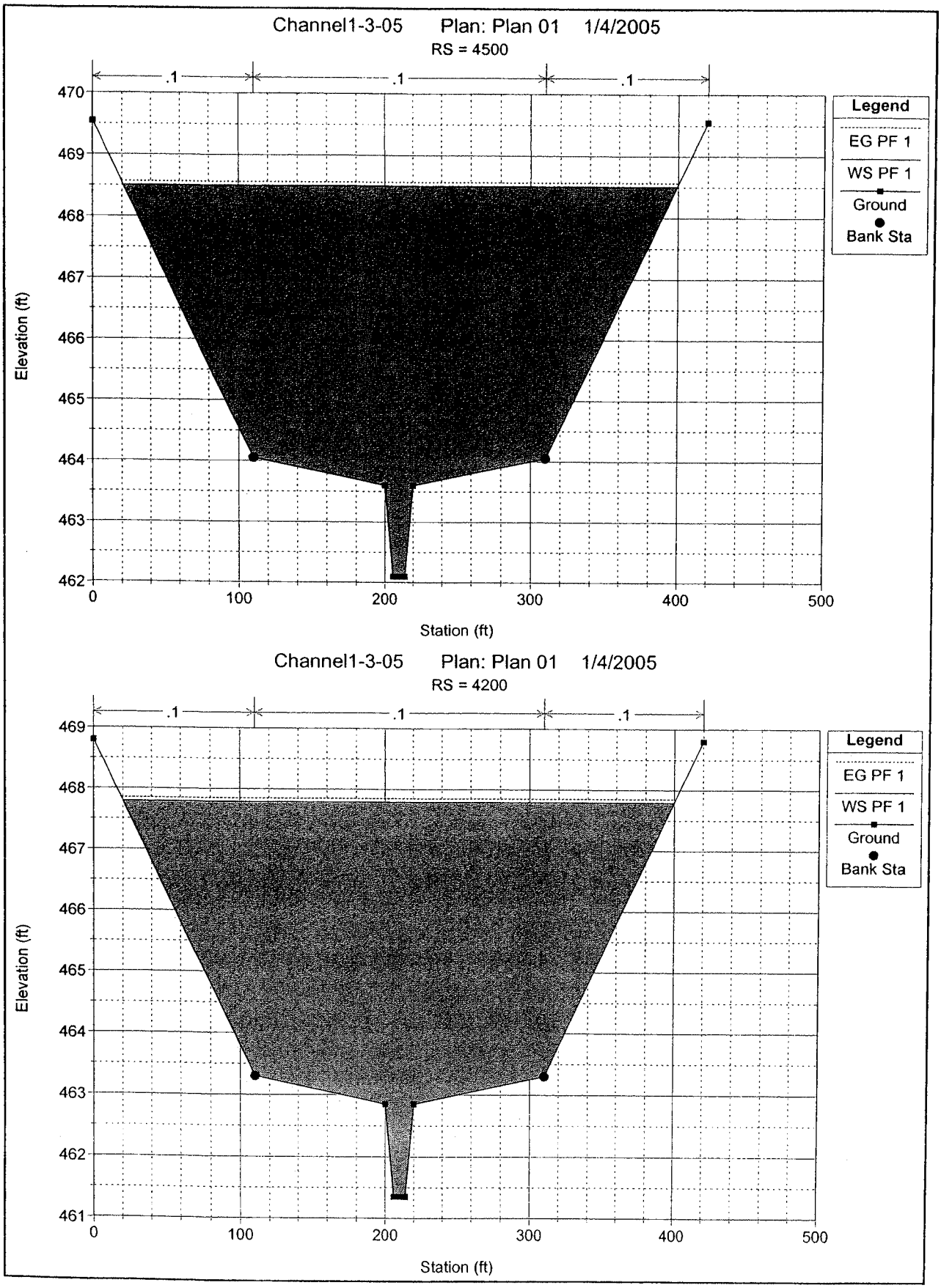
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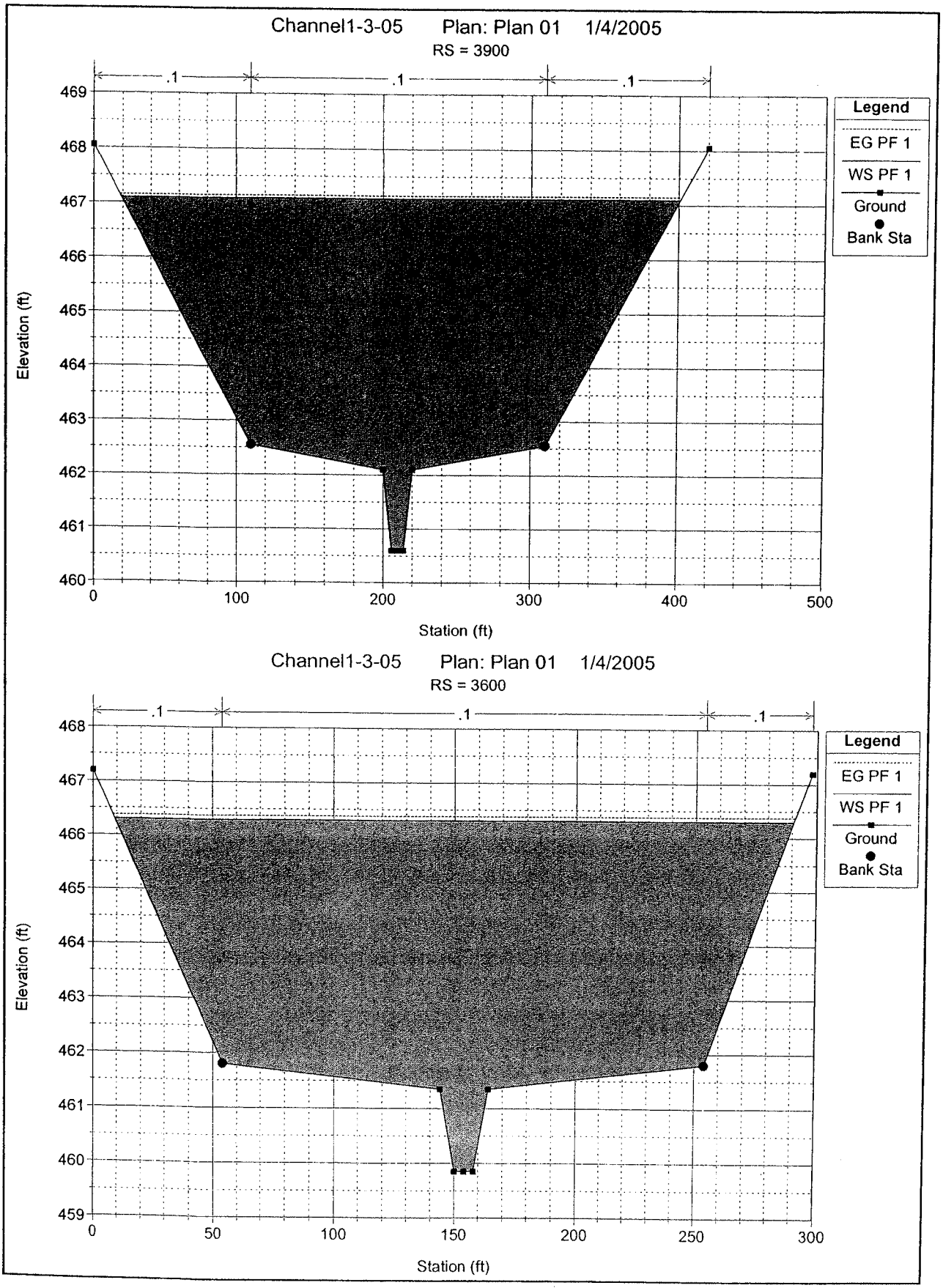
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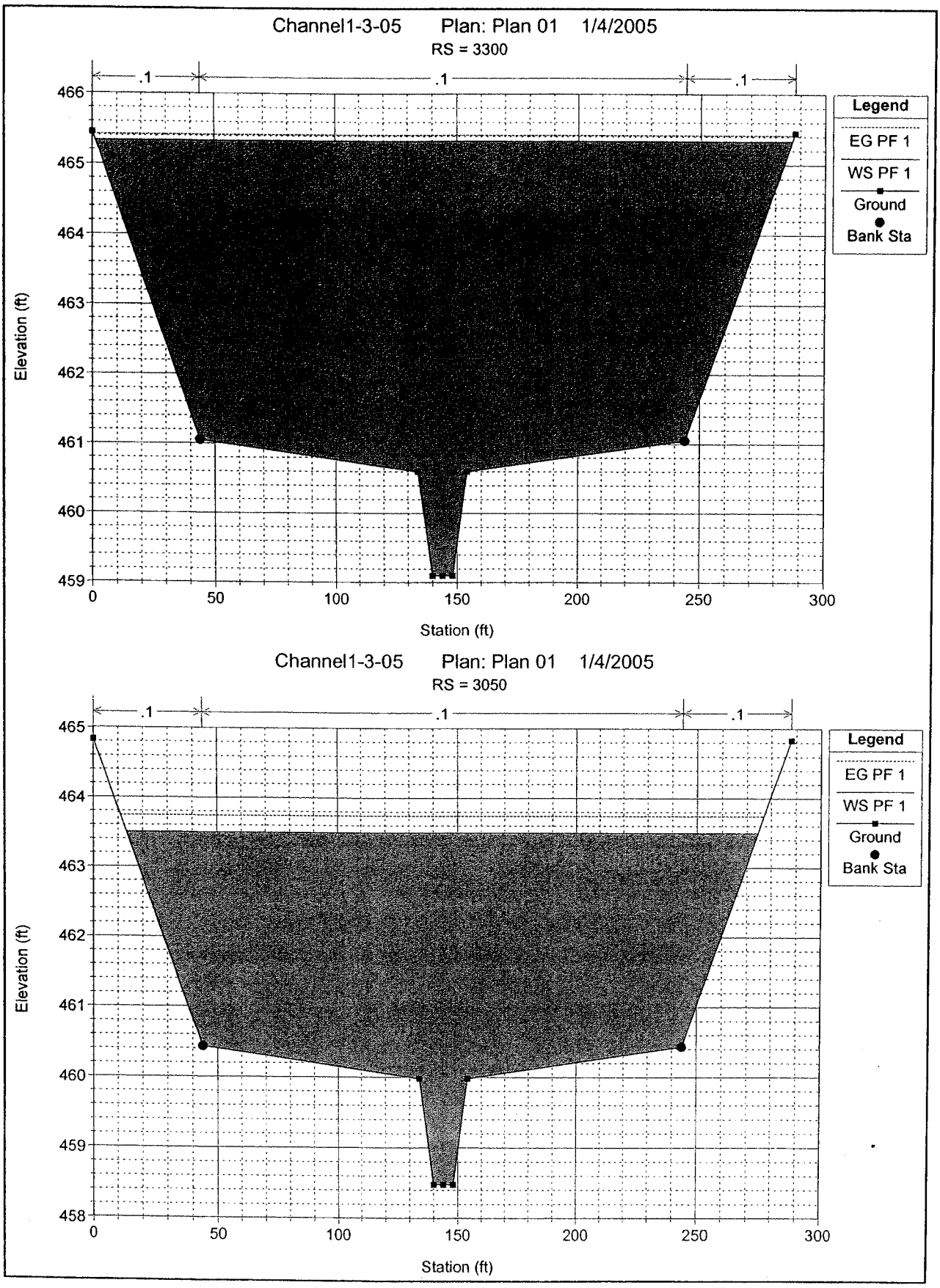
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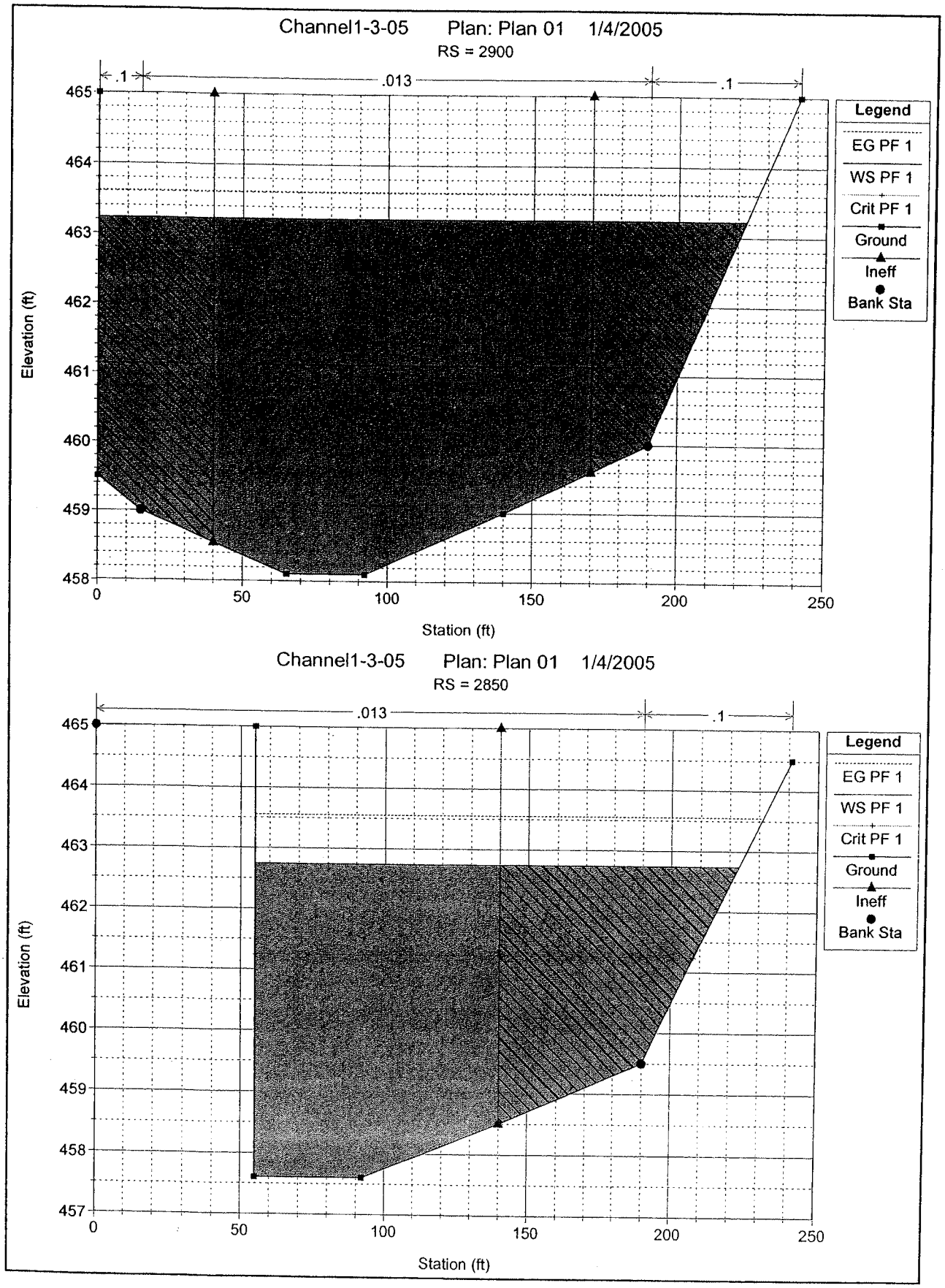
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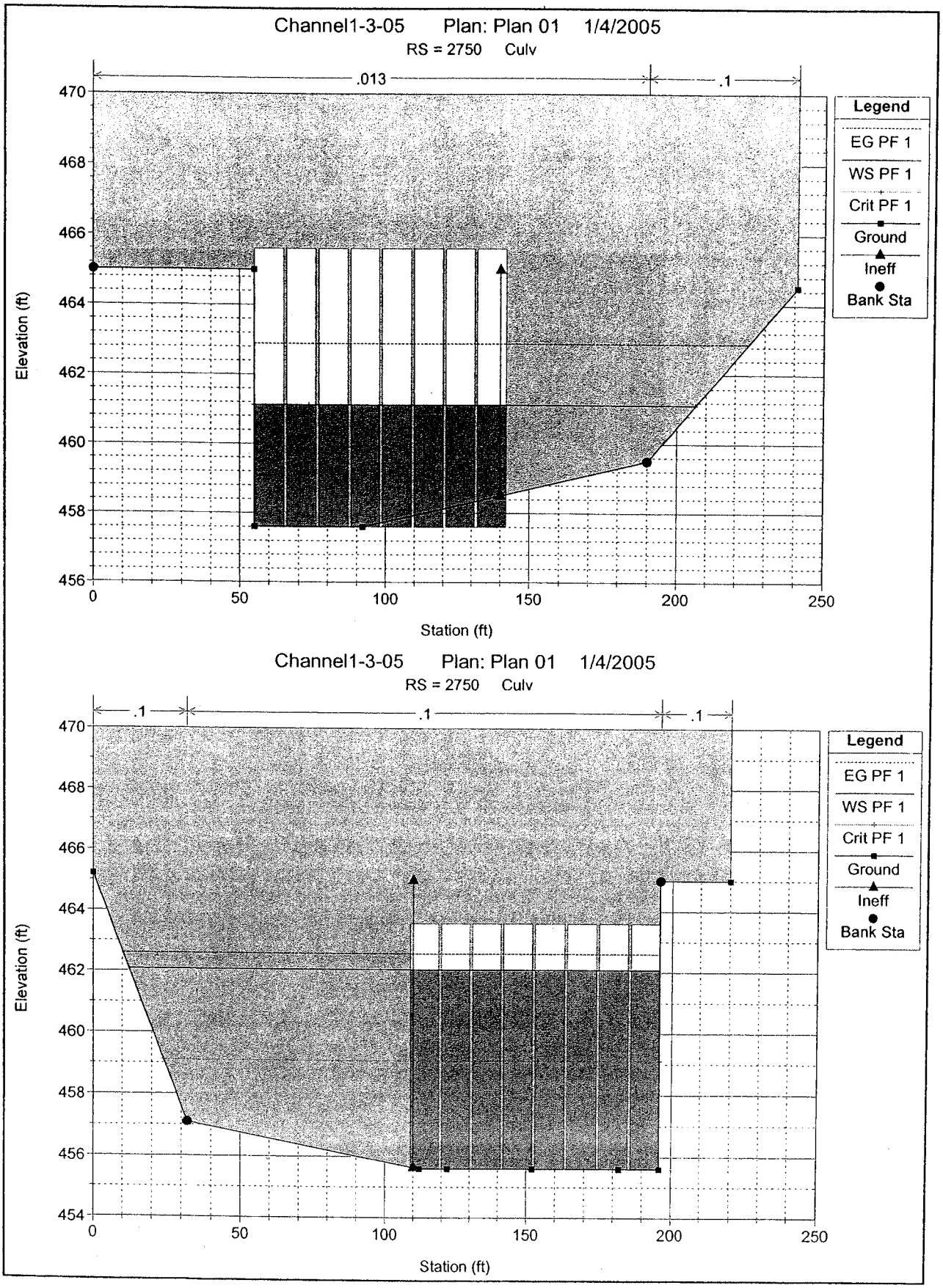
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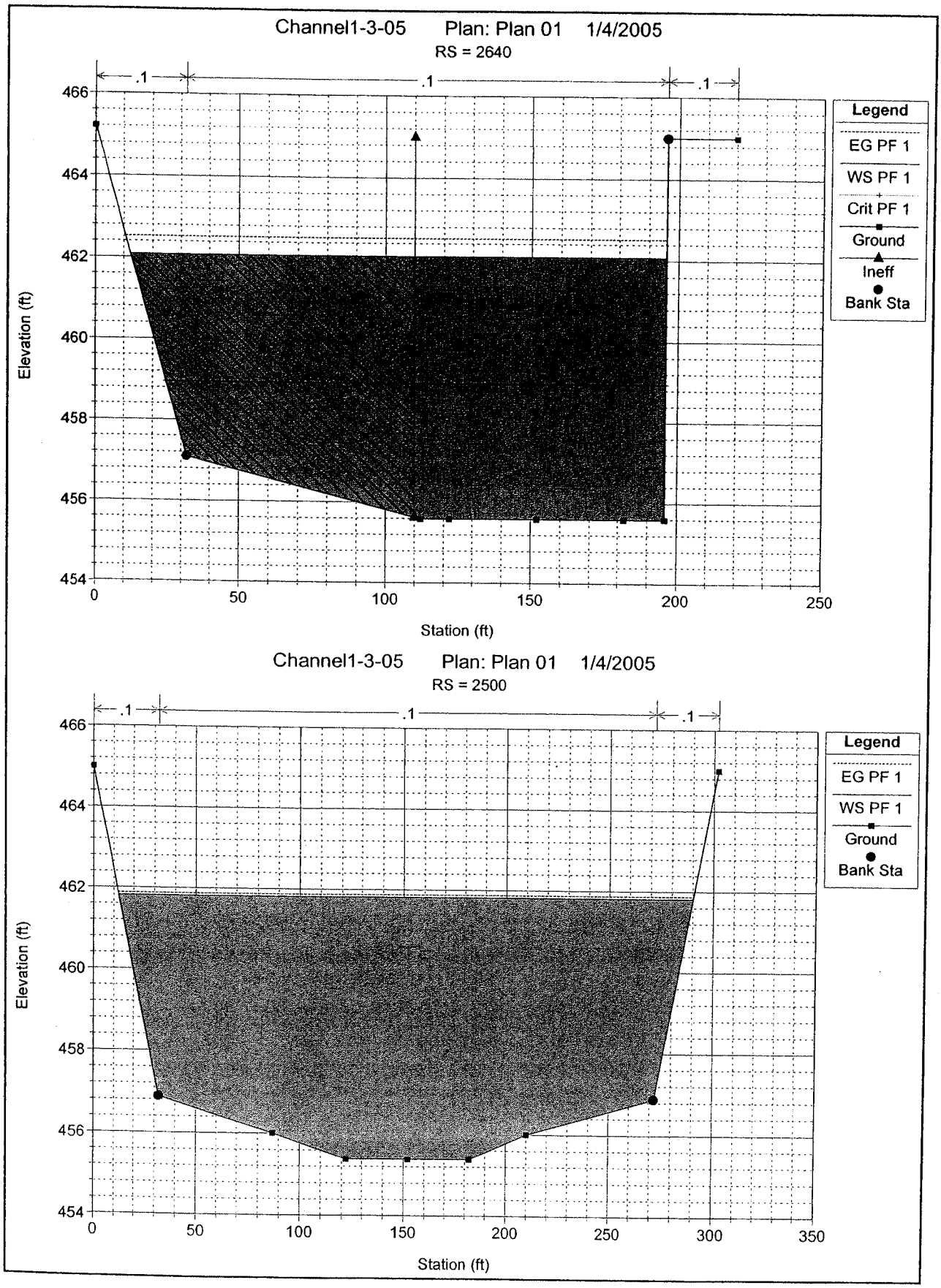
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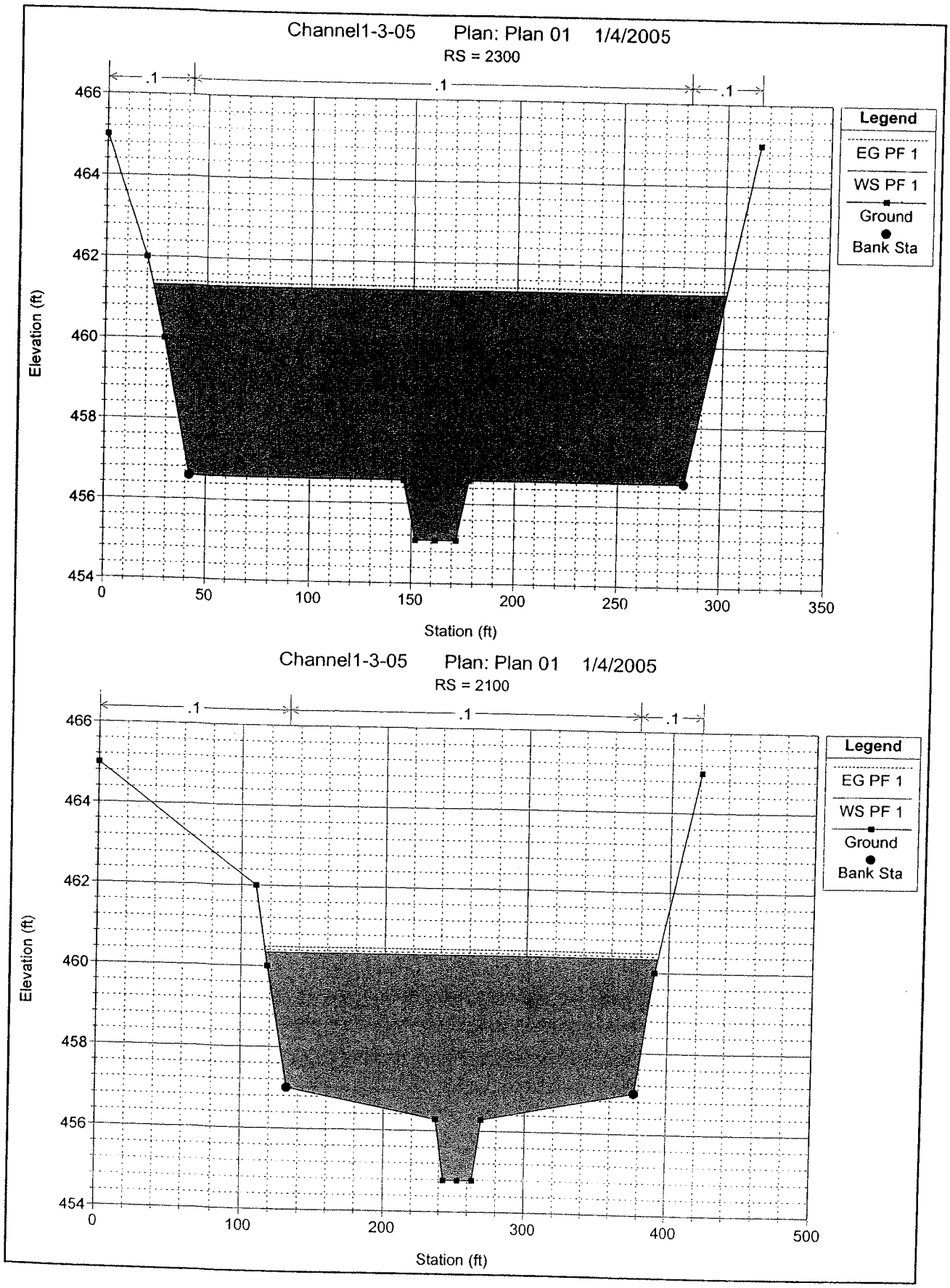
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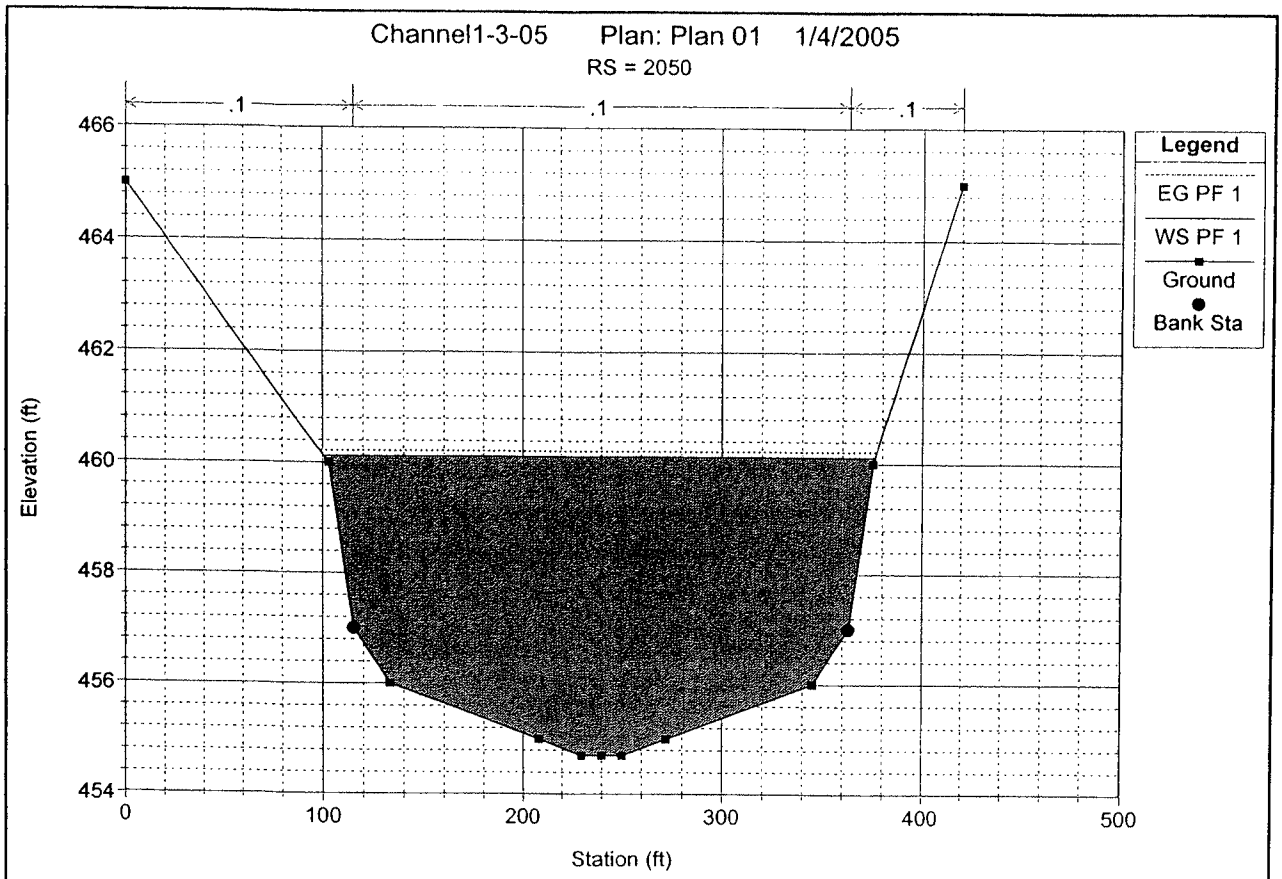
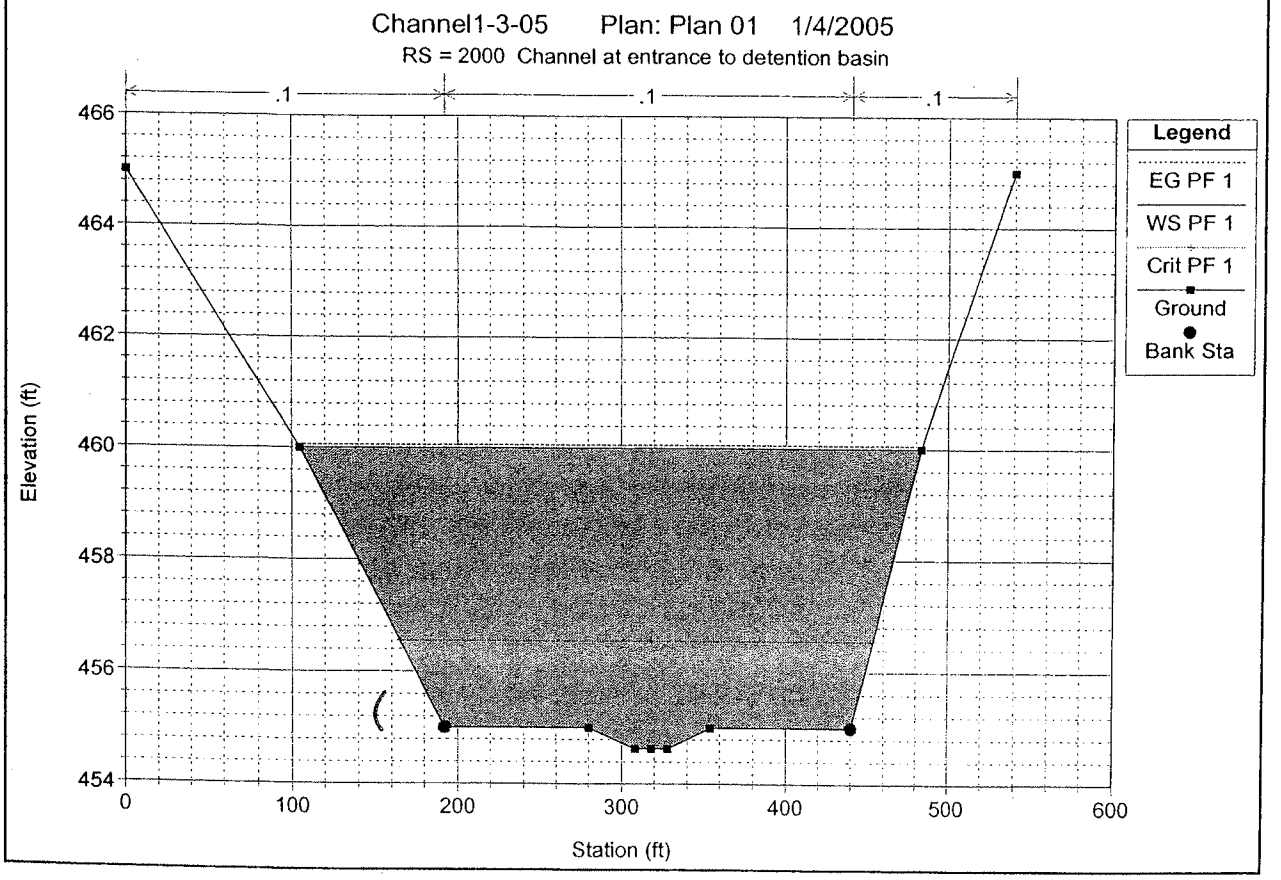
100
200
300
400
500
Station (ft)
Legend
EG PF 1
WS PF 1
Ground
Bank Sta


Channel1-3-05 Plan: Plan 01 1/4/2005
RS = 2050
.1
.1
.1
Legend
EG PF 1
WS PF 1
Ground
Bank Sta
Elevation (ft)
466
464
462
460
458
456
454
0
100
200
300
400
500
Station (ft)


Channel1-3-05 Plan: Plan 01 1/4/2005
RS = 2000 Channel at entrance to detention basin
.1
.1
.1
Legend
EG PF 1
WS PF 1
Crit PF 1
Ground
Bank Sta
Elevation (ft)
466
464
462
460
458
456
454
0
100
200
300
400
500
600
Station (ft)

Worksheet
Worksheet for Trapezoidal Channel

Project Description	
Worksheet	Trapezoidal Channel - 1
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Discharge

Input Data		
Mannings Coefficient	0.045	
Slope	0.006150	ft/ft
Depth	4.00	ft
Left Side Slope	1.50	H : V
Right Side Slope	1.50	H : V
Bottom Width	50.00	ft

Results		
Discharge	1,331.30	cfs
Flow Area	224.0	ft²
Wetted Perimeter	64.42	ft
Top Width	62.00	ft
Critical Depth	2.73	ft
Critical Slope	0.022466	ft/ft
Velocity	5.94	ft/s
Velocity Head	0.55	ft
Specific Energy	4.55	ft
Froude Number	0.55	
Flow Type	Subcritical	

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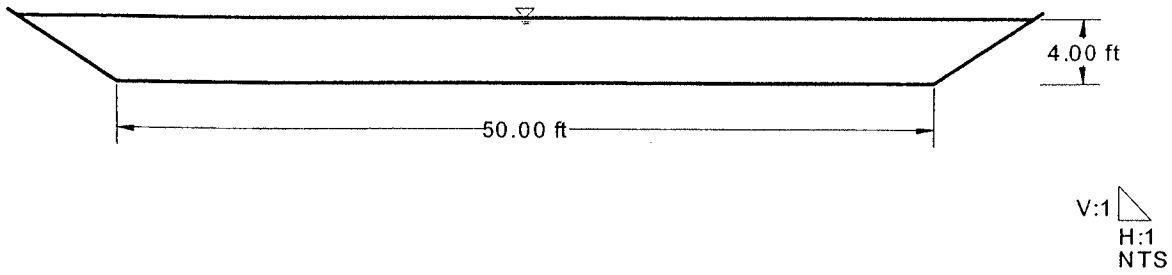
Kimley-Horn and Associates
37 Brookside Road Waterbury, CT 06708 USA (203) 755-1666

Cross Section
Cross Section for Trapezoidal Channel

Project Description	
Worksheet	Trapezoidal Channel - 1
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Discharge

Section Data		
Mannings Coefficient	0.045	
Slope	0.006150	ft/ft
Depth	4.00	ft
Left Side Slope	1.50	H : V
Right Side Slope	1.50	H : V
Bottom Width	50.00	ft
Discharge	1,331.30	cfs



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37 Brookside Road Waterbury, CT 06708 USA (203) 755-1666
Project Engineer: Michael Knapton

V. PROPOSED DRAINAGE FACILITIES

For most of the Mesa, drainage facilities are constructed as part of development or road projects, and include only facilities in the immediate vicinity of the projects. For the proposed future private development, no designs are available to show these future facilities. Caltrans has prepared plans for their SR-905 project, and those facilities are shown on the attached map.

The only Master Planned facility which needs to be constructed before development takes place is the Main Channel and Detention basin in the East Watershed. Details of this system are presented in Section VI.

VI. PROPOSED DRAINAGE ALTERNATIVES

The historical drainage on the Mesa, with its flat terrain and shallow swales for drainage paths, did not become a problem until development started taking place in the 1960s. This development started concentrating flows in culverts under roads and redefined some of the historical drainage paths. Some of the development solved problems in some areas, but impacted other areas by moving the problem downstream. One of these areas is the existing creek that parallels La Media Road and eventually crosses the border into Mexico. The frequent flooding along portions of this channel is a constraint to future development for some of the areas along the creek.

1. NO PROJECT

The alternative of doing nothing to improve the drainage along the main creek channel would prevent future development from taking place along portions of La Media Road. The existing creek is not deep enough to allow the adjacent properties to drain effectively. To provide continued access along the truck route during storms, if the channel is not constructed, the roads will need to be raised or alternative routes identified. The existing intersection of Airway Road and La Media Road floods after any significant precipitation. The adjacent roads are too low to allow significant flows to pass under them, so they flood frequently. If the roads are raised to allow more flow to pass under them, they will impact the already-developed adjacent property, parts of which would now be lower than the roads, creating even more difficult drainage issues for the properties.

2. CONCRETE CHANNEL

The 1999 Otay Mesa Drainage Study recommended a concrete channel from Otay Mesa Road to the Border Detention Basin. The recommended plan was a concrete channel along the east side of La Media Road until reaching Siempre Viva Road, where it crossed under La Media and followed on the north side of Siempre Viva to box culverts under Siempre Viva that connected to the Border Detention Basin. All of the concrete channel alternatives assumed that the existing creek with its habitat would continue to carry low flows. The 1999 cost for this alternative was $10.6 million, which would be approximately $14.9 million in 2005 dollars without land acquisition.

3. LA MEDIA CHANNEL AND BORDER DETENTION BASIN

The largest watershed on the Mesa is the East Watershed, which covers an area at 6.78 square miles (4,340 Acres). All of the flow from this watershed collects at a concentration point at a large culvert where it crosses the border with Mexico and flows under the airport access road and airport runway before flowing into the Tijuana River.

This portion at the Mesa is extremely flat, and the adjacent properties can not effectively drain into the existing small creek channel without raising the elevations of the roads and developments near the creek. To allow for future development and to accommodate runoff from proposed future projects, a new channel is required with inverts from 3 to 5 feet below the existing creek channel.

The proposed channel has a bottom width that varies from 240 feet at the new border detention basin to 200 feet from north of Siempre Viva Road to the Airway Road/La Media Road intersection. The side slopes will vary between 4:1 to 10:1. Heavy riparian vegetation will be allowed to grow in the channel and no annual maintenance will be required. Once the vegetation has matured, maintenance of dead or fallen trees may be required every few years. There will be a 12 foot wide access road on each bank. The Channel will contain the 100 year flood flow with mature vegetation growth.

From the Airway Road/La Media Road intersection, a 35 foot wide concrete channel along the east side of La Media Road will connect with the proposed Caltrans culverts which will be constructed with SR 905. The RCB culverts under the intersection will need to accommodate existing utilities in both roads, which may impact the intersection and the utilities.

The Border Detention Basin will be designed to attenuate peak flows from 5 year to 100 year storms. The outlet structure will be less than six feet high, and will not be under the jurisdiction of the State of California DSOD. The design of the outlet structure will be prepared with final plans for the project. The Detention Basin will be approximately 1700' by 1500' and cover an area of approximately 58 acres.

Border Detention Basin

Area:	58 Acres
Max. Water Depth:	6.0 Feet
Max. Storage Volume:	308 AF

The basin will be graded to appear natural. Natural vegetation will be allowed to grow in the basin and no annual maintenance will be required. A low-flow stream will be created through the basin. A Maintenance Assessment District may be created for maintaining the channel and detention basin.

The basin and channel will require the removal of approximately 915,000 CY of soil. It is assumed that this export will be used on adjacent properties to raise the building pad grades thereby limiting the haul distance. A preliminary cost estimate was prepared which reflects both the construction costs and the land acquisition costs. A Property Ownership Map which shows the ownership within the East Watershed is attached.

La Media Channel and Border Detention Basin

Preliminary Opinion of Probable Construction Cost

2/8/2005

Kimley-Horn and Associates

Construction Items

Item No.	Description	Quantity	Units	Unit Price	Cost
1	Excavation	822,500	CY	$2	$1,645,000
2	Airway Road culvert (6~5'wx5'h)	300	CY	$1,500	$450,000
3	La Media/Airway Road intersection culvert (6~10'wx6'h)	1,500	CY	$1,500	$2,250,000
4	Siempre Viva Road culvert (8~10'wx8'h)	1,490	CY	$1,500	$2,235,000
5	Detention Basin Outlet Structure	1	LS	$100,000	$100,000
6	Traffic Control	1	LS	$100,000	$100,000
7	Utility Relocation	1	LS	$150,000	$150,000
8	Street Repair	1	LS	$50,000	$50,000
9	Erosion Control	1	LS	$50,000	$50,000
10	Revegetation	1	LS	$600,000	$600,000
		Subtotal			$7,630,000
		Contingency	20%		$1,526,000
		Total			$9,156,000

Land Acquisition

1	Land Acquisition (outside MHPA)*	2,610,000	SF	$4	$10,440,000
2	Land Acquisition (inside MHPA)**	1,820,000	SF	$1	$1,820,000
		Subtotal			$12,260,000
		Contingency	20%		$2,452,000
		Total			$14,712,000

Total Cost (Construction and Land Acquisition) $23,868,000

Notes: * Includes area of detention basin and channel south of Siempre Viva

** Includes entire area within MHPA boundary

*** Estimate does not include engineering, environmental, geotechnical, surveying, etc.

K:\095407000\Excel\[cost estimate.xls]Sheet1

VII. RECOMMENDED DRAINAGE DESIGN CRITERIA

Since the five watershed areas on the Mesa flow in every direction except east, they flow into different watersheds with different constraints and impacts. The runoff from the five watersheds will have different criteria for design of drainage facilities.

West Perimeter Watershed

This watershed consists of smaller Mesa-top watersheds with a total area of approximately 254 acres that drain to the west to three separate creeks in canyons and gullies. These creeks are carried under the SD&AE and Trolley tracks and through San Ysidro in buried storm drain systems. The storm drains under the tracks have hydraulic capacities of 30 cfs (18" RCP) and 125 cfs (36" RCP) based on the San Ysidro Boulevard Area Master Drainage plan prepared by BSI Consultants, February 15, 1996. Sub-basins OT3-7 and OT3-8 combine downstream into a single creek that flows to the 36" RCP. The current study estimates 140 cfs (Q100) will flow off of the Mesa into this sub-basin. This study does not address the capacity of the downstream system or include the hydrologic analysis for areas to the west of the Mesa, but clearly the 125 cfs capacity of the existing system will be exceeded. This area will need to be addressed in more detail during design of the upstream tributary development. Detention Basins are recommended which will reduce peak flows in the sub-basin to minimize impacts on the downstream system. These detention basins will reduce the peak, 50-year, and 100-year flow to predevelopment levels. Because of the unstable soils in this area, care should be taken that the proposed detention basins and relocated drainage facilities do not contribute to an increase in the risk of slides through increased saturation of the soil.

West Watershed

The West Watershed consists of smaller Mesa-top watersheds that drain into the tributary canyons of Spring Canyon. All of the flow from the watershed flows into Mexico at the Spring Canyon concentration point. Detention basins will be required to reduce the post-development peak flows to predevelopment levels for the 50-year and 100-year storm. If the detention basins concentrate flows at the upper edge of canyons, care must be taken to ensure that erosion potential is not increased downstream.

East Watershed

The East Watershed flows to Mexico at a single concentration point between Britannia and La Media roads. Requirements for the control of peak runoff from development in this watershed already exist. The "Notice" dated August 7, 1987 (page 2), sets criteria for detention basins and for storm drain sizing. As part of the future storm drain project in this watershed, a single detention basin will be constructed at the border. The construction of this basin will eliminate the need for individual on-site detention basins for subsequent development.

North Perimeter Watershed

These small watersheds along the northern edge of the Mesa flow into small canyons that flow into the Otay River. There are no peak flow attenuation requirements for flows from these watersheds. There may be water quality issues with the Otay River, and there may be erosion issues from storm drains on the Mesa. Only approximately 14 acres of Neighborhood 6 are in this watershed.

VIII. STORM WATER QUALITY REQUIREMENTS

Because of problems related to the poor water quality of storm water runoff from urban conveyance systems, the City requires that storm water Best Management Practices (BMPs) be constructed for all new projects. The storm water discharge contains pollution such as chemicals, trash, sediment, bacteria, metals, oil and grease. Construction projects which add impervious areas and change drainage patterns increase the discharge of these pollutants.

The Municipal Storm Water National Pollutant Discharge Elimination System Permit (NPDES Municipal Permit), approved February 21, 2001 by the San Diego Regional Water Quality Control Board (RWQCB), requires the City to implement regulations for constructing storm water BMPs for development projects.

In 2003, as part of the San Diego Municipal Code, the City published "Storm Water Standards – A Manual for Construction & Permanent Storm Water Best Management Practices Requirements." This manual is the reference document for all of the storm water issues encountered in development, including BMPs. Included in this report are Appendix C – Example Permanent Storm Water Best Management Practices, and the Storm Water Requirements Applicability Checklist from the City's Manual. Before preparing a drainage study, the "Storm Water Requirements Applicability Checklist" is completed. This checklist is used to determine the priority level of the project. Most of the projects on the Mesa will require Priority Project Permanent Storm Water BMPs and High Priority Construction Storm Water BMPs.

All projects subject to the priority permanent BMP requirements must include a "Water Quality Technical Report." From the manual, the report will include:

1. A drainage study report prepared by a civil engineer, hydrologist, or hydrogeologist registered in the State of California, with experience in the science of stream and river generated surface features (i.e., fluvial geomorphology) and water resources management, satisfactory to the City Engineer. The report shall consider the project area's location (from the larger watershed perspective), topography, soil and vegetation conditions, percent impervious area, natural and infrastructure drainage features, and any other relevant hydrologic and environmental factors to be protected specific to the project area's watershed.
2. A field reconnaissance to observe and report on downstream conditions, including undercutting erosion, slope stability, vegetative stress (due to flooding, erosion, water quality degradation, or loss of water supplies) and the area's susceptibility to erosion or habitat alteration as a result of any future upstream development.
3. A hydrologic analysis to include rainfall runoff characteristics from the project area including at a minimum, peak runoff, time of concentration, and detention volume (if appropriate). These characteristics shall be developed for the two-year and ten-year frequency, six-hour or 24-hour, type B storm for the coastal areas of San Diego County. The largest peak flow should be included in the report. The report shall also report the project's conditions of concern based on the hydrologic and downstream conditions discussed above. Where downstream conditions of concern have been identified, the drainage study shall establish that pre-project hydrologic conditions that minimize impacts on those downstream conditions of concern would be either improved or maintained by the proposed project, satisfactory to the City Engineer, by incorporating the permanent BMP requirements.

Appendix D of the Manual includes detailed guidelines for the Water Quality Technical Report.

There are numerous alternative permanent BMPs that can be used for each project. The alternatives include Site Design BMPs, Source Control BMPs, and Treatment Control BMPs. The Site Design BMPs are primary ways to reduce storm water runoff through means such as increased pervious areas, increased infiltration, use of natural channels, and appropriate landscaping. All of these except dry wells are applicable to the Mesa. Source Control BMPs are meant to control pollutants at their source before they enter storm water, and are all applicable to the Mesa. Treatment Control BMPs treat the storm water before it leaves the property, and include natural methods such as biofilters, detention basins, wetlands, and porous pavement, and mechanical methods such as filters and separators. The one Treatment Control BMP that is not applicable to the Mesa is infiltration, which is not very effective on the Mesa because of the clay soils.

Most of Otay Mesa drains to the south across the border with Mexico and eventually into the Tijuana River. A small portion flows north into the Otay River, and the far western part of the Mesa flows to the west through San Ysidro and then into the Tijuana River. The Tijuana River has been identified by the 2002 Clean Water Act as a "Section 303(d) Water Quality Limited" river. The pollutants of concern which are included in the attached pages from the USEPA, need to be listed, and the new development project's potential impacts on these pollutants need to be included in the project's drainage report.

Recommended Storm Water Policies

1. **Apply water quality protection measures to land development projects during project design, permitting, construction, and operations in order to minimize the quantity of runoff generated on-site, the disruption of natural water flows and the contamination of storm water runoff.**

    a. Increase on-site infiltration, and preserve, restore or incorporate natural drainage systems into site design
    b. Reduce the amount of impervious surfaces through selection of materials, site planning, and narrowing street widths where possible.
    c. Increase the use of natural vegetation and landscaping in drainage design.
    d. Avoid conversion of areas particularly susceptible to erosion and sediment loss (e.g.: steep slopes), and where unavoidable, enforce regulations that minimize these impacts.
    e. Avoid land use, site development, and zoning regulations that limit impacts on, and protect the natural integrity of topography, drainage systems, and water bodies.
    f. Maintain landscape design standards that minimize the use of pesticides and herbicides.
    g. Enforce maintenance requirements in development permit conditions.

2. **Require construction contractors to comply with accepted storm water pollution prevention planning practices for all projects.**

    a. Minimize the amount of graded land surface exposed to erosion and enforce control ordinances
    b. Continue routine inspection practices to check for proper erosion control methods and housekeeping practices during construction.
    c. Ensure that contractors are aware of and implement urban runoff control programs.

3. **Encourage measures to promote the proper collection and disposal of pollutants at the source, rather than allowing them to enter the storm drain system.**

    a. Promote the provision of used oil recycling and/or hazardous waste recycling facilities and drop-off locations.
    b. Follow up on complaints of illegal discharges and accidental spills to storm drains, waterways, and canyons.

REFERENCES

This Water Quality Technical Report incorporates, by reference, the appropriate elements of the following documents and plans required by local; State or Federal agencies.

1. Municipal Storm Water National Pollutant Discharge Elimination System (NPDES) Permit

2. City of San Diego Storm Water Standards

3. Drainage Study for the Otay Mesa Community Plan

4. California Stormwater BMP Handbook, "Extended Detention Basin – TC-22" New Development and Redevelopment, January 2003

5. California Stormwater BMP Handbook, "Vegetated Swale – TC-30" New Development and Redevelopment, January 2003

Attachment 6
Geotechnical and Groundwater Investigation Report

Attach project's geotechnical and groundwater investigation report. Refer to Appendix C.4 to determine the reporting requirements.

DUE DILIGENCE GEOTECHNICAL INVESTIGATION

THE COLLECTION AT CACTUS
NORTHEAST CORNER OF AIRWAY ROAD AND CACTUS ROAD
SAN DIEGO, CALIFORNIA

GEOCON
INCORPORATED

GEOTECHNICAL
ENVIRONMENTAL
MATERIALS

PREPARED FOR

JPI
SAN DIEGO, CALIFORNIA

MAY 18, 2023
PROJECT NO. G2338-42-02

Project No. G2338-42-02
May 18, 2023

JPI
11988 El Camino Real, Suite 200
San Diego, California 92130

Attention: Mr. Conner Kloeppel

Subject: DUE DILIGENCE GEOTECHNICAL INVESTIGATION
THE COLLECTION AT CACTUS
NORTHEAST CORNER OF AIRWAY ROAD AND CACTUS COURT
SAN DIEGO, CALIFORNIA

Dear Mr. Kloeppel:

In accordance with your request, we have performed a due diligence geotechnical investigation for the subject project. The accompanying report presents the findings of our study and our conclusions and recommendations pertaining to geotechnical aspects of developing the property as proposed.

It is our opinion that the site can be developed as currently proposed, provided the recommendations of this report are followed.

Should you have questions regarding this report, or if we may be of further service, please contact the undersigned at your convenience.

Very truly yours,

GEOCON INCORPORATED

Lilian E. Rodriguez
RCE 83227

Rodney C. Mikesell
GE 2533

Rupert S. Adams
CEG 2561

LER:RCM:RSA:arm

(e-mail) Addressee

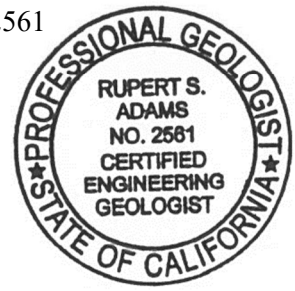


TABLE OF CONTENTS

1. PURPOSE AND SCOPE 1

2. SITE AND PROJECT DESCRIPTION 2

3. SOIL AND GEOLOGIC CONDITIONS 2
   - 3.1 Topsoil (Unmapped) 3
   - 3.2 Terrace Deposits-Clay Member (Qtc) 3
   - 3.3 Terrace Deposits-Sand/Gravel Member (Qtg) 3
   - 3.4 Otay Formation (To) 4

4. GROUNDWATER 4

5. GEOLOGIC HAZARDS 4
   - 5.1 Geologic Hazard Category 4
   - 5.2 Ground Rupture 4
   - 5.3 Seismicity 5
   - 5.4 Liquefaction Potential 5
   - 5.5 Tsunamis and Seiches 5
   - 5.6 Subsidence 5
   - 5.7 Flooding 5

6. CONCLUSIONS AND RECOMMENDATIONS 6
   - 6.1 General 6
   - 6.2 Excavation and Soil Characteristics 6
   - 6.3 Temporary Excavations 7
   - 6.4 Grading 8
   - 6.5 Slopes 9
   - 6.6 Seismic Design Criteria – 2022 California Building Code 10
   - 6.7 Foundation and Concrete Slabs-On-Grade Recommendations 12
   - 6.8 Retaining Walls 18
   - 6.9 Lateral Loading 20
   - 6.10 Storm Water Management 21
   - 6.11 Site Drainage and Moisture Protection 23
   - 6.12 Grading and Foundation Plan Review 23

LIMITATIONS AND UNIFORMITY OF CONDITIONS

MAPS AND ILLUSTRATIONS
- Figure 1, Geologic Map

APPENDIX A
- PREVIOUS FIELD INVESTIGATIONS

APPENDIX B
- LABORATORY TESTING

APPENDIX C
- RECOMMENDED GRADING SPECIFICATIONS

LIST OF REFERENCES

DUE DILIGENCE GEOTECHNICAL INVESTIGATION

1. PURPOSE AND SCOPE

This report contains the results of our due diligence geotechnical investigation for the proposed Collections at Cactus development located northeast of the Airway Road and Cactus Road intersection in San Diego, California (see Vicinity Map).

Vicinity Map

The purpose of this due diligence geotechnical investigation is to evaluate general site geology and soil conditions, identify geotechnical constraints that could impact development of the property, and provide geotechnical recommendations for remedial grading, shallow foundations, and retaining walls.

To aid in the preparation of this report, we reviewed the following plans and geotechnical report:

1. *Conceptual Site Plan,* prepared by Summa Architects, undated.

2. *Geotechnical Investigation, Otay Central Village, Planning Areas 10-13 and 17, Airway Road and Cactus Road, San Diego, California*, prepared by Geocon Incorporated, dated April 9, 2019 (Project No. G2338-42-01).

The scope of this investigation included: a review of readily available published and unpublished geologic literature, a review of the referenced geotechnical report, engineering analysis, and preparation of this report. We previously excavated 3 exploratory borings and 16 exploratory trenches to a maximum depth of 16 feet below ground surface, performed infiltration testing, and performed laboratory testing of soil samples. The locations of the previous exploratory borings, trenches, and infiltration tests are shown on the Geologic Map, Figure 1. We used a CAD file of the conceptual site plan to generate Figure 1. Logs of the exploratory trenches, borings, infiltration test-borings, and a detailed discussion of the field investigations are presented in Appendix A. Appendix B presents details of the laboratory tests and a summary of the test results, and Appendix C presents recommended grading specifications.

The conclusions and recommendations presented herein are based on our analysis of the data obtained from the exploratory field investigations, laboratory test results, and our experience with similar soil and geologic conditions on this and adjacent properties.

2. SITE AND PROJECT DESCRIPTION

The project site is approximately 40 acres in size, bounded by the 905 freeway on the north, Airway Road on the south, Cactus Road on the west, and a partially graded vacant lot to the east. An automobile/truck service yard and several single-story residential homes are located west of the site along Cactus Road.

The property is characterized by gently sloping topography (Figure 1), draining from the southeast to the northwest to a drainage channel running parallel to the east-bound lanes of the 905 freeway. Existing site elevations range from approximately 494 to 515 feet Mean Sea Level (MSL). Based on a review of historical aerial photographs, previous land uses include cultivation of small orchards and arable farming.

Based on the conceptual site plan (Reference 1), the proposed development consists of constructing multi-story residential buildings including townhomes, stacked flats, and apartments. The project will also have a 3.5-acre park, parking lots, and a biofiltration basins for storm water management. Based on preliminary grading information, planned grading will result in cuts and fills of approximately 5 feet or less from existing grades to construct planned sheet grade elevations across the site.

3. SOIL AND GEOLOGIC CONDITIONS

We encountered topsoil underlain by Pleistocene terrace deposits during our field investigation. Descriptions of these geologic units are described herein and shown on the exploratory trench and boring logs in Appendix A.

3.1 Topsoil (Unmapped)

Topsoil blankets the entire site and is generally composed of very soft to stiff, sandy clay and loose, silty to clayey sand. The topsoil thickness ranges from approximately one to four feet. Topsoil is compressible in its present condition and will require removal and decompaction.

3.2 Terrace Deposits-Clay Member (Qtc)

The Pleistocene-age upper Terrace Deposit clay member (Qtc) consists of a highly expansive clay, encountered in all exploratory trenches except TP-1 and TP-2, located in the northwest corner of the site (Figure 1). The clay member is approximately two to greater than 14 feet thick, consisting of firm to hard, damp to moist, grayish brown to olive brown, clay, silty clay, and sandy clay. The base of the clay member was not found along the south side of the site in trenches TP-12 through TP-14.

Expansion testing performed on this site and other adjacent sites indicates the upper Terrace Deposit clay member has highly expansive characteristics. The clay will require remedial grading in the form of removal and replacement with *low* expansive soils within the upper 5 feet of planned finish grade. Trenches excavated on adjacent properties found that the clay is occasionally interbedded with dense, cemented silty to clayey sandstone. Where cemented zones are encountered, excavations may generate oversize material requiring special handling and placement.

3.3 Terrace Deposits-Sand/Gravel Member (Qtg)

The Pleistocene-age lower terrace member (Qtg) underlies the upper clay member, and consists of medium dense to very dense, damp to moist, reddish- to yellowish-brown, medium dense to dense, Clayey and Silty Sand with varying amounts of cobble. This unit is massive to weakly stratified, with occasional discontinuous cobble and gravel lenses. The surrounded gravel and cobble clasts range from 3- to 18-inches in diameter, and are derived from volcanic, metasedimentary and granitic rocks. Cobble clast size generally increases with depth and may exceed 18-inches in deeper excavations.

Excavation of the Qtg member will require moderate to heavy effort with conventional heavy-duty earth-moving equipment. Larger than normal excavators may be required to excavate deeper utility trenches.

Typically, in the Otay area, the upper clay deposit (Qtc) is removed, and the underlying sandy/gravel unit (Qtg) is mined to provide select capping material. The clay soils are then replaced and compacted in the mined excavation at depths of at least five feet below planned finish grade. Deeper burial depths may be required if subterranean building levels are planned.

3.4 Otay Formation (To)

The Otay Formation underlies the terrace deposits and is generally composed of dense to hard, light olive to gray-brown, horizontally interbedded clayey siltstones and silty fine-grained sandstone. The Otay Formation was not encountered to the maximum explored depth of 16-feet below site grades; however, it may be encountered during site grading. The Otay Formation typically possess low to moderate expansion, good shear strength characteristics, and is generally suitable for support of structural loads and/or fills in its present condition.

4. GROUNDWATER

We did not encounter groundwater in the trenches or borings during our field investigations. Based on the proposed improvements, we do not expect groundwater to have an adverse impact on the project; however, it is not uncommon for groundwater or seepage conditions to develop where none previously existed. Groundwater elevations are dependent on seasonal precipitation, irrigation, land use, among other factors, and vary as a result. Proper surface drainage will be important to the future performance of the project.

5. GEOLOGIC HAZARDS

5.1 Geologic Hazard Category

Based on our review of geologic literature and experience with the soil and geologic conditions in the general area, it is our opinion that known active, potentially active, or inactive faults are not located at the site. The site is not within a State of California Earthquake Fault Zone.

The site is described in City of San Diego (2008) as having Geologic Hazard Category 53; *Level or sloping terrane, unfavorable geologic structure, Low to moderate risk.*

5.2 Ground Rupture

The USGS (2019) and Kennedy & Tan (2008) show that there are no mapped Quaternary faults crossing or trending toward the property. The site is not located within a currently established Alquist-Priolo Earthquake Fault Zone (CEG, 2021a).

There are no active faults, potentially active faults, inactive faults, or activity unknown faults at the site or trending toward the site. The nearest active fault is the Rose Canyon Fault, which lies approximately 9 miles west of the site. The risk associated with ground rupture hazard is low.

5.3 Seismicity

Considerations important in seismic design include frequency and duration of motion and soil conditions underlying the site. Seismic design of structures should be evaluated in accordance with the California Building Code currently adopted by the City of San Diego. The risk associated with strong seismic ground motion hazard is high; however, the risk is no greater than that for the site vicinity.

5.4 Liquefaction Potential

The potential for liquefaction occurring within the site soils is considered to be very low due to the lack of a near surface groundwater table, and the density of the terrace deposits.

5.5 Tsunamis and Seiches

The site is not mapped within a State of California tsunami hazard zone (CGS, 2021b). The site is not located near a large body of water. The risk associated with flooding due to tsunami or seiche hazard is low.

5.6 Subsidence

Based on the subsurface soil conditions observed, the risk associated with ground subsidence is low.

5.7 Flooding

The site is not mapped in a Special Flood Hazard Area as defined by FEMA (2020). The risk of inundation hazard due to flooding is low.

6. CONCLUSIONS AND RECOMMENDATIONS

6.1 General

6.1.1 From a geotechnical engineering standpoint, it is our opinion that the site is suitable for the proposed development provided the recommendations presented herein are implemented in design and construction of the project.

6.1.2 The site is underlain by Pleistocene-age terrace deposits mantled by topsoil. Laboratory tests indicate the topsoil and the upper terrace deposit member (Qtc) exhibit *very high* expansion characteristics (EI greater than 130). Remedial will be required for the onsite topsoil and clayey portions of the old terrace deposits. The lower sandy portions of the terrace deposits (Qtg) are suitable for the support of the proposed loads or additional engineered fill.

6.1.3 We did not encounter groundwater during the field investigation. We expect excavations for the proposed improvements will be relatively shallow; therefore, we do not expect groundwater to have an adverse impact on the project as currently proposed.

6.1.4 The site is located approximately nine miles east of the Newport-Inglewood/Rose Canyon fault zone. Based on our review of available literature, active, potentially active, or presumed inactive faults do not cross the site.

6.1.5 With the exception of possible strong seismic shaking, we did not observe or know of significant geologic hazards that would adversely affect the proposed development.

6.1.6 The risks associated with soil liquefaction and flooding hazards are low.

6.1.7 The proposed structures can be supported on a shallow foundation system founded entirely on properly compacted fill soil.

6.1.8 Subsurface conditions observed may be extrapolated to reflect general soil/geologic conditions; however, some variations in subsurface conditions between trench and boring locations should be anticipated.

6.2 Excavation and Soil Characteristics

6.2.1 Excavation of the onsite soils should be possible with moderate to heavy effort using conventional, heavy-duty equipment during grading and trenching operations.

6.2.2 The soil encountered in our field investigation is considered to be both "expansive" (Expansion Index [EI] greater than 20) and "non-expansive" (EI of 20 and less) as defined by 2022 California Building Code (CBC) Section 1803.5.3. Table 6.2 presents soil classifications based on the expansion index.

TABLE 6.2
EXPANSION CLASSIFICATION BASED ON EXPANSION INDEX

Expansion Index (EI)	ASTM D 4829 Expansion Classification	2022 CBC Expansion Classification
0 – 20	Very Low	Non-Expansive
21 – 50	Low	Expansive
51 – 90	Medium	
91 – 130	High	
Greater Than 130	Very High	

6.2.3 We performed laboratory tests on samples of the site materials to evaluate the percentage of water-soluble sulfate content. Appendix B presents the results from the laboratory water-soluble sulfate content tests. The test results indicate that on-site materials at the locations tested possess "S0" sulfate exposure to concrete structures, as defined by 2016 CBC Section 1904 and ACI 318-14 Chapter 19. The presence of water-soluble sulfates is not a visually discernible characteristic. Therefore, other soil samples from the site could yield different concentrations. Additionally, over time landscaping activities (i.e. addition of fertilizers and other soil nutrients) may affect the concentration.

6.2.4 Geocon Incorporated does not practice in the field of corrosion engineering. Therefore, if improvements that could be susceptible to corrosion are planned, further evaluation by a corrosion engineer may be needed.

6.3 Temporary Excavations

6.3.1 Temporary excavations should be constructed in conformance with OSHA requirements. The on-site Terrace Deposits and proposed compacted fill should be considered Type B soil in accordance with OSHA requirements. In general, special shoring requirements will not be necessary if temporary excavations are less than 4 feet high. Temporary excavation depths greater than 4 feet should be laid back at an appropriate inclination or shored. The soils exposed in these excavations should not become saturated or allowed to dry. Surcharge loads should not be permitted within a distance equal to the depth of the excavation from the top of the excavation. The top of the excavation should be a minimum of 15 feet from the edge of existing improvements. Excavations steeper than those recommended or closer than 15 feet

from an existing surface improvement should be shored in accordance with applicable OSHA codes and regulations.

6.4 Grading

6.4.1 All grading should be performed in accordance with the *Recommended Grading Specifications* contained in Appendix C. Where the recommendations of Appendix C conflict with this section of the report, the recommendations of this section take precedence.

6.4.2 Prior to commencing grading, a preconstruction conference should be held at the site with the owner or developer, grading contractor, civil engineer, and geotechnical engineer in attendance. Special soil handling and/or the grading plans can be discussed at that time.

6.4.3 Grading should be performed in conjunction with the observation and compaction testing services of Geocon Incorporated. Fill soil should be observed on a full-time basis during placement and tested to check in-place dry density and moisture content.

6.4.4 Site preparation should begin with removal of all deleterious material and vegetation. The depth of removal should be such that material exposed in cut areas or soil to be used for fill is relatively free of organic matter. Deleterious material generated during stripping and/or site demolition should be exported from the site.

6.4.5 Abandoned utilities should be removed and the subsequent depressions and/or trenches backfilled with properly compacted fill as part of the remedial grading.

6.4.6 Compressible surficial soils (topsoil and weathered portion of Terrace Deposits) should be removed to firm natural ground and properly recompacted prior to placing structural fill and/or loading.

6.4.7 After removal of compressible soils, the upper portion of the Terrace Deposits – Clay Member should be removed to a depth of at least 5 feet below finish pad grade or 3 feet below the bottom of building footings, whichever results in a deeper excavation. The resulting excavation should be replaced with “low” to “medium” expansive soils (EI less than 90). The expansive clays should be placed and compacted to a depth no closer than 5 feet below finish subgrade elevation and 3 feet below building footings. Typically, this requires removal of the upper Terrace Deposit Clay, mining of the underlying sand and gravel, placing the clay at the base of the mined excavation and then utilizing the mined sand and gravel soils to construct the 5-foot cap of low expansive soil. Geocon Incorporated should be contacted if alternate recommendations, such as lime treatment of the expansive clay soils, is desired.

6.4.8 If grading results in a cut to fill transition within the sand and gravel Terrace Deposits, the cut portion of the pad should be undercut to a depth of at least 3 feet below pad grade, or 1 foot below the bottom of building footings, whichever results in a deeper excavation, are the undercut area replaced with "low" to "medium" expansive soils. All building pad undercuts should extend to at least 5 feet horizontally beyond the building pad limits.

6.4.9 Prior to placing fill, the upper 12 inches at the base of removals and areas to receive fill should be scarified, moisture conditioned as necessary and recompacted. Soils derived from onsite excavations are suitable for reuse as fill if free from vegetation, debris and other deleterious material. Fill lifts should be no thicker than will allow for adequate bonding and compaction. Fill, backfill, and scarified ground surfaces, should be compacted to a dry density of at least 90 percent of maximum dry density at or slightly above optimum moisture content, as determined in accordance with ASTM D 1557.

6.4.10. Oversize rock greater than 12 inches should be placed at least 5 feet below finish pad grade or 3 feet below the deepest utility, whichever is greater. Rock greater than 6 inches should not be placed in the upper 3 feet below building pad grade. Oversize rock that cannot be placed as recommended should be exported off site.

6.4.11 Imported fill should consist of granular soil with a *low* to *medium* expansion potential (EI of 50 or less), be is free of deleterious material or stones larger than 3 inches, and compacted as recommended above. Geocon Incorporated should be notified of the import soil source and should perform laboratory testing prior to its arrival at the site to evaluate its suitability as fill material.

6.5 Slopes

6.5.1 Fill slopes are proposed along the west side of Cactus Road to the northwest of the site. Fill slopes will have maximum heights on the order of 10 to 15 feet and inclined at 2:1 (horizontal to vertical) or flatter.

6.5.2 The outer 15 feet (or a distance equal to the height of the slope, whichever is less) of fill slopes should consist of properly compacted granular soil fill to reduce the potential for surface sloughing. All fill slopes should be track walked upon completion such that the fill soils are uniformly compacted to at least 90 percent relative compaction to the face of the finish slope.

6.5.3 All slopes should be planted, drained, and maintained to reduce erosion.

6.6 Seismic Design Criteria – 2022 California Building Code

6.6.1 Table 6.6.1 summarizes site-specific design criteria obtained from the 2022 California Building Code (CBC; Based on the 2021 International Building Code [IBC] and ASCE 7-16), Chapter 16 Structural Design, Section 1613 Earthquake Loads. We used SEAOC (2019) to calculate the seismic design parameters. The short spectral response uses a period of 0.2 second. We evaluated the Site Class based on the discussion in Section 1613.2.2 of the 2022 CBC and Table 20.3-1 of ASCE 7-16. The values presented herein are for the risk-targeted maximum considered earthquake (MCE_R). Sites designated as Site Class D, E and F may require additional analyses if requested by the project structural engineer and client.

TABLE 6.6.1
2022 CBC SEISMIC DESIGN PARAMETERS

Parameter	Value	2022 CBC Reference
Site Class	D	Section 1613.2.2
MCE_R Ground Motion Spectral Response Acceleration – Class B (short), S_S	0.752g	Figure 1613.2.1(1)
MCE_R Ground Motion Spectral Response Acceleration – Class B (1 sec), S_1	0.276g	Figure 1613.2.1(3)
Site Coefficient, F_A	1.199	Table 1613.2.3(1)
Site Coefficient, F_V	2.048	Table 1613.2.3(2)
Site Class Modified MCE_R Spectral Response Acceleration (short), S_{MS}	0.902g	Section 1613.2.3 (Eqn 16-20)
Site Class Modified MCE_R Spectral Response Acceleration – (1 sec), S_{M1}	0.565g	Section 1613.2.3 (Eqn 16-21)
5% Damped Design Spectral Response Acceleration (short), S_{DS}	0.601g	Section 1613.2.4 (Eqn 16-22)
5% Damped Design Spectral Response Acceleration (1 sec), S_{D1}	0.377g	Section 1613.2.4 (Eqn 16-23)

6.6.2 Using the code-based values presented in this Table 6.6.1, in lieu of a performing a ground motion hazard analysis, requires the exceptions outlined in ASCE 7-16 Section 11.4.8 be followed by the project structural engineer. Per Section 11.4.8 of ASCE/SEI 7-16, a ground motion hazard analysis should be performed for projects for Site Class "E" sites with Ss greater than or equal to 1.0g and for Site Class "D" and "E" sites with S_1 greater than 0.2g. Section 11.4.8 also provides exceptions which indicates that the ground motion hazard analysis may be waived provided the exceptions are followed.

6.6.3 Table 6.6.2 presents the mapped maximum considered geometric mean (MCE_G) seismic design parameters for projects located in Seismic Design Categories of D through F in accordance with ASCE 7-16.

TABLE 6.6.2
ASCE 7-16 PEAK GROUND ACCELERATION

Parameter	Value	ASCE 7-16 Reference
Mapped MCE_G Peak Ground Acceleration, PGA	0.328g	Figure 22-9
Site Coefficient, F_{PGA}	1.272	Table 11.8-1
Site Class Modified MCE_G Peak Ground Acceleration, PGA_M	0.417g	Section 11.8.3 (Eqn 11.8-1)

6.6.4 Conformance to the criteria in Tables 6.6.1 and 6.6.2 for seismic design does not constitute any kind of guarantee or assurance that significant structural damage or ground failure will not occur in the event of a large earthquake. The primary goal of seismic design is to protect life, not to avoid all damage, since such design may be economically prohibitive.

6.6.5 The project structural engineer and architect should evaluate the appropriate Risk Category and Seismic Design Category for the planned structures. The values presented herein assume a Risk Category II and a Seismic Design Category D. Table 6.6.3 presents a summary of the risk categories in accordance with ASCE 7-16.

TABLE 6.6.3
ASCE 7-16 RISK CATEGORIES

Risk Category	Building Use	Examples
I	Low risk to Human Life at Failure	Barn, Storage Shelter
II	Nominal Risk to Human Life at Failure (Buildings Not Designated as I, III or IV)	Residential, Commercial and Industrial Buildings
III	Substantial Risk to Human Life at Failure	Theaters, Lecture Halls, Dining Halls, Schools, Prisons, Small Healthcare Facilities, Infrastructure Plants, Storage for Explosives/Toxins
IV	Essential Facilities	Hazardous Material Facilities, Hospitals, Fire and Rescue, Emergency Shelters, Police Stations, Power Stations, Aviation Control Facilities, National Defense, Water Storage

6.7 Foundation and Concrete Slabs-On-Grade Recommendations

6.7.1 The foundation recommendations herein are for proposed one- to three-story residential structures. The foundation recommendations have been separated into three categories based on either the maximum and differential fill thickness or Expansion Index. The foundation category criteria are presented in Table 6.7.1. Final foundation categories for individual lots will be presented in our as-graded report once fill thickness, differential fill thickness, and expansion index of finish grade soils are known.

TABLE 6.7.1
FOUNDATION CATEGORY CRITERIA

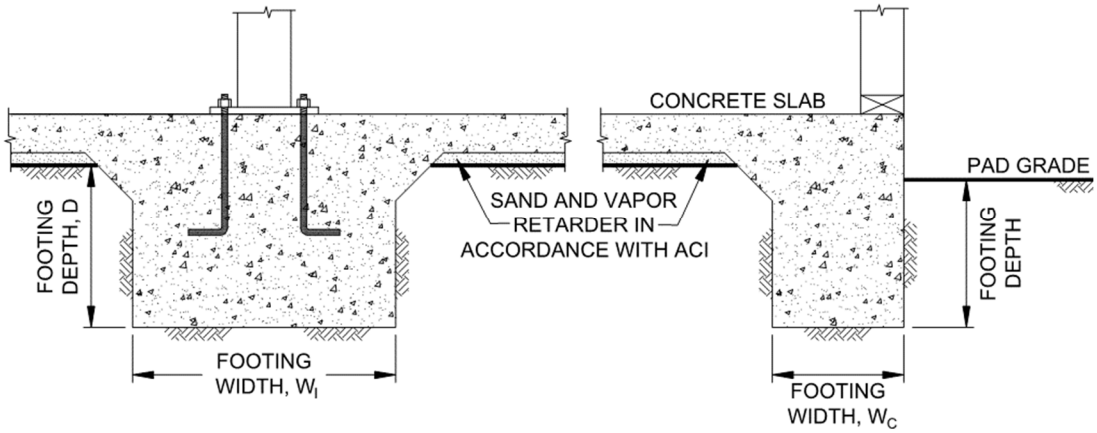
Foundation Category	Maximum Fill Thickness, T (feet)	Differential Fill Thickness, D (feet)	Expansion Index (EI)
I	T<20	--	EI≤50
II	20≤T<50	10≤D<20	50<EI≤90
III	T≥50	D≥20	90<EI≤130

6.7.2 Table 6.7.2 presents minimum foundation and interior concrete slab design criteria for conventional foundation systems.

TABLE 6.7.2
CONVENTIONAL FOUNDATION RECOMMENDATIONS BY CATEGORY

Foundation Category	Minimum Footing Embedment Depth, D (inches)	Minimum Continuous Footing Reinforcement	Minimum Footing Width (Inches)
I	12	Two No. 4 bars, one top and one bottom	12 – Continuous, W_C 24 – Isolated, W_I
II	18	Four No. 4 bars, two top and two bottom	
III	24	Four No. 5 bars, two top and two bottom	

6.7.3 The foundations should be embedded in accordance with the recommendations herein and the Wall/Column Footing Dimension Detail. The embedment depths should be measured from the lowest adjacent pad grade for both interior and exterior footings. Footings should be deepened such that the bottom outside edge of the footing is at least 7 feet horizontally from the face of the slope (unless designed with a post-tensioned foundation system as discussed herein).



Wall/Column Footing Dimension Detail

6.7.4 The proposed structures can be supported on a shallow foundation system founded in compacted fill. Table 6.7.3 provides a summary of the foundation design recommendations.

TABLE 6.7.3
SUMMARY OF FOUNDATION RECOMMENDATIONS

Parameter	Value
Allowable Bearing Capacity	2,000 psf
Bearing Capacity Increase	500 psf per Foot of Depth
	300 psf per Foot of Width
Maximum Allowable Bearing Capacity	3,500 psf
Estimated Total Settlement	1 Inch
Estimated Differential Settlement	½ Inch in 40 Feet

6.7.5 The bearing capacity values presented herein are for dead plus live loads and may be increased by one-third when considering transient loads due to wind or seismic forces.

6.7.6 The concrete slab-on-grades should be designed in accordance with Table 6.7.4.

TABLE 6.7.4
CONVENTIONAL SLAB-ON-GRADE RECOMMENDATIONS BY CATEGORY

Foundation Category	Minimum Concrete Slab Thickness (inches)	Interior Slab Reinforcement	Typical Slab Underlayment
I	4	6 x 6 - 10/10 welded wire mesh at slab mid-point	3 to 4 Inches of Sand/Gravel/Base
II	4	No. 3 bars at 24 inches on center, both directions	
III	5	No. 3 bars at 18 inches on center, both directions	

6.7.7 Slabs that may receive moisture-sensitive floor coverings or may be used to store moisture-sensitive materials should be underlain by a vapor retarder. The vapor retarder design should be consistent with the guidelines presented in the American Concrete Institute's (ACI) *Guide for Concrete Slabs that Receive Moisture-Sensitive Flooring Materials* (ACI 302.2R-06). The vapor retarder used should be specified by the project architect or developer based on the type of floor covering that will be installed and if the structure will possess a humidity controlled environment.

6.7.8 The bedding sand thickness should be determined by the project foundation engineer, architect, and/or developer. However, we should be contacted to provide recommendations if the bedding sand is thicker than 6 inches. It is common to see 3 inches and 4 inches of sand below the concrete slab-on-grade for 5-inch and 4-inch thick slabs, respectively, in the southern California area.

6.7.9 The foundation design engineer should provide appropriate concrete mix design criteria and curing measures to assure proper curing of the slab by reducing the potential for rapid moisture loss and subsequent cracking and/or slab curl. We suggest that the foundation design engineer present the concrete mix design and proper curing methods on the foundation plans. It is critical that the foundation contractor understands and follows the recommendations presented on the foundation plans.

6.7.10 As an alternative to the conventional foundation recommendations, consideration should be given to the use of post-tensioned concrete slab and foundation systems for the support of the proposed structures. The post-tensioned systems (foundation dimensions and embedment depths, slab thickness and steel placement) should be designed by a structural engineer experienced in post-tensioned slab design and design criteria of the Post-Tensioning Institute (PTI) DC 10.5-12 *Standard Requirements for Design and Analysis of Shallow Post-Tensioned*

Concrete Foundations on Expansive Soils or *WRI/CRSI Design of Slab-on-Ground Foundations*, as required by the 2022 California Building Code Section 1808.6.2. Although this procedure was developed for expansive soil conditions, it can also be used to reduce the potential for foundation distress due to differential fill settlement. The post-tensioned design should incorporate the geotechnical parameters presented in Table 6.7.5 for the particular Foundation Category designated. The parameters presented in Table 6.7.5 are based on the guidelines presented in the PTI DC 10.5 design manual.

TABLE 6.7.5
POST-TENSIONED FOUNDATION SYSTEM DESIGN PARAMETERS

Post-Tensioning Institute (PTI) DC 10.5 Design Parameters	Foundation Category		
	I	II	III
Thornthwaite Index	-20	-20	-20
Equilibrium Suction	3.9	3.9	3.9
Edge Lift Moisture Variation Distance, e_M (feet)	5.3	5.1	4.9
Edge Lift, y_M (inches)	0.61	1.10	1.58
Center Lift Moisture Variation Distance, e_M (feet)	9.0	9.0	9.0
Center Lift, y_M (inches)	0.30	0.47	0.66

6.7.11 The foundations for the post-tensioned slabs should be embedded in accordance with the recommendations of the structural engineer. If a post-tensioned mat foundation system is planned, the slab should possess a thickened edge with a minimum width of 12 inches and extend below the clean sand or crushed rock layer.

6.7.12 If the structural engineer proposes a post-tensioned foundation design method other than PTI DC 10.5:

- The deflection criteria presented in Table 6.7.5 are still applicable.
- Interior stiffener beams should be used for Foundation Categories II and III.
- The width of the perimeter foundations should be at least 12 inches.
- The perimeter footing embedment depths should be at least 12 inches, 18 inches and 24 inches for foundation categories I, II, and III, respectively. The embedment depths should be measured from the lowest adjacent pad grade.

6.7.13 Our experience indicates post-tensioned slabs may be susceptible to excessive edge lift, regardless of the underlying soil conditions. Placing reinforcing steel at the bottom of the perimeter footings and the interior stiffener beams may mitigate this potential. The structural

engineer should design the foundation system to reduce the potential of edge lift occurring for the proposed structures.

6.7.14 During the construction of the post-tension foundation system, the concrete should be placed monolithically. Under no circumstances should cold joints form between the footings/grade beams and the slab during the construction of the post-tension foundation system unless designed by the structural engineer.

6.7.15 Category I, II, or III foundations may be designed for an allowable soil bearing pressure of 2,000 pounds per square foot (psf) (dead plus live load). This bearing pressure may be increased by one-third for transient loads due to wind or seismic forces. The estimated maximum total and differential settlement for the planned structures due to foundation loads is 1 inch and ½ inch, respectively.

6.7.16 Isolated footings outside of the slab area, if present, should have the minimum embedment depth and width recommended for conventional foundations for a particular Foundation Category. The use of isolated footings, which are located beyond the perimeter of the building and support structural elements connected to the building, are not recommended for Category III. Where this condition cannot be avoided, the isolated footings should be connected to the building foundation system with grade beams. In addition, consideration should be given to connecting patio slabs, which exceed 5 feet in width, to the building foundation to reduce the potential for future separation to occur.

6.7.17 Interior stiffening beams should be incorporated into the design of the foundation system in accordance with the PTI design procedures.

6.7.18 Special subgrade presaturation is not deemed necessary prior to placing concrete; however, the exposed foundation and slab subgrade soil should be moisture conditioned, as necessary, to maintain a moist condition as would be expected in any such concrete placement.

6.7.19 Where buildings or other improvements are planned near the top of a slope 3:1 (horizontal:vertical) or steeper, special foundation and/or design considerations are recommended due to the tendency for lateral soil movement to occur.

- For fill slopes less than 20 feet high or cut slopes regardless of height, footings should be deepened such that the bottom outside edge of the footing is at least 7 feet horizontally from the face of the slope.
- When located next to a descending 3:1 (horizontal:vertical) fill slope or steeper, the foundations should be extended to a depth where the minimum horizontal distance is

equal to H/3 (where H equals the vertical distance from the top of the fill slope to the base of the fill soil) with a minimum of 7 feet but need not exceed 40 feet. The horizontal distance is measured from the outer, deepest edge of the footing to the face of the slope. A post-tensioned slab and foundation system or mat foundation system can be used to reduce the potential for distress in the structures associated with strain softening and lateral fill extension. Specific design parameters or recommendations for either of these alternatives can be provided once the building location and fill slope geometry have been determined.

- If swimming pools are planned, Geocon Incorporated should be contacted for a review of specific site conditions.

- Swimming pools located within 7 feet of the top of cut or fill slopes are not recommended. Where such a condition cannot be avoided, the portion of the swimming pool wall within 7 feet of the slope face be designed assuming that the adjacent soil provides no lateral support. This recommendation applies to fill slopes up to 30 feet in height, and cut slopes regardless of height. For swimming pools located near the top of fill slopes greater than 30 feet in height, additional recommendations may be required and Geocon Incorporated should be contacted for a review of specific site conditions.

- Although other improvements, which are relatively rigid or brittle, such as concrete flatwork or masonry walls, may experience some distress if located near the top of a slope, it is generally not economical to mitigate this potential. It may be possible, however, to incorporate design measures which would permit some lateral soil movement without causing extensive distress. Geocon Incorporated should be consulted for specific recommendations.

6.7.20 The recommendations of this report are intended to reduce the potential for cracking of slabs and foundations due to expansive soil (if present), differential settlement of fill soil with varying thicknesses. However, even with the incorporation of the recommendations presented herein, foundations, stucco walls, and slabs-on-grade placed on such conditions may still exhibit some cracking due to soil movement and/or shrinkage. The occurrence of concrete shrinkage cracks is independent of the supporting soil characteristics. Their occurrence may be reduced by limiting the slump of the concrete, proper concrete placement and curing, and by the placement of crack control joints at periodic intervals, in particular, where re-entrant slab corners occur.

6.7.21 Concrete slabs should be provided with adequate crack-control joints, construction joints and/or expansion joints to reduce unsightly shrinkage cracking. The design of joints should consider criteria of the American Concrete Institute (ACI) when establishing crack-control spacing. Additional steel reinforcing, concrete admixtures and/or closer crack control joint spacing should be considered where concrete-exposed finished floors are planned.

6.7.22 Geocon Incorporated should be consulted to provide additional design parameters as required by the structural engineer.

6.8 Retaining Walls

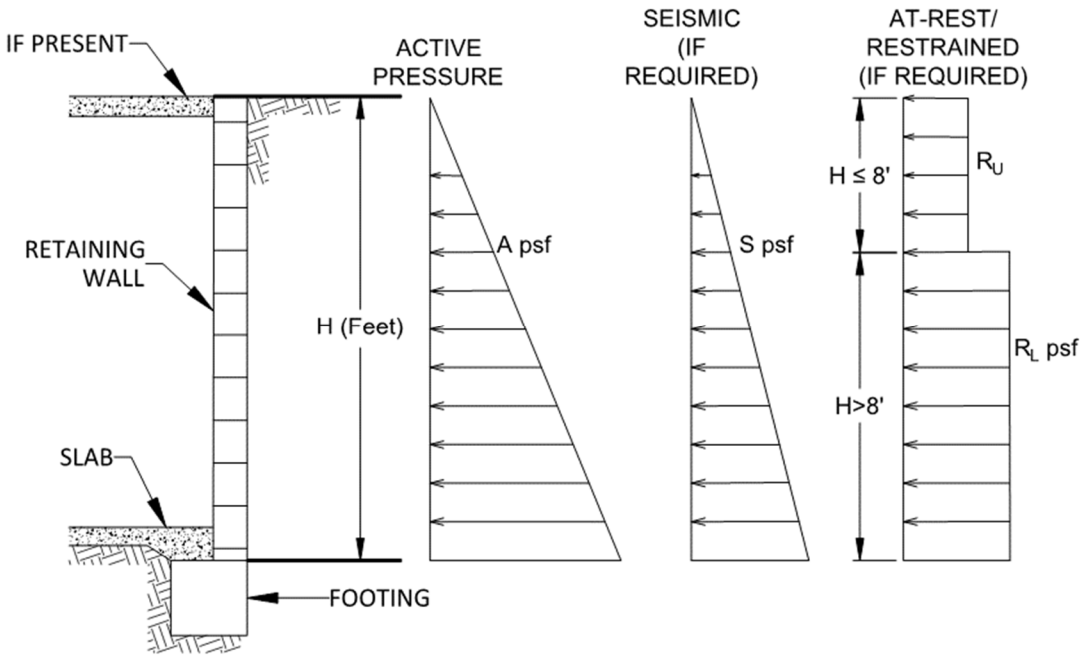
6.8.1 Retaining walls, if planned, should be designed using the values presented in Table 6.8.1. Soil with an expansion index (EI) of greater than 90 should not be used as backfill soil behind retaining walls.

TABLE 6.8.1
RETAINING WALL DESIGN RECOMMENDATIONS

Parameter	Value
Active Soil Pressure, A (Fluid Density, Level Backfill)	40 pcf
Active Soil Pressure, A (Fluid Density, 2:1 Sloping Backfill)	55 pcf
Seismic Pressure, S	15H psf
At-Rest/Restrained Walls Additional Uniform Pressure, R_U (0 to 8 Feet High)	7H psf
At-Rest/Restrained Walls Additional Uniform Pressure, R_L (8+ Feet High)	13H psf
Expected Expansion Index for the Subject Property	EI≤90

H equals the height of the retaining portion of the wall

6.8.2 The project retaining walls should be designed as shown in the Retaining Wall Loading Diagram.



Retaining Wall Loading Diagram

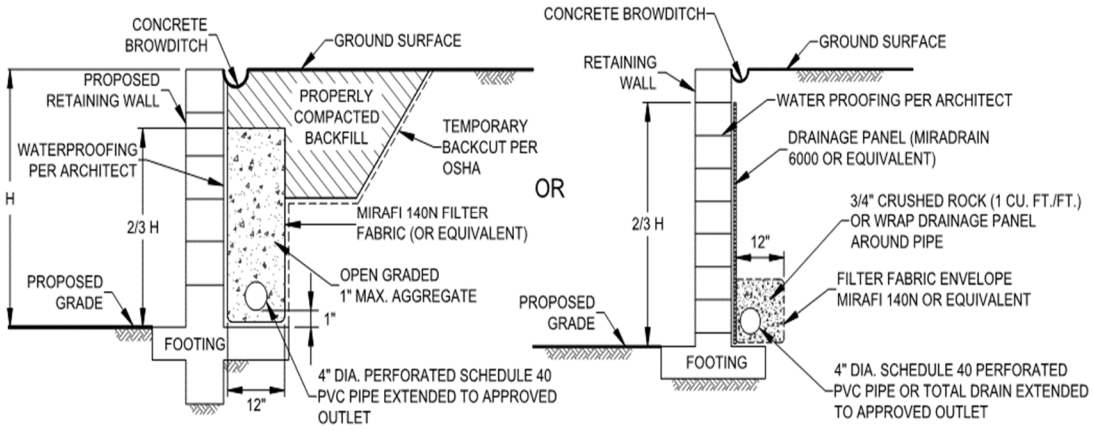
6.8.3 Unrestrained walls are those that are allowed to rotate more than 0.001H (where H equals the height of the retaining portion of the wall) at the top of the wall.

6.8.4 Where walls are restrained from movement at the top (at-rest condition), an additional uniform pressure should be applied to the wall. For retaining walls subject to vehicular loads within a horizontal distance equal to two-thirds the wall height, a surcharge equivalent to 2 feet of fill soil should be added to the upper 10 feet of the retaining wall.

6.8.5 The structural engineer should determine the Seismic Design Category for the project in accordance with Section 1613 of the 2022 CBC or Section 11.6 of ASCE 7-16. For structures assigned to Seismic Design Category of D, E, or F, retaining walls that support more than 6 feet of backfill should be designed with seismic lateral pressure in accordance with Section 1803.5.12 of the 2022 CBC. The seismic load is dependent on the retained height where H is the height of the wall, in feet, and the calculated loads result in pounds per square foot (psf) exerted at the base of the wall and zero at the top of the wall.

6.8.6 It is not necessary to consider active pressure acting on foundation keyways.

6.8.7 Drainage openings through the base of the wall (weep holes) should not be used where the seepage could be a nuisance or otherwise adversely affect the property adjacent to the base of the wall. The recommendations herein assume a properly compacted granular (EI of 50 or less) free-draining backfill material with no hydrostatic forces or imposed surcharge load. The retaining wall should be properly drained as shown in the Typical Retaining Wall Drainage Detail. If conditions different than those described are expected, or if specific drainage details are desired, Geocon Incorporated should be contacted for additional recommendations.



Typical Retaining Wall Drainage Detail

6.8.8 In general, wall foundations should be designed in accordance with Table 6.8.2. The proximity of the foundation to the top of a slope steeper than 3:1 could impact the allowable soil bearing pressure. Therefore, retaining wall foundations should be deepened such that the bottom outside edge of the footing is at least 7 feet horizontally from the face of the slope.

TABLE 6.8.2
SUMMARY OF RETAINING WALL FOUNDATION RECOMMENDATIONS

Parameter	Value
Minimum Retaining Wall Foundation Width	12 inches
Minimum Retaining Wall Foundation Depth	12 Inches
Minimum Concrete Reinforcement	Per Structural Engineer
Allowable Bearing Capacity	2,000 psf
Estimated Total Settlement	1 Inch
Estimated Differential Settlement	½ Inch in 40 Feet

6.8.9 The recommendations presented herein are generally applicable to the design of rigid concrete or masonry retaining walls. Geocon Incorporated should be consulted for additional recommendations for other types of walls (such as mechanically stabilized earth [MSE] walls, soil nail walls, or soldier pile walls).

6.8.10 Unrestrained walls will move laterally when backfilled and loading is applied. The amount of lateral deflection is dependent on the wall height, the type of soil used for backfill, and loads acting on the wall. The retaining walls and improvements above the retaining walls should be designed to incorporate an appropriate amount of lateral deflection as determined by the structural engineer.

6.8.11 Soil contemplated for use as retaining wall backfill, including imported soil, should be identified in the field prior to backfill. Geocon Incorporated should be provide with samples to evaluate its suitability. Modified lateral earth pressures may be necessary if the backfill soil does not meet the required expansion index or shear strength.

6.8.12 City or regional standard wall designs are based on a specific active lateral earth pressure and soil friction angle. The on-site soil may or may not meet the values for standard wall designs. Geocon Incorporated should be consulted to assess the suitability of the on-site soil for use as wall backfill if standard wall designs will be used.

6.9 Lateral Loading

6.9.1 Table 6.9 should be used to help design the proposed structures and improvements to resist lateral loads for the design of footings or shear keys. The allowable passive pressure assumes a horizontal surface extending at least 5 feet, or three times the surface generating the passive pressure, whichever is greater. The upper 12 inches of material in areas not protected by floor slabs or pavement should not be included in design for passive resistance.

TABLE 6.9
SUMMARY OF LATERAL LOAD DESIGN RECOMMENDATIONS

Parameter	Value
Passive Pressure Fluid Density	300 pcf
Coefficient of Friction (Concrete and Soil)	0.35
Coefficient of Friction (Along Vapor Barrier)	0.2 to 0.25*

*Per manufacturer's recommendations.

6.9.2 The passive and frictional resistant loads can be combined for design purposes. The lateral passive pressures may be increased by one-third when considering transient loads due to wind or seismic forces.

6.10 Storm Water Management

6.10.1 If storm water management devices are not properly designed and constructed, there is a risk for distress to improvements and properties located hydrologically down gradient or adjacent to these devices. Factors such as the amount of water being detained, its residence time, and soil permeability have an important effect on seepage transmission and the potential adverse impacts that may occur if the storm water management features are not properly designed and constructed. We have not performed a hydrogeological study at the site. If infiltration of storm water runoff into the subsurface occurs, downstream improvements may be subjected to seeps, springs, slope instability, raised groundwater, movement of foundations and slabs, or other undesirable impacts as a result of water infiltration.

6.10.2 We performed 4 borehole field-saturated, hydraulic conductivity tests at the site using a Soil Moisture Corp Aardvark Permeameter at the locations presented on the Geologic Map, Figure 1. Table 6.10.1 presents the results of the saturated hydraulic conductivity testing.

TABLE 6.10.1
FIELD-SATURATED, INFILTRATION TEST RESULTS

Test No.	Depth (inches)	Surficial Soil or Geologic Unit	Field Infiltration Rate, I (in/hr)	Factored* Field Infiltration Rate, I (in/hr)
A-1	65	Qt	0.322	0.161
A-2	60	Qt	0.027	0.0135
A-3	35.5	Topsoil/Qt	0.035	0.0175
A-4	66	Qt	0.063	0.0315

*Factor of Safety of 2.0 for feasibility determination.

6.10.3 We used the guidelines presented in the Riverside County Low Impact Development BMP Design Handbook which references the United States Bureau of Reclamation Well Permeameter Test Method (USBR 7300-89). Based on this widely accepted guideline, the saturated hydraulic conductivity (Ksat) is equal to the infiltration rate. Therefore, the Ksat value determined from the Aardvark Permeameter test is the unfactored infiltration rate. The Ksat (infiltration rate) equation provided in the Riverside County Handbook was used to compute the unfactored infiltration rate.

6.10.4 Soil permeability values from in-situ tests can vary significantly from one location to another due to the non-homogeneous characteristics inherent to most soil. However, if a sufficient amount of field and laboratory test data is obtained, a general trend of soil permeability can usually be evaluated. For this project and for storm water purposes, the test results presented herein should be considered approximate values.

6.10.5 Infiltration categories include full infiltration, partial infiltration and no infiltration. Table 6.10.2 presents the commonly accepted definitions of the potential infiltration categories based on the infiltration rates.

TABLE 6.10.2
INFILTRATION CATEGORIES

Infiltration Category	Field Infiltration Rate, I (inches/hour)	Factored Infiltration Rate*, I (inches/hour)
Full Infiltration	$I > 1.0$	$I > 0.5$
Partial Infiltration	$0.10 < I \leq 1.0$	$0.05 < I \leq 0.5$
No Infiltration (Infeasible)	$I < 0.10$	$I < 0.05$

*Using a Factor of Safety of 2.

6.10.6 We evaluated the site for areas of potential infiltration. The entire site is underlain by clayey Terrace Deposits. In the area of the proposed basin, the infiltration rates are sufficiently low that full or partial infiltration is not feasible. Additionally, the clayey Terrace Deposits are highly expansive. Infiltrating into the expansive soils could cause soil movement and associated distress to adjacent improvements. Based on our exploratory borings, we do not expect other areas on the site will have infiltration characteristics that are significantly higher and suitable for infiltration.

6.10.7 In our professional opinion and based on our site-specific investigation, there are no areas of the site where storm water infiltration is feasible. The infiltration rates are too low and/or there is an un-mitigatable risk of lateral flow to adjacent rights-of-way, utility trenches, and future buildings.

6.11 Site Drainage and Moisture Protection

6.11.1 Adequate site drainage is critical to reduce potential differential soil movement; erosion; and subsurface seepage. Under no circumstances should water be allowed to pond adjacent to footings. The site should be graded and maintained such that surface drainage is directed away from structures in accordance with 2022 CBC 1804.4. Surface drainage should be directed away from the top of slopes into swales or other controlled drainage devices. Roof and pavement drainage should be directed into conduits that carry runoff away from the proposed structure.

6.11.2 In the case of basement walls or building walls retaining landscaping areas, a water-proofing system should be used on the wall and joints, and a Miradrain drainage panel (or similar) should be placed over the waterproofing. The project architect or civil engineer should provide detailed specifications on the plans for all waterproofing and drainage.

6.11.3 Underground utilities must be leak free. Utility and irrigation lines should be checked at appropriate intervals for leaks. Detected leaks should be promptly repaired. Detrimental soil movement could occur if water is allowed to infiltrate the soil.

6.11.4 Landscaping planters adjacent to paved areas are not recommended due to the risk of surface or irrigation water infiltrating the pavement subgrade and base course. Area drains to collect and transmit excess irrigation water into drainage structures and impervious above-grade planter boxes can be used. A cutoff wall along the edge of the pavement extending at least 6 inches below the bottom of the base material should be considered.

6.12 Grading and Foundation Plan Review

6.12.1 Geocon Incorporated should review the grading and foundation plans for the project prior to final design submittal to determine if additional analysis and/or recommendations are required.

LIMITATIONS AND UNIFORMITY OF CONDITIONS

1. The firm that performed the geotechnical investigation for the project should be retained to provide testing and observation services during construction to provide continuity of geotechnical interpretation and to check that the recommendations presented for geotechnical aspects of site development are incorporated during site grading, construction of improvements, and excavation of foundations. If another geotechnical firm is selected to perform the testing and observation services during construction operations, that firm should prepare a letter indicating their intent to assume the responsibilities of project geotechnical engineer of record. A copy of the letter should be provided to the regulatory agency for their records. In addition, that firm should provide revised recommendations concerning the geotechnical aspects of the proposed development, or a written acknowledgement of their concurrence with the recommendations presented in our report. They should also perform additional analyses deemed necessary to assume the role of Geotechnical Engineer of Record.

2. The recommendations of this report pertain only to the site investigated and are based upon the assumption that the soil conditions do not deviate from those disclosed in the investigation. If any variations or undesirable conditions are encountered during construction, or if the proposed construction will differ from that anticipated herein, Geocon Incorporated should be notified so that supplemental recommendations can be given. The evaluation or identification of the potential presence of hazardous or corrosive materials was not part of the scope of services provided by Geocon Incorporated.

3. This report is issued with the understanding that it is the responsibility of the owner or his representative to ensure that the information and recommendations contained herein are brought to the attention of the architect and engineer for the project and incorporated into the plans, and the necessary steps are taken to see that the contractor and subcontractors carry out such recommendations in the field.

4. The findings of this report are valid as of the present date. However, changes in the conditions of a property can occur with the passage of time, whether they be due to natural processes or the works of man on this or adjacent properties. In addition, changes in applicable or appropriate standards may occur, whether they result from legislation or the broadening of knowledge. Accordingly, the findings of this report may be invalidated wholly or partially by changes outside our control. Therefore, this report is subject to review and should not be relied upon after a period of three years.

THE COLLECTION AT CACTUS
SAN DIEGO, CALIFORNIA

PA-11

PA-12

APPROX. LIMITS OF SITE

OTAY MESA FWY

CACTUS RD

AIRWAY ROAD

CONTINENTAL RD

Qtg

Qtc/Qtg

Qtc

A-1

A-2

A-3

A-4

B-1

B-2

B-3

TP-1

TP-2 (3)

TP-3 (8)

TP-4 (8)

TP-5 (6)

TP-6 (5.5)

TP-7 (5)

TP-8

TP-9 (4)

TP-10 (4.5)

TP-11 (5)

TP-12 (14+)

TP-13 (11+)

TP-14 (±9)

TP-15 (4.5)

TP-16 (5)

B-1 (9)

B-2 (7)

B-3 (6)

LOT A - SPPA-17-PARK
3.50 AC

REC AREA

LEASE/ CLUB 3,500 SF

LEASE/ CLUB 3,000 SF

2,500 SF LEASE/ CLUB

W.Q. BASIN

W.Q. 7,906 BOT.

W.Q. 9,272 BOT.

PED NODE

WORKSPACES

0' 75' 150' 225' 300'

SCALE 1"=150'(on 11x17)

GEOCON LEGEND

Qtc.....TERRACE DEPOSITS - CLAY MEMBER

Qtg.....TERRACE DEPOSITS - SAND/GRAVEL MEMBER

?.....APPROX. LOCATION OF GEOLOGIC CONTACT (Queried Where Uncertain)

B-3.....APPROX. LOCATION OF PRELIMINARY BORING

A-4.....APPROX. LOCATION OF INFILTRATION TESTING

TP16.....APPROX. LOCATION OF EXPLORATORY TEST PIT

(5).....APPROX. DEPTH (In Feet) TO CONTACT BETWEEN Qtc AND Qtg

GEOCON INCORPORATED

GEOTECHNICAL ■ ENVIRONMENTAL ■ MATERIALS

6960 FLANDERS DRIVE - SAN DIEGO, CALIFORNIA 92121 - 2974

PHONE 858 558-6900 - FAX 858 558-6159

PROJECT NO. G2338 - 42 - 02

FIGURE 1

DATE 05 - 18 - 2023

GEOLOGIC MAP

Plotted:05/17/2023 12:43PM | By:ALVIN LADRILLONO | File Location:Y:\PROJECTS\G2338-42-02 (Paez Property)\SHEETS\G2338-42-02 Geo Map.dwg

APPENDIX A

APPENDIX A

PREVIOUS FIELD INVESTIGATIONS

We performed field investigations on November 27, 2018, and March 8, 2019. The investigations consisted of drilling three, small-diameter borings, excavating four infiltration-test borings, and excavating 16 backhoe trenches. The approximate locations of the previous exploratory trenches, borings and infiltration tests are shown on the Geologic Map, Figure 1.

The geotechnical borings were drilled to depths of approximately 10 feet below existing grade using a CME 95 drill rig equipped with hollow-stem augers. The infiltration-test borings were drilled to depths of approximately 4.5 to 6 feet.

The exploratory trenches were excavated to a maximum depth of 16 feet below existing grades using a John Deere 555 backhoe equipped with a 24-inch-wide bucket. Bulk samples were obtained for laboratory testing.

The soil conditions encountered in the excavations were visually classified and logged in general accordance with American Society for Testing and Materials (ASTM) practice for Description and Identification of Soils (Visual Manual Procedure D 2488). The logs of the previous trenches are presented on Figures A-1 through A-16 and the logs of previous borings performed are presented on Figures A-17 through A-19.

PROJECT NO. G2338-42-01

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	**BORING B 1** ELEV. (MSL.) **506'** DATE COMPLETED **11-27-2018** EQUIPMENT **CME 95** BY: **N. BORJA**	PENETRATION RESISTANCE (BLOWS/FT.)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
					MATERIAL DESCRIPTION			
0				SM/SC	**TOPSOIL** Loose, dry to damp, dark brown, Silty to Clayey, fine to coarse SAND			
2								
				CL	**TERRACE DEPOSITS-CLAY MEMBER (Qtc)** Firm, moist, dark olive brown, Sandy CLAY			
4								
6								
8								
				SM	**TERRACE DEPOSITS-GRAVEL MEMBER (Qtg)** Medium dense, damp, tan brown, Silty, fine to coarse SAND			
10					BORING TERMINATED AT 10 FEET Groundwater not encountered			

Figure A-17,
Log of Boring B 1, Page 1 of 1

G2338-42-01 (BORING AND TEST PIT).GPJ

SAMPLE SYMBOLS

... SAMPLING UNSUCCESSFUL
... STANDARD PENETRATION TEST
... DRIVE SAMPLE (UNDISTURBED)
... DISTURBED OR BAG SAMPLE
... CHUNK SAMPLE
... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. G2338-42-01

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	**BORING B 2** ELEV. (MSL.) **511'** DATE COMPLETED **11-27-2018** EQUIPMENT **CME 95** BY: **N. BORJA**	PENETRATION RESISTANCE (BLOWS/FT.)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
					MATERIAL DESCRIPTION			
0				SM	**TOPSOIL** Loose, dry, dark grayish brown, Silty, fine to medium SAND			
2				CL	**TERRACE DEPOSITS-CLAY MEMBER (Qtc)** Firm, damp, dark olive brown, Sandy CLAY			
4				SC	Loose to medium dense, damp, very light gray, Clayey, fine to medium SAND			
6								
8				SM	**TERRACE DEPOSITS-GRAVEL MEMBER (Qtg)** Medium dense, dry, tan brown, Silty, fine to coarse SAND -Excavates with gravel at 9 feet			
					BORING TERMINATED AT 9.5 FEET Groundwater not encountered			

Figure A-18,
Log of Boring B 2, Page 1 of 1

G2338-42-01 (BORING AND TEST PIT).GPJ

SAMPLE SYMBOLS

- ... SAMPLING UNSUCCESSFUL
- ... STANDARD PENETRATION TEST
- ... DRIVE SAMPLE (UNDISTURBED)
- ... DISTURBED OR BAG SAMPLE
- ... CHUNK SAMPLE
- ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. G2338-42-01

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	**BORING B 3** ELEV. (MSL.) **507.5'** DATE COMPLETED **11-27-2018** EQUIPMENT **CME 95** BY: **N. BORJA**	PENETRATION RESISTANCE (BLOWS/FT.)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
					MATERIAL DESCRIPTION			
0				SM	**TOPSOIL** Loose, dry, dark grayish brown, Silty, fine to coarse SAND			
2				CL	**TERRACE DEPOSITS-CLAY MEMBER (Qtc)** Firm, damp, olive brown, Sandy CLAY			
4				SM	Loose to medium dense, damp, grayish brown to brown, Silty, fine to medium SAND			
6				SM	**TERRACE DEPOSITS-GRAVEL MEMBER (Qtg)** Dense to very dense, dry, light brown to yellowish brown, Silty, fine to coarse SAND; little gravel			
					REFUSAL AT 7.5 FEET Groundwater not encountered			

Figure A-19,
Log of Boring B 3, Page 1 of 1

G2338-42-01 (BORING AND TEST PIT).GPJ

SAMPLE SYMBOLS

... SAMPLING UNSUCCESSFUL
... STANDARD PENETRATION TEST
... DRIVE SAMPLE (UNDISTURBED)
... DISTURBED OR BAG SAMPLE
... CHUNK SAMPLE
... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. G2338-42-01

TEST PIT TP 1

ELEV. (MSL.) **497'** DATE COMPLETED **03-08-2019**

EQUIPMENT **Backhoe** BY: **R. ADAMS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT.)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0	TP1-1			CL	**TOPSOIL (Ts)** Soft, moist, dark brown, Sandy CLAY; trace silt			
				SC	**TERRACE DEPOSITS-Sand/Gravel Member (Qtg)** Medium dense, damp to moist, pale yellowish brown, Clayey, fine grained SAND			
2								
4	TP1-2				-Becomes medium- to coarse-grained, trace cobble, trace silt			
6				SC	Dense, damp, yellowish brown, medium- to coarse-grained SAND; trace clay, trace subrounded cobble			
8								
					TRENCH TERMINATED AT 9 FEET Groundwater not encountered Backfilled 03-08-2019			

Figure A-1,
Log of Test Pit TP 1, Page 1 of 1

G2338-42-01 (BORING AND TEST PIT).GPJ

SAMPLE SYMBOLS

- ... SAMPLING UNSUCCESSFUL
- ... STANDARD PENETRATION TEST
- ... DRIVE SAMPLE (UNDISTURBED)
- ... DISTURBED OR BAG SAMPLE
- ... CHUNK SAMPLE
- ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. G2338-42-01

TEST PIT TP 2

ELEV. (MSL.) **503'** DATE COMPLETED **03-08-2019**

EQUIPMENT **Backhoe** BY: **R. ADAMS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT.)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0	TP1-1			CL	**TOPSOIL (Ts)** Soft to moist, wet, dark brown to black, Sandy CLAY			
2								
4				SC	**TERRACE DEPOSITS-Sand/Gravel Member (Qtg)** Medium dense to dense, damp, yellowish brown, Clayey, medium coarse SAND; trace cobble, pockets of dark brown, Sandy CLAY throughout			
6				SM	Dense, damp, pale brown to yellowish brown, Silty, fine to coarse SAND; trace clay, trace sub-rounded cobble up to 10-inch diameter			
8								
10					-Becomes weakly cemented; excavating to a clayey sand with gravel and cobble			
12					TRENCH TERMINATED AT 12 FEET Groundwater not encountered Backfilled 03-08-2019			

Figure A-2,
Log of Test Pit TP 2, Page 1 of 1

G2338-42-01 (BORING AND TEST PIT).GPJ

SAMPLE SYMBOLS

... SAMPLING UNSUCCESSFUL
... STANDARD PENETRATION TEST
... DRIVE SAMPLE (UNDISTURBED)
... DISTURBED OR BAG SAMPLE
... CHUNK SAMPLE
... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. G2338-42-01

TEST PIT TP 3

ELEV. (MSL.) **504'** DATE COMPLETED **03-08-2019**

EQUIPMENT **Backhoe** BY: **R. ADAMS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT.)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0				CH	**TOPSOIL (Ts)** Soft to firm, moist, grayish brown to black, Silty CLAY; trace sand			
2				CH	**TERRACE DEPOSITS-Clay Member (Qtc)** Firm to stiff, moist, grayish brown, Sandy CLAY; trace rock fragments, trace sand			
4	TP3-1				-Becomes stiff to very stiff			
6				CH	Very stiff, moist, grayish brown to reddish brown, Sandy CLAY			
8	TP3-2			SM	**TERRACE DEPOSITS-Sand/Gravel Member (Qtg)** Dense, damp, reddish brown to grayish brown (mottled), Silty, fine to medium SAND; trace clay, trace cobble up to 6-inch diameter			
10					-Some gravel and cobble up to 8-inch diameter			
12					TRENCH TERMINATED AT 12 FEET Groundwater not encountered Backfilled 03-08-2019			

Figure A-3,
Log of Test Pit TP 3, Page 1 of 1

G2338-42-01 (BORING AND TEST PIT).GPJ

SAMPLE SYMBOLS

... SAMPLING UNSUCCESSFUL
... STANDARD PENETRATION TEST
... DRIVE SAMPLE (UNDISTURBED)
... DISTURBED OR BAG SAMPLE
... CHUNK SAMPLE
... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. G2338-42-01

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	TEST PIT TP 4 ELEV. (MSL.) **506'** DATE COMPLETED **03-08-2019** EQUIPMENT **Backhoe** BY: **R. ADAMS** MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT.)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0				CH	**TOPSOIL (Ts)** Soft, wet, brown to grayish brown, CLAY; trace silt; trace sand			
2								
4				CH	**TERRACE DEPOSITS-Clay Member (Qtc)** Firm to stiff, damp to moist, brownish gray, CLAY -Becomes stiff to very stiff, on blocky texture, manganese films noted on parking surfaces			
6								
8				SC	**TERRACE DEPOSITS-Sand/Gravel (Qtg)** Medium dense to dense, damp, reddish brown to grayish brown (mottled), Clayey, fine- to medium-grained SAND; trace silt			
10				SM	Dense, damp, grayish brown, Silty, medium to coarse SAND; trace clay; some gravel/cobble up to 10-inch diameter			
					TRENCH TERMINATED AT 11 FEET Groundwater not encountered Backfilled 03-08-2019			

Figure A-4,
Log of Test Pit TP 4, Page 1 of 1

G2338-42-01 (BORING AND TEST PIT).GPJ

SAMPLE SYMBOLS

... SAMPLING UNSUCCESSFUL
... STANDARD PENETRATION TEST
... DRIVE SAMPLE (UNDISTURBED)
... DISTURBED OR BAG SAMPLE
... CHUNK SAMPLE
... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. G2338-42-01

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	TEST PIT TP 5 ELEV. (MSL.) 507' DATE COMPLETED 03-08-2019 EQUIPMENT Backhoe BY: R. ADAMS MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT.)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0	TP5-1			CH	**TOPSOIL (Ts)** Soft, damp to wet, brown, CLAY; trace sand; few rootlets			
2	TP5-2			CH	**TERRACE DEPOSITS-Clay Member (Qtc)** Firm to stiff, damp to moist, whitish gray, CLAY			
4								
6				SM	**TERRACE DEPOSITS-Sand/Gravel Member (Qtg)** Dense, damp, pale yellowish gray, Silty, coarse SAND; trace small cobble			
8	TP5-3							
					TRENCH TERMINATED AT 9 FEET Groundwater not encountered Backfilled 03-08-2019			

Figure A-5,
Log of Test Pit TP 5, Page 1 of 1

G2338-42-01 (BORING AND TEST PIT).GPJ

SAMPLE SYMBOLS

... SAMPLING UNSUCCESSFUL
... STANDARD PENETRATION TEST
... DRIVE SAMPLE (UNDISTURBED)
... DISTURBED OR BAG SAMPLE
... CHUNK SAMPLE
... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. G2338-42-01

TEST PIT TP 6

ELEV. (MSL.) **507'** DATE COMPLETED **03-08-2019**

EQUIPMENT **Backhoe** BY: **R. ADAMS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT.)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0				CH	**TOPSOIL (Ts)** Very soft to soft, wet, grayish brown to brown, CLAY			
2				SC	**TERRACE DEPOSITS-Clay Member (Qtc)** Firm to stiff, damp to moist, grayish brown, Sandy CLAY; trace rounded gravel -Becomes hard and blocky, trace carbonate and manganese			
4	TP6-1			CH	Hard, dry to damp, yellowish brown, Sandy CLAY			
6				SM	**TERRACE DEPOSITS-Sand/Gravel Member (Qtg)** Dense, dry to damp, yellowish brown, Silty, fine to coarse SAND; trace small cobble, angular to sub-rounded			
8					-Becomes reddish brown			
10					TRENCH TERMINATED AT 10 FEET Groundwater not encountered Backfilled 03-08-2019			

Figure A-6,
Log of Test Pit TP 6, Page 1 of 1

G2338-42-01 (BORING AND TEST PIT).GPJ

SAMPLE SYMBOLS

... SAMPLING UNSUCCESSFUL
... STANDARD PENETRATION TEST
... DRIVE SAMPLE (UNDISTURBED)
... DISTURBED OR BAG SAMPLE
... CHUNK SAMPLE
... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. G2338-42-01

TEST PIT TP 7

ELEV. (MSL.) **501'** DATE COMPLETED **03-08-2019**

EQUIPMENT **Backhoe** BY: **R. ADAMS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT.)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0				CH	**TOPSOIL (Ts)** Stiff, firm, damp to moist, dark brown, Silty CLAY; trace plastic debris			
2								
4				CH	**TERRACE DEPOSITS-Clay Member (Qtc)** Stiff to hard, dry to damp, whitish gray to grayish brown, Sandy CLAY			
6				SC	**TERRACE DEPOSITS-Sand/Gravel Member (Qtg)** Dense, damp, yellowish gray to yellowish brown, Clayey, medium coarse SAND; trace cobble up to 8-inch diameter			
8					-Becomes reddish brown			
10					-Becomes very dense, little cobble and rock fragments up to 12-inch diameter			
12					-Becomes reddish brown to greenish brown (mottled); Cobble up to 20-inch diameter			
14	TP7-1			SC/CL	Dense, damp, yellowish brown, greenish gray (mottled), Clayey SAND and Sandy CLAY (Interbedded); some cobble up to 10-inch diameter			
16					TRENCH TERMINATED AT 16 FEET Groundwater not encountered Backfilled 03-08-2019			

Figure A-7,
Log of Test Pit TP 7, Page 1 of 1

G2338-42-01 (BORING AND TEST PIT).GPJ

SAMPLE SYMBOLS

... SAMPLING UNSUCCESSFUL
... STANDARD PENETRATION TEST
... DRIVE SAMPLE (UNDISTURBED)
... DISTURBED OR BAG SAMPLE
... CHUNK SAMPLE
... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. G2338-42-01

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	TEST PIT TP 8 ELEV. (MSL.) **501'** DATE COMPLETED **03-08-2019** EQUIPMENT **Backhoe** BY: **R. ADAMS**	PENETRATION RESISTANCE (BLOWS/FT.)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
					MATERIAL DESCRIPTION			
0				CH	**TOPSOIL (Ts)** Firm, damp, brownish black, CLAY; trace sand -Cobble lens			
2				CH	**TERRACE DEPOSITS-Clay (Qtc)** Stiff to hard, damp grayish yellow (mottled), Sandy CLAY; trace cobble			
4				SC	**TERRACE DEPOSITS-Sand/Gravel Member (Qtg)** Dense, damp, reddish brown to grayish brown, Clayey SAND; trace cobble up to 8-inch diameter -Becomes dense to very dense, reddish brown; some cobble up to 6-inch diameter			
6					TRENCH TERMINATED AT 6 FEET Groundwater not encountered Backfilled 03-08-2019			

Figure A-8,
Log of Test Pit TP 8, Page 1 of 1

G2338-42-01 (BORING AND TEST PIT).GPJ

SAMPLE SYMBOLS

... SAMPLING UNSUCCESSFUL
... STANDARD PENETRATION TEST
... DRIVE SAMPLE (UNDISTURBED)
... DISTURBED OR BAG SAMPLE
... CHUNK SAMPLE
... WATER TABLE OR SEEPAGE

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GEOCON

PROJECT NO. G2338-42-01

TEST PIT TP 9

ELEV. (MSL.) **505'** DATE COMPLETED **03-08-2019**

EQUIPMENT **Backhoe** BY: **R. ADAMS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT.)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0				CH	**TOPSOIL (Ts)** Firm to stiff, moist, dark brown, CLAY; trace sand			
2	TP9-1			CH	**TERRACE DEPOSITS-Clay Member (Qtc)** Stiff, damp, grayish brown, CLAY; trace sand, trace carbonate			
4				SC	**TERRACE DEPOSITS-Sand/Gravel Member (Qtg)** Dense, damp, yellowish brown, Clayey, medium to coarse SAND; trace cobble and gravel up to 6-inch diameter			
6					-Little cobble up to 8-inch diameter			
					TRENCH TERMINATED AT 7 FEET Groundwater not encountered Backfilled 03-08-2019			

Figure A-9,
Log of Test Pit TP 9, Page 1 of 1

G2338-42-01 (BORING AND TEST PIT).GPJ

SAMPLE SYMBOLS

... SAMPLING UNSUCCESSFUL
... STANDARD PENETRATION TEST
... DRIVE SAMPLE (UNDISTURBED)
... DISTURBED OR BAG SAMPLE
... CHUNK SAMPLE
... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. G2338-42-01

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	TEST PIT TP 10 ELEV. (MSL.) **509'** DATE COMPLETED **03-08-2019** EQUIPMENT **Backhoe** BY: **R. ADAMS** MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT.)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0				CH	**TOPSOIL (Ts)** Soft, moist to wet, brownish black, CLAY; trace carbonate			
2				CH	**TERRACE DEPOSITS-Clay Member (Qtc)** Firm to stiff, damp, brown to grayish brown, Sandy CLAY; trace cobble			
4								
6	TP10-1			SC	**TERRACE DEPOSITS-Sand/Gravel Member (Qtg)** Medium dense to dense, grayish brown to pale yellowish brown, Clayey SAND; trace cobble			
8				SM-SW	Medium dense to dense, grayish brown to dark brown, Silty, medium to coarse SAND; trace cobble, friable with low cohesion			
10					TRENCH TERMINATED AT 10 FEET Groundwater not encountered Backfilled 03-08-2019			

Figure A-10,
Log of Test Pit TP 10, Page 1 of 1

G2338-42-01 (BORING AND TEST PIT).GPJ

SAMPLE SYMBOLS

... SAMPLING UNSUCCESSFUL
... STANDARD PENETRATION TEST
... DRIVE SAMPLE (UNDISTURBED)
... DISTURBED OR BAG SAMPLE
... CHUNK SAMPLE
... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. G2338-42-01

TEST PIT TP 11

ELEV. (MSL.) **509'** DATE COMPLETED **03-08-2019**

EQUIPMENT **Backhoe** BY: **R. ADAMS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT.)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0				CH	**TOPSOIL (Ts)** Soft to firm, moist, dark brown to black, CLAY			
2				CH	**TERRACE DEPOSITS-Clay Member (Qtc)** Firm, damp, brownish gray, CLAY; trace sand; trace carbonate			
4								
6				SC	**TERRACE DEPOSITS-Sand/Gravel Member (Qtg)** Medium dense to dense, damp, pale yellowish brown, Clayey, fine to medium SAND; trace cobble			
				SM	Dense, damp, dark brown, Silty, medium to coarse SAND			
8					TRENCH TERMINATED AT 8 FEET Groundwater not encountered Backfilled 03-08-2019			

Figure A-11,
Log of Test Pit TP 11, Page 1 of 1

G2338-42-01 (BORING AND TEST PIT).GPJ

SAMPLE SYMBOLS

- ... SAMPLING UNSUCCESSFUL
- ... STANDARD PENETRATION TEST
- ... DRIVE SAMPLE (UNDISTURBED)
- ... DISTURBED OR BAG SAMPLE
- ... CHUNK SAMPLE
- ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. G2338-42-01

TEST PIT TP 12

ELEV. (MSL.) **511'** DATE COMPLETED **03-08-2019**

EQUIPMENT **Backhoe** BY: **R. ADAMS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT.)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0				CH	**TOPSOIL (Ts)** Soft, wet, brown, CLAY			
2	TP12-1			SC	Medium dense, dry to damp, whitish brown, Clayey, fine to coarse SAND; abundant caliche; trace gravel			
4	TP12-2			CH	**TERRACE DEPOSITS-Clay Member (Qtc)** Firm to stiff, damp, reddish gray, Sandy CLAY; blocky texture; manganese films along fractures			
8					-Mottled (red gray)			
10				CL	Stiff to very hard, dry to damp, reddish gray and greenish gray (mottled) Silty CLAY			
12	TP12-3							
14					TRENCH TERMINATED AT 14 FEET Groundwater not encountered Backfilled 03-08-2019			

Figure A-12,
Log of Test Pit TP 12, Page 1 of 1

G2338-42-01 (BORING AND TEST PIT).GPJ

SAMPLE SYMBOLS

... SAMPLING UNSUCCESSFUL
... STANDARD PENETRATION TEST
... DRIVE SAMPLE (UNDISTURBED)
... DISTURBED OR BAG SAMPLE
... CHUNK SAMPLE
... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. G2338-42-01

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	TEST PIT TP 13 ELEV. (MSL.) 513' DATE COMPLETED 03-08-2019 EQUIPMENT Backhoe BY: R. ADAMS MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT.)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0				CH	**TOPSOIL (Ts)** Soft, moist to wet, brownish black, CLAY; trace rounded gravel			
2				CH	**TERRACE DEPOSITS-Clay Member (Qtc)** Firm to stiff, damp, grayish brown CLAY; trace sand; trace carbonate			
4				CL	Stiff to hard, dry to damp, yellowish brown to reddish brown, CLAY; blocky texture (peds) with manganese films along fractures			
6					-Crumbly block texture with abundant carbonate			
8					-Becomes hard with blocky texture			
10					-Very hard excavation PRACTICAL REFUSAL AT 11 FEET Groundwater not encountered Backfilled 03-08-2019			

Figure A-13,
Log of Test Pit TP 13, Page 1 of 1

G2338-42-01 (BORING AND TEST PIT).GPJ

SAMPLE SYMBOLS

... SAMPLING UNSUCCESSFUL
... STANDARD PENETRATION TEST
... DRIVE SAMPLE (UNDISTURBED)
... DISTURBED OR BAG SAMPLE
... CHUNK SAMPLE
... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. G2338-42-01

TEST PIT TP 14

ELEV. (MSL.) **508'** DATE COMPLETED **03-08-2019**

EQUIPMENT **Backhoe** BY: **R. ADAMS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT.)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0				CH	**TOPSOIL (Ts)** Soft, moist, dark brown, CLAY; trace carbonate			
2				CH	**TERRACE DEPOSITS-Clay Member (Qtc)** Firm to stiff, damp, brownish gray to black, CLAY; trace sand			
4	TP14-1			CL/SC	Stiff, damp, yellowish brown to orange brown, Silty CLAY and Clayey SAND mixture			
6								
8								
10				SC	**TERRACE DEPOSITS-Sand/Gravel Member (Qtg)** Dense, damp, yellowish brown, Clayey SAND; trace cobble			
					TRENCH TERMINATED AT 11 FEET Groundwater not encountered Backfilled 03-08-2019			

Figure A-14,
Log of Test Pit TP 14, Page 1 of 1

G2338-42-01 (BORING AND TEST PIT).GPJ

SAMPLE SYMBOLS

... SAMPLING UNSUCCESSFUL
... STANDARD PENETRATION TEST
... DRIVE SAMPLE (UNDISTURBED)
... DISTURBED OR BAG SAMPLE
... CHUNK SAMPLE
... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. G2338-42-01

TEST PIT TP 15

ELEV. (MSL.) **509'** DATE COMPLETED **03-08-2019**

EQUIPMENT **Backhoe** BY: **R. ADAMS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT.)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0				CH	**TOPSOIL (Ts)** Soft, moist, dark brownish black CLAY			
2				CH	**TERRACE DEPOSITS-Clay Member (Qtc)** Stiff, damp, grayish brown, Sandy CLAY; trace gravel; trace carbonate			
4								
6				SC	**TERRACE DEPOSITS-Sand/Gravel Member (Qtg)** Dense, damp, pale yellowish brown to grayish brown, Clayey, fine to coarse SAND; trace gravel			
8					TRENCH TERMINATED AT 6 FEET Groundwater not encountered Backfilled 03-08-2019			
10								
12								
14								
16								

Figure A-15,
Log of Test Pit TP 15, Page 1 of 1

G2338-42-01 (BORING AND TEST PIT).GPJ

SAMPLE SYMBOLS

- ... SAMPLING UNSUCCESSFUL
- ... STANDARD PENETRATION TEST
- ... DRIVE SAMPLE (UNDISTURBED)
- ... DISTURBED OR BAG SAMPLE
- ... CHUNK SAMPLE
- ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

PROJECT NO. G2338-42-01

TEST PIT TP 16

ELEV. (MSL.) **507'** DATE COMPLETED **03-08-2019**

EQUIPMENT **Backhoe** BY: **R. ADAMS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT.)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0				CH	**TOPSOIL (Ts)** Soft, moist to wet, brownish black, CLAY			
2	TP16-1			CH	**TERRACE DEPOSITS-Clay Member (Qtc)** Stiff, damp to moist, whitish gray, Sandy CLAY; trace silt			
4								
6				SM	**TERRACE DEPOSITS-Sand/Gravel Member (Qtg)** Dense, damp, Silty, medium to coarse SAND; trace clay; trace cobble up to 6-inch diameter			
					TRENCH TERMINATED AT 7 FEET Groundwater not encountered Backfilled 03-08-2019			

Figure A-16,
Log of Test Pit TP 16, Page 1 of 1

G2338-42-01 (BORING AND TEST PIT).GPJ

SAMPLE SYMBOLS

- ... SAMPLING UNSUCCESSFUL
- ... STANDARD PENETRATION TEST
- ... DRIVE SAMPLE (UNDISTURBED)
- ... DISTURBED OR BAG SAMPLE
- ... CHUNK SAMPLE
- ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

APPENDIX B

APPENDIX B

LABORATORY TESTING

We performed laboratory tests in accordance with generally accepted test methods of the American Society for Testing and Materials (ASTM) or other suggested procedures. We tested selected samples for maximum dry density and optimum moisture content, direct shear, expansion, plasticity, water-soluble sulfate, chloride ion content, and gradation characteristics. The results of our laboratory tests are presented in the following tables and figure.

SUMMARY OF LABORATORY MAXIMUM DRY DENSITY AND OPTIMUM MOISTURE CONTENT TEST RESULTS ASTM D 1557

Sample No.	Description	Maximum Dry Density (pcf)	Optimum Moisture Content (%)
TP 1-1	Dark brown, Sandy CLAY; trace gravel (CL)	127.6	9.7
TP 1-2	Brown, Clayey, fine to coarse SAND; trace gravel (SC)	126.7	10.6
TP 5-3	Brown, Silty, fine to coarse SAND; trace gravel (SM)	126.7	10.4
TP 10-1	Brown, Silty, fine to coarse SAND; trace gravel (SM)	130.4	8.4

SUMMARY OF LABORATORY DIRECT SHEAR TEST RESULTS ASTM D 3080

Sample No.	Dry Density (pcf)	Moisture Content (%)		Cohesion (psf)	Angle of Shear Resistance (degrees)
		Initial	Final		
TP 1-2*	115.0	10.2	15.3	330	36
TP 10-1*	117.4	8.6	13.2	0	40

*Sample remolded to approximately 90 percent of the maximum dry density near optimum moisture content.

SUMMARY OF LABORATORY EXPANSION INDEX TEST RESULTS ASTM D 4829

Sample No.	Moisture Content (%)		Dry Density (pcf)	Expansion Index	2022 CBC Expansion Classification	ASTM Soil Expansion Classification
	Before Test	After Test				
TP 1-1	9.7	18.1	111.2	29	Expansive	Low
TP 1-2	8.8	15.8	113.1	11	Non-Expansive	Very Low
TP 3-1	14.3	38.9	93.9	147	Expansive	Very High
TP 10-1	7.8	15.3	118.5	0	Non-Expansive	Very Low

SUMMARY OF LABORATORY PLASTICITY INDEX TEST RESULTS
ASTM D 4318

Sample No.	Depth (feet)	Geologic Unit	Liquid Limit	Plastic Limit	Plasticity Index
TP 1-1	1	Topsoil	42	16	26
TP 5-2	2 to 4	Qtc	66	18	48

SUMMARY OF LABORATORY WATER-SOLUBLE SULFATE TEST RESULTS
CALIFORNIA TEST NO. 417

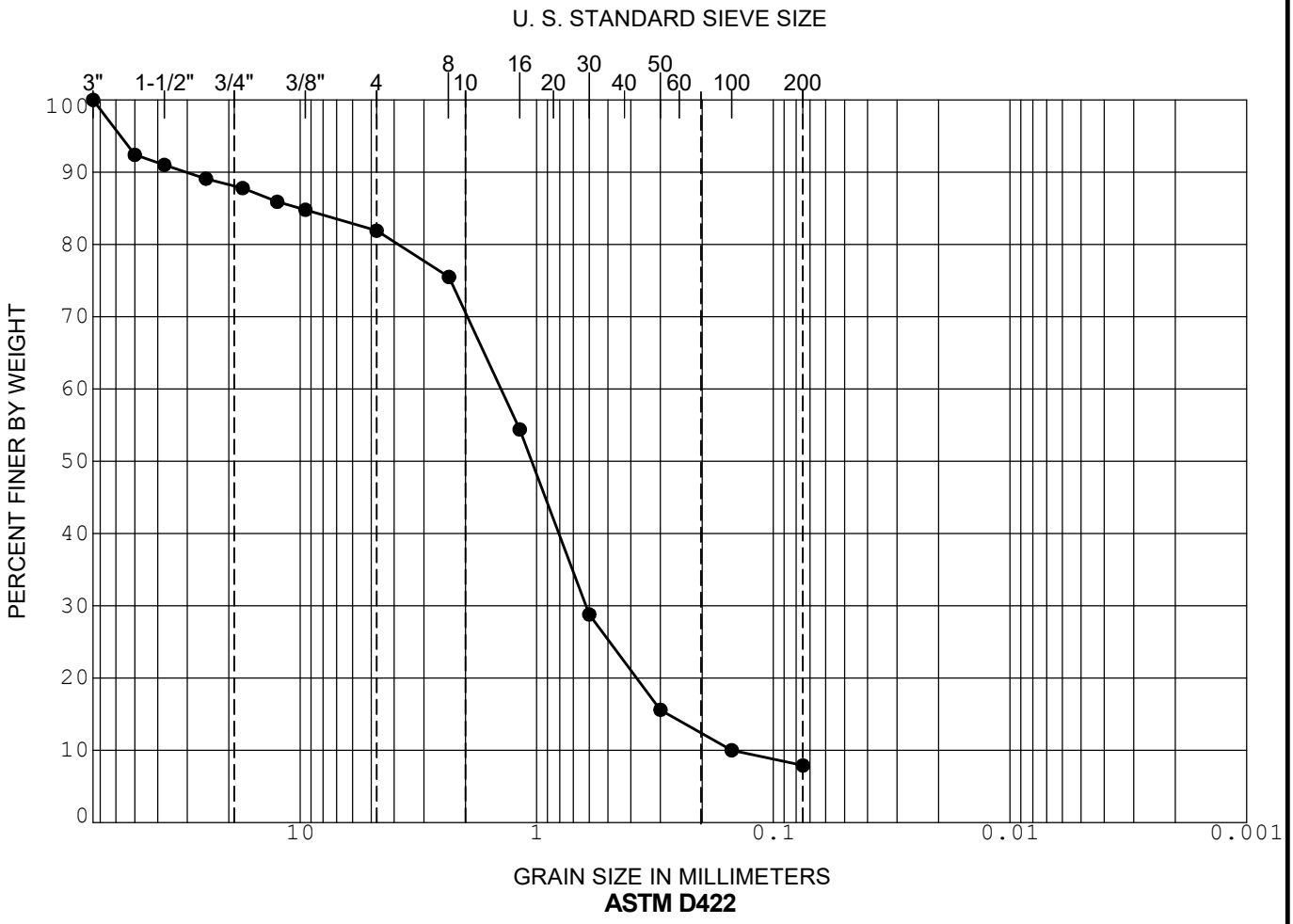
Sample No.	Water-Soluble Sulfate (%)	Sulfate Class
TP 5-3	0.014	S0

SUMMARY OF LABORATORY CHLORIDE ION CONTENT TEST RESULTS
CALIFORNIA TEST NO. 422

Sample No.	Chloride Ion Content (%)	Chloride Ion Content (ppm)
TP 5-3	0.011	111

PROJECT NO. G2338-42-01

GRAVEL		SAND			SILT OR CLAY
COARSE	FINE	COARSE	MEDIUM	FINE	



ASTM D422

	SAMPLE	DEPTH (ft)	CLASSIFICATION	NAT WC	LL	PL	PI
●	TP10-1	1.0	(SW-SM) Well graded SAND with silt and gravel				
⊠							
▲							

GRADATION CURVE

OTAY CENTRAL VILLAGE
PLANNING AREAS 10-13 AND 17, AIRWAY ROAD AND CACTUS ROAD
SAN DIEGO, CALIFORNIA

G2338-42-01 (BORING AND TEST PIT).GPJ

Figure B-1

GEOCON

APPENDIX C

APPENDIX C

RECOMMENDED GRADING SPECIFICATIONS

FOR

THE COLLECTION AT CACTUS
NORTHEAST CORNER OF
AIRWAY ROAD AND CACTUS ROAD
SAN DIEGO, CALIFORNIA

PROJECT NO. G2338-42-02

RECOMMENDED GRADING SPECIFICATIONS

1. GENERAL

1.1 These Recommended Grading Specifications shall be used in conjunction with the Geotechnical Report for the project prepared by Geocon. The recommendations contained in the text of the Geotechnical Report are a part of the earthwork and grading specifications and shall supersede the provisions contained hereinafter in the case of conflict.

1.2 Prior to the commencement of grading, a geotechnical consultant (Consultant) shall be employed for the purpose of observing earthwork procedures and testing the fills for substantial conformance with the recommendations of the Geotechnical Report and these specifications. The Consultant should provide adequate testing and observation services so that they may assess whether, in their opinion, the work was performed in substantial conformance with these specifications. It shall be the responsibility of the Contractor to assist the Consultant and keep them apprised of work schedules and changes so that personnel may be scheduled accordingly.

1.3 It shall be the sole responsibility of the Contractor to provide adequate equipment and methods to accomplish the work in accordance with applicable grading codes or agency ordinances, these specifications and the approved grading plans. If, in the opinion of the Consultant, unsatisfactory conditions such as questionable soil materials, poor moisture condition, inadequate compaction, and/or adverse weather result in a quality of work not in conformance with these specifications, the Consultant will be empowered to reject the work and recommend to the Owner that grading be stopped until the unacceptable conditions are corrected.

2. DEFINITIONS

2.1 **Owner** shall refer to the owner of the property or the entity on whose behalf the grading work is being performed and who has contracted with the Contractor to have grading performed.

2.2 **Contractor** shall refer to the Contractor performing the site grading work.

2.3 **Civil Engineer** or **Engineer of Work** shall refer to the California licensed Civil Engineer or consulting firm responsible for preparation of the grading plans, surveying and verifying as-graded topography.

2.4 **Consultant** shall refer to the soil engineering and engineering geology consulting firm retained to provide geotechnical services for the project.

2.5 **Soil Engineer** shall refer to a California licensed Civil Engineer retained by the Owner, who is experienced in the practice of geotechnical engineering. The Soil Engineer shall be responsible for having qualified representatives on-site to observe and test the Contractor's work for conformance with these specifications.

2.6 **Engineering Geologist** shall refer to a California licensed Engineering Geologist retained by the Owner to provide geologic observations and recommendations during the site grading.

2.7 **Geotechnical Report** shall refer to a soil report (including all addenda) which may include a geologic reconnaissance or geologic investigation that was prepared specifically for the development of the project for which these Recommended Grading Specifications are intended to apply.

3. MATERIALS

3.1 Materials for compacted fill shall consist of any soil excavated from the cut areas or imported to the site that, in the opinion of the Consultant, is suitable for use in construction of fills. In general, fill materials can be classified as *soil* fills, *soil-rock* fills or *rock* fills, as defined below.

3.1.1 **Soil fills** are defined as fills containing no rocks or hard lumps greater than 12 inches in maximum dimension and containing at least 40 percent by weight of material smaller than ¾ inch in size.

3.1.2 **Soil-rock fills** are defined as fills containing no rocks or hard lumps larger than 4 feet in maximum dimension and containing a sufficient matrix of soil fill to allow for proper compaction of soil fill around the rock fragments or hard lumps as specified in Paragraph 6.2. **Oversize rock** is defined as material greater than 12 inches.

3.1.3 **Rock fills** are defined as fills containing no rocks or hard lumps larger than 3 feet in maximum dimension and containing little or no fines. Fines are defined as material smaller than ¾ inch in maximum dimension. The quantity of fines shall be less than approximately 20 percent of the rock fill quantity.

3.2 Material of a perishable, spongy, or otherwise unsuitable nature as determined by the Consultant shall not be used in fills.

3.3 Materials used for fill, either imported or on-site, shall not contain hazardous materials as defined by the California Code of Regulations, Title 22, Division 4, Chapter 30, Articles 9

and 10; 40CFR; and any other applicable local, state or federal laws. The Consultant shall not be responsible for the identification or analysis of the potential presence of hazardous materials. However, if observations, odors or soil discoloration cause Consultant to suspect the presence of hazardous materials, the Consultant may request from the Owner the termination of grading operations within the affected area. Prior to resuming grading operations, the Owner shall provide a written report to the Consultant indicating that the suspected materials are not hazardous as defined by applicable laws and regulations.

3.4 The outer 15 feet of *soil-rock* fill slopes, measured horizontally, should be composed of properly compacted *soil* fill materials approved by the Consultant. *Rock* fill may extend to the slope face, provided that the slope is not steeper than 2:1 (horizontal:vertical) and a soil layer no thicker than 12 inches is track-walked onto the face for landscaping purposes. This procedure may be utilized provided it is acceptable to the governing agency, Owner and Consultant.

3.5 Samples of soil materials to be used for fill should be tested in the laboratory by the Consultant to determine the maximum density, optimum moisture content, and, where appropriate, shear strength, expansion, and gradation characteristics of the soil.

3.6 During grading, soil or groundwater conditions other than those identified in the Geotechnical Report may be encountered by the Contractor. The Consultant shall be notified immediately to evaluate the significance of the unanticipated condition.

4. CLEARING AND PREPARING AREAS TO BE FILLED

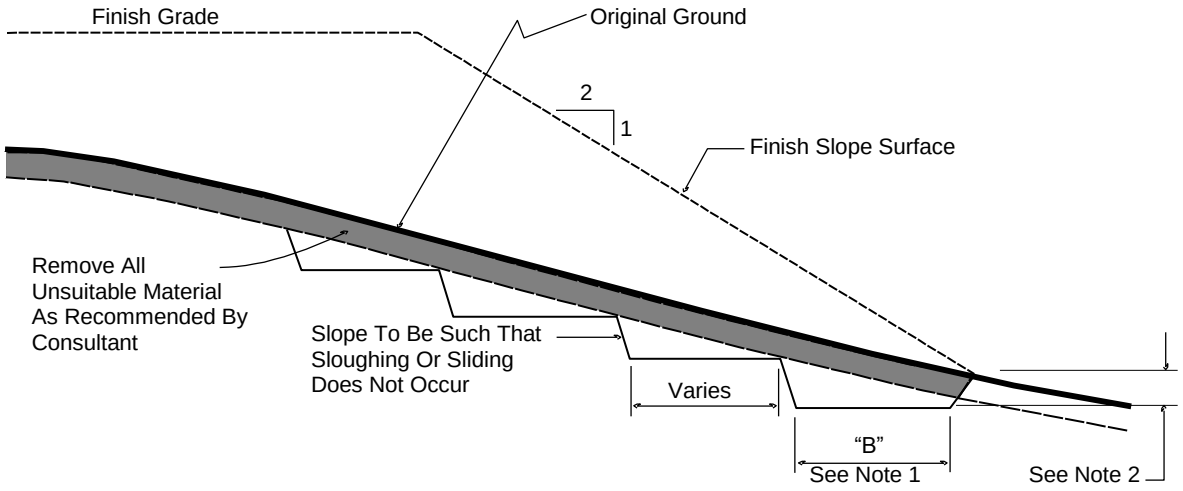
4.1 Areas to be excavated and filled shall be cleared and grubbed. Clearing shall consist of complete removal above the ground surface of trees, stumps, brush, vegetation, man-made structures, and similar debris. Grubbing shall consist of removal of stumps, roots, buried logs and other unsuitable material and shall be performed in areas to be graded. Roots and other projections exceeding 1½ inches in diameter shall be removed to a depth of 3 feet below the surface of the ground. Borrow areas shall be grubbed to the extent necessary to provide suitable fill materials.

4.2 Asphalt pavement material removed during clearing operations should be properly disposed at an approved off-site facility or in an acceptable area of the project evaluated by Geocon and the property owner. Concrete fragments that are free of reinforcing steel may be placed in fills, provided they are placed in accordance with Section 6.2 or 6.3 of this document.

4.3 After clearing and grubbing of organic matter and other unsuitable material, loose or porous soils shall be removed to the depth recommended in the Geotechnical Report. The depth of removal and compaction should be observed and approved by a representative of the Consultant. The exposed surface shall then be plowed or scarified to a minimum depth of 6 inches and until the surface is free from uneven features that would tend to prevent uniform compaction by the equipment to be used.

4.4 Where the slope ratio of the original ground is steeper than 5:1 (horizontal:vertical), or where recommended by the Consultant, the original ground should be benched in accordance with the following illustration.

TYPICAL BENCHING DETAIL



No Scale

DETAIL NOTES: (1) Key width "B" should be a minimum of 10 feet, or sufficiently wide to permit complete coverage with the compaction equipment used. The base of the key should be graded horizontal, or inclined slightly into the natural slope.

(2) The outside of the key should be below the topsoil or unsuitable surficial material and at least 2 feet into dense formational material. Where hard rock is exposed in the bottom of the key, the depth and configuration of the key may be modified as approved by the Consultant.

4.5 After areas to receive fill have been cleared and scarified, the surface should be moisture conditioned to achieve the proper moisture content, and compacted as recommended in Section 6 of these specifications.

5. COMPACTION EQUIPMENT

5.1 Compaction of *soil* or *soil-rock* fill shall be accomplished by sheepsfoot or segmented-steel wheeled rollers, vibratory rollers, multiple-wheel pneumatic-tired rollers, or other types of acceptable compaction equipment. Equipment shall be of such a design that it will be capable of compacting the *soil* or *soil-rock* fill to the specified relative compaction at the specified moisture content.

5.2 Compaction of *rock* fills shall be performed in accordance with Section 6.3.

6. PLACING, SPREADING AND COMPACTION OF FILL MATERIAL

6.1 *Soil* fill, as defined in Paragraph 3.1.1, shall be placed by the Contractor in accordance with the following recommendations:

6.1.1 *Soil* fill shall be placed by the Contractor in layers that, when compacted, should generally not exceed 8 inches. Each layer shall be spread evenly and shall be thoroughly mixed during spreading to obtain uniformity of material and moisture in each layer. The entire fill shall be constructed as a unit in nearly level lifts. Rock materials greater than 12 inches in maximum dimension shall be placed in accordance with Section 6.2 or 6.3 of these specifications.

6.1.2 In general, the *soil* fill shall be compacted at a moisture content at or above the optimum moisture content as determined by ASTM D 1557.

6.1.3 When the moisture content of *soil* fill is below that specified by the Consultant, water shall be added by the Contractor until the moisture content is in the range specified.

6.1.4 When the moisture content of the *soil* fill is above the range specified by the Consultant or too wet to achieve proper compaction, the *soil* fill shall be aerated by the Contractor by blading/mixing, or other satisfactory methods until the moisture content is within the range specified.

6.1.5 After each layer has been placed, mixed, and spread evenly, it shall be thoroughly compacted by the Contractor to a relative compaction of at least 90 percent. Relative compaction is defined as the ratio (expressed in percent) of the in-place dry density of the compacted fill to the maximum laboratory dry density as determined in accordance with ASTM D 1557. Compaction shall be continuous over the entire area, and compaction equipment shall make sufficient passes so that the specified minimum relative compaction has been achieved throughout the entire fill.

6.1.6 Where practical, soils having an Expansion Index greater than 50 should be placed at least 3 feet below finish pad grade and should be compacted at a moisture content generally 2 to 4 percent greater than the optimum moisture content for the material.

6.1.7 Properly compacted *soil* fill shall extend to the design surface of fill slopes. To achieve proper compaction, it is recommended that fill slopes be over-built by at least 3 feet and then cut to the design grade. This procedure is considered preferable to track-walking of slopes, as described in the following paragraph.

6.1.8 As an alternative to over-building of slopes, slope faces may be back-rolled with a heavy-duty loaded sheepsfoot or vibratory roller at maximum 4-foot fill height intervals. Upon completion, slopes should then be track-walked with a D-8 dozer or similar equipment, such that a dozer track covers all slope surfaces at least twice.

6.2 *Soil-rock* fill, as defined in Paragraph 3.1.2, shall be placed by the Contractor in accordance with the following recommendations:

6.2.1 Rocks larger than 12 inches but less than 4 feet in maximum dimension may be incorporated into the compacted *soil* fill, but shall be limited to the area measured 15 feet minimum horizontally from the slope face and 5 feet below finish grade or 3 feet below the deepest utility, whichever is deeper.

6.2.2 Rocks or rock fragments up to 4 feet in maximum dimension may either be individually placed or placed in windrows. Under certain conditions, rocks or rock fragments up to 10 feet in maximum dimension may be placed using similar methods. The acceptability of placing rock materials greater than 4 feet in maximum dimension shall be evaluated during grading as specific cases arise and shall be approved by the Consultant prior to placement.

6.2.3 For individual placement, sufficient space shall be provided between rocks to allow for passage of compaction equipment.

6.2.4 For windrow placement, the rocks should be placed in trenches excavated in properly compacted *soil* fill. Trenches should be approximately 5 feet wide and 4 feet deep in maximum dimension. The voids around and beneath rocks should be filled with approved granular soil having a Sand Equivalent of 30 or greater and should be compacted by flooding. Windrows may also be placed utilizing an "open-face" method in lieu of the trench procedure, however, this method should first be approved by the Consultant.

6.2.5 Windrows should generally be parallel to each other and may be placed either parallel to or perpendicular to the face of the slope depending on the site geometry. The minimum horizontal spacing for windrows shall be 12 feet center-to-center with a 5-foot stagger or offset from lower courses to next overlying course. The minimum vertical spacing between windrow courses shall be 2 feet from the top of a lower windrow to the bottom of the next higher windrow.

6.2.6 Rock placement, fill placement and flooding of approved granular soil in the windrows should be continuously observed by the Consultant.

6.3 *Rock* fills, as defined in Section 3.1.3, shall be placed by the Contractor in accordance with the following recommendations:

6.3.1 The base of the *rock* fill shall be placed on a sloping surface (minimum slope of 2 percent). The surface shall slope toward suitable subdrainage outlet facilities. The *rock* fills shall be provided with subdrains during construction so that a hydrostatic pressure buildup does not develop. The subdrains shall be permanently connected to controlled drainage facilities to control post-construction infiltration of water.

6.3.2 *Rock* fills shall be placed in lifts not exceeding 3 feet. Placement shall be by rock trucks traversing previously placed lifts and dumping at the edge of the currently placed lift. Spreading of the *rock* fill shall be by dozer to facilitate *seating* of the rock. The *rock* fill shall be watered heavily during placement. Watering shall consist of water trucks traversing in front of the current rock lift face and spraying water continuously during rock placement. Compaction equipment with compactive energy comparable to or greater than that of a 20-ton steel vibratory roller or other compaction equipment providing suitable energy to achieve the required compaction or deflection as recommended in Paragraph 6.3.3 shall be utilized. The number of passes to be made should be determined as described in Paragraph 6.3.3. Once a *rock* fill lift has been covered with *soil* fill, no additional *rock* fill lifts will be permitted over the *soil* fill.

6.3.3 Plate bearing tests, in accordance with ASTM D 1196, may be performed in both the compacted *soil* fill and in the *rock* fill to aid in determining the required minimum number of passes of the compaction equipment. If performed, a minimum of three plate bearing tests should be performed in the properly compacted *soil* fill (minimum relative compaction of 90 percent). Plate bearing tests shall then be performed on areas of *rock* fill having two passes, four passes and six passes of the compaction equipment, respectively. The number of passes required for the *rock* fill shall be determined by comparing the results of the plate bearing tests for the *soil* fill and the *rock* fill and by evaluating the deflection

variation with number of passes. The required number of passes of the compaction equipment will be performed as necessary until the plate bearing deflections are equal to or less than that determined for the properly compacted *soil* fill. In no case will the required number of passes be less than two.

6.3.4 A representative of the Consultant should be present during *rock* fill operations to observe that the minimum number of "passes" have been obtained, that water is being properly applied and that specified procedures are being followed. The actual number of plate bearing tests will be determined by the Consultant during grading.

6.3.5 Test pits shall be excavated by the Contractor so that the Consultant can state that, in their opinion, sufficient water is present and that voids between large rocks are properly filled with smaller rock material. In-place density testing will not be required in the *rock* fills.

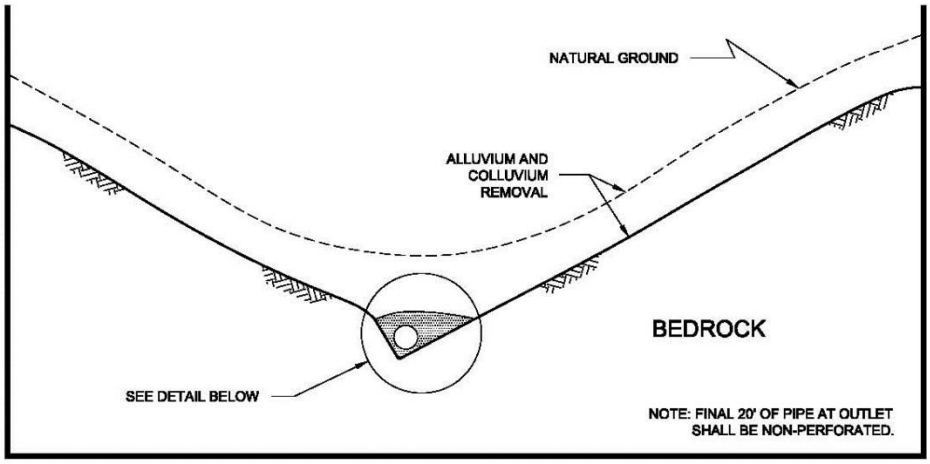
6.3.6 To reduce the potential for "piping" of fines into the *rock* fill from overlying *soil* fill material, a 2-foot layer of graded filter material shall be placed above the uppermost lift of *rock* fill. The need to place graded filter material below the *rock* should be determined by the Consultant prior to commencing grading. The gradation of the graded filter material will be determined at the time the *rock* fill is being excavated. Materials typical of the *rock* fill should be submitted to the Consultant in a timely manner, to allow design of the graded filter prior to the commencement of *rock* fill placement.

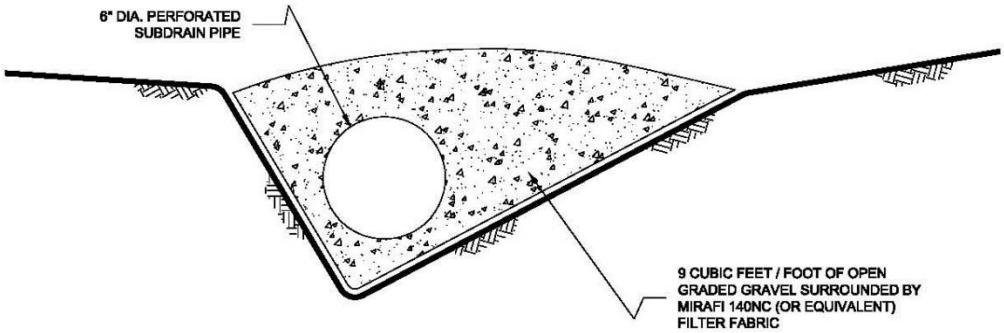
6.3.7 *Rock* fill placement should be continuously observed during placement by the Consultant.

7. SUBDRAINS

7.1 The geologic units on the site may have permeability characteristics and/or fracture systems that could be susceptible under certain conditions to seepage. The use of canyon subdrains may be necessary to mitigate the potential for adverse impacts associated with seepage conditions. Canyon subdrains with lengths in excess of 500 feet or extensions of existing offsite subdrains should use 8-inch-diameter pipes. Canyon subdrains less than 500 feet in length should use 6-inch-diameter pipes.

TYPICAL CANYON DRAIN DETAIL





NOTES:

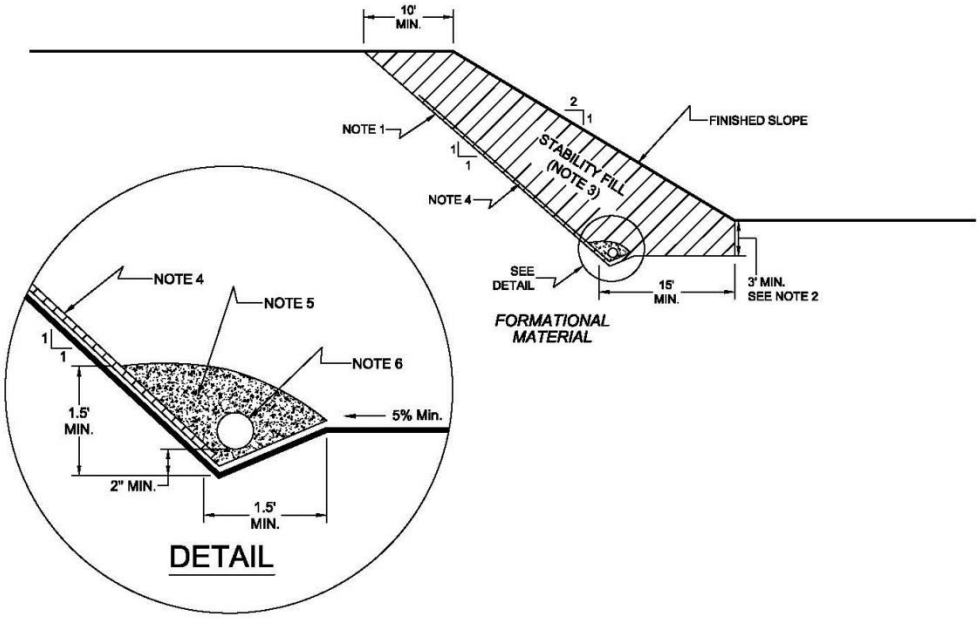
1.....6-INCH DIAMETER, SCHEDULE 80 PVC PERFORATED PIPE FOR FILLS
IN EXCESS OF 100-FEET IN DEPTH OR A PIPE LENGTH OF LONGER THAN 500 FEET.

2.....6-INCH DIAMETER, SCHEDULE 40 PVC PERFORATED PIPE FOR FILLS
LESS THAN 100-FEET IN DEPTH OR A PIPE LENGTH SHORTER THAN 500 FEET.

NO SCALE

7.2 Slope drains within stability fill keyways should use 4-inch-diameter (or lager) pipes.

TYPICAL STABILITY FILL DETAIL



NOTES:

1.....EXCAVATE BACKCUT AT 1:1 INCLINATION (UNLESS OTHERWISE NOTED).

2.....BASE OF STABILITY FILL TO BE 3 FEET INTO FORMATIONAL MATERIAL, SLOPING A MINIMUM 5% INTO SLOPE.

3.....STABILITY FILL TO BE COMPOSED OF PROPERLY COMPACTED GRANULAR SOIL.

4.....CHIMNEY DRAINS TO BE APPROVED PREFABRICATED CHIMNEY DRAIN PANELS (MIRADRAIN G200N OR EQUIVALENT) SPACED APPROXIMATELY 20 FEET CENTER TO CENTER AND 4 FEET WIDE. CLOSER SPACING MAY BE REQUIRED IF SEEPAGE IS ENCOUNTERED.

5.....FILTER MATERIAL TO BE 3/4-INCH, OPEN-GRADED CRUSHED ROCK ENCLOSED IN APPROVED FILTER FABRIC (MIRAFI 140NC).

6.....COLLECTOR PIPE TO BE 4-INCH MINIMUM DIAMETER, PERFORATED, THICK-WALLED PVC SCHEDULE 40 OR EQUIVALENT, AND SLOPED TO DRAIN AT 1 PERCENT MINIMUM TO APPROVED OUTLET.

NO SCALE

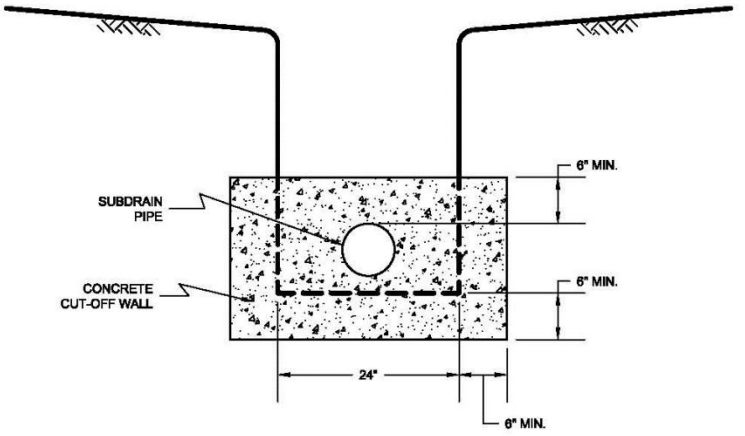
7.3 The actual subdrain locations will be evaluated in the field during the remedial grading operations. Additional drains may be necessary depending on the conditions observed and the requirements of the local regulatory agencies. Appropriate subdrain outlets should be evaluated prior to finalizing 40-scale grading plans.

7.4 *Rock* fill or *soil-rock* fill areas may require subdrains along their down-slope perimeters to mitigate the potential for buildup of water from construction or landscape irrigation. The subdrains should be at least 6-inch-diameter pipes encapsulated in gravel and filter fabric. *Rock* fill drains should be constructed using the same requirements as canyon subdrains.

7.5 Prior to outletting, the final 20-foot segment of a subdrain that will not be extended during future development should consist of non-perforated drainpipe. At the non-perforated/ perforated interface, a seepage cutoff wall should be constructed on the downslope side of the pipe.

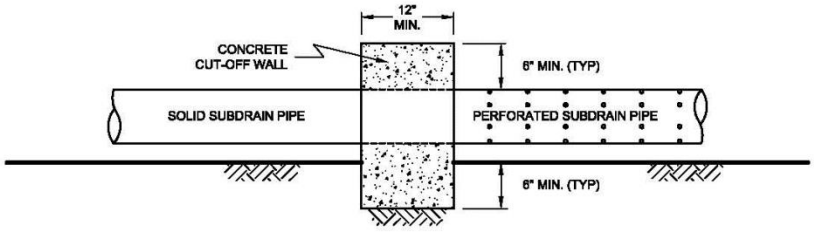
TYPICAL CUT OFF WALL DETAIL

FRONT VIEW



NO SCALE

SIDE VIEW

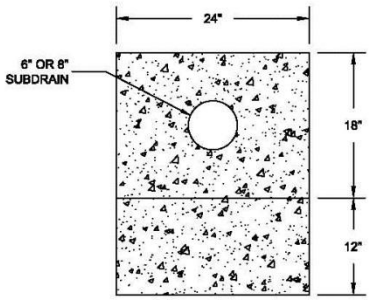


NO SCALE

7.6 Subdrains that discharge into a natural drainage course or open space area should be provided with a permanent headwall structure.

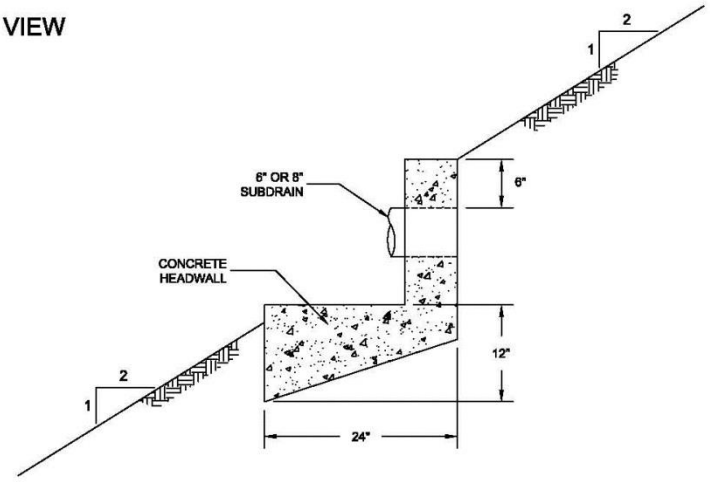
TYPICAL HEADWALL DETAIL

FRONT VIEW



NO SCALE

SIDE VIEW



NOTE: HEADWALL SHOULD OUTLET AT TOE OF FILL SLOPE OR INTO CONTROLLED SURFACE DRAINAGE

NO SCALE

7.7 The final grading plans should show the location of the proposed subdrains. After completion of remedial excavations and subdrain installation, the project civil engineer should survey the drain locations and prepare an "as-built" map showing the drain locations. The final outlet and connection locations should be determined during grading operations. Subdrains that will be extended on adjacent projects after grading can be placed on formational material and a vertical riser should be placed at the end of the subdrain. The grading contractor should consider videoing the subdrains shortly after burial to check proper installation and functionality. The contractor is responsible for the performance of the drains.

8. OBSERVATION AND TESTING

8.1 The Consultant shall be the Owner's representative to observe and perform tests during clearing, grubbing, filling, and compaction operations. In general, no more than 2 feet in vertical elevation of *soil* or *soil-rock* fill should be placed without at least one field density test being performed within that interval. In addition, a minimum of one field density test should be performed for every 2,000 cubic yards of *soil* or *soil-rock* fill placed and compacted.

8.2 The Consultant should perform a sufficient distribution of field density tests of the compacted *soil* or *soil-rock* fill to provide a basis for expressing an opinion whether the fill material is compacted as specified. Density tests shall be performed in the compacted materials below any disturbed surface. When these tests indicate that the density of any layer of fill or portion thereof is below that specified, the particular layer or areas represented by the test shall be reworked until the specified density has been achieved.

8.3 During placement of *rock* fill, the Consultant should observe that the minimum number of passes have been obtained per the criteria discussed in Section 6.3.3. The Consultant should request the excavation of observation pits and may perform plate bearing tests on the placed *rock* fills. The observation pits will be excavated to provide a basis for expressing an opinion as to whether the *rock* fill is properly seated and sufficient moisture has been applied to the material. When observations indicate that a layer of *rock* fill or any portion thereof is below that specified, the affected layer or area shall be reworked until the *rock* fill has been adequately seated and sufficient moisture applied.

8.4 A settlement monitoring program designed by the Consultant may be conducted in areas of *rock* fill placement. The specific design of the monitoring program shall be as recommended in the Conclusions and Recommendations section of the project Geotechnical Report or in the final report of testing and observation services performed during grading.

8.5 We should observe the placement of subdrains, to check that the drainage devices have been placed and constructed in substantial conformance with project specifications.

8.6 Testing procedures shall conform to the following Standards as appropriate:

8.6.1 Soil and Soil-Rock Fills:

8.6.1.1 Field Density Test, ASTM D 1556, *Density of Soil In-Place By the Sand-Cone Method.*

8.6.1.2 Field Density Test, Nuclear Method, ASTM D 6938, *Density of Soil and Soil-Aggregate In-Place by Nuclear Methods (Shallow Depth).*

8.6.1.3 Laboratory Compaction Test, ASTM D 1557, *Moisture-Density Relations of Soils and Soil-Aggregate Mixtures Using 10-Pound Hammer and 18-Inch Drop*.

8.6.1.4. Expansion Index Test, ASTM D 4829, *Expansion Index Test*.

9. PROTECTION OF WORK

9.1 During construction, the Contractor shall properly grade all excavated surfaces to provide positive drainage and prevent ponding of water. Drainage of surface water shall be controlled to avoid damage to adjoining properties or to finished work on the site. The Contractor shall take remedial measures to prevent erosion of freshly graded areas until such time as permanent drainage and erosion control features have been installed. Areas subjected to erosion or sedimentation shall be properly prepared in accordance with the Specifications prior to placing additional fill or structures.

9.2 After completion of grading as observed and tested by the Consultant, no further excavation or filling shall be conducted except in conjunction with the services of the Consultant.

10. CERTIFICATIONS AND FINAL REPORTS

10.1 Upon completion of the work, Contractor shall furnish Owner a certification by the Civil Engineer stating that the lots and/or building pads are graded to within 0.1 foot vertically of elevations shown on the grading plan and that all tops and toes of slopes are within 0.5 foot horizontally of the positions shown on the grading plans. After installation of a section of subdrain, the project Civil Engineer should survey its location and prepare an *as-built* plan of the subdrain location. The project Civil Engineer should verify the proper outlet for the subdrains and the Contractor should ensure that the drain system is free of obstructions.

10.2 The Owner is responsible for furnishing a final as-graded soil and geologic report satisfactory to the appropriate governing or accepting agencies. The as-graded report should be prepared and signed by a California licensed Civil Engineer experienced in geotechnical engineering and by a California Certified Engineering Geologist, indicating that the geotechnical aspects of the grading were performed in substantial conformance with the Specifications or approved changes to the Specifications.

LIST OF REFERENCES

CGS (2021a), *EQ Zapp: California Earthquake Hazards Zone Application*, web application that queries California Geological Survey mapped earthquake hazard zones, https://www.conservation.ca.gov/cgs/geohazards/eq-zapp, accessed April, 2023.

CGS (2021b), *California Tsunami Maps and Data*, web application for accessing tsunami inundation hazard, https://www.conservation.ca.gov/cgs/tsunami/maps, accessed April, 2023.

City of San Diego (2008), *Seismic Safety Study, Geologic Hazards and Faults, Map Sheet 7*.

FEMA (2020), *Flood Insurance Rate Map (FIRM), Map Numbers 06073C2178G and 06073C2200G, Effective May 16, 2012*, http://www.fema.gov/portal/home, accessed April, 2023.

Geocon Incorporated, *Geotechnical Investigation, Otay Central Village, Planning Areas 10 – 13 and 17, Airway Road and Cactus Road, San Diego California,* dated April 8, 2019 (Project No. G2338-42-01).

Kennedy, M. P., and Tan, S. S., (2008), *Geologic Map of the San Diego 30′ x 60′ Quadrangle, California*, USGS Regional Geologic Map Series, 1:100,000 Scale, Map No. 3.

Kennedy, M. P., and Tan, S. S., (2002), *Geologic Map of Otay Mesa 7.5′ Quadrangle, San Diego County, California*: A Digital Database, USGS Regional Geologic Map Series, 1:24,000 Scale.

SEAOC (2020), *OSHPD Seismic Design Maps*: Structural Engineers Association of California website, http://seismicmaps.org/, accessed March, 2023.

USGS (2019), *Quaternary Fault and Fold Database of the United States*: U.S. Geological Survey website, https://www.usgs.gov/programs/earthquake-hazards/faults, accessed March, 2023.

STORM WATER MANAGEMENT INVESTIGATION

THE COLLECTIONS AT CACTUS
NORTHEAST CORNER OF AIRWAY ROAD AND CACTUS ROAD
SAN DIEGO, CALIFORNIA

GEOCON
INCORPORATED

GEOTECHNICAL
ENVIRONMENTAL
MATERIALS

PREPARED FOR

JPI
SAN DIEGO, CALIFORNIA

JANUARY 25, 2024
PROJECT NO. G2338-42-02

Project No. G2338-42-02
January 25, 2024

JPI
11988 El Camino Real, Suite 200
San Diego, California 92130

Attention: Mr. Conner Kloeppel

Subject: STORM WATER MANAGEMENT INVESTIGATION
THE COLLECTIONS AT CACTUS
NORTHEAST CORNER OF AIRWAY ROAD AND CACTUS COURT
SAN DIEGO, CALIFORNIA

References:
1. *Soil and Geologic Reconnaissance and Infiltration Testing, Otay Central Village, Planning Areas 10-13 and 17, Airway Road and Cactus Road, San Diego, California*, prepared by Geocon Incorporated, dated February 6, 2019 (Project No. G2338-42-01).
2. *Geotechnical Investigation, Otay Central Village, Planning Areas 10-13 and 17, Airway Road and Cactus Road, San Diego, California*, prepared by Geocon Incorporated, dated April 9, 2019 (Project No. G2338-42-01).
3. *Due Diligence Geotechnical Investigation, The Collections at Cactus, Northeast Corner of Airway Road and Cactus Court, San Diego, California*, prepared by Geocon Incorporated, dated May 18, 2023 (Project No. G2338-42-01).
4. *DMA Exhibit, Proposed Conditions, Collections at Cactus, City of San Diego, California*, prepared by Project Design Consultants, dated October 30, 2023 (Job No. 4481).

Dear Mr. Kloeppel:

In accordance with the request of Project Design Consultants and your authorization, we have prepared a storm water management investigation report for the proposed Collections at Cactus project located in the City of San Diego, California.

SITE AND PROJECT DESCRIPTION

The project site is approximately 40 acres in size, bounded by the SR-905 freeway on the north, Airway Road on the south, Cactus Road on the west, and a partially graded vacant lot to the east. An automobile/truck service yard and several single-story residential homes are located west of the site along Cactus Road.

The property is characterized by gently sloping topography, draining from the southeast to the northwest to a drainage channel running parallel to the east-bound lanes of the SR-905 freeway. Existing site

elevations range from approximately 494 to 515 feet Mean Sea Level (MSL). Based on a review of historical aerial photographs, previous land uses include cultivation of small orchards and arable farming.

We understand the proposed development consists of constructing multi-story residential buildings including townhomes, stacked flats, and apartments. The project will also have a 3.5-acre park, parking lots, and biofiltration basins for storm water management. Based on preliminary grading information, the majority of planned grading will result in cuts and fills of approximately 5 feet or less from existing grades to construct planned sheet grade elevations across the site. A retaining wall with heights between 1 and 10 feet is planned on the northeast site perimeter.

SOIL AND GEOLOGIC CONDITIONS

We encountered topsoil and terrace deposits (clay and sand/gravel members) during our previous geologic reconnaissance and geotechnical investigation as summarized in References 1 and 2. Although not encountered during our investigations, the Otay Formation is expected to be present below the terrace deposits. The surficial soil and geologic units are discussed below. A geologic map is provided as Figure 1 using the referenced DMA map as our base map.

Topsoil (Unmapped)

Topsoil blankets the entire site and is generally composed of very soft to stiff, sandy clay and loose, silty to clayey sand. The topsoil thickness ranges from approximately one to four feet. Topsoil is compressible in its present condition.

Terrace Deposits-Clay Member (Qtc)

The Pleistocene-age upper terrace deposit clay member (Qtc) consists of a highly expansive clay, encountered across the site. The clay member is approximately two to greater than 14 feet thick, consisting of firm to hard, damp to moist, grayish brown to olive brown, clay, silty clay, and sandy clay. The base of the clay member was not found along the south side of the site in trenches TP-12 through TP-14, and is deeper than 14 feet.

Expansion testing performed on this site and other adjacent sites indicates the upper terrace deposit clay member has highly expansive characteristics. Infiltration should be considered infeasible in the clay member of the Terrace Deposits due to its expansion characteristics.

Terrace Deposits-Sand/Gravel Member (Qtg)

The Pleistocene-age lower terrace member (Qtg) underlies the upper clay member, and consists of medium dense to very dense, damp to moist, reddish- to yellowish-brown, medium dense to dense,

clayey, and silty sand with varying amounts of cobble. This unit is massive to weakly stratified, with occasional discontinuous cobble and gravel lenses. The surrounding gravel and cobble clasts range from 3- to 18-inches in diameter, and are derived from volcanic, metasedimentary, and granitic rocks. Cobble clast size generally increases with depth and may exceed 18-inches in deeper excavations.

Otay Formation (To)

The Otay Formation underlies the terrace deposits and is generally composed of dense to hard, light olive to gray-brown, horizontally interbedded clayey siltstones and silty fine-grained sandstone. The Otay Formation was not encountered to the maximum explored depth of 16-feet below site grades. The Otay Formation typically possess low to moderate expansion, good shear strength characteristics, and is generally suitable for support of structural loads and/or fills in its present condition.

GROUNDWATER

We did not encounter groundwater in the trenches or borings during our field investigations. Based on the proposed improvements, we do not expect groundwater to have an adverse impact on the project; however, it is not uncommon for groundwater or seepage conditions to develop where none previously existed. Groundwater elevations are dependent on seasonal precipitation, irrigation, land use, among other factors, and vary as a result. Proper surface drainage will be important to the future performance of the project.

STORM WATER MANAGEMENT INVESTIGATION

We understand storm water management devices are being proposed in accordance with the 2021 City of San Diego Storm Water Standards (SWS). If not properly constructed, there is a potential for distress to improvements and properties located hydrologically down gradient or adjacent to these devices. Factors such as the amount of water to be detained, its residence time, and soil permeability have an important effect on seepage transmission and the potential adverse impacts that may occur if the storm water management features are not properly designed and constructed. We have not performed a hydrogeological study at the site. If infiltration of storm water runoff occurs, downstream properties may be subjected to seeps, springs, slope instability, raised groundwater, movement of foundations and slabs, or other undesirable impacts because of water infiltration.

Hydrologic Soil Group

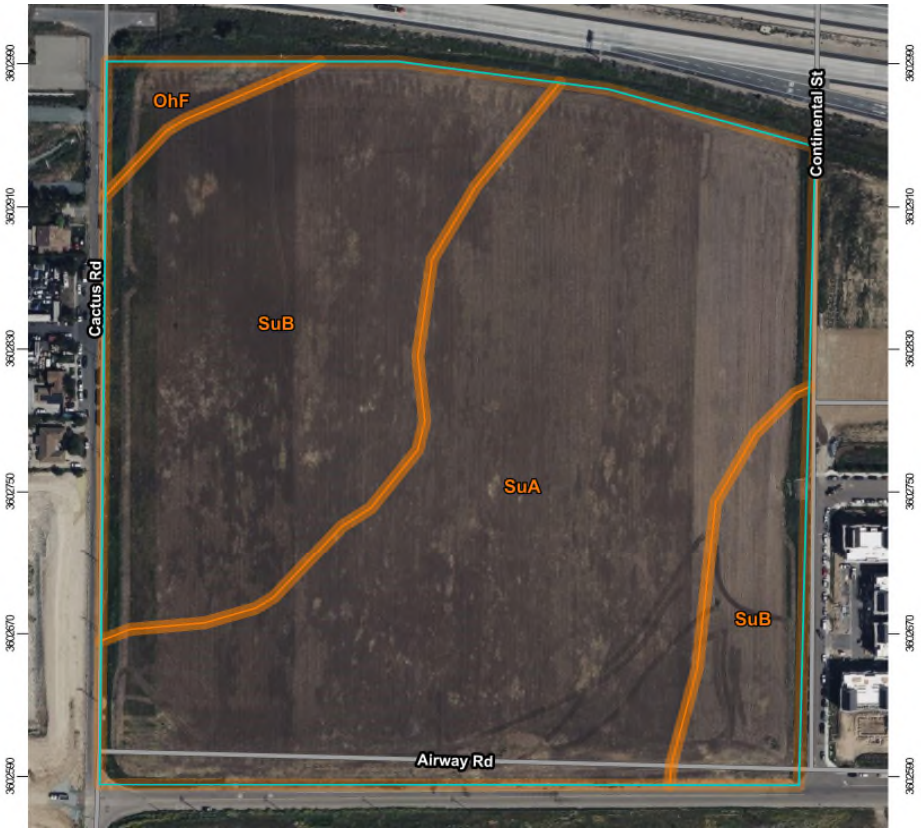
The United States Department of Agriculture (USDA), Natural Resources Conservation Services, possesses general information regarding the existing soil conditions for areas within the United States. The USDA website also provides the Hydrologic Soil Group. Table 1 presents the descriptions of the hydrologic soil groups. If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter

is for drained areas and the second is for undrained areas. In addition, the USDA website also provides an estimated saturated hydraulic conductivity for the existing soil.

TABLE 1
HYDROLOGIC SOIL GROUP DEFINITIONS

Soil Group	Soil Group Definition
A	Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.
B	Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.
C	Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.
D	Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high-water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

The Hydrologic Soil Group Map presents output from the USDA website.



Hydrologic Soil Group Map

Table 2 presents the information from the USDA website for the subject property.

TABLE 2
USDA WEB SOIL SURVEY – HYDROLOGIC SOIL GROUP

Map Unit Name	Map Unit Symbol	Approximate Percentage of Property	Hydrologic Soil Group	k_{SAT} of Most Limiting Layer (Inches/ Hour)
Olivenhain cobbly loam, 30 to 50 percent slopes	OhF	2	D	0.00 – 0.06
Stockpen gravelly clay loam, 0 to 2 percent slopes	SuA	57	D	0.00 – 0.06
Stockpen gravelly clay loam, 2 to 5 percent slopes	SuB	41	D	0.00 – 0.06

In-Situ Testing

We performed constant-head infiltration tests at the locations shown on the Geologic Map, Figure 1. Table 3 presents the results of the infiltration tests. The field data sheets are attached herein. We applied a feasibility factor of safety of 2.0 to our estimated infiltration rates. Soil infiltration rates from in-situ tests can vary significantly from one location to another due to the heterogeneous characteristics inherent to most soil.

TABLE 3
INFILTRATION TEST RESULTS

Test No.	Geologic Unit	Test Elevation (feet, MSL)	Field-Saturated Hydraulic Conductivity/Infiltration Rate, k_{sat} (inch/hour)	Worksheet Infiltration Rate[1] (inch/hour)
A-1	Qtc	91.5	0.322	0.161
A-2	Qtg	91.0	0.027	0.014
A-3	Qtg	92.0	0.035	0.018
A-4	Qtg	92.5	0.063	0.032

[1] Using a Factor of Safety of 2.

Infiltration categories include full infiltration, partial infiltration and no infiltration. Table 4 presents the commonly accepted definitions of the potential infiltration categories based on the infiltration rates.

TABLE 4
INFILTRATION CATEGORIES

Infiltration Category	Field Infiltration Rate, I (Inches/Hour)	Factored Infiltration Rate[1], I (Inches/Hour)
Full Infiltration	$I > 1.0$	$I > 0.5$
Partial Infiltration	$0.10 < I \leq 1.0$	$0.05 < I \leq 0.5$
No Infiltration (Infeasible)	$I < 0.10$	$I < 0.05$

[1] Using a Factor of Safety of 2.

Based on our observations and test results, the factored infiltration rates at test locations A-2 through A-4 indicated rates less than 0.05 inches per hour. The factored infiltration rate at test location A-1 indicated a rate less than 0.5 and greater than 0.05 inches per hour. However, due to the high expansion characteristics of the onsite soils, and the low infiltration rates at test locations A-2 through A-4, partial and full infiltration on the property is considered infeasible, and the site possesses a "No Infiltration" condition.

GEOLOGIC HAZARDS AND CONSIDERATIONS

Groundwater Elevations

We did not encounter groundwater during our previous investigations to depths of 16 feet below existing grades. Therefore, infiltration due to groundwater elevations would be considered feasible based on groundwater elevations.

Soil or Groundwater Contamination

We are unaware of contaminated soil or groundwater contamination on the property. Therefore, infiltration associated with this risk is considered feasible.

New or Existing Utilities

Utilities are located onsite and adjacent to the property within the existing streets. Full and partial infiltration near these utilities should be considered infeasible within these areas.

Existing and Planned Structures

Existing buildings exist to the east and west of the property. Existing city right-of-way and streets, and SR-905 surround the site. Water should not be allowed to infiltrate in areas where it could affect the neighboring properties and existing adjacent structures, improvements, and roadways.

CONCLUSIONS AND RECOMMENDATIONS

Storm Water Evaluation Narrative

The in-place infiltration test locations were selected in areas likely used for potential infiltration devices. We performed 4 infiltration tests within the underlying terrace deposits and the results indicate three of the four tests have a factored rate that is less than 0.05 inches per hour (with an applied factor of safety of 2). The site is underlain by topsoil and terrace deposits overlying Otay Formation. The topsoil and clay member of the terrace deposits exhibit high expansive characteristics, and water that is allowed to infiltrate in highly expansive soils will likely cause distress to proposed and existing structures and improvements. Therefore, full and partial infiltration is considered infeasible at the site.

Storm Water Infiltration Conclusion

Based on the results of our infiltration tests, and the presence of highly expansive soils onsite, we opine full and partial infiltration on the property is considered infeasible and the property possesses a "No Infiltration" condition in accordance with the 2021 SWS.

Storm Water Infiltration Recommendations

Liners and subdrains should be incorporated into the design and construction of the planned storm water devices. The liners should be impermeable (e.g. High-density polyethylene, HDPE, with a thickness of about 30 mil or equivalent Polyvinyl Chloride, PVC) to prevent water migration. The subdrains should be perforated within the liner area, installed at the base and above the liner, be at least 3 inches in diameter and consist of Schedule 40 PVC pipe. The subdrains outside of the liner should consist of solid pipe. The penetration of the liners at the subdrains should be properly waterproofed. The subdrains should be connected to a proper outlet. The devices should also be installed in accordance with the manufacturer's recommendations.

Storm Water Standard Worksheets

The SWS requests the geotechnical engineer complete the *Categorization of Infiltration Feasibility Condition* (Worksheet C.4-1 or Form I-8) worksheet information to help evaluate the potential for infiltration on the property. The attached Worksheet C.4-1 presents the completed information for the submittal process.

The regional storm water standards also have a worksheet (Worksheet D.5-1 or Form I-9) that helps the project civil engineer estimate the factor of safety based on several factors. Table 5 describes the suitability assessment input parameters related to the geotechnical engineering aspects for the factor of safety determination.

TABLE 5
SUITABILITY ASSESSMENT RELATED CONSIDERATIONS FOR INFILTRATION FACILITY SAFETY FACTORS

Consideration	High Concern – 3 Points	Medium Concern – 2 Points	Low Concern – 1 Point
Assessment Methods	Use of soil survey maps or simple texture analysis to estimate short-term infiltration rates. Use of well permeameter or borehole methods without accompanying continuous boring log. Relatively sparse testing with direct infiltration methods	Use of well permeameter or borehole methods with accompanying continuous boring log. Direct measurement of infiltration area with localized infiltration measurement methods (e.g., Infiltrometer). Moderate spatial resolution	Direct measurement with localized (i.e. small-scale) infiltration testing methods at relatively high resolution or use of extensive test pit infiltration measurement methods.
Predominant Soil Texture	Silty and clayey soils with significant fines	Loamy soils	Granular to slightly loamy soils
Site Soil Variability	Highly variable soils indicated from site assessment or unknown variability	Soil boring/test pits indicate moderately homogenous soils	Soil boring/test pits indicate relatively homogenous soils
Depth to Groundwater/ Impervious Layer	<5 feet below facility bottom	5-15 feet below facility bottom	>15 feet below facility bottom

Based on our geotechnical investigation and the previous table, Table 6 presents the estimated factor values for the evaluation of the factor of safety. This table only presents the suitability assessment safety factor (Part A) of the worksheet. The project civil engineer should evaluate the safety factor for design (Part B) and use the combined safety factor for the design infiltration rate.

TABLE 6
FACTOR OF SAFETY WORKSHEET DESIGN VALUES – PART A[1]

Suitability Assessment Factor Category	Assigned Weight (w)	Factor Value (v)	Product (p = w x v)
Assessment Methods	0.25	2	0.50
Predominant Soil Texture	0.25	3	0.75
Site Soil Variability	0.25	2	0.50
Depth to Groundwater/ Impervious Layer	0.25	1	0.25
Suitability Assessment Safety Factor, S_A = □p			2.00

[1.] The project civil engineer should complete Worksheet D.5-1 or Form I-9 using the data on this table. Additional information is required to evaluate the design factor of safety.

Should you have questions regarding this report, or if we may be of further service, please contact the undersigned at your convenience.

Very truly yours,

GEOCON INCORPORATED

Lilian E. Rodriguez
RCE 83227

Rodney C. Mikesell
GE 2533

LER:RCM:arm

(e-mail) Addressee

Categorization of Infiltration Feasibility Condition based on Geotechnical Conditions	Worksheet C.4-1: Form I-8A[10]
Part 1 - Full Infiltration Feasibility Screening Criteria	
DMA(s) Being Analyzed:	**Project Phase:**
Collections at Cactus	Entitlement
Criteria 1: Infiltration Rate Screening	
1A	Is the mapped hydrologic soil group according to the NRCS Web Soil Survey or UC Davis Soil Web Mapper Type A or B and corroborated by available site soil data[11]? ☐ Yes; the DMA may feasibly support full infiltration. Answer "Yes" to Criteria 1 Result or continue to Step 1B if the applicant elects to perform infiltration testing. ☐ No; the mapped soil types are A or B but is not corroborated by available site soil data (continue to Step 1B). ☒ No; the mapped soil types are C, D, or "urban/unclassified" and is corroborated by available site soil data. Answer "No" to Criteria 1 Result. ☐ No; the mapped soil types are C, D, or "urban/unclassified" but is not corroborated by available site soil data (continue to Step 1B).
1B	Is the reliable infiltration rate calculated using planning phase methods from Table D.3-1? ☐ Yes; Continue to Step 1C. ☐ No; Skip to Step 1D.
1C	Is the reliable infiltration rate calculated using planning phase methods from Table D.3-1 greater than 0.5 inches per hour? ☐ Yes; the DMA may feasibly support full infiltration. Answer "Yes" to Criteria 1 Result. ☐ No; full infiltration is not required. Answer "No" to Criteria 1 Result.
1D	**Infiltration Testing Method.** Is the selected infiltration testing method suitable during the design phase (see Appendix D.3)? Note: Alternative testing standards may be allowed with appropriate rationales and documentation. ☐ Yes; continue to Step 1E. ☐ No; select an appropriate infiltration testing method.

[9] Note that it is not required to investigate each and every criterion in the worksheet, a single "no" answer in Part 1, Part 2, Part 3, or Part 4 determines a full, partial, or no infiltration condition.

[10] This form must be completed each time there is a change to the site layout that would affect the infiltration feasibility condition. Previously completed forms shall be retained to document the evolution of the site storm water design.

[11] Available data include site-specific sampling or observation of soil types or texture classes, such as obtained from borings or test pits necessary to support other design elements.

Categorization of Infiltration Feasibility Condition based on Geotechnical Conditions	Worksheet C.4-1: Form I-8A[10]
1E	**Number of Percolation/Infiltration Tests.** Does the infiltration testing method performed satisfy the minimum number of tests specified in Table D.3-2? ☐ Yes; continue to Step 1F. ☐ No; conduct appropriate number of tests.
IF	**Factor of Safety.** Is the suitable Factor of Safety selected for full infiltration design? See guidance in D.5; Tables D.5-1 and D.5-2; and Worksheet D.5-1 (Form I-9). ☐ Yes; continue to Step 1G. ☐ No; select appropriate factor of safety.
1G	**Full Infiltration Feasibility.** Is the average measured infiltration rate divided by the Factor of Safety greater than 0.5 inches per hour? ☐ Yes; answer "Yes" to Criteria 1 Result. ☐ No; answer "No" to Criteria 1 Result.
Criteria 1 Result	Is the estimated reliable infiltration rate greater than 0.5 inches per hour within the DMA where runoff can reasonably be routed to a BMP? ☐ Yes; the DMA may feasibly support full infiltration. Continue to Criteria 2. ☒ No; full infiltration is not required. Skip to Part 1 Result.

Summarize infiltration testing methods, testing locations, replicates, and results and summarize estimates of reliable infiltration rates according to procedures outlined in D.5. Documentation should be included in project geotechnical report.

We performed 4 infiltration tests in terrace deposits within areas of the site that may be considered for storm water devices. Three of the four tests have a rate less than 0.05 inches per hour (with an applied factor of safety of 2). Therefore, full infiltration is considered infeasible at the site.

Categorization of Infiltration Feasibility Condition based on Geotechnical Conditions		Worksheet C.4-1: Form I-8A[10]	
Criteria 2: Geologic/Geotechnical Screening			
2A	If all questions in Step 2A are answered "Yes," continue to Step 2B. For any "No" answer in Step 2A answer "No" to Criteria 2, and submit an "Infiltration Feasibility Condition Letter" that meets the requirements in Appendix C.1.1. The geologic/geotechnical analyses listed in Appendix C.2.1 do not apply to the DMA because one of the following setbacks cannot be avoided and therefore result in the DMA being in a no infiltration condition. The setbacks must be the closest horizontal radial distance from the surface edge (at the overflow elevation) of the BMP.		
2A–1	Can the proposed full infiltration BMP(s) avoid areas with existing fill materials greater than 5 feet thick below the infiltrating surface?	☐ Yes	☐ No
2A-2	Can the proposed full infiltration BMP(s) avoid placement within 10 feet of existing underground utilities, structures, or retaining walls?	☐ Yes	☐ No
2A-3	Can the proposed full infiltration BMP(s) avoid placement within 50 feet of a natural slope (>25%) or within a distance of 1.5H from fill slopes where H is the height of the fill slope?	☐ Yes	☐ No
2B	When full infiltration is determined to be feasible, a geotechnical investigation report must be prepared that considers the relevant factors identified in Appendix C.2.1. If all questions in Step 2B are answered "Yes," then answer "Yes" to Criteria 2 Result. If there are "No" answers continue to Step 2C.		
2B–1	**Hydroconsolidation.** Analyze hydroconsolidation potential per approved ASTM standard due to a proposed full infiltration BMP. Can full infiltration BMPs be proposed within the DMA without increasing hydroconsolidation risks?	☐ Yes	☐ No
2B-2	**Expansive Soils.** Identify expansive soils (soils with an expansion index greater than 20) and the extent of such soils due to proposed full infiltration BMPs. Can full infiltration BMPs be proposed within the DMA without increasing expansive soil risks?	☐ Yes	☐ No

Categorization of Infiltration Feasibility Condition based on Geotechnical Conditions		Worksheet C.4-1: Form I-8A[10]	
2B-3	**Liquefaction**. If applicable, identify mapped liquefaction areas. Evaluate liquefaction hazards in accordance with Section 6.4.2 of the City of San Diego's Guidelines for Geotechnical Reports (2011 or most recent edition). Liquefaction hazard assessment shall take into account any increase in groundwater elevation or groundwater mounding that could occur as a result of proposed infiltration or percolation facilities. Can full infiltration BMPs be proposed within the DMA without increasing liquefaction risks?	☐ Yes	☐ No
2B-4	**Slope Stability**. If applicable, perform a slope stability analysis in accordance with the ASCE and Southern California Earthquake Center (2002) Recommended Procedures for Implementation of DMG Special Publication 117, Guidelines for Analyzing and Mitigating Landslide Hazards in California to determine minimum slope setbacks for full infiltration BMPs. See the City of San Diego's Guidelines for Geotechnical Reports (2011) to determine which type of slope stability analysis is required. Can full infiltration BMPs be proposed within the DMA without increasing slope stability risks?	☐ Yes	☐ No
2B-5	**Other Geotechnical Hazards.** Identify site-specific geotechnical hazards not already mentioned (refer to Appendix C.2.1). Can full infiltration BMPs be proposed within the DMA without increasing risk of geologic or geotechnical hazards not already mentioned?	☐ Yes	☐ No
2B-6	**Setbacks.** Establish setbacks from underground utilities, structures, and/or retaining walls. Reference applicable ASTM or other recognized standard in the geotechnical report. Can full infiltration BMPs be proposed within the DMA using established setbacks from underground utilities, structures, and/or retaining walls?	☐ Yes	☐ No

Categorization of Infiltration Feasibility Condition based on Geotechnical Conditions		Worksheet C.4-1: Form I-8A[10]	
2C	**Mitigation Measures.** Propose mitigation measures for each geologic/geotechnical hazard identified in Step 2B. Provide a discussion of geologic/geotechnical hazards that would prevent full infiltration BMPs that cannot be reasonably mitigated in the geotechnical report. See Appendix C.2.1.8 for a list of typically reasonable and typically unreasonable mitigation measures. Can mitigation measures be proposed to allow for full infiltration BMPs? If the question in Step 2 is answered "Yes," then answer "Yes" to Criteria 2 Result. If the question in Step 2C is answered "No," then answer "No" to Criteria 2 Result.	☐ Yes	☐ No
Criteria 2 Result	Can infiltration greater than 0.5 inches per hour be allowed without increasing risk of geologic or geotechnical hazards that cannot be reasonably mitigated to an acceptable level?	☐ Yes	☐ No

Summarize findings and basis; provide references to related reports or exhibits.

We performed 4 infiltration tests in terrace deposits within areas of the site that may be considered for storm water devices. Three of the four tests have a rate less than 0.05 inches per hour (with an applied factor of safety of 2). Therefore, full infiltration is considered infeasible at the site.

Part 1 Result – Full Infiltration Geotechnical Screening[12]	Result
If answers to both Criteria 1 and Criteria 2 are "Yes", a full infiltration design is potentially feasible based on Geotechnical conditions only. If either answer to Criteria 1 or Criteria 2 is "No", a full infiltration design is not required.	☐ Full infiltration Condition ☒ Complete Part 2

[12] To be completed using gathered site information and best professional judgement considering the definition of MEP in the MS4 Permit. Additional testing and/or studies may be required by City Engineer to substantiate findings.

Categorization of Infiltration Feasibility Condition based on Geotechnical Conditions	Worksheet C.4-1: Form I-8A[10]
Part 2 – Partial vs. No Infiltration Feasibility Screening Criteria	
DMA(s) Being Analyzed:	**Project Phase:**
Collections at Cactus	Entitlement
Criteria 3: Infiltration Rate Screening	
3A	**NRCS Type C, D, or "urban/unclassified":** Is the mapped hydrologic soil group according to the NRCS Web Soil Survey or UC Davis Soil Web Mapper is Type C, D, or "urban/unclassified" and corroborated by available site soil data? ☐ Yes; the site is mapped as C soils and a reliable infiltration rate of 0.15 in/hr. is used to size partial infiltration BMPS. Answer "Yes" to Criteria 3 Result. ☐ Yes; the site is mapped as D soils or "urban/unclassified" and a reliable infiltration rate of 0.05 in/hr. is used to size partial infiltration BMPS. Answer "Yes" to Criteria 3 Result. ☒ No; infiltration testing is conducted (refer to Table D.3-1), continue to Step 3B.
3B	**Infiltration Testing Result:** Is the reliable infiltration rate (i.e. average measured infiltration rate/2) greater than 0.05 in/hr. and less than or equal to 0.5 in/hr? ☐ Yes; the site may support partial infiltration. Answer "Yes" to Criteria 3 Result. ☒ No; the reliable infiltration rate (i.e. average measured rate/2) is less than 0.05 in/hr., partial infiltration is not required. Answer "No" to Criteria 3 Result.
Criteria 3 Result	Is the estimated reliable infiltration rate (i.e., average measured infiltration rate/2) greater than or equal to 0.05 inches/hour and less than or equal to 0.5 inches/hour at any location within each DMA where runoff can reasonably be routed to a BMP? ☐ Yes; Continue to Criteria 4. ☒ No: Skip to Part 2 Result.
Summarize infiltration testing and/or mapping results (i.e. soil maps and series description used for infiltration rate). We performed 4 infiltration tests in terrace deposits within areas of the site that may be considered for storm water devices. Three of the four tests have a rate less than 0.05 inches per hour (with an applied factor of safety of 2). Therefore, full infiltration is considered infeasible at the site.	

Categorization of Infiltration Feasibility Condition based on Geotechnical Conditions		Worksheet C.4-1: Form I-8A[10]	
Criteria 4: Geologic/Geotechnical Screening			
4A	If all questions in Step 4A are answered "Yes," continue to Step 4B. For any "No" answer in Step 4A answer "No" to Criteria 4 Result, and submit an "Infiltration Feasibility Condition Letter" that meets the requirements in Appendix C.1.1. The geologic/geotechnical analyses listed in Appendix C.2.1 do not apply to the DMA because one of the following setbacks cannot be avoided and therefore result in the DMA being in a no infiltration condition. The setbacks must be the closest horizontal radial distance from the surface edge (at the overflow elevation) of the BMP.		
4A–1	Can the proposed partial infiltration BMP(s) avoid areas with existing fill materials greater than 5 feet thick?	☒ Yes	☐ No
4A-2	Can the proposed partial infiltration BMP(s) avoid placement within 10 feet of existing underground utilities, structures, or retaining walls?	☒ Yes	☐ No
4A-3	Can the proposed partial infiltration BMP(s) avoid placement within 50 feet of a natural slope (>25%) or within a distance of 1.5H from fill slopes where H is the height of the fill slope?	☒ Yes	☐ No
4B	When full infiltration is determined to be feasible, a geotechnical investigation report must be prepared that considers the relevant factors identified in Appendix C.2.1 If all questions in Step 4B are answered "Yes," then answer "Yes" to Criteria 4 Result. If there are any "No" answers continue to Step 4C.		
4B–1	**Hydroconsolidation.** Analyze hydroconsolidation potential per approved ASTM standard due to a proposed full infiltration BMP. Can partial infiltration BMPs be proposed within the DMA without increasing hydroconsolidation risks?	☒ Yes	☐ No
4B-2	**Expansive Soils.** Identify expansive soils (soils with an expansion index greater than 20) and the extent of such soils due to proposed full infiltration BMPs. Can partial infiltration BMPs be proposed within the DMA without increasing expansive soil risks?	☐ Yes	☒ No

Categorization of Infiltration Feasibility Condition based on Geotechnical Conditions		Worksheet C.4-1: Form I-8A[10]	
4B-3	**Liquefaction**. If applicable, identify mapped liquefaction areas. Evaluate liquefaction hazards in accordance with Section 6.4.2 of the City of San Diego's Guidelines for Geotechnical Reports (2011). Liquefaction hazard assessment shall take into account any increase in groundwater elevation or groundwater mounding that could occur as a result of proposed infiltration or percolation facilities. Can partial infiltration BMPs be proposed within the DMA without increasing liquefaction risks?	☒ Yes	☐ No
4B-4	**Slope Stability**. If applicable, perform a slope stability analysis in accordance with the ASCE and Southern California Earthquake Center (2002) Recommended Procedures for Implementation of DMG Special Publication 117, Guidelines for Analyzing and Mitigating Landslide Hazards in California to determine minimum slope setbacks for full infiltration BMPs. See the City of San Diego's Guidelines for Geotechnical Reports (2011) to determine which type of slope stability analysis is required. Can partial infiltration BMPs be proposed within the DMA without increasing slope stability risks?	☒ Yes	☐ No
4B-5	**Other Geotechnical Hazards.** Identify site-specific geotechnical hazards not already mentioned (refer to Appendix C.2.1). Can partial infiltration BMPs be proposed within the DMA without increasing risk of geologic or geotechnical hazards not already mentioned?	☒ Yes	☐ No
4B-6	**Setbacks.** Establish setbacks from underground utilities, structures, and/or retaining walls. Reference applicable ASTM or other recognized standard in the geotechnical report. Can partial infiltration BMPs be proposed within the DMA using recommended setbacks from underground utilities, structures, and/or retaining walls?	☒ Yes	☐ No
4C	**Mitigation Measures.** Propose mitigation measures for each geologic/geotechnical hazard identified in Step 4B. Provide a discussion on geologic/geotechnical hazards that would prevent partial infiltration BMPs that cannot be reasonably mitigated in the geotechnical report. See Appendix C.2.1.8 for a list of typically reasonable and typically unreasonable mitigation measures. Can mitigation measures be proposed to allow for partial infiltration BMPs? If the question in Step 4C is answered "Yes," then answer "Yes" to Criteria 4 Result. If the question in Step 4C is answered "No," then answer "No" to Criteria 4 Result.	☐ Yes	☒ No

Categorization of Infiltration Feasibility Condition based on Geotechnical Conditions		Worksheet C.4-1: Form I-8A[10]	
Criteria 4 Result	Can infiltration of greater than or equal to 0.05 inches/hour and less than or equal to 0.5 inches/hour be allowed without increasing the risk of geologic or geotechnical hazards that cannot be reasonably mitigated to an acceptable level?	☐ Yes	☒ No

Summarize findings and basis; provide references to related reports or exhibits.

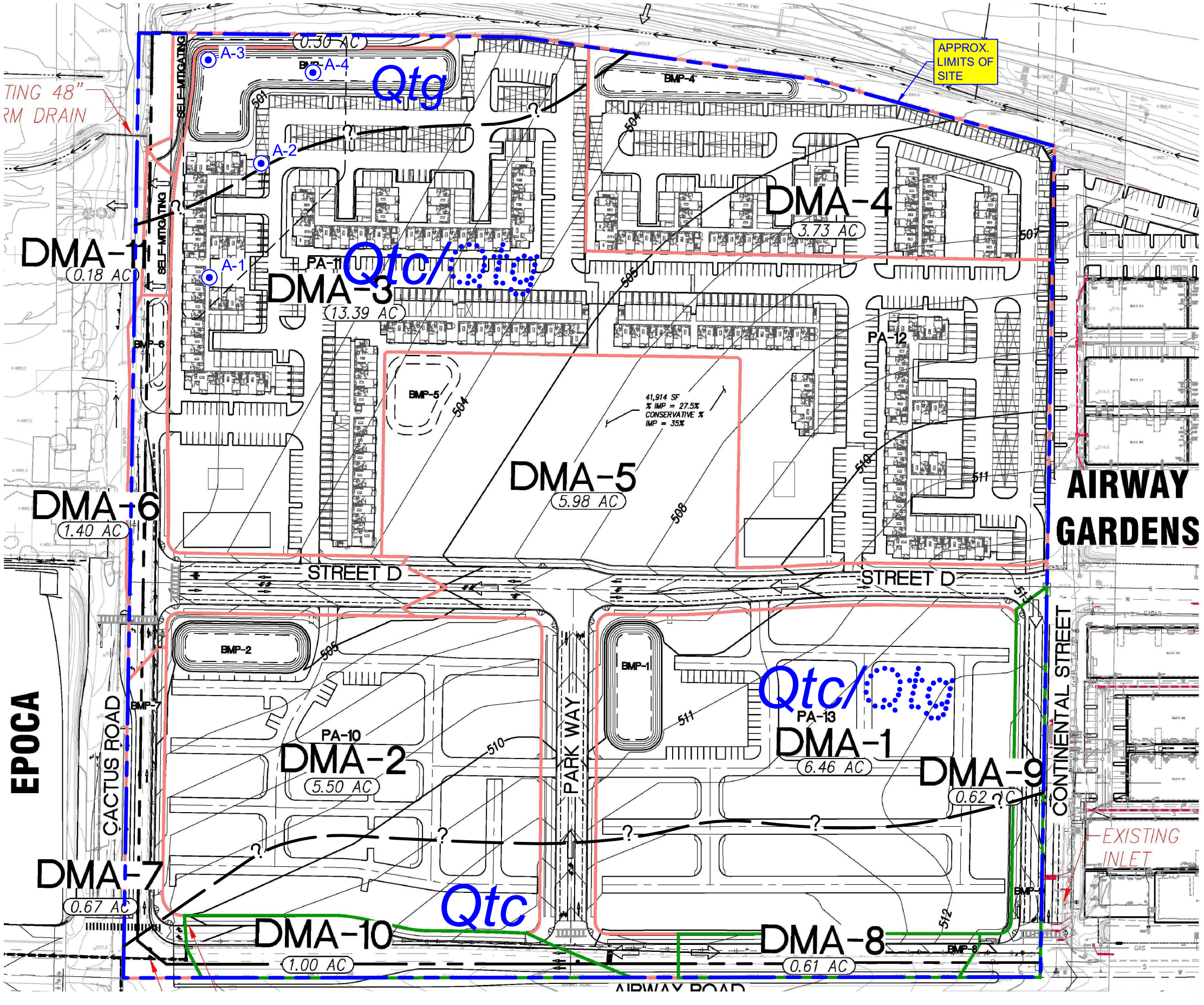
We performed 4 infiltration tests in terrace deposits within areas of the site that may be considered for storm water devices. Three of the four tests have a rate less than 0.05 inches per hour (with an applied factor of safety of 2). Therefore, full infiltration is considered infeasible at the site.

The site is underlain by topsoil and terrace deposits overlying Otay Formation. The topsoil and clay member of the terrace deposits exhibit high expansive characteristics, and water that is allowed to infiltrate in highly expansive soils will likely cause distress to proposed and existing structures and improvements. Therefore, full and partial infiltration is considered infeasible at the site.

Part 2 – Partial Infiltration Geotechnical Screening Result[13]	Result
If answers to both Criteria 3 and Criteria 4 are "Yes", a partial infiltration design is potentially feasible based on geotechnical conditions only. If answers to either Criteria 3 or Criteria 4 is "No", then infiltration of any volume is considered to be infeasible within the site.	☐ Partial Infiltration Condition ☒ No Infiltration Condition

[13] To be completed using gathered site information and best professional judgement considering the definition of MEP in the MS4 Permit. Additional testing and/or studies may be required by City Engineer to substantiate findings.

THE COLLECTIONS AT CACTUS
SAN DIEGO, CALIFORNIA



0' 75' 150' 225' 300'

SCALE 1"=150'(on 11x17)

GEOCON LEGEND

Qtc .....TERRACE DEPOSITS - CLAY MEMBER

Qtg .....TERRACE DEPOSITS - SAND/GRAVEL MEMBER

~?~ .....APPROX. LOCATION OF GEOLOGIC CONTACT (Queried Where Uncertain)

A-4 ◉ .....APPROX. LOCATION OF INFILTRATION TESTING

GEOLOGIC MAP

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PROJECT NO. G2338 - 42 - 02
FIGURE 1
DATE 01 - 25 - 2024

Plotted:01/25/2024 12:55PM | By:ALVIN LADRILLONO | File Location:Y:\PROJECTS\G2338-42-02 (Paez Property)\SHEETS\G2338-42-02 Geo Map.20.dwg