NOISE IMPACT ANALYSIS

Alante 10211 Rancho Carmel Drive San Diego, California 92128

Prepared For

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1.0 EXECUTIVE SUMMARY

The proposed project, known as Alante, consists of the construction of a four-story, 50-unit residential building on top of an existing parking structure to be retained. The project site is located at 10211 Rancho Carmel Drive in the City of San Diego, California.

The current and future noise environment primarily consists of traffic noise from Rancho Carmel Drive, Ted Williams Parkway, and Interstate 15 (I-15). Future noise impacts at building facades are expected to range from 56 CNEL at the east-facing facade on the second floor, to approximately 71 CNEL at the west-facing facade of the first floor.

The City of San Diego Noise Element to the General Plan requires that residential outdoor use areas be protected from noise levels greater than 65 CNEL. As designed, future traffic noise levels are expected to be 65 CNEL or less at all common outdoor use areas and private balconies where noise standards would apply, with the exception of the private balconies at the northwest corner of the building. Additional project design features would be required in these locations. With solid balcony barriers with a height of 3.5 feet at the first floor and four feet at the second through fourth floors at the northwest corner of the building, future traffic noise levels are expected to be reduced to be 65 CNEL and therefore would be in compliance with City of San Diego exterior noise standards. More information is provided in Section 5.1.

The City of San Diego and State of California require interior noise levels of 45 CNEL or less in residential units. Calculations show that future noise levels on site exceed 60 CNEL at most facades, and therefore interior noise levels may exceed 45 CNEL within units. Due to high noise levels on-site, an exterior-to-interior analysis should be performed when building plans become available, prior to the issuance of building permits. The required interior noise levels are feasible and can be achieved with readily available building materials and construction methods. It is anticipated that a typical exterior wall, windows and glass doors with an STC rating of 28, and mechanical ventilation in units will be sufficient for achieving compliant interior noise levels; however, this should be confirmed when construction documents become available.

Noise from the anticipated HVAC equipment on site has been calculated to determine impacts at off-site receivers. Calculations show that noise levels from the mechanical equipment will be in compliance with the City of San Diego noise regulations found within the Municipal Code. No project design features are deemed necessary to control project-generated noise impacts from mechanical equipment. Project-generated traffic noise is also expected to be less than significant.

Noise levels from temporary construction activities associated with this project are expected to comply with the applicable City of San Diego construction noise limits at all surrounding property lines, with activity limited to the daytime hours of 7 a.m. to 7 p.m. during all phases of construction. Construction is prohibited between the hours of 7 p.m. and 7 a.m. and on Sundays or legal holidays. Though it is not required by regulations, the general good practice construction noise control methods listed herein should be followed, as a courtesy to surrounding properties.

The proposed project is not expected to result in any potentially significant noise impacts by the standards of the California Environmental Quality Act (CEQA). Noise impacts are summarized in Section 5.5.

2.0 INTRODUCTION

This acoustical analysis report is submitted to satisfy the noise requirements of the City of San Diego. Its purpose is to assess noise impacts from nearby roadway traffic to identify project features or requirements necessary to achieve exterior noise levels of 65 CNEL or less at outdoor use areas, and interior noise levels of 45 CNEL or less in habitable residential spaces. In addition, this report assesses noise impacts from potential project-related noise sources, such as mechanical equipment and project-generated traffic, as well as temporary construction noise. This analysis aims to determine if additional project design features are necessary and feasible to reduce these impacts to comply with the applicable noise regulations of the City of San Diego Noise Element to the General Plan and Municipal Code. Potential impacts will also be assessed for significance per the California Environmental Quality Act (CEQA).

All noise level or sound level values presented herein are expressed in terms of decibels, with Aweighting to approximate the hearing sensitivity of humans. Time-averaged noise levels are expressed by the symbol L_{EQ} , for a specified duration. The Community Noise Equivalent Level (CNEL) is a calculated 24-hour weighted average, where sound levels during evening hours of 7 p.m. to 10 p.m. have an added 5 dB weighting, and sound levels during nighttime hours of 10 p.m. to 7 a.m. have an added 10 dB weighting. This is similar to the Day-Night sound level, L_{DN} , which is a 24-hour average with an added 10 dB weighting on the same nighttime hours but no added weighting on the evening hours. According to the California Department of Transportation's Technical Noise Supplement to the Traffic Noise Analysis Protocol (see reference), peak hour traffic noise levels are typically found to be close to predicted CNEL values. Sound levels expressed in CNEL are always based on A-weighted decibels. These metrics are used to express noise levels for both measurement and municipal regulations, for land use guidelines, and for enforcement of noise ordinances. Further explanation can be provided upon request.

Sound pressure is the actual noise experienced by a human or registered by a sound level instrument. When sound pressure is used to describe a noise source, the distance from the noise source must be specified in order to provide complete information. Sound power, on the other hand, is a specialized analytical metric to provide information without the distance requirement, but it may be used to calculate the sound pressure at any desired distance.

2.1 **Project Description**

The proposed project, known as Alante, consists of the construction of a four-story, 50-unit residential building on top of an existing parking structure to be retained. The project proposes a mixture of one and two-bedroom units with common and private outdoor use areas for residents. For additional project details, please refer to the project plans provided in Appendix A.

The project site is surrounded by an abandoned golf course to the north, multifamily residential uses to the southeast/east, and commercial uses to the south (across Provencal Place). The property to the west of the site (across Rancho Carmel Drive) is a public park. Single-family residential properties are located at a considerable distance from the project site to the north, beyond the abandoned golf course.

2.2 **Project Location**

The project site is located at 10211 Rancho Carmel Drive in the City of San Diego, California. The Assessor's Parcel Number (APN) is 313-680-18-00. The site is currently occupied by an existing two-story parking garage. For a graphical representation of the site, please refer to the Vicinity Map, Assessor's Parcel Map, Satellite Aerial Photograph, and Topographic Map, provided as Figures 1 through 4, respectively.

2.3 Applicable Noise Regulations

This acoustical report is submitted to satisfy the acoustical requirements of the City of San Diego Noise Element to the General Plan and Municipal Code.

The City of San Diego Noise Element to the General Plan and California Building Code require interior noise levels not exceeding 45 CNEL in habitable residential space. The City of San Diego requires that noise levels at residential outdoor use areas do not exceed 65 CNEL. This exterior noise standard applies to common outdoor use areas and private patios or balconies with a depth of greater than six feet.

The City of San Diego Municipal Code, Section 59.5.0401 specifies noise limits based on the land use of the properties in question. Although the City of San Diego Municipal Code states that noise limits apply "on the boundaries of the property," as the intent of the code is to protect actual occupied areas, noise levels have been evaluated at the nearest noise-sensitive receivers beyond adjacent roadways and sidewalks. The most restrictive nighttime noise limits at surrounding land uses are 50 dBA for high-density multi-family residential (to the southeast) and 60 dBA at commercial properties to the south. There are no exterior noise limits in the code that would apply to the abandoned golf course to the north or the public park to the west, but for purposes of this analysis, the single-family residential limit of 40 dBA has been applied for a worst-case analysis.

Additionally, Section 59.5.0404 of the City of San Diego Municipal Code states that construction activity is prohibited between the hours of 7 p.m. and 7 a.m. and on Sundays or legal holidays. During permissible hours of operation, noise levels from construction activity must be limited to a twelve-hour average of no greater than 75 dBA at any property line zoned for residential use.

Also, the City of San Diego Significance Determination Thresholds (Section K) should be used to determine whether or not a project will have a significant impact on surrounding properties. In order to determine whether or not a project will have a significant impact on surrounding properties, the following must be considered:

- 1. Would the project result or create a significant increase (3 dBA or more) in the existing ambient noise levels?
- 2. Would the project expose people to noise levels which exceed the City's adopted noise ordinance or are incompatible with Table K-4?
- 3. Would the project expose people to current or future transportation noise levels which exceed standards established in the Transportation Element of the General Plan or an adopted airport Comprehensive Land Use Plan?
- 4. Would the project result in land uses which are not compatible with aircraft noise levels as defined by an adopted airport Comprehensive Land Use Plan (CLUP)?

Please refer to Appendix B for pertinent sections of the City of San Diego Noise Element to the General Plan, the City of San Diego Municipal Code, and Significance Determination Thresholds.

3.0 ENVIRONMENTAL SETTING

3.1 Existing Noise Environment

The primary noise sources in the vicinity of the project site includes automobile and truck traffic noise from Rancho Carmel Drive, Ted Williams Parkway, and Interstate 15 (I-15). No other noise source is considered significant.

3.1.1 Roadway Traffic Noise

Current traffic volumes are given based on traffic counts from the San Diego Association of Governments (SANDAG) Transportation Data, traffic counts by Linscott Law and Greenspan (LLG) for the traffic impact study for the project, and the Caltrans Traffic Census (see references).

Rancho Carmel Drive is a four-lane, two-way Major Arterial running north-south along the west boundary of the project site. The posted speed limit is 45 mph. In the vicinity of the project site, Rancho Carmel Drive currently carries a traffic volume of approximately 14,500 Average Daily Trips (ADT) as of the year 2013 according to SANDAG counts. LLG existing traffic counts show volumes of 13,700 ADT south of Provencal Place and 11,630 ADT north of Provencal Place. As SANDAG counts exceed those provided by LLG, SANDAG counts will be used for current traffic modeling.

Ted Williams Parkway is a six-lane, two-way Prime Arterial running east-west to the south of the project site. The posted speed limit is 55 mph. In the vicinity of the project site, Ted Williams Parkway currently carries a traffic volume of approximately 35,300 ADT as of the year 2014 according to SANDAG counts. LLG existing traffic counts show a volume of 43,590 ADT for this roadway. As LLG counts exceed those provided by SANDAG, LLG counts will be used for current traffic modeling.

I-15 is a 14-lane, two-way Freeway running north-south to the west of the project site. The posted speed limit is 65 mph. In the vicinity of the project site, I-15 currently carries a traffic volume of approximately 238,000 ADT as of the year 2017, according to Caltrans traffic counts.

Caltrans traffic information shows that the segment of I-15 near the proposed project site currently carries approximately 3.46% medium trucks and 3.64% heavy trucks. No current or future truck percentages were available for other roadways in the vicinity of the project site. However, based on neighboring and surrounding land use, roadway classification, professional experience and on-site observations, a truck percentage mix of 3.0% medium and 2.0% heavy trucks was used for Ted Williams Parkway, and a mix of 1.0% medium and 1.0% heavy trucks was used for Rancho Carmel Drive.

Current and future traffic volumes and vehicle mixes for roadway sections near the project site are shown in Table 1. For more information, please refer to Appendix C: Cadna Analysis Data and Results.

Table 1. Overall Roadway Traffic Information							
Deschusse Norma	Speed Limit	Vehicle Mix (%)		Current Traffic	Future Traffic		
Roadway Name	(mph)	Medium Trucks	Heavy Trucks	(Year)	(2035)		
Rancho Carmel Drive	45	1.0	1.0	14,500 (2013)	23,100 / 22,100*		
Ted Williams Parkway	55	3.0	2.0	43,590 (2019)	67,800		
I-15 Northbound	65	3.46	3.64	119,000 (2017)	134,400		
I-15 Southbound	65	3.46	3.64	119,000 (2017)	127,000		

*Future traffic volumes for Rancho Carmel Drive are given for segments north and south of Provencal Place, respectively.

Without existing or proposed on-site structures, the current traffic noise contours calculated at ground level showed that traffic noise impacts to the project site are between 61 and 70 CNEL. For a graphical representation of these contours, please refer to Figure 5: Satellite Aerial Photograph Showing Current Traffic CNEL Contours and Noise Measurement Location.

3.1.2 Measured Noise Level

An on-site inspection and traffic noise measurement were made on the afternoon of May 20, 2019. The noise measurement was made using the methodology described in Section 4.1 at the northeast corner of Rancho Carmel Drive and Provencal Place, approximately 50 feet from the Rancho Carmel Drive centerline. The microphone was placed at approximately five feet above the road grade. Traffic volumes for Rancho Carmel Drive were recorded for automobiles, medium-size trucks, and large trucks during the measurement period. After a continuous 15-minute sound level measurement, no changes in the L_{EQ} were observable and results were recorded. The measured noise level and related weather conditions are found in Table 2.

Table 2. On-Site Noise Measurement Conditions and Results				
Date	Monday, May 20, 2019			
Time	4:22 p.m. – 4:39 p.m.			
Cloudy skies, 11 mph wind, temperature in the low 60s with moderate humidity				
Measured Noise Level 69.7 dBA LEQ				

3.1.3 Calculated Noise Level

Noise levels were calculated for the site using the methodology described in Section 4.1 for the location, conditions, and traffic volumes counted during the noise measurements. The calculated noise levels (L_{EQ}) were compared with the measured on-site noise level to determine if adjustments or corrections (calibration) should be applied to the traffic noise prediction model. Adjustments are intended to account for site-specific variances in overall reflectivity or absorption, which may not be accurately represented by the default settings in the model.

The measured noise level of 69.7 dBA L_{EQ} at the northeast corner of Rancho Carmel Drive and Provencal Place was compared to the calculated (modeled) noise level of 69.7 dBA L_{EQ} , for the same weather conditions and traffic flow. According to the Federal Highway Administration's Highway Traffic Noise: Analysis and Abatement Guide (see reference), a traffic noise model is considered validated if the measured and calculated noise impacts differ by three decibels or less. No adjustment was deemed necessary to model future noise levels for this noise model as the difference between the measured and calculated levels was found to be less than three decibels. The traffic noise model is assumed to be representative of actual traffic noise that is experienced on site. This information is presented in Table 3.

Table 3. Calculated versus Measured Traffic Noise Data					
Calibration Receiver Position Calculated Measured Difference Correction					
50 feet from Rancho Carmel Drive centerline	69.7 dBA L _{EQ}	69.7 dBA L _{EQ}	0 dB	None applied	

3.2 Future Noise Environment

3.2.1 Future Transportation Noise

The future on-site noise environment will be the result of the same noise sources. The future (year 2035) traffic volumes for surrounding local roadways were provided in the LLG traffic study. Future traffic volumes for I-15 and Ted Williams Parkway were provided by the SANDAG Series 13 Transportation Forecast Information Center (see reference). By the year 2035, the traffic volume of Rancho Carmel Drive is expected to increase to approximately 22,100 ADT north of Provencal Place and 23,100 ADT and 23,100 ADT south of Provencal Place. According to the traffic study, the traffic volume of Ted Williams Parkway is expected to increase to approximately 48,000 ADT by the year 2035; however, SANDAG projects approximately 67,800 ADT by the year 2035. The higher of the two values was used for the modeling of future traffic noise impacts to the site. In 2035, the traffic volume of I-15 is expected to increase to approximately 134,000 ADT traveling northbound and 127,000 ADT traveling southbound.

The same truck percentages from the current traffic volumes were used for future traffic volume modeling. Additional information is provided in Appendix C: Cadna Analysis Data and Results.

Future traffic noise contours were calculated at ground level and showed that traffic noise impacts to the project site will increase slightly to be between 63 and 72 CNEL. For a graphical representation of these contours, please refer to Figure 6: Satellite Aerial Photograph Showing Future Traffic CNEL Contours and Noise Measurement Location.

3.2.2 Mechanical Equipment On-Site

The primary source of noise generated by the proposed project is anticipated to be HVAC equipment. Equipment will be roof-mounted on the buildings. A typical HVAC unit was selected that is assumed to be representative of a unit that could be used on site for each residential unit. The typical unit selected is manufactured by Carrier, and is model number CA13NA030 (2.5-ton capacity). Sound power levels have been provided by the manufacturer in octave band values and a sound rating value. As the sum of octave band noise levels given was found to be slightly less than the given sound rating, the octave band noise levels were increased accordingly such that the

total sum was equal to the sound rating. The resultant estimated spectrum for the unit is shown below in Table 4. Manufacturer data sheets have been provided as Appendix D.

Table 4. Sound Power Levels of Carrier CA13NA030 (Typical 2.5-ton Unit)								
Source	Sound Power at Octave Band Frequency (dBA)						Total	
oouree	125	250	500	1K	2K	4K	8K	(dBA)
Carrier CA13NA030	52.7	62.2	66.2	67.2	65.2	60.2	55.2	72

Operational mechanical noise levels have been calculated for the project site using the above information. Results of this analysis are provided in Section 5.3.1.

3.2.3 Project-Generated Traffic

A traffic impact study conducted by Linscott Law and Greenspan shows traffic volumes generated by the proposed project and the distribution of these trips on surrounding roadways. The impacts of project-generated traffic noise have been assessed using these trip generation values and the existing, opening year (year 2022), and future (year 2035) traffic volumes for surrounding roadways. Project traffic volumes and the analysis of project-generated traffic noise is provided in Section 5.3.2.

3.2.4 Temporary Construction Equipment

In order to evaluate anticipated temporary construction noise impacts, information from the project applicant and typical assumptions have been made regarding stages of construction and equipment to be used. The equipment list in Table 5 is typical of what is expected to be used on site based on the information provided and professional experience. Construction equipment noise levels were obtained from the DEFRA Construction Equipment Noise Database (see reference).

Table 5. Anticipated Construction Stages and Equipment Noise Levels						
Stage of Construction	Equipment	Duty Cycle (%)	Noise Level, at 50 feet (dBA)			
Linderground Litilities	Backhoe	40	64			
Underground Unities	Concrete Saw	20	80			
Equipation Exervation	Drill Rig	20	79			
Foundation	Dump Truck	40	75			
	Concrete Saw	20	80			
Carago Boinforcomont	Concrete Mixer Truck	40	71			
Galage Reinforcement	Concrete Pump	20	71			
	Jackhammer	20	79			
	Crane	16	66			
Vertical Construction	Concrete Mixer Truck	40	71			
	Concrete Pump	20	71			

These noise levels have been incorporated into the temporary construction noise analysis for the site, provided in Section 5.4.

4.0 METHODOLOGY AND EQUIPMENT

4.1 Methodology

4.1.1 Field Measurement

Typically, a "one-hour" equivalent sound level measurement (L_{EQ} , A-Weighted) is recorded for at least one noise-sensitive location on the site. During the on-site noise measurement, start and end times are recorded, vehicle counts are made for cars, medium trucks (double-tires/two axles), and heavy trucks (three or more axles) for the corresponding road segment(s). Supplemental sound measurements of one hour or less in duration are often made to further describe the noise environment of the site.

For measurements of less than one hour in duration, the measurement time is long enough for a representative traffic volume to occur and the noise level (L_{EQ}) to stabilize. The vehicle counts are then converted to one-hour equivalent volumes by applying an appropriate factor. Other field data gathered include measuring or estimating distances, angles-of-view, slopes, elevations, roadway grades, and vehicle speeds. This information is subsequently verified using available maps and records.

4.1.2 Roadway Noise Calculation

The Traffic Noise Model (TNM) calculation protocol in Cadna Version 2019 (based on the methodology used in TNM Version 2.5, released in February 2004 by the U.S. Department of Transportation) was used for all traffic modeling in the preparation of this report. Using the TNM protocol, the CNEL is calculated as 0.092 times the ADT for surrounding roadways, based on the studies made by Wyle Laboratories (see reference). CNEL is calculated for desired receptor locations using road alignment, elevations, lane configurations, projected traffic volumes, estimated truck mixes, and vehicle speeds. Noise attenuation methods may be analyzed, tested, and planned with Cadna, as required.

In order to determine the estimated traffic volumes of roadways during the traffic noise measurement made on site for model calibration, the approximate percentage of the Average Daily Trips (ADT) value for the time period in which the measurement is made is incorporated into the traffic model. These percentages have been established in a study performed by Katz-Okitsu and Associates, Traffic Engineers (see reference). For purposes of calibrating the Cadna TNM, 8.6% of the ADT values for the current environment were used in calculations (for roadways that were not manually counted) to account for traffic between the hours of 4 p.m. and 5 p.m. in the vicinity of the project site. In addition, in order to determine anticipated minimum ambient noise levels at the site for determination of the significance of noise impacts, traffic noise levels have been calculated as 0.1% of the ADT values for the current environment, to account for the lowest amount of traffic that would occur during a single hour of the day.

4.1.3 Cadna Noise Modeling Software

Modeling of the outdoor noise environment is accomplished using Cadna Version 2019, which is a model-based computer program developed by DataKustik for predicting noise impacts in a wide variety of conditions. Cadna (Computer Aided Noise Abatement) assists in the calculation, presentation, assessment, and alleviation of noise exposure. It allows for the input of project information such as noise source data, barriers, structures, and topography to create a detailed model and uses the most up-to-date calculation standards to predict outdoor noise impacts. Noise standards used by Cadna that are particularly relevant to this analysis include ISO 9613 (Attenuation of sound during propagation outdoors). Cadna provides results that are in line with basic acoustical calculations for distance attenuation and barrier insertion loss.

4.1.4 Formulas and Calculations

Decibel Addition

To determine the combined logarithmic noise level of two known noise source levels, the values are converted to the base values, added together, and then converted back to the final logarithmic value, using the following formula:

$$L_{c} = 10\log(10^{L1/10} + 10^{L2/10} + 10^{LN/10})$$

where L_c = the combined noise level (dB), and L_N = the individual noise sources (dB).

This procedure is also valid when used successively for each added noise source beyond the first two. The reverse procedure can be used to estimate the contribution of one source when the contribution of another concurrent source is known and the combined noise level is known. These methods can be used for L_{EQ} or other metrics (such as L_{DN} or CNEL), as long as the same metric is used for all components.

Project-Generated Traffic Noise Impacts

Changes in traffic noise levels can be predicted by inputting the ratio of the two scenarios into the following logarithmic equation:

$$\Delta = 10 \log(V2/V1)$$

where: Δ = Change in sound energy, V1 = original or existing traffic volume, and V2 = future or cumulative traffic volume.

Construction Vibration Calculations

The construction vibration assessment contained herein is evaluated using calculations of peak particle velocity (PPV). PPV at receivers is calculated as follows:

$$PPV_{equip} = PPV_{ref} \times (25/D)^{1.5}$$

where PPV_{equip} is the peak particle velocity (in inches per second) of the equipment, adjusted for distance,

 $\mathsf{PPV}_{\mathsf{ref}}$ is the reference vibration level (in inches per second) at a distance of 25 feet from the equipment, and

D is the distance from the equipment to the receiver.

4.2 Measurement Equipment

The following equipment was used at the site to measure existing noise levels:

- Larson Davis Model LxT Type 1 Integrating Sound Level Meter, Serial #4084
- Larson Davis Model CA250 Type 1 Calibrator, Serial #2106

The sound level meter was field-calibrated immediately prior to the noise measurement and checked afterward, to ensure accuracy. All sound level measurements conducted and presented in this report, in accordance with the regulations, were made with a sound level meter that conforms to the American National Standards Institute specifications for sound level meters (ANSI S1.4). All instruments are maintained with National Bureau of Standards traceable calibration, per the manufacturers' standards.

5.0 NOISE IMPACTS

5.1 Exterior

5.1.1 Noise Impacts to Outdoor Use Areas

As per the City of San Diego Noise Element to the General Plan, outdoor use areas of multi-family land uses should not exceed 65 CNEL for residential areas. The common outdoor use areas are located on the first and second floors, and a private balcony is provided for each unit. The City of San Diego requires compliance with this noise standard at balconies with a depth of greater than six feet. Common areas and balconies with a depth exceeding six feet were evaluated to determine if traffic noise levels exceed 65 CNEL. For both common areas and balconies, receivers were placed at a height of four feet (relative to the deck floor height) to estimate the height of a seated adult.

Future traffic noise levels for the common outdoor use areas are shown in Table 6, and take the shielding provided by the building into account. Receiver locations are shown in Figure 7.

Table 6. Future Traffic Noise Levels at Common Outdoor Use Areas					
Receiver	Exterior Noise Level (CNEL)				
OU1	First Floor Common Area	64			
OU2	Second Floor Common Area	65			

As shown in Table 6, exterior traffic noise levels at the common areas are not expected to exceed the 65 CNEL noise limit set by the City of San Diego. For this reason, no additional project design

features are required for the proposed common areas. The common outdoor use areas are therefore expected to comply with the City of San Diego Noise Element to the General Plan as designed.

Private balconies are located around the perimeter of the building at all units, and balconies with a depth exceeding six feet are located along the north building facade. Future traffic noise levels at private outdoor balconies are shown in Table 7. Receiver locations are shown in Figure 7.

Table 7. Future Traffic Noise Levels at Private Balconies						
Dessiver	Leastian	Exterior Noise Level (CNEL)				
Receiver	Location	First Floor	Second Floor	Third Floor	Fourth Floor	
OU3	Northwest	69	68	68	68	
OU4	North	65	64	64	64	
OU5	North	63	63	63	63	
OU6	North	65	64	65	65	
OU7	North	63	62	63	64	
OU8	North	60	60	60	61	
OU9	North	62	61	62	62	

As shown above, private balconies at the northwest corner of the building are expected to be exposed to traffic noise levels that exceed 65 CNEL in the future noise environment, and therefore, additional project design features are required in those areas.

The proposed project currently incorporates balcony barrier walls at all balconies. With proposed balcony barriers at the northwest corner of the building modified to be constructed as a solid sound barrier with a minimum height of 3.5 feet at the first floor and four feet at the second through fourth floors, noise impacts would be reduced to be 65 CNEL in these locations. With these project design features in place, all private outdoor use areas would be expected to comply with the City of San Diego Noise Element to the General Plan.

The required balcony barriers should be 3.5 feet high at the first floor and four feet high at the second through fourth floors, relative to the deck floor height. A sound wall should be solid and constructed of masonry, wood, plastic, fiberglass, steel, or a combination of those materials, with no cracks or gaps, through or below the wall. Any seams or cracks must be filled or caulked as much as possible. If wood is used, it can be tongue and groove and must be at least 7/8-inch thick or have a surface density of at least 3½ pounds per square foot. Where architectural or aesthetic factors allow, glass or clear plastic may be used, if it is desirable to preserve a view. A glass or plexiglass railing wall should be sufficient for sound attenuation in these locations.

5.1.2 Noise Impacts at Building Facades

Future traffic noise impacts at building facades were calculated and show that noise levels are expected to range from approximately 56 CNEL at the east-facing facade on the second floor, to approximately 71 CNEL at the west-facing facade of the first floor. Noise levels are shown in Table 8, and receiver locations are shown in Figure 8.

Table 8. Future Traffic Noise Levels at Building Facades							
Boosiyar	Leastion		Exterior Noise Level (CNEL)				
Receiver	Location	First Floor	Second Floor	Third Floor	Fourth Floor		
F1	West	71	70	70	70		
F2	North	66	66	66	66		
F3	North	64	63	64	65		
F4	North	63	62	63	63		
F5	North	61	61	61	62		
F6	East	56	57	58	59		
F7	South	63	64	64	65		
F8	South	63	65	65	65		
F9	South	67	67	67	67		

5.2 Interior

The State of California and the City of San Diego require buildings to be designed in order to attenuate, control, and maintain interior noise levels to 45 CNEL or less in habitable residential space. Current exterior building construction is generally expected to achieve at least 15 decibels of exterior-to-interior noise attenuation, with windows opened, according to the U.S. EPA (see reference). Therefore, proposed project building structures exposed to exterior noise levels greater than 60 CNEL could be subject to interior noise levels exceeding the 45 CNEL noise limit for residential habitable space.

As shown in Table 8, the maximum future noise impact anticipated at project building facades is above 60 CNEL. As building facade noise impacts are expected to exceed 60 CNEL, interior noise levels may exceed 45 CNEL with standard building construction. Therefore, a detailed interior noise analysis should be performed for this project prior to the issuance of building permits, to determine design elements necessary to maintain compliant interior noise levels. However, the required interior noise levels are feasible and can be achieved with readily available building materials and construction methods. From a preliminary review, it is anticipated that a typical exterior wall, windows and glass doors with an STC rating of 28, and mechanical ventilation in units will be sufficient for achieving compliant interior noise levels; however, this can be confirmed when construction documents become available.

5.3 Permanent Project-Related Noise Impacts

5.3.1 Mechanical Equipment Noise

Noise levels from HVAC units were calculated in Cadna at the nearest properties using data presented in Section 3.2.2. All equipment was assumed to be in constant operation for 100 percent of the time, although in actuality, equipment will only operate intermittently. Calculations consider the topography of the surrounding area as well as shielding that would be provided by the proposed on-site structure, with the exception of any parapet walls. For this reason, the analysis is considered to represent a conservative estimate of noise impacts at off-site receivers.

Table 9 shows the project-related mechanical noise impacts at surrounding receivers. All receivers have been calculated at a height of five feet above their respective grade with the exception of receiver R5, which was calculated at a height of 15 feet above grade to account for receivers at the second story of the adjacent residential property. Additional information is provided in Appendix C: Cadna Analysis Data and Results. For a graphic showing mechanical equipment noise source and receiver locations, please refer to Figure 9.

Table 9. Project-Related Mechanical Noise Impacts					
Receiver	Description	Noise Limit (dBA)	Noise Level (dBA)		
R1	North Property Line	40	31		
R2	South Property Line (Across Provencal)	60	36		
R3	Southeast Property Line	50	31		
R4	Southeast Residential Building, 1st Floor	50	28		
R5	Southeast Residential Building, 2nd Floor	50	29		
R6	West Property Line (Across Rancho Carmel)	40	25		

As shown above, noise levels at adjacent property lines are anticipated to comply with the applicable nighttime noise limits of the City of San Diego with the project as currently designed. For these reasons, no additional project design features are deemed necessary to reduce noise impacts from rooftop mechanical equipment.

5.3.2 Project-Generated Traffic Noise

According to LLG traffic projections, the proposed project is anticipated to add the following number of ADT to surrounding roadways:

- 50 ADT to Rancho Carmel Drive, north of Provencal Place
- 260 ADT to Rancho Carmel Drive, south of Provencal Place
- 200 ADT to Ted Williams Parkway
- 30 ADT to Sabre Springs Parkway

An analysis of the potential change in traffic noise levels to the surrounding area has been evaluated based on these traffic projections in comparison to existing, opening year (2022), and future (2035) traffic volumes. A significant impact is generally expected to be an increase of three decibels. Project-generated traffic noise increases are shown in Table 10.

Table 10. Anticipated Traffic Noise Increases with Project-Generated Traffic						
		Traffic Volu	Noise Level			
Road Segment	Scenario	No Project	With Project	Increase (dB)		
	Existing	11,630	11,680	0.0		
Rancho Carmel Drive (North of Provencal)	Opening Year (2022)	12,340	12,390	0.0		
	Future (2035)	22,100	22,150	0.0		
	Existing	13,700	13,960	0.1		
Rancho Carmel Drive (South of Provencal)	Opening Year (2022)	14,540	14,800	0.1		
	Future (2035)	23,100	23,360	0.0		
	Existing	43,590	43,790	0.0		
Ted Williams Parkway	Opening Year (2022)	46,260	46,760	0.0		
	Future (2035)	48,000	48,200	0.0		
	Existing	16,750	16,780	0.0		
Sabre Springs Parkway	Opening Year (2022)	17,780	17,810	0.0		
	Future (2035)	19,560	19,590	0.0		

As shown in Table 10, based on the minimal amount of traffic generated by the project relative to traffic volumes without the project, the increase in noise levels on surrounding roadways will be well below the three-decibel threshold of significance. Project-generated traffic noise levels are therefore less than significant.

5.4 Temporary Construction Noise Impacts

According to the City of San Diego Municipal Code, construction activity is prohibited between the hours of 7 p.m. and 7 a.m. and on Sundays or legal holidays. During permissible hours of operation, noise levels from construction activity must be limited to a twelve-hour average of no greater than 75 dBA at any property line zoned for residential use.

Noise levels were calculated at the nearest receiver to the southeast, as any other off-site receivers are located at a greater distance from the project site and therefore would be exposed to lesser noise impacts. Construction noise sources were placed near the center of the work area to

evaluate typical impacts to this receiver as equipment moves around the property. The approximate center of work is located roughly 75 feet from the nearest sensitive receiver location on the southeast property. Noise calculations consider typical duty cycles of equipment, to account for periods of activity and inactivity on the site.

Calculated construction noise impacts are shown in Table 11. A graphical representation of evaluated source and receiver locations is shown in Figure 10. Please refer to Appendix E for additional information.

Table 11. Temporary Construction Noise Levels at Nearest Residential Receiver (Southeast)					
Stage	12-Hour Average Noise Level (dBA)				
Underground Utilities	Backhoe, Concrete Saw	70			
Foundation Excavation	Drill Rig, Dump Truck	71			
Garage Reinforcement	Concrete Saw, Concrete Mixer Truck, Concrete Pump, Jackhammer	73			
Vertical Construction	Crane, Concrete Mixer Truck, Concrete Pump	66			

As shown in Table 11, based on the typical noise levels and duty cycles of construction equipment, 12-hour average hourly noise levels are anticipated to remain below 75 dBA at the nearest noise-sensitive property lines. Any other noise-sensitive properties are located at a greater distance from on-site activity and therefore would be exposed to lesser noise levels.

Despite the fact that noise impacts are expected to remain in compliance with the construction noise limit of the City of San Diego, the following "good practice" measures should still be practiced as a courtesy to residential neighbors.

- 1. Staging areas should be placed as far as possible from residential receivers (west side of the property).
- 2. Place stationary equipment in locations that will have a lesser noise impact on nearby sensitive receivers.
- 3. Turn off equipment when not in use.
- 4. Limit the use of enunciators or public address systems, except for emergency notifications.
- 5. Equipment used in construction should be maintained in proper operating condition, and all loads should be properly secured, to prevent rattling and banging.
- 6. Schedule work to avoid simultaneous construction activities that both generate high noise levels.
- 7. Use equipment with effective mufflers.
- 8. Minimize the use of backup alarms.

With operating hours limited to those permitted by the City of San Diego and adherence to the general good practice construction noise control techniques, temporary construction noise impacts are expected to be less than significant at surrounding properties.

5.5 CEQA Significance Determination

5.5.1 City of San Diego Significance Determination Thresholds

The noise impacts to the project site and from the project site on surrounding properties was taken into account using methodology given in the City of San Diego's CEQA Significance Determination Thresholds document. In order to determine whether or not the project will have a significant impact on surrounding properties, the City's Initial Study Checklist was used, and is addressed as follows:

1. Would the project result in a significant increase (3 dBA or more) in the existing ambient noise levels?

Minimum ambient noise levels were projected using the methodology detailed in Section 4.1.2 and were combined with the projected HVAC equipment noise impacts to determine the cumulative noise impact and the increase in ambient noise levels resulting from operation of the project. Results are shown in Table 12.

Table 12. Calculated Cumulative Noise Impacts at Surrounding Property Lines						
Receiver Number	Receiver Location	Noise Level (dBA)				Impost
		Minimum Ambient	HVAC	Cumulative	Ambient Increase	inpact
R1	North Property Line	45.6	31.1	45.8	0.2	Less than Significant
R2	South Property Line (Across Provencal)	44.4	35.5	44.9	0.5	Less than Significant
R3	Southeast Property Line	44.7	30.9	44.9	0.2	Less than Significant
R4	Southeast Residential Building, 1st Floor	43.9	27.5	44.0	0.1	Less than Significant
R5	Southeast Residential Building, 2nd Floor	42.8	29.2	43.0	0.2	Less than Significant
R6	West Property Line (Across Rancho Carmel)	50.4	25.3	50.4	0.0	Less than Significant

The results in Table 12 demonstrate that the increase in ambient noise levels from HVAC operation will be less than 3 dBA. Additionally, as demonstrated in Section 5.3.2 of this report, noise impacts from project-generated traffic are not expected to cause a significant increase (greater than three decibels) on any surrounding roadway. This impact is also considered to be less than significant.

As the project creates less than a 3 dBA increase in the existing ambient noise levels, its impact is considered to be less than significant at surrounding properties.

2. Would the project expose people to noise levels which exceed the City's adopted noise ordinance or are incompatible with Table K-4?

Per the analysis shown in Sections 5.3 and 5.4, noise impacts from the proposed project would not exceed the City's adopted noise ordinance. It is the understanding of the undersigned that Table K-4 is no longer applicable, as the City of San Diego Noise Element to the General Plan was updated in 2015. For this reason, Table NE-3 shall be used to demonstrate compliance. As the maximum property line noise limit of 36 dBA at the south property line is well below the most restrictive limit in Table NE-3 of the City of San Diego Noise Element to the General Plan (60 CNEL), the project will also not exceed any of the limits in this table. Please see Appendix B for a copy of Table NE-3.

3. Would the project expose people to current or future transportation noise levels which exceed standards established in the Transportation Element to the General Plan or an adopted airport Comprehensive Land Use Plan?

As shown in Section 5.1, with solid balcony barrier walls incorporated as project design features in the required locations, noise impacts at outdoor use areas of the project site would be adequately controlled to be 65 CNEL or less, in compliance with the transportation noise standards of the City of San Diego Noise Element to the General Plan. Therefore, the project will not expose people to current or future transportation noise levels which exceed standards established in the General Plan. The project is also not located within an airport influence area and therefore would not be subject to compliance with an airport Comprehensive Land Use Plan.

4. Would the project result in land uses which are not compatible with aircraft noise levels as defined by an adopted airport Comprehensive Land Use Plan (CLUP)?

The proposed project lies outside any airport noise exposure areas, and would therefore not result in any land uses which are not compatible with aircraft noise levels as defined by an adopted airport CLUP.

Using the methodology given in the City of San Diego's Significance Determination Thresholds Document, it has been determined that the proposed project will have a less than significant impact on surrounding properties.

5.5.2 CEQA Guidelines Environmental Checklist

Noise impacts from the project site are summarized below and classified per the noise portion of the CEQA Environmental Checklist form. This list summarizes conclusions made within the report and classifies the level of significance as: Potentially Significant Impact, Less than Significant with Mitigation Incorporated, Less than Significant Impact, or No Impact.

Italics are used to denote language from the CEQA Environmental Checklist form.

- XII. NOISE—Would the project result in:
- a) Generation of a substantial temporary or permanent increase in ambient noise levels in the vicinity of the project in excess of standards established in the local general plan or noise ordinance, or applicable standards of other agencies?

Less Than Significant Impact. Operational noise impacts calculated in Section 5.3.1 are not expected to generate a substantial permanent increase in ambient noise levels in the vicinity of the

project site. A substantial increase would be considered an increase of three decibels or more, which would represent a doubling of sound energy. The comparison of HVAC noise impacts to existing minimum ambient noise projections is shown in Table 12, and demonstrates a less than significant increase in ambient noise levels.

Additionally, as demonstrated in Section 5.3.2 of this report, noise impacts from project-generated traffic are not expected to cause a significant increase (greater than three decibels) on any surrounding roadway. This impact is also considered to be less than significant.

As shown in Section 5.4 of this report, noise from temporary construction is expected be less than significant considering the anticipated construction schedule and assuming that equipment is maintained in proper operating condition and using appropriate mufflers. Noise impacts from anticipated construction activity are expected to remain at or below the 75 dBA construction noise limit set by the City of San Diego. Additionally, no construction activity will take place during the more sensitive nighttime hours when ambient noise levels tend to be lower, as per City of San Diego requirements. For these reasons, this impact is deemed to be less than significant.

As demonstrated above, the project is not expected to cause a substantial permanent or temporary increase in ambient noise levels, and therefore, this impact can be classified as less than significant.

b) Generation of excessive groundborne vibration or groundborne noise levels?

Less Than Significant Impact. The proposed foundation excavation phase of construction is expected to generate the highest vibration levels of the four phases, as it consists of caisson drilling. According to the Federal Transit Administration Transit Noise and Vibration Assessment Manual (see reference), caisson drilling generates a peak particle velocity (PPV) of approximately 0.089 inches/second at a distance of 25 feet from equipment. The evaluation of an impact's significance can be determined by reviewing both the likelihood of annoyance to individuals as well as the potential for damage to existing structures. According to the Caltrans Transportation and Construction Vibration Guidance Manual (see reference), the appropriate threshold for damage to modern residential structures is a PPV of 0.5 inches/second. Annoyance is assessed based on levels of perception, with a PPV of 0.01 being considered "barely perceptible," 0.04 inches/second as "distinctly perceptible," 0.1 inches/second as "strongly perceptible," and 0.4 inches/second as "severe."

The location of caisson drilling is currently unknown; however, it is estimated that the nearest location would be approximately 25 feet from the nearest residential structure, when caissons are drilled beneath the eastern portion of the building. At this distance, the PPV would be approximately 0.089 inches/second. This level of vibration falls well below the building damage PPV criteria of 0.5 inches/second. The impact falls between the "distinctly perceptible" and "strongly perceptible" PPV criteria for annoyance; however, vibration would be reduced to "distinctly perceptible" levels by the time drilling is located at a distance of 50 feet from receivers, and "barely perceptible" at 100 feet from receivers. As construction vibration is not anticipated to cause damage to off-site buildings and will only approach the threshold of "strongly perceptible" vibration for a short period of time when work is performed on the eastern portion of the building, it is the opinion of the undersigned that temporary construction vibration impacts would not be "excessive" and therefore are less than significant. Please refer to Appendix E for additional information.

c) For a project located within the vicinity of a private airstrip or an airport land use plan or, where such a plan has not been adopted, within two miles of a public airport or public use airport, would the project expose people residing or working in the project area to excessive noise levels?

No Impact. The project site is not located within an airport land use plan nor is it located within two miles of a private airstrip, public airport, or public use airport. Therefore, the proposed project would not expose people working in the project area to excessive noise levels from such uses.

6.0 CONCLUSION

The City of San Diego Noise Element to the General Plan requires that residential outdoor use areas be protected from noise levels greater than 65 CNEL. As designed, future traffic noise levels are expected to be 65 CNEL or less at all common outdoor use areas and private balconies where noise standards would apply, with the exception of the private balconies at the northwest corner of the building. Additional project design features would be required in these locations. With solid balcony barriers with a height of 3.5 feet at the first floor and four feet at the second through fourth floors at the northwest corner of the building, future traffic noise levels are expected to be reduced to be 65 CNEL and therefore would be in compliance with City of San Diego exterior noise standards. More information is provided in Section 5.1.

The City of San Diego and State of California require interior noise levels of 45 CNEL or less in residential units. Calculations show that future noise levels on site exceed 60 CNEL at most facades, and therefore interior noise levels may exceed 45 CNEL within units. Due to high noise levels on-site, an exterior-to-interior analysis should be performed when building plans become available, prior to the issuance of building permits. The required interior noise levels are feasible and can be achieved with readily available building materials and construction methods. It is anticipated that a typical exterior wall, windows and glass doors with an STC rating of 28, and mechanical ventilation in units will be sufficient for achieving compliant interior noise levels; however, this should be confirmed when construction documents become available.

Noise from the anticipated HVAC equipment on site has been calculated to determine impacts at off-site receivers. Calculations show that noise levels from the mechanical equipment will be in compliance with the City of San Diego noise regulations found within the Municipal Code. No project design features are deemed necessary to control project-generated noise impacts from mechanical equipment. Project-generated traffic noise is also expected to be less than significant.

Noise levels from temporary construction activities associated with this project are expected to comply with the applicable City of San Diego construction noise limits at all surrounding property lines, with activity limited to the daytime hours of 7 a.m. to 7 p.m. during all phases of construction. Construction is prohibited between the hours of 7 p.m. and 7 a.m. and on Sundays or legal holidays. Though it is not required by regulations, the general good practice construction noise control methods listed herein should be followed, as a courtesy to surrounding properties.

The proposed project is not expected to result in any potentially significant noise impacts by the standards of the California Environmental Quality Act (CEQA). Noise impacts are summarized in Section 5.5.

7.0 CERTIFICATION

All recommendations for noise control are based on the best information available at the time our consulting services are provided. However, as there are many factors involved in sound transmission, and Eilar Associates has no control over the construction, workmanship or materials, Eilar Associates is specifically not liable for final results of any recommendations or implementation of the recommendations.

This report is based on the related project information received and measured noise levels, and represents a true and factual analysis of the acoustical impact issues associated with the Alante project, to be located in the City of San Diego, California. This report was prepared by Amy Hool and Jonathan Brothers.

Amy Hool, Senior Acoustical Consultant

Jonathan Brothers, Principal Acoustical Consultant

8.0 REFERENCES

- 1. City of San Diego Noise Element to the General Plan, June 2015.
- 2. City of San Diego Municipal Code, Article 9.5: Noise Abatement and Control.
- 3. City of San Diego Significance Determination Thresholds, January 2011.
- 4. California Environmental Quality Act (CEQA), Statute and Guidelines, 2018.
- 5. San Diego Association of Governments (SANDAG) Website, Demographics and Other Data, 2013 Transportation Data, http://www.sandag.org/resources/demographics_and_other_data/transportation/adtv/index.asp.
- 6. Linscott Law and Greenspan Engineers, Traffic Projections for Alante, Provided September 5, 2019.
- 7. Caltrans Traffic Census, 2016 Traffic Volumes on California State Highways, http://www.dot.ca.gov/trafficops/census/.
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- 9. Federal Highway Administration, Highway Traffic Noise: Analysis and Abatement Guide, December 2011.
- 10. San Diego Association of Governments (SANDAG) Traffic Forecast Information Center, Series 13, http://tfic.sandag.org.
- 11. Department for Environment Food and Rural Affairs (DEFRA), Update of Noise Database for Prediction of Noise on Construction and Open Sites, 2005.
- 12. DataKustik, CadnaA (Computer Aided Noise Abatement), Version 2019.
- 13. Wyle Laboratories, Development of Ground Transportation Systems Noise Contours for the San Diego Region, December 1973.
- 14. Katz-Okitsu and Associates Traffic Engineers, Traffic Distribution Study, 1986.
- 15. U.S. Environmental Protection Agency Office of Noise Abatement and Control, Information on Levels of Environmental Noise Requisite to Protect Public Health and Welfare With an Adequate Margin of Safety, March 1974.
- 16. Federal Transit Administration (FTA), Transit Noise and Vibration Impact Assessment, May 2006.
- 17. California Department of Transportation (Caltrans), Transportation and Construction Vibration Guidance Manual, September 2013.

FIGURES





Assessor's Parcel Map Job # S190506.2



Satellite Aerial Photograph Job # S190506.2





Satellite Aerial Photograph Showing Current Traffic CNEL Contours and Noise Measurement Location Job # S190506.2



Satellite Aerial Photograph Showing Future Traffic CNEL Contours and Noise Measurement Location Job # S190506.2







Satellite Aerial Photograph Showing Mechanical Equipment Noise Source and Receiver Locations Job # S190506.2



Satellite Aerial Photograph Showing Construction Noise Source and Receiver Locations Job # S190506.2

APPENDIX A

Project Plans
												5						
AB	BREVIATIONS							PROJECT DESC	RIPTIÓN					A				
ABV AFF ACOUS	above above finis hed floor acoustical	EXH GR EXP EX	eshaust air grill espansion / exposed espansion joint	LIT LIW LIWC	light light weight light weight concrete	RAIG REV ROW	rebum air grāl revense right of way	This project is located on the east po neighborhood of San Diego, GA. The	rtion of Rancho Carmel Drive at the intense site is approximately 19,906 55.	tion of Provence	al Place in the Cannel Mountain Reach							
ACT ADI	acoustical celling tile adjacent	EXT	esterior	UR LUIM	Bving room Iuminous	RD RR	roof drain roof raiter	Currently on the site eals it a 2 level residential development, will be built affordable units. A relature of 1-bei	sark and ride parking structure that was but t over top of the existing parking structure. room and 2-bedroom units are distributed	t in 1991 that wi The 50 apartment provenceut the 1	ellinentials. The proposed project, a 50 unit ents willinglude 35 maniet rate and 35 building levels 1 through. The estation particle				2			
AGGR	aggregate air conditioning	FO	face of face of concrete	MB	machine bolt	RM RO	room rough opening	structure is located on the basement ground floor levelse II house the rest	and ground licor level. The addition of an dential lobby, leasing office, mail, delivery	levator wills en opport, child tra	vice the parting and residential levels. The responsation support, rideshare internation				dim-	-		·
AUM	aluminum	FOM	face of masonny face of stud	MR	manufactured	я.	saven kentber	trash, motorcycle an d bicycle storag level parking level will provide the ec bicycle storages. The first level reside	, two handicapped parking spaces, and the lating standard and compact parking space ntial level includes 13 units, a co-working space	existing standars elevator generation acc. with kitcher	nd and compact parting spaces. The lasten rator room, electricuitility room, motorcycli methe, and a common open executives	e and with				a	зP	a
AB APPROX	anchor bolt approximate	FAM CTF	I family center finish	MIL MIR	manufactured lumber manufacturer	SCHED	schedule screen	BBQ. The second thru fourth levels additional storage units and private it	contai n residential units with an additional al conies.	ommon space ro	confidences on level 3. All levels contain	270			UTA			
ARCH AD	architectural area drain	FF FIN GR	finished floor finish grade	MBL MAG	masonny	SOP	scupper sheathing	The project is located within the Par	ling Standard Transk Rioriky Area, which n	julines aero parki	ting spaces, however the editing puriling				the second se	2		
ASPH	as phait as phait tile	FEC	fine extinguisher fine extinguisher cabinet	MO MBA	master bath	SMT	sheet sheet metal	points, however this project is provide	car spaces, s motorcycle spaces, and an is ling 8 points.	ciespacies. The	e interportación intrenely resparentielle a a		D. S.		and the second se		7722 WW	100000
BA.	bath	FP	fixed	M DR MATL	master bedroom material	SMT	shelf and pole shower	The project qualifies for 3 incentives requirement which with the use of 3	All a oning requirements have been met e incentives, an the project will be able to be	upt for North s submitted admi	ide setback, Lot Courrage and Storage inistratively and not as a discretionary proj	jecz.	at a second			Cherring	Dailyn An	di hai shurra
BING	beening	FUT	flature flat wall paint	MICH	maaimum mechanical	SIM SH	single hung	The proposed housing project is prive	ately funded and is considered to be a privi	e housing proje	et.				15	1 100 000 000		
BR BLW	belroom below	FUR	floor floor dnán	MED	medicine cabinet medium	54D G	siking glass door									7 809-039	4710 F BOR-0	100-4-1008
BUOG	blocking	FMC	floor material change	MTR.	metal	SC SC	solid core						Card Line			<u> </u>		
BOT	board boltom	FURSK	floor sink fluorescent	MID	nicrowawe relidelle	SPEC	sound transmission class specification / specified	PROJECT INFO	/ BUILDING ANALY	SIS			19					
BLDG	building	FT	foot / Ret / Sire treated	MISC	niscellaneous	54 54	square foot / square leet	OTTE CLIMANA DV						The second				
CAR	cableat	FAU	forced air unit	MOV	movable	STD	standard	Site Area (Approx)	19,906 3F				and the second		P			
OPT CANTE	carpet	FRDR	frendi do or fuelese	NAT	natural	STOR	storage	Base Zone Planned Community	RM 4-10 CARMEL MOUNTAIN RANCH				CODE ANALYSIS	DIRECTORY	SHEET INDEX			
0	cast iron catch basin	FURR	furring	N NA	north not applicable	SAR SUSP	supply air register suspended / suspension	Overlay Jones	Transit Priority Area Residential Tandem Parking Overlay				JURISDICTION HAVING AUTHORITY		ACCES THE SAMET			
cue cu	celling celling joint	GALV	galianized garbage disposal	NC NTS	not in contract not to scale	SYMM	symmetrical		MC/G Miramar - Airport Influence Area MC/G Miramar - Airport Land Use Compat	alityOverlay			City of San Blegs, California	Creative Concernantities	AGLO EXETTING PERMITED TS & SITE PLAN AGLI EXETTING PERMITED TS & SITE PLAN			
CEM	cement center	GA. GT	gauge girder truss	ND	number	TEL	belephone tempered	Geological Hazard Category Ube	53 Existing: Rerk and Ride Radility Mu	s Family Reside	ential		GOVERNING CODES These doos meets and this project shall conform with the	San Bigo, CA. 92127				
G.	center line ceramic tile	GL	glass glas Iam beam	OFF OC	office on center	TEXT	teature thickness		Built in 1991. MIN/MAX	Proposed			Tolixering codes: 2016 Celifornie Code of Regulations Tible 36	858.415. 8701 Pas	CITY CRAWINGS			
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CMU COND	concrete masonry unit condition	HŞ HOW	hard sufface hardware	OH	over head	TOP TOW	tope of parapet top of wall	Structure Height Roor Area Ratio	3.60	2.39			2016 California Green Building Standards Code 2016 California Energy Code with	STRUCTURAL ENGINEER	A300 BIGEMENT FLOCE PLAN	L H	JEI	N
CONSTR	construction continuous	HOWD	handwood header	PT PG	paint paint grade	т	trash compactor tread	Gross Roor Area Lot Coverage	71,662 SF 60 % 11,944 SF	47,625F 63% *			2016 California Energy IPIG ency Randards. PLANNING ZONE Research Land Land Land Land Land Land Land Land	Inscholtbre Binactural Engineering Inc. ATTN: Share Lothcop	A 201 GROUND IL GOR FLAN A 201 FIRST IL COR FLAN	100	RN	Ň
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OVE	counter	HT HD	height hold down	PAR PART	parapet parti al	U/G U/S	under group under slab	Common Outdoor Open Space	25 56/0U 1,250 SF	4,853 SF			OCCUPANCY CLASSIFICATION Press Tables IIII II-2 Residential Apartments	Far: 994, 600,0006 Email: Harred Barenghistracion	A 205 FOURTH RUDOR PLAN A 206 KDOF RUNN	~	우립	8
0	deck jola t deep/dryver	HC	holiow core holiow metal	P BD PTN	particle board partition	UNO	unies s nobed otherwis e unin al	Refuse & Recyclable	192 (96/96) SF	203 SF			IF1 Eduting Porting Gerages TYPE OF CONSTRUCTION Intervention	CIVILENGINEER	A201 ELEVATIONS A202 ELEVATIONS	1	U Z	ш
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DH	double hung double hung	INT	Interior	PROP	property	WIC	walk in dos et	Pian 3 288/28A	817 SF 73 SF 4 U	its				ATTN: John Patterson 4000 Eccentric Video Bed, Sec. 300 Ban J				
DN	down	JAN	janitor John	QT	quany ble	W	washer washer	Plan 5 288/28A	902 SF 72 SF 16 L	ns nits		-	An automaticFlim spelokter system is required. Drawings prepared by synon's fire protection.	Sen Blego, CA 92121 Phone: 858,558,8977				
DWG	drawing	JST	joint	R	radius/riser	WP	waterproof	B	uilding Floor Area	115 3	Open Space	real and a second se	A one inch or proder water envice and meter will be required to ensure asseguate water denrands: are met in the event of a fire aprintize activation during periods of other was a making elemands are occurring, i.e.	Email john@gmplandarch.com				
EA. E	each east	KIP KUT	king post kitchen	RCP	reflected ceiling plan/ refinitionced concrete plane	WWF	weided wire fabric weided wire mesh	G ara ge Ba sement 9,748 SF	Common Residential Stor 664 SF 705	ge CF 10	GFA Private Com 2,412,5F**	mon	segular inspection or permit					
EN ELEC	edge nalling dectrical	LB	in bolt / pound	REF	ndrigerator / reference resistor	w	west where occurs	Ground 11,540 SF First	1,171 SF 733 2,048 SF 9,085 SF 1,88	CF 12	2,590 SF** 12,196 SF 92,2 SF 78	5 SF	A Property Owner's Real Report form for work required to have special					
EL ELEV	denation denator	LAM	laminated lands cape	REINF	reinforced / reinforcement required	WDW W/	window with	Second	1,603 SF 9,085 SF 1,88 1,603 SF 9,147 SF 1,88	105 1	11,809 SF 922 SF 38	£ SF	inspections, beating and situational observations must be completed by the property owner, property warrange against of record, acchiese of moved, acchiese of moved and updatable is and this explaints B					
ET EQ	end jack truss equal	LAU	laundry lavatory	RS RESL	ns.avn ns.Best	W/O WD	with out wood	Fourth Total 11 540 SE	1,603 SF 9,147 SF 1,88	105 1	11,8095 8515 (76225) 15465 156	441	Special Impections required:					
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GR	APHIC LEGEND							TRANSPORTATION A	MENITY REQUIREMENT		PARKING CALCULATION							
GENER	41	ELECT	RICAL			MECH	ANI CAL / PLUMBING	Regulared Provided Transit and Ride	2 poir share Information 1 poir	s sicro	tus sevens granularitent) room Dwelling Units	26						
1	revision mark		duples: wall receptade (J.107 typ)	®r	recis sed fluorescent: light flature	\ge	air duct (in cross-section)	Delivery Support Child Transport	tion Storage 1 poir	s 2 Bedr 8 Bicycle	e Spaces / 100 Dwelling Unit	0.6				DRAWN BY ST	W. DATE	05 28 39
	wa .	-	duples wall recepted e 1/2 switched	Ow	motion detected light flature	-0	thermostat	Co-Working Spi	ce 2 poir	E Total R	e Spaces/ 2011 Diversiting Unit Resputent Micycle Spaces (Reaktoretind)	22				8/39/18	PurvingFre-A gal ut	in
4	A building section mark	-040	duplex wallreceptacle, GPO waterproof duplex	-9	> well bracket light flature	844	ceiling return air grūle	FAR. DENSITY BOALD	S. & INCENTIVE CALCULATION	N N		-43	2°	12 17	2- 			
		=	weilreceptade,GPG \$000 outlet (110/1typ)		Op photo reactive	6∟∄	wall return air grille	Total Building Area	5, 61 THEE HTTV E CALCOLATI	F 2 Bede	room Deutling Units	26	VICINITY MAP	LEGAL DESCRIPTION	PRINTS			
	A elevation mark MOS sheet number reference	#	tourplex wall receptacle (110V typ)		1 undercabinet light fixture	Ŧ	type " 8" vent through roof (VTR)	Lot Size (Approx) Building FAR	19,905	IF Moton	rcycle Spaces / Unit Result al Mathematic Sector	<u>n1</u>						
	10 almatics and		220V (or 200V3-phase) wallreceptacle		fluorescent light fluture isonition how/see theme	$^{\odot}$	eshaust fan vented to exterior	Base Zone	RM 4-	Provid	led Matercyclin Specas		- Coltan	ASSESSORS PARCEL MUMBERS 3 13-080-18-00	DATE: DESCRIPTION:			
1	bi y aheet number reference	÷	duplex celling receptacle single-pole, double throw switch	U C	noted WP)	\oslash_{w}	write House eshaust ran, shoan SSQTXE w/smart sensor control or equal, 6" min duct	Residential Maed Use B onus Underground Parking Roman	200	VEHICI 1, Pede	LE SRACES (THA-RESIDENTIAL)	TAN145-BC		ASSESSORS PARCEL DESCRIPTION	OIL 25:10 Planning Department Pre-Application	-		_
	G R M-space name/number	-68-3	3-way switch	ĕ	floor light flature	0	humidiatat fan, Broan QTXELLOS	Alicentel e RAR Alicentel e RAR	3.60	2 Bedr	room Dwelling Uwits	34		THE LINKS INJERSED TO HERE BELOW & STUATED IN THE CITY OF SAN DEED, IN THE COUNTY OF SAN DEED, STATE OF CALIFORNIA, AND & DESCRIBEDAS KOLLOW'S		<u> </u>		
01	#floor Snish / ceiling height	-69-4	é-way pelitch dimmer	-8	chime.	-CH	6" min duct	Base Allowable Densky (100/SF	400 5	Provid	ded Spaces	60		LOT 18 OF RESUBLICION OF CAMMEL MICHINER, MICH				
	changes in elevation	-09-16	photoelectric switch	-0	arroke detector - direct wire to panel		receiped exhaust tan and light flatu re range hood with exhaust tan and	Attowable D'Us Pre-bonus	50 D Low (60 B Moderate 80% ANE) (370% A M	Requir	red ADA Sporter	0		UNETS 4 AND 30, IN THE CITY OF SAN DEED, COUNTY DESAN DEED, STATEOF CALFORNIA, ACCORDING TO MAP THEREOF ING. 12516, FALEDIN THE OFFICE OF THE COUNTY REPORTED				
	- reade at estation	-69-VS	vacancy sensor		carbon monoxide detector	~~~ 	light Sael gas, supply with shutoff solve	Low Income (U) DUs. Moderate Income BBI This	10 5	Provid	Sed ADA Speces as Part of Triad	0		OF SAIN DISCO COUNTY, DECEMBER 13, 1989.	-			
	optio nal line - noted in italia	۲	support 1000)	-	television outlet	-0	loose (lo glighter) key valve	Percentage of U & MI D Uz	20% 10%	Total R	Regulivat Velic in Spanne				REVISIONS			
	Nidden line	0	ceiling light fluture	-00 Γh	garage door opener	-++	hose bib	Censity Bonus & Incentives	Low (60 B Moderate 80% AME) (120% AME)	Total P	Provided Velicite Space	10					at he water to perform	d harden a withi
-	center line	Orc	surface mounted porcelain societ se/ pull-chain	U T	internally Ruminated address	-0 []	ice maker line w/ shutoff valve	Bensity Bonus Allowable Blux Post-bonus	35.00% 0.00% 67				SITE LIGELL Rendu Certan Dr.		DATE: DESCRIPTION:	property of Arthony and a restance of the second se	B ^o flags alater a flaidhinn all a gcogradhan in dalara R pa spacasta rép, an flaidh	Radia in m
-		Or	surface mounted Successent light Sature	_ L _	numbersligible from the street, low voltage type		gas meter	Incentives. Mioumble Number of Incentives	2 1				Bin Diego, Cal Krose			all storts sparts	nd ar dat Salad for an a pryskalar of Last Santal	ther page into
		R	recessed celling light fluture	¥	cellingthn	0	dryer venit through roof	nequested incentives 1. Setbacks on North Sid e								3	1000	
		۲	recessed wall-wather light future	\int	0	\triangle	shower head	2. Lot Coverage 3. Storage					a forman in the	1		1 8	-000	





A100









A104



A105







APPENDIX B

Applicable Noise Regulations

Noise Element





- NE-A.2. Assure the appropriateness of proposed developments relative to existing and future noise levels by consulting the guidelines for noise-compatible land use (shown on Table NE-3) to minimize the effects on noise-sensitive land uses.
- NE-A.3. Limit future residential and other noise-sensitive land uses in areas exposed to high levels of noise.
- NE-A.4. Require an acoustical study consistent with Acoustical Study Guidelines (Table NE-4) for proposed developments in areas where the existing or future noise level exceeds or would exceed the "compatible" noise level thresholds as indicated on the Land Use Noise Compatibility Guidelines (Table NE-3), so that noise mitigation measures can be included in the project design to meet the noise guidelines.
- NE-A.5. Prepare noise studies to address existing and future noise levels from noise sources that are specific to a community when updating community plans.

Land Use Category	Exterior Noise Exposu (dBA CNEL)					
	60 	65	5 7() 7	5	
Parks and Recreational						
Parks, Active and Passive Recreation						
Outdoor Spectator Sports, Golf Courses; Water Recreational Facilities; Indoor Recreation Facilities						
Agricultural						
Crop Raising & Farming; Community Gardens, Aquaculture, Dairies; Horticulture Nurseries & Greenhouses; Animal Raising, Maintain & Keeping; Commercial Stables						
Residential						
Single Dwelling Units; Mobile Homes		45				
Multiple Dwelling Units *For uses affected by aircraft noise, refer to Policies NE-D.2. & NE-D.3.		45	45*			
Institutional						
Hospitals; Nursing Facilities; Intermediate Care Facilities; Kindergarten through Grade 12Educational Facilities; Libraries; Museums; Child Care Facilities		45				
Other Educational Facilities including Vocational/Trade Schools and Colleges and Universities		45	45			
Cemeteries						
Retail Sales						
Building Supplies/Equipment; Food, Beverages & Groceries; Pets & Pet Supplies; Sundries, Pharmaceutical, & Convenience Sales; Wearing Apparel & Accessories			50	50		

TABLE NE-3 Land Use - Noise Compatibility Guidelines





Land Use	Category			Ex	Exterior Noise Ex (dBA CNEL			osure		
				6	0 6	5 7	0 7	5 I		
Commercial .	Services									
Building Serv Maintenance religious asse			50	50						
Visitor Accor	mmodations				45	45	45			
Offices										
Business & P Corporate He	Professional; Govern eadquarters	nment; Medical, I	Dental & Health Practitioner; Regional &			50	50			
Vehicle and V	Vehicular Equipmer	nt Sales and Servi	ices Use							
Commercial Sales & Rent	or Personal Vehicle als; Vehicle Equipr	Repair & Maintennent & Supplies	enance; Commercial or Personal Vehicle Sales & Rentals; Vehicle Parking							
Wholesale, D	istribution, Storage	e Use Category								
Equipment & Wholesale D	Materials Storage	Yards; Moving &	& Storage Facilities; Warehouse;							
Industrial										
Heavy Manu Terminals; M	facturing; Light Ma lining & Extractive	nufacturing; Mar Industries	ine Industry; Trucking & Transportation							
Research & I	Development						50			
	Compatible	Indoor Uses	Standard construction methods should a acceptable indoor noise level. Refer to S	ttenuate ection 1	exteri	or nois	e to an	l		
	Compatible	Outdoor Uses	Activities associated with the land use n	nay be c	arried	out.				
45 50	Conditionally	Indoor Uses	Building structure must attenuate exterior noise to the indoor noise level indicated by the number (45 or 50) for occupied areas. Refer to Section I.							
45, 50	Compatible	Outdoor Uses	Feasible noise mitigation techniques should be analyzed and incorporated make the outdoor activities acceptable. Refer to Section I.							
	Incompetible	Indoor Uses	New construction should not be underta	ken.						
	Incompatible	Outdoor Uses	Severe noise interference makes outdoor activities unacceptable.							



TABLE NE-4 Acoustical Study Guidelines

An acoustical study should include, but is not limited to the following analysis:

Provide noise level measurements to describe existing local conditions and the predominant noise sources.

Measure existing single event noise levels (SENEL, SEL, or Time Above) within airport influence areas.

Estimate existing and projected noise levels (CNEL) and compare them to levels on Table NE-3. For parks, may consider motor vehicle traffic noise measurements during the one-hour period where the worst-case traffic noise levels are expected to occur from dawn to dusk at a park.

Recommend appropriate mitigation measures to achieve acceptable noise levels on Table NE-3.

Estimate noise exposure levels with recommended mitigation measures.

Describe a post-project assessment to evaluate the effectiveness of the proposed mitigation measures.

B. Motor Vehicle Traffic Noise

Goal

 Minimal excessive motor vehicle traffic noise on residential and other noise-sensitive land uses.

Discussion

Motor vehicle traffic noise is a major contributor of noise within the City. Excessive noise levels along arterial roads, interstate freeways, and state highways affect much of the urban environment. Traffic noise level is dependent upon traffic volume, speed, flow, vehicle mix, pavement type and condition, the use of barriers, as well as distance to the receptor.

Local roadway design features and traffic management and calming techniques can minimize noise from traffic speed and frequent vehicle acceleration and deceleration, and innovative roadway paving material can further reduce traffic noise. Vehicles equipped with a properly functioning muffler system help to limit excessive exhaust noise. Future use of hybrid transit buses could help to reduce noise along mixed-use transit corridors.

At higher speeds, typically on freeways, highways and primary arterials, the noise from tire/pavement interaction can be greater than from vehicle exhaust and engine noise. The use of lower noise paving surfaces can reduce tire/pavement interaction noise. For noise-sensitive land uses adjacent to freeways and highways, these uses should be buffered from excessive noise levels by intervening, less sensitive, industrial-commercial uses or shielded by sound walls or landscaped berms. The City can, however, influence daily traffic volumes and reduce peak-hour



Article 9.5: Noise Abatement and Control

Division 4: Limits

("Noise Level Limits, Standards and Control" added 9–18–1973 by O–11122 N.S.) (Retitled to "Limits" on 9–22–1976 by O–11916 N.S.)

§59.5.0401 Sound Level Limits

(a) It shall be unlawful for any person to cause noise by any means to the extent that the one-hour average sound level exceeds the applicable limit given in the following table, at any location in the City of San Diego on or beyond the boundaries of the property on which the noise is produced. The noise subject to these limits is that part of the total noise at the specified location that is due solely to the action of said person.

Land Use	Time of Day	One-Hour Average Sound Level (decibels)
1. Single Family Resident	tial 7 a.m. to 7 p.m.	50
	7 p.m. to 10 p.m.	45
	10 p.m. to 7 a.m.	40
2. Multi-Family Resident	ial 7 a.m. to 7 p.m.	55
(Up to a maximum den	sity 7 p.m. to 10 p.m.	50
of 1/2000)	10 p.m. to 7 a.m.	45
3. All other Residential	7 a.m. to 7 p.m.	60
	7 p.m. to 10 p.m.	55
	10 p.m. to 7 a.m.	50
4. Commercial	7 a.m. to 7 p.m.	65
	7 p.m. to 10 p.m.	60
	10 p.m. to 7 a.m.	60
5. Industrial or Agricultur	any time	75

TABLE OF APPLICABLE LIMITS

(b) The sound level limit at a location on a boundary between two zoning districts is the arithmetic mean of the respective limits for the two districts.
 Permissible construction noise level limits shall be governed by Sections 59.5.0404 of this article.



- (c) Fixed-location public utility distribution or transmission facilities located on or adjacent to a property line shall be subject to the noise level limits of Part A. of this section, measured at or beyond six feet from the boundary of the easement upon which the equipment is located.
- (d) This section does not apply to firework displays authorized by permit from the Fire Department.
- (e) This section does not apply to noise generated by helicopters at heliports or helistops authorized by a conditional use permit, nor to any roller coaster operated on City–owned parkland.

(Amended 9–11–1989 by O–17337 N.S.) (Amended 11-28-2005 by O-19446 N.S.; effective 2-9-2006.)

§59.5.0402 Motor Vehicles

- (a) Off–Highway
 - (1) Except as otherwise provided for in this article, it shall be unlawful to operate any motor vehicle of any type on any site, other than on a public street or highway as defined in the California Vehicle Code, in any manner so as to cause noise in excess of those noise levels permitted for on- highway motor vehicles as specified in the table for "45 mile- per-hour or less speed limits" contained in Section 23130 of the California Vehicle Code, and as corrected for distances set forth in subsection A.2. below.
 - (2) Corrections

The maximum noise level as the off-highway vehicle passes may be measured at a distance of other than fifty (50) feet from the center line of travel, provided the measurement is further adjusted by adding algebraically the applicable correction as follows:



Distance (Feet)	Correction (decibels)
25	-6
28	-5
32	-4
35	-3
40	-2
45	-1
50 (preferred distance)	0
56	+1
63	+2
70	+3
80	+4
90	+5
100	+6

- (3) A measured noise level thus corrected shall be deemed in violation of this section if it exceeds the applicable noise–level limit as specified above.
- (b) Nothing in this section shall apply to authorized emergency vehicles when being used in emergency situations, including the blowing of sirens and/or horns.

("Motor Vehicles" renumbered from Sec. 59.5.0403 on 9–22–1976 by O–11916 N.S.)

§59.5.0403 Watercraft

Violations for excessive noise of watercraft operating in waters under the jurisdiction of The City of San Diego shall be prosecuted under applicable provisions of the California Harbors and Navigation Code. Permits issued by The City of San Diego for the operation of watercraft not in compliance with noise criteria of the Harbors and Navigation Code shall be reviewed and approved by the Administrator prior to issuance.

("Watercraft" renumbered from Sec. 59.5.0407 and amended 9–22–1976 by O-11916 N.S.)



§59.5.0404 Construction Noise

- (a) It shall be unlawful for any person, between the hours of 7:00 p.m. of any day and 7:00 a.m. of the following day, or on legal holidays as specified in Section 21.04 of the San Diego Municipal Code, with exception of Columbus Day and Washington's Birthday, or on Sundays, to erect, construct, demolish, excavate for, alter or repair any building or structure in such a manner as to create disturbing, excessive or offensive noise unless a permit has been applied for and granted beforehand by the Noise Abatement and Control Administrator. In granting such permit, the Administrator shall consider whether the construction noise in the vicinity of the proposed work site would be less objectionable at night than during the daytime because of different population densities or different neighboring activities; whether obstruction and interference with traffic particularly on streets of major importance, would be less objectionable at night than during the daytime; whether the type of work to be performed emits noises at such a low level as to not cause significant disturbances in the vicinity of the work site; the character and nature of the neighborhood of the proposed work site; whether great economic hardship would occur if the work were spread over a longer time; whether proposed night work is in the general public interest; and he shall prescribe such conditions, working times, types of construction equipment to be used, and permissible noise levels as he deems to be required in the public interest.
- (b) Except as provided in subsection C. hereof, it shall be unlawful for any person, including The City of San Diego, to conduct any construction activity so as to cause, at or beyond the property lines of any property zoned residential, an average sound level greater than 75 decibels during the 12–hour period from 7:00 a.m. to 7:00 p.m.
- (c) The provisions of subsection B. of this section shall not apply to construction equipment used in connection with emergency work, provided the Administrator is notified within 48 hours after commencement of work.
 (Amended 1–3–1984 by O–16100 N.S.)

§59.5.0406 Refuse Vehicles and Parking Lot Sweepers

No person shall operate or permit to be operated a refuse compacting, processing, or collection vehicle between the hours of 7:00 p.m. to 6:00 a.m. or a parking lot sweeper between the hours of 7:00 p.m. to 7:00 a.m. in any residential area unless a permit has been applied for and granted by the Administrator. *("Refuse Vehicles" added 9–18–1973 by O–11122 N.S.; amended 9–22–1976 by*

O–11916 N.S.)

(Amended 6-9-2010 by O-19960 N.S.; effective 7-9-2010.)



4. Is the site currently being mined?

If an economically feasible mineral extraction operation is the site's current use, and the site is not exhausted, a different use of the site would likely result in a significant impact on the availability of a locally important mineral recovery site.

K. NOISE

Noise is defined as unwanted or objectionable sound. Noise levels compatible with a person's life, health and enjoyment of property are regulated by Local, State, and Federal regulations, including the City of San Diego Progress Guide and General Plan, City Noise Abatement and Control Ordinance, California Noise Insulation Standards (Title 24), the State Public Utilities Code regulating airports, and other regulations. A direct and/or indirect noise impact should be evaluated in relation to applicable City standards, particularly, the City of San Diego Progress Guide and General Plan (Transportation Element). The following significance thresholds are in accordance with the City's Progress Guide and General Plan (Transportation Element) Land Use Compatibility with Annual Community Noise Equivalent Levels (CNEL).

Measurement of sound involves three variables, (1) magnitude; (2) frequency; and (3) duration. Noise levels in the City of San Diego are expressed and compared as dB (A) CNEL.

Definitions

The following definitions shall have the same meaning as defined in the Section 59.5.0102 of the City of San Diego Municipal Code:

A-Weighting

As in decibel A-weighting (dB [A]). Represents the frequency characteristics of the average human ear for various sound intensities. An A-Weight sound filters out lower frequencies, and provides a good indicator of the annoyance potential of a noise.

Average Sound Level

A sound level typical of the sound levels at a certain place during a given period of time, averaged by the general rule of combination for sound levels, said general rule being set forth in American National Standard Specifications for Sound Level Meters 1.4-1971. Average sound level is also called equivalent continuous sound level. (Leq)

Community Noise Equivalent Level (CNEL)

An average sound level during a 24-hour day, obtained after addition of five (5) decibels to sound levels in the evening from 7:00 p.m. to 10:00 p.m., and after addition of ten (10) decibels to sound levels in the night before 7:00 a.m. and after 10:00 p.m.

CNEL recognizes that noise annoyance is related to duration, how often the noise is present, how long it persists, and when it occurs.

Decibel (dB)

A unit measure of sound (noise) level.

Just as feet is used to measure distances, decibels are used to measure sound (noise) levels. The decibel is defined as 10 times the common logarithm of the ratio of two amounts of sound power.

The human ear can hear sounds from less than 10 dB to over 100 dB (sounds which are 100,000 times greater that the faintest sounds). Table K-1 shows the approximate relationship between sound level changes and peoples judgment of the relative loudness of the change.

Sound Level Change	Acoustic Energy Change	Relative Loudness
0 dB	0	Reference Point
3 dB	50 %	Perceptible Change
10 dB	90 %	Twice as Loud
20 dB	99 %	Four Times as Loud
30 dB	99.9 %	Eight Times as Loud
40 dB	99.99 %	Sixteen Times as Loud

Table K-1 RELATIVE LOUDNESS

Source: Miller 1989 pg. 1-6

Noise Level

The same as sound level. The terms may be used interchangeably.

Sound Level

In decibels, that quantity measured with a sound level meter as defined herein, by use of the "A" frequency weighting and "fast" time averaging unless some other time averaging is specified.

Sound Level Meter

An instrument for the measurement of sound, including a microphone, an amplifier, an attenuator, networks at least for standardized frequency weighting A, and an indicating instrument having at least the standardized dynamic characteristic "fast," as specified in American National Standard Specification for Sound Level Meters S1. 4-1971 or its successor.

INITIAL STUDY CHECKLIST QUESTIONS

The following questions are from the City's Initial Study Checklist and are used to provide guidance to determine potential significant impacts related to Noise:

Would the project:

- 1. Result or create a significant increase in the existing ambient noise levels?
- 2. Exposure of people to noise levels which exceed the City's adopted noise ordinance or are incompatible with Table K-4?

- 3. Exposure of people to current or future transportation noise levels which exceed standards established in the Transportation Element of the General Plan or an adopted airport Comprehensive Land Use Plan?
- 4. Result in land uses which are not compatible with aircraft noise levels as defined by an adopted airport Comprehensive Land Use Plan (CLUP)?

SIGNIFICANCE THRESHOLDS

1. Interior and Exterior Noise Impacts from Traffic Generated Noise (Table K-2 below provides the general thresholds of significance for uses affected by traffic noise.)

Structure or Proposed Use that would be impacted by Traffic Noise	Interior Space	Exterior Useable Space ²²	General Indication of Potential Significance		
Single-family detached	45 dB	65 Db			
Multi-family, schools, libraries, hospitals, day care, hotels, motels, parks, convalescent homes.	- Development Services Dcpartment (DSD) ensures 45 dB pursuant to Title 24	65 dB	Structure or outdoor useable area ²³ is < 50 feet from the center of the closest (outside) lane on a street with existing or future ADTs > 7500^{24}		
Offices, Churches, Business, Professional Uses	n/a	70 dB	Structure or outdoor usable area is < 50 feet from the center of the closest lane on a street with existing or future ADTs > 20,000		
Commercial, Retail, Industrial, Outdoor Spectator Sports Uses	n/a	75 dB	Structure or outdoor usable area is < 50 feet from the center of the closest lane on a street with existing or future ADTs > 40,000		

Table K-2 TRAFFIC NOISE SIGNIFICANCE THRESHOLDS (db(A) CNEL)

Source: 1) City of San Diego Acoustical Report Guidelines (December 2003) and 2) City of San Diego Progress Guide and General Plan (Transportation Element)

²² If a project is currently at or exceeds the significance thresholds for traffic noise described above and noise levels would result in less than a 3 dB increase, then the impact is not considered significant.

²³ Exterior usable areas do not include residential front yards or balconies, unless the areas such as balconies are part of the required usable open space calculation for multi-family units.

²⁴ Traffic counts are available from:

- San Diego Regional Association of Governments (SANDAG) Regional Economic Development Information
- System (REDI): http://cart.sandag.cog.ca.us/REDI/
- SANDAG Traffic Forecast Information Center: http://pele.sandag.org/trfic.html

2. HUD-Funded projects and Noise

If a project is receiving U.S. Department of Housing and Urban Development (HUD) funding, noise analysis and mitigation must be in accordance with the HUD Noise Guidebook²⁵ Minimum attenuation requirements are prescribed in Title 24 of the Code of Federal Regulations²⁶ (24 CFR 51.104(a)) which are the HUD Environmental Criteria and Standards.

3. Airport Noise Impacts

If the project is proposed within the Airport Environs Overlay Zone (AEOZ) as defined in Chapter 13, Article 2, Division 3 of the San Diego Municipal Code, the potential exterior noise impacts from aircraft noise would not constitute a significant environmental impact.

However, interior noise impacts will be regulated by the requirement for residential development within the AEOZ to reduce interior noise levels attributable to airport noise to 45 dB Community Noise Equivalent Level (CNEL). Interior noise levels for new construction of multi-family units are addressed by the Building Development Review Division (BDR) of the City's Development Services Department (DSD) and do not need to be mitigated through conditions in the environment report, but the BDR requirements should be noted. BDR requires additional insulation and upgraded building materials so that interior noise levels do \not exceed 45 dB(A) CNEL. The requirements for an acoustical testing are defined in the City of San Diego Municipal Code, Chapter 13, Article 2, Division 3, §132.0308, "Acoustical Testing of Interior Noise Levels."

Requirements for noise studies are found in the Municipal Code at Chapter 13, Article 2, Division 3, §132.0308. This section of the municipal code applies to "development" as defined at, § 113.0103 to include "constructing, reconstructing, converting, establishing, altering, maintaining, relocating, demolishing, using, or enlarging any building, structure, improvement, lot, or premises."

Remodels and additions to single-family and multi-family residences subject to airport noise levels above 65 dB (A) CNEL ordinarily would not be considered a significant issue and a noise study would not be required for the purposes of CEQA analysis. However, new construction of hospitals, schools, day care centers, or other sensitive uses subject to airport noise levels in excess of 65 dB(A) CNEL would be considered a significant issue and a noise study would be required that could recommend measures to mitigate potential noise impacts to a level below significance. Table K-3 below addresses the general impacts from airport noise thresholds.

²⁵ http://www.hud.gov/offices/cpd/energyenviron/environment/resources/guidebooks/noise/index.cfm

²⁶ http://www.access.gpo.gov/nara/cfr/cfr-table-search.html#page1

	Tabl	e K-3	
IMPACTS	FROM	AIRPORT	NOISE

Structure or Proposed Use that would be impacted by Airport Noise	Regulation
Structure within an AEOZ	Exterior noise is one factor in determining land use compatibility. See Table K-4 and the applicable Comprehensive Land Use Plan (CLUP).
New Single Family and Multi-family	Building Development Review Division (BDR) of Development Services Department (DSD) ensures 45 dB interior noise levels. Discuss Airport noise impact & BDR requirements (insulation and upgraded building materials to ensure 45 dB(A) CNEL) in environmental document See also § 132.0309 Requirement for Avigation Easement
Remodels and additions to existing single and multi-family	Noise study & mitigation not required for airport noise > 65 dB(A) CNEL. See also § 132.0309 Requirement for Avigation Easement. For development within the 60 dB CNEL contour of Lindbergh Field the applicant must demonstrate that indoor noise levels that are attributable to airport operations shall not exceed 45 dB. Refer to § 132.0306 of the Municipal Code.
New construction of hospitals, schools, day care centers or other sensitive uses	Noise study and mitigation required for airport noise > 65 dB(A) CNEL. See also § 132.0309 Requirement for Avigation Easement.

4. Noise from Adjacent Stationary Uses (Noise Generators)

A project which would generate noise levels at the property line which exceed the City's Noise Ordinance Standards is considered potentially significant (such as potentially a carwash or projects operating generators or noisy equipment).

If a non-residential use, such as a commercial, industrial or school use, is proposed to abut an existing residential use, the decibel level at the property line should be the arithmetic mean of the decibel levels allowed for each use as set forth in Section 59.5.0401 of the Municipal Code. Although the noise level above could be consistent with the City's Noise Ordinance Standards, a noise level above 65 dB (A) CNEL at the residential property line could be considered a significant environmental impact.

1. Impacts to Sensitive Wildlife

Noise mitigation may be required for significant noise impacts to certain avian species during their breeding season, depending upon the location of the project such as in or adjacent to an MHPA, whether or not the project is occupied by the California gnatcatcher, least Bell's vireo, southern willow flycatcher, least tern, cactus wren, tricolored blackbird or western snowy plover, and whether or not noise levels from the project, including construction during the breeding season of these species would exceed 60dB(A) or existing ambient noise level if above 60dB(A). In addition, please note that significant noise impacts to the California gnatcatcher are only analyzed if the project is within an MHPA; there are no restrictions for the gnatcatcher outside the MHPA any time of year. Please see Biological Resources Section, Step 2, Note (f).

6. Temporary Construction Noise

Temporary construction noise which exceeds 75 dB (A) L_{eq} at a sensitive receptor would be considered significant. Construction noise levels measured at or beyond the property lines of any property zoned residential shall not exceed an average sound level greater than 75decibles (dB) during the 12-hour period from 7:00 a.m. to 7:00 p.m. In addition, construction activity is prohibited between the hours of 7:00 p.m. of any day and 7:00 a.m. of the following day, or on legal holidays as specified in Section 21.04 of the San Diego Municipal Code, with exception of Columbus Day and Washington's Birthday, or on Sundays, that would create disturbing, excessive, or offensive noise unless a permit has been applied for and granted beforehand by the Noise Abatement and Control Administrator, in conformance with San Diego Municipal Code Section 59.5.0404.

Additionally, where temporary construction noise would substantially interfere with normal business communication, or affect sensitive receptors, such as day care facilities, a significant noise impact may be identified.

7. Noise/Land Use Compatibility

Noise is one factor to be considered in determining whether a land use is compatible. Land use compatibility noise factors are presented in Table K-4. Compatible land uses are shaded. Incompatible land uses are unshaded. The transition zone between compatible and incompatible should be evaluated by the environmental planner to determine whether the use would be acceptable based on all available information and the extent to which the noise from the proposed project would affect the surrounding uses.

	Table K-4 City of San Diego Noise Land Use Compatibility Chart										
		Annual Community Noise Equivalent Level in Decibels									
	Land Use	50	55	60	65	70	75				
1	Outdoor amphitheaters										
2	2 Schools, libraries										
3	Nature preserves, wildlife preserves										
4	Residential single-family, multi-family, mobile homes, transient housing										
5	Retirement homes, intermediate care facilities, convalescent homes										
6	Hospitals										
7	Parks, playgrounds										
8	3 Office buildings, business and professional										
9	Auditoriums, concert halls, indoor arenas, churches										
10	Riding stables, water recreation facilities										
11	outdoor spectator sports, golf courses										
12	livestock farming, animal breeding										
13	Commercial-retail, shopping centers, restaurants, movie theaters										
14	Commercial-wholesale, industrial manufacturing, utilities										
15	Agriculture (except livestock), extractive industry, farming										
16	Cemeteries										

APPENDIX C

Cadna Analysis Data and Results

Eilar Associates, Inc.

210 South Juniper Street, Suite 100 Escondido, California 92025-4230 Phone: (760) 738-5570

Date: 07 Jun 2019

Calculation Configuration

Configuration	
Parameter	Value
General	
Country	(user defined)
Max. Error (dB)	0.00
Max. Search Radius (#(Unit,LEN))	2000.00
Min. Dist Src to Rcvr	0.00
Partition	
Raster Factor	0.50
Max. Length of Section (#(Unit,LEN))	1000.00
Min. Length of Section (#(Unit,LEN))	1.00
Min. Length of Section (%)	0.00
Proj. Line Sources	On
Proj. Area Sources	On
Ref. Time	
Reference Time Day (min)	960.00
Reference Time Night (min)	480.00
Daytime Penalty (dB)	0.00
Recr. Time Penalty (dB)	6.00
Night-time Penalty (dB)	10.00
DTM	
Standard Height (m)	0.00
Model of Terrain	Triangulation
Reflection	
max. Order of Reflection	0
Search Radius Src	100.00
Search Radius Rcvr	100.00
Max. Distance Source - Rcvr	1000.00 1000.00
Min. Distance Rvcr - Reflector	1.00 1.00
Min. Distance Source - Reflector	0.10
Industrial (ISO 9613)	
Lateral Diffraction	some Obj
Obst. within Area Src do not shield	On
Screening	Excl. Ground Att. over Barrier
	Dz with limit (20/25)
Barrier Coefficients C1,2,3	3.0 20.0 0.0
Temperature (#(Unit,TEMP))	10
rel. Humidity (%)	70
Ground Absorption G	0.50
Wind Speed for Dir. (#(Unit,SPEED))	3.0
Roads (TNM)	
Railways (Schall 03 (1990))	
Strictly acc. to Schall 03 / Schall-Transrapid	
Aircraft (???)	
Strictly acc. to AzB	

Receivers

	Name	M.	ID	Lev	el Lr	Limit.	Value	Land Use			Height	Coordinates		
				Day	Night	Day	Day Night		Type Auto Noise Type			Х	Y	Z
				(dBA)	(dBA)	(dBA)	(dBA)				(m)	(m)	(m)	(m)
I	Cal			69.7	-65.9	0.0	0.0		х	Total	1.52 r	543.88	337.71	173.52

Roads

Name	M.	ID		Lme		Cou	nt Data	exact Count Data						Speed	Speed Limit SCS		Surface		Gradient	Mul	t. Reflee	ction
			Day	Evening	Night	DTV	Str.class.		М			p (%)		Auto	Truck	Dist.	Dstro	Туре		Drefl	Hbuild	Dist.
			(dBA)	(dBA)	(dBA)			Day	Evening	Night	Day	Evening	Night	(km/h)	(km/h)		(dB)		(%)	(dB)	(m)	(m)
Rancho Carmel Dr		RO_1	65.8	0.0	0.0			1136.0	0.0	0.0	1.0	0.0	0.0	72		15.24	0.0	1	0.0	0.0		
I-15 NB		RO_3	80.1	0.0	0.0			10234.0	0.0	0.0	7.1	0.0	0.0	105		33.53	0.0	1	0.0	0.0		
I-15 SB		RO_4	80.1	0.0	0.0			10234.0	0.0	0.0	7.1	0.0	0.0	105		33.53	0.0	1	0.0	0.0		
Ted Williams		RO_2	73.1	0.0	0.0			3749.0	0.0	0.0	5.0	0.0	0.0	89		24.38	0.0	1	0.0	0.0		

Geometry - Roads

Name	He	eight		Coordinates							
	Begin	End	x	у	Z	Ground	(m)	(%)			
	(m)	(m)	(m)	(m)	(m)	(m)					
Rancho Carmel Dr			497.74	135.08	175.00	175.00					
			501.94	213.20	175.00	175.00					
			505.30	257.30	173.00	173.00					
			526.11	329.14	172.00	172.00					
			598.26	519.95	174.00	172.00					
I-15 NB			-242.64	-478.34	159.00	159.00					
			185.32	347.46	177.00	177.00					
			445.68	859.53	186.00	186.00					
I-15 SB			411.71	892.06	186.00	186.00					
			146.48	366.07	177.00	177.00					
			-281.96	-465.76	159.00	159.00					
Ted Williams			996.59	337.98	201.00	201.00					
			880.67	245.58	197.00	197.00					
			713.51	145.61	188.00	188.00					
			595.06	111.17	186.00	180.00					
			500.98	112.85	180.00	180.00					
			401.02	112.85	180.00	180.00					
			236.38	108.65	176.00	176.00					
			83.49	96.05	176.00	176.00					

Terrain Contours

Name	M.	ID	OnlyPts	Hei	ght	C	oordinates	
				Begin	End	x	у	Z
				(m)	(m)	(m)	(m)	(m)
North Course		C1				563.50	372.00	173.00
						574.17	404.35	171.00
						780.62	480.39	186.00
						809.63	466.72	189.00
						813.30	433.03	188.00
						790.95	411.69	187.00
						683.23	374.00	177.00
						637.54	357.99	175.00
						615.53	355.99	174.00
						563.84	372.00	171.00
172		C2		172.00		556.00	365.82	172.00
						547.38	345.86	172.00
						545.49	336.20	172.00
						553.90	329.89	172.00
						564.44	327.46	172.00
						577.64	326.32	172.00
						598.23	328.84	172.00
						624.91	336.41	172.00
						626.27	339.42	172.00
						626.02	348.78	172.00
						625.54	351.95	172.00
						605.37	347.96	172.00
						583.31	351.95	172.00
						555.79	367.08	172.00
North Res		C3				426.09	539.36	169.00
						482.39	475.49	170.00
						540.38	425.07	171.00
						573.16	417.92	171.00
						630.30	430.53	174.00
						788.30	492.30	189.00
						862.67	528.85	200.00
						599.42	522.13	172.00
						445.42	523.81	170.00
Southeast		C4				538.65	306.85	173.00
						520.65	171.32	175.00
						633.94	170.79	183.00
						726.06	190.90	187.00
						776.36	226.90	187.00
						864.77	269.79	194.00
						855.24	441.32	196.00
						767.89	377.26	183.00
						723.41	366.14	182.00
						678.94	337.55	182.00
						620.71	329.61	178.00

Name	Μ.	ID	OnlyPts	Height Coordinates						
				Begin	End	х	у	Z		
				(m)	(m)	(m)	(m)	(m)		
						590.53	301.02	175.00		
						536.53	307.38	173.00		
West		C5				466.40	173.26	173.00		
						326.99	154.58	176.00		
						133.56	129.90	176.00		
						196.26	293.99	172.00		
						302.31	520.11	175.00		
						399.03	492.76	166.00		
						534.43	410.05	168.00		
						502.42	312.67	172.00		
						483.74	262.64	171.00		
						468.40	179.93	173.00		
I-15 E		C6				-217.71	-485.05	159.00		
						206.52	336.72	177.00		
						471.22	855.55	186.00		
I-15 W		C7				-306.65	-442.69	159.00		
						117.57	379.08	177.00		
						382.28	897.90	186.00		
TW N		C8				985.66	349.66	201.00		
						873.96	261.25	197.00		
						709.84	160.13	188.00		
						593.90	127.83	180.00		
TW S		C9				1005.78	320.54	201.00		
						894.07	232.13	197.00		
						729.96	131.01	188.00		
						614.01	98.72	180.00		

Eilar Associates, Inc.

210 South Juniper Street, Suite 100 Escondido, California 92025-4230 Phone: (760) 738-5570

Date: 07 Jun 2019

Calculation Configuration

Configuration	
Parameter	Value
General	
Country	(user defined)
Max. Error (dB)	0.00
Max. Search Radius (#(Unit,LEN))	2000.00
Min. Dist Src to Rcvr	0.00
Partition	
Raster Factor	0.50
Max. Length of Section (#(Unit,LEN))	1000.00
Min. Length of Section (#(Unit,LEN))	1.00
Min. Length of Section (%)	0.00
Proj. Line Sources	On
Proj. Area Sources	On
Ref. Time	
Reference Time Day (min)	960.00
Reference Time Night (min)	480.00
Daytime Penalty (dB)	0.00
Recr. Time Penalty (dB)	6.00
Night-time Penalty (dB)	10.00
DTM	
Standard Height (m)	0.00
Model of Terrain	Triangulation
Reflection	
max. Order of Reflection	0
Search Radius Src	100.00
Search Radius Rcvr	100.00
Max. Distance Source - Rcvr	1000.00 1000.00
Min. Distance Rvcr - Reflector	1.00 1.00
Min. Distance Source - Reflector	0.10
Industrial (ISO 9613)	
Lateral Diffraction	some Obj
Obst. within Area Src do not shield	On
Screening	Excl. Ground Att. over Barrier
	Dz with limit (20/25)
Barrier Coefficients C1,2,3	3.0 20.0 0.0
Temperature (#(Unit,TEMP))	10
rel. Humidity (%)	70
Ground Absorption G	0.50
Wind Speed for Dir. (#(Unit,SPEED))	3.0
Roads (TNM)	
Railways (Schall 03 (1990))	
Strictly acc. to Schall 03 / Schall-Transrapid	
Aircraft (???)	
Strictly acc. to AzB	

Roads

Name	M.	ID		Lme		Cou	nt Data	exact Coun				a		Speed Limit		SCS	Surface		Gradient	Gradient Mult.		ction
			Day	Evening	Night	DTV	Str.class.		М			p (%)		Auto	Truck	Dist.	Dstro	Туре		Drefl	Hbuild	Dist.
			(dBA)	(dBA)	(dBA)			Day	Evening	Night	Day	Evening	Night	(km/h)	(km/h)		(dB)		(%)	(dB)	(m)	(m)
Rancho Carmel Dr		RO_1	67.0	0.0	0.0			1334.0	0.0	0.0	2.0	0.0	0.0	72		15.24	0.0	1	0.0	0.0		
Ted Williams		RO_2	73.4	0.0	0.0			4010.0	0.0	0.0	5.0	0.0	0.0	89		24.38	0.0	1	0.0	0.0		
I-15 NB		RO_3	80.4	0.0	0.0			10948.0	0.0	0.0	7.1	0.0	0.0	105		33.53	0.0	1	0.0	0.0		
I-15 SB		RO_4	80.4	0.0	0.0			10948.0	0.0	0.0	7.1	0.0	0.0	105		33.53	0.0	1	0.0	0.0		

Geometry - Roads

Name	He	eight		Coordinates							
	Begin	End	x	у	Z	Ground	(m)	(%)			
	(m)	(m)	(m)	(m)	(m)	(m)					
Rancho Carmel Dr			497.74	135.08	175.00	175.00					
			501.94	213.20	175.00	175.00					
			505.30	257.30	173.00	173.00					
			526.11	329.14	172.00	172.00					
			598.26	519.95	174.00	172.00					
Ted Williams			996.59	337.98	201.00	201.00					
			880.67	245.58	197.00	197.00					
			713.51	145.61	188.00	188.00					
			595.06	111.17	186.00	180.00					
			500.98	112.85	180.00	180.00					
			401.02	112.85	180.00	180.00					
			236.38	108.65	176.00	176.00					
			83.49	96.05	176.00	176.00					
I-15 NB			-242.64	-478.34	159.00	159.00					
			185.32	347.46	177.00	177.00					
			445.68	859.53	186.00	186.00					
I-15 SB			411.71	892.06	186.00	186.00					
			146.48	366.07	177.00	177.00					
			-281.96	-465.76	159.00	159.00					

Terrain Contours

Name	M.	ID	OnlyPts	Hei	ght	C	oordinates	
				Begin	End	x	у	Z
				(m)	(m)	(m)	(m)	(m)
North Course		C1				563.50	372.00	173.00
						574.17	404.35	171.00
						780.62	480.39	186.00
						809.63	466.72	189.00
						813.30	433.03	188.00
						790.95	411.69	187.00
						683.23	374.00	177.00
						637.54	357.99	175.00
						615.53	355.99	174.00
						563.84	372.00	171.00
172		C2		172.00		556.00	365.82	172.00
						547.38	345.86	172.00
						545.49	336.20	172.00
						553.90	329.89	172.00
						564.44	327.46	172.00
						577.64	326.32	172.00
						598.23	328.84	172.00
						624.91	336.41	172.00
						626.27	339.42	172.00
						626.02	348.78	172.00
						625.54	351.95	172.00
						605.37	347.96	172.00
						583.31	351.95	172.00
						555.79	367.08	172.00
North Res		C3				426.09	539.36	169.00
						482.39	475.49	170.00
						540.38	425.07	171.00
						573.16	417.92	171.00
						630.30	430.53	174.00
						788.30	492.30	189.00
						862.67	528.85	200.00
						599.42	522.13	172.00
						445.42	523.81	170.00
Southeast		C4				538.65	306.85	173.00
						520.65	171.32	175.00
						633.94	170.79	183.00
						726.06	190.90	187.00
						776.36	226.90	187.00
						864.77	269.79	194.00
						855.24	441.32	196.00
						767.89	377.26	183.00
						723.41	366.14	182.00
						678.94	337.55	182.00
						620.71	329.61	178.00
Name	Μ.	ID	OnlyPts	Height		C	oordinates	
--------	----	----	---------	--------	-----	---------	------------	--------
				Begin	End	x	у	Z
				(m)	(m)	(m)	(m)	(m)
						590.53	301.02	175.00
						536.53	307.38	173.00
West		C5				466.40	173.26	173.00
						326.99	154.58	176.00
						133.56	129.90	176.00
						196.26	293.99	172.00
						302.31	520.11	175.00
						399.03	492.76	166.00
						534.43	410.05	168.00
						502.42	312.67	172.00
						483.74	262.64	171.00
						468.40	179.93	173.00
I-15 E		C6				-217.71	-485.05	159.00
						206.52	336.72	177.00
						471.22	855.55	186.00
I-15 W		C7				-306.65	-442.69	159.00
						117.57	379.08	177.00
						382.28	897.90	186.00
TW N		C8				985.66	349.66	201.00
						873.96	261.25	197.00
						709.84	160.13	188.00
						593.90	127.83	180.00
TW S		C9				1005.78	320.54	201.00
						894.07	232.13	197.00
						729.96	131.01	188.00
						614.01	98.72	180.00

210 South Juniper Street, Suite 100 Escondido, California 92025-4230 Phone: (760) 738-5570

Date: 18 Sep 2019

Configuration	
Parameter	Value
General	
Country	(user defined)
Max. Error (dB)	0.00
Max. Search Radius (#(Unit,LEN))	2000.00
Min. Dist Src to Rcvr	0.00
Partition	
Raster Factor	0.50
Max. Length of Section (#(Unit,LEN))	1000.00
Min. Length of Section (#(Unit,LEN))	1.00
Min. Length of Section (%)	0.00
Proj. Line Sources	On
Proj. Area Sources	On
Ref. Time	
Reference Time Day (min)	960.00
Reference Time Night (min)	480.00
Daytime Penalty (dB)	0.00
Recr. Time Penalty (dB)	6.00
Night-time Penalty (dB)	10.00
DTM	
Standard Height (m)	0.00
Model of Terrain	Triangulation
Reflection	
max. Order of Reflection	0
Search Radius Src	100.00
Search Radius Rcvr	100.00
Max. Distance Source - Rcvr	1000.00 1000.00
Min. Distance Rvcr - Reflector	1.00 1.00
Min. Distance Source - Reflector	0.10
Industrial (ISO 9613)	
Lateral Diffraction	some Obj
Obst. within Area Src do not shield	On
Screening	Excl. Ground Att. over Barrier
	Dz with limit (20/25)
Barrier Coefficients C1,2,3	3.0 20.0 0.0
Temperature (#(Unit,TEMP))	10
rel. Humidity (%)	70
Ground Absorption G	0.50
Wind Speed for Dir. (#(Unit,SPEED))	3.0
Roads (TNM)	
Railways (Schall 03 (1990))	
Strictly acc. to Schall 03 / Schall-Transrapid	
Aircraft (???)	
Strictly acc. to AzB	

Roads

Name	M.	ID		Lme		Cou	nt Data	a exact Cou			Int Data Speed			Speed	d Limit	SCS	Surf	face	Gradient	Mul	t. Reflec	ction
			Day	Evening	Night	DTV	Str.class.		М			p (%)		Auto	Truck	Dist.	Dstro	Туре		Drefl	Hbuild	Dist.
			(dBA)	(dBA)	(dBA)			Day	Evening	Night	Day	Evening	Night	(km/h)	(km/h)		(dB)		(%)	(dB)	(m)	(m)
Rancho Carmel Dr		RO_1	68.8	0.0	0.0			2033.0	0.0	0.0	2.0	0.0	0.0	72		15.24	0.0	1	0.0	0.0		
Rancho Carmel Dr		RO_1	69.0	0.0	0.0			2125.0	0.0	0.0	2.0	0.0	0.0	72		15.24	0.0	1	0.0	0.0		
Ted Williams		RO_2	75.3	0.0	0.0			6238.0	0.0	0.0	5.0	0.0	0.0	89		24.38	0.0	1	0.0	0.0		
I-15 NB		RO_3	80.9	0.0	0.0			12365.0	0.0	0.0	7.1	0.0	0.0	105		33.53	0.0	1	0.0	0.0		
I-15 SB		RO_4	80.7	0.0	0.0			11684.0	0.0	0.0	7.1	0.0	0.0	105		33.53	0.0	1	0.0	0.0		

Geometry - Roads

Name	Н	eight		Coordinat	es		Dist	LSlope
	Begin	End	x	у	Z	Ground	(m)	(%)
	(m)	(m)	(m)	(m)	(m)	(m)		
Rancho Carmel Dr			497.74	135.08	175.00	175.00		
			501.94	213.20	175.00	175.00		
			505.30	257.30	173.00	173.00		
			526.11	329.14	172.00	172.00		
			527.30	332.29	172.03	172.00		
Rancho Carmel Dr			527.30	332.29	172.03	172.00		
			598.26	519.95	174.00	172.00		
Ted Williams			996.59	337.98	201.00	201.00		
			880.67	245.58	197.00	197.00		
			713.51	145.61	188.00	188.00		
			595.06	111.17	186.00	180.00		
			500.98	112.85	180.00	180.00		
			401.02	112.85	180.00	180.00		
			236.38	108.65	176.00	176.00		
			83.49	96.05	176.00	176.00		
I-15 NB			-242.64	-478.34	159.00	159.00		
			185.32	347.46	177.00	177.00		
			445.68	859.53	186.00	186.00		
I-15 SB			411.71	892.06	186.00	186.00		
			146.48	366.07	177.00	177.00		
			-281.96	-465.76	159.00	159.00		

Terrain Contours

Name	Μ.	ID	OnlyPts	Hei	ght	C	oordinates	
				Begin	End	x	у	Z
				(m)	(m)	(m)	(m)	(m)
North Course		C1				563.50	372.00	173.00
						574.17	404.35	171.00
						780.62	480.39	186.00
						809.63	466.72	189.00
						813.30	433.03	188.00
						790.95	411.69	187.00
						683.23	374.00	177.00
						637.54	357.99	175.00
						615.53	355.99	174.00
						563.84	372.00	171.00
172		C2		172.00		556.00	365.82	172.00
						547.38	345.86	172.00
						545.49	336.20	172.00
						553.90	329.89	172.00
						564.44	327.46	172.00
						577.64	326.32	172.00
						598.23	328.84	172.00
						624.91	336.41	172.00
						626.27	339.42	172.00
						626.02	348.78	172.00
						625.54	351.95	172.00
						605.37	347.96	172.00
						583.31	351.95	172.00
						555.79	367.08	172.00
North Res		C3				426.09	539.36	169.00
						482.39	475.49	170.00
						540.38	425.07	171.00
						560.70	420.64	171.00
North Res		C3				560.70	420.64	171.00
						573.16	417.92	171.00
						630.30	430.53	174.00
						788.30	492.30	189.00
						862.67	528.85	200.00
						599.42	522.13	172.00
						445.42	523.81	170.00
Southeast		C4				538.65	306.85	173.00
						520.65	171.32	175.00
						633.94	170.79	183.00
						726.06	190.90	187.00
						776.36	226.90	187.00
						864.77	269.79	194.00
						855.24	441.32	196.00
						767.89	377.26	183.00
						723.41	366.14	182.00

Name	М.	ID	OnlyPts	Height		C	oordinates	
				Begin	End	x	у	Z
				(m)	(m)	(m)	(m)	(m)
						678.94	337.55	182.00
						620.71	329.61	178.00
						590.53	301.02	175.00
						536.53	307.38	173.00
West		C5				466.40	173.26	173.00
						326.99	154.58	176.00
						133.56	129.90	176.00
						196.26	293.99	172.00
						302.31	520.11	175.00
						399.03	492.76	166.00
						534.43	410.05	168.00
						502.42	312.67	172.00
						483.74	262.64	171.00
						468.40	179.93	173.00
I-15 E		C6				-217.71	-485.05	159.00
						206.52	336.72	177.00
						471.22	855.55	186.00
I-15 W		C7				-306.65	-442.69	159.00
						117.57	379.08	177.00
						382.28	897.90	186.00
TW N		C8				985.66	349.66	201.00
						873.96	261.25	197.00
						709.84	160.13	188.00
						593.90	127.83	180.00
TW S		C9				1005.78	320.54	201.00
						894.07	232.13	197.00
						729.96	131.01	188.00
						614.01	98.72	180.00

210 South Juniper Street, Suite 100 Escondido, California 92025-4230 Phone: (760) 738-5570

Date: 19 Sep 2019

Configuration	
Parameter	Value
General	
Country	(user defined)
Max. Error (dB)	0.00
Max. Search Radius (#(Unit,LEN))	2000.00
Min. Dist Src to Rcvr	0.00
Partition	
Raster Factor	0.50
Max. Length of Section (#(Unit,LEN))	1000.00
Min. Length of Section (#(Unit,LEN))	1.00
Min. Length of Section (%)	0.00
Proj. Line Sources	On
Proj. Area Sources	On
Ref. Time	
Reference Time Day (min)	960.00
Reference Time Night (min)	480.00
Daytime Penalty (dB)	0.00
Recr. Time Penalty (dB)	6.00
Night-time Penalty (dB)	10.00
DTM	
Standard Height (m)	0.00
Model of Terrain	Triangulation
Reflection	
max. Order of Reflection	0
Search Radius Src	100.00
Search Radius Rcvr	100.00
Max. Distance Source - Rcvr	1000.00 1000.00
Min. Distance Rvcr - Reflector	1.00 1.00
Min. Distance Source - Reflector	0.10
Industrial (ISO 9613)	
Lateral Diffraction	some Obj
Obst. within Area Src do not shield	On
Screening	Excl. Ground Att. over Barrier
	Dz with limit (20/25)
Barrier Coefficients C1,2,3	3.0 20.0 0.0
Temperature (#(Unit,TEMP))	10
rel. Humidity (%)	70
Ground Absorption G	0.50
Wind Speed for Dir. (#(Unit,SPEED))	3.0
Roads (TNM)	
Railways (Schall 03 (1990))	
Strictly acc. to Schall 03 / Schall-Transrapid	
Aircraft (???)	
Strictly acc. to AzB	

Receivers

Name	M.	ID	Leve	el Lr	Limit.	Value		Land	d Use	Height		C	oordinates	
			Day	Night	Day	Night	Туре	Auto	Noise Type			Х	Y	Z
			(dBA)	(dBA)	(dBA)	(dBA)				(m)		(m)	(m)	(m)
OU1			64.4	-73.1	65.4	0.0				178.10	а	566.10	331.62	178.10
OU2			65.2	-71.8	65.4	0.0				181.15	а	559.40	334.66	181.15
OU3-1			68.7	-69.5	65.4	0.0				178.10	а	557.76	360.39	178.10
OU3-2			68.1	-69.8	65.4	0.0				181.15	а	557.76	360.39	181.15
OU3-3			67.7	-70.3	65.4	0.0				184.20	а	557.76	360.39	184.20
OU3-4			68.0	-70.2	65.4	0.0				187.25	а	557.76	360.39	187.25
OU4-1			64.5	-73.1	65.4	0.0				178.10	а	566.79	356.87	178.10
OU4-2			63.8	-73.3	65.4	0.0				181.15	а	566.79	356.87	181.15
OU4-3			64.0	-73.4	65.4	0.0				184.20	а	566.79	356.87	184.20
OU4-4			64.1	-73.5	65.4	0.0				187.25	а	566.79	356.87	187.25
OU5-1			63.0	-74.3	65.4	0.0				178.10	а	573.46	354.03	178.10
OU5-2			62.5	-74.4	65.4	0.0				181.15	а	573.46	354.03	181.15
OU5-3			62.7	-74.5	65.4	0.0				184.20	а	573.46	354.03	184.20
OU5-4			63.1	-74.4	65.4	0.0				187.25	а	573.46	354.03	187.25
OU6-1			64.8	-73.9	65.4	0.0				178.10	а	579.87	351.36	178.10
OU6-2			64.2	-74.1	65.4	0.0				181.15	а	579.87	351.36	181.15
OU6-3			64.9	-74.1	65.4	0.0				184.20	а	579.87	351.36	184.20
OU6-4			65.2	-74.0	65.4	0.0				187.25	а	579.87	351.36	187.25
OU7-1			62.8	-74.6	65.4	0.0				178.10	а	586.43	348.89	178.10
OU7-2			62.4	-74.6	65.4	0.0				181.15	а	586.43	348.89	181.15
OU7-3			63.1	-74.5	65.4	0.0				184.20	а	586.43	348.89	184.20
OU7-4			63.7	-74.4	65.4	0.0				187.25	а	586.43	348.89	187.25
OU8-1			60.2	-76.3	65.4	0.0				178.10	а	595.98	344.64	178.10
OU8-2			59.7	-76.3	65.4	0.0				181.15	а	595.98	344.64	181.15
OU8-3			60.4	-76.4	65.4	0.0				184.20	а	595.98	344.64	184.20
OU8-4			60.8	-76.3	65.4	0.0				187.25	а	595.98	344.64	187.25
OU9-1			62.3	-75.7	65.4	0.0				178.10	а	608.06	342.22	178.10
OU9-2			60.7	-75.8	65.4	0.0				181.15	а	608.06	342.22	181.15
OU9-3			61.5	-75.8	65.4	0.0				184.20	а	608.06	342.22	184.20
OU9-4			62.3	-75.6	65.4	0.0				187.25	а	608.06	342.22	187.25

Roads

Name	M.	ID		Lme		Cou	Int Data exact Cour			Int Data Speed Limit			SCS	Surface	Gradient	Mul	t. Reflee	ction			
			Day	Evening	Night	DTV	Str.class.		М			p (%)		Auto	Truck	Dist.	Dstro Type		Drefl	Hbuild	Dist.
			(dBA)	(dBA)	(dBA)			Day	Evening	Night	Day	Evening	Night	(km/h)	(km/h)		(dB)	(%)	(dB)	(m)	(m)
Rancho Carmel Dr		RO_1	68.4	0.0	0.0			1858.0	0.0	0.0	2.0	0.0	0.0	72		15.24	0.0 1	0.0	0.0		
Ted Williams		RO_2	75.3	0.0	0.0			6238.0	0.0	0.0	5.0	0.0	0.0	89		24.38	0.0 1	0.0	0.0		
I-15 NB		RO_3	80.9	0.0	0.0			12365.0	0.0	0.0	7.1	0.0	0.0	105		33.53	0.0 1	0.0	0.0		
I-15 SB		RO_4	80.7	0.0	0.0			11684.0	0.0	0.0	7.1	0.0	0.0	105		33.53	0.0 1	0.0	0.0		

Geometry - Roads

Name	He	eight		Coordinate	es		Dist	LSlope
	Begin	End	x	у	Z	Ground	(m)	(%)
	(m)	(m)	(m)	(m)	(m)	(m)		
Rancho Carmel Dr			497.74	135.08	175.00	175.00		
			501.94	213.20	175.00	175.00		
			505.30	257.30	173.00	173.00		
			526.11	329.14	172.00	172.00		
			598.26	519.95	174.00	172.00		
Ted Williams			996.59	337.98	201.00	201.00		
			880.67	245.58	197.00	197.00		
			713.51	145.61	188.00	188.00		
			595.06	111.17	186.00	180.00		
			500.98	112.85	180.00	180.00		
			401.02	112.85	180.00	180.00		
			236.38	108.65	176.00	176.00		
			83.49	96.05	176.00	176.00		
I-15 NB			-242.64	-478.34	159.00	159.00		
			185.32	347.46	177.00	177.00		
			445.68	859.53	186.00	186.00		
I-15 SB			411.71	892.06	186.00	186.00		
			146.48	366.07	177.00	177.00		
			-281.96	-465.76	159.00	159.00		

Buildings

Name	M.	ID	RB	Residents	Absorption	Height	
						Begin	
						(m)	
	+		х	0			
	+		х	0			

Geometry - Buildings

New				Desident	Alexand	L La Sach A		0		
Name	M.	טו	кВ	Residents	Absorption	Height		Coordinat	es	
L						Begin	X	у	Z	Ground
						(m)	(m)	(m)	(m)	(m)
	+		Х	0			546.92	338.60	176.88	172.00
							554.93	334.96	176.88	172.00
							554.07	332.44	176.88	172.00
							564.99	328.01	176.88	172.00
							574.39	328.01	176.88	172.00
							575.78	331.25	176.88	172.00
							588.15	327.35	176.88	172.00
							590.07	327.48	176.88	172.00
							590.87	329.66	176.88	172.00
							617.40	336.02	176.88	172.00
							624.29	337.41	176.88	172.00
							622.76	342.37	176.88	172.00
							625.74	342.83	176.88	172.00
							624.62	348.33	176.88	172.00
							601.45	343.63	176.88	172.00
							556.59	361.96	176.88	172.00
	+		х	0			548.04	341.39	189.50	176.88
							549.78	340.76	189.50	176.88
							548.59	337.82	189.50	176.88
							555.14	335.17	189.50	176.88
							555.71	336.71	189.50	176.88
							557.78	335.79	189.50	176.88
							558.81	337.78	189.50	176.88
							560.96	336.75	189.50	176.88
							561.89	339.18	189.50	176.88
							565.78	337.46	189.50	176.88
							566.32	338.98	189.50	176.88
							572.53	336.46	189.50	176.88
							572.17	334.90	189.50	176.88
							578.91	331.87	189.50	176.88
							579.37	333.42	189.50	176.88
							585.59	330.88	189.50	176.88
							585.12	329.38	189.50	176.88
							588.44	327.85	189.50	176.88
							589.66	330.20	189.50	176.88
							589.95	329.81	189.50	176.88

Name	M.	ID	RB	Residents	Absorption	Height		Coordinate	es	
						Begin	x	У	Z	Ground
						(m)	(m)	(m)	(m)	(m)
							592.36	328.93	189.50	176.88
							603.14	331.10	189.50	176.88
							609.23	332.35	189.50	176.88
							608.66	334.20	189.50	176.88
							613.87	335.30	189.50	176.88
							612.13	341.95	189.50	176.88
							608.86	341.32	189.50	176.88
							608.15	340.21	0.00	0.00
							605.09	341.29	189.50	176.88
							597.99	344.42	189.50	176.88
							597.40	342.89	189.50	176.88
							594.37	344.19	189.50	176.88
							594.92	345.59	189.50	176.88
							588.16	348.38	189.50	176.88
							587.88	347.08	0.00	0.00
							584.78	348.22	189.50	176.88
							585.15	349.72	0.00	0.00
							581.81	351.27	189.50	176.88
							581.27	349.70	0.00	0.00
							578.04	350.99	0.00	0.00
							578.80	352.33	189.50	176.88
							575.36	353.65	189.50	176.88
							574.94	352.55	189.50	176.88
							571.88	353.91	189.50	176.88
							572.34	354.98	189.50	176.88
							568.91	356.55	189.50	176.88
							568.60	355.24	189.50	176.88
							564.94	356.62	189.50	176.88
							565.49	357.89	189.50	176.88
							559.09	360.78	189.50	176.88
							558.60	359.23	189.50	176.88
							555.91	360.41	189.50	176.88
							550.62	347.60	189.50	176.88
							552.39	346.79	189.50	176.88
							551.17	343.98	189.50	176.88
							549.52	344.75	189.50	176.88

Terrain Contours

Name	Μ.	ID	OnlyPts	Hei	ght	C	oordinates	
				Begin	End	x	у	z
				(m)	(m)	(m)	(m)	(m)
North Course		C1				563.50	372.00	173.00
						574.17	404.35	171.00
						780.62	480.39	186.00
						809.63	466.72	189.00
						813.30	433.03	188.00
						790.95	411.69	187.00
						683.23	374.00	177.00
						637.54	357.99	175.00
						615.53	355.99	174.00
						563.84	372.00	171.00
172		C2		172.00		556.00	365.82	172.00
						547.38	345.86	172.00
						545.49	336.20	172.00
						553.90	329.89	172.00
						564.44	327.46	172.00
						577.64	326.32	172.00
						598.23	328.84	172.00
						624.91	336.41	172.00
						626.27	339.42	172.00
						626.02	348.78	172.00
						625.54	351.95	172.00
						605.37	347.96	172.00
						583.31	351.95	172.00
						555.79	367.08	172.00
North Res		C3				426.09	539.36	169.00
						482.39	475.49	170.00
						540.38	425.07	171.00
						573.16	417.92	171.00
						630.30	430.53	174.00
						788.30	492.30	189.00
						862.67	528.85	200.00
						599.42	522.13	172.00
O south a set		0.4				445.42	523.81	170.00
Southeast		64				538.65	306.85	173.00
						520.65	171.32	175.00
						633.94	170.79	183.00
	-					726.06	190.90	187.00
	<u> </u>					//0.30	226.90	101.00
	-					864.77	269.79	194.00
	-					855.24	441.32	196.00
						767.89	377.26	183.00
	-					/23.41	366.14	182.00
	-					678.94	337.55	182.00
						620.71	329.61	178.00

Name	Μ.	ID	OnlyPts	Hei	ight	C	oordinates	
				Begin	End	х	у	Z
				(m)	(m)	(m)	(m)	(m)
						590.53	301.02	175.00
						536.53	307.38	173.00
West		C5				466.40	173.26	173.00
						326.99	154.58	176.00
						133.56	129.90	176.00
						196.26	293.99	172.00
						302.31	520.11	175.00
						399.03	492.76	166.00
						534.43	410.05	168.00
						502.42	312.67	172.00
						483.74	262.64	171.00
						468.40	179.93	173.00
I-15 E		C6				-217.71	-485.05	159.00
						206.52	336.72	177.00
						471.22	855.55	186.00
I-15 W		C7				-306.65	-442.69	159.00
						117.57	379.08	177.00
						382.28	897.90	186.00
TW N		C8				985.66	349.66	201.00
						873.96	261.25	197.00
						709.84	160.13	188.00
						593.90	127.83	180.00
TW S		C9				1005.78	320.54	201.00
						894.07	232.13	197.00
						729.96	131.01	188.00
						614.01	98.72	180.00

210 South Juniper Street, Suite 100 Escondido, California 92025-4230 Phone: (760) 738-5570

Date: 19 Sep 2019

Configuration	
Parameter	Value
General	
Country	(user defined)
Max. Error (dB)	0.00
Max. Search Radius (#(Unit,LEN))	2000.00
Min. Dist Src to Rcvr	0.00
Partition	
Raster Factor	0.50
Max. Length of Section (#(Unit,LEN))	1000.00
Min. Length of Section (#(Unit,LEN))	1.00
Min. Length of Section (%)	0.00
Proj. Line Sources	On
Proj. Area Sources	On
Ref. Time	
Reference Time Day (min)	960.00
Reference Time Night (min)	480.00
Daytime Penalty (dB)	0.00
Recr. Time Penalty (dB)	6.00
Night-time Penalty (dB)	10.00
DTM	
Standard Height (m)	0.00
Model of Terrain	Triangulation
Reflection	
max. Order of Reflection	0
Search Radius Src	100.00
Search Radius Rcvr	100.00
Max. Distance Source - Rcvr	1000.00 1000.00
Min. Distance Rvcr - Reflector	1.00 1.00
Min. Distance Source - Reflector	0.10
Industrial (ISO 9613)	
Lateral Diffraction	some Obj
Obst. within Area Src do not shield	On
Screening	Excl. Ground Att. over Barrier
	Dz with limit (20/25)
Barrier Coefficients C1,2,3	3.0 20.0 0.0
Temperature (#(Unit,TEMP))	10
rel. Humidity (%)	70
Ground Absorption G	0.50
Wind Speed for Dir. (#(Unit,SPEED))	3.0
Roads (TNM)	
Railways (Schall 03 (1990))	
Strictly acc. to Schall 03 / Schall-Transrapid	
Aircraft (???)	
Strictly acc. to AzB	

Receivers

		-												
Name	Μ.	ID	Leve	əl Lr	Limit.	Value		Land	d Use	Height		C	oordinates	
			Day	Night	Day	Night	Туре	Auto	Noise Type			Х	Y	Z
			(dBA)	(dBA)	(dBA)	(dBA)				(m)		(m)	(m)	(m)
OU3-1			63.6	-75.5	65.4	0.0				178.10	а	558.25	359.53	178.10
OU3-2	+		64.5	-72.4	65.4	0.0				181.15	а	558.25	359.53	181.15
OU3-3	+		64.7	-72.4	65.4	0.0				184.20	а	558.25	359.53	184.20
OU3-4	+		65.0	-72.9	65.4	0.0				187.25	а	558.25	359.53	187.25

Roads

Name	M.	ID		Lme		Cou	nt Data		e	xact Cou	int Data	1		Speed	l Limit	SCS	Surf	ace	Gradient	Mul	t. Reflee	ction
			Day	Evening	Night	DTV	Str.class.		М			p (%)		Auto	Truck	Dist.	Dstro	Туре		Drefl	Hbuild	Dist.
			(dBA)	(dBA)	(dBA)			Day	Evening	Night	Day	Evening	Night	(km/h)	(km/h)		(dB)		(%)	(dB)	(m)	(m)
Rancho Carmel Dr		RO_1	68.4	0.0	0.0			1858.0	0.0	0.0	2.0	0.0	0.0	72		15.24	0.0	1	0.0	0.0		
Ted Williams		RO_2	75.3	0.0	0.0			6238.0	0.0	0.0	5.0	0.0	0.0	89		24.38	0.0	1	0.0	0.0		
I-15 NB		RO_3	80.9	0.0	0.0			12365.0	0.0	0.0	7.1	0.0	0.0	105		33.53	0.0	1	0.0	0.0		
I-15 SB		RO_4	80.7	0.0	0.0			11684.0	0.0	0.0	7.1	0.0	0.0	105		33.53	0.0	1	0.0	0.0		

Geometry - Roads

Name	He	eight		Coordinate	es		Dist	LSlope
	Begin	End	x	у	Z	Ground	(m)	(%)
	(m)	(m)	(m)	(m)	(m)	(m)		
Rancho Carmel Dr			497.74	135.08	175.00	175.00		
			501.94	213.20	175.00	175.00		
			505.30	257.30	173.00	173.00		
			526.11	329.14	172.00	172.00		
			598.26	519.95	174.00	172.00		
Ted Williams			996.59	337.98	201.00	201.00		
			880.67	245.58	197.00	197.00		
			713.51	145.61	188.00	188.00		
			595.06	111.17	186.00	180.00		
			500.98	112.85	180.00	180.00		
			401.02	112.85	180.00	180.00		
			236.38	108.65	176.00	176.00		
			83.49	96.05	176.00	176.00		
I-15 NB			-242.64	-478.34	159.00	159.00		
			185.32	347.46	177.00	177.00		
			445.68	859.53	186.00	186.00		
I-15 SB			411.71	892.06	186.00	186.00		
			146.48	366.07	177.00	177.00		
			-281.96	-465.76	159.00	159.00		

Barriers

Name	M.	ID	Abso	orption	Z-Ext.	Cant	ilever	H	eight	
			left	right		horz.	vert.	Begin	End	
					(m)	(m)	(m)	(m)	(m)	
B3-1	+				1.07					
B3-2	+				1.22					
B3-3	+				1.22					
B3-4	+				1.22					

Geometry - Barriers

Name	M.	ID	Abso	orption	Z-Ext.	Cant	ilever	He	eight		Coordinate	es	
			left	right		horz.	vert.	Begin	End	x	У	Z	Ground
					(m)	(m)	(m)	(m)	(m)	(m)	(m)	(m)	(m)
B3-1	+				1.07					555.94	360.43	177.95	172.00
										556.65	362.43	177.95	172.00
										559.49	361.25	177.95	172.00
										559.18	360.51	177.95	172.00
B3-2	+				1.22					555.94	360.43	181.15	172.00
										556.65	362.43	181.15	172.00
										559.49	361.25	181.15	172.00
										559.18	360.51	181.15	172.00
B3-3	+				1.22					555.94	360.43	184.20	172.00
										556.65	362.43	184.20	172.00
										559.49	361.25	184.20	172.00
										559.18	360.51	184.20	172.00
B3-4	+				1.22					555.94	360.43	187.25	172.00
										556.65	362.43	187.25	172.00
										559.49	361.25	187.25	172.00
										559.18	360.51	187.25	172.00

Buildings

	_	-					
Name	M.	ID	RB	Residents	Absorption	Height	
						Begin	
						(m)	
	+		х	0			
	+		х	0			

Geometry - Buildings

Name	M.	ÍD	RB	Residents	Absorption	Height		Coordinat	es	
					•	Begin	x	y	Z	Ground
						(m)	(m)	(m)	(m)	(m)
	+		х	0		. ,	546.92	338.60	176.88	172.00
							554.93	334.96	176.88	172.00
							554.07	332.44	176.88	172.00
							564.99	328.01	176.88	172.00
							574.39	328.01	176.88	172.00
							575.78	331.25	176.88	172.00
							588.15	327.35	176.88	172.00
							590.07	327.48	176.88	172.00
							590.87	329.66	176.88	172.00
							617.40	336.02	176.88	172.00
							624.29	337.41	176.88	172.00
							622.76	342.37	176.88	172.00
							625.74	342.83	176.88	172.00
							624.62	348.33	176.88	172.00
							601.45	343.63	176.88	172.00
							556.59	361.96	176.88	172.00
	+		х	0			547.96	341.49	189.50	176.88
							549.70	340.86	189.50	176.88
							548.50	337.92	189.50	176.88
							555.05	335.27	189.50	176.88
							555.63	336.82	189.50	176.88
							557.70	335.89	189.50	176.88
							558.72	337.88	189.50	176.88
							560.88	336.86	189.50	176.88
							561.81	339.28	189.50	176.88
							565.69	337.56	189.50	176.88
							566.24	339.09	189.50	176.88
							572.45	336.57	189.50	176.88
							572.09	335.01	189.50	176.88
							578.82	331.97	189.50	176.88
							579.29	333.52	189.50	176.88
							585.50	330.98	189.50	176.88
							585.04	329.48	189.50	176.88
							588.36	327.96	189.50	176.88
							589.57	330.30	189.50	176.88
							589.87	329.91	189.50	176.88

Name	M.	ID	RB	Residents	Absorption	Height		Coordinat	es	
						Begin	x	У	Z	Ground
						(m)	(m)	(m)	(m)	(m)
							592.28	329.03	189.50	176.88
							603.06	331.21	189.50	176.88
							609.15	332.45	189.50	176.88
							608.58	334.30	189.50	176.88
							613.79	335.41	189.50	176.88
							612.04	342.05	189.50	176.88
							608.78	341.43	189.50	176.88
							608.07	340.32	0.00	0.00
							605.00	341.39	189.50	176.88
							597.91	344.52	189.50	176.88
							597.32	342.99	189.50	176.88
							594.29	344.30	189.50	176.88
							594.84	345.69	189.50	176.88
							588.07	348.49	189.50	176.88
							587.79	347.18	0.00	0.00
							584.69	348.32	189.50	176.88
							585.06	349.83	0.00	0.00
							581.73	351.37	189.50	176.88
							581.19	349.81	0.00	0.00
							577.96	351.10	0.00	0.00
							578.72	352.43	189.50	176.88
							575.28	353.75	189.50	176.88
							574.86	352.66	189.50	176.88
							571.79	354.01	189.50	176.88
							572.25	355.08	189.50	176.88
							568.83	356.66	189.50	176.88
							568.52	355.34	189.50	176.88
							564.86	356.73	189.50	176.88
							565.40	358.00	189.50	176.88
							559.00	360.88	189.50	176.88
							558.51	359.33	189.50	176.88
							555.83	360.52	189.50	176.88
							550.53	347.70	189.50	176.88
							552.31	346.89	189.50	176.88
							551.08	344.08	189.50	176.88
							549.44	344.85	189.50	176.88

Terrain Contours

Name	Μ.	ID	OnlyPts	Hei	ght	C	oordinates	
				Begin	End	x	у	Z
				(m)	(m)	(m)	(m)	(m)
North Course		C1				563.50	372.00	173.00
						574.17	404.35	171.00
						780.62	480.39	186.00
						809.63	466.72	189.00
						813.30	433.03	188.00
						790.95	411.69	187.00
						683.23	374.00	177.00
						637.54	357.99	175.00
						615.53	355.99	174.00
						563.84	372.00	171.00
172		C2		172.00		556.00	365.82	172.00
						547.38	345.86	172.00
						545.49	336.20	172.00
						553.90	329.89	172.00
						564.44	327.46	172.00
						577.64	326.32	172.00
						598.23	328.84	172.00
						624.91	336.41	172.00
						626.27	339.42	172.00
						626.02	348.78	172.00
						625.54	351.95	172.00
						605.37	347.96	172.00
						583.31	351.95	172.00
						555.79	367.08	172.00
North Res		C3				426.09	539.36	169.00
						482.39	475.49	170.00
						540.38	425.07	171.00
						573.16	417.92	171.00
						630.30	430.53	174.00
						788.30	492.30	189.00
						862.67	528.85	200.00
						599.42	522.13	172.00
						445.42	523.81	170.00
Southeast		C4				538.65	306.85	173.00
						520.65	171.32	175.00
						633.94	170.79	183.00
						726.06	190.90	187.00
						776.36	226.90	187.00
						864.77	269.79	194.00
						855.24	441.32	196.00
						767.89	377.26	183.00
						723.41	366.14	182.00
						678.94	337.55	182.00
						620.71	329.61	178.00

Name	Μ.	ID	OnlyPts	s Height		C	oordinates	
				Begin	End	х	у	Z
				(m)	(m)	(m)	(m)	(m)
						590.53	301.02	175.00
						536.53	307.38	173.00
West		C5				466.40	173.26	173.00
						326.99	154.58	176.00
						133.56	129.90	176.00
						196.26	293.99	172.00
						302.31	520.11	175.00
						399.03	492.76	166.00
						534.43	410.05	168.00
						502.42	312.67	172.00
						483.74	262.64	171.00
						468.40	179.93	173.00
I-15 E		C6				-217.71	-485.05	159.00
						206.52	336.72	177.00
						471.22	855.55	186.00
I-15 W		C7				-306.65	-442.69	159.00
						117.57	379.08	177.00
						382.28	897.90	186.00
TW N		C8				985.66	349.66	201.00
						873.96	261.25	197.00
						709.84	160.13	188.00
						593.90	127.83	180.00
TW S		C9				1005.78	320.54	201.00
						894.07	232.13	197.00
						729.96	131.01	188.00
						614.01	98.72	180.00

210 South Juniper Street, Suite 100 Escondido, California 92025-4230 Phone: (760) 738-5570

Date: 19 Sep 2019

Configuration	
Parameter	Value
General	
Country	(user defined)
Max. Error (dB)	0.00
Max. Search Radius (#(Unit,LEN))	2000.00
Min. Dist Src to Rcvr	0.00
Partition	
Raster Factor	0.50
Max. Length of Section (#(Unit,LEN))	1000.00
Min. Length of Section (#(Unit,LEN))	1.00
Min. Length of Section (%)	0.00
Proj. Line Sources	On
Proj. Area Sources	On
Ref. Time	
Reference Time Day (min)	960.00
Reference Time Night (min)	480.00
Daytime Penalty (dB)	0.00
Recr. Time Penalty (dB)	6.00
Night-time Penalty (dB)	10.00
DTM	
Standard Height (m)	0.00
Model of Terrain	Triangulation
Reflection	
max. Order of Reflection	0
Search Radius Src	100.00
Search Radius Rcvr	100.00
Max. Distance Source - Rcvr	1000.00 1000.00
Min. Distance Rvcr - Reflector	1.00 1.00
Min. Distance Source - Reflector	0.10
Industrial (ISO 9613)	
Lateral Diffraction	some Obj
Obst. within Area Src do not shield	On
Screening	Excl. Ground Att. over Barrier
	Dz with limit (20/25)
Barrier Coefficients C1,2,3	3.0 20.0 0.0
Temperature (#(Unit,TEMP))	10
rel. Humidity (%)	70
Ground Absorption G	0.50
Wind Speed for Dir. (#(Unit,SPEED))	3.0
Roads (TNM)	
Railways (Schall 03 (1990))	
Strictly acc. to Schall 03 / Schall-Transrapid	
Aircraft (???)	
Strictly acc. to AzB	

Receivers

Name	M.	ID	Leve	el Lr	Limit.	Value	e Land Use		Height Coordinates					
			Day	Night	Day	Night	Туре	Auto	Noise Type			Х	Y	Z
			(dBA)	(dBA)	(dBA)	(dBA)				(m)		(m)	(m)	(m)
F1-1			70.9	-66.7	65.4	0.0				178.40	а	551.10	350.14	178.40
F1-2			70.2	-67.2	65.4	0.0				181.45	а	551.10	350.14	181.45
F1-3			70.2	-67.5	65.4	0.0				184.50	а	551.10	350.14	184.50
F1-4			69.9	-68.0	65.4	0.0				187.55	а	551.10	350.14	187.55
F2-1			66.3	-71.4	65.4	0.0				178.40	а	563.81	359.51	178.40
F2-2			66.1	-71.5	65.4	0.0				181.45	а	563.81	359.51	181.45
F2-3			66.4	-71.7	65.4	0.0				184.50	а	563.81	359.51	184.50
F2-4			66.4	-71.9	65.4	0.0				187.55	а	563.81	359.51	187.55
F3-1			64.1	-73.7	65.4	0.0				178.40	а	579.25	353.10	178.40
F3-2			63.4	-73.9	65.4	0.0				181.45	а	579.25	353.10	181.45
F3-3			63.9	-73.9	65.4	0.0				184.50	а	579.25	353.10	184.50
F3-4			64.5	-73.8	65.4	0.0				187.55	а	579.25	353.10	187.55
F4-1			62.6	-74.9	65.4	0.0				178.40	а	592.59	347.63	178.40
F4-2			62.1	-75.0	65.4	0.0				181.45	а	592.59	347.63	181.45
F4-3			62.7	-75.0	65.4	0.0				184.50	а	592.59	347.63	184.50
F4-4			63.3	-75.0	65.4	0.0				187.55	а	592.59	347.63	187.55
F5-1			61.4	-75.9	65.4	0.0				178.40	а	609.99	342.02	178.40
F5-2			60.7	-75.9	65.4	0.0				181.45	а	609.99	342.02	181.45
F5-3			61.4	-76.0	65.4	0.0				184.50	а	609.99	342.02	184.50
F5-4			62.1	-75.8	65.4	0.0				187.55	а	609.99	342.02	187.55
F6-1			56.0	-77.7	65.4	0.0				178.40	а	613.20	339.27	178.40
F6-2			56.9	-77.7	65.4	0.0				181.45	а	613.20	339.27	181.45
F6-3			57.7	-77.7	65.4	0.0				184.50	а	613.20	339.27	184.50
F6-4			58.7	-77.6	65.4	0.0				187.55	а	613.20	339.27	187.55
F7-1			62.7	-74.5	65.4	0.0				178.40	а	584.37	328.45	178.40
F7-2			63.6	-73.9	65.4	0.0				181.45	а	584.37	328.45	181.45
F7-3			64.3	-73.7	65.4	0.0				184.50	а	584.37	328.45	184.50
F7-4			64.8	-73.5	65.4	0.0				187.55	а	584.37	328.45	187.55
F8-1			62.9	-74.0	65.4	0.0				178.40	а	568.86	333.85	178.40
F8-2			64.3	-72.9	65.4	0.0				181.45	а	568.86	333.85	181.45
F8-3			64.6	-72.9	65.4	0.0				184.50	а	568.86	333.85	184.50
F8-4			64.9	-72.8	65.4	0.0				187.55	а	568.86	333.85	187.55
F9-1			67.1	-69.8	65.4	0.0				178.40	а	552.92	335.30	178.40
F9-2			67.0	-70.0	65.4	0.0				181.45	а	552.92	335.30	181.45
F9-3			67.2	-70.2	65.4	0.0				184.50	а	552.92	335.30	184.50
F9-4			67.4	-70.3	65.4	0.0				187.55	а	552.92	335.30	187.55

Roads

Name	M.	ID		Lme		Cou	Int Data exact Count D			int Data	a	Speed Limit		l Limit	SCS	Surf	ace	Gradient	Mul	t. Reflee	ction	
			Day	Evening	Night	DTV	Str.class.		М			p (%)		Auto	Truck	Dist.	Dstro	Туре		Drefl	Hbuild	Dist.
			(dBA)	(dBA)	(dBA)			Day	Evening	Night	Day	Evening	Night	(km/h)	(km/h)		(dB)		(%)	(dB)	(m)	(m)
Rancho Carmel Dr		RO_1	68.4	0.0	0.0			1858.0	0.0	0.0	2.0	0.0	0.0	72		15.24	0.0	1	0.0	0.0		
Ted Williams		RO_2	75.3	0.0	0.0			6238.0	0.0	0.0	5.0	0.0	0.0	89		24.38	0.0	1	0.0	0.0		
I-15 NB		RO_3	80.9	0.0	0.0			12365.0	0.0	0.0	7.1	0.0	0.0	105		33.53	0.0	1	0.0	0.0		
I-15 SB		RO_4	80.7	0.0	0.0			11684.0	0.0	0.0	7.1	0.0	0.0	105		33.53	0.0	1	0.0	0.0		

Geometry - Roads

Name	He	eight		Coordinat	es		Dist	LSlope
	Begin	End	x	У	Z	Ground	(m)	(%)
	(m)	(m)	(m)	(m)	(m)	(m)		
Rancho Carmel Dr			497.74	135.08	175.00	175.00		
			501.94	213.20	175.00	175.00		
			505.30	257.30	173.00	173.00		
			526.11	329.14	172.00	172.00		
			598.26	519.95	174.00	172.00		
Ted Williams			996.59	337.98	201.00	201.00		
			880.67	245.58	197.00	197.00		
			713.51	145.61	188.00	188.00		
			595.06	111.17	186.00	180.00		
			500.98	112.85	180.00	180.00		
			401.02	112.85	180.00	180.00		
			236.38	108.65	176.00	176.00		
			83.49	96.05	176.00	176.00		
I-15 NB			-242.64	-478.34	159.00	159.00		
			185.32	347.46	177.00	177.00		
			445.68	859.53	186.00	186.00		
I-15 SB			411.71	892.06	186.00	186.00		
			146.48	366.07	177.00	177.00		
			-281.96	-465.76	159.00	159.00		

Buildings

Name	M.	ID	RB	Residents	Absorption	Height
						Begin
						(m)
	+		х	0		
	+		х	0		

Geometry - Buildings

Name -				Desidert	A la a mati	Lainkt		Co o rolling of		
Name	IVI.	טו	кВ	Residents	Absorption	Height		Coordinat	es	
						Begin	X	У	Z	Ground
						(m)	(m)	(m)	(m)	(m)
	+		Х	0			546.92	338.60	176.88	172.00
							554.93	334.96	176.88	172.00
							554.07	332.44	176.88	172.00
							564.99	328.01	176.88	172.00
							574.39	328.01	176.88	172.00
							575.78	331.25	176.88	172.00
							588.15	327.35	176.88	172.00
							590.07	327.48	176.88	172.00
							590.87	329.66	176.88	172.00
							617.40	336.02	176.88	172.00
							624.29	337.41	176.88	172.00
							622.76	342.37	176.88	172.00
							625.74	342.83	176.88	172.00
							624.62	348.33	176.88	172.00
							601.45	343.63	176.88	172.00
							556.59	361.96	176.88	172.00
	+		х	0			548.09	341.43	189.50	176.88
							549.82	340.80	189.50	176.88
							548.63	337.86	189.50	176.88
							555.18	335.21	189.50	176.88
							555.75	336.75	189.50	176.88
							557.82	335.83	189.50	176.88
							558.85	337.82	189.50	176.88
							561.00	336.80	189.50	176.88
							561.94	339.22	189.50	176.88
							565.82	337.50	189.50	176.88
							566.36	339.02	189.50	176.88
							572.57	336.50	189.50	176.88
							572.21	334.94	189.50	176.88
							578.95	331.91	189.50	176.88
							579.41	333.46	189.50	176.88
							585.63	330.92	189.50	176.88
							585.16	329.42	189.50	176.88
							588.48	327.89	189.50	176.88
							589.70	330.24	189.50	176.88
							589.99	329.85	189.50	176.88

Name	M.	ID	RB	Residents	Absorption	Height	t Coordinates			
						Begin	x	У	Z	Ground
						(m)	(m)	(m)	(m)	(m)
							592.41	328.97	189.50	176.88
							603.19	331.15	189.50	176.88
							609.28	332.39	189.50	176.88
							608.70	334.24	189.50	176.88
							613.91	335.34	189.50	176.88
							612.17	341.99	189.50	176.88
							608.90	341.36	189.50	176.88
							608.19	340.25	0.00	0.00
							605.13	341.33	189.50	176.88
							598.04	344.46	189.50	176.88
							597.44	342.93	189.50	176.88
							594.41	344.23	189.50	176.88
							594.96	345.63	189.50	176.88
							588.20	348.42	189.50	176.88
							587.92	347.12	0.00	0.00
							584.82	348.26	189.50	176.88
							585.19	349.76	0.00	0.00
							581.85	351.31	189.50	176.88
							581.31	349.74	0.00	0.00
							578.08	351.03	0.00	0.00
							578.85	352.37	189.50	176.88
							575.40	353.69	189.50	176.88
							574.99	352.59	189.50	176.88
							571.92	353.95	189.50	176.88
							572.38	355.02	189.50	176.88
							568.95	356.60	189.50	176.88
							568.64	355.28	189.50	176.88
							564.99	356.66	189.50	176.88
							565.53	357.94	189.50	176.88
							559.13	360.82	189.50	176.88
							558.64	359.27	189.50	176.88
							555.95	360.46	189.50	176.88
							550.66	347.64	189.50	176.88
							552.43	346.83	189.50	176.88
							551.21	344.02	189.50	176.88
							549.57	344.79	189.50	176.88

Terrain Contours

Name	Μ.	ID	OnlyPts	Hei	ght	C	oordinates	
				Begin	End	x	у	z
				(m)	(m)	(m)	(m)	(m)
North Course		C1				563.50	372.00	173.00
						574.17	404.35	171.00
						780.62	480.39	186.00
						809.63	466.72	189.00
						813.30	433.03	188.00
						790.95	411.69	187.00
						683.23	374.00	177.00
						637.54	357.99	175.00
						615.53	355.99	174.00
						563.84	372.00	171.00
172		C2		172.00		556.00	365.82	172.00
						547.38	345.86	172.00
						545.49	336.20	172.00
						553.90	329.89	172.00
						564.44	327.46	172.00
						577.64	326.32	172.00
						598.23	328.84	172.00
						624.91	336.41	172.00
						626.27	339.42	172.00
						626.02	348.78	172.00
						625.54	351.95	172.00
						605.37	347.96	172.00
						583.31	351.95	172.00
						555.79	367.08	172.00
North Res		C3				426.09	539.36	169.00
						482.39	475.49	170.00
						540.38	425.07	171.00
						573.16	417.92	171.00
						630.30	430.53	174.00
						788.30	492.30	189.00
						862.67	528.85	200.00
						599.42	522.13	172.00
						445.42	523.81	170.00
Southeast		C4				538.65	306.85	173.00
						520.65	171.32	175.00
						633.94	170.79	183.00
						726.06	190.90	187.00
						776.36	226.90	187.00
						864.77	269.79	194.00
						855.24	441.32	196.00
						767.89	377.26	183.00
						723.41	366.14	182.00
						678.94	337.55	182.00
						620.71	329.61	178.00

Name	Μ.	ID	OnlyPts	s Height		C	oordinates	
				Begin	End	х	У	Z
				(m)	(m)	(m)	(m)	(m)
						590.53	301.02	175.00
						536.53	307.38	173.00
West		C5				466.40	173.26	173.00
						326.99	154.58	176.00
						133.56	129.90	176.00
						196.26	293.99	172.00
						302.31	520.11	175.00
						399.03	492.76	166.00
						534.43	410.05	168.00
						502.42	312.67	172.00
						483.74	262.64	171.00
						468.40	179.93	173.00
I-15 E		C6				-217.71	-485.05	159.00
						206.52	336.72	177.00
						471.22	855.55	186.00
I-15 W		C7				-306.65	-442.69	159.00
						117.57	379.08	177.00
						382.28	897.90	186.00
TW N		C8				985.66	349.66	201.00
						873.96	261.25	197.00
						709.84	160.13	188.00
						593.90	127.83	180.00
TW S		C9				1005.78	320.54	201.00
						894.07	232.13	197.00
						729.96	131.01	188.00
						614.01	98.72	180.00

210 South Juniper Street, Suite 100 Escondido, California 92025-4230 Phone: (760) 738-5570

Date: 18 Sep 2019

Configuration	
Parameter	Value
General	
Country	(user defined)
Max. Error (dB)	0.00
Max. Search Radius (#(Unit,LEN))	2000.00
Min. Dist Src to Rcvr	0.00
Partition	
Raster Factor	0.50
Max. Length of Section (#(Unit,LEN))	1000.00
Min. Length of Section (#(Unit,LEN))	1.00
Min. Length of Section (%)	0.00
Proj. Line Sources	On
Proj. Area Sources	On
Ref. Time	
Reference Time Day (min)	960.00
Reference Time Night (min)	480.00
Daytime Penalty (dB)	0.00
Recr. Time Penalty (dB)	6.00
Night-time Penalty (dB)	10.00
DTM	
Standard Height (m)	0.00
Model of Terrain	Triangulation
Reflection	
max. Order of Reflection	0
Search Radius Src	100.00
Search Radius Rcvr	100.00
Max. Distance Source - Rcvr	1000.00 1000.00
Min. Distance Rvcr - Reflector	1.00 1.00
Min. Distance Source - Reflector	0.10
Industrial (ISO 9613)	
Lateral Diffraction	some Obj
Obst. within Area Src do not shield	On
Screening	Excl. Ground Att. over Barrier
	Dz with limit (20/25)
Barrier Coefficients C1,2,3	3.0 20.0 0.0
Temperature (#(Unit,TEMP))	10
rel. Humidity (%)	70
Ground Absorption G	0.50
Wind Speed for Dir. (#(Unit,SPEED))	3.0
Roads (TNM)	
Railways (Schall 03 (1990))	
Strictly acc. to Schall 03 / Schall-Transrapid	
Aircraft (???)	
Strictly acc. to AzB	

Receivers

Name	M.	ID	Lev	el Lr	Limit.	Value		Land	d Use	Height		Co	oordinates	
			Day	Night	Day	Night	Туре	Auto	Noise Type			Х	Y	Z
			(dBA)	(dBA)	(dBA)	(dBA)				(m)		(m)	(m)	(m)
North		R1	31.1	31.1	0.0	0.0		х	Total	1.52	r	584.93	353.45	173.63
South		R2	35.5	35.5	0.0	0.0		х	Total	1.52	r	584.28	296.01	176.39
Southeast		R3	30.9	30.9	0.0	0.0		х	Total	1.52	r	592.35	327.63	173.57
Southeast Res1		R4	27.5	27.5	0.0	0.0		х	Total	1.52	r	621.86	332.54	176.73
Southeast Res2		R5	29.2	29.2	0.0	0.0		х	Total	4.57	r	621.86	332.54	179.78
West		R6	25.3	25.3	0.0	0.0		х	Total	1.52	r	520.71	359.53	171.71

Point Sources

Name	M. I	D	Result. PV	٧L		Lw/L	.i	(Correction	n	Soun	d Reduction	Attenuation	Ope	erating T	ïme	K0	Freq.	Direct.	Height	Co	ordinates	
		Day	Evening	Night	Type	Value	norm.	Day	Evening	Night	R	Area		Day	Special	Night				-	X	Y	Z
		(dBA) (dBA)	(dBA)			dB(A)	dB(A)	dB(A)	dB(A)		(m²)		(min)	(min)	(min)	(dB)	(Hz)		(m)	(m)	(m)	(m)
AC	1	72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	566.44	346.41	190.72
AC	2	2 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	567.60	345.96	190.72
AC	3	5 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	568.76	345.46	190.72
AC	4	72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	569.79	345.13	190.72
AC	5	5 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	570.91	344.59	190.72
AC	e	i 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	572.12	344.13	190.72
AC	7	72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	573.12	343.73	190.72
AC	1	72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	574.37	343.15	190.72
AC	9	72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	575.39	342.76	190.72
AC	1	0 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	576.52	342.32	190.72
AC	1	1 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	577.68	341.82	190.72
AC	1	2 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	578.79	341.34	190.72
AC	1	3 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	579.91	340.96	190.72
AC	1	4 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	580.91	340.46	190.72
AC		5 72	0 72 0	72.0	L w	142		0.0	0.0	0.0							0.0		(none)	190 72 a	582 10	339.96	190 72
AC		6 72	0 72.0	72.0	L w	1 42		0.0	0.0	0.0							0.0		(none)	190 72 a	583.27	339.46	190 72
AC		7 72	0 72.0	72.0	Lw	142		0.0	0.0	0.0							0.0		(none)	190 72 a	584.37	339.13	190.72
AC		8 72	0 72.0	72.0	Lw	142		0.0	0.0	0.0							0.0		(none)	190.72 a	585.60	338.67	190.72
AC		9 72	0 72.0	72.0	Lw	142		0.0	0.0	0.0							0.0		(none)	190.72 a	586.35	338.21	190.72
AC		0 72	0 72.0	72.0	Lw	142		0.0	0.0	0.0							0.0		(none)	190.72 a	587.56	337.76	190.72
		1 72	0 72.0	72.0		1/2		0.0	0.0	0.0							0.0		(none)	190.72 a	588.95	337.73	100.72
AC		1 72	0 72.0	72.0		L42		0.0	0.0	0.0							0.0		(10110)	100.72	500.95	226.90	190.72
AC	4	2 72	0 72.0	72.0		L42		0.0	0.0	0.0							0.0		(nono)	190.72 a	501.14	330.00	190.72
AC		3 72	0 72.0	72.0		L42		0.0	0.0	0.0							0.0		(nono)	190.72 a	502.16	225.00	190.72
AC		4 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	592.10	335.90	190.72
AC		5 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	500.01	345.26	190.72
AC	4	0 72	0 72.0	72.0	LW	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	500.97	344.84	190.72
AC	4	7 72	0 72.0	72.0	LW	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	508.14	344.30	190.72
AC	4	0 72	0 72.0	72.0	LW	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	509.41	343.84	190.72
AC	4	9 72	0 72.0	72.0	LW	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	570.47	343.38	190.72
AC		0 72	0 72.0	72.0	LW	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	571.64	342.94	190.72
AC		<u>1 72</u>	0 72.0	72.0	LW	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	572.70	342.59	190.72
AC		2 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	5/3./2	342.15	190.72
AC	3	3 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	575.06	341.59	190.72
AC	3	4 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	576.04	341.19	190.72
AC	3	5 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	577.20	340.69	190.72
AC	3	6 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	578.35	340.30	190.72
AC	3	7 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	579.49	339.84	190.72
AC	3	8 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	580.62	339.32	190.72
AC	3	9 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	581.58	338.88	190.72
AC	4	0 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	582.72	338.55	190.72
AC	4	1 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	583.87	338.01	190.72
AC	4	2 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	585.00	337.55	190.72
AC	4	3 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	586.16	337.09	190.72
AC	4	4 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	587.27	336.61	190.72
AC	4	5 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	588.37	336.13	190.72
AC	4	6 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	589.41	335.69	190.72
AC	4	7 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	590.56	335.25	190.72
AC	4	8 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	591.68	334.80	190.72
AC	2	9 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	564.92	345.67	190.72
AC	5	0 72	0 72.0	72.0	Lw	L42		0.0	0.0	0.0							0.0		(none)	190.72 a	565.43	346.90	190.72

Buildings

Name	M.	ID	RB	Residents	Absorption	Height
						Begin
						(m)
	+		х	0		
	+		х	0		

Geometry - Buildings

Name	M.	ID	RB	Residents	Absorption	Heiaht		Coordinat	es	
						Begin	x	V	7	Ground
						(m)	(m)	(m)	 (m)	(m)
	+		x	0		()	546.92	338.60	176.88	172.00
			~				554.93	334.96	176.88	172.00
							554.07	332.44	176.88	172.00
							564.99	328.01	176.88	172.00
							574.39	328.01	176.88	172.00
							575.78	331.25	176.88	172.00
							588.15	327.35	176.88	172.00
							590.07	327.48	176.88	172.00
							590.87	329.66	176.88	172.00
							617.40	336.02	176.88	172.00
							624.29	337.41	176.88	172.00
							622.76	342.37	176.88	172.00
							625.74	342.83	176.88	172.00
							624.62	348.33	176.88	172.00
							601.45	343.63	176.88	172.00
							556.59	361.96	176.88	172.00
	+		х	0			548.49	341.19	189.50	176.88
							550.23	340.56	189.50	176.88
							549.04	337.62	189.50	176.88
							555.59	334.97	189.50	176.88
							556.16	336.51	189.50	176.88
							558.23	335.59	189.50	176.88
							559.26	337.58	189.50	176.88
							561.41	336.55	189.50	176.88
							562.34	338.98	189.50	176.88
							565.47	337.72	189.50	176.88
							566.11	339.08	189.50	176.88
							571.89	336.63	189.50	176.88
							571.36	335.26	189.50	176.88
							577.64	332.46	189.50	176.88
							578.23	333.88	189.50	176.88
							583.92	331.47	189.50	176.88
							583.29	330.04	189.50	176.88
							586.71	328.61	189.50	176.88
							587.63	330.76	189.50	176.88
							590.40	329.61	189.50	176.88

Name	M.	ID	RB	Residents	Absorption	Height Coordi		Coordinat	nates			
						Begin	x	У	Z	Ground		
						(m)	(m)	(m)	(m)	(m)		
							590.76	330.18	189.50	176.88		
							591.36	329.81	189.50	176.88		
							607.53	334.00	189.50	176.88		
							607.19	335.49	189.50	176.88		
							610.82	336.69	189.50	176.88		
							609.07	343.17	189.50	176.88		
							606.07	342.41	189.50	176.88		
							605.54	341.09	189.50	176.88		
							595.76	345.13	189.50	176.88		
							595.25	343.79	189.50	176.88		
							592.49	345.10	189.50	176.88		
							593.12	346.33	189.50	176.88		
							586.82	349.04	189.50	176.88		
							586.33	347.73	189.50	176.88		
							583.53	348.71	189.50	176.88		
							584.15	350.17	189.50	176.88		
							577.87	352.72	189.50	176.88		
							577.27	351.46	189.50	176.88		
							574.68	352.73	189.50	176.88		
							575.16	353.90	189.50	176.88		
							568.70	356.60	189.50	176.88		
							568.20	355.37	189.50	176.88		
							565.39	356.42	189.50	176.88		
							565.94	357.69	189.50	176.88		
							559.85	360.44	189.50	176.88		
							559.02	358.82	189.50	176.88		
							556.36	360.21	189.50	176.88		
							551.07	347.40	189.50	176.88		
							552.84	346.59	189.50	176.88		
							551.62	343.78	189.50	176.88		
							549.97	344.55	189.50	176.88		

Terrain Contours

Name	M.	ID	OnlyPts	Hei	ght	C	oordinates	
				Begin	End	x	у	z
				(m)	(m)	(m)	(m)	(m)
North Course		C1				563.50	372.00	173.00
						574.17	404.35	171.00
						780.62	480.39	186.00
						809.63	466.72	189.00
						813.30	433.03	188.00
						790.95	411.69	187.00
						683.23	374.00	177.00
						637.54	357.99	175.00
						615.53	355.99	174.00
						563.84	372.00	171.00
172		C2		172.00		556.00	365.82	172.00
						547.38	345.86	172.00
						545.49	336.20	172.00
						553.90	329.89	172.00
						564.44	327.46	172.00
						577.64	326.32	172.00
						598.23	328.84	172.00
						624.91	336.41	172.00
						626.27	339.42	172.00
						626.02	348.78	172.00
						625.54	351.95	172.00
						605.37	347.96	172.00
						583.31	351.95	172.00
						555.79	367.08	172.00
North Res		C3				426.09	539.36	169.00
						482.39	475.49	170.00
						540.38	425.07	1/1.00
						573.16	417.92	171.00
						630.30	430.53	174.00
						788.30	492.30	189.00
						862.67	528.85	200.00
						599.42	522.13	172.00
Couthoost		04				445.42	523.81	170.00
Southeast		64				538.65	306.85	173.00
						520.65	171.32	175.00
						633.94	170.79	183.00
						776.00	190.90	107.00
						110.30	220.90	107.00
						804.77	269.79	194.00
						855.24	441.32	196.00
	<u> </u>					767.89	377.26	183.00
						/23.41	366.14	182.00
						678.94	337.55	182.00
						620.71	329.61	178.00

Name	Μ.	ID	OnlyPts	Height		C	oordinates	
				Begin	End	х	у	Z
				(m)	(m)	(m)	(m)	(m)
						590.53	301.02	175.00
						536.53	307.38	173.00
West		C5				466.40	173.26	173.00
						326.99	154.58	176.00
						133.56	129.90	176.00
						196.26	293.99	172.00
						302.31	520.11	175.00
						399.03	492.76	166.00
						534.43	410.05	168.00
						502.42	312.67	172.00
						483.74	262.64	171.00
						468.40	179.93	173.00
I-15 E		C6				-217.71	-485.05	159.00
						206.52	336.72	177.00
						471.22	855.55	186.00
I-15 W		C7				-306.65	-442.69	159.00
						117.57	379.08	177.00
						382.28	897.90	186.00
TW N		C8				985.66	349.66	201.00
						873.96	261.25	197.00
						709.84	160.13	188.00
						593.90	127.83	180.00
TW S		C9				1005.78	320.54	201.00
						894.07	232.13	197.00
						729.96	131.01	188.00
						614.01	98.72	180.00

Sound Level Spectra

Name	ID	Туре		Oktave Spectrum (dB)							Source				
			Weight.	31.5	63	125	250	500	1000	2000	4000	8000	А	lin	
Carrier CA13NA030	L42	Lw	А			52.7	62.2	66.2	67.2	65.2	60.2	55.2	72.0	75.7	Manufacturer

210 South Juniper Street, Suite 100 Escondido, California 92025-4230 Phone: (760) 738-5570

Date: 07 Jun 2019

Configuration	
Parameter	Value
General	
Country	(user defined)
Max. Error (dB)	0.00
Max. Search Radius (#(Unit,LEN))	2000.00
Min. Dist Src to Rcvr	0.00
Partition	
Raster Factor	0.50
Max. Length of Section (#(Unit,LEN))	1000.00
Min. Length of Section (#(Unit,LEN))	1.00
Min. Length of Section (%)	0.00
Proj. Line Sources	On
Proj. Area Sources	On
Ref. Time	
Reference Time Day (min)	960.00
Reference Time Night (min)	480.00
Daytime Penalty (dB)	0.00
Recr. Time Penalty (dB)	6.00
Night-time Penalty (dB)	10.00
DTM	
Standard Height (m)	0.00
Model of Terrain	Triangulation
Reflection	-
max. Order of Reflection	0
Search Radius Src	100.00
Search Radius Rcvr	100.00
Max. Distance Source - Rcvr	1000.00 1000.00
Min. Distance Rvcr - Reflector	1.00 1.00
Min. Distance Source - Reflector	0.10
Industrial (ISO 9613)	
Lateral Diffraction	some Obj
Obst. within Area Src do not shield	On
Screening	Excl. Ground Att. over Barrier
	Dz with limit (20/25)
Barrier Coefficients C1,2,3	3.0 20.0 0.0
Temperature (#(Unit,TEMP))	10
rel. Humidity (%)	70
Ground Absorption G	0.50
Wind Speed for Dir. (#(Unit,SPEED))	3.0
Roads (TNM)	
Railways (Schall 03 (1990))	
Strictly acc. to Schall 03 / Schall-Transrapid	
Aircraft (???)	
Strictly acc. to AzB	
Receivers

Name	M.	ID	Lev	el Lr	Limit.	Value		Land	Height		Coordinates			
			Day	Night	Day	Night	Type Auto Noise Type				Х	Y	Z	
			(dBA)	(dBA)	(dBA)	(dBA)				(m)		(m)	(m)	(m)
North		R1	45.6	-71.3	0.0	0.0		х	Total	1.52	r	584.93	353.45	173.63
South		R2	44.4	-72.3	0.0	0.0		х	Total	1.52	r	584.28	296.01	176.39
Southeast		R3	44.7	-73.0	0.0	0.0		х	Total	1.52	r	592.35	327.63	173.57
Southeast Res1		R4	43.9	-73.9	0.0	0.0		х	Total	1.52	r	621.86	332.54	176.73
Southeast Res2		R5	42.8	-73.5	0.0	0.0		х	Total	4.57	r	621.86	332.54	179.78
West		R6	50.4	-65.5	0.0	0.0		х	Total	1.52	r	520.71	359.53	171.71

Roads

Name	M.	ID		Lme		Cou	Int Data exact Count Data			nt Data	1		Speed Limit		SCS	Surf	ace	Gradient	Mul	t. Reflee	ction	
			Day	Evening	Night	DTV	Str.class.		М			p (%)		Auto	Truck	Dist.	Dstro	Туре		Drefl	Hbuild	Dist.
			(dBA)	(dBA)	(dBA)			Day	Evening	Night	Day	Evening	Night	(km/h)	(km/h)		(dB)		(%)	(dB)	(m)	(m)
Rancho Carmel Dr		RO_1	47.5	0.0	0.0			15.0	0.0	0.0	2.0	0.0	0.0	72		15.24	0.0	1	0.0	0.0		
Ted Williams		RO_2	53.8	0.0	0.0			44.0	0.0	0.0	5.0	0.0	0.0	89		24.38	0.0	1	0.0	0.0		
I-15 NB		RO_3	60.8	0.0	0.0			119.0	0.0	0.0	7.1	0.0	0.0	105		33.53	0.0	1	0.0	0.0		
I-15 SB		RO_4	60.8	0.0	0.0			119.0	0.0	0.0	7.1	0.0	0.0	105		33.53	0.0	1	0.0	0.0		

Geometry - Roads

Name	He	eight		Coordinat	es		Dist	LSlope
	Begin	End	x	у	Z	Ground	(m)	(%)
	(m)	(m)	(m)	(m)	(m)	(m)		
Rancho Carmel Dr			497.74	135.08	175.00	175.00		
			501.94	213.20	175.00	175.00		
			505.30	257.30	173.00	173.00		
			526.11	329.14	172.00	172.00		
			598.26	519.95	174.00	172.00		
Ted Williams			996.59	337.98	201.00	201.00		
			880.67	245.58	197.00	197.00		
			713.51	145.61	188.00	188.00		
			595.06	111.17	186.00	180.00		
			500.98	112.85	180.00	180.00		
			401.02	112.85	180.00	180.00		
			236.38	108.65	176.00	176.00		
			83.49	96.05	176.00	176.00		
I-15 NB			-242.64	-478.34	159.00	159.00		
			185.32	347.46	177.00	177.00		
			445.68	859.53	186.00	186.00		
I-15 SB			411.71	892.06	186.00	186.00		
			146.48	366.07	177.00	177.00		
			-281.96	-465.76	159.00	159.00		

Terrain Contours

Name	Μ.	ID	OnlyPts	Hei	ght	Coordinates				
				Begin	End	x	у	z		
				(m)	(m)	(m)	(m)	(m)		
North Course		C1				563.50	372.00	173.00		
						574.17	404.35	171.00		
						780.62	480.39	186.00		
						809.63	466.72	189.00		
						813.30	433.03	188.00		
						790.95	411.69	187.00		
						683.23	374.00	177.00		
						637.54	357.99	175.00		
						615.53	355.99	174.00		
						563.84	372.00	171.00		
172		C2		172.00		556.00	365.82	172.00		
						547.38	345.86	172.00		
						545.49	336.20	172.00		
						553.90	329.89	172.00		
						564.44	327.46	172.00		
						577.64	326.32	172.00		
						598.23	328.84	172.00		
						624.91	336.41	172.00		
						626.27	339.42	172.00		
						626.02	348.78	172.00		
						625.54	351.95	172.00		
						605.37	347.96	172.00		
						583.31	351.95	172.00		
						555.79	367.08	172.00		
North Res		C3				426.09	539.36	169.00		
						482.39	475.49	170.00		
						540.38	425.07	171.00		
						573.16	417.92	171.00		
						630.30	430.53	174.00		
						788.30	492.30	189.00		
						862.67	528.85	200.00		
						599.42	522.13	172.00		
O south a set		04				445.42	523.81	170.00		
Southeast		64				538.65	306.85	173.00		
						520.65	171.32	175.00		
						633.94	170.79	183.00		
	-					726.06	190.90	187.00		
	<u> </u>					//0.30	226.90	101.00		
	-					864.77	269.79	194.00		
	-					855.24	441.32	196.00		
						767.89	377.26	183.00		
	-					/23.41	366.14	182.00		
	-					678.94	337.55	182.00		
						620.71	329.61	178.00		

Name	Μ.	ID	OnlyPts	Hei	ght	C	oordinates	
				Begin	End	х	у	Z
				(m)	(m)	(m)	(m)	(m)
						590.53	301.02	175.00
						536.53	307.38	173.00
West		C5				466.40	173.26	173.00
						326.99	154.58	176.00
						133.56	129.90	176.00
						196.26	293.99	172.00
						302.31	520.11	175.00
						399.03	492.76	166.00
						534.43	410.05	168.00
						502.42	312.67	172.00
						483.74	262.64	171.00
						468.40	179.93	173.00
I-15 E		C6				-217.71	-485.05	159.00
						206.52	336.72	177.00
						471.22	855.55	186.00
I-15 W		C7				-306.65	-442.69	159.00
						117.57	379.08	177.00
						382.28	897.90	186.00
TW N		C8				985.66	349.66	201.00
						873.96	261.25	197.00
						709.84	160.13	188.00
						593.90	127.83	180.00
TW S		C9				1005.78	320.54	201.00
						894.07	232.13	197.00
						729.96	131.01	188.00
						614.01	98.72	180.00

APPENDIX D

Manufacturer Data Sheets

CA13NA 018–060 Base Series Air Conditioner with Puron[®] Refrigerant



Product Data



Carrier's CA13 has been designed utilizing Carrier's Puron refrigerant. The environmentally sound refrigerant allows you to make a responsible decision in the protection of the earth's ozone layer.

This product has been designed and manufactured to meet Energy Star[®] criteria for energy efficiency when matched with appropriate coil components. Refer to the combination ratings in the Product Data for system combinations that meet Energy Star[®] guidelines.

INDUSTRY LEADING FEATURES / BENEFITS

Efficiency

- 13.0 SEER / 10.9 11 EER (based on tested combination)
- Microtube Technology[™] refrigeration system
- Energy Star[®] combinations

Reliability

- Puron[®] refrigerant environmentally sound, won't deplete the ozone layer and low lifetime servce cost.
- Scroll compressor
- Internal pressure relief valve
- Internal thermal overload
- Filter drier

Durability

WeatherArmor[™] protection package:

- Solid, durable sheet metal construction
- Dense wire coil guard

Applications

- Long-line up to 250 feet (76.20 m) total equivalent length, up to 200 feet (60.96 m) condenser above evaporator, or up to 80 ft. (24.38 m) evaporator above condenser (See Longline Guide for more information.)
- Low ambient (down to -20°F/-28.9°C)) with accessory kit

NOTE: Ratings contained in this document are subject to change at any time. Always refer to the AHRI directory (www.ahridirectory.org) for the most up-to-date ratings information.

PRODUCT NUMBER NOMENCLATURE



A-WEIGHTED SOUND POWER (dBA)

	Standard		TYPICAL OCTAVE BAND SPECTRUM (dBA without tone adjustment)										
UNIT SIZE - SERIES	Rating (dBA)	125	250	500	1000	2000	4000	8000					
018–A	71	49.5	59.0	63.0	66.5	62.5	58.5	54.0					
024–A	73	50.5	61.0	67.0	68.0	65.0	60.0	55.5					
030–A	72	52.0	61.5	65.5	66.5	64.5	59.5	54.5					
036–C	74	53.5	63.5	68.5	69.5	67.0	65.0	58.5					
042–A	75	56.0	64.5	69.5	71.0	66.0	64.0	59.0					
048–C	76	54.0	63.0	69.5	71.5	70.0	66.0	58.5					
060-C	79	57.5	67.0	72.0	75.0	72.5	68.0	61.0					

NOTE: Tested in compliance with AHRI 270-2008 (not listed with AHRI)

A-WEIGHTED SOUND POWER (dBA) WITH SOUND SHIELD

UNIT SIZE – SERIES	Standard		TYPICAL OCTAVE BAND SPECTRUM (dBA without tone adjustment)										
	Rating (dBA)	125	250	500	1000	2000	4000	8000					
018–A	70	53.5	60.0	62.0	65.5	62.0	57.5	52.5					
024–A	73	53.0	62.0	67.5	68.0	65.0	60.0	53.5					
030–A	71	54.0	61.5	65.5	66.0	63.5	58.5	52.0					
036–C	74	54.0	63.5	68.0	69.0	66.5	64.0	58.5					
042–A	74	55.5	64.0	69.0	69.5	65.5	63.5	57.5					
048–C	76	55.0	63.0	69.5	71.0	68.5	65.0	58.0					
060–C	79	57.5	68.0	72.5	74.5	72.5	68.0	60.5					

NOTE: Tested in compliance with AHRI 270–2008 (not listed with AHRI)

METERING DEVICE

UNIT SIZE – SERIES	INDOOOR	REQUIRED SUBCOOLING °F (°C)
18–A		10 (5.6)
24–A		10 (5.6)
30–A		10 (5.6)
36–C	TXV*	12 (6.7)
42–A		10 (5.6)
48–C		15 (8.3)
60-C		15 (8.3)

* TXV must be ordered separately when indoor coil is not equipped with a TXV. TXV must be hard-shutoff type.

APPENDIX E

Construction Noise and Vibration Calculations

Job:	Alante
Job #:	S190506
Date:	5/30/2019
Source:	Backhoe
Receiver:	Southeast

Noise Source]
Noise Level (dBA)	64	at	50	feet	
Distances					-
Source Elevation	0	feet	at	5	feet above grade
Receiver Elevation:	0	feet	at	5	feet above grade
Source to Receiver Distance:	75	feet	-		
Path Calculation					
Source to Receiver Direct Path	Distance:	75	feet		
Sound Pressure Level	60.5	at	75	feet	1
Hours of Use:	12	2.14			
Duty Cycle (%):	40				
Level During 12 Hour day:	56.5				

Summation	
Number of Sources:	2
Level during 12 hour day:	69.7

Job: Job #: Date:	Alante S190506 5/30/2019	
Source:	Concrete Saw	
Receiver:	Southeast	
	Noise Source	
	Noise Level (dBA) 80	

Noise Level (dBA)	80	at	50	feet	
					1
Distances					
Source Elevation	0	feet	at	5	feet above grade
Receiver Elevation:	0	feet	at	5	feet above grade
Source to Receiver Distance:	75	feet			
Path Calculation					
Source to Receiver Direct Path	Distance:	75	feet		
Cound Drocours Lough	70 E	-	75	fact	1
Sound Pressure Level	/6.5	at	/5	teet	
Hours of Use:	12				
Duty Cycle (%):	20				
Level During 12 Hour day:	69.5				

Job:	Alante
Job #:	S190506
Date:	5/30/2019
Source:	Drill Rig
Receiver:	Southeast

Noise Source					7
Noise Level (dBA)	79	at	50	feet	
Distances					
Source Elevation	0	feet	at	5	feet above grade
Receiver Elevation:	0	feet	at	5	feet above grade
Source to Receiver Distance:	75	feet	-		
Path Calculation					
Source to Receiver Direct Path	Distance:	75	feet		
Sound Prossuro Loval	75 5	at	75	foot	Г
Hours of Use	12	aı	15	1661	
Duty Cycle (%):	20				
Level During 12 Hour day:	68.5				

Summation	
Number of Sources:	2
Level during 12 hour day:	71.0

Job:	Alante
Job #:	S190506
Date:	5/30/2019
Source:	Dump Truck
Receiver:	Southeast

				٦
Noise Source				
Noise Level (dBA) 75	at	50	feet	
Distances				
Source Elevation 0	feet	at	5	feet above grade
Receiver Elevation: 0	feet	at	5	feet above grade
Source to Receiver Distance: 75	feet			
			1	
Path Calculation				
Source to Receiver Direct Path Distance	e: 75	feet		
Sound Pressure Level 71.5	at	75	feet	1
Hours of Use: 12				
Duty Cycle (%): 40	_			
Level During 12 Hour day: 67.5	_			

Job:	Alante
Job #:	S190506
Date:	5/30/2019
Source:	Concrete Saw
Receiver:	Southeast

Noise Source					7
Noise Level (dBA)	80	at	50	feet	
Distances					
Source Elevation	0	feet	at	5	feet above grade
Receiver Elevation:	0	feet	at	5	feet above grade
Source to Receiver Distance:	75	feet	-		
Path Calculation					
Source to Receiver Direct Path	n Distance:	75	feet		
Sound Pressure Level	76.5	at	75	feet	7
Hours of Use:	12	-			
Duty Cycle (%):	20	-			
Level During 12 Hour day:	69.5	-			

Summation	
Number of Sources:	4
Level during 12 hour day:	72 0
Level during 12 hour day.	12.9

Job:	Alante
Job #:	S190506
Date:	5/30/2019
Source:	Concrete Mixer Truck
Receiver:	Southeast

					7
Noise Source					
Noise Level (dBA)	71	at	50	feet	
Distances					
Source Elevation	0	feet	at	5	feet above grade
Receiver Elevation:	0	feet	at	5	feet above grade
Source to Receiver Distance:	75	feet	-		-
			1		
Path Calculation					
Source to Receiver Direct Path D	Distance:	75	feet		
Sound Pressure Level	67.5	at	75	feet	1
Hours of Use:	12				
Duty Cycle (%):	40				
Level During 12 Hour day:	63.5				

Job:	Alante
Job #:	S190506
Date:	5/30/2019
Source:	Concrete Pump Truck
Receiver:	Southeast

Noise Source]
Noise Level (dBA) 71	at	50	feet	
Distances				
Source Elevation 0	feet	at	5	feet above grade
Receiver Elevation: 0	feet	at	5	feet above grade
Source to Receiver Distance: 75	feet	-		-
Path Calculation				
Source to Receiver Direct Path Distance:	75	feet		
Sound Pressure Level 67.5 Hours of Use: 12	at	75	feet]
Duty Cycle (%): 20				
Level During 12 Hour day: <u>60.5</u>				

Noise Attenuation by Distance Calculation

Job: Alante Job #: S190506 Date: 5/30/2019 Source: Jackhammer Receiver: Southeast

Noise Source]
Noise Level (dBA)	79	at	50	feet	
Distances					
Source Elevation	0	feet	at	5	feet above grade
Receiver Elevation:	0	feet	at	5	feet above grade
Source to Receiver Distance:	75	feet			_
Path Calculation					
Source to Receiver Direct Path D	istance:	75	feet		
Sound Pressure Level	75 5	at	75	feet	7
Hours of Use:	12	<u> </u>	.0		
Duty Cycle (%):	20	-			
Level During 12 Hour day:	68.5				

Job:	Alante
Job #:	S190506
Date:	5/30/2019
Source:	Crane
Receiver:	Southeast

Noise Source					7
Noise Level (dBA)	66	at	50	feet	
Distances					
Source Elevation	0	feet	at	5	feet above grade
Receiver Elevation:	0	feet	at	5	feet above grade
Source to Receiver Distance:	75	feet	-		_ 0
Path Calculation					
Source to Receiver Direct Path	Distance:	75	feet		
Sound Pressure Level	62.5	at	75	feet	7
Hours of Use:	12				
Duty Cycle (%):	16				
Level During 12 Hour day:	54.5				

Summation	
Number of Sources:	3
Level during 12 hour day:	65.6
_	

Job:	Alante
Job #:	S190506
Date:	5/30/2019
Source:	Concrete Mixer Truck
Receiver:	Southeast

Noise Source					
Noise Level (dBA)	71	at	50	feet	
Distances					
Source Elevation	0	feet	at	5	feet above grade
Receiver Elevation:	0	feet	at	5	feet above grade
Source to Receiver Distance:	75	feet	•		-
Path Calculation					
Source to Receiver Direct Path I	Distance:	75	feet		
Sound Pressure Level	67.5	at	75	feet]
Hours of Use:	12				
Duty Cycle (%):	40				
Level During 12 Hour day:	63.5				

Job:	Alante
Job #:	S190506
Date:	5/30/2019
Source:	Concrete Pump Truck
Receiver:	Southeast

Noise Source				1
Noise Level (dBA) 71	at	50	feet	
Distances				
Source Elevation 0	feet	at	5	feet above grade
Receiver Elevation: 0	feet	at	5	feet above grade
Source to Receiver Distance: 75	feet	-		-
Path Calculation				
Source to Receiver Direct Path Distance:	75	feet		
Sound Pressure Level 67.5	at	75	feet]
Hours of Use: 12				
Duty Cycle (%): 20				
Level During 12 Hour day: 60.5				

Construction Vibration Calculation

Job:AlanteJob #:\$190506Date:6/7/2019Source 1:Caisson DrillingReceiver:Southeast

/ibration Source				
Vibration Level (PPV, in/sec	c) <u>0.089</u>	at	25	feet
ath Calculation				
Source to Receiver Direct	t Path Distance:	25	feet	
/ibration Level (PPV, in/sec)	0.089	at	25	feet

Path Calculation				
Source to Receiver Direc	t Path Distance:	45	feet	
Vibration Level (PPV, in/sec)	0.037	at	45	feet

Path Calculation				
Source to Receiver Direct	Path Distance:	100	feet	
Vibration Level (PPV, in/sec)	0.011	at	100	feet