

HYDROLOGY & HYDRAULIC REPORT

DATED: 10/22/20

For

Superstar Car Wash

Prepared for:

Reza Amirrezvani

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Project Location:

6270 Miramar Road, San Diego, CA 92121

APN 343-252-34

Prepared By:

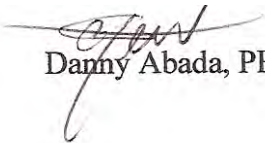
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Danny Abada, PE



DECLARATION OF RESPONSIBLE CHARGE

I, HEREBY DECLARE THAT I AM THE CIVIL ENGINEER OF WORK FOR THIS PROJECT, THAT I HAVE EXERCISED RESPONSIBLE CHARGE OVER THE DESIGN OF THIS PROJECT AS DEFINED IN SECTION 6703 OF THE BUSINESS AND PROFESSIONAL CODE AND THAT THE DESIGN IS CONSISTENT WITH CURRENT DESIGN STANDARDS.

I UNDERSTAND THAT THE CHECK OF PROJECT DRAWINGS AND SPECIFICATIONS BY THE CITY OF SAN DIEGO IS CONFINED TO A REVIEW ONLY AND DOES NOT RELIEVE ME, AS ENGINEER OF WORK, OF MY RESPONSIBILITIES FOR PROJECT DESIGN.



10/22/20

Danny Abada
REGISTERED CIVIL ENGINEER
Spear & Associates Inc.

DATE



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I. INTRODUCTION

This hydrology report was prepared for Superstar Car Wash located at 6270 Miramar Road, San Diego, CA 92121. The site encompasses approximately 0.71 acres.

The site is currently developed with a commercial building and parking lot. The project will re-develop the site with a car wash facility, parking lot and landscaping. The runoff will be directed to a biofiltration basin for treatment.

The existing topography slopes in a southerly direction with elevations ranging from approximately 405 to 400. The site drains south towards Miramar Road then continues west, then north to Miramar Mall, then northwest to Carrol Canyon Creek, Los Penasquitos Creek, Los Penasquitos Lagoon and The Pacific Ocean approximately 6.2 miles west.

The development will maintain existing drainage patterns; post development runoff will be directed to biofiltration/Detention basin for stormwater treatment. The outlet flows will be directed to the same drainage system as in pre-development.

We have used the County of San Diego Hydrology Manual to determine the run-off from the site for the 100yr, flow. Based on the soil hydrologic group map of the County Hydrology Manual, the project soil uniformly consists of type D across all sub areas. Peak flow rates were calculated using the rational method. Times of concentrations were calculated using the Manning's equation to obtain velocities using average overland flow rates.

The existing site's impervious area of 24,516 square feet will be reduced to 22,560 square feet. Water quality will be addressed with biofiltration basins to treat the projects anticipated and expected pollutants. Refer to the Storm Water Quality Management Plan for more detailed information.

II. DISCUSSION/CONCLUSION

Post development peak flows, flow volumes and velocities for the 100yr event will not exceed pre-development rates with reduced site imperviousness, the use of a detention basin, an efficient site design and maximizing onsite times of concentration. No increased negative impact to any adjacent properties is anticipated from this development.

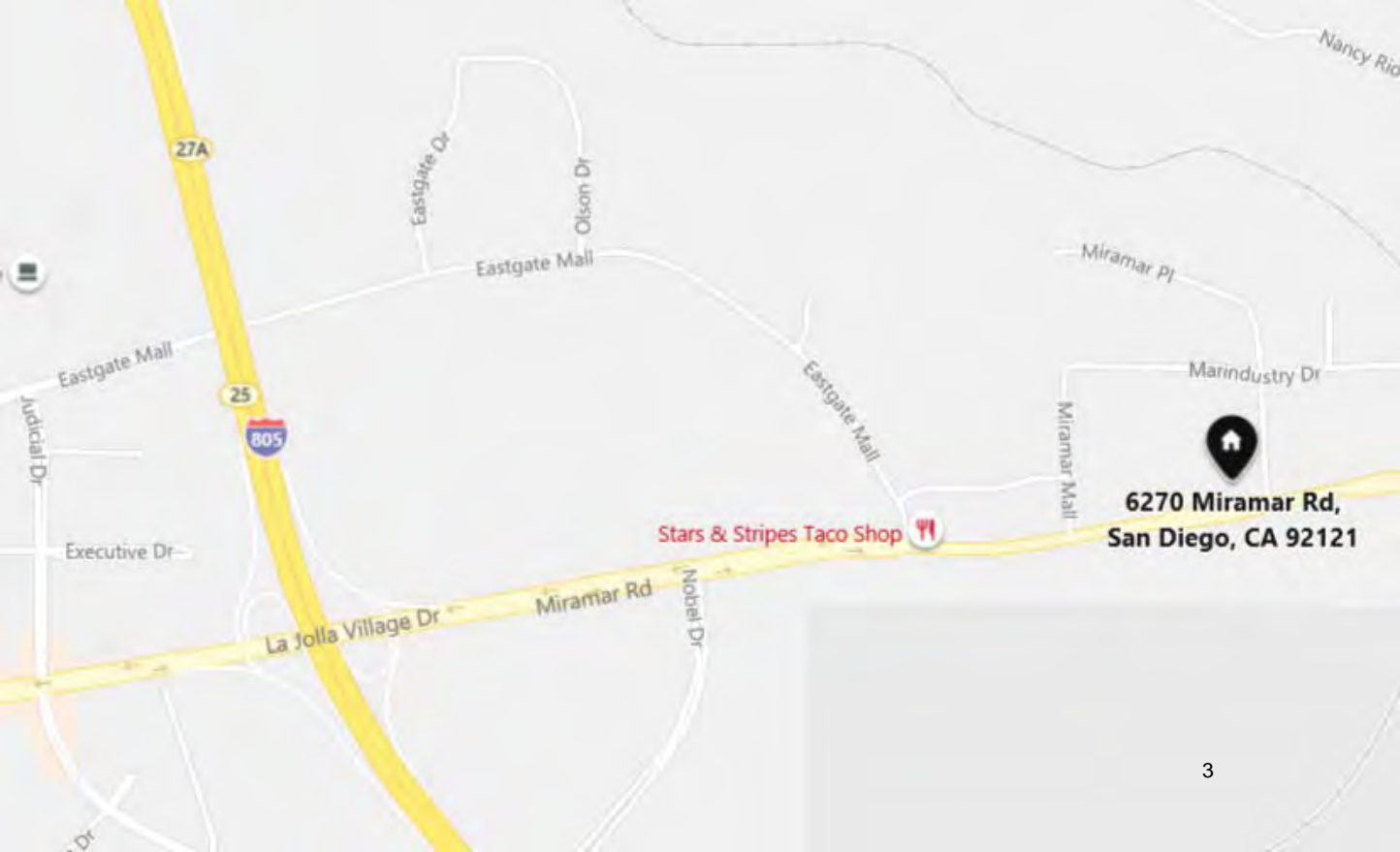
No increased peak runoff flow into the existing stormdrain system is anticipated as a result of this development.

The project will not conduct activities that would trigger a Clean Water Act Section 401 or 404 Certification.

Summary of flow rates

<i>Storm Event</i>	<i>100-yr cfs</i>
Pre-Development	2.9
Post-Development	2.4

ATTACHMENT A





6270 Miramar Rd.

Miramar Rd

Miramar Pl

ATTACHMENT B

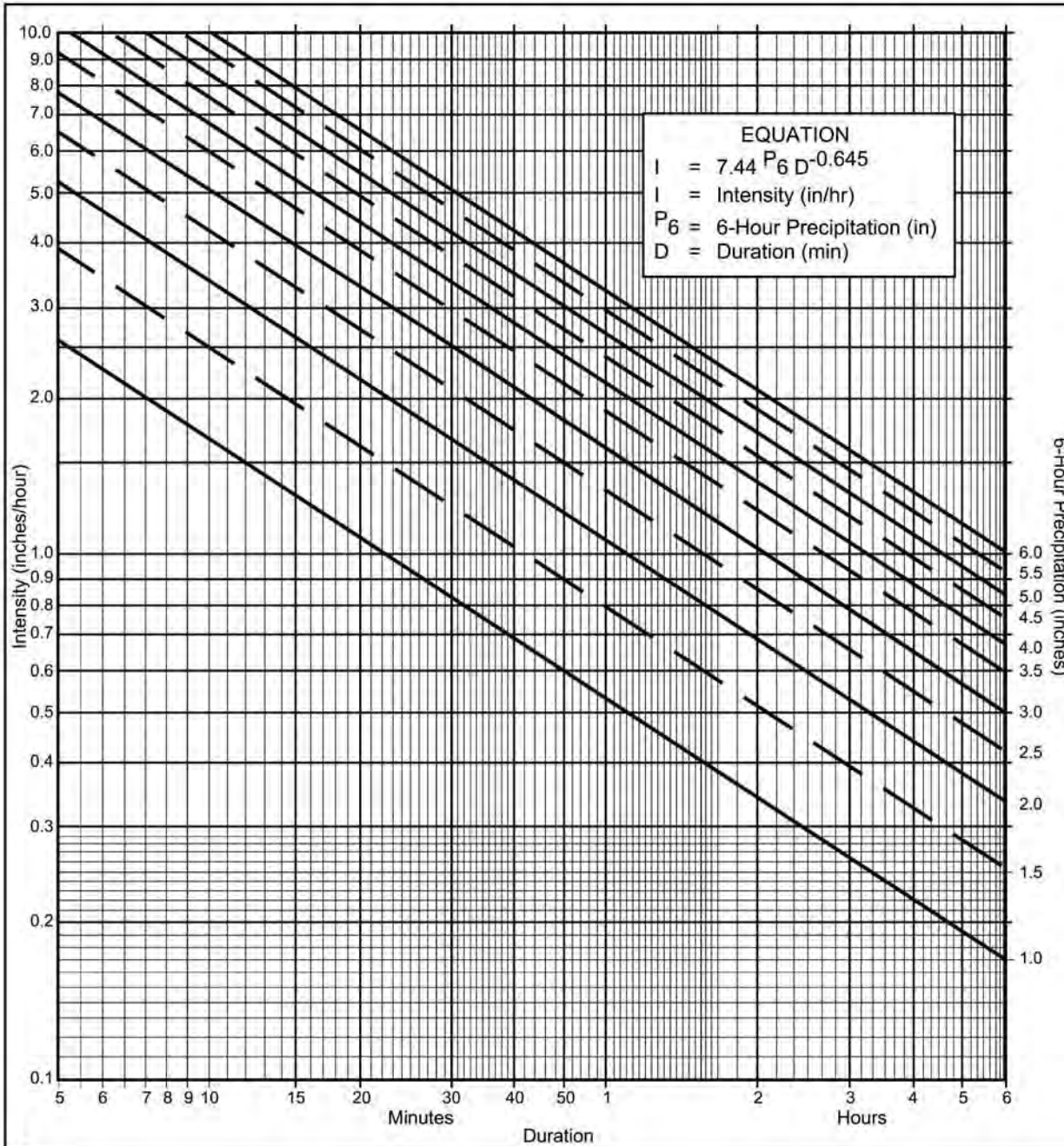
Post-Development

Rational Method, 100yr Event

REACH	TC	C	A	CA	ΣCA	P_6	I	Q cfs
Site	7.8	0.75	0.71	0.53	0.53	2.32	4.59	2.4

Pre-Development

REACH	TC	C	A	CA	ΣCA	P_6	I	Q cfs
Site	6.4	0.78	0.71	0.55	0.55	2.32	5.21	2.9



Directions for Application:

- (1) From precipitation maps determine 6 hr and 24 hr amounts for the selected frequency. These maps are included in the County Hydrology Manual (10, 50, and 100 yr maps included in the Design and Procedure Manual).
- (2) Adjust 6 hr precipitation (if necessary) so that it is within the range of 45% to 65% of the 24 hr precipitation (not applicable to Desert).
- (3) Plot 6 hr precipitation on the right side of the chart.
- (4) Draw a line through the point parallel to the plotted lines.
- (5) This line is the intensity-duration curve for the location being analyzed.

Application Form:

- (a) Selected frequency 100 year
- (b) $P_6 = 2.32$ in., $P_{24} = 3.93$, $\frac{P_6}{P_{24}} = 59$ %⁽²⁾
- (c) Adjusted $P_6^{(2)} =$ _____ in.
- (d) $t_x =$ _____ min.
- (e) $I =$ _____ in./hr.

Note: This chart replaces the Intensity-Duration-Frequency curves used since 1965.

P6	1	1.5	2	2.5	3	3.5	4	4.5	5	5.5	6
5	2.63	3.95	5.27	6.59	7.90	9.22	10.54	11.86	13.17	14.49	15.81
7	2.12	3.18	4.24	5.30	6.36	7.42	8.48	9.54	10.60	11.66	12.72
10	1.68	2.53	3.37	4.21	5.05	5.90	6.74	7.58	8.42	9.27	10.11
15	1.30	1.95	2.59	3.24	3.89	4.54	5.19	5.84	6.49	7.13	7.78
20	1.08	1.62	2.15	2.69	3.23	3.77	4.31	4.85	5.39	5.93	6.46
25	0.93	1.40	1.87	2.33	2.80	3.27	3.73	4.20	4.67	5.13	5.60
30	0.83	1.24	1.66	2.07	2.49	2.90	3.32	3.73	4.15	4.56	4.98
40	0.69	1.03	1.38	1.72	2.07	2.41	2.76	3.10	3.45	3.79	4.13
50	0.60	0.90	1.19	1.49	1.79	2.09	2.39	2.69	2.98	3.28	3.58
60	0.53	0.80	1.06	1.33	1.59	1.86	2.12	2.39	2.65	2.92	3.18
90	0.41	0.61	0.82	1.02	1.23	1.43	1.63	1.84	2.04	2.25	2.45
120	0.34	0.51	0.68	0.85	1.02	1.19	1.36	1.53	1.70	1.87	2.04
150	0.29	0.44	0.59	0.73	0.88	1.03	1.18	1.32	1.47	1.62	1.76
180	0.26	0.39	0.52	0.65	0.78	0.91	1.04	1.18	1.31	1.44	1.57
240	0.22	0.33	0.43	0.54	0.65	0.76	0.87	0.98	1.08	1.19	1.30
300	0.19	0.28	0.38	0.47	0.56	0.66	0.75	0.85	0.94	1.03	1.13
360	0.17	0.25	0.33	0.42	0.50	0.58	0.67	0.75	0.84	0.92	1.00

Intensity-Duration Design Chart - Template

FIGURE

3-1



NOAA Atlas 14, Volume 6, Version 2
 Location name: San Diego, California, USA*
 Latitude: 32.8781°, Longitude: -117.1792°
 Elevation: 406.24 ft**
 * source: ESRI Maps
 ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

[PF_tabular](#) | [PF_graphical](#) | [Maps_&_aerials](#)

PF tabular

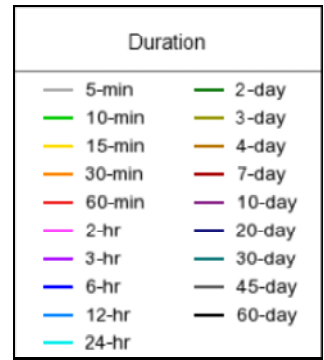
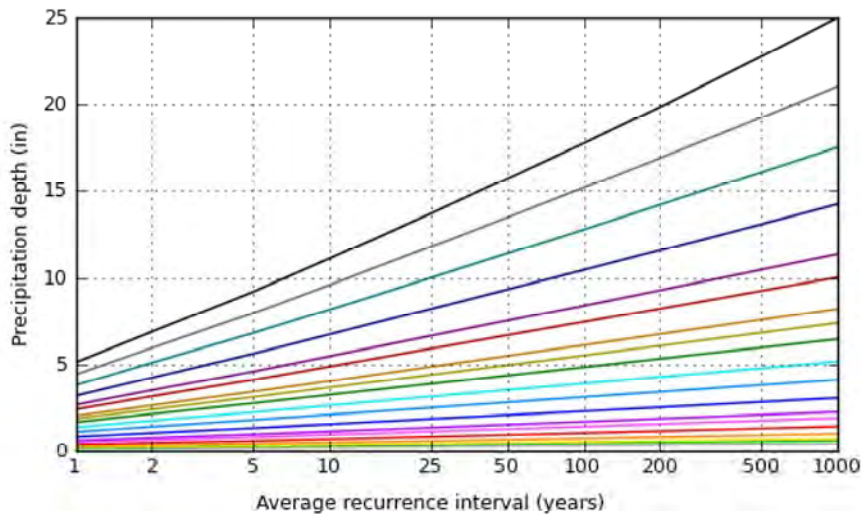
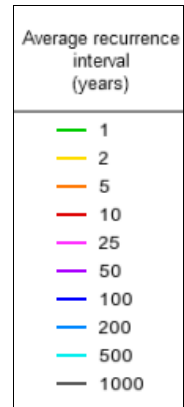
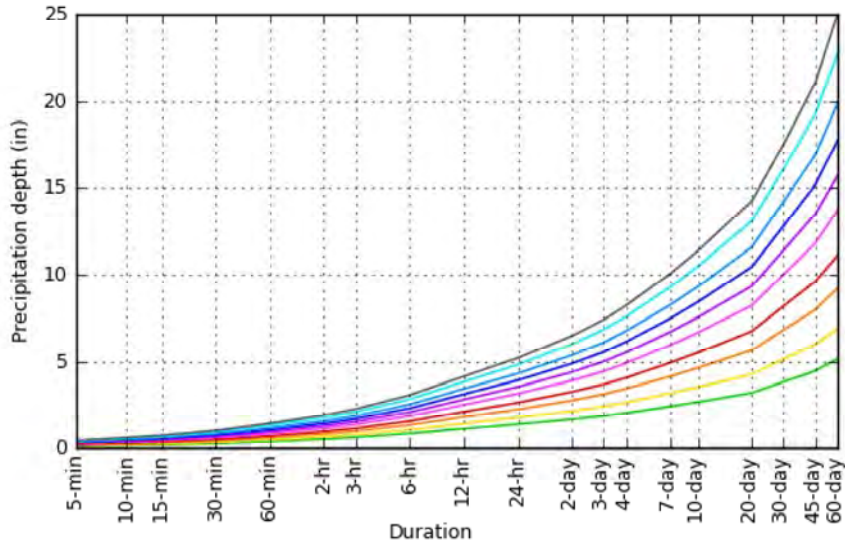
PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)¹										
Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	0.110 (0.092-0.132)	0.139 (0.116-0.167)	0.176 (0.147-0.213)	0.207 (0.171-0.252)	0.248 (0.198-0.313)	0.279 (0.219-0.361)	0.311 (0.237-0.412)	0.344 (0.255-0.469)	0.388 (0.275-0.553)	0.422 (0.289-0.624)
10-min	0.158 (0.132-0.190)	0.199 (0.167-0.240)	0.253 (0.211-0.305)	0.296 (0.246-0.361)	0.355 (0.284-0.449)	0.400 (0.313-0.517)	0.446 (0.340-0.591)	0.493 (0.365-0.673)	0.556 (0.394-0.793)	0.605 (0.414-0.895)
15-min	0.191 (0.160-0.229)	0.241 (0.202-0.290)	0.306 (0.255-0.369)	0.358 (0.297-0.437)	0.430 (0.344-0.543)	0.484 (0.379-0.625)	0.540 (0.411-0.715)	0.596 (0.441-0.814)	0.673 (0.477-0.959)	0.732 (0.500-1.08)
30-min	0.263 (0.221-0.317)	0.332 (0.279-0.401)	0.422 (0.353-0.511)	0.495 (0.410-0.604)	0.594 (0.475-0.750)	0.669 (0.524-0.864)	0.746 (0.569-0.988)	0.824 (0.610-1.13)	0.930 (0.659-1.33)	1.01 (0.691-1.50)
60-min	0.373 (0.313-0.449)	0.471 (0.395-0.568)	0.598 (0.500-0.723)	0.702 (0.581-0.856)	0.841 (0.673-1.06)	0.948 (0.742-1.22)	1.06 (0.805-1.40)	1.17 (0.864-1.59)	1.32 (0.933-1.88)	1.43 (0.979-2.12)
2-hr	0.514 (0.431-0.619)	0.646 (0.542-0.779)	0.818 (0.683-0.989)	0.956 (0.792-1.17)	1.14 (0.913-1.44)	1.28 (1.00-1.66)	1.43 (1.09-1.89)	1.57 (1.16-2.14)	1.77 (1.25-2.52)	1.91 (1.31-2.83)
3-hr	0.617 (0.518-0.743)	0.776 (0.650-0.935)	0.980 (0.819-1.19)	1.15 (0.949-1.40)	1.37 (1.09-1.73)	1.53 (1.20-1.98)	1.70 (1.30-2.26)	1.87 (1.39-2.56)	2.10 (1.49-3.00)	2.28 (1.56-3.36)
6-hr	0.840 (0.704-1.01)	1.06 (0.886-1.27)	1.34 (1.12-1.62)	1.56 (1.30-1.91)	1.86 (1.49-2.35)	2.09 (1.63-2.70)	2.32 (1.77-3.07)	2.54 (1.88-3.47)	2.85 (2.02-4.06)	3.08 (2.10-4.55)
12-hr	1.12 (0.940-1.35)	1.42 (1.19-1.71)	1.81 (1.51-2.18)	2.11 (1.75-2.58)	2.52 (2.02-3.18)	2.83 (2.21-3.65)	3.13 (2.38-4.14)	3.43 (2.54-4.69)	3.84 (2.72-5.47)	4.14 (2.83-6.12)
24-hr	1.38 (1.21-1.60)	1.77 (1.55-2.05)	2.26 (1.98-2.63)	2.65 (2.30-3.11)	3.16 (2.67-3.82)	3.55 (2.93-4.37)	3.93 (3.17-4.95)	4.31 (3.40-5.58)	4.81 (3.65-6.48)	5.19 (3.81-7.22)
2-day	1.67 (1.47-1.94)	2.16 (1.89-2.51)	2.77 (2.43-3.23)	3.26 (2.84-3.83)	3.91 (3.30-4.73)	4.39 (3.63-5.42)	4.87 (3.94-6.15)	5.36 (4.22-6.94)	5.99 (4.54-8.07)	6.48 (4.75-9.00)
3-day	1.87 (1.64-2.17)	2.42 (2.13-2.81)	3.13 (2.74-3.64)	3.69 (3.21-4.33)	4.43 (3.74-5.36)	4.99 (4.13-6.16)	5.54 (4.48-6.99)	6.10 (4.81-7.90)	6.84 (5.18-9.20)	7.40 (5.43-10.3)
4-day	2.04 (1.80-2.37)	2.66 (2.33-3.09)	3.44 (3.02-4.01)	4.07 (3.54-4.77)	4.90 (4.13-5.93)	5.52 (4.56-6.81)	6.14 (4.96-7.74)	6.76 (5.33-8.75)	7.58 (5.75-10.2)	8.21 (6.03-11.4)
7-day	2.42 (2.13-2.81)	3.17 (2.79-3.69)	4.14 (3.63-4.82)	4.91 (4.27-5.76)	5.93 (5.00-7.18)	6.69 (5.54-8.26)	7.46 (6.03-9.41)	8.23 (6.48-10.7)	9.25 (7.01-12.4)	10.0 (7.36-13.9)
10-day	2.68 (2.35-3.11)	3.53 (3.10-4.10)	4.62 (4.05-5.39)	5.50 (4.78-6.45)	6.66 (5.61-8.06)	7.53 (6.23-9.29)	8.40 (6.79-10.6)	9.28 (7.31-12.0)	10.5 (7.92-14.1)	11.3 (8.32-15.8)
20-day	3.20 (2.81-3.72)	4.27 (3.75-4.96)	5.64 (4.94-6.57)	6.74 (5.86-7.91)	8.21 (6.92-9.94)	9.32 (7.71-11.5)	10.4 (8.44-13.2)	11.6 (9.11-15.0)	13.1 (9.91-17.6)	14.2 (10.4-19.8)
30-day	3.83 (3.37-4.45)	5.13 (4.51-5.96)	6.82 (5.97-7.94)	8.17 (7.11-9.59)	9.99 (8.43-12.1)	11.4 (9.41-14.0)	12.8 (10.3-16.1)	14.2 (11.2-18.4)	16.1 (12.2-21.6)	17.5 (12.9-24.3)
45-day	4.45 (3.91-5.16)	5.97 (5.24-6.94)	7.96 (6.98-9.28)	9.58 (8.33-11.2)	11.8 (9.93-14.2)	13.5 (11.1-16.6)	15.2 (12.3-19.1)	16.9 (13.3-21.9)	19.2 (14.6-25.9)	21.0 (15.4-29.2)
60-day	5.15 (4.52-5.97)	6.89 (6.05-8.01)	9.20 (8.06-10.7)	11.1 (9.64-13.0)	13.7 (11.5-16.6)	15.7 (13.0-19.4)	17.7 (14.3-22.4)	19.9 (15.6-25.7)	22.7 (17.2-30.6)	25.0 (18.3-34.7)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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PF graphical

PDS-based depth-duration-frequency (DDF) curves
Latitude: 32.8781°, Longitude: -117.1792°



Maps & aerals

Small scale terrain



Large scale terrain



Large scale map



Large scale aerial



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BMP Sizing Calculator

HYDRO UNIT NAME	PENASQUITOS
HYDRO AREA NAME	Miramar Reservoir
HYDRO SUBAREA NAME	SAME AS HANAME
HYDRO BASIN NUMBER	906.10
HYDRO SOIL GROUP	D
RAIN GAUGE BASIN	Oceanside Basin

[Zoom to](#)

**Table 3-1
RUNOFF COEFFICIENTS FOR URBAN AREAS**

Land Use		Runoff Coefficient "C"				
NRCS Elements	County Elements	% IMPER.	Soil Type			
			A	B	C	D
Undisturbed Natural Terrain (Natural)	Permanent Open Space	0*	0.20	0.25	0.30	0.35
Low Density Residential (LDR)	Residential, 1.0 DU/A or less	10	0.27	0.32	0.36	0.41
Low Density Residential (LDR)	Residential, 2.0 DU/A or less	20	0.34	0.38	0.42	0.46
Low Density Residential (LDR)	Residential, 2.9 DU/A or less	25	0.38	0.41	0.45	0.49
Medium Density Residential (MDR)	Residential, 4.3 DU/A or less	30	0.41	0.45	0.48	0.52
Medium Density Residential (MDR)	Residential, 7.3 DU/A or less	40	0.48	0.51	0.54	0.57
Medium Density Residential (MDR)	Residential, 10.9 DU/A or less	45	0.52	0.54	0.57	0.60
Medium Density Residential (MDR)	Residential, 14.5 DU/A or less	50	0.55	0.58	0.60	0.63
High Density Residential (HDR)	Residential, 24.0 DU/A or less	65	0.66	0.67	0.69	0.71
High Density Residential (HDR)	Residential, 43.0 DU/A or less	80	0.76	0.77	0.78	0.79
Commercial/Industrial (N. Com)	Neighborhood Commercial	80	0.76	0.77	0.78	0.79
Commercial/Industrial (G. Com)	General Commercial	85	0.80	0.80	0.81	0.82
Commercial/Industrial (O.P. Com)	Office Professional/Commercial	90	0.83	0.84	0.84	0.85
Commercial/Industrial (Limited I.)	Limited Industrial	90	0.83	0.84	0.84	0.85
Commercial/Industrial (General I.)	General Industrial	95	0.87	0.87	0.87	0.87

*The values associated with 0% impervious may be used for direct calculation of the runoff coefficient as described in Section 3.1.2 (representing the pervious runoff coefficient, C_p , for the soil type), or for areas that will remain undisturbed in perpetuity. Justification must be given that the area will remain natural forever (e.g., the area is located in Cleveland National Forest).

DU/A = dwelling units per acre

NRCS = National Resources Conservation Service

Runoff Coefficient Adjustment

Post Development Area

Total Area 31008
Impervious: 22560 72.76%

$$C = 0.90 \times (\% \text{ Impervious}) + C_p \times (1 - \% \text{ Impervious})$$

$$\% \text{ impervious} = 72.76\%$$

$$C_p = 0.35 \quad (\text{Table 3.1, soil type D, 0\% impervious, County Hydrology Manual})$$

$$\mathbf{C = 0.75}$$

Pre Development Area

Total Area 31008
Impervious: 24516 79.06%

$$C = 0.90 \times (\% \text{ Impervious}) + C_p \times (1 - \% \text{ Impervious})$$

$$\% \text{ impervious} = 79.06\%$$

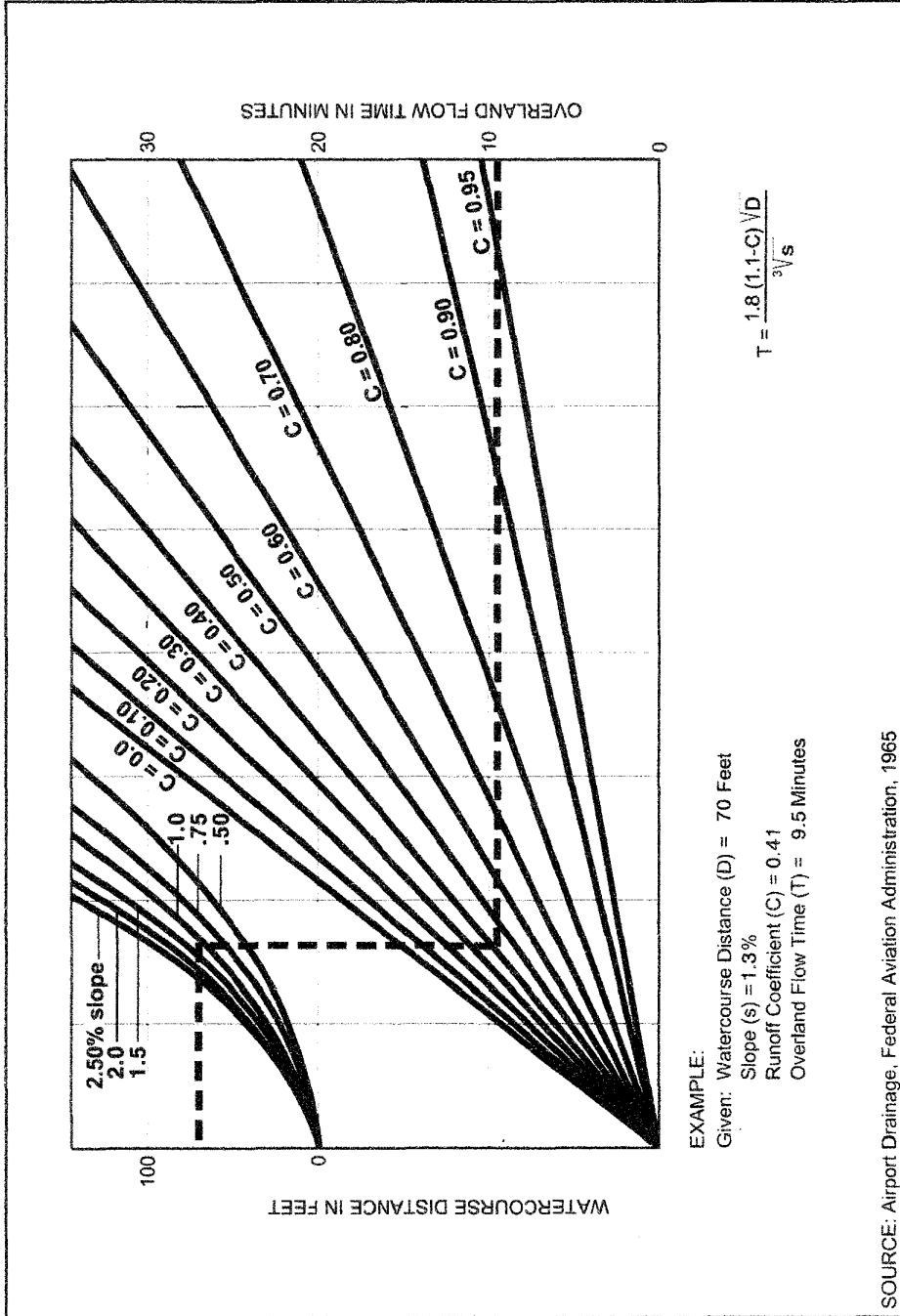
$$C_p = 0.35 \quad (\text{Table 3.1, soil type D, 0\% impervious, County Hydrology Manual})$$

$$\mathbf{C = 0.78}$$

Time of Concentration

Location	Initial Average	Initial L (ft)	Initial Travel Time	Add'l L (ft)	Average	Notes	Average Q	Additional TC	Total TC
	slope %		T (min)		slope %		Mannings Eq.	(travel time)	T (min)
									(5 minutes min)
Pre Dev.									
Site	1.25	50	3.8	190	1.25		1.2	2.6	6.4
Post Dev.									
Site	1	50	4.5	215	0.6		1.1	3.3	7.8

		Pre-Dev	Post-Dev
Initial Travel Time	Initial TC	Site	Site
(Figure 3-3)	C =	0.78	0.75
	D ft =	50	50
	S % =	1.25	1
	T =	3.78	4.45



FIGURE

3-3

Rational Formula - Overland Time of Flow Nomograph

Channel Report

Pre Dev TC Flow Path Velocity Average Q

Triangular

Side Slopes (z:1) = 100.00, 100.00
Total Depth (ft) = 0.12

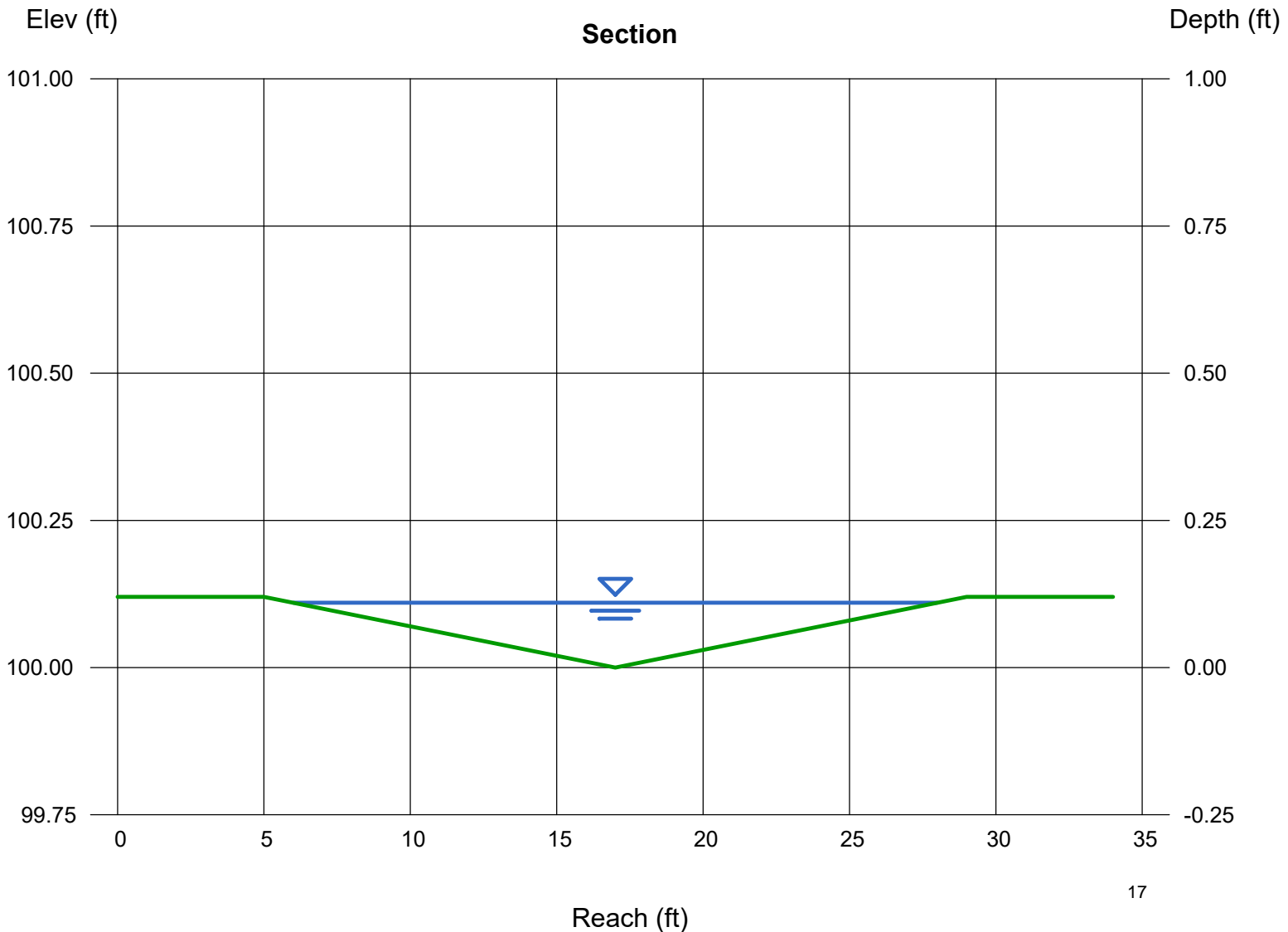
Invert Elev (ft) = 100.00
Slope (%) = 1.25
N-Value = 0.016

Calculations

Compute by: Known Q
Known Q (cfs) = 1.50

Highlighted

Depth (ft) = 0.11
Q (cfs) = 1.500
Area (sqft) = 1.21
Velocity (ft/s) = 1.24
Wetted Perim (ft) = 22.00
Crit Depth, Yc (ft) = 0.11
Top Width (ft) = 22.00
EGL (ft) = 0.13



Channel Report

Post Dev TC Flow Path Velocity Average Q

Gutter

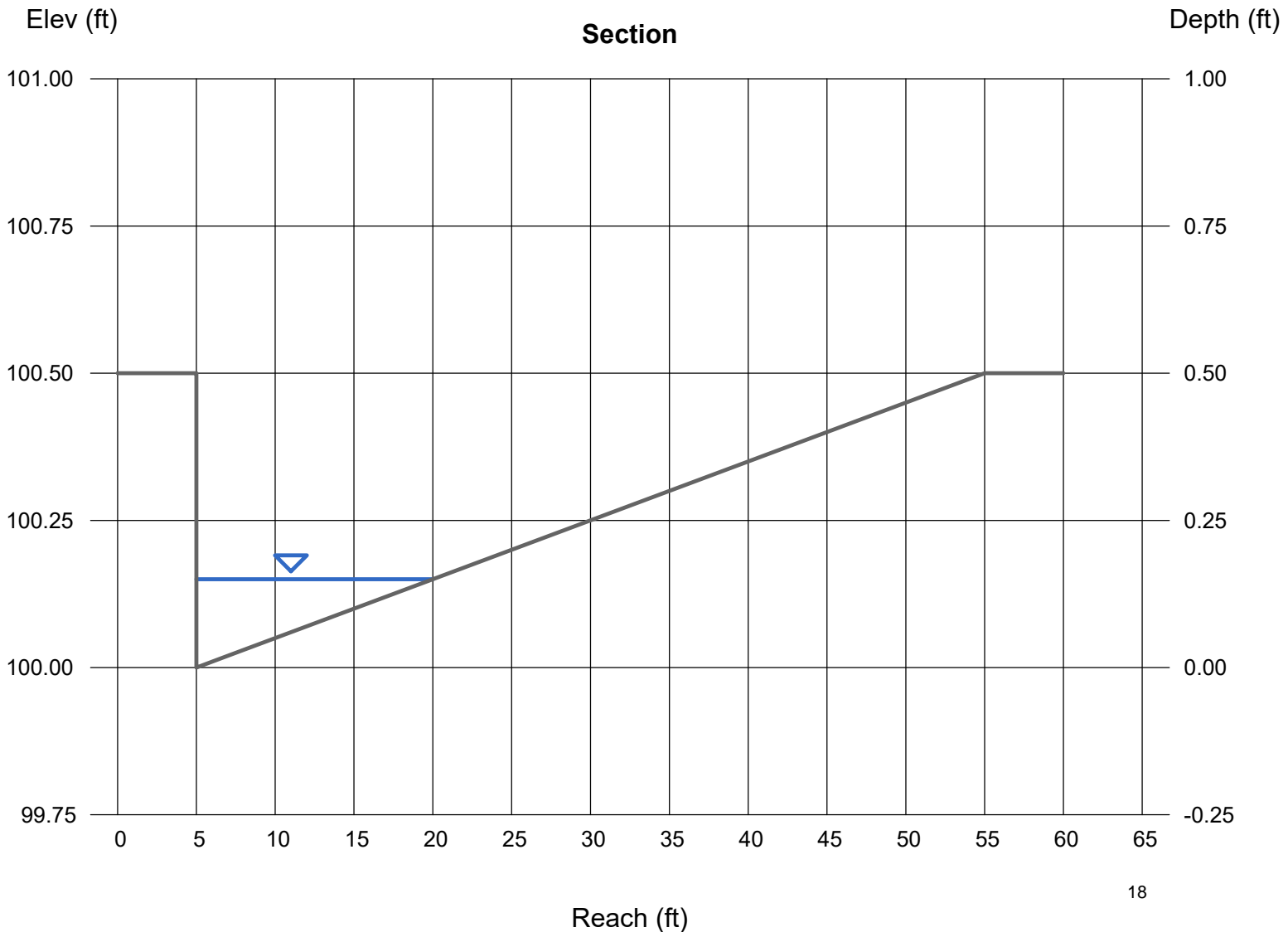
Cross Sl, Sx (ft/ft) = 0.01
 Cross Sl, Sw (ft/ft) = 0.01
 Gutter Width (ft) = 1.50
 Invert Elev (ft) = 100.00
 Slope (%) = 0.60
 N-Value = 0.016

Highlighted

Depth (ft) = 0.15
 Q (cfs) = 1.200
 Area (sqft) = 1.13
 Velocity (ft/s) = 1.07
 Wetted Perim (ft) = 15.15
 Crit Depth, Yc (ft) = 0.13
 Spread Width (ft) = 15.00
 EGL (ft) = 0.17

Calculations

Compute by: Known Q
 Known Q (cfs) = 1.20



Channel Report

Pre Dev Q100 Outlet Flow

Circular

Diameter (ft) = 1.00

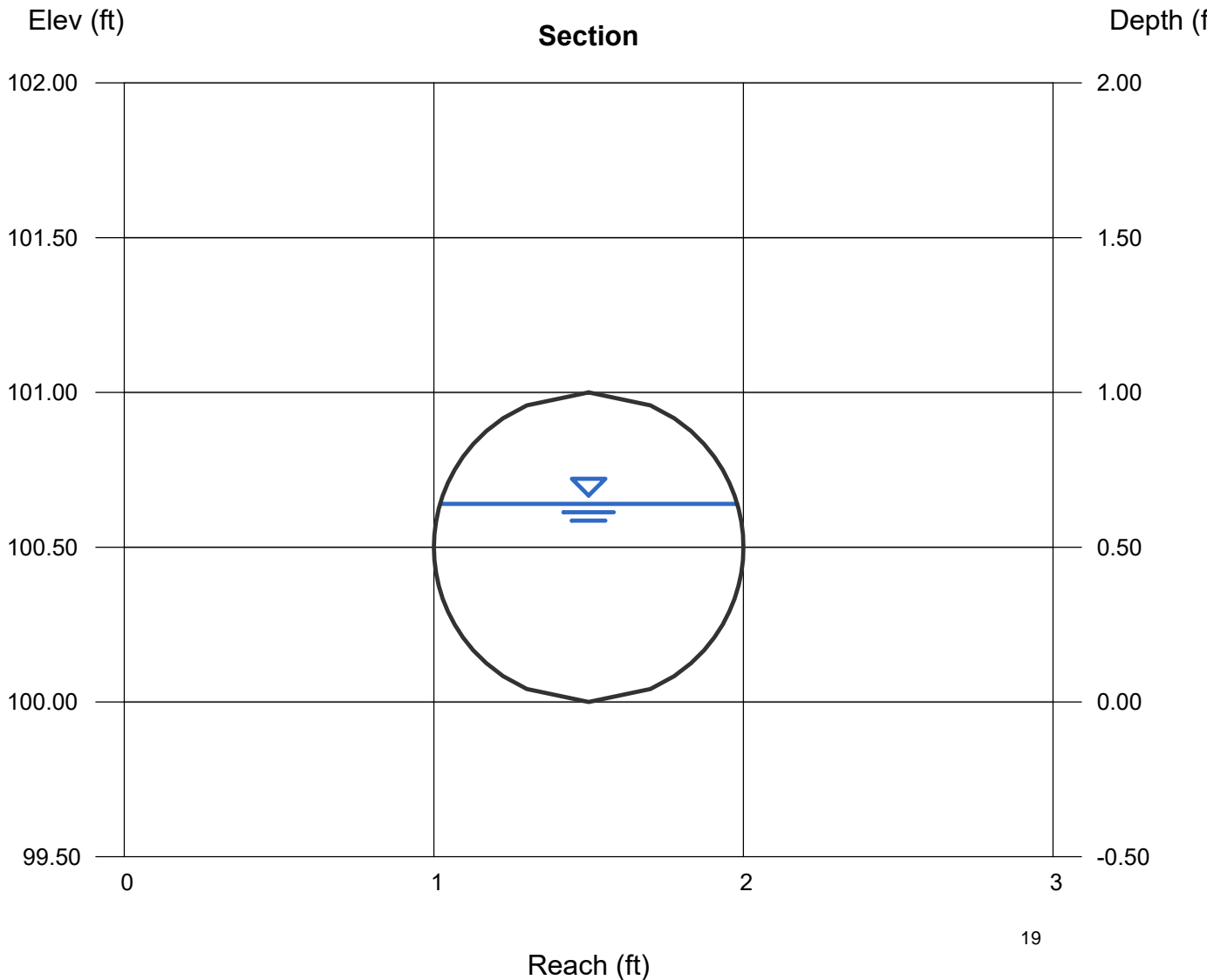
Invert Elev (ft) = 100.00
Slope (%) = 0.60
N-Value = 0.009

Highlighted

Depth (ft) = 0.64
Q (cfs) = 2.900
Area (sqft) = 0.53
Velocity (ft/s) = 5.46
Wetted Perim (ft) = 1.85
Crit Depth, Yc (ft) = 0.73
Top Width (ft) = 0.96
EGL (ft) = 1.10

Calculations

Compute by: Known Q
Known Q (cfs) = 2.90



Channel Report

Q100 (2) 10in Pipes exiting the Biofiltration Basin. 1.2 cfs each (2.4 cfs total)

Circular

Diameter (ft) = 0.83

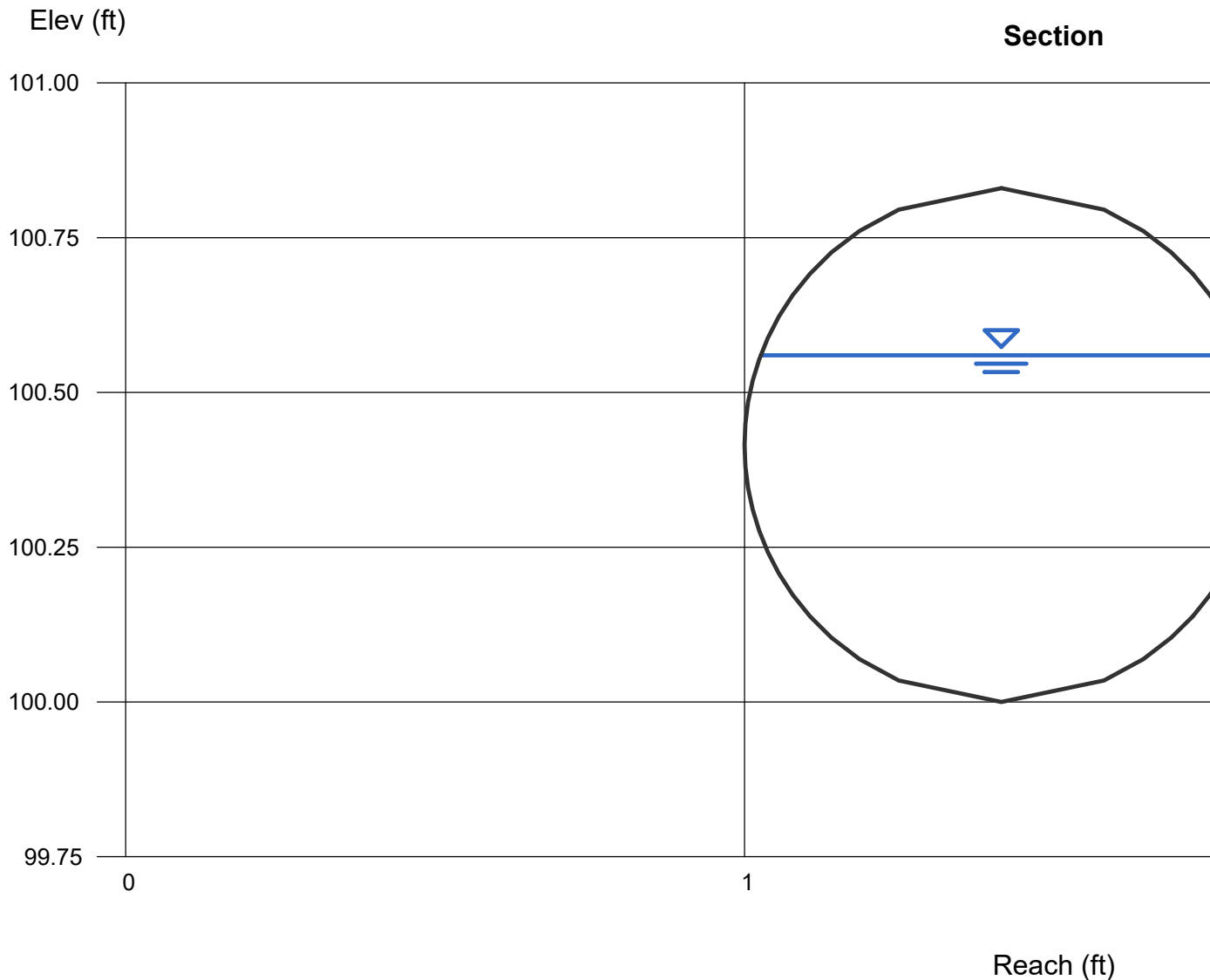
Invert Elev (ft) = 100.00
Slope (%) = 0.50
N-Value = 0.013

Calculations

Compute by: Known Q
Known Q (cfs) = 1.20

Highlighted

Depth (ft) = 0.56
Q (cfs) = 1.200
Area (sqft) = 0.39
Velocity (ft/s) = 3.08
Wetted Perim (ft) = 1.60
Crit Depth, Yc (ft) = 0.49
Top Width (ft) = 0.78
EGL (ft) = 0.71



Channel Report

Post Dev Q100 Outlet Flow (exist 12in pipe)

Circular

Diameter (ft) = 1.00

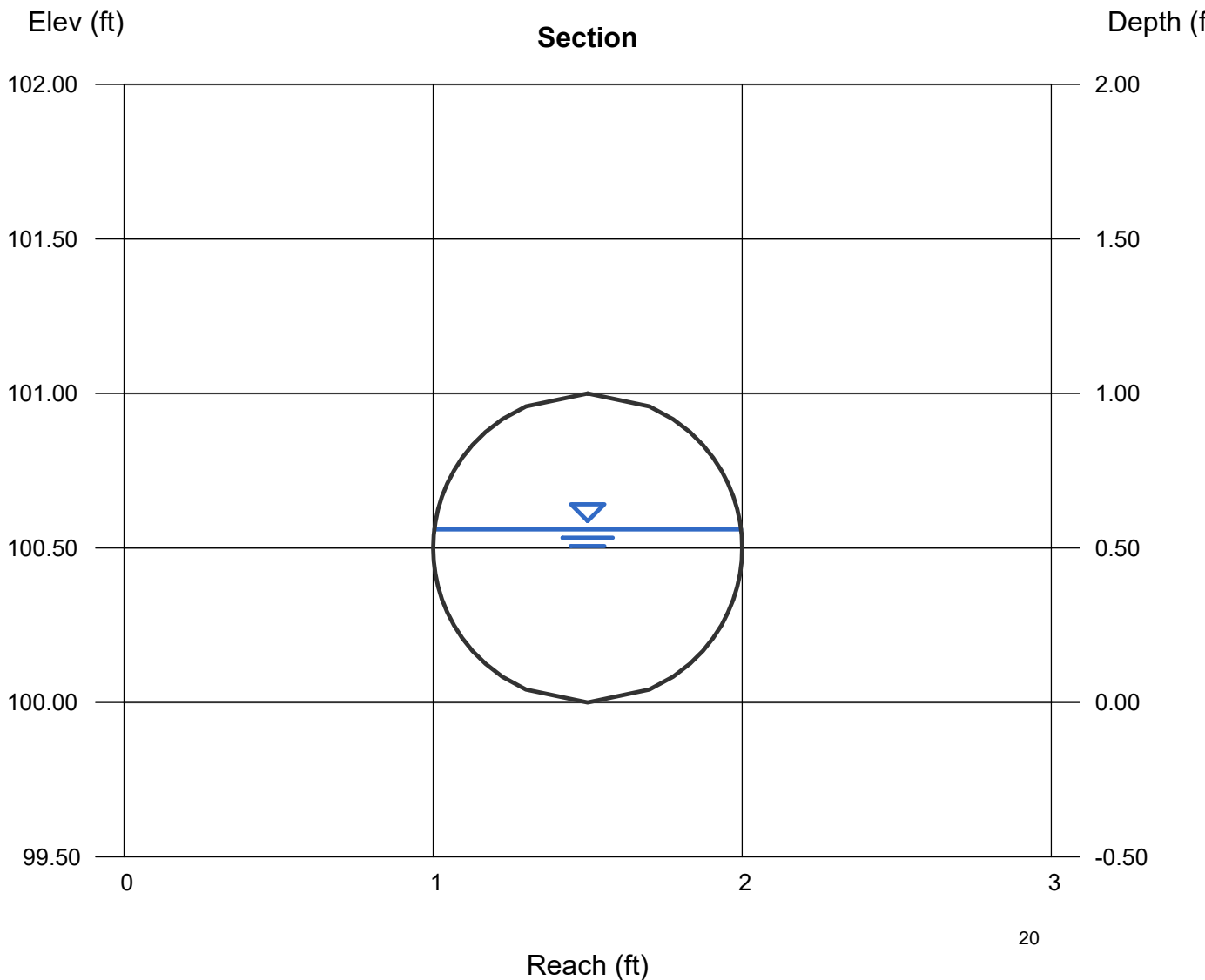
Invert Elev (ft) = 100.00
Slope (%) = 0.60
N-Value = 0.009

Highlighted

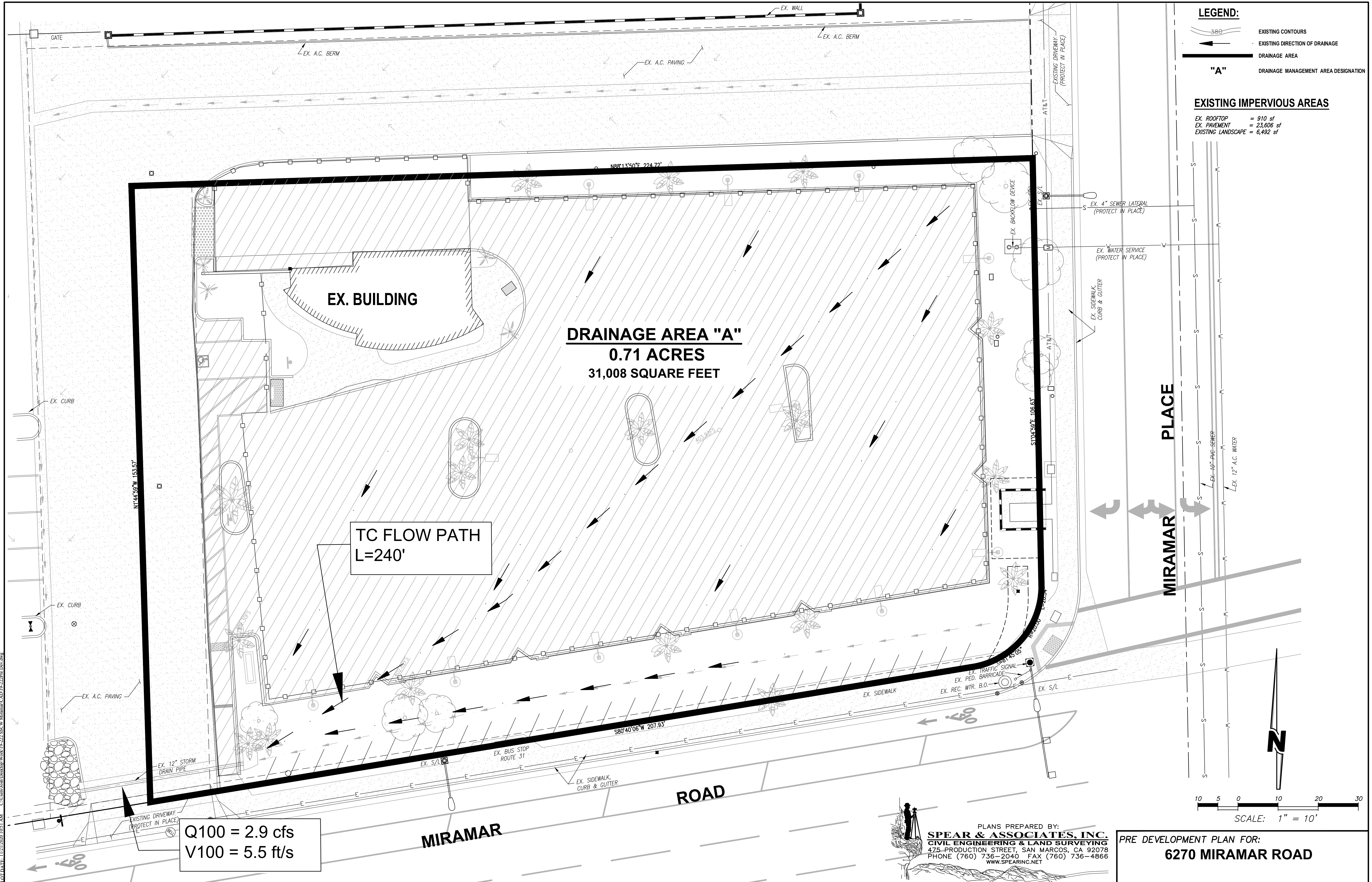
Depth (ft) = 0.56
Q (cfs) = 2.400
Area (sqft) = 0.45
Velocity (ft/s) = 5.28
Wetted Perim (ft) = 1.69
Crit Depth, Yc (ft) = 0.67
Top Width (ft) = 0.99
EGL (ft) = 0.99

Calculations

Compute by: Known Q
Known Q (cfs) = 2.40



ATTACHMENT C



LEGEND:

- EXISTING CONTOURS
- EXISTING DIRECTION OF DRAINAGE
- DRAINAGE AREA
- "A" DRAINAGE MANAGEMENT AREA DESIGNATION

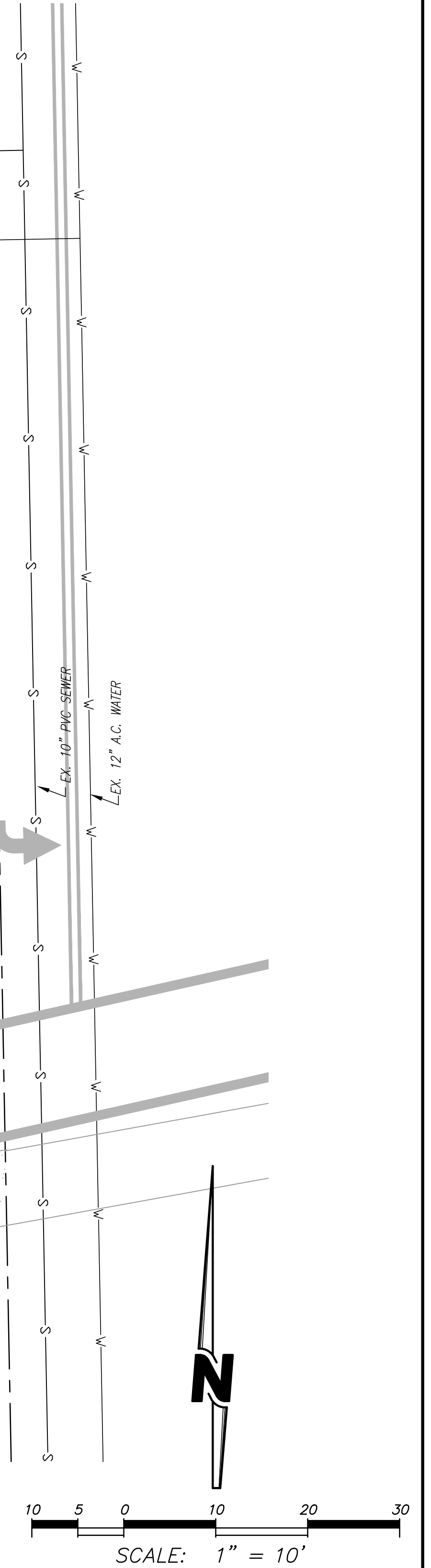
EXISTING IMPERVIOUS AREAS

EX. ROOFTOP = 910 sf
 EX. PAVEMENT = 23,606 sf
 EXISTING LANDSCAPE = 6,492 sf

DRAINAGE AREA "A"
 0.71 ACRES
 31,008 SQUARE FEET

TC FLOW PATH
 L=240'

Q100 = 2.9 cfs
V100 = 5.5 ft/s

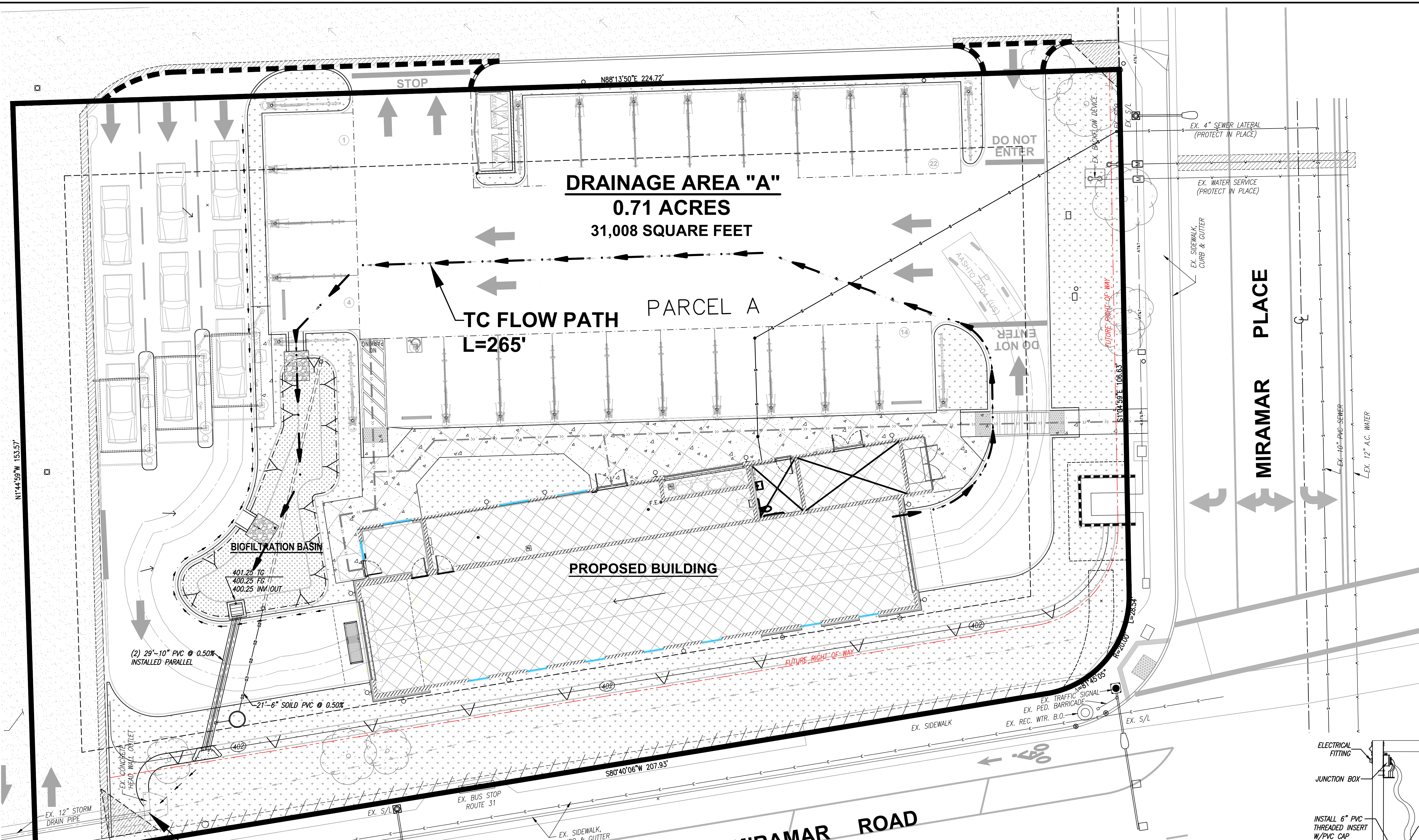
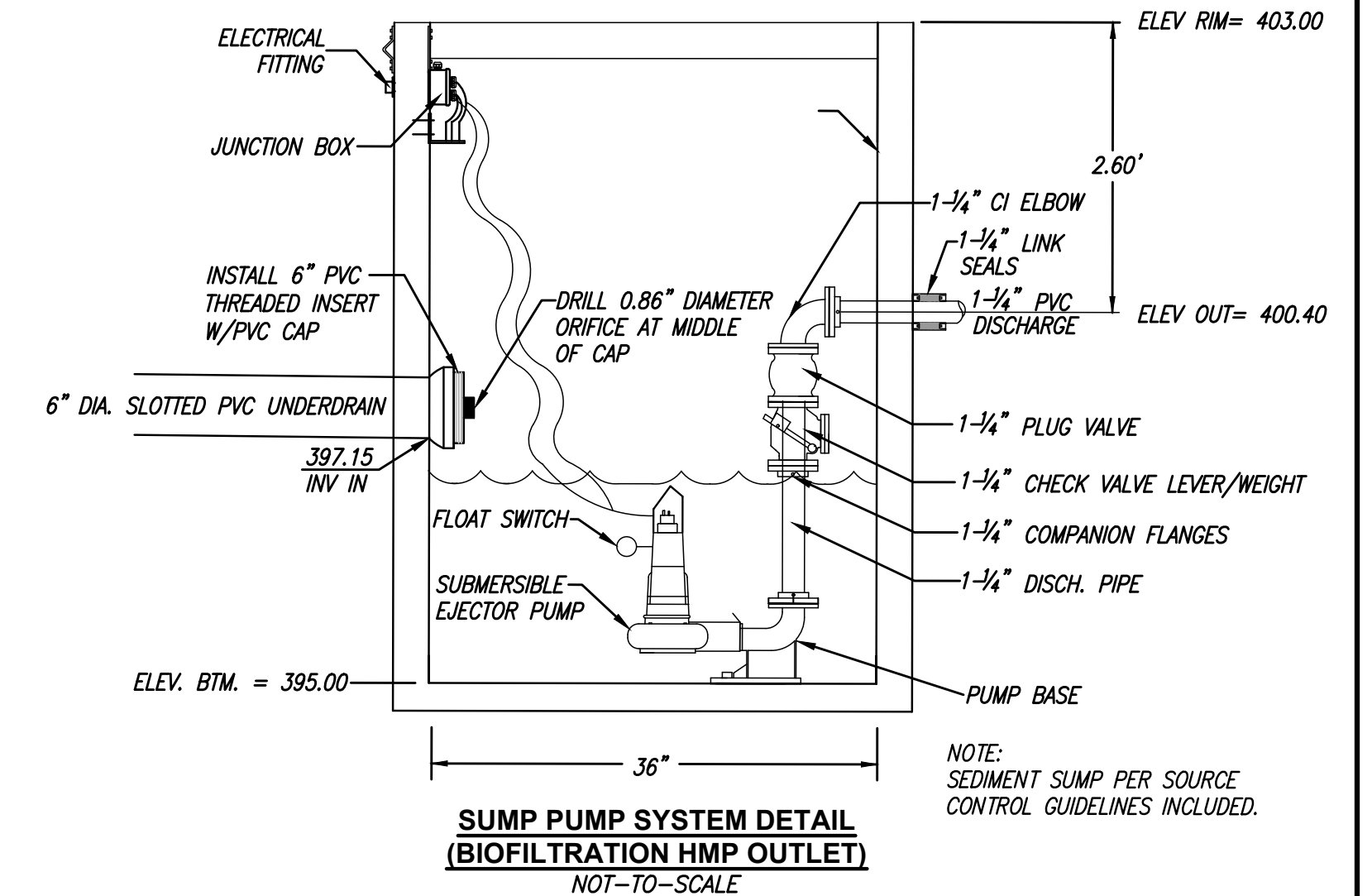
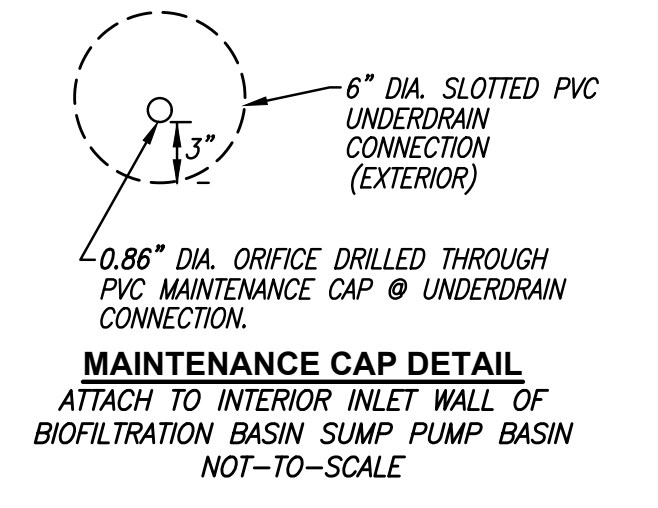
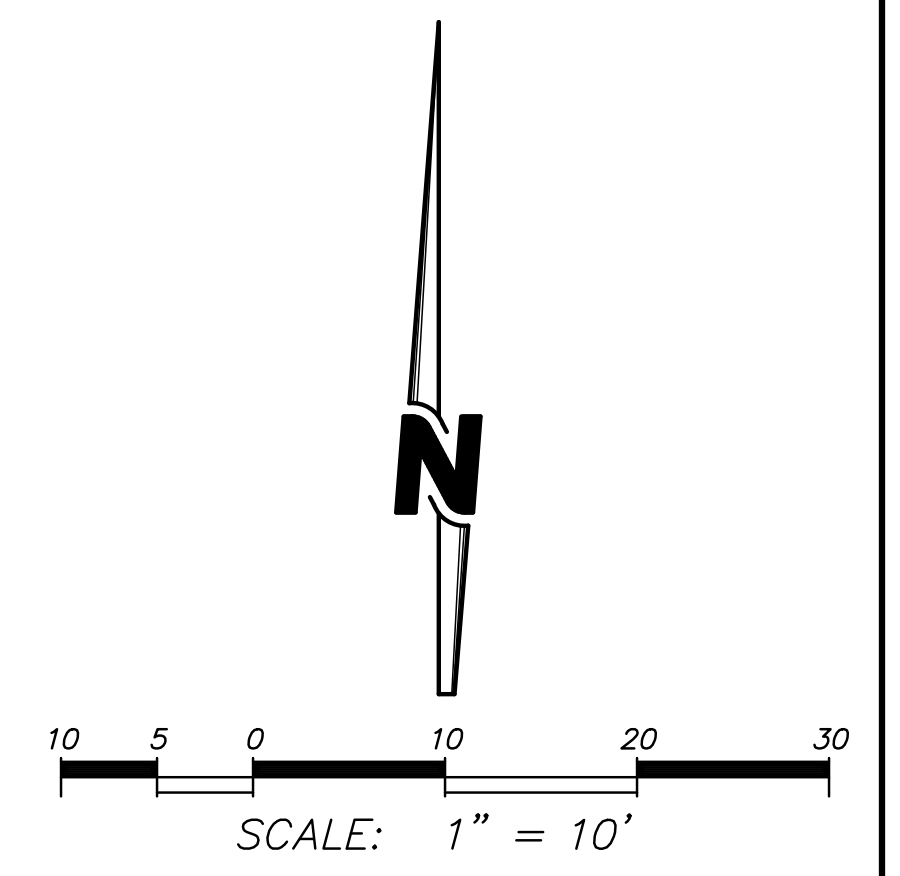
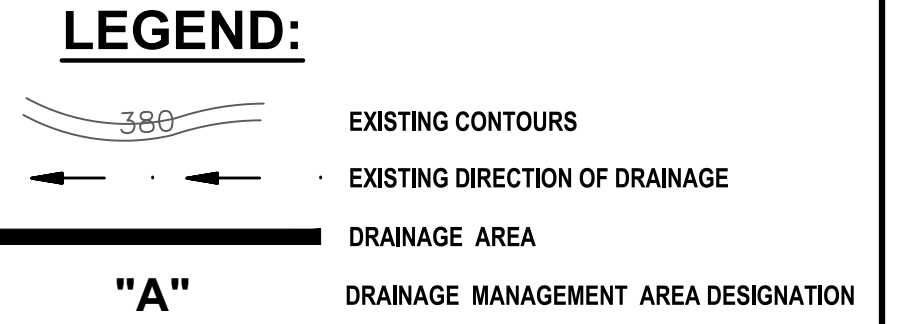


PLANS PREPARED BY:
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PRE DEVELOPMENT PLAN FOR:
6270 MIRAMAR ROAD

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DRAINAGE AREA DMA BREAKDOWN			
DRAINAGE AREA SURFACE	SYMBOL	SOIL TYPE	DRAINAGE AREA 'A'
BUILDING ROOFTOP	[Symbol]	TYPE D	3,945 SQ FT
PARKING/DRIVE AISLE IMPERVIOUS AREA	[Symbol]	TYPE D	14,750 SQ FT
HARSCAPING/SIDEWALK	[Symbol]	TYPE D	1,525 SQ FT
EXIST. IMPERVIOUS AREA	[Symbol]	TYPE D	2,340 SQ FT
LANDSCAPING AREA	[Symbol]	TYPE D	8,448 SQ FT
			TOTAL LOT AREA = 31,008 SQ FT



POC
 Q100 = 2.4 cfs
 V100 = 5.3 ft/s

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POST DEVELOPMENT PLAN FOR:
6270 MIRAMAR ROAD

PL01 DATE: 11/01/2020 10:50 AM C:\Users\jacob\Desktop\Work\19-222-SS&W\Miramar\CAD\19-222\Plan\Dev.dwg

