# HYDROLOGY REPORT

FOR

5228 CHELSEA STREET APN: 415-062-10 DATE: OCTOBER 03, 2016

PREPARED BY:
SAN DIEGO LAND SURVEYING AND ENGINEERING INC.
9665 CHESAPEAKE DRIVE, SUITE 445
SAN DIEGO, CA. 92123

CITY OF SAN DIEGO PTS 502954

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## **EXHIBITS**

HYDROLOGY	MAP	_	EXISTING	CONDITION	EXHIBIT	A
HYDROLOGY	MAP	_	PROPOSED	CONDITION	EXHIBIT	В

PAGE 1

#### PROJECT DESCRIPTION:

#### EXISTING PROJECT SITE DESCRIPTION:

The site is 0.2040 acres in size and is occupied by single story single family home. The site splits the storm runoff in two directions. A portion of the site drains is to the south and to the Pacific Ocean. A portion of the site drains to Chelsea Street. This public road drains to the north. There are block retaining walls or screen walls on the north and south property lines. The east property line is Chelsea Street. Therefor none or minimal offsite water drains onto the site.

See the 20 scale drainage areas map in Exhibit A for more detail of the project.

The existing impervious area is 3,496 SF. or 0.0803 AC. 39.4%

#### PROPOSED PROJECT DESCRIPTION:

The project will consist of remodel or removal of the existing home and the construction of a new single family home. The disturbed area is about 6000 square feet. The existing utilities will be reused, reducing the impact to the public right-of-way.

See the 20 scale drainage areas map in Exhibit B for more detail of the proposed project.

The proposed impervious area is 5,783 SF. or 0.1328 AC. 65.1%

### STANDARDS AND METHODS:

#### PURPOSE OF CALCULATIONGS:

Calculate the storm runoff generated by the residential site and the impact to the downstream lands.

### HYDROLOGIC MODEL AND METHODS USED:

This report uses the "Rational Method" as demonstrated in the County of San Diego Storm Drain Manual.

$$Q = CIA$$

### WATER QUALITY DESIGN STORM:

The design storm for this report shall be the 50 year storm for private drainage and the 100 year storm for public storm drain structures and flow paths. The 85% storm will be used for any storm water treatment structures that are required.

#### ANALYSIS AND CONCLUSIONS

#### PRE-DEVELOPMENT RUNOFF VOLUMES AND PEAK FLOWS:

Runoff factor "C" for medium density residential (4.3 DU/A) with a soil type of "D" from table 3-1 "Runoff Coefficients for Urban Areas" from the above manual and attached in Appendix "B" is 0.52. See Exhibit "A" for plan view of the drainage area.

Modify C factor for actual impervious area.

Actual impervious area = 
$$\frac{.394 + .52}{2}$$
 = **0.46**

Time of concentration is composed of "Maximum Overland Flow Length" plus "Travel Time" to point of discharge. The maximum overland flow length is taken form Table 3-2, included in Appendix C, for medium density residential (4.3 DU/A) with a grade of 2% is 8.1 mins. for the first 80 feet. There is no "Travel Time as the drainage area does not exceed 80 feet in length. 8.1 mins.

Using the 50 year storm and the rainfall intensity-duration-frequency curves from the chart in Appendix "D". Determine rainfall intensity "I". For  $8.1 \, \text{min.}$ ,  $50 \, \text{year storm}$ , the rainfall intensity =  $3.54 \, \cdot$ 

Using the 100 year storm and the rainfall intensity-duration-frequency curves from the chart in Appendix "D". Determine rainfall intensity "I". For 5 min., 100 year storm, the rainfall intensity = 3.92.

Zone Existing Area E1 = 0.1402 acres This area consists of the portion of the site that drains to the Pacific Ocean.

Q50 = CIA = 
$$.46 \times 3.54 \times 0.1402 = 0.23$$
 CFS  
Q100 = CIA =  $.46 \times 3.92 \times 0.1402 = 0.25$  CFS

Zone Existing Area E2 = 0.0638 acres This area consists of the portion of the site that drains to Chelsea Road.

Q50 = CIA = 
$$.46 \times 3.54 \times 0.0638 = 0.10 \text{ CFS}$$
  
Q100 = CIA =  $.46 \times 3.92 \times 0.0638 = 0.12 \text{ CFS}$ 

#### Total project runoff:

$$Q50 = 0.23 + 0.10 = 0.33 \text{ CFS}$$
  
 $Q100 = 0.25 + 0.12 = 0.37 \text{ CFS}$ 

#### POST-PROJECT RUNOFF VOLUMES AND PEAK FLOWS:

Runoff factor "C" for medium density residential  $(4.3 \ DU/A)$  with a soil type of "D" from table 3-1 "Runoff Coefficients for Urban Areas" from the above manual and attached in Appendix "B" is 0.52. See Exhibit "A" for plan view of the drainage area.

Modify C factor for actual impervious area.

Actual impervious area = 
$$\frac{.651 + .52}{2}$$
 = **0.59**

Time of concentration is composed of "Maximum Overland Flow Length" plus "Travel Time" to point of discharge. The maximum overland flow length is taken form Table 3-2, included in Appendix C, for medium density residential (4.3 DU/A) with a grade of 2% is 8.1 mins. for the first 80 feet. There is no "Travel Time as the drainage area does not exceed 80 feet in length. 8.1 mins.

Using the 50 year storm and the rainfall intensity-duration-frequency curves from the chart in Appendix "D". Determine rainfall intensity "I". For 8.1 min., 50 year storm, the rainfall intensity = 3.54.

Using the 100 year storm and the rainfall intensity-duration-frequency curves from the chart in Appendix "D". Determine rainfall intensity "I". For 5 min., 100 year storm, the rainfall intensity = 3.92.

Zone Proposed Area P1 = 0.1383 acres This area consists of the portion of the site that drains to Chelsea Road.

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Q50 = CIA = .59 \times 3.54 \times 0.1383 = 0.29 CFS
Q100 = CIA = .59 \times 3.92 \times 0.1383 = 0.32 CFS
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Zone Proposed Area P2 = 0.0658 acres This area consists of the portion of the site that drains to the Pacific Ocean.

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Q50 = CIA = .59 \times 3.54 \times 0.0658 = 0.14 CFS
Q100 = CIA = .59 \times 3.92 \times 0.0658 = 0.15 CFS
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#### Total project runoff:

Q50 = 0.29 + 0.14 = 0.43 CFSQ100 = 0.32 + 0.15 = 0.47 CFS

#### CONCLUSION:

The most important design change from the existing condition is that the amount of area that drains to the Pacific Ocean has been greatly reduced. The existing runoff to the rear of the site of 0.25 CFS (100 year storm) is reduced to 0.15 CFS (100 year storm). This includes storm water that falls on a portion of the site that is the coastal bluffs.

The majority of the site and its storm runoff will be directed to the front yard landscaping and the public street (Chelsea Street).

Total street side runoff is less than .5 CFS and can sheet flow over the curb.

#### CERTIFICATION STATEMENT:

This Hydrology Report has been prepared under the direction of the following registered civil engineer. The registered civil engineer (Engineer) attests to the technical information contained herein and the engineering data upon which the following design, recommendations, conclusions and decisions are based. The selection, sizing, and design of storm water treatment and other control measures in this report meet the requirements of the Regional Water Quality Control Board Order R9-2013-0001 and subsequent amendments.

ENGINEER OF WORK:

DATE: 10-03-2016

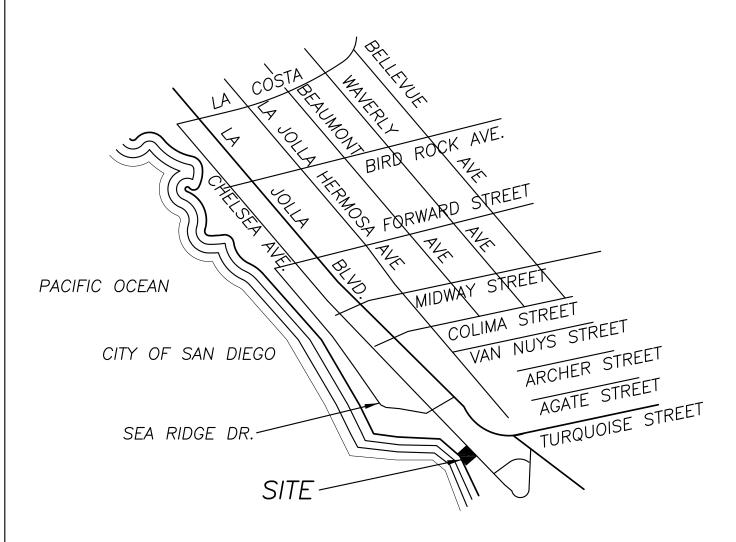
MICHAEL LEE SMITH, RCE 35471 MY REGISTRATION EXPIRES ON 9/30/2017



# APPENDIX A

VICINITY MAP





# VICINITY MAP

NOT TO SCALE

# APPENDIX B

COUNTY OF SAN DIEGO STORM DRAIN MANUAL TABLE 3-1, RUNOFF COEFFICIENTS FOR URBAN AREA

San Diego County Hydrology Manual Date: June 2003

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Table 3-1 RUNOFF COEFFICIENTS FOR URBAN AREAS

La	Land Use		Ru	Runoff Coefficient "C"	"C.,	
				Soil	Soil Type	
NRCS Elements	County Elements	% IMPER.	A	В	C	D
Undisturbed Natural Terrain (Natural)	Permanent Open Space	*0	0.20	0.25	0.30	0.35
Low Density Residential (LDR)	Residential, 1.0 DU/A or less	10	0.27	0.32	0.36	0.41
Low Density Residential (LDR)	Residential, 2.0 DU/A or less	20	0.34	0.38	0.42	0.46
Low Density Residential (LDR)	Residential, 2.9 DU/A or less	25	0.38	0.41	0.45	0.49
Medium Density Residential (MDR)	Residential, 4.3 DU/A or less	30	0.41	0.45	0.48	0.52
Medium Density Residential (MDR)	Residential, 7.3 DU/A or less	- 40	0.48	0.51	0.54	0.57
Medium Density Residential (MDR)	Residential, 10.9 DU/A or less	45	0.52	0.54	0.57	09.0
Medium Density Residential (MDR)	Residential, 14.5 DU/A or less	50	0.55	0.58	09'0	0.63
High Density Residential (HDR)	Residential, 24.0 DU/A or less	65	99.0	0.67	69.0	0.71
High Density Residential (HDR)	Residential, 43.0 DU/A or less	80	92.0	0.77	0.78	0.79
Commercial/Industrial (N. Com)	Neighborhood Commercial	80	92.0	0.77	0.78	0.79
Commercial/Industrial (G. Com)	General Commercial	85	08.0	0.80	0.81	0.82
Commercial/Industrial (O.P. Com)	Office Professional/Commercial	06	0.83	0.84	0.84	0.85
Commercial/Industrial (Limited I.)	Limited Industrial	06	0.83	0.84	0.84	0.85
Commercial/Industrial (General I.)	General Industrial	95	0.87	0.87	0.87	0.87

\*The values associated with 0% impervious may be used for direct calculation of the runoff coefficient as described in Section 3.1.2 (representing the pervious runoff coefficient, Cp, for the soil type), or for areas that will remain undisturbed in perpetuity. Justification must be given that the area will remain natural forever (e.g., the area is located in Cleveland National Forest).

DU/A = dwelling units per acre NRCS = National Resources Conservation Service

# APPENDIX C

COUNTY OF SAN DIEGO STORM DRAIN MANUAL FIGURE 3-1, TIME OF CONCENTRATION CHARTS

Section: Page:	12 of 26
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Note that the Initial Time of Concentration should be reflective of the general land-use at the upstream end of a drainage basin. A single lot with an area of two or less acres does not have a significant effect where the drainage basin area is 20 to 600 acres.

Table 3-2 provides limits of the length (Maximum Length (L<sub>M</sub>)) of sheet flow to be used in hydrology studies. Initial Ti values based on average C values for the Land Use Element are also included. These values can be used in planning and design applications as described below. Exceptions may be approved by the "Regulating Agency" when submitted with a detailed study.

MAXIMUM OVERLAND FLOW LENGTH (L<sub>M</sub>)

Table 3-2

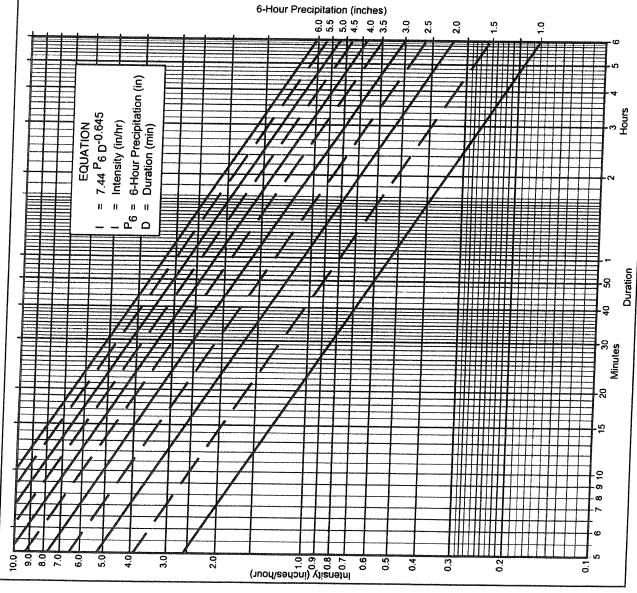
& INITIAL TIME OF CONCENTRATION (T)

Element*	DU/		5%		%		ONC	1	%		%	10	1%
	Acre	L <sub>M</sub>	Ti	L <sub>M</sub>	Ti	L <sub>M</sub>	Ti						
Natural		50	13.2	70	12.5	85	10.9	100	10.3	100	8.7	100	6.9
LDR	1	50	12.2	70	11.5	85	10.0	100	9.5	100	8.0	100	6.4
LDR	2	50	11.3	70	10.5	85	9.2	100	8.8	100	7.4	100	5.8
LDR	2.9	50	10.7	70	10.0	85	8.8	95	8.1	100	7.0	100	5.6
MDR	4.3	50	10.2	70	9.6	80	8.1	95	7.8	100	6.7	100	5.3
MDR	7.3	50	9.2	65	8.4	80	7.4	95	7.0	100	6.0	100	4.8
MDR	10.9	50	8.7	65	7.9	80	6.9	90	6.4	100	5.7	100	4.5
MDR	14.5	50	8.2	65	7.4	80	6.5	90	6.0	100	5.4	100	4.3
HDR	24	50	6.7	65	6.1	75	5.1	90	4.9	95	4.3	100	3.5
HDR	43	50	5.3	65	4.7	75	4.0	85	3.8	95	3.4	100	2.7
N. Com		50	5.3	60	4.5	75	4.0	85	3.8	95	3.4	100	2.7
G. Com		50	4.7	60	4.1	75	3.6	85	3.4	90	2.9	100	2.4
O.P./Com		50	4.2	60	3.7	70	3.1	80	2.9	90	2.6	100	2.2
Limited I.		50	4.2	60	3.7	70	3.1	80	2.9	90	2.6	100	2.2
General I.	-	50	3.7	60	3.2	70	2.7	80	2.6	90	2.3	100	1.9

<sup>\*</sup>See Table 3-1 for more detailed description

# APPENDIX D

COUNTY OF SAN DIEGO STORM DRAIN MANUAL FIGURE 3-1, INTENSITY DURATION DESIGN CHART



# Directions for Application:

- for the selected frequency. These maps are included in the County Hydrology Manual (10, 50, and 100 yr maps included (1) From precipitation maps determine 6 hr and 24 hr amounts in the Design and Procedure Manual).
  - (2) Adjust 6 hr precipitation (if necessary) so that it is within the range of 45% to 65% of the 24 hr precipitation (not applicable to Desert).
    - (3) Plot 6 hr precipitation on the right side of the chart.
- (4) Draw a line through the point parallel to the plotted lines.
  - (5) This line is the intensity-duration curve for the location being analyzed.

# Application Form:

- (a) Selected frequency SO year
- (2)% \ P6 = 24 = = (b)  $P_6 = \frac{1.8}{1.8}$  in.,  $P_{24} = \frac{3.1}{3.1}$ 
  - (c) Adjusted  $P_6^{(2)} = \frac{118}{118}$  in.
    - % min. (d) t<sub>x</sub> = \_
      - (e) I = 3.5 1/in./hr.

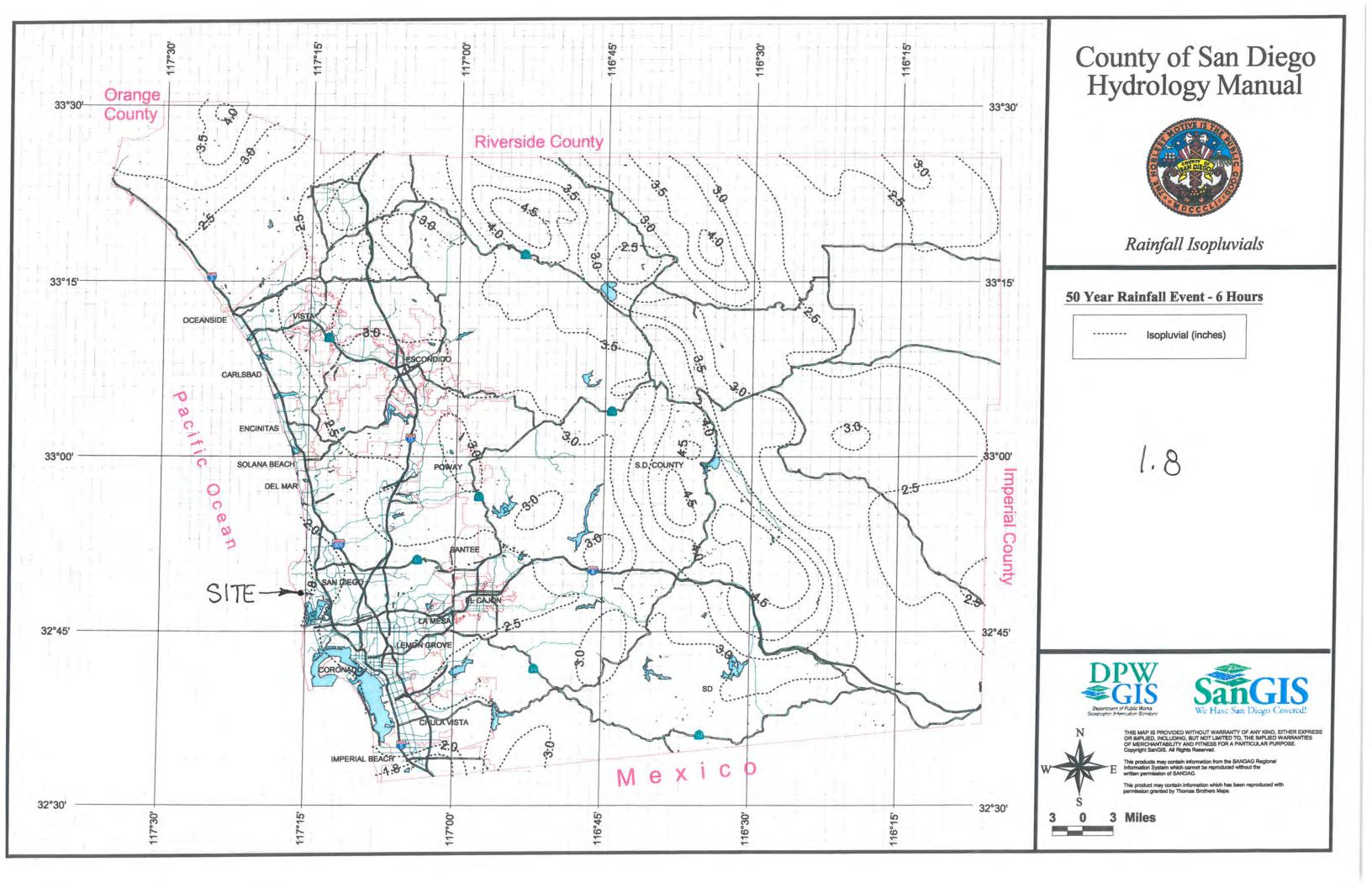
Note: This chart replaces the Intensity-Duration-Frequency curves used since 1965.

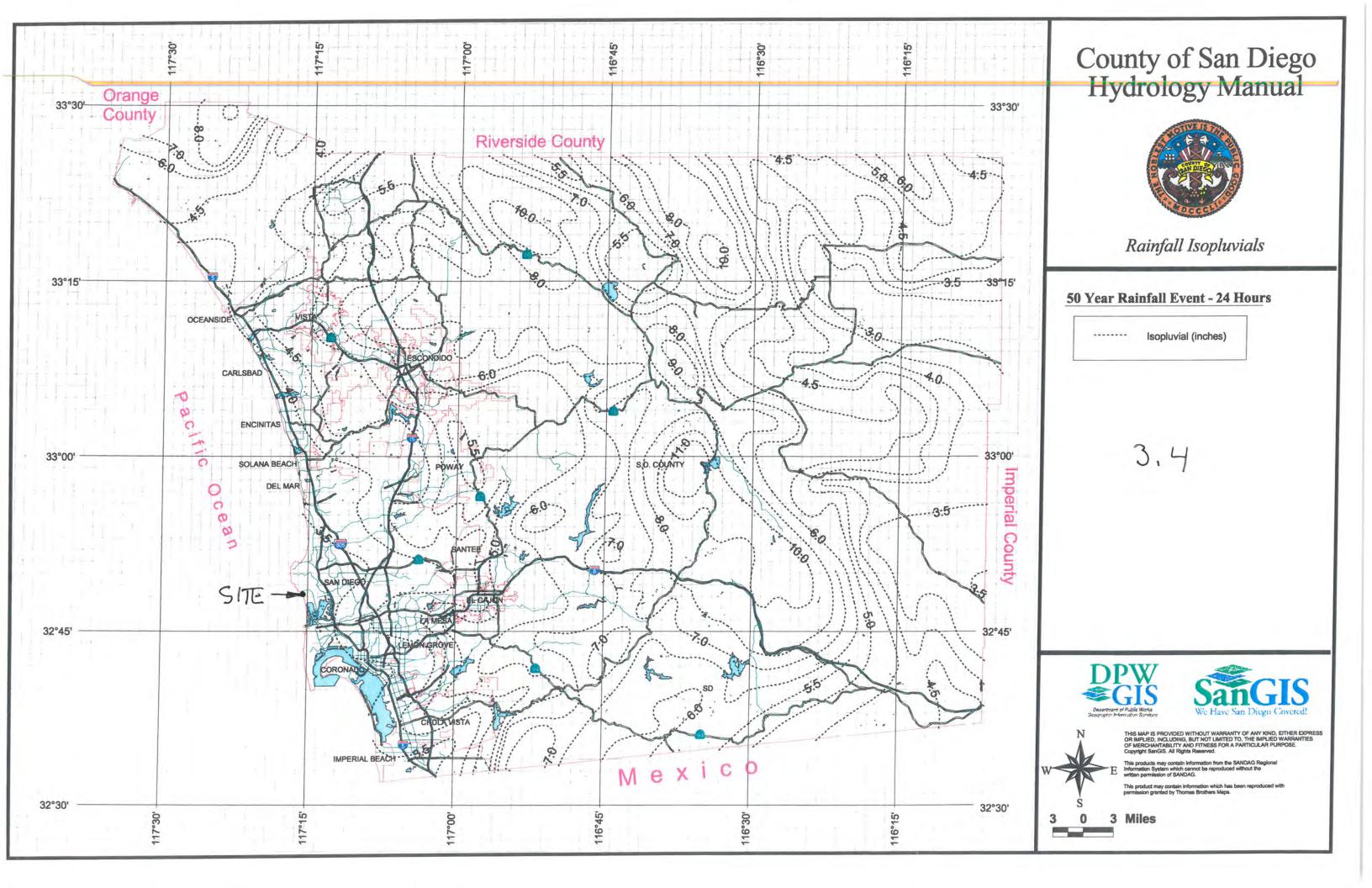
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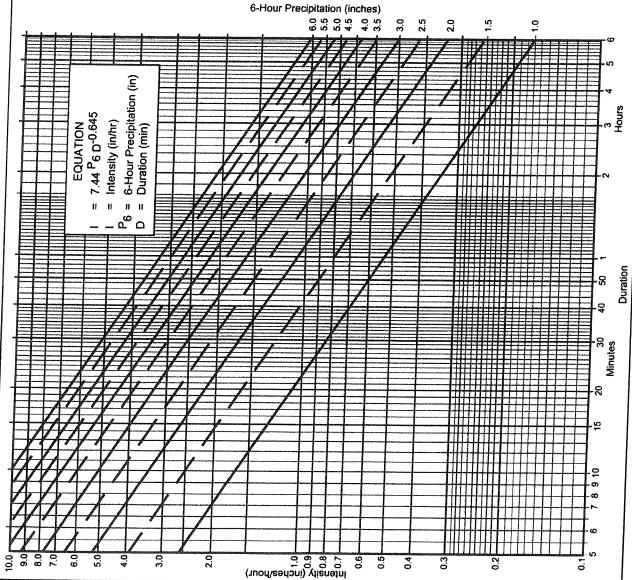
Intensity-Duration Design Chart - Template

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# Directions for Application:

- for the selected frequency. These maps are included in the (1) From precipitation maps determine 6 hr and 24 hr amounts County Hydrology Manual (10, 50, and 100 yr maps included in the Design and Procedure Manual).
  - (2) Adjust 6 hr precipitation (if necessary) so that it is within the range of 45% to 65% of the 24 hr precipitation (not applicable to Desert).
    - (3) Plot 6 hr precipitation on the right side of the chart.
- (4) Draw a line through the point parallel to the plotted lines.
  - (5) This line is the intensity-duration curve for the location being analyzed.

# Application Form:

- (a) Selected frequency 100 year
- (b)  $P_6 = \frac{2.0}{10.0}$  in.,  $P_{24} = \frac{3.0}{3.0}$

%(2)

- (c) Adjusted  $P_6^{(2)} = 2.0$  in.
  - ₩ min. (d)  $t_{\chi} =$ 
    - (e) I = 3,92in./hr.

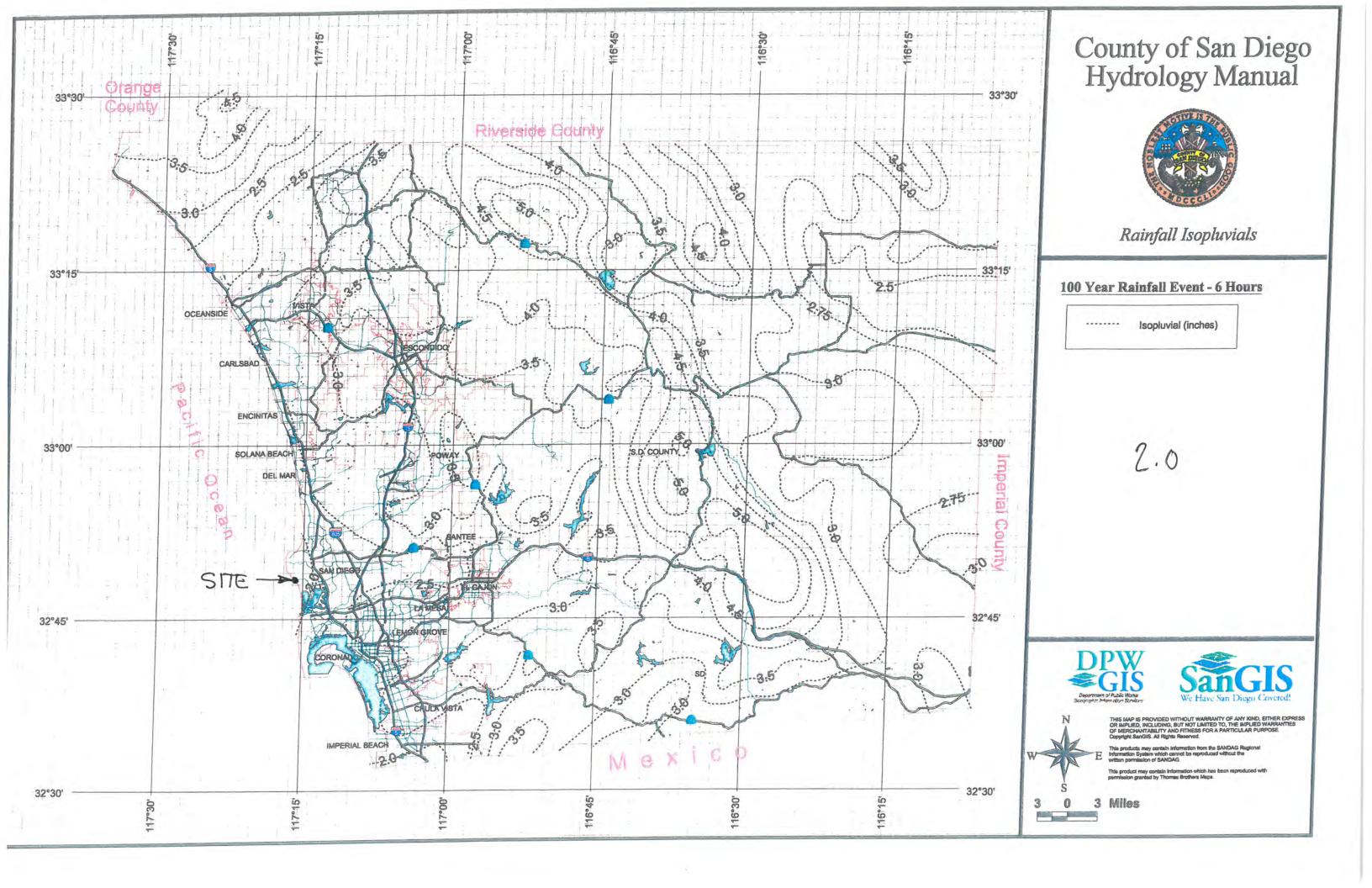
Note: This chart replaces the Intensity-Duration-Frequency curves used since 1965.

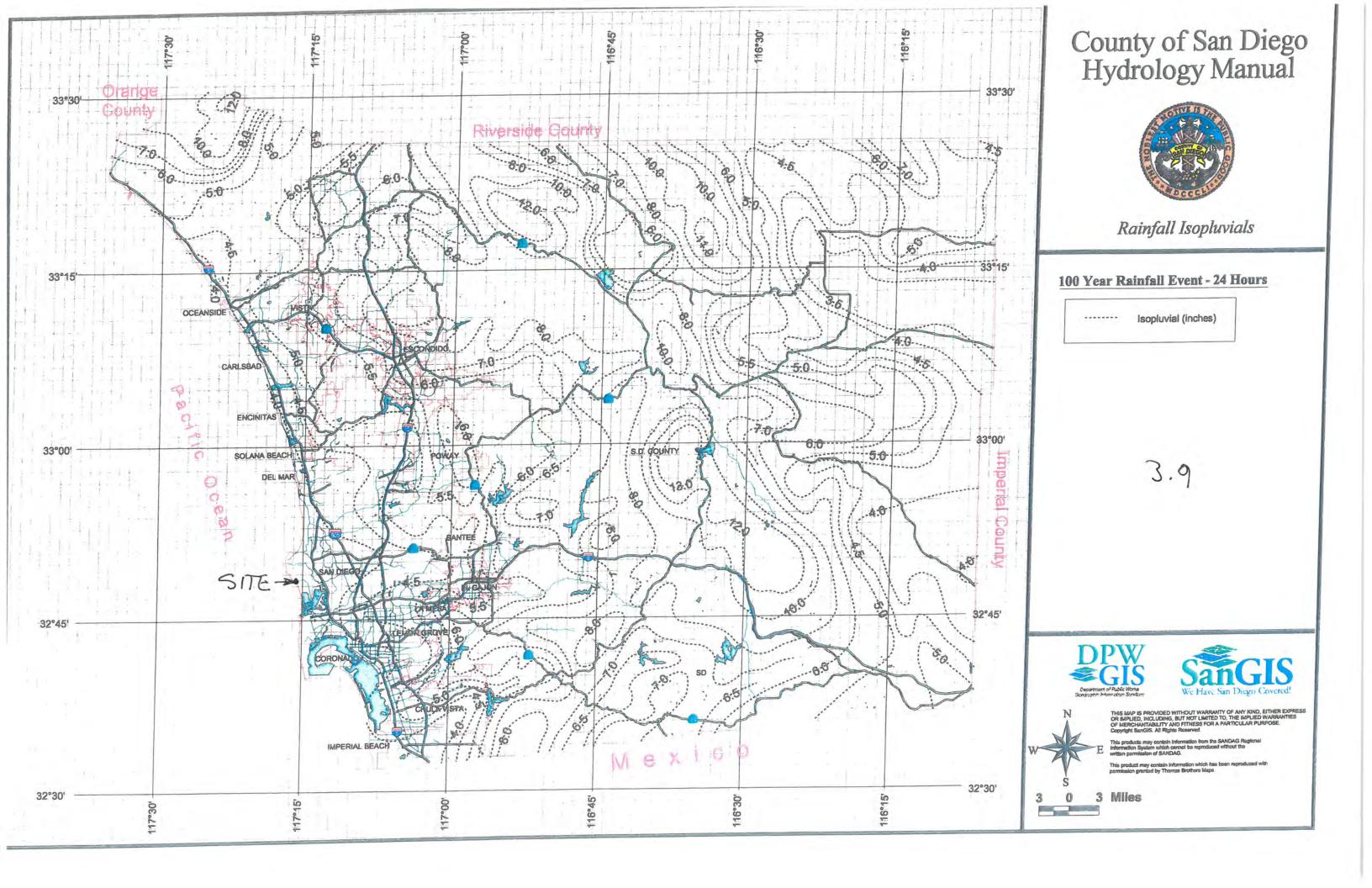
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Intensity-Duration Design Chart - Template

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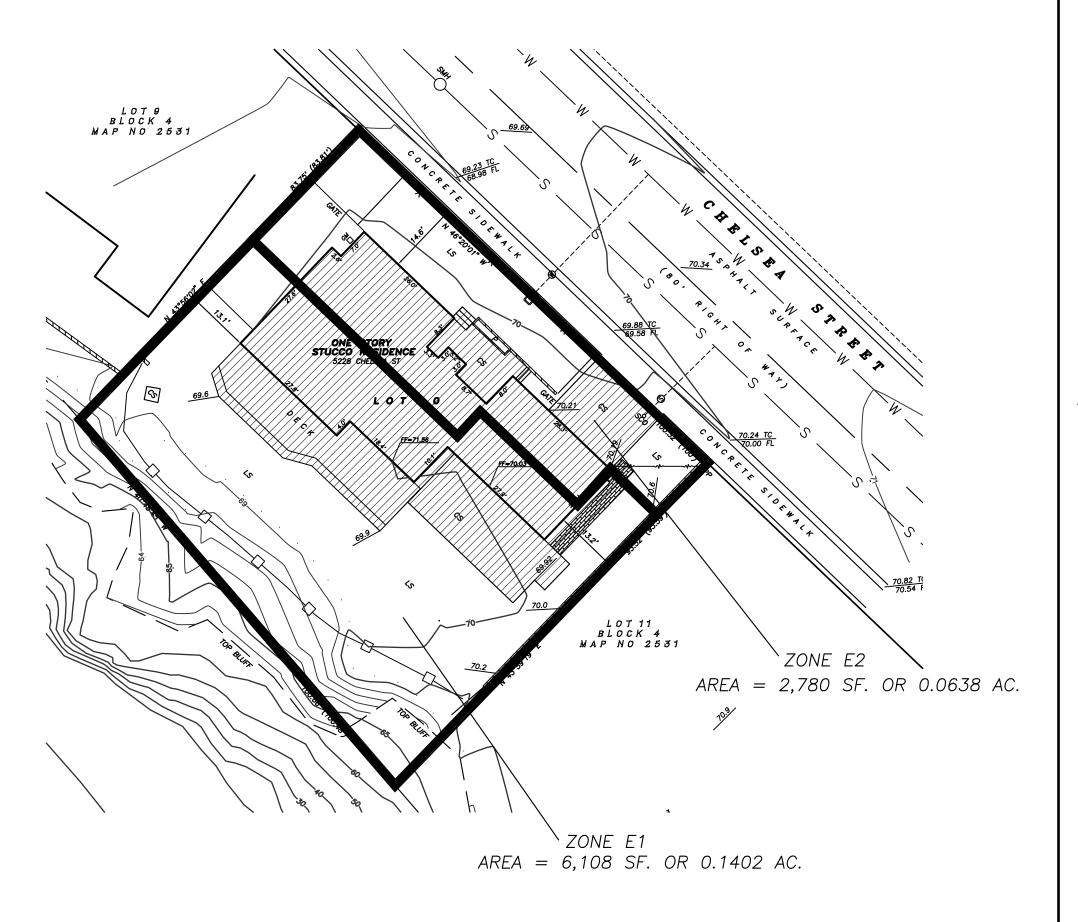
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# EXHIBIT A

# EXISTING CONDITIONS DRAINAGE AREAS MAP



# EXHIBIT A

HYDROLOGY MAP
EXISTING CONDITIONS



SCALE 1" = 20'

PROJECT AREA

AREA = 8,888 SF. OR 0.2040 AC.

ZONE E1 AREA = 6,108 SF. OR 0.1402 AC.

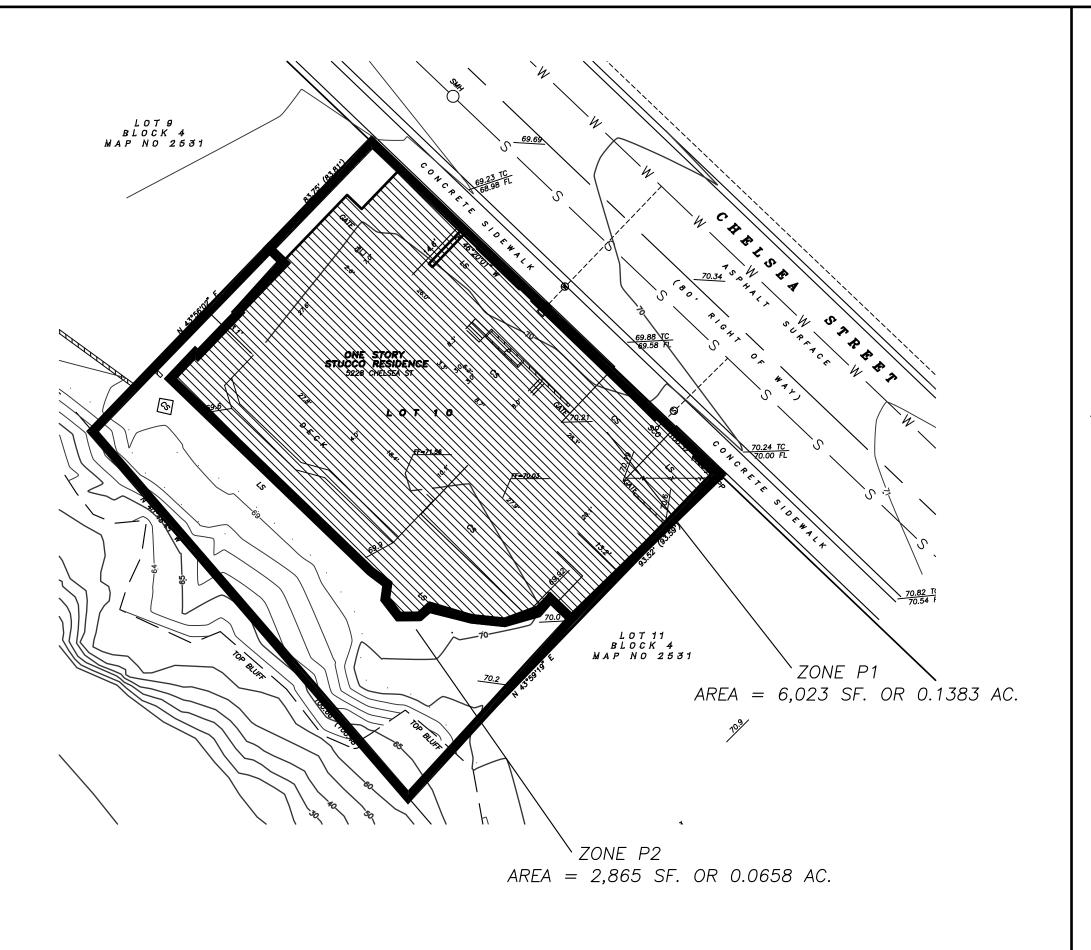
ZONE E2

AREA = 2,780 SF. OR 0.0638 AC.

IMPERVIOUS AREA AREA = 3,496 SF. OR 0.0803 AC. 60.7% OF SITE

# EXHIBIT B

# PROPOSED CONDITIONS DRAINAGE AREAS MAP



# EXHIBIT B

HYDROLOGY MAP
PROPOSED CONDITIONS



SCALE 1" = 20'

PROJECT AREA

AREA = 8,888 SF. OR 0.2040 AC.

ZONE P1 AREA = 6,023 SF. OR 0.1383 AC.

ZONE P2

AREA = 2,865 SF. OR 0.0658 AC.

IMPERVIOUS AREA

AREA = 5,783 SF. OR 0.1328 AC.
65.1% OF SITE