

1126

PASTS

FIELD BOOK

No. 385 F

126

1126

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THE FREDERICK POST CO.

ENGINEERING and DRAFTING SUPPLIES

IRVING PARK STATION

CHICAGO, ILL.

92 FIFTH ST.
PORTLAND, ORE.

79 NEW MONTGOMERY ST.
SAN FRANCISCO, CAL.

AGENTS FOR

"BERGER" TRANSITS and LEVELS

"GURLEY" SURVEYING and HYDRAULIC INSTRUMENTS

"CHICAGO" STEEL TAPES, etc.

20' wide Alley R 9 to 30th Bet Juniper & Kalmia 3/10/25
 X Sec mill.

B.M.	4.58	294.29	289.71	SE 30 th & Kalmia
		00 = W Line 30 th		
N		4.59	289.70	on paving
E		5.18	289.01	" "
S		5.00	289.29	" "
		50' N		
S		4.6	289.7	" "
E		4.65	289.64	" "
N		4.2	290.1	" "
		100' W		
N		4.0	290.5	" "
E		4.22	290.07	" "
S		4.0	290.3	" "
		160' W		
S		2.8	291.5	" "
SE		3.32	290.97	" "
E		3.32	290.97	" "
N		2.8	291.5	" "
		168' W		
N		2.6	291.7	" "
E		2.7	291.6	" "
S		2.7	291.6	" "
		196' W = Gen. on N. DIT 2' out		
S		2.9	291.4	" "
E		2.7	291.6	" "
N		2.5	291.8	" "

29th

ST



30th

ST.

294.29

228' W = E End 4 Garages on N. ent floors on line

N	2.8	291.5
E	2.8	291.5
S	3.3	291.0

250' W

S	3.7	290.6
E	3.5	290.8
N	3.2	291.1

277' W = W End 4 Garages on N. on line

N	3.0	291.3
E	3.6	290.7
S	3.5	290.8

291' W = Gar. on N. ent floor 2nd out

S	3.8	290.5
E	3.8	290.5
N	3.1	291.2

320' W = Garage on N. 1st Back on s. 1st Back

N	3.7	290.6
E	3.7	290.6
S	3.8	290.5

T.P. 0.43 291.15 3.57 290.72

393' W = E End 5 Garages on S ent floors 3rd Back

3	0.4	290.8	on floor
S	0.6	290.6	
E	0.6	290.6	
N	0.5	290.7	

291.15

2

437' W = W End 5 Garages on S

N	0.9	290.3
E	0.7	290.5
S	0.7	290.5
3	0.5	290.7

444' W = Double Garage on S 1st out

S	1.4	289.8
E	1.5	289.7
N	1.3	289.9

500' W

N	2.7	288.5
E	3.0	288.2
S	3.0	288.2

540' W

S	3.8	287.4
E	4.8	286.4
N	4.9	286.3

545' W

N	5.2	286.0
E	5.1	286.1
S	5.2	286.0

590' W

S	7.4	283.8
E	7.4	283.8
N	7.9	283.3

291.15

3

617' W

N	12.2	279.0
W	10.6	280.6
E	10.7	280.5
S	9.4	281.8

644' W

S	14.3	276.9
E	15.4	275.6
N	15.1	276.1

650' N

N	15.9	275.3
E	16.3	274.9
S	16.5	274.7

100's (cont)

1/4	5.4	363.5
C	5.3	363.6
1/4	5.2	363.7
.cb	5.3	363.6
W	5.1	363.8

120's

W	5.2	363.7
cb	5.2	363.7
1/4	4.9	364.0
+5	4.7	364.7
E	4.8	364.1
1/4	5.4	363.5
cb	5.3	363.6
E	5.3	363.6

140's

E	5.3	363.6
cb	5.5	363.4
1/4	5.5	363.4
e	5.4	363.5
1/4	5.4	363.5
cb	5.4	363.5
W	5.5	363.4

200's

W	5.7	363.2
cb	5.5	363.4
1/4	5.5	363.4
C	5.5	363.4

1/4	5.7	363.2
cb	5.7	363.2
E	5.6	363.3

230's

E	5.6	363.3
cb	5.7	363.2
1/4	5.5	363.4
E	5.9	363.0
1/4	4.7	364.2
cb	5.3	363.6
W	5.7	363.2

250's

W	6.0	362.9
cb	5.9	363.0
1/4	5.8	363.1
C	5.7	363.2
1/4	5.7	363.2
cb	5.6	363.3
E	5.8	363.1

275's

C	5.9	363.0
cb	6.0	362.9
1/4	5.8	363.1
E	6.0	362.9
1/4	5.9	363.0
cb	5.4	363.5
W	6.0	362.9

57° 57'
E.S.D

6

300's

W	5.9	363.0
+7	5.1	363.8
cb	5.0	363.9
1/4	5.8	363.1
e	5.9	363.0
1/4	5.8	363.1
cb	5.9	363.0
E	5.9	363.0

315's

E	6.0	362.9
cb	5.9	363.0
1/4	6.0	362.9
C	6.2	362.7
1/4	5.9	363.0
cb	5.9	363.0
W	5.9	363.0

350's

W	6.2	362.7
cb	6.1	362.8
1/4	6.0	362.9
e	6.0	362.9
1/4	6.1	362.8
cb	6.2	362.7
E	6.1	362.8

370's

E	6.0	362.9
cb	6.2	362.7
1/4	5.8	363.1
C	5.3	363.6
+5	6.3	363.6
+8	4.1	364.8
1/4	4.4	364.5
cb	5.9	363.0
W	4.4	362.5

400's

W	5.9	363.0
cb	6.1	362.8
1/4	5.6	363.3
C	5.8	363.1
1/4	6.0	362.9
cb	6.2	362.7
E	6.2	362.7

415's

E	6.2	362.7
cb	6.2	362.7
1/4	6.1	362.8
C	5.8	363.1
1/4	6.1	362.8
cb	6.1	362.8
W	5.0	363.9

5th ST
E.S.D.

7

430'S

W	6.2	362.7
CB	6.1	362.8
1/4	6.2	362.7
C	6.2	362.7
1/4	6.3	362.6
CB	6.3	362.6
E	6.2	362.7

445'S

C	6.2	362.7
CB	6.2	362.7
1/4	4.7	364.2
+7	4.3	364.6
C	4.6	364.3
1/4	6.0	362.9
CB	6.0	362.9
W	5.8	363.1

465'S

W	4.8	364.1
CB	5.5	363.4
1/4	6.1	362.8
+7	6.1	362.8
C	5.3	363.6
1/4	5.6	363.3
+7	6.3	362.6
CB	6.3	362.6
E	6.2	362.7

478'S

E	5.9	363.0
CB	6.1	362.8
1/4	6.4	362.5
C	6.4	362.5
1/4	6.1	362.8
CB	6.8	362.1
+4	6.0	362.9
W	5.9	363.0

495'S

W	4.6	364.3
CB	5.9	363.0
1/4	6.3	362.6
C	5.9	363.0
+9	6.3	362.6
1/4	5.5	363.4
+8	4.1	364.8
CB	4.2	364.7
E	5.6	363.3

515'S

E	6.1	362.8
CB	6.1	362.8
1/4	6.6	362.3
C	6.3	362.6
1/4	6.1	362.8
CB	6.1	362.8
W	6.3	362.6

540'S

w	6.5	362.4
cb	6.3	362.6
1/4	6.1	362.8
e	6.0	362.9
+10	5.4	363.5
1/4	5.5	363.4
cb	6.2	362.7
e	5.8	363.1

570'S

e	6.2	362.7
cb	6.2	362.7
1/4	6.3	362.6
e	6.1	362.8
1/4	5.0	363.9
+7	4.9	364.0
cb	5.5	363.4
w	5.8	363.1

590'S

w	6.5	362.4
cb	6.6	362.3
1/4	6.1	362.8
e	5.7	363.2
1/4	6.2	362.7
cb	6.2	362.7
e	6.0	362.9

606.5 = N Line Orange

5455
E.S.D.

8

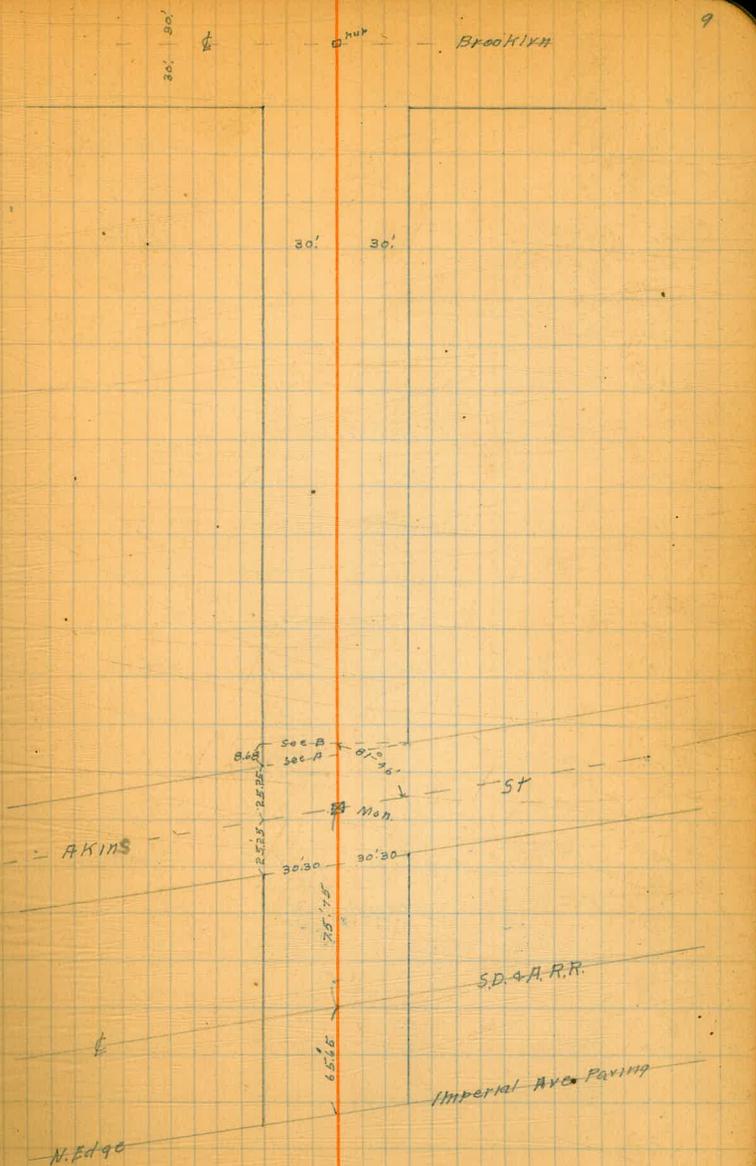
e	6.0	362.9	
cb	6.2	362.6	on emb cb
1/4	6.1	362.8	
e	6.0	362.9	
1/4	6.3	362.6	
cb	6.4	362.5	dirt
cb	6.0	362.8	Not done on cb
w	6.0	362.9	

60' wide
10' obs
10' 1/2

FERGUS ST
3/11/25 Miller
X Sec from N. Line Imp. Ave Paving to S. Line Brooklyn

N.M. AKINS
& Ferguson

B.M. Spk	5.04	184.78	179.74	
		00 = N. Edge PAVING		
W		2.79	182.0	on paving
C		2.50	182.3	
E		2.20	182.6	
		5' N		
C		2.4	182.4	
cb		2.5	182.3	
1/4		2.7	182.1	
C		2.7	182.1	
1/4		2.9	181.9	
cb		3.0	181.8	
W		3.1	181.7	
		13' N		
-10		6.4	178.4	
W		6.0	178.8	
cb		5.4	179.4	
1/4		5.8	179.0	
C		6.1	178.7	
1/4		6.0	178.8	
cb		5.9	178.9	
E		6.0	178.8	
+10		5.8	179.0	
		21' N		
-10		6.1	178.7	
E		6.3	178.5	



184.78

21' N (60M)

cb	6.3	178.5
1/4	6.3	178.5
c	6.3	178.5
1/4	6.4	178.4
cb	6.1	178.7
w	6.0	178.8
+10	6.2	178.6

27' N

-10	8.4	176.4
w	7.6	177.2
cb	7.5	177.3
1/4	8.0	176.8
c	8.2	176.6
1/4	8.1	176.7
cb	8.0	176.8
E	7.8	177.0
+10	7.5	177.3

47' N

-10	7.1	177.7
E	7.8	177.0
cb	7.9	176.9
1/4	8.0	176.8
c	7.9	176.9
1/4	8.0	176.8
cb	7.6	177.2
w	7.1	177.7
+10	7.1	177.7

184.78

FERGUS

10

57' N.

w	3.7	181.6
cb	3.3	181.5
1/4	3.0	181.8
c	2.8	182.0
1/4	2.6	182.2
cb	2.4	182.4
E	2.2	182.6

65.65 N = 4 SP47 RR

E	1.31	183.47 on rail hayardose
c	1.82	182.26 " " "
w	2.33	182.45 " " "

75' N

w	2.8	182.0
cb	2.5	182.3
1/4	3.0	182.8
c	2.2	182.6
1/4	1.8	183.0
cb	1.4	183.4
E	1.6	183.2

88' N

-15	10.4	174.4
c	10.3	174.5
cb	10.7	174.1
1/4	10.8	174.0
c	10.6	174.6
1/4	10.7	174.1

184.74

cb	10.7	174.1
W	10.7	174.1
+15	10.9	173.9
	105' N	
-15	10.2	174.6
W	10.0	174.8
cb	9.7	175.1
1/4	10.4	174.4
E	9.9	174.9
1/4	10.1	174.7
cb	9.9	174.9
E	9.9	174.9
+15	9.9	174.9
	111' N	
-5	4.9	179.9
E	5.2	179.6
cb	5.2	179.6
1/4	5.2	179.6
E	5.5	179.3
1/4	5.6	179.2
cb	8.6	176.2
W	9.5	175.3
+12	10.0	174.8
	716.12 N = 5 line A.K.M. to width 12' chs. 25' W	
W	5.6	179.2
cb	5.6	179.2

184.78

FERGUS 11

1/4	5.5	179.3
E	5.3	179.5
1/4	5.2	179.6
cb	5.1	179.7
E	5.0	179.8
	S. cb	
E	5.3	179.5
cb	5.2	179.6
1/4	5.2	179.6
E	5.4	179.4
1/4	5.5	179.3
cb	5.6	179.2
W	5.6	179.2
	S 1/4	
W	5.7	179.1
cb	5.7	179.1
1/4	5.7	179.1
E	5.6	179.2
1/4	5.6	179.2
cb	5.6	179.2
E	5.4	179.4
	4 A.K.M.	
E	5.1	179.7
cb	5.3	179.5
1/4	5.4	179.4
E	5.5	179.3

184.78

1/4	5.6	179.2
cb	5.7	179.1
W	5.6	179.2
N. 1/4		
W	5.7	179.1
cb	5.5	179.3
1/4	5.3	179.5
E	5.2	179.6
1/4	5.3	179.5
cb	5.2	179.6
E	5.1	179.7
N. 1/4		
E	5.1	179.7
cb	5.4	179.4
1/4	5.4	179.4
E	5.4	179.4
1/4	5.3	179.5
cb	5.5	179.3
W	5.6	179.2
Sec A = N line		
W	5.8	179.0
cb	5.5	179.3
1/4	5.2	179.6
E	5.2	179.6
1/4	5.3	179.5
cb	5.3	179.5
E	5.4	179.4

184.78

FERGUS 12

Sec A = N line Akin on E 8.68 N of N. line on W - 00

E	5.4	179.4
cb	5.3	179.5
1/4	5.3	179.5
E	5.3	179.5
1/4	5.0	179.8
cb	5.3	179.5
W	5.8	179.0
15' N. of Sec B.		
W	5.5	179.3
cb	5.0	179.8
1/4	4.7	180.1
E	4.9	179.9
1/4	4.9	179.9
cb	4.8	180.0
E	4.6	180.2
40' N. of B		
E	2.7	182.1
cb	2.4	182.4
1/4	2.6	182.2
E	2.8	182.0
1/4	3.1	181.7
cb	3.3	181.5
W	3.0	181.8
70' N		
W	1.0	183.8
cb	0.9	183.9

184.78

1/4			1.1	183.7
e			0.9	183.9
1/4			0.7	184.1
eb			0.5	184.3
e			0.7	184.1
T.P.	12.85	197.42	0.01	184.77
		95'N		
e			12.1	185.5
eb			12.0	185.6
1/4			12.0	185.6
e			11.4	186.2
1/4			10.9	186.7
eb			10.2	187.4
w			9.6	188.0
		130'N		
w			4.6	191.0
eb			7.5	190.1
1/4			7.8	189.8
e			8.0	189.6
1/4			8.2	189.4
eb			8.3	189.3
e			8.5	189.1
		175'N		
e			4.2	193.4
eb			4.4	193.2
1/4			4.1	193.5

197.62

FERGUS

13

e			3.3	194.3
1/4			3.0	194.6
eb			2.8	194.8
w			2.6	195.0
		215'N		
w			0.0	197.6
eb			0.3	197.3
1/4			0.5	197.1
e			1.0	196.6
1/4			1.6	196.0
eb			1.7	195.9
e			1.9	195.7
T.P.	12.01	209.57	0.06	197.54
		255'N		
e			11.8	197.8
eb			12.0	197.6
1/4			12.0	197.6
e			12.2	197.4
1/4			11.8	197.8
eb			11.8	197.8
w			11.3	198.3
		300'N		
w			10.5	199.1
eb			10.3	199.3
1/4			10.5	199.1
e			10.5	199.1

209.57

1/4	10.5	199.1
cb	10.3	199.3
E	10.1	199.5
350' N.		
E	8.6	201.0
cb	8.7	200.9
1/4	8.6	201.0
C	8.6	201.0
1/4	8.5	201.1
cb	8.9	200.7
W	8.9	200.7
400' N.		
W	8.0	201.6
cb	7.7	201.9
1/4	7.5	202.1
e	7.4	202.2
1/4	7.1	202.5
cb	7.0	202.6
E	6.9	202.7
435'		
E	5.7	203.9
cb	5.7	203.9
1/4	5.8	203.8
C	6.1	203.5
1/4	6.0	203.6
cb	6.0	203.6
W	5.6	204.0

209.57

FERCUS

14

425' N.		
W	4.7	204.9
cb	4.7	204.9
1/4	4.4	205.2
C	3.9	205.7
1/4	3.3	206.3
cb	3.7	205.9
E	3.7	205.9
500' N.		
E	1.7	207.9
cb	1.7	207.8
1/4	1.6	208.0
C	1.8	207.8
1/4	2.0	207.6
cb	2.0	207.6
W	2.1	207.5
T.P.	13.05	222.40
	0.22	209.35
525' N.		
W	12.4	210.0
cb	13.0	209.4
1/4	12.9	209.5
E	12.7	209.7
1/4	12.8	209.6
cb	12.7	209.7
E	12.8	209.6

222.40

555' N

E	10.4	212.0
cb	10.1	212.3
1/4	10.3	212.1
C	10.3	212.1
1/4	10.3	212.1
cb	10.5	211.9
E	10.7	211.7

580' N

W	8.9	213.5
cb	8.8	213.6
1/4	9.2	213.2
C	9.1	213.3
1/4	9.2	213.2
cb	9.3	213.1
E	9.2	213.2

610' N

E	6.6	215.8
cb	7.0	215.4
1/4	7.1	215.3
C	7.0	215.4
1/4	7.0	215.4
cb	6.6	215.8
W	5.3	217.1

635' N

W	4.4	218.0
cb	5.1	217.3

222.40

FERGUS 15

1/4	5.2	217.2
E	5.3	217.1
1/4	5.1	217.3
cb	4.7	217.7
E	4.4	218.0

655' N

E	3.6	218.8
cb	3.2	219.2
1/4	3.5	218.9
C	3.5	218.9
1/4	3.5	218.9
cb	3.3	219.1
W	1.5	220.9

T.P.	13.06	735.24	0.18	222.22
		700' N.		
W			12.4	222.9
cb			12.6	222.7
1/4			12.6	222.7
E			12.9	222.4
1/4			13.2	222.1
cb			13.3	222.0
E			13.2	222.1

730' N

E	10.5	224.8
cb	10.7	224.6
1/4	10.7	224.6
C	10.2	225.1

235.28

1/4	9.9	225.4
cb	10.1	225.2
W	9.8	225.5
775' N		
W	6.8	228.5
cb	7.5	227.8
1/4	7.4	227.9
C	7.1	228.2
1/4	7.5	227.8
cb	7.6	227.7
E	7.3	228.0
820' N		
E	5.1	230.2
cb	5.2	230.1
1/4	5.5	229.8
C	5.8	229.5
1/4	6.2	229.1
cb	6.2	229.1
W	6.0	229.3
870' N		
W	3.8	231.5
cb	3.8	231.5
1/4	3.6	231.7
C	3.5	231.8
1/4	3.4	231.9
cb	3.5	231.8
E	3.5	231.8

235.78

FERGUS

16

900' N				
E		1.6	233.7	
cb		1.6	233.7	
1/4		1.6	233.7	
C		1.7	233.6	
1/4		2.0	233.3	
cb		2.2	233.1	
W		2.5	232.8	
T.P.	11.88	246.98	0.18	235.10
950' N				
W		11.0	236.0	
cb		11.3	235.7	
1/4		11.0	236.0	
C		10.6	236.4	
1/4		10.6	236.4	
cb		10.5	236.5	
E		10.3	236.7	
1000' S				
E		7.4	239.6	
cb		7.3	239.7	
1/4		7.3	239.7	
+C		8.0	239.0	
E		7.7	239.3	
1/4		7.6	239.4	
cb		8.7	238.3	
W		8.6	238.4	

246.98

1035' N.

17

W	6.4	240.6
cb	6.1	240.9
1/4	5.7	241.3
c	5.3	241.7
1/4	5.5	241.5
1/4	5.0	242.0
cb	5.0	242.0
E	4.9	242.1

1060' N

E	3.5	243.5
cb	2.9	244.1
1/4	2.5	244.5
1/6	3.4	243.6
c	3.4	243.6
1/4	4.2	242.8
cb	4.7	242.3
W	5.2	241.8

10855' N = S line Brooklyn

W	3.5	243.5
cb	2.9	244.1
1/4	2.7	244.3
c	2.4	244.6
1/4	2.6	244.4
1/4	2.0	245.0
cb	1.5	245.5
E	1.2	245.8

T.P. B.M. Nails

2.58 244.10

F.L.C. Field #33404
S.W. Brooklyn + Ferris

80' wide
14' chs
13' 2 1/2"

National Ave
2.5cc. 40' to 41' ST

3 1/2" / 25
mills

5. W 13' Mob
39 7/8" Florence

6994

699

18

B.M.	3.43	96.27	92.84	
T.P.	4.77	91.29	9.75	86.52
T.P.	1.62	81.23	11.58	79.71
T.P.	1.51	69.94	12.90	68.43
B.M.		7.54 (69.94)	65.40	Top Hydrant S.W. 40' National
W. Line 40' ST 60' wide 10' chs 10' 4"				
S		6.8	63.1 ✓	
cb		7.05	61.9 ✓	ancmt cb.
+1		7.5	64.1 ✓	
1/4		6.8	63.1 ✓	
c		6.3	63.6 ✓	
1/4		6.2	63.7 ✓	
+12		5.7	62.1 ✓	o
cb		5.00	62.9 ✓	ancmt cb
N		4.7	65.1 ✓	
W cb.				
N		5.0	62.9 ✓	
cb		5.7	62.1 ✓	
+1		6.3	63.6 ✓	
1/4		6.6	63.3 ✓	
c		6.6	63.3 ✓	
1/4		7.2	64.7 ✓	
+12		7.9	64.0 ✓	
cb		7.4	64.5 ✓	
S		7.2	64.7 ✓	

S	7.5	64.1 ✓
cb	7.7	64.1 ✓
+1	8.3	61.6 ✓
1/4	7.6	64.3 ✓
c	7.1	64.8 ✓
1/4	6.9	63.0 ✓
+12	6.6	63.3 ✓
cb	5.7	62.1 ✓
N	5.2	64.7 ✓
E		
N	5.3	62.1 ✓
cb	5.7	62.0 ✓
+2	7.1	64.8 ✓
1/4	7.2	64.7 ✓
c	7.4	64.5 ✓
1/4	8.0	61.9 ✓
+12	8.9	61.0 ✓
cb	8.0	61.9 ✓
S	8.1	61.8 ✓
E 1/4		
S	8.6	61.3 ✓
cb	8.6	61.3 ✓
+2	7.6	60.3 ✓
1/4	8.4	61.5 ✓
c	7.7	64.1 ✓
1/4	7.3	64.1 ✓

69.94

(69.9)

+12	7.5	62.2 ✓
cb	6.7	63.4 ✓
N	5.3	64.6 ✓
E. CB		
N	5.4	64.5 ✓
cb	7.5	64.4 ✓
+1	7.9	64.0 ✓
1/4	7.7	64.4 ✓
C	8.0	61.9 ✓
1/4	8.6	61.5 ✓
cb	9.7	60.4 ✓
S	11.2	58.7 ✓
00 = E. LHC 40 ⁺⁺ ST		
S	10.3	59.6 ✓
cb	9.0	60.9 ✓
1/4	8.9	61.0 ✓
C	8.2	61.7 ✓
1/4	8.1	61.8 ✓
+12	8.1	61.8 ✓
cb	7.4	62.5 ✓
N	6.4	63.1 ✓
30' E		
N	8.0	61.9 ✓
cb	8.4	61.5 ✓
+2	9.6	60.3 ✓
1/4	9.5	60.4 ✓

69.94

National 19

(69.9)

C	9.3	60.6 ✓
1/4	10.1	59.8 ✓
cb	10.8	59.1 ✓
S	11.8	58.1 ✓
T.P.	7.30	60.99
		11.25
		58.69
		70.8
		(61.0)
S	4.6	56.2 ✓
cb	3.3	57.7 ✓
1/4	3.0	58.0 ✓
C	2.4	58.6 ✓
1/4	2.1	58.9 ✓
+11	2.2	58.8 ✓
cb	1.0	60.0 ✓
N	0.4	60.6 ✓
100' E		
N	3.2	57.8 ✓
cb	3.1	57.9 ✓
+2	4.2	56.8 ✓
1/4	4.2	56.8 ✓
C	4.4	56.6 ✓
1/4	4.8	56.4 ✓
cb	5.7	55.3 ✓
S	6.3	54.7 ✓
150' E		
1/4	7.4	51.2 ✓
S	9.3	51.7 ✓
cb	8.3	54.7 ✓

60.99

	61.0	
+10	7.4	53.6 ✓
1/4	7.5	53.5 ✓
C	7.0	54.0 ✓
1/4	7.2	53.8 ✓
cb	7.5	53.5 ✓
N	7.3	53.7 ✓

175' N.

-10	12.5	48.5 ✓
N	11.1	49.9 ✓
cb	8.6	52.4 ✓
1/4	8.0	53.0 ✓
C	8.0	53.0 ✓
1/4	8.5	52.5 ✓
+7	8.8	52.2 ✓
cb	13.0	48.0 ✓
+4	14.9	46.1 ✓
S	15.8	45.2 ✓
+15	16.9	44.1 ✓

198'E

-15	16.8	44.1 ✓
S	15.7	45.3 ✓
+6	15.4	45.2 ✓
cb	13.0	48.0 ✓
+7	9.2	51.8 ✓
1/4	9.0	52.0 ✓
C	8.5	52.5 ✓

60.99

National 20

	61.0	
1/4	8.6	52.4 ✓
cb	8.8	52.2 ✓
+8	11.9	49.1 ✓
N	12.1	48.9 ✓
+10	10.6	50.2 ✓

212'E

N	6.8	52.4 ✓
+1	7.0	52.0 ✓
+3	9.0	52.0 ✓
cb	9.2	51.8 ✓
1/4	9.1	51.9 ✓
C	9.1	51.9 ✓
1/4	9.4	51.6 ✓
cb	9.8	51.2 ✓
S	10.4	50.6 ✓

230'E

S	10.2	50.8 ✓
20	10.1	50.9 ✓
1/4	9.6	51.2 ✓
C	9.4	51.6 ✓
1/4	9.4	51.6 ✓
+12	9.4	51.6 ✓
cb	8.5	52.5 ✓
+12	8.4	52.6 ✓
N	5.3	55.2 ✓

60.99

265' E

61.0

N	6.2	51.8 ✓
+1	6.3	51.7 ✓
+3	8.9	51.1 ✓
cb	9.6	51.6 ✓
+1	10.2	50.8 ✓
1/4	10.4	50.6 ✓
c	10.3	50.7 ✓
1/4	10.6	50.6 ✓
cb	10.9	50.2 ✓
+3	10.5	50.5 ✓
s	11.0	50.0 ✓

300' E

s	11.9	49.2 ✓
+11	11.7	49.8 ✓
cb	12.1	48.9 ✓
1/4	11.5	49.5 ✓
c	11.1	49.9 ✓
1/4	11.1	49.9 ✓
+10	11.3	49.7 ✓
cb	10.3	50.7 ✓
+10	9.8	51.2 ✓
+12	6.5	51.5 ✓
N	6.5	51.5 ✓

330' E

N	6.5	50.5 ✓
+2	6.5	50.5 ✓

60.99

National 21

61.0

+4	10.0	51.0 ✓
cb	10.9	50.1 ✓
+1	12.1	48.9 ✓
1/4	12.1	48.9 ✓
c	12.2	48.8 ✓
1/4	12.5	48.5 ✓
cb	12.8	48.1 ✓
+3	12.6	48.4 ✓
s	13.2	47.8 ✓
T.P	320 52.02	12.17 48.82

355' E

s	54.0	5.8 46.2 ✓
+11	5.2	46.8 ✓
cb	5.2	46.9 ✓
1/4	4.6	47.4 ✓
c	4.7	47.8 ✓
1/4	4.1	47.9 ✓
+11	4.1	47.9 ✓
cb	2.6	49.0 ✓
+9	2.4	49.6 ✓
+12	0.0	-
N	0.0	-

300' E

N	4.6	47.4 ✓
cb	6.1	45.9 ✓
1/4	6.7	45.3 ✓

52.02

		52.0	
C		6.9	451 ✓
1/4		6.9	451 ✓
cb		7.5	445 ✓
S		8.0	460 ✓
	450.2		
S		10.1	419 ✓
cb		10.2	418 ✓
1/4		9.4	426 ✓
C		9.2	428 ✓
1/4		9.3	427 ✓
+7		9.1	429 ✓
cb		8.4	436 ✓
N		8.1	439 ✓
	580.2		
N		10.2	418 ✓
cb		10.9	411 ✓
+8		11.1	409 ✓
+10		11.8	402 ✓
1/4		11.8	402 ✓
e		11.6	404 ✓
1/4		11.8	404 ✓
cb		12.1	399 ✓
S		12.3	397 ✓
	530.2		
S		14.2	378 ✓
cb		13.3	387 ✓

Dist Floor
Garage

52.02

National

27

		52.0	
1/4		13.3	387 ✓
e		13.4	386 ✓
+10		13.6	384 ✓
1/4		13.2	388 ✓
+5		12.2	398 ✓
cb		11.9	401 ✓
1/4		11.5	405 ✓
T.P.	111	40.34	12.79 39.23
		545.2	40.3
N		0.0	F
cb		0.8	38.5 ✓
+8		1.2	39.1 ✓
1/4		2.6	37.7 ✓
e		2.7	37.8 ✓
1/4		2.8	37.5 ✓
+8		3.4	36.9 ✓
cb		5.0	35.3 ✓
S		7.8	32.5 ✓
+10		9.6	30.2 ✓
	565.2		
-15		13.3	47.0 ✓
S		12.5	47.8 ✓
+8		11.5	48.8 ✓
cb		8.8	31.5 ✓
+8		4.6	35.7 ✓
1/4		4.7	35.6 ✓

40.34

40.3

c

c	4.5	358 ✓
+10	4.0	365 ✓
14	2.7	376 ✓
+2	1.9	384 ✓
cb	1.6	387 ✓
N	0.6	392 ✓

5.80' E

N	1.0	393 ✓
+3	1.8	385 ✓
cb	2.3	380 ✓
+4	2.3	380 ✓
14	4.1	367 ✓
+3	5.6	347 ✓
c	5.9	344 ✓
14	5.9	344 ✓
+5	6.5	338 ✓
cb	10.6	292 ✓
+5	13.0	273 ✓
S	13.2	271 ✓
+15	13.4	269 ✓

600' E = W. Line 4185 ST

-15	13.5	268 ✓
S	13.4	269 ✓
+12	13.1	272 ✓
cb	12.3	280 ✓
+11	7.8	305 ✓

40.34

National

23

40.3

14	7.8	305 ✓
c	7.8	305 ✓
14	7.7	306 ✓
+8	5.4	348 ✓
cb	3.1	372 ✓
N	3.3	370 ✓

60' wide
10' chs
10' W

Upas St

X Sec from E. Line Arizona to W. Line Louisiana

3/21/25
P.M.

B.M.B.P. 5.42

278.80

273.38

S.E. Arizona
+ M.V.H.C.

E. Line Arizona 60' wide 10' chs 10' W

N.	8.9	✓ 269.9
cb	8.5	✓ 270.3
1/4	8.4	✓ 270.2
E	8.2	✓ 270.6
1/4	8.0	✓ 270.8
cb	7.8	✓ 271.0
S	7.7	✓ 271.1
	E ch	
S	7.8	✓ 271.0
cb	8.0	✓ 270.8
1/4	8.1	✓ 270.7
E	8.3	✓ 270.5
1/4	8.4	✓ 270.2
cb	8.8	✓ 270.0
N	9.9	✓ 268.9
	9.86	✓ 268.9
		one mt cb
	6' W of E ch	
N	9.8	✓ 269.0
cb	9.4	✓ 269.4
1/4	9.1	✓ 269.7
E	8.8	✓ 270.2
1/4	8.7	✓ 270.1
cb	8.4	✓ 270.4
S	8.2	✓ 270.6

278.80

24

Arizona

S	8.1	✓ 270.7
cb	8.1	✓ 270.7
1/4	8.2	✓ 270.6
E	8.4	✓ 270.4
1/4	8.7	✓ 270.1
cb	9.1	✓ 269.7
N	9.3	✓ 269.5
	W. ch	
	8.9	✓ 269.9
	8.86	✓ 269.9
		one mt cb
N	8.7	✓ 270.1
cb	8.7	✓ 270.1
1/4	8.6	✓ 270.2
E	8.5	✓ 270.3
1/4	8.3	✓ 270.5
cb	8.0	✓ 270.8
S		
	00 = W. Line Arizona	
S	7.5	✓ 271.3
cb	7.8	✓ 271.0
1/4	7.9	✓ 270.9
E	8.2	✓ 270.6
1/4	8.2	✓ 270.6
cb	8.3	✓ 270.5
N	8.4	✓ 270.4
	5' W.	
N	7.9	✓ 270.9
cb	8.0	✓ 270.8

278.80

278.8

1/4	7.8	271.0 ✓
e	7.7	271.1 ✓
1/4	7.6	271.2 ✓
eb	7.3	271.5 ✓
S	7.3	271.5 ✓

8' W

S	7.1	271.7 ✓
eb	6.9	271.9 ✓
1/4	6.4	272.4 ✓
C	6.5	272.3 ✓
1/4	6.7	272.1 ✓
eb	6.7	272.1 ✓
N	6.9	271.9 ✓

35' W

N	6.0	272.8 ✓
eb	5.9	272.9 ✓
1/4	5.5	273.3 ✓
C	5.5	273.3 ✓
1/4	5.2	273.6 ✓
eb	5.7	273.1 ✓
S	5.8	273.0 ✓

45' W

S	4.5	274.3 ✓
eb	4.4	274.4 ✓
1/4	3.9	274.9 ✓
C	4.4	274.8 ✓

278.8

Upas

25

1/4	4.7	274.1 ✓
eb	4.9	273.9 ✓
N	5.2	273.6 ✓

100' W

N	3.6	275.2 ✓
eb	3.4	275.4 ✓
1/4	3.3	275.5 ✓
C	3.1	275.7 ✓
1/4	3.0	275.8 ✓
eb	3.1	275.7 ✓
S	3.1	275.7 ✓

135' W

S	1.4	277.0 ✓
eb	1.8	277.0 ✓
1/4	1.5	277.3 ✓
C	1.5	277.3 ✓
1/4	1.8	277.0 ✓
eb	1.6	277.2 ✓
N	1.7	277.1 ✓
T.P.	6.66	284.37
	1.09	277.71

165' W

N	4.6	279.8 ✓
eb	4.9	279.5 ✓
1/4	5.2	279.2 ✓
C	5.3	279.1 ✓
1/4	5.4	279.0 ✓

-eb

284.37

284.4

cb 5.9 278.6V

S 5.7 279.7V

200' W

S 4.6 279.8V

cb 4.4 280.0V

1/4 4.1 280.3V

C 3.7 280.7V

1/4 3.5 280.9V

cb 3.4 281.0V

N 3.1 281.3V

240' W

N 2.9 281.5V

cb 3.1 281.3V

1/4 3.2 281.2V

C 3.5 280.9V

1/4 3.9 280.5V

cb 4.1 280.3V

S 4.2 280.2V

60' wide 10' obs'd by R 75' W = E. line Texas

S 4.2 280.2V

cb 4.0 280.4V

1/4 3.8 280.6V

C 3.8 280.6V

1/4 3.7 280.7V

cb 3.6 280.8V

N 3.3 281.1V

284.37

Upas ST 26

E. cb

284.4

N 3.37 280.7V No yardage
except cb

N 3.8 280.6V

cb 3.9 280.5V

1/4 3.7 280.7V

C 3.5 280.9V

1/4 3.6 280.8V

cb 3.9 280.5V

S 4.0 280.4V

E Texas

S 3.8 280.6V

cb 3.6 280.8V

1/4 3.3 281.1V

C 3.4 281.0V

1/4 3.5 280.9V

cb 3.8 280.6V

N 4.0 280.4V

W. cb

N 4.4 280.0V No yardage
except cb

N 4.8 279.6V

cb 4.3 280.1V

1/4 3.7 280.7V

C 3.2 281.2V

1/4 3.3 281.1V

cb 3.6 280.8V

S 3.8 280.6V

284.37
000 W Line Texas 284.4

S	3.9	280.3 V
cb	3.7	280.7 V
1/4	3.4	281.0 V
C	3.2	281.2 V
+44	3.2	281.2 V
+6	3.4	281.0 V
+9	4.2	280.2 V
cb	4.2	280.2 V
+5	4.9	279.5 V
N	4.1	280.3 V
5' W.		
N.	3.4	281.0 V
+4	5.1	279.3 V
+6	4.4	280.0 V
cb	4.3	280.1 V
+4	3.2	281.2 V
1/4	3.3	281.1 V
C	3.3	281.1 V
1/4	3.5	280.9 V
cb	3.8	280.6 V
S	4.1	280.3 V
35' W.		
S	4.7	279.7 V
cb	4.3	280.1 V
1/4	4.1	280.3 V
C	3.7	280.7 V

284.37 UPAS 27

284.4

1/4	3.9	280.5 V
+7	4.2	280.2 V
cb	5.2	279.2 V
+8	5.4	279.0 V
N	4.4	280.0 V
65' W.		
N	5.3	279.1 V
cb	5.4	279.0 V
1/4	4.7	279.7 V
C	4.4	280.0 V
1/4	4.4	280.0 V
cb	5.0	279.4 V
S	5.4	279.0 V
90' W.		
S	5.1	279.3 V
cb	5.4	279.0 V
1/4	4.9	279.5 V
C	4.7	279.7 V
1/4	5.0	279.4 V
cb	5.5	278.9 V
+5	6.0	278.4 V
N	5.5	278.9 V
125' W.		
N	5.7	278.7 V
cb	5.8	278.6 V
1/4	5.2	279.2 V

284.37

284.4

c	5.0	279.4 ✓
1/4	5.1	279.3 ✓
cb	5.9	278.5 ✓
s	6.1	278.3 ✓
150' W		
s	4.1	278.3 ✓
cb	5.9	278.5 ✓
1/4	5.6	278.8 ✓
c	5.5	278.9 ✓
1/4	5.4	279.0 ✓
cb	5.7	278.7 ✓
+4	5.9	278.5 ✓
1/1	5.7	278.7 ✓
175' W		
N	5.2	279.2 ✓
+3	6.3	278.1 ✓
cb	6.1	278.3 ✓
+3	5.4	279.0 ✓
1/4	5.2	279.2 ✓
c	5.2	279.2 ✓
1/4	5.3	279.1 ✓
cb	5.7	278.7 ✓
s	6.3	278.1 ✓
200' W		
s	6.3	278.1 ✓
cb	6.1	278.3 ✓

284.37

284.4

2pas 28

1/4	5.3	279.1 ✓
c	5.2	279.2 ✓
1/4	5.3	279.1 ✓
+8	5.4	279.0 ✓
cb	6.0	278.4 ✓
+8	6.5	277.9 ✓
N	5.2	279.2 ✓
235' W		
N	5.6	278.8 ✓
+2	6.7	277.7 ✓
cb	6.3	278.1 ✓
+2	5.6	278.8 ✓
1/4	5.7	278.7 ✓
c	5.3	279.1 ✓
1/4	5.8	278.6 ✓
cb	6.4	277.8 ✓
s	6.7	277.7 ✓
273.4' W = E Line Louisiana 40' wide 10' cbs 10' W		
s	6.9	277.5 ✓
cb	6.6	277.8 ✓
1/4	6.5	277.9 ✓
c	6.5	277.9 ✓
1/4	6.4	278.0 ✓
cb	6.7	277.7 ✓
+8	7.2	277.2 ✓
N	6.2	278.2 ✓

28437

E. CB

284.4

N	6.42	278.0	no yardage on ent. cb.
N	6.6	277.8 ✓	
cb	6.8	277.6 ✓	
1/4	6.7	277.7 ✓	
c	6.6	277.8 ✓	
1/4	6.7	277.7 ✓	
cb	6.8	277.6 ✓	
S	6.9	277.5 ✓	
S	7.0	277.4 ✓	
cb	7.0	277.4 ✓	
1/4	6.8	277.6 ✓	
c	6.9	277.5 ✓	
1/4	6.8	277.6 ✓	
cb	6.7	277.7 ✓	
N	6.6	277.8 ✓	

W. CB

7.0

6.95

277.4 ✓

no yardage
on ent. cb

N	7.3	277.1 ✓	on ground
cb	7.4	277.0 ✓	
1/4	7.5	276.9 ✓	
c	7.5	276.9 ✓	
1/4	7.4	277.0 ✓	
cb	7.3	277.1 ✓	
S	7.0	277.4 ✓	

28437

W. Line Louisiana

284.4

UPAS

29

S	7.2	277.2 ✓	
cb	7.3	277.1 ✓	
1/4	7.4	277.0 ✓	
c	7.8	276.6 ✓	
1/4	7.8	276.6 ✓	
cb	7.2	277.2 ✓	
N	7.2	277.2 ✓	
		278.0	
T.P.	3.93	R 81.88	6.42
			277.95
chkan B.M. B.P.	5.36	276.52	= 276.50

N.E. Myrtle

Louisiana

s/sols Moore

Cross Section of Flaxia
UNA to Wodenic60' wide
14' abo
13' 1/2'

1945

30

onse Hub Bndt
UNA

5.80

1945'

13.65

25' w of WL of UNA

-10	13.0	6.4
S	12.8	6.6
cb	12.8	6.6
1/4	12.7	6.7
e	12.5	6.9
1/4	12.6	6.8
cb	12.8	6.6
N	13.0	6.4
+10	12.8	6.6

WL of UNA =

60' wide

-10	12.4	7.0	10' abo
N	12.5	6.9	10' 1/2'
cb	12.6	6.8	
1/4	12.0	7.4	
e	11.6	7.8	
1/4	12.0	7.4	
cb	12.5	6.9	
S	12.8	6.6	

w/cb

S	12.1	7.3
cb	11.7	7.7
1/4	11.5	7.9
e	11.4	8.0
1/4	11.6	7.8

cb	12.2	7.7
N	12.3	7.1
+10	12.3	7.1

+5

-10	12.3	7.1
N	12.3	7.1
cb	12.1	7.3
1/4	11.4	8.0
e	11.3	8.1
1/4	11.2	8.2
cb	11.1	8.3
S	11.7	7.7

w 1/4

S	8.7	10.7
cb	10.3	9.1
1/4	10.7	8.7
e	11.9	8.4
1/4	11.0	8.4
cb	11.9	7.5
N	12.1	7.3
+10	12.2	7.2

-10	12.0	7.4
N	11.9	7.5
cb	12.0	7.4
+6	11.6	7.8

1945

+8		10.4	9.0
1/2		10.3	9.1
e		10.3	9.1
1/4		9.5	9.9
cb		9.3	10.1
S		8.3	11.1 -
	E 1/4		
S		7.3	12.1 -
cb		8.2	11.4
+7		8.5	10.9
+8		9.8	9.6
1/4		10.2	9.4
+3		10.1	9.3
+5		9.1	10.3
c		9.4	10.0
1/2		9.6	9.8
+4		10.1	9.3
+6		11.4	8.0
cb		11.6	7.8
N		11.8	7.6 -
+10		11.9	7.5
	+5		
-10		11.7	7.7
N		11.7	7.7 -
cb		11.4	8.0
+6		11.3	8.1

1945

HCHSIA

31

+9		9.2	10.4
1/4		9.0	10.4
c		8.8	10.6
1/4		8.2	11.4
+4		8.2	11.4
+5		9.2	10.4
+9		9.3	10.1
+11		7.7	11.7
cb		7.3	12.1
S		7.2	12.4 -
	E cb		
S		7.1	12.3 -
cb		6.9	12.5
+4		7.0	12.4
1/2		7.7	11.7
c		8.3	11.1
1/4		8.5	10.9
+4		8.9	10.5
+6		10.9	8.5
cb		11.0	8.4
N		11.7	7.7 -
+10		11.7	7.7
	EL of WNA St = 0+00		
-10		11.5	7.9
N		11.4	8.0 -
cb		10.7	8.7

19.45

+6	9.0	104
1/4	7.5	119
C	6.9	145
1/4	6.0	134
CB	6.7	147
S	6.4	13.0 -
17' E'		
S	1.2	18.2 -
cb	3.1	16.3
+6	3.6	15.8
+7	5.5	13.9
+9	4.6	14.8
1/4	4.4	15.0
C	4.4	15.0
+1	5.2	14.4
+2	6.8	12.6
1/4	4.6	14.8
+8	5.3	13.1
cb	6.9	12.5
N	10.1	9.3 -
+10	10.4	9.0
39' E'		
-10	5.0	14.4
N	1.8	17.6 -
cb	0.4	19.0
+6	0.5	18.9

19.45

FICASIA 32

+9	1.6	17.8
1/4	1.7	17.7
C	1.6	17.8
1/4	1.1	18.3
+6	2.3	17.1
T.P.	10.34	28.64 ✓ 1.15
+10	7.9	20.7
cb	7.9	20.7
S	7.7	20.9 -
50' E		
S	7.1	21.5 -
cb	7.1	21.5
+5	7.0	21.6
+7	10.5	18.1
+8	10.5	18.1
+9	9.3	19.3
1/4	9.1	19.5
C	9.6	19.0
1/4	9.6	19.0
+7	8.4	20.2
cb	8.1	20.5
N	8.4	20.2 -
60' E		
N	8.0	20.6 -
cb	7.2	21.4
+3	7.3	21.3

2864

+9	9.0	19.6
1/4	8.9	19.7
c	8.8	19.8
1/4	8.5	20.1
+5	8.8	19.8
+9	6.6	22.0
cb	6.7	21.9
S	7.0	21.6 -
75' E		
S	6.5	22.1 -
cb	6.2	22.4
+5	6.3	22.3
+7	8.3	20.3
1/4	8.0	20.6
c	7.9	20.7
1/4	8.1	20.5
+7	8.2	20.4
+11	6.5	22.1
cb	6.4	22.2
N	7.0	21.6 -
100' E		
N	6.2	22.4 -
cb	6.0	22.6
+3	5.8	22.8
+7	7.8	20.8
1/4	7.6	21.0

2864

FICAFIA 33

c	7.0	21.6
1/4	7.3	21.3
+7	7.7	20.9
+9	6.0	22.6
cb	6.0	22.6
S	6.1	22.5 -
150' E		
S	5.7	22.9 -
cb	5.6	23.0
+5	5.7	22.9
+6	6.8	21.8
1/4	6.6	22.0
c	6.2	22.4
1/4	6.6	22.0
+7	6.7	21.9
+11	5.5	23.1
cb	5.5	23.1
N	5.7	22.9 -
200' E		
N	5.2	23.4 -
cb	5.3	23.3
+6	5.4	23.2
+7	6.1	22.5
1/4	6.2	22.4
c	5.9	22.7
1/4	6.3	22.3

286H

+7	6.4	77.7
+10	5.6	73.0
cb	5.5	73.1
S	5.5	73.1 -
225' E		
S	5.1	73.5 -
cb	5.0	73.6
+5	5.1	73.5
+6	6.3	77.3
1/4	5.8	77.8
c	5.5	73.1
1/4	5.8	77.8
+7	5.5	73.1
+8	4.7	73.9
cb	5.1	73.5
N	5.2	73.4 -
250' E		
N	6.1	77.5 -
cb	5.1	73.5
+5	4.7	73.9
+7	5.6	73.0
1/4	5.5	73.1
c	5.2	73.4
1/4	5.5	73.1
+7	6.2	77.4
+9	4.8	73.9

286H

FCA CIA 34

cb	4.8	73.8
S	4.8	73.8 -
275' E		
S	4.9	73.7 -
cb	4.8	73.8
+4	5.0	73.6
+6	6.0	77.6
1/4	5.5	73.1
c	5.4	73.7
1/4	6.0	77.6
cb	6.0	77.6
N	7.5	77.1 -
300' E		
N	8.0	70.6 -
cb	7.1	77.5
1/4	6.1	77.5
c	5.6	73.0
1/4	5.6	73.0
+9	5.9	77.7
+10	5.1	73.5
cb	5.0	73.6
S	4.9	73.7 -
319.1' E = well at 3846 on N. 80' wide		
S	4.8	73.8 10' cb
cb	4.6	74.0 13' 1/4
+3	5.0	73.6

2864

+2	7.0	71.6
+7	7.8	70.8
+11	5.8	77.8
1/2	5.5	73.1
c	5.0	73.6
1/4	5.1	73.5
+7	5.2	73.7
+9	4.5	74.1
cb	3.6	75.0
S	3.6	75.0 -
	E 1/4	
S	3.0	75.6 -
cb	3.0	75.6
+4	3.1	75.5
+5	4.8	73.8
1/2	4.7	73.9
c	4.4	74.1
1/4	4.7	73.9
cb	4.6	74.0
N	4.8	73.8 -
	E cb	
N'	4.4	74.1 -
cb	4.1	74.5
1/2	4.1	74.5
c	3.8	74.8
1/2	4.1	74.5

2864

FCH & I.A. 36

+8	4.3	74.3
+9	2.5	76.1
cb	2.4	76.1
S	2.4	76.1 -
	+6	
N 1/2	3.9	74.7
cb	4.1	74.5
N'	4.6	74.0 -
	+7	
N'	3.2	75.4 -
cb	3.4	75.4
+6	5.3	73.3
+8	4.2	74.4
N 1/4	3.9	74.7
	EL of 38th. to N = 00.00	
S	2.2	76.4 -
cb	2.1	76.5
+4	2.3	76.3
+5	3.6	75.0
1/2	3.6	75.0
c	3.0	75.6
1/4	3.5	75.1
+5	3.5	75.1
+7	4.5	74.1
+11	4.9	73.7
+12	2.4	76.1
cb	2.2	76.1

28.64

N	2.6	26.0 -
25° E		
N	0.7	27.9 -
cb	0.5	28.1
+2	0.5	28.1
+3	3.8	24.8
+6	3.7	24.9
+7	2.8	25.8
1/2	2.6	26.0
C	2.2	26.4
1/2	2.5	26.1
+5	3.7	24.9
+9	3.0	25.6
+10	1.7	26.9
cb	1.5	27.1
S	1.7	26.9 -
75° E		
S	1.3	27.3 -
cb	1.2	27.4
+5	1.3	27.3
+6	2.9	25.7
+8	3.4	25.2
+9	2.3	26.3
1/2	2.0	26.6
C	1.2	27.4
1/2	1.4	27.1

28.64

FCHS 17 37

+7	2.2	26.4
cb	0.0	28.6
T.P.	9.54	37.85 ✓
N	0.33	28.31
	8.7	29.1 -
125° E		
N	8.6	29.4 -
cb	8.9	28.9
+6	10.1	27.7
1/2	10.1	27.7
C	9.9	27.9
1/2	10.5	27.3
+8	11.2	26.6
+9	10.2	27.6
cb	10.3	27.5
S	10.7	27.1 -
175° E -		
S	10.0	27.8 -
cb	9.5	28.3
+8	10.2	27.6
1/2	9.6	28.7
C	9.2	28.6
1/2	9.3	28.5
+8	9.7	28.1
+9	8.6	29.4
cb	8.3	29.5
N	7.9	29.9 -

37.85

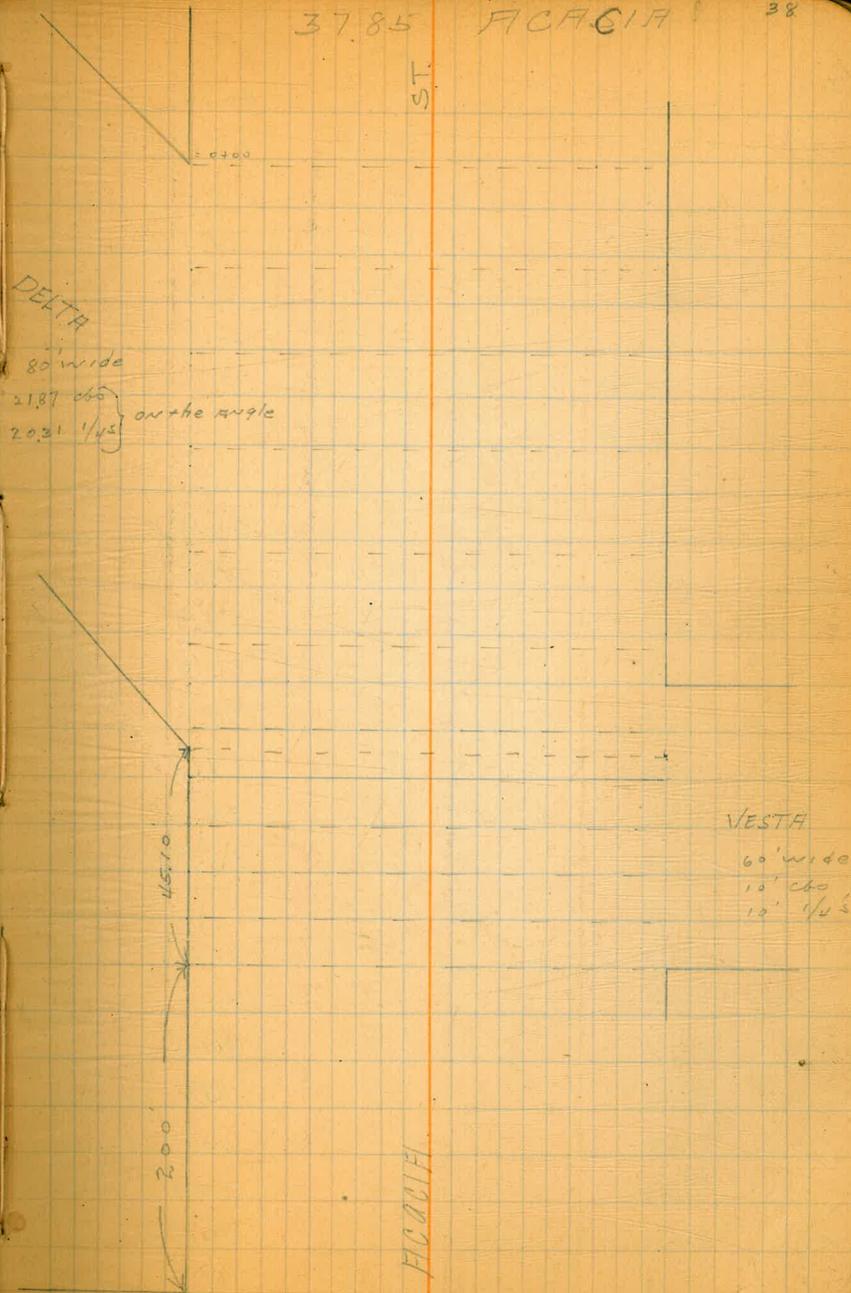
200' E = W/L of Vesta to South

N		7.5	30.3	-
db		7.9	29.9	
+3		8.2	29.6	
+5		9.0	28.8	
1/4		8.7	29.1	
c		8.6	29.2	
1/4		9.6	28.7	
+7		9.6	28.7	
+8		9.2	28.6	
db		9.3	28.5	
S		9.5	28.3	-
check B.M. spike	Vesta + Hicacia	7.69	30.16	30.17
W/L of Vesta				
S		9.2	28.6	-
db		9.2	28.6	
1/4		9.3	28.5	
c		8.4	29.4	
1/4		8.6	29.2	
+10		8.5	29.3	
+11		8.0	29.8	
cb		7.7	30.1	
N		7.4	30.4	-
W/L of Vesta				
N		6.9	30.9	-
+10		7.3	30.5	

37.85

FICACIA

38



38+h

37.85

cb	7.8	30.0
+8	8.3	29.5
1/4	8.1	29.7
e	8.1	29.7
1/4	8.8	29.0
cb	9.2	28.6
S	9.2	28.6

E. of Vesta to South

S	8.8	29.0
cb	9.3	28.5
+7	9.3	28.5
1/4	8.6	29.4
e	7.8	30.0
1/4	7.8	30.0
+8	8.1	29.7
cb	7.1	30.7
N	6.5	31.3

E. 1/4 of Vesta to S

N	6.1	31.7
cb	6.4	31.6
+2	6.4	31.4
+4	7.4	30.4
+11	7.6	30.2
1/4	7.4	30.4
e	7.6	30.2
1/4	8.1	29.7

37.85

FCH&IA 39

+4	8.1	29.7
+7	9.0	28.8
+10	8.2	29.6
cb	8.2	29.4
S	8.5	29.3

+5 = NL of DELTA ST

S	8.4	29.4
cb	8.0	29.8
+5	8.1	29.7
+6	8.7	29.1
+9	8.7	29.1
+10	8.1	29.7
1/4	7.8	30.0
e	7.6	30.4
1/4	7.2	30.6
+2	7.0	30.8
+2	7.7	30.1
+10	7.6	30.4
cb	6.1	31.7
N	5.5	32.3

E. 1/4 of Vesta to South

N	4.9	32.9
cb	5.7	32.1
+4	6.1	31.7
+5	7.4	30.4
+8	7.5	30.3

37.85

+9	7.0	30.8
1/4	6.9	30.9
c	7.3	30.5
1/4	7.6	30.7
+5	8.1	29.7
+6	8.8	29.0
+8	8.6	29.1
+9	7.6	30.4
cb	7.6	30.1
S	8.0	29.8 -

EL of Vesta to S

S	7.9	29.9 -
cb	7.7	30.1
+3	7.2	30.6
+5	8.2	29.6
1/4	7.3	30.5
c	6.7	31.1
1/4	6.4	31.4
+8	6.4	31.4
cb	7.0	30.8
tr	4.9	32.9
N	4.0	33.8 -

Ncb of DELTA

N	3.6	32.7 -
+5	4.0	33.8
+10	7.0	30.8
+11	7.0	30.8

37.85

FICACIA

40

cb	6.3	31.5
1/4	6.1	31.7
c	6.4	31.4
1/4	7.1	30.7
+2	8.1	29.7
+10	7.5	30.3
cb	7.6	30.4
S	7.7	30.1 -

+6

Ncb	5.6	32.2
+8	6.0	31.8
+10	6.4	31.4
+11	5.1	32.7
+13	4.6	33.2
N	3.2	34.6 -

+10

N	5.4	32.4 -
+3	5.5	32.3
Ncb	5.2	32.6

N 1/4 of DELTA

S	7.2	30.6 -
cb	6.9	30.9
+5	6.9	30.9
+6	7.8	30.0
+8	7.8	30.0
1/4	6.9	30.9

3785

c	5.8	340
1/4	5.2	346
cb	4.5	333
N	4.2	336 -

E of DELTA

N'	2.8	350 -
cb	3.6	344
1/4	4.6	337
c	5.1	327
1/4	6.5	313
+7	7.4	304
+9	6.4	314
cb	6.7	311
S	6.9	309 -

S 1/2 of DELTA

S	6.1	309 -
cb	6.5	313
+4	6.2	316
+6	6.9	309
1/4	5.6	344
c	4.7	331
1/4	4.2	336
+6	4.8	330
+10	3.5	343
cb	4.1	337
+4	3.1	347

3785

ACACIA 41

N	2.3	35.5 -
+17		
N	2.8	35.0 -
+1	1.9	35.9
cb	2.9	34.9
+4	3.3	34.5
+8	5.1	34.7
+11	4.3	33.5
1/4	4.2	33.6
C	4.4	33.4

S of DELTA

N	1.7	361 -
cb	2.9	349
+4	3.2	346
+7	5.0	348
1/4	4.3	33.5
c	4.4	33.4
1/4	5.5	32.3
+8	6.6	31.4
+9	5.8	31.0
cb	5.8	31.0
S	5.9	31.9 -

SL of DELTA = 0400

S	4.9	34.9 -
cb	5.2	34.6
+5	5.2	34.6

3785

tb		5.9	31.9
1/4		5.0	31.8
c		4.1	33.7
1/4		4.1	33.7
+7		4.6	33.7
+9		3.3	34.5
cb		2.8	35.0
N		1.9	35.9
ON BM	10.50	40.67	30.17
	25' E		
N		4.6	36.1
cb		5.5	35.7
+4		5.7	35.0
+8		7.3	33.4
1/4		6.7	34.0
e		6.4	34.3
1/4		7.4	33.3
+7		8.0	32.7
+8		7.2	33.5
cb		7.5	33.4
S		7.5	33.4
	50' E		
S		6.9	33.8
cb		6.7	34.0
+5		6.6	34.1
+6		7.3	33.4

ACACIA +
Vesta

40.67

ACACIA 42

1/4		6.5	34.4
c		5.8	34.9
1/4		6.1	34.6
+7		6.8	33.9
+9		5.5	35.4
cb		5.2	35.5
N		4.7	36.0
	75' E		
N		4.5	36.7
cb		4.8	35.9
+4		4.8	35.9
+5		6.2	34.5
1/4		5.4	35.3
c		5.0	35.7
1/4		5.9	34.8
+7		7.0	33.7
+8		6.2	34.5
cb		6.4	34.3
S		6.8	33.9
	125' E		
S		6.5	34.7
cb		5.8	34.9
+5		5.4	35.3
+6		6.3	34.4
1/4		5.6	35.1
c		4.6	36.1

4067

1/2	4.8	35.9
+6	5.2	35.5
+8	5.7	35.0
+9	5.2	35.5
+10	4.2	36.5
cb	4.3	36.4
N	4.0	36.7 -

175° E

N	3.6	37.1 -
cb	3.9	36.8
+2	3.9	36.8
+4	5.0	35.7
+8	4.4	36.3
1/4	4.3	36.4
c	4.1	36.6
1/4	4.9	35.8
+7	5.7	35.0
+8	4.8	35.9
cb	5.1	35.6
S	5.5	35.4 -

200° E

S	5.6	35.1 -
cb	5.0	35.7
+5	4.4	36.3
+6	5.4	35.3
1/4	4.8	35.9

4067

FCHC17 43

e	4.1	36.6
1/4	4.3	36.4
+9	4.6	36.1
+10	4.1	36.6
cb	4.0	36.7
N	3.8	36.9 -

250° E

N	4.0	36.7 -
cb	4.2	36.5
+3	4.3	36.4
+5	4.7	36.0
1/4	4.3	36.4
c	4.0	36.7
1/4	4.7	36.0
+7	5.1	35.6
+8	4.5	36.4
cb	4.5	36.4
S	4.5	36.4 -

300° E

S	4.4	36.3 -
cb	4.2	36.5
+6	4.2	36.5
+8	4.5	36.4
1/4	4.1	36.6
c	3.2	37.5
1/4	3.6	37.1

40.67

+9		4.1	36.6
+10		3.3	37.4
cb		3.3	37.4
N		3.4	37.3
T.P.	629	44.30 ✓	2.66
			38.01

350° E

N		6.0	38.3 ✓
cb		5.8	38.5
+4		5.8	38.5
+7		7.1	37.7
+8		6.6	37.7
1/4		6.7	38.1
c		6.1	38.7
1/4		6.7	37.6
+7		7.2	37.1
+8		6.4	37.9
cb		6.6	37.7
S		6.9	37.4 ✓

375° E

S		6.8	37.5 ✓
cb		6.5	37.8
+5		6.3	38.0
+6		6.9	37.4
1/4		6.4	37.9
c		5.7	38.6
1/4		5.8	38.5

4430

ACACIA 44

+3		5.8	38.5
+7		6.5	37.8
+9		5.5	38.8
cb		5.5	38.8
N		5.3	39.0 ✓

400° E

N		5.0	39.3 ✓
cb		5.4	38.9
+4		5.5	38.8
+5		6.0	38.3
+11		5.6	38.7
1/4		5.6	38.7
c		5.5	38.8
1/4		6.1	38.7
+7		6.6	37.7
+8		5.7	38.6
cb		6.0	38.3
S		6.2	38.1 ✓

425° E

S		6.8	37.5 ✓
cb		6.1	38.5
+6		6.0	38.3
+7		6.6	37.7
1/4		6.1	38.7
c		5.5	38.8
1/4		5.6	38.7

44.30

+8	5.8	38.5
+9	5.1	39.7
cb	5.1	39.7
N	5.8	38.5

469.80 = Intersection of Wloden & ACACIA STS

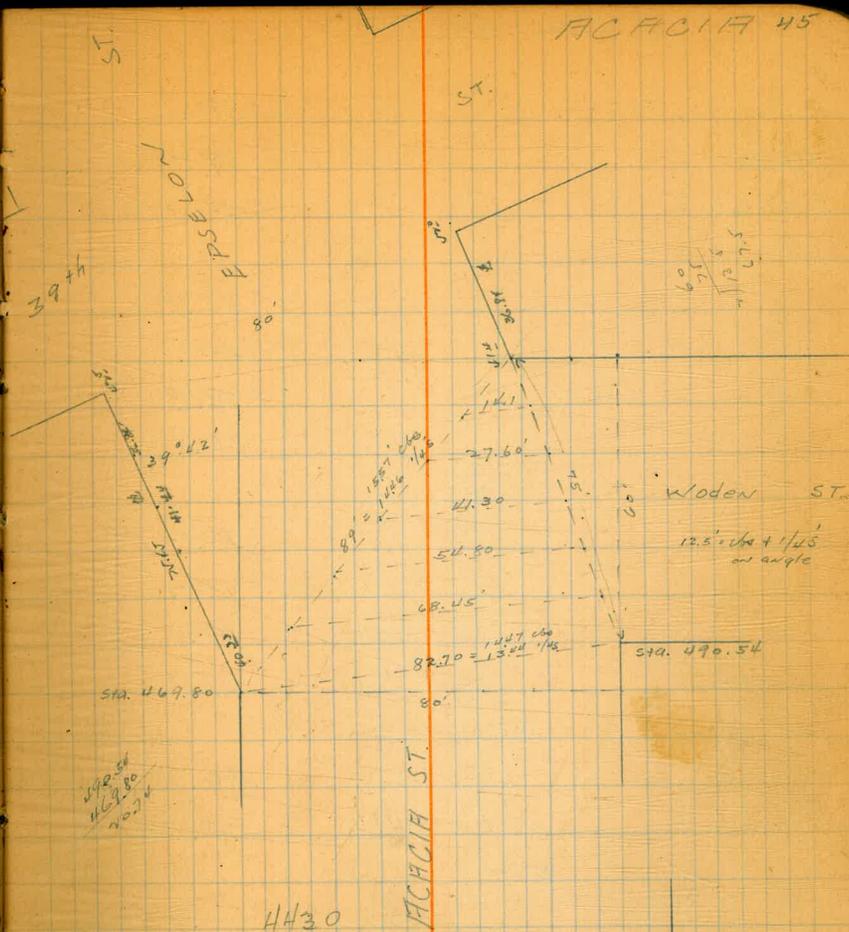
N	3.8	40.5
cb	4.2	39.9
+5	4.5	39.8
+6	5.2	39.1
1/4	5.3	39.0
c	5.3	39.0
1/4	5.8	38.5
+8	6.3	38.0
+9	5.6	38.7
cb	5.6	38.7
S	5.6	38.7

469.80 E - Wloden & ACACIA

490.54 E on S - Wloden

S	6.0	38.3
cb	5.5	38.8
+4	5.3	39.0
+5	5.9	38.4
1/4	5.4	38.9
c	5.1	39.7
1/4	5.1	39.7
+9	5.0	39.3

ACACIA 45



44.30

+10	4.5	39.8
cb	4.4	39.9
N	3.8	40.5
	w/ob	
N	4.0	40.3
+5	4.2	40.1
+6	4.7	39.6
+30	4.6	39.7

4430

+56		5.5	38.8
+57		4.9	39.4
S = +68.45		5.2	39.1
	+6		
N		4.4	39.9
+20		4.3	40.0
+40		5.0	39.3
S = +61.20		5.5	38.8
	W 1/4		
N		4.1	40.4
+15		4.1	40.4
+35		4.7	39.6
S = +54.80		5.1	39.7
	E		
N		3.6	40.7
S = +41.30		4.6	39.7
	E 1/4		
N		3.6	40.7
S +27.60		4.6	39.7
	+6		
N		3.8	40.5
S +21.1		4.8	39.5
	E ct		
N		4.3	40.0
+8		3.1	41.5
S +14.1		3.3	41.0

44.30

ACACIA

36

SL. ERSELOW + EL of Woden			
		3.1	41.5
Check BRT SW. Plover + Woden		4.82	39.58
			39.51

	20.44		
		8.14 (cont) 20.4	
F 8		4.5	15.9 ✓
cb		3.1	17.3 ✓
N		3.3	17.1 ✓
	6+37	4' W of E 1/4	
-5		4.9	15.5 ✓
N		4.9	15.5 ✓
cb		4.6	15.8 ✓
1/4		4.1	16.3 ✓
c		4.0	16.4 ✓
1/4		4.3	16.1 ✓
FF		4.6	15.8 ✓
+9		7.1	13.3 ✓
cb		7.0	13.4 ✓
S		6.4	14.0 ✓
+5		6.3	14.1 ✓
	0+43	10' W of E 1/4	
-2		4.8	15.6 ✓
S		4.8	15.6 ✓
cb		4.8	15.6 ✓
1/4		4.6	15.8 ✓
c		4.1	16.3 ✓
1/4		4.2	16.2 ✓
cb		4.6	15.8 ✓
N		4.8	15.6 ✓
+2		4.8	15.6 ✓

	20.44		Juniper 49
		No yardage 2.36 2 of Gen E. Rail. no yardage	
		20.4	
N		4.35	16.09 ✓
C		4.22	16.22 ✓
S		4.12	16.32 ✓
	0+50	6'	
N		4.9	15.5 ✓
cb		4.9	15.5 ✓
1/4		4.6	15.8 ✓
c		4.6	15.8 ✓
1/4		4.6	15.8 ✓
cb		4.7	15.7 ✓
S		4.6	15.8 ✓
	0+56	6' W of 6'	
S		4.8	15.6 ✓
cb		4.8	15.6 ✓
1/4		4.8	15.6 ✓
c		4.5	15.9 ✓
1/4		4.5	15.9 ✓
cb		4.8	15.6 ✓
N		4.9	15.5 ✓
	0+62	12' W of 6'	
-5		6.2	14.2 ✓
N		6.1	14.3 ✓
cb		5.5	14.9 ✓
1/4		5.1	15.3 ✓
c		5.0	15.4 ✓
1/4		5.9	14.5 ✓

20.44

20.4

cb		7.3	13.1 ✓
S		4.6	13.8 ✓
+5		4.0	14.4 ✓
	0+67		
	W. 1/4		
-5		6.2	14.2 ✓
S		6.6	13.8 ✓
cb		7.6	12.8 ✓
1/4		6.3	14.1 ✓
c		5.1	10.3 ✓
1/4		5.2	15.2 ✓
cb		6.0	14.4 ✓
N		6.3	14.1 ✓
+5		6.3	14.1 ✓
	0+84		
	W. CB.		
-5		6.6	13.8 ✓
N		6.6	13.8 ✓
cb		5.9	14.5 ✓
1/4		5.7	14.7 ✓
c		5.8	14.6 ✓
+8		5.9	14.5 ✓
1/4		6.5	13.9 ✓
#19		7.6	12.8 ✓
cb		7.2	13.2 ✓
S		5.1	15.3 ✓

20.44

Juniper 50

20.4

00 = W. Line California

S		6.4	14.0 ✓
cb		7.5	12.9 ✓
+6		7.7	12.7 ✓
1/4		6.9	13.5 ✓
c		6.1	14.3 ✓
1/4		6.0	14.4 ✓
cb		6.5	13.9 ✓
N		6.6	13.8 ✓
+5		6.6	13.8 ✓
	20' W		
-5		6.6	13.8 ✓
N		6.6	13.8 ✓
cb		6.8	13.6 ✓
1/4		6.4	14.0 ✓
c		6.4	14.0 ✓
1/4		7.3	13.1 ✓
+7		8.1	12.3 ✓
cb		7.9	12.5 ✓
S		8.1	12.3 ✓
+5		7.7	12.7 ✓
	50' W		
-5		8.4	12.0 ✓
S		7.7	12.7 ✓
cb		8.1	12.3 ✓
+4		8.5	11.9 ✓

20.44

50'W 20.4

1/4	7.6	12.8 ✓
C	6.8	13.6 ✓
1/4	7.0	13.4 ✓
cb	7.3	13.1 ✓
N	7.8	12.6 ✓
+5	7.8	12.6 ✓

110'W

N	7.5	12.9 ✓
cb	8.0	12.4 ✓
1/4	7.4	13.0 ✓
C	7.4	13.0 ✓
+10	7.7	12.7 ✓
1/4	8.6	11.8 ✓
cb	8.1	12.3 ✓
S	7.8	12.6 ✓

130'W

S	8.3	12.1 ✓
cb	9.2	11.2 ✓
1/4	9.0	11.4 ✓
+3	7.8	12.6 ✓
C	7.6	12.8 ✓
1/4	7.7	12.7 ✓
cb	7.5	12.9 ✓
N	7.0	13.4 ✓

20.44

JUNIPER 51

160'W 20.4

-5	9.2	11.2 ✓
N	9.2	11.2 ✓
cb	8.2	12.2 ✓
1/4	8.0	12.4 ✓
C	8.0	12.4 ✓
1/4	8.6	11.8 ✓
+6	9.4	11.0 ✓
cb	9.1	11.3 ✓
S	8.7	11.7 ✓
+5	8.7	11.7 ✓

185'W

-5	9.5	10.9 ✓
S	9.5	10.9 ✓
cb	10.0	10.4 ✓
1/4	8.6	11.8 ✓
C	8.5	11.9 ✓
1/4	8.5	11.9 ✓
cb	9.2	11.2 ✓
N	9.2	11.2 ✓
+5	10.0	10.4 ✓

200'W = E Line Atlantic 100' wide 10' dia 17' dia

-5	10.4	10.0 ✓
N	10.4	10.0 ✓
+10	10.5	9.9 ✓
cb	9.2	11.2 ✓
1/4	8.9	11.5 ✓

20.44

20.4

0	9.0	11.4 ✓
1/4	9.2	11.2 ✓
eb	10.3	10.1 ✓
S	9.7	10.7 ✓
+5	9.7	10.7 ✓
0+16		
	E:eb Atlantic	
-5	10.1	10.3 ✓
S	10.1	10.3 ✓
eb	10.4	10.0 ✓
+6	11.0	9.4 ✓
1/4	10.0	10.4 ✓
E	9.4	11.0 ✓
1/4	9.6	10.8 ✓
eb	9.9	10.5 ✓
+4	11.4	8.8 ✓
N	11.1	9.3 ✓
+5	11.0	9.4 ✓
0+33		
	E. 1/4	
-5	11.3	9.1 ✓
N	11.8	8.6 ✓
eb	11.7	8.7 ✓
+3	10.3	10.1 ✓
1/4	10.1	10.3 ✓
E	9.9	10.5 ✓
1/4	11.4	9.0 ✓
eb	11.0	9.4 ✓

20.44

Jupiter 52

20.4

S	10.5	9.9 ✓
+5	10.5	9.9 ✓
0+50		
	E	
-5	11.2	9.2 ✓
S	11.2	9.2 ✓
eb	11.1	9.3 ✓
+6	12.3	8.1 ✓
1/4	11.4	9.0 ✓
E	10.4	10.0 ✓
1/4	10.4	10.0 ✓
+9	10.6	9.8 ✓
eb	12.2	8.2 ✓
N	11.5	8.9 ✓
+5	11.5	8.9 ✓
0+67		
	W. 1/4	
-5	11.9	8.5 ✓
N	11.9	8.5 ✓
+8	11.8	8.6 ✓
eb	11.0	9.4 ✓
1/4	10.7	9.7 ✓
E	10.8	9.6 ✓
+10	10.9	9.5 ✓
1/4	11.9	8.5 ✓
eb	12.1	8.3 ✓
S	11.4	9.0 ✓
+5	11.4	9.0 ✓

	20.44	20.4	
-5	OT 84	W. CB	12.5 7.9 ✓
S			12.5 7.9 ✓
CB			11.7 8.7 ✓
1/4			11.3 9.1 ✓
C			11.0 9.4 ✓
1/4			10.9 9.5 ✓
CB			11.2 9.2 ✓
N			11.8 8.6 ✓
+5			11.8 8.6 ✓

00 = W. Line Atlantic

-5			12.0 8.4 ✓
N			12.0 8.4 ✓
CB			11.6 8.8 ✓
1/4			11.3 9.1 ✓
C			11.4 9.0 ✓
1/4			12.1 8.3 ✓
+6.7			12.6 7.8 ✓
CB			11.4 9.0 ✓
S			12.3 8.1 ✓
+5			12.3 8.1 ✓

50' W

-5			11.6 8.8 ✓
S			11.6 8.8 ✓
+10			13.2 7.2 ✓
CB			13.2 7.2 ✓
+6			13.3 7.1 ✓

	20.44	20.4	Juniper 53
1/4			12.2 8.2 ✓
C			12.0 8.4 ✓
1/4			11.8 8.6 ✓
CB			12.2 8.2 ✓
N			12.7 7.7 ✓
T.P.	2.21	12.03	10.62 9.82 ✓

100' W = E Line Belt

N			12.0 4.8 7.2 ✓
+10			3.9 8.1 ✓
CB			3.9 8.1 ✓
1/4			4.1 7.9 ✓
C			4.2 7.8 ✓
1/4			4.7 7.3 ✓
CB			4.9 7.1 ✓
S			5.0 7.0 ✓
	OT 16	E. CB	
S			4.3 7.7 ✓
CB			4.3 7.7 ✓
1/4			4.8 7.2 ✓
C			4.2 7.8 ✓
1/4			4.1 7.9 ✓
CB			4.3 7.7 ✓
N			5.0 7.0 ✓

12.03

0733

E. 114

12.0

N	5.7	6.3 ✓
cb	5.0	7.0 ✓
1/4	4.6	7.4 ✓
E	4.7	7.3 ✓
1/4	5.1	6.9 ✓
cb	4.8	7.2 ✓
S	4.4	7.6 ✓

E

S	4.7	7.3 ✓
cb	4.8	7.2 ✓
1/4	5.2	6.8 ✓
E	5.0	7.0 ✓
1/4	5.4	6.6 ✓
cb	5.5	6.5 ✓
N	6.4	5.6 ✓

0767

W. 114

N	6.7	5.3 ✓
cb	6.3	5.7 ✓
1/4	6.2	5.8 ✓
E	6.2	5.8 ✓
1/4	6.2	5.8 ✓
cb	6.3	5.7 ✓
S	6.3	5.7 ✓

07707

3.67 W of W. 114 trail

S	6.43	5.60 ✓
E	6.54	5.49 ✓
N	6.46	5.57 ✓

12.03

Juniper 54

0784

W. CB

12.0

S	6.5	5.5 ✓
cb	6.4	5.6 ✓
1/4	6.5	5.5 ✓
E	6.6	5.4 ✓
1/4	6.4	5.4 ✓
cb	6.5	5.5 ✓
N	6.7	5.3 ✓

00 = W. Line Belt SR

N	5.6	6.4 ✓
cb	5.8	6.2 ✓
1/4	5.4	6.6 ✓
E	5.2	6.8 ✓
1/4	5.2	6.8 ✓
cb	5.4	6.6 ✓
S	5.3	6.7 ✓

100'W

S	5.3	6.7 ✓
cb	5.4	6.6 ✓
1/4	5.1	6.9 ✓
E	5.0	7.0 ✓
1/4	5.0	7.0 ✓
cb	5.2	6.8 ✓
N	4.9	7.1 ✓

12.03

200'w 12.0

N	5.8	6.2 ✓
cb	6.0	6.0 ✓
1/4	6.0	6.0 ✓
E	6.0	6.0 ✓
1/4	6.1	5.9 ✓
cb	6.0	6.0 ✓
S	5.9	6.1 ✓

290'w

S	6.8	5.2 ✓
cb	6.7	5.3 ✓
1/4	7.0	5.0 ✓
E	7.2	4.8 ✓
1/4	7.2	4.8 ✓
cb	7.3	4.7 ✓
N	7.2	4.8 ✓

307'w

N	7.4	4.6 ✓
cb	7.2	4.8 ✓
1/4	6.6	5.4 ✓
E	6.1	5.9 ✓
1/4	6.2	5.8 ✓
cb	6.7	5.3 ✓
S	7.0	5.0 ✓

Juniper 55

Ingraham St X Sec of Center 30.
 from S line of Diamond Ave to g Line

5/22/10
 mile

1774 - Home Diamond

B.M. T.P. 2.04 84.84 82.84 Book 112B P.

00 = S. Line Diamond Ave

W		2.2	82.7 ✓
+5		2.2	82.7 ✓
E		1.9	83.0 ✓
+10		2.1	82.8 ✓
E		2.0	82.9 ✓

50' S

E		3.1	81.8 ✓
+5		3.2	81.7 ✓
E		2.9	82.0 ✓
+10		3.3	81.6 ✓
W		3.5	81.4 ✓

100' S

W		4.7	80.2 ✓
+5		4.5	80.4 ✓
E		4.2	80.7 ✓
+10		4.2	80.7 ✓
E		4.2	80.7 ✓

150' S

E		5.3	79.6 ✓
+5		5.2	79.7 ✓
E		5.1	79.8 ✓
+10		5.6	79.3 ✓
W		5.7	79.2 ✓

8488

56

200' S

W		7.1	77.8 ✓
+5		6.9	78.0 ✓
E		6.2	78.2 ✓
+10		6.6	78.3 ✓
E		6.4	78.5 ✓

270' S = N. Line Emerald Ave

E		8.4	76.5 ✓
+5		8.2	76.7 ✓
E		8.0	76.9 ✓
+10		8.4	76.5 ✓
W		8.6	76.3 ✓

40' S =

W		9.7	75.2 ✓
+5		9.5	75.4 ✓
E		8.9	76.0 ✓
+10		9.1	75.8 ✓
E		9.1	75.8 ✓

80' S = S. Line Emerald = 00

E		10.1	74.8 ✓
+5		10.1	74.8 ✓
E		9.7	75.2 ✓
+10		10.1	74.8 ✓
W		10.4	74.5 ✓

50' S

W		11.2	73.7 ✓
+5		11.1	73.8 ✓

8488

50' S (Con)

C		10.6	74.3 ✓
+10		11.0	73.9 ✓
E		11.0	73.9 ✓

100' S

E		12.0	72.9 ✓
+5		11.9	73.0 ✓
C		11.5	73.4 ✓
+10		12.2	72.7 ✓
W		12.5	72.4 ✓

T.P.	0.47	72.46	12.89	71.99 ✓
------	------	-------	-------	---------

150' S

N		1.3	71.2 ✓
+5		1.1	71.4 ✓
C		0.5	72.0 ✓
+10		0.7	71.8 ✓
E		0.9	71.6 ✓

200' S

E		2.0	70.5 ✓
+5		1.8	70.7 ✓
C		1.2	71.3 ✓
+10		1.8	70.7 ✓
W		2.0	70.5 ✓

270' S = N Line Field spar

W		3.3	69.2 ✓
+5		3.0	69.5 ✓
C		2.7	69.8 ✓

7246

Ingram

57

+10		3.1	69.4 ✓
E		3.2	69.3 ✓

40' S = 4

E		4.0	68.5 ✓
+5		3.9	68.6 ✓
C		3.2	69.3 ✓
+10		3.6	68.9 ✓
W		4.0	68.5 ✓

80' S = S. Line Field spar = 00

W		4.9	67.6 ✓
+5		4.7	67.8 ✓
C		4.3	68.2 ✓
+10		4.7	67.8 ✓
E		4.9	67.6 ✓

50' S

E		5.9	66.6 ✓
+5		5.8	66.7 ✓
C		5.4	67.1 ✓
+10		5.8	66.7 ✓
W		4.0	66.5 ✓

100' S

E		7.3	65.2 ✓
+5		7.0	65.5 ✓
C		6.6	65.9 ✓
+10		6.8	65.7 ✓
E		6.9	65.6 ✓

150' S

E	8.3	64.2 ✓
+5	8.1	64.4 ✓
C	7.9	64.6 ✓
+10	8.2	64.3 ✓
W	8.5	64.0 ✓

200' S

W	9.4	63.1 ✓
+5	9.3	63.2 ✓
C	9.0	63.5 ✓
+10	9.0	63.5 ✓
E	9.0	63.5 ✓

270' S = N. Line Garret.

E	9.6	62.9 ✓
+5	9.6	62.9 ✓
C	9.8	62.7 ✓
+10	9.9	62.5 ✓
W	10.0	62.5 ✓

30' S = N. Line Paving

W	10.11	62.4 ✓
+5	10.09	62.37 ✓ on paving
C	10.08	62.38 ✓ " "
+10	10.04	62.42 ✓ " "
E	10.1	62.4 ✓

50' S = S. edge Paving

E	10.1	62.4 ✓
+5	10.14	62.32 ✓ on paving

C	10.22	62.24 ✓ on paving
+10	10.20	62.26 ✓ " "
W	10.2	62.3 ✓

80' S = S. Line Garret = 0.0

W	10.2	62.3 ✓
+5	10.2	62.3 ✓
C	10.2	62.3 ✓
+10	10.2	62.3 ✓
E	10.2	62.3 ✓

→ T.P. 7.40

ch Kan BM.

→ B.M. 4.34

	7.24	63.22 ✓	Bolt Head dia. Pil.
	2.14	68.48 = 68.44	S.M. Error in Garret Top Cur to N.E. Garret + HAINES
	67.56	63.22	Bolt Head

50' S

E	5.4	62.2 ✓
+5	5.5	62.1 ✓
C	5.3	62.3 ✓
+10	6.0	61.6 ✓
W	5.7	61.9 ✓

100' S

W	6.0	61.6 ✓
+5	6.0	61.6 ✓
C	5.5	62.1 ✓
+10	5.7	61.9 ✓
E	5.4	62.2 ✓

67.56

140' S

E	5.5	62.1 ✓
+5	5.4	62.2 ✓
E	5.5	62.1 ✓
+10	6.1	61.5 ✓
W	6.2	61.4 ✓

200' S

W	5.0	62.6 ✓
+5	4.7	62.9 ✓
E	4.1	63.5 ✓
+10	4.4	63.2 ✓
E	4.6	63.0 ✓

235' S

E	3.8	63.8 ✓
+5	3.9	63.7 ✓
E	3.5	64.1 ✓
+10	4.1	63.5 ✓
W	4.3	63.3 ✓

270' S = N. Line Har Blend

W	4.5	63.1 ✓
+5	4.4	63.2 ✓
E	4.0	63.6 ✓
+10	4.3	63.3 ✓
E	4.4	63.2 ✓

40' S = ~~E~~

E	4.5	63.1 ✓
+5	4.4	63.2 ✓

67.56

Ingraham 59

E	4.1	63.5 ✓
+10	4.5	63.1 ✓
W	4.6	63.0 ✓

80' S = S. Line Har Blend = 00

W	4.7	62.9 ✓
+5	4.7	62.9 ✓
E	4.4	63.2 ✓
+10	4.8	62.8 ✓
E	4.9	62.7 ✓

50' S

E	5.8	61.8 ✓
+5	5.8	61.8 ✓
E	5.3	62.3 ✓
+10	5.4	62.2 ✓
W	5.4	62.2 ✓

100' S

W	6.5	61.1 ✓
+5	6.5	61.1 ✓
E	6.4	61.2 ✓
+10	7.0	60.6 ✓
E	7.1	60.5 ✓

135' S

E	7.7	59.9 ✓
+5	7.7	59.9 ✓
E	7.0	60.6 ✓
+10	7.3	60.3 ✓
W	7.1	60.5 ✓

67.56

160' S

W	8.7	58.9 ✓
+5	8.6	59.0 ✓
C	8.1	59.5 ✓
+10	8.3	59.3 ✓
E	8.2	59.4 ✓

215' S

E	10.0	57.6 ✓
+5	9.9	57.7 ✓
C	9.6	58.0 ✓
+10	9.9	57.7 ✓
W	10.0	57.6 ✓

270' S = N. Line Grand Ave

W	11.5	56.1 ✓
+5	11.4	56.2 ✓
C	11.2	56.4 ✓
+10	11.8	55.8 ✓
E	11.8	55.8 ✓

62.5 S = ~~2~~

E	11.5	56.1 ✓
+5	11.6	56.0 ✓
C	11.6	56.0 ✓
+10	11.9	55.7 ✓
W	11.9	55.7 ✓

125' S = S. Line Grand = 00

W	12.9	54.7 ✓
+5	13.0	54.6 ✓

67.56

Ingraham 60

E	12.8	54.8 ✓
+10	13.1	54.5 ✓
E	13.3	54.3 ✓
T.P.	0.10	55.57
		12.69

50' S

E	2.4	53.2 ✓
+5	2.0	53.6 ✓
C	1.4	54.2 ✓
+10	1.7	53.9 ✓
W	1.5	54.1 ✓

100' S

W	2.7	52.9 ✓
+5	2.8	52.8 ✓
C	2.1	53.5 ✓
+10	3.0	52.6 ✓
E	3.5	52.1 ✓

150' S

E	4.5	51.1 ✓
+5	4.0	51.6 ✓
C	3.2	52.4 ✓
+10	3.7	51.9 ✓
W	3.7	51.9 ✓

200' S

W	4.7	50.9 ✓
+5	4.7	50.9 ✓
C	4.2	51.4 ✓

55.57

200 S (cont)

T10 5.1 50.5 ✓

E 5.5 50.1 ✓

R 70' S = N Line Thomas Ave

E 6.7 48.9 ✓

T5 6.2 49.4 ✓

E 5.4 50.2 ✓

T10 5.8 49.8 ✓

W 6.0 49.6 ✓

40' S = ϕ

W 6.2 49.4 ✓

T5 6.0 49.6 ✓

E 5.9 49.7 ✓

T10 6.8 48.8 ✓

E 7.1 48.5 ✓

80' S = S Line Thomas Ave

E 7.9 47.8 ✓

T5 7.4 48.2 ✓

E 6.5 49.1 ✓

T10 6.6 49.0 ✓

W 6.9 48.8 ✓

50' S

W 7.3 48.3 ✓

T5 7.6 48.0 ✓

E 7.5 48.1 ✓

T10 8.2 47.4 ✓

E 8.5 47.1 ✓

55.57

Ingraham 61

100' S

E 9.1 46.5 ✓

T5 8.7 46.9 ✓

E 8.3 47.3 ✓

T10 8.2 47.4 ✓

W 8.4 47.2 ✓

150' S

W 9.0 46.6 ✓

T5 9.0 46.6 ✓

E 9.0 46.6 ✓

T10 9.6 46.0 ✓

E 9.8 45.8 ✓

200' S

E 10.6 45.0 ✓

T5 10.3 45.3 ✓

E 9.8 45.8 ✓

T10 10.1 45.5 ✓

W 10.1 45.5 ✓

R 70' S = N Line Reed Ave

W 10.7 44.9 ✓

T5 10.3 45.3 ✓

E 10.2 45.4 ✓

T10 10.7 44.9 ✓

E 11.1 44.5 ✓

40' S = ϕ

E 11.0 44.6 ✓

T5 10.6 45.0 ✓

35.57

4 (con)

C		10.4	45.2 ✓
+10		10.5	45.1 ✓
W		10.6	45.0 ✓
T.P.	7.14	52.74	9.97 45.60 ✓

80' S = S. Line Reed Ave

W		7.9	44.8 ✓
+5		7.6	45.1 ✓
C		7.6	45.1 ✓
+10		7.9	44.8 ✓
E		8.0	44.7 ✓

50' S

E		7.4	45.3 ✓
+5		7.3	45.4 ✓
C		7.0	45.7 ✓
+10		7.2	45.5 ✓
W		7.1	45.6 ✓

100' S

W		6.7	46.0 ✓
+5		6.6	46.1 ✓
C		6.5	46.2 ✓
+10		6.7	46.0 ✓
E		6.9	45.8 ✓

150' S

E		6.4	46.3 ✓
+5		6.2	46.5 ✓
C		6.0	46.7 ✓

52.74

Ingraham 62

+10		6.0	46.7 ✓
W		5.7	47.0 ✓

200' S

W		5.2	47.5 ✓
+5		5.0	47.7 ✓
C		5.0	47.7 ✓
+10		5.2	47.5 ✓
E		5.4	47.3 ✓

270' S = N. Line Oliver Ave

E		4.9	47.8 ✓
+5		4.7	48.0 ✓
C		4.3	48.4 ✓
+10		4.3	48.4 ✓
W		4.6	48.1 ✓

40' S = 4

W		4.6	48.1 ✓
+5		4.5	48.2 ✓
C		4.5	48.2 ✓
+10		4.7	48.0 ✓
E		4.8	47.9 ✓

80' S = S. Line Oliver

E		4.9	47.8 ✓
+5		4.8	47.9 ✓
C		4.6	48.1 ✓
+10		4.7	48.0 ✓
W		4.5	48.2 ✓

52.74

50' S

W	4.7	48.0 ✓
+5	4.9	47.8 ✓
E	4.7	48.0 ✓
+10	5.1	47.6 ✓
E	5.2	47.5 ✓

100' S

E	5.2	47.5 ✓
+5	5.2	47.5 ✓
E	4.9	47.8 ✓
+10	5.0	47.7 ✓
W	4.9	47.8 ✓

150' S

W	5.3	47.4 ✓
+5	5.3	47.4 ✓
E	5.0	47.7 ✓
+10	5.3	47.4 ✓
E	5.5	47.2 ✓

200' S

E	6.0	46.7 ✓
+5	5.9	46.8 ✓
E	5.6	47.1 ✓
+10	5.4	47.3 ✓
W	5.2	47.5 ✓

T.P. 2.36 49.64 5.46 47.28 ✓

49.64

Ingraham

63

255.97 S = N line PL. 1800

W	3.1	46.5 ✓
+5	2.7	46.9 ✓
E	2.8	46.8 ✓
+10	3.0	46.6 ✓
E	3.3	46.3 ✓

72' S = Pacific

E	3.6	46.0 ✓
+5	3.3	46.3 ✓
E	3.5	46.1 ✓
+10	3.5	46.1 ✓
W	3.7	45.9 ✓

144' S = S. line Pacific = 00

W	4.6	45.0 ✓
+5	4.4	45.2 ✓
E	3.7	45.9 ✓
+10	3.9	45.7 ✓
E	4.2	45.4 ✓

49.64

50' S

E	4.2	45.4 ✓
+5	4.0	45.6 ✓
C	3.9	45.7 ✓
+10	4.3	45.3 ✓
W	4.3	45.3 ✓

100' S.

W	4.8	44.8 ✓
+5	4.6	45.0 ✓
C	4.4	45.2 ✓
+10	4.4	45.2 ✓
E	4.5	45.1 ✓

150' S

E	4.5	45.1 ✓
+5	4.3	45.3 ✓
C	4.2	45.4 ✓
+10	4.5	45.1 ✓
W	4.7	44.9 ✓

200' S.

W	4.9	44.7 ✓
+5	4.6	45.0 ✓
C	4.3	45.3 ✓
+10	4.4	45.2 ✓
E	4.5	45.1 ✓

250' S.

E	4.6	45.0 ✓
+5	4.4	45.2 ✓
C	4.5	45.1 ✓

49.64

Ingraham 64

+10	4.5	45.1 ✓
W	4.2	45.0 ✓

300' S

W	4.6	45.0 ✓
+5	4.6	45.0 ✓
C	4.3	45.3 ✓
+10	4.5	45.1 ✓
E	4.6	45.0 ✓

350' S.

E	4.8	44.8 ✓
+5	4.6	45.0 ✓
C	4.4	45.2 ✓
+10	4.6	45.0 ✓
W	4.7	44.9 ✓

400' S.

W	5.1	44.5 ✓
+5	4.9	44.7 ✓
C	4.9	44.7 ✓
+10	5.0	44.6 ✓
E	5.0	44.6 ✓

450' S.

E	5.0	44.6 ✓
+5	4.9	44.7 ✓
C	4.8	44.8 ✓
+10	4.9	44.7 ✓
W	5.2	44.4 ✓

49.64

500' S

W	5.2	44.4 ✓
+5	5.2	44.4 ✓
C	4.9	44.7 ✓
+10	5.2	44.4 ✓
E	5.2	44.4 ✓

525' S = N. Line Sunset Ave

E	5.4	44.2 ✓
+5	5.2	44.4 ✓
C	4.9	44.7 ✓
+10	5.1	44.5 ✓
W	5.3	44.3 ✓

37.5' S = ϕ

N	5.4	44.2 ✓
+5	5.1	44.5 ✓
C	5.1	44.5 ✓
+10	5.0	44.6 ✓
E	5.2	44.4 ✓

75' S = S. Line Sunset Ave = 00

E	6.0	43.6 ✓
+5	5.7	43.9 ✓
C	5.4	44.2 ✓
+10	5.6	44.8 ✓
W	5.9	43.7 ✓

50' S

W	6.6	43.0 ✓
+5	6.3	43.3 ✓

49.64

Inverham 65

C	5.7	43.9 ✓
+10	6.1	43.5 ✓
E	4.3	43.3 ✓

100' S

E	7.2	42.4 ✓
+5	7.0	42.6 ✓
C	6.8	42.8 ✓
+10	7.1	42.5 ✓
W	7.1	42.5 ✓

150' S

W	7.9	41.7 ✓
+5	7.8	41.8 ✓
C	7.4	42.2 ✓
+10	7.7	41.9 ✓
E	8.1	41.5 ✓

200' S

E	8.5	41.1 ✓
+5	8.3	41.3 ✓
C	7.8	41.8 ✓
+10	8.2	41.4 ✓
W	8.6	41.0 ✓

250' S

W	9.3	40.3 ✓
+5	9.0	40.6 ✓
C	8.5	41.1 ✓
+10	8.9	40.7 ✓
E	9.2	40.4 ✓

T.P.	0.64	49.64	41.48	8.80	40.84
			300' S.		
E				1.9	39.6 ✓
+5				1.6	39.9 ✓
E				0.9	40.6 ✓
+10				1.4	40.1 ✓
W				1.5	40.0 ✓
			350' S.		
W				2.5	39.0 ✓
+5				2.3	39.2 ✓
E				1.8	39.7 ✓
+10				2.1	39.4 ✓
E				2.2	39.3 ✓
			400' S.		
E				3.2	38.3 ✓
+5				2.7	38.8 ✓
E				2.3	39.2 ✓
+10				2.9	38.6 ✓
W				3.0	38.5 ✓
			450' S.		
W				3.9	37.6 ✓
+5				3.6	37.9 ✓
E				3.3	38.2 ✓
+10				3.4	38.1 ✓
E				3.8	37.7 ✓

		41.48	Ingram 66
		500' S.	
E			4.7 36.8 ✓
+5			4.5 37.0 ✓
E			4.1 37.4 ✓
+10			4.4 37.1 ✓
W			4.6 36.9 ✓
		550' S.	
W			5.2 36.3 ✓
+5			5.2 36.3 ✓
E			4.8 36.7 ✓
+10			5.0 36.5 ✓
E			5.2 36.3 ✓
		600' S = N. Line Roosevelt Ave	
E			5.8 35.7 ✓
+5			5.3 36.2 ✓
E			5.5 36.0 ✓
+10			5.7 35.8 ✓
W			5.7 35.8 ✓
		375' S = ϕ	
W			6.1 35.4 ✓
+5			6.1 35.4 ✓
E			5.7 35.8 ✓
+10			6.0 35.5 ✓
E			6.1 35.4 ✓
		75' S = S. Line Roosevelt = 00	
E			6.9 34.6 ✓
+5			6.3 35.2 ✓

41.48

C	6.0	35.5 ✓
+10	6.5	35.0 ✓
W	6.8	34.7 ✓

50'S

W	7.5	34.0 ✓
+5	7.3	34.2 ✓
C	6.7	34.8 ✓
+10	7.3	34.2 ✓
E	7.7	33.8 ✓

100'S

E	8.6	32.9 ✓
+5	8.2	33.3 ✓
C	7.5	34.0 ✓
+10	8.2	33.3 ✓
W	8.5	33.0 ✓

150'S

W	9.3	32.2 ✓
+5	8.9	32.6 ✓
C	8.5	33.0 ✓
+10	8.8	32.7 ✓
E	9.1	32.4 ✓

200'S

E	10.0	31.5 ✓
+5	9.7	31.8 ✓
C	9.0	32.5 ✓
+10	9.6	31.9 ✓
W	10.0	31.5 ✓

41.48

Ingraham

67

250'S

W	10.6	30.9 ✓
+5	10.4	31.1 ✓
C	9.8	31.7 ✓
+10	10.3	31.2 ✓
E	10.7	30.8 ✓

300'S

E	11.4	30.1 ✓
+5	10.8	30.7 ✓
C	10.4	31.1 ✓
+10	10.9	30.6 ✓
W	11.5	30.0 ✓

350'S

W	12.2	29.3 ✓
+5	11.9	29.6 ✓
C	11.1	30.4 ✓
+10	11.6	29.9 ✓
E	12.2	29.3 ✓

T.P. 251

32.77

11.22

30.26 ✓

400'S

E	4.0	28.8 ✓
+5	3.4	29.4 ✓
C	3.0	29.8 ✓
+10	3.7	29.1 ✓
W	4.2	28.6 ✓

450'S

W	4.8	28.0 ✓
---	-----	--------

32.77

+5	4.4	28.4 ✓
C	3.8	29.0 ✓
+10	4.5	28.3 ✓
E	4.9	27.9 ✓
	500' S	
E	5.6	27.2 ✓
+5	5.2	27.6 ✓
C	4.8	28.0 ✓
+10	5.3	27.5 ✓
W	5.6	27.2 ✓
	550' S	
W	5.8	27.0 ✓
+5	5.5	27.3 ✓
C	5.5	27.3 ✓
+10	5.7	27.1 ✓
E	6.0	26.8 ✓
	600' S = N. line La Playa Ave	
E	6.7	26.1 ✓
+5	6.4	26.4 ✓
C	6.1	26.7 ✓
+10	6.4	26.4 ✓
W	6.5	26.3 ✓
	37.5' S = ϕ	
W	6.4	26.4 ✓
+5	6.4	26.4 ✓
C	6.2	26.6 ✓

32.77

Inqrahim 68

+10	6.4	26.4 ✓
E	6.7	26.1 ✓
	75' S = S. line La Playa Ave = 00	
E	7.0	25.8 ✓
+5	6.7	26.1 ✓
C	6.3	26.5 ✓
+10	6.6	26.2 ✓
W	6.7	26.1 ✓
	50' S	
W	7.3	25.5 ✓
+5	7.0	25.8 ✓
C	6.9	25.9 ✓
+10	7.1	25.7 ✓
E	7.4	25.4 ✓
	100' S	
E	7.4	25.4 ✓
+5	7.1	25.7 ✓
C	6.6	26.2 ✓
+10	7.2	25.6 ✓
W	7.5	25.3 ✓
	150' S	
W	7.8	25.3 ✓
+5	7.0	25.8 ✓
C	6.5	26.3 ✓
+10	6.9	25.9 ✓
E	7.2	25.6 ✓

32.77

200' S.

E	4.9	25.9 ✓
+5	6.6	26.2 ✓
C	6.0	26.8 ✓
+10	6.7	26.1 ✓
W	7.1	25.7 ✓

250' S

W	6.0	26.8 ✓
+5	3.8	27.0 ✓
C	5.0	27.8 ✓
+10	5.7	27.1 ✓
E	6.0	26.8 ✓

300' S

E	5.1	27.7 ✓
+5	4.5	28.3 ✓
C	4.1	28.7 ✓
+10	4.5	28.3 ✓
W	4.9	27.9 ✓

350' S

W	3.9	28.9 ✓
+5	3.6	29.2 ✓
C	3.1	29.7 ✓
+10	3.5	29.3 ✓
E	3.9	28.9 ✓

T.P.	5.88	36.87	1.78	30.99 ✓
------	------	-------	------	---------

400' S

E	6.9	30.00 ✓
---	-----	---------

Ingraham 69

36.87

+5	6.7	30.2 ✓
C	6.0	30.9 ✓
+10	6.4	30.3 ✓
W	6.8	30.1 ✓

450' S

W	5.6	31.3 ✓
+5	5.4	31.5 ✓
C	4.6	32.3 ✓
+10	5.1	31.8 ✓
E	5.7	31.2 ✓

500' S

E	4.7	32.2 ✓
+5	4.3	32.6 ✓
C	4.0	32.9 ✓
+10	4.5	32.4 ✓
W	4.7	32.2 ✓

560.92 S = S. Line Fortuna Park Add. = N. Line of 60' proposed St.

W	3.0	33.9 ✓
+5	3.1	33.8 ✓
C	3.3	33.6 ✓
+10	3.3	33.6 ✓
E	3.2	33.7 ✓
+22.5 = E Line Ingraham	3.2	33.7 ✓

30' S = E proposed St

-22.5 = E Line Ingraham	3.2	33.7 ✓
E	3.2	33.7 ✓

36.87

+5	3.2	33.7 ✓
±	3.2	33.7 ✓
+10	3.2	33.7 ✓
W	3.2	33.7 ✓

60' S = S. Line Proposed ST.

W	3.1	33.8 ✓
+5	3.0	33.9 ✓
±	3.0	33.9 ✓
+10	2.9	34.0 ✓
E	2.9	34.0 ✓

122.5 = E. Line Ingraham

Set BM. at Mon
S. Line To Park
at Ingraham

3.0	33.9 ✓
4.52	32.35 ✓

X Sec. Ctn. 30' of 60' Proposed ST from E. Line
Ingraham C. to Mission View Blvd. thence on Mission
View Blvd N. E. to end Lamont St Parking

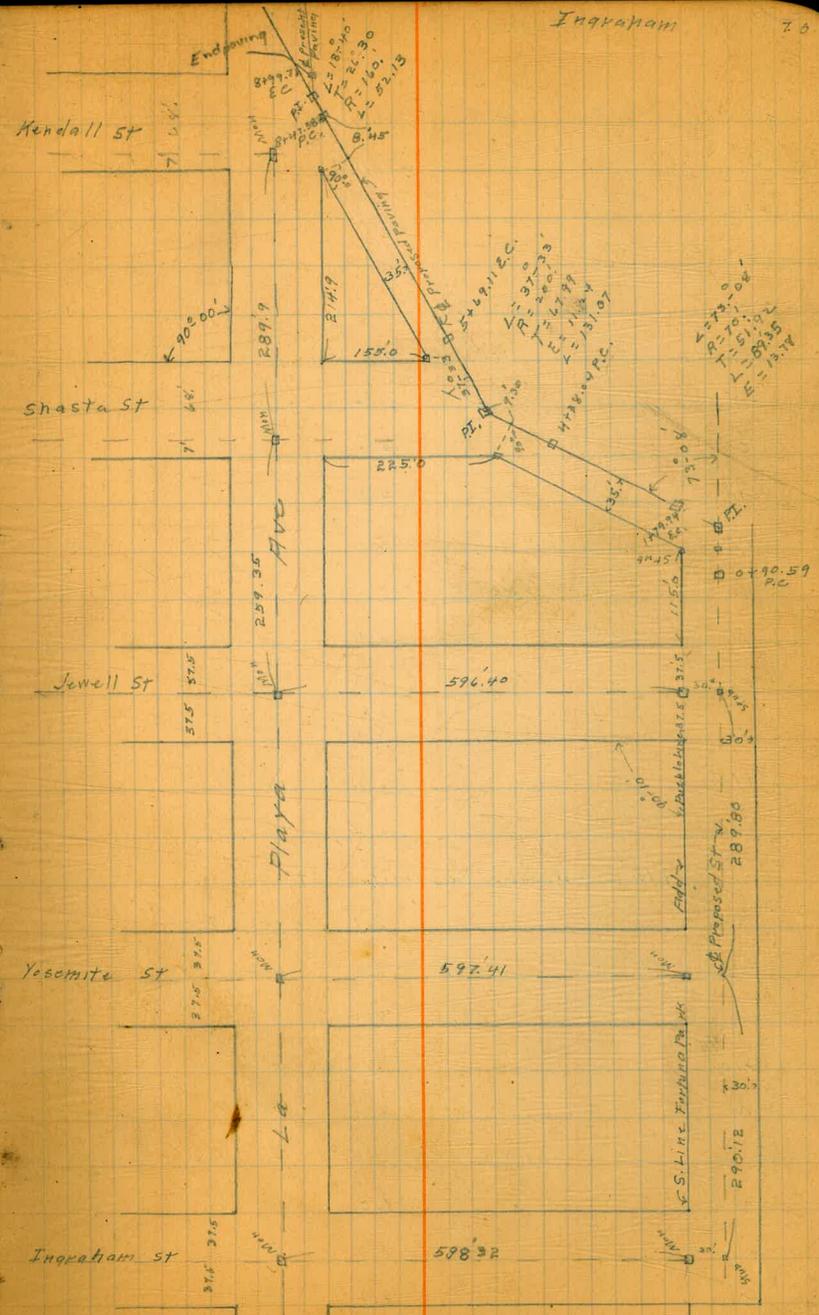
36.87

00 = E Line Ingraham

S	3.2	33.7 ✓
+5	3.2	33.7 ✓
±	3.2	33.7 ✓
+10	3.4	33.5 ✓
N	3.3	33.6 ✓

50' E.

N	4.1	32.8 ✓
---	-----	--------



3687

50' E (EWH)

+5	4.2	32.7 ✓
C	4.0	32.9 ✓
+10	4.0	32.9 ✓
S	4.0	32.9 ✓

100' E.

S	5.1	31.8 ✓
+5	5.2	31.7 ✓
C	5.1	31.8 ✓
+10	5.1	31.8 ✓
N	5.0	31.9 ✓

150' E

N	6.5	30.4 ✓
+5	6.5	30.4 ✓
C	6.4	30.5 ✓
+10	6.2	30.7 ✓
S	6.3	30.6 ✓

215' E. = W. Line Yosemite ST

S	8.1	28.8 ✓
+5	8.2	28.7 ✓
C	8.2	28.7 ✓
+10	8.2	28.7 ✓
N	8.2	28.7 ✓

37.5 E = ϕ

N	9.0	27.9 ✓
+5	8.9	28.0 ✓
C	8.9	28.0 ✓

3687

Ingraham + Mission New Bl⁷¹

+10	8.8	28.1 ✓
S	8.9	28.0 ✓

75' E = E. Line Yosemite

S	9.4	27.5 ✓
+5	9.4	27.5 ✓
C	9.3	27.6 ✓
+10	9.4	27.5 ✓
N	9.4	27.5 ✓

50' E

N	9.9	27.0 ✓
+5	10.1	26.8 ✓
C	10.1	26.8 ✓
+10	10.2	26.7 ✓
S	10.2	26.7 ✓

100' E

S	10.7	26.2 ✓
+5	10.7	26.2 ✓
C	10.6	26.3 ✓
+10	10.7	26.2 ✓
N	10.7	26.2 ✓

150' E

N	11.3	25.6 ✓
+5	11.3	25.6 ✓
C	11.4	25.5 ✓
+10	11.5	25.4 ✓
S	11.5	25.4 ✓

36.87

215' ESW Line Jewell St.

S	12.7	24.2 ✓
+5	12.7	24.2 ✓
C	12.7	24.2 ✓
+10	12.5	24.4 ✓
N	12.5	24.4 ✓

T.P.

529

30.32

11.84

25.03

Set BM-Mon. ϕ Jewell
& S. Line of Turner Park

7.00

23.32

37.5 E. = ϕ

N	6.5	23.8 ✓
+5	6.6	23.7 ✓
C	6.7	23.6 ✓
+10	6.9	23.4 ✓
S	7.0	23.3 ✓

75' E = E. Line Jewell = 0+00

S	7.5	22.8 ✓
+5	7.4	22.9 ✓
C	7.3	23.0 ✓
+10	7.1	23.2 ✓
N	7.0	23.3 ✓

0+50

N	7.2	23.1 ✓
+5	7.3	23.0 ✓
C	7.4	22.9 ✓
+10	7.7	22.6 ✓
S	7.7	22.6 ✓

3032

Mission View Blvd 72

0+90.59 = P.C.

S	7.2	23.1 ✓
+5	7.3	23.0 ✓
C	7.1	23.2 ✓
+10	7.0	23.3 ✓
N	7.0	23.0 ✓

1+35.26 = C+P.C.

+5	6.2	24.1 ✓
N.W.	6.2	24.1 ✓
+5	6.3	24.0 ✓
C	6.5	23.8 ✓
+10	6.5	23.8 ✓
SE	6.8	23.5 ✓
+5	6.9	23.4 ✓

1+79.94 = E.C.

S.E.	6.6	23.7 ✓
+5	6.8	23.5 ✓
C	6.6	23.7 ✓
+10	7.0	23.3 ✓
N.W.	6.9	23.4 ✓

2+50

N.W.	6.9	23.4 ✓
+5	6.5	23.8 ✓
C	6.7	23.6 ✓
+10	6.8	23.5 ✓
S.E.	6.5	23.8 ✓

30.32

3+00

SE	6.2	24.1 ✓
+5	6.4	23.9 ✓
C	6.4	23.9 ✓
+10	6.3	24.0 ✓
N.W.	6.6	23.7 ✓

3+50

N.W.	6.6	23.7 ✓
+5	6.5	23.8 ✓
C	6.5	23.8 ✓
+10	6.4	23.9 ✓
S.E.	6.3	24.0 ✓

4+00

S.E.	6.2	24.1 ✓
+5	6.4	23.9 ✓
C	6.3	24.0 ✓
+10	6.3	24.0 ✓
N.W.	6.6	23.7 ✓

4+38.04 = PC.

N.W.	6.8	23.5 ✓
+5	6.4	23.9 ✓
C	6.3	24.0 ✓
+10	6.5	23.8 ✓
S.E.	6.3	24.0 ✓

5+03.58 = CTR C.

SE	6.3	24.0 ✓
+5	6.2	24.1 ✓

30.37

Mission Viejo Blvd 73

C	5.9	24.4 ✓
+10	5.9	24.4 ✓
NW	5.9	24.4 ✓

5+69.11 = E.C.

N	6.3	24.0 ✓
+5	6.3	24.0 ✓
C	5.9	24.4 ✓
+10	6.1	24.2 ✓
S	6.0	24.3 ✓
T.P.	4.59	28.78

6+00

S	4.4	24.4 ✓
+5	4.4	24.4 ✓
C	4.4	24.4 ✓
+10	4.3	24.5 ✓
N	4.5	24.3 ✓

6+50

N	4.2	24.6 ✓
+5	4.1	24.7 ✓
C	3.9	24.9 ✓
+10	4.3	24.5 ✓
S	4.1	24.7 ✓

7+00

S	4.2	24.6 ✓
+5	4.2	24.6 ✓
C	3.9	24.9 ✓

~~28.78~~
28.78

7+00 (com)

+10 4.2 24.6 ✓

N 4.4 24.4 ✓

7+50

N 4.3 24.5 ✓

+5 4.2 24.6 ✓

C 4.3 24.5 ✓

+10 4.5 24.3 ✓

S 4.7 24.1 ✓

8+00

S 4.4 24.4 ✓

+5 4.6 24.2 ✓

C 4.5 24.3 ✓

+10 4.2 24.6 ✓

N 4.4 24.4 ✓

8+47.52 P.C.

N 4.2 24.6 ✓

+5 4.0 24.8 ✓

C 4.1 24.7 ✓

+10 4.6 24.2 ✓

S 4.7 24.1 ✓

8+99.71 E.C.

S 4.9 23.9 ✓

+5 4.8 24.0 ✓

C 4.7 24.1 ✓

+10 4.7 24.1 ✓

N 4.7 24.1 ✓

Mission View Blvd 74

7+00 = W. End Present Paving

N+5

4.70 24.08 ✓ on paving

C

4.50 24.28 ✓ " "

+10

4.67 24.11 ✓ " "

chk on Return M.E. Cor
LaPlaza & Kendall

4.02

Moore
6/25/25

CROSS SECTION of S 1/2 = 40' wide
GUNN ST
14' s/w

349.51

75

30th to RAY ST

S.W. B.P.	558	349.51	343.93
		EL 30th	
SL		5.40	
+ 4.5 = S edge sidewalk		5.47	
+ 9.5 = N edge sidewalk		5.53	
10' Return on cement		5.6	
S 1/4		5.6	
⊕		5.3	
	5' E		
⊕		5.3	
+ 4		5.0	
S 1/4		5.1	
⊕		4.7	
+ 4.5 N edge s/w		5.46	
+ 9.5 S ✓ ✓		5.39	
SL		4.9	
	50' E		
SL		4.5	
+ 4.5 S edge s/w		5.12	
+ 9.5		5.19	
⊕		4.3	
1/4		4.7	
⊕		4.9	
	100' E		
⊕		4.4	

Note:
5' sidewalk for
entire length on
south side of Gunn
No curb in

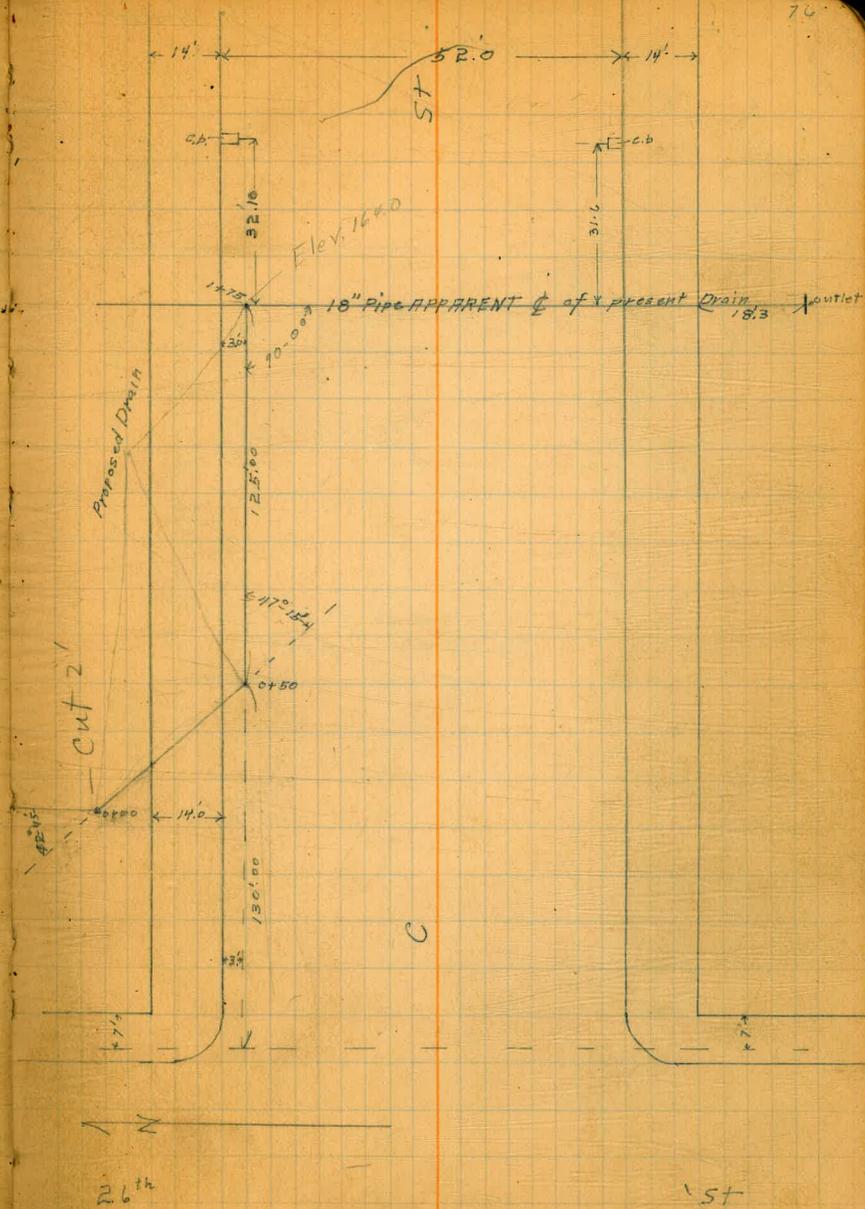
N 1/2 of street
has been graded
and sidewalk +
curb in O.K.

S 1/4		4.6
⊕		4.3
+ 4.5 N edge s/w		4.72
+ 9.5 S ✓ ✓		4.74
SL		4.5
	150' E	
SL		4.9
+ 4.5 S edge s/w		4.53
+ 9.5 N ✓ ✓		4.55
⊕		4.3
S 1/4		4.6
⊕		4.4
	200' E = W L RAY ST.	
⊕		4.0
S 1/4		4.3
+ 12		4.8
⊕ on cen return		4.33
+ 4.5 N edge s/w		4.29
+ 9.5 S ✓ ✓		4.26
SL		4.2

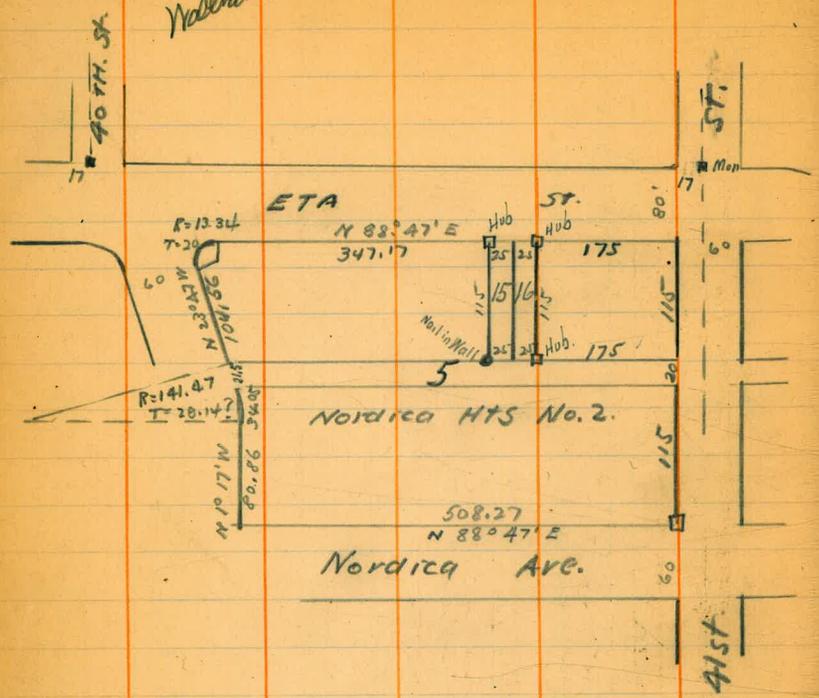
Drain
C. St East of 26

11/28/25
mills

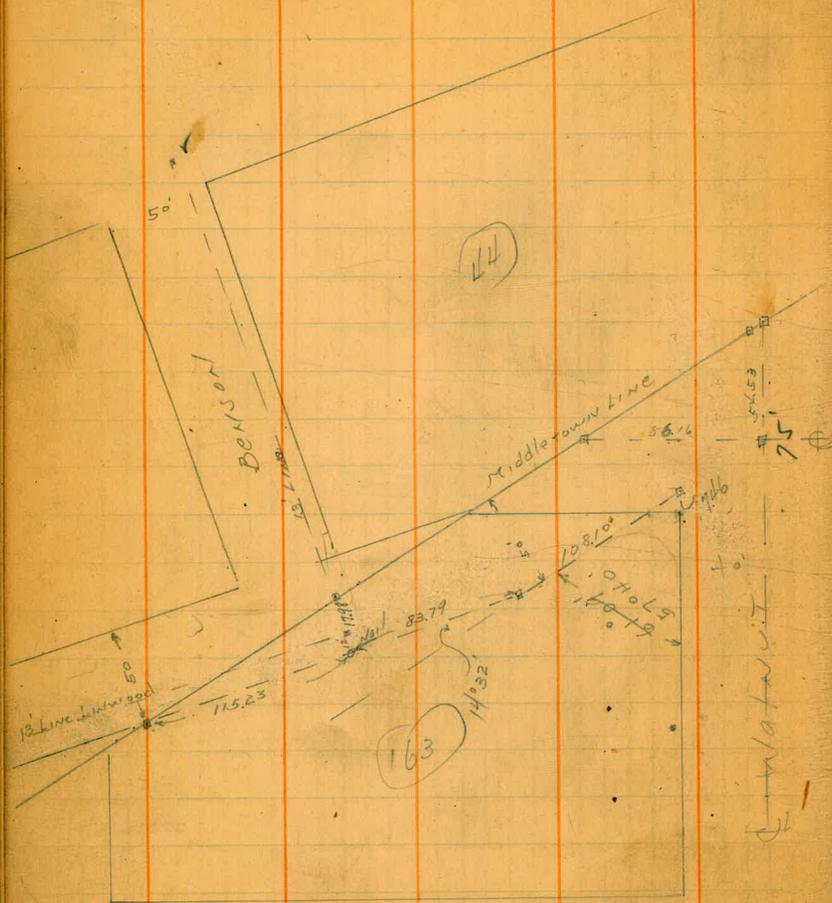
B.M.				197.00	N.W. 26 th + E
T.P.	0.37	197.37	12.08	185.29	
100' N. of 4+00			13.6	173.3	
60' N. of 4+00			13.6	173.3	
20' N. of 4+00			12.2	174.7	
0+00			11.6	175.3	
0+05			10.7	176.2	
0+18			5.3	181.6	
0+32			3.50	183.36	on edge walk
0+46			4.60	182.26	on cmt curb
0+46.2			5.8	181.1	gutter
0+50 Δ			6.5	180.4	
1+00			11.8	175.1	
T.P.	4.03	177.96	12.93	173.93	
1+25			5.1	172.9	
1+50			6.6	171.4	
1+75			7.1	170.9	
1+75 apparent connection with existing 18" cmt pipe					
T.P.	2.72	168.09	12.59	165.37	
Flowline of 18" cmt. Pipe outlet					
			11.77	156.32	



2/28/26
Survey Lots 15 & 16 Nordica
Hghts # 2 for Mc Rau
Suzanne
Walbrecht



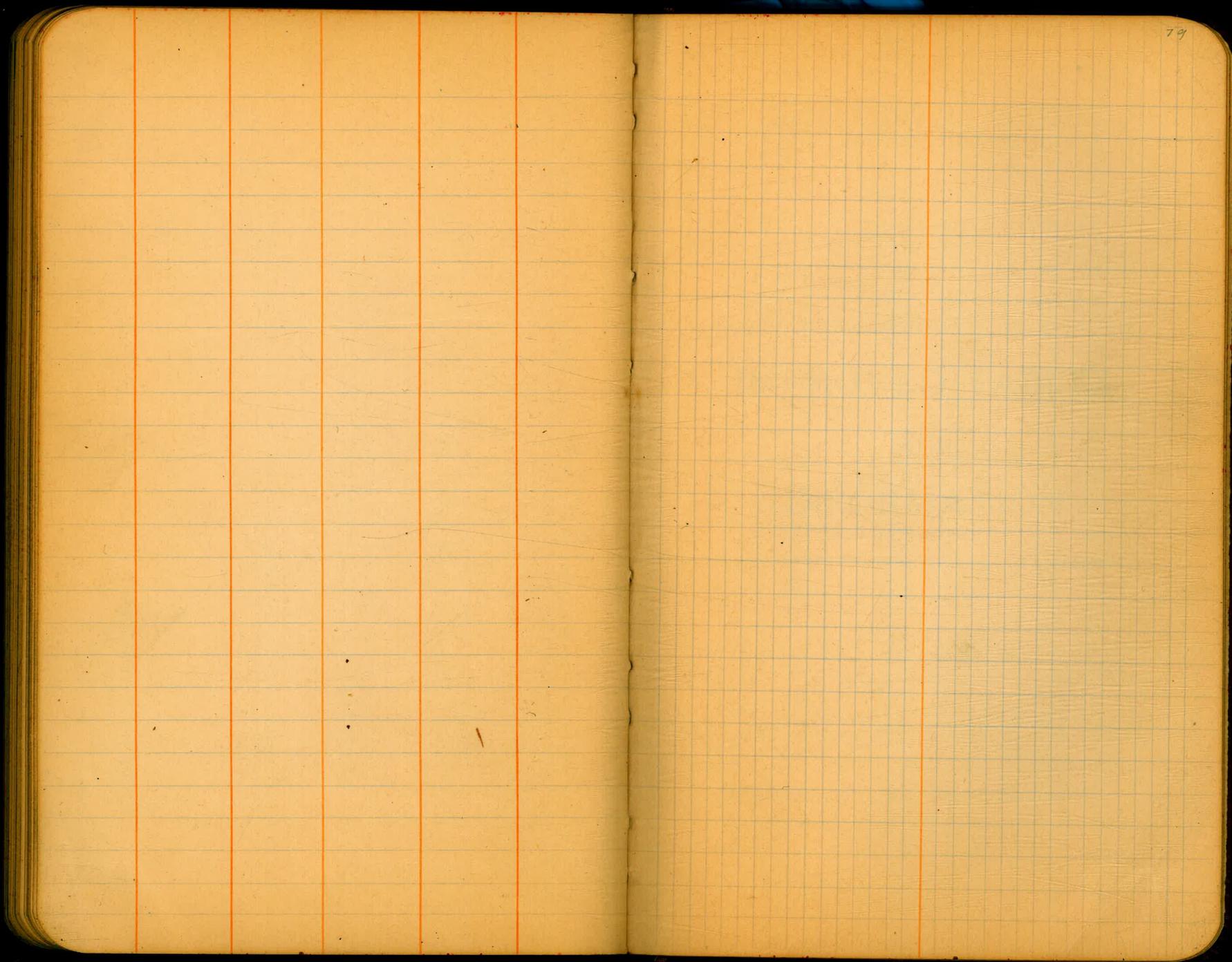
Survey for opening of Linwood Moore
 thru BIK 163 Middletown 6/11/66



57-40'
 90-00-30
 147-40-30
 32-19-30

union

to
 163



N 6276.50 Louis

4

39° 42' 6" = ACACIA
Epsilon

155
37.5

192.5
70

262.5
37.5

300.0

2031 = 1/2
21.87 = cb = DEITA

115
24.41

90.59

45
31

76
45

12° 30'

1447 cb
1324 1/2
NWK other

35.20
6.21

28.99

37.5
15

22.5

79.98
45

124.96
80
45

125

49
23

19.3
81.8

25
93

3.23
14

183

