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X Sec - TENNYSON -	Chatsworth	to Sterne.	1 to 7
" " "	Willow	to "	31 to 40
" " STERNE	"	to Tennyson	7 to 20
" " RESSELL	"	to Udahl	20 - 25
" " CAPISTRANO	Voltaire	to Quimby	40 - 48
" " PLUM.	Russell	to Udahl	25 31
" " Chatsworth	Macauley	to Voltaire	58 - 76
" " Voltaire	Chatsworth	to clove	49 - 58
" " Chatsworth Blvd.	Macaulay	to Voltaire	58 - 76

Flood Page Rewinden 9/27/29

X section Tennyson St

60' St
10' Cbs
10' Yds

E Line Chatsworth to E Line Sterne

B.M.S.E.B.P.	7.36	104.01		96.65 Chatsworth & Tennyson

0 – 25 = E Edge Paving on Chtswth

N.L. Tennyson projected	7.58	96.45
E Cb Tennyson "	7.66	96.35
1/4 " "	7.78	96.23
℄ " "	7.85	96.16
1/4 " "	7.92	96.09
S Cb " "	8.00	96.01
S.L. " "	8.18	95.83

0 – 10 = E Cb Chtsworth

S.L. Top Cb	7.36	96.65
S.L. in cement Gutter	8.36	95.65
S Cb	8.1	95.9
1/4	8.0	96.0
℄	7.9	96.1
1/4	7.7	96.3
N Cb	7.6	96.4
N Line in Cmt Gutter	7.82	96.19
N.L. Top Cb	6.90	97.11

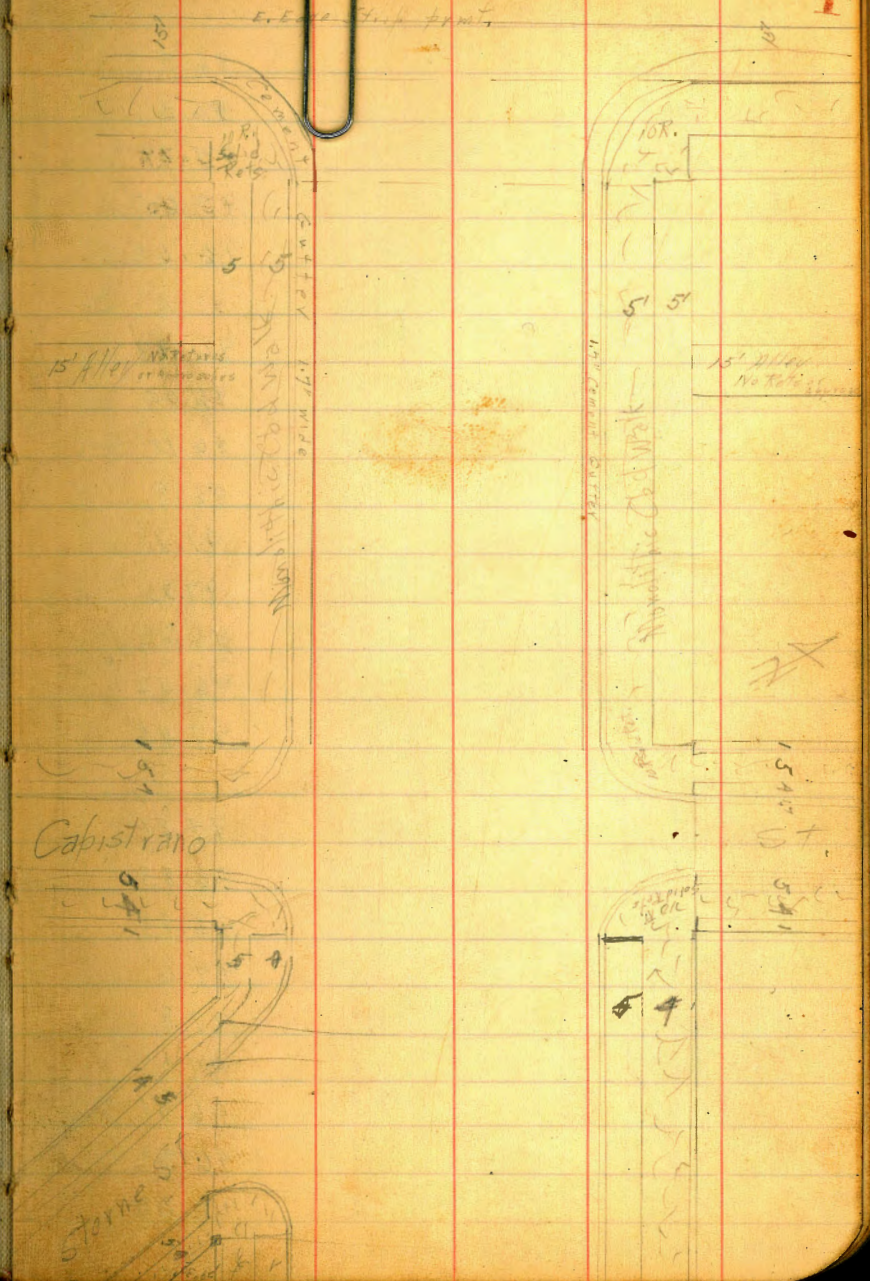
Plotted 10/11/29 BH.

0+00 = E.L. Chatsworth

Cbs., S. walk in good condition Gutters Not much Good

N Cb Top	6.86	97.15
Gut	7.80	96.21
+ 1.7 = edge of Cmt Gutter	7.64	96.37
1/4	7.6	96.4

Chatsworth St



	104.01		
	+		
℄		7.5	96.5
1/4		7.7	96.3
+8.3 = Edge of Cement Gutter		8.22	95.79
Gut		8.36	95.65
SCb Top		7.39	96.62
	0+50		
SCb Top		7.01	96.97
Gut.		8.01	96.00
+1.7		7.90	96.11
1/4		7.2	96.8
℄		6.6	97.4
1/4		6.8	97.2
+8.3		7.39	96.62
Gut		7.49	96.52
NCb Top		6.55	97.46
	1+00		
NCb Top		6.20	97.81
Gut.		7.18	96.83
+1.7		7.04	96.97
1/4		6.4	97.6
℄		6.2	97.8
1/4		6.8	97.2
+8.3		7.50	96.51
Gut		7.68	96.33
SCb Top		6.68	97.33

	104.01		
	1+36.92 = W.L. Alley		2
3.2		5.2	98.8
+4 = Edge of Walk		6.39	97.62
SCb Top		6.53	97.48
Gut		7.50	96.51
+1.7		7.31	96.70
1/4		6.5	97.5
℄		5.9	98.1
1/4		6.1	97.9
+8.3		6.81	97.20
Gut		6.95	97.06
NCb		5.96	98.05
+6		5.83	98.18
N.L.		4.8	99.2
	1+41.2 = E.L. Alley		
N.L.		5.5	98.5
+4		5.73	98.28
Cb		5.85	98.16
Gut		6.73	97.28
+1.7		6.62	97.39
1/4		6.1	97.9
℄		5.8	98.2
1/4		6.5	97.5
+8.3		7.33	96.78
Gut		7.42	96.69
Cb		6.41	97.60
+6		6.27	97.74
S.L.		5.5	98.5

	1040		
	1+92		
SCb.	6.05	97.96	
Gut	7.01	97.00	
+1.7	6.90	97.11	
1/4	6.2	97.8	
E	5.4	98.6	
1/4	5.8	98.2	
+8.3	6.24	97.77	
Gut	6.35	97.66	
NCb.	5.41	98.60	
	2+40		
NCb.	4.89	99.12	
Gut	5.83	98.18	
+1.7	5.78	98.23	
1/4	5.3	98.7	
E	4.9	99.1	
1/4	5.7	98.3	
+8.3	6.56	97.45	
Gut	6.68	97.33	
SCb.	5.73	98.28	
	2+90		
SCb.	5.35	98.66	
Gut	6.27	97.74	
+1.7	6.14	97.87	
1/4	5.2	98.8	
E	4.4	99.6	

	1040		
1/4		4.7	99.3
+8.3		5.33	98.68
Gut		5.43	98.58
NCb		4.49	99.52
	3+05 = Brk in Grade ✓		
NCb.		4.38	99.67
Gut		5.28	98.73
+1.7 Gutter Broken out			
1/4		4.6	99.4
E		4.2	99.8
1/4		5.0	99.0
+8.3		5.17	98.04
Gut		6.10	97.91
SCb		5.18	98.83
	3+40		
SCb.		4.42	99.59
Gut		5.31	98.70
+1.7		5.24	98.77
1/4		4.4	99.6
E		3.7	100.3
1/4		4.1	99.9
+8.3		4.40	99.61
Gut		4.50	99.51
NCb Job		3.58	100.43

		104.01						
		3+90						
N Cb			2.48	101.53				
Gut			3.40	100.61				
+1.7			3.30	100.71				
1/4			2.9	101.1				
℄			2.9	101.1				
1/4			3.5	100.5				
+8.3			4.19	99.82				
Gut			4.28	99.73				
SCb			3.37	100.64				
T.P.	104.6	112.62	1.85	102.16 TP				
		4+40						
S Cb.			10.84	101.78				
Gut			11.75	100.87				
+1.7			11.69	100.93				
1/4			11.0	101.6				
℄			10.7	102.4				
1/4			10.3	102.3				
+8.3			10.70	101.92				
Gut			10.89	101.75				
NCb			9.93	102.69				
		4+90						
NCb			8.81	103.81				
Gut			9.69	102.93				
+1.7			9.57	103.05				
1/4			9.0	103.6				

						112.62		
					℄		8.7	103.9
					1/4		9.4	103.2
					+8.3		10.52	102.10
					Gut		10.68	101.94
					SCb		9.80	102.82
					5+61.92 = W.C. Capistrano			
					SCb.		9.51	103.11
					Gut		10.40	102.22
					+1.7		10.26	102.36
					1/4		9.1	103.5
					℄		8.4	104.2
					1/4		8.6	104.0
					+8.3		9.74	103.38
					Gut		9.34	103.28
					NCb.		8.50	104.12
						W.Cb		
					N.L. Cb top		7.86	104.76
					N.L. Gut		8.66	103.96
					Cb.		8.5	104.1
					1/4		8.3	104.3
					℄		8.3	104.3
					1/4		9.0	103.6
					Cb		9.6	103.0
					St Gut		10.38	102.24
					St. Tk.		9.53	103.09

112,62

W 1/4

S.L.		9.8	102.8
Cb.		9.2	103.4
1/4		8.7	103.9
℄		8.2	104.4
1/4		8.0	104.6
Cb.		8.1	104.5
N.L.		7.8	104.8
	℄		
N.L.		7.7	104.9
Cb.		7.8	104.8
1/4		7.7	104.9
℄		8.0	104.6
1/4		8.4	104.2
Cb.		9.0	103.6
S.L.		9.6	103.0
	E 1/4		
S.L.		9.6	103.0
Cb.		9.0	103.6
1/4		8.5	104.1
℄		7.8	104.8
1/4		7.5	105.1
Cb.		7.4	105.2
N.L.		7.3	105.3
	E Cb.		
N.L. Top		6.98	105.64

112,62

Gut		7.2	105.4
Cb		7.1	105.5
1/4		7.3	105.3
℄		7.7	104.9
1/4		8.2	104.4
Cb.		8.6	104.0
S.L.		9.2	103.4
Cb Broken out all around Return			
0+00 = E.L. Capistrano			
S.L.		8.0	104.6
Cb Cb broken out		8.0	104.6
1/4		7.2	105.4
℄		7.0	105.6
1/4		6.7	105.9
Cb Top		6.50	106.12
N.L.		6.1	106.5
0+28.36 = Line of Sterne St on S.			
N.L.		1.5	111.1
+5 = edge walk toward Cb		2.42	110.20
Cb		2.61	110.01
Gut		3.5	109.1
1/4		3.3	109.3
℄		4.2	108.4
1/4		4.4	108.2
+7		4.8	107.8

No Gutters in this Block

	+	H	−	Elev
Cb line Cb gone			5.6	107.0
+3			4.2	108.4
+5 edge Walk			3.99	108.63
S.L.			3.8	108.8
W. Cb of Sterne (20.7)				
S.L. W. Cb of Sterne St			0.60	112.02
Gut. (cb undermined)			1.9	110.7
Cb.			2.0	110.6
1/4			1.8	110.8
℄			0.7	111.9
1/4			0.9	111.7
Gut			0.5	112.1
T.P.	11.81	123.91	1.07	111.10
Cb (broken down)			10.60	112.81
+5 on S. Walk			10.42	112.99
N.L.			9.8	113.6
W ¼ Sterne				
N.L.			7.5	115.9
+5 = Walk			7.69	115.73
Cb Line end of (cb gone)			8.9	114.5
1/4			8.9	114.5
℄			8.7	114.7
1/4			9.1	114.3
Cb Good			9.4	114.0
S.L.			9.4	114.0

	+	H	−	Elev
℄ Sterne				
S.L.			5.5	117.9
Cb.			6.1	117.3
1/4			6.1	117.3
℄			6.2	117.2
1/4			6.1	117.3
Gut			6.5	116.9
Cb (sunken)			5.06	118.35
+5 = walk			4.85	118.56
N.L.			4.5	118.9
E ¼ Sterne				
N.L.			1.8	121.6
+5 = Walk			1.91	121.50
Cb			2.11	121.30
Gut			2.7	120.7
1/4			3.4	120.0
℄			3.2	120.2
1/4			3.2	120.2
Cb			3.5	119.9
S.L.			3.0	120.4
E Cb line of Sterne Projected				
S.L.			0.7	123.2
Cb			1.0	122.4
1/4			0.4	123.0
℄			0.0	123.4
1/4			0.1	123.3

123.41

	+	⊼	−	Elev
T.P.	9.66	132.67	0.40	123.01
Gut.			9.3	123.4
Cb.			8.50	124.17
+5 on walk			8.34	124.33
N.L.			7.9	124.8
E.L. Sterne				
N.L.			5.1	127.6
+5			5.36	127.31
Cb.			6.4	126.3
1/4			6.7	126.0
℄			6.3	126.4
1/4			6.8	125.9
Gut			7.2	125.5
Cb. Top P.C. Ret			6.78	125.89
S.L.			6.4	126.3
T.P. Nail in Bank ∠ of Sterne			0.22	132.45

See P 30 this book for continued Notes on Tennyson

Xsection Sterne St 60' St 10' Cbs

7

	+	⊼	−	Elev	
T.P.	8.79	121.39		111.60 Sec b.6.	
See A = S.L. Tennyson					
intersection				10.8	109.6
+10				9.84	110.55
+20 Top Cb				8.30	112.09
+20 Gutter				9.2	111.2
+30				8.0	112.4
+40				6.2	114.2
+50				4.5	115.9
+60				2.2	118.2
+70				0.9	119.5
+80				0.0	120.4
+90	1.2				121.6
1+00	2.8				123.2
1+00	3.5				123.9
1+21.39	4.8				125.2
See B from W.L. Sterne to S.L. Tennyson					
N.L.				6.5	113.9
+5 edge of walk toward Cb.				6.92	113.47
Cb Top				6.95	113.44
Gutter				9.0	111.4
+5				8.4	112.0
See C from W.L. Sterne to S.L. Tennyson					
N.L.				2.5	117.9
+5 edge Walk				2.75	117.64

Plotted 10/14-29 GBH

		120.39			
	+	⊼	−	Elev	
Cb			2.83	117.56	
Gutter			4.7	115.7	
1/4			3.6	116.8	
℄ = St. Tennyson			2.2	118.2	
T.P.	9.21	127.87	1.73	118.66	
Sec D from W.L. Sterne to St. Tennyson					
W.L.			6.2	121.7	
+ 5 = edge of Walk			6.56	121.31	
Cb. line Cb broken down			8.1	119.8	
1/4			7.7	120.2	
℄			6.3	121.6	
1/4			6.4	121.5	
+ 4			6.4	121.5	
Sec 0+00. from W.					
W.L.			3.2	124.7	
+ 5 = edge of Walk Toward Cb			3.13	124.74	
Cb. Line (Cb broken)			3.4	124.5	
Gutter			4.9	123.0	
1/4			3.9	124.0	
℄			2.8	125.1	
1/4			2.8	125.1	
Gut			2.4	125.5	
Cb. Top. (good)			2.12	125.75	
E.L. = St. Tennyson			1.67	126.20	
T.P.	12.51	139.96	0.42	127.45	

		139.96			
	+	⊼	−	Elev	
		0+25			
E.L.			10.5	129.5	
+ 1.5			11.2	128.8	
+ 5	on walk		11.46	128.50	
+ 5	on dirt		12.0	128.06	
+ 5.5			12.0	128.0	
Cb.			11.68	128.28	
Gut			12.5	127.5	
1/4			12.2	127.8	
℄			12.2	127.8	
1/4			13.2	126.8	
Cb Line			15.1	124.9	
+ 5 = walk			12.63	127.33	
W.L.			13.0	127.0	
T.P.	12.82	145.27	7.51	132.45	
		0+50			
W.L.			15.6	129.7	
+ 5 = Walk			15.31	129.96	
Cb. (Cb broken out			16.3	129.0	
1/4			15.6	129.7	
℄			14.5	130.8	
1/4			14.6	130.7	
Gut			15.1	130.2	
Cb			14.33	130.94	
+ 5			14.18	131.09	

	+	H.I.	−	Elev	
		145.27			
+9			14.1	1	131.2
E.L.			13.6		131.7
		0+75			
E.L.				12.7	132.6
+2				11.43	133.84
+5 = edge of walk				11.51	133.76
Cb.				11.7	133.56
Gutter				12.6	132.7
℄				12.0	133.3
℄				11.8	133.5
1/4				12.5	132.8
Gutter				13.1	132.2
Cb.				12.74	132.53
+5 = edge of walk				12.75	132.52
W.L.				13.0	132.3
		1+00			
W.L.				10.2	135.1
+5				10.13	135.14
Cb.				10.15	135.12
Gut.				10.7	134.6
1/4				9.7	135.4
℄				9.3	136.0
1/4				9.3	136.0
Gut				10.7	135.1
Cb.				9.06	136.21

	+	H.I.	−	Elev	
		145.27			
+5			8.88		136.39
+8			8.7		136.6
E.L.			8.3		137.0
		1+25			
E.L.			5.9		139.4
+5 = walk			6.17		139.10
Cb.			6.43		138.84
Gut			7.5		137.8
1/4			6.5		138.8
℄			6.4		138.9
1/4			7.3		138.0
Gut			8.2		137.1
Cb.			7.63		137.64
+5			7.48		137.79
W.L.			7.9		137.4
		1+50			
W.L.			5.0		140.3
+1			4.78		140.49
+5			4.96		140.31
Cb.			5.00		140.27
Gut			5.4		139.9
1/4			4.7		140.6
℄			3.9		141.4
1/4			3.9		141.4
Cut			4.4		140.9

	+	π	−	Elev
		145.27		
Cb			3.73	141.54
+5			3.53	141.74
+9			3.46	141.81
E.L.			3.0	142.3
		1+75		
E.L.			0.3	145.0
+1			0.79	144.48
+5			0.94	144.33
Cb.			1.01	144.26
Gut			2.0	143.3
1/4			1.4	143.9
℄			1.4	143.9
1/4			2.2	143.1
Gut			2.9	142.4
Cb			2.45	142.82
+5			2.39	142.88
+9			2.28	142.99
W.L.			2.5	142.8
T.P.	11.89	155.79	1.37	143.90
		2+00		
W.L.			10.5	145.3
+1 } on walk			10.23	145.56
+5 }			10.32	145.47
Cb			10.20	145.59
Gut			10.[illegible]	145.4

	+	π	−	Elev
		155.79		
1/4			10.0	145.8
℄			9.3	146.5
1/4			9.5	146.3
+8			9.5	146.3
+9 m/ Gut			11.0	144.8
Cb (curb is undermined from sta 1+90 to sta. 2+40)			9.00	146.89
+5 on walk (bank sloughed over sidewalk)			8.86	146.93
E.L.			7.4	148.4
		2+25		
E.L. } bank sloughed onto walk			4.6	151.2
+5 on walk }			6.32	149.47
Cb.			6.46	149.33
Gut			8.2	147.6
+3			7.0	148.8
1/4			6.9	148.9
℄			6.8	149.0
1/4			7.7	148.1
Gut			8.3	147.5
Cb			7.74	148.05
+5			7.78	148.01
+9			7.68	148.11
W.L.			8.0	147.8
		2+50		
W.L.			5.4	150.4
+1			5.31	150.48

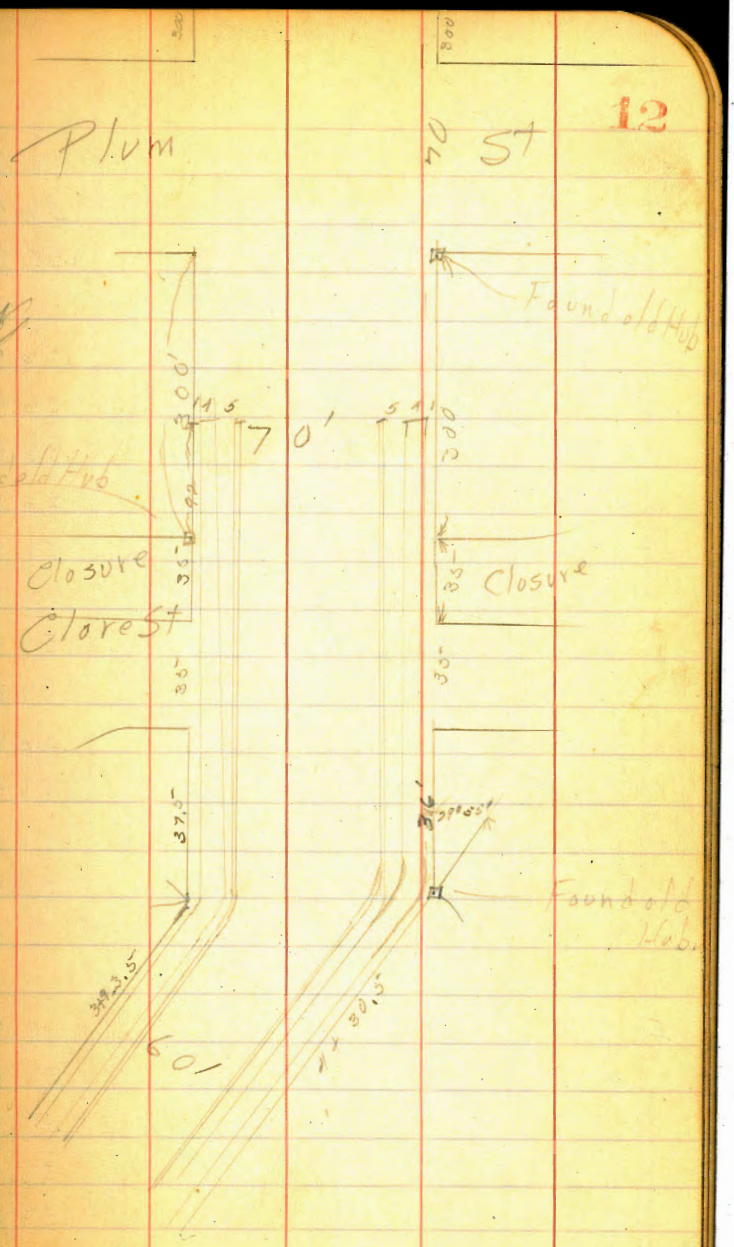
155.79

	+		−	Elev
+ 5			5.34	150.45
Cb			5.37	150.42
Gut			6.1	149.7
℄			5.3	150.5
℄			4.7	151.1
℄			4.8	151.0
Gut			4.9	150.9
Cb.			4.01	151.78
+ 5			3.88	151.91
E.L.			1.9	153.9
	2 + 75			
E.L.			0.1	155.7
+ 5			2.10	153.69
Cb.			2.17	153.62
Gut			3.1	152.7
℄			2.8	153.0
℄			2.8	153.0
℄			3.3	152.5
Gut			4.0	151.8
Cb.			3.36	152.43
+ 5			3.32	152.47
W.L.			3.1	152.7
T.P.	8.38	161.49	2.68	153.11
		3+00		
W.L.			7.7	153.8

161.49

	+	−	Elev
+ 5		7.60	153.89
Cb.		7.65	153.84
Gut		8.3	153.2
℄		7.7	153.8
℄		7.2	154.3
℄		7.2	154.3
Gut		7.6	153.9
Cb		6.67	154.87
+ 5		6.57	154.92
E.L.		4.9	156.6
	3+25		
E.L.		4.3	157.2
+ 3 Top of slope of bank		5.4	156.1
+ 5 edge of walk		5.73	155.76
Cb		5.84	155.65
Gut		6.7	154.8
℄		6.2	155.3
℄		6.1	155.4
℄		6.4	155.1
Gut		7.3	154.2
Cb.		6.78	154.71
+ 5		6.69	154.80
+ 9		6.66	154.83
W.L.		6.9	154.6

	+	I	−	Elev
		3+50		
W.L.			6.0	155.5
+1			5.72	155.77
+3			5.80	155.69
Cb			5.93	155.56
Gut			6.7	154.8
Rd			5.6	155.9
℄			5.3	156.2
Rd			5.4	156.1
G			5.8	155.7
Cb			5.14	156.35
+5			5.07	156.42
+6			5.0	156.5
E.L.			3.3	158.2
		3+75		
E.L.			3.3	158.2
+2			4.2	157.3
+3			4.46	157.03
Cb.			4.53	156.96
G.			5.2	156.3
Rd			4.8	156.7
℄			4.5	157.0
Rd			5.0	156.5
G.			5.9	155.6
Cb.			5.73	156.26



	+	⊼	−	Elev
		161.49		
+5			5.15	156.34
+9			5.04	156.45
W.L.			5.6	155.9
		3+93.5 = Δ on E		
W.L.			5.1	156.4
+1			4.56	156.93
+5			4.63	156.86
Cb.			4.71	156.78
G.			5.4	156.1
1/4			4.4	157.1
℄			4.1	157.4
1/4			4.3	157.2
G			4.7	156.8
Cb.			4.09	157.40
+5			3.89	157.60
E.L.			3.6	157.9
		3+93.5 on N.E. to 4+30.5 on S.W. = 70' St		
		10' Cbs 12.5 1/4s		
E.L. or N.L.			3.6	157.9
+5			3.81	157.68
Cb.			3.95	157.54
G			4.6	156.9
1/4			3.9	157.6
℄			3.5	158.0
1/4			4.1	157.4

	+	⊼	−	Elev
		161.49		
G.			4.6	156.9
Cb.			3.93	157.56
+5			3.80	157.69
W.L. or S.L.			3.9	157.6
		4+31 on N to 4+66.5 on S = W.L. Clove St		
S.L. − 5			4.8	156.7
S.L.			3.3	158.2
+5			3.27	158.22
Cb			3.33	158.16
G			4.1	157.4
1/4			3.3	158.2
℄			2.7	158.8
1/4			3.2	158.3
G			3.8	157.7
Cb			3.28	158.21
+5			3.08	158.41
+7			2.9	158.6
N.L.			1.4	160.1
		+35 = old ℄ Clove St = New E.L. Clove		
		No Cbs or 1/4s taken on this intersection as Grading, Cbs & S. walks continue across it on uniform grade		
N.L.			2.2	159.3
+5 = edge of walk			2.38	159.11
Cb.			2.57	158.92
G			3.2	158.3

	+	161.49	−	Elev
1/4			2.6	158.9
℄			3.3	159.2
1/4			2.9	158.6
G			3.6	158.9
Cb.			2.84	158.65
+5			2.76	158.73
+9			2.77	158.72
S.L.			3.4	158.1
+30			19.9	141.6
+35			21.0	140.5
	+35 = Old E.L. Clare = 0+00			
−20			9.9	151.6
−15			9.7	151.8
S.L.			3.3	158.2
+1			2.38	159.11
+5			2.27	159.22
Cb.			2.49	159.00
G			3.2	158.3
1/4			2.6	158.9
℄			1.7	159.8
1/4			1.9	159.6
T.P.	10.03	169.62	1.90	159.59
G			10.6	159.0
			9.98	159.64
			9.80	159.82
			9.7	159.9

	+	169.42	−	Elev
	0+50			
N.L.			8.5	161.1
+5			8.80	160.82
Cb.			9.07	160.55
G			9.8	159.8
1/4			9.3	160.3
℄			9.5	160.1
1/4			9.5	160.1
G.			10.1	159.5
Cb.			9.41	160.21
+5			9.28	160.34
+9			9.21	160.41
S.L.			9.5	160.1
+5			9.5	160.1
	0+92 = End of Cb & Walks			
S.L.			7.6	162.0
+1			8.20	161.42
+5			8.38	161.24
Cb.			8.49	161.13
G			8.9	160.7
1/4			8.4	161.2
℄			8.4	161.2
1/4			8.3	161.3
G			8.4	161.2
Cb			7.92	161.70

	+	π	−	Elev
		169.62		
+5			7.82	161.80
+9			7.70	161.92
N.L.			7.6	162.0
		1+00 = 70'S + 18' Cbs 8.5 1/4s		
N.L.			7.6	162.0
Cb.			8.1	161.5
1/4			8.0	161.6
℄			7.8	161.8
1/4			7.9	161.7
Cb.			8.1	161.5
+16			8.4	161.2
S.L.			7.5	162.1
		1+25		
S.L.			4.1	165.5
Cb.			5.0	164.6
+3			5.9	163.7
1/4			5.7	163.9
℄			5.7	163.9
1/4			6.1	163.5
Cb.			6.7	162.9
S.L.	N		6.6	163.0
		1+50		
S.L.	N		6.0	163.6
Cb.			5.7	163.9
1/4			5.3	164.3

	+	π	−	Elev
		169.62		
℄			5.0	164.6
1/4			5.0	164.6
+8			5.0	164.6
Cb.			4.6	165.0
S.L.			3.1	166.5
		1+75		
S.L.			3.6	166.0
Cb			3.1	166.5
+2			3.4	166.2
+4			4.6	165.0
1/4			4.7	164.9
℄			4.5	165.1
1/4			4.9	164.7
Cb			5.3	164.3
+10			5.7	163.9
N.L.			4.9	164.7
		2+00		
N.L.			6.0	163.6
+14			5.7	163.9
Cb.			5.2	164.4
1/4			4.6	165.0
℄			4.2	165.4
1/4			4.4	165.2
+3			4.4	165.2
+5			3.3	166.3

	+	169.62 ⊼	−	Elev
Cb			3.3	166.3
S.L.			3.2	166.4
		2+25		
S.L.			3.3	166.3
Cb.			4.4	165.2
1/4			4.8	164.8
℄			4.2	165.4
1/4			4.4	165.2
Cb			5.0	164.6
N.L.			6.2	163.4
		2+50		
N.L.			6.5	163.1
Cb			5.4	164.2
1/4			5.0	164.6
℄			4.8	164.8
1/4			5.3	164.3
Cb			5.3	164.3
S.L.			3.9	165.7
		2+75		
S.L.			4.1	165.5
Cb.			5.7	163.9
1/4			5.9	163.7
℄			5.2	164.4
1/4			5.4	164.2
Cb.			5.7	163.9

	+	169.62 ⊼	−	Elev
+3			5.6	164.0
+5			4.5	165.1
N.L.			6.2	163.4
		3+00 = W.L. Plum St.		
		70' St 18' cbs 8.5' ½s		
N.L.			7.2	162.4
+12			6.1	163.5
+13			6.8	162.8
Cb			6.4	163.2
1/4			6.2	163.4
℄			6.3	163.3
1/4			6.6	163.0
Cb.			6.2	163.4
S.L.			4.3	165.3
		W.Cb Plum		
S.L.			6.4	163.2
Cb.			7.0	162.6
1/4			7.1	162.5
℄			6.7	162.9
1/4			7.0	162.6
Cb			7.3	162.3
N.L.			7.7	161.9
		W 1/4		
N.L.			7.8	161.8
Cb			7.8	161.8

169.62

	+	⊼	−	Elev	
1/4				7.8	161.8
℄				7.6	162.0
1/4				7.3	162.3
Cb				7.2	162.4
S.L.				6.3	163.3
		℄ P/vm			
S.L.				6.8	162.8
Cb				7.3	162.3
1/4				7.3	162.3
℄				7.3	162.3
1/4				7.9	161.7
Cb				7.9	161.7
N.L.				7.7	161.9
		E 1/4			
N.L.				7.6	162.0
Cb.				8.0	161.6
1/4				7.3	162.3
℄				7.1	162.5
1/4				7.5	162.1
Cb.				7.5	162.1
S.L.				7.0	162.6
		E Cb P/vm			
S.L.				5.5	164.1
Cb				7.0	162.6
1/4				7.8	161.8

169.63

	+	⊼	−	Elev	
℄				7.7	161.9
1/4				7.8	161.8
Cb.				8.4	161.2
N.L.				8.0	161.6
		E.L. P/vm = 0+00			
N.L.				8.1	161.5
Cb.				8.4	161.2
1/4				8.6	161.0
℄				7.1	162.5
1/4				7.1	162.5
Cb.				6.0	163.6
S.L.				3.9	165.7
T.P.	7.61	174.54		3.69	166.93
		0+25			
S.L.				7.8	163.7
+ 4				7.7	163.8
+ 10				10.3	164.2
Cb.				11.3	163.2
1/4				11.7	162.8
℄				11.9	162.6
1/4				12.7	161.8
Cb				13.7	160.8
N.L.				13.2	161.3
+ 15				12.4	162.1

	+	17454 ℄	−	Elev
		0+50		
N.L. −15			12.6	161.9
N.L.			12.6	161.9
+8			12.5	162.0
Cb			11.7	162.8
1/4			11.8	162.7
℄			11.4	163.1
1/4			12.5	162.0
Cb.			12.4	162.1
+8			12.1	162.4
+15			7.1	167.4
S.L.			7.1	167.4
		0+65		
S.L.			7.2	167.8
Cb.			7.5	167.0
1/4			9.7	164.8
℄			10.9	163.6
1/4			11.0	163.5
Cb.			11.9	162.6
+9.			12.5	162.0
N.L.			11.2	163.3
+9			12.4	162.1
+15			12.3	162.2
		0+70		
N.L. −20			11.0	163.5

From Sta 0+50 to Wil. Willow Stream has been partly filled

	+	17454 ℄	−	Elev
N.L. −14			8.8	165.7
N.L −9			10.4	164.1
N.L.			8.9	165.6
Cb.			8.7	165.8
1/4			9.1	165.4
℄			9.0	165.5
1/4			8.0	166.5
Cb.			7.3	167.2
S.L.			7.1	167.4
		1+00		
S.L.			6.4	167.9
Cb.			7.5	167.0
1/4			7.5	167.0
℄			7.1	167.4
1/4			7.4	167.1
Cb			7.2	167.3
N.L.			7.4	167.1
+8			7.8	166.7
+18			10.8	163.7
		1+50		
−12			9.4	165.1
−6			5.8	168.7
N.L.			6.3	168.2
Cb			5.8	168.7
1/4			5.9	168.6

174.54

	+	℄	−	Elev
℄			6.4	168.1
1/4			6.2	168.3
Cb			6.3	168.2
S.L.			6.4	168.1
		2+00		
S.L.			5.4	169.1
Cb.			5.4	169.1
1/4			5.0	169.5
℄			3.5	171.0
1/4			4.4	170.1
Cb.			4.3	170.2
N.L.			1.0	170.5
+ 3			4.1	170.4
+ 10			7.3	167.2
		2+50		
− 10			5.9	168.6
− 2			3.3	171.2
N.L.			3.1	171.4
Cb.			3.0	171.5
1/4			2.3	172.2
℄			2.5	172.0
1/4			2.2	172.3
Cb.			2.1	172.4
+ 5			1.8	172.7
+ 10			3.3	171.2
S.L.			3.5	171.0

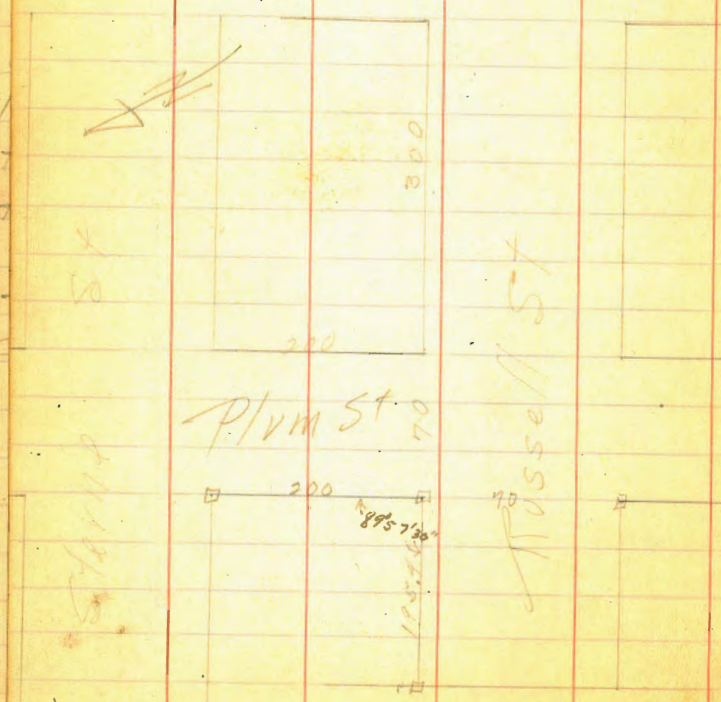
174.34

	+	℄	−	Elev
		2+75		
S.L.			3.0	171.5
Cb.			2.6	171.9
1/4			2.4	172.1
℄			2.3	172.2
1/4			1.9	172.6
Cb			2.2	172.3
+ 15			2.4	172.1
N.L.			3.2	171.3
+ 1			4.0	170.5
+ 5			4.1	170.4
		2+95		
N.L.			1.9	172.6
Cb.			2.0	172.5
1/4			2.3	172.2
℄			2.4	172.1
1/4			2.6	171.9
Cb			2.8	171.7
S.L.			2.7	171.8
		3+00 = W.L. Willow		
S.L.			2.6	171.9
+ 10 end of Cb on 43° ℄			2.66	171.88
Cut on pvmt			3.16	171.38
Cb Line on pvmt			2.92	171.62
1/4	"	"	2.66	171.88

174.54

	+	π	—	Elev	
℄	on pvmt		2.51	172.03	
1/4	" "		2.47	172.07	
Cb Line +7.5	" "		2.37	172.17	
Gutter	" "		2.34	172.20	
End Cb on 43' R			1.54	173.00	
N.L.			1.4	173.1	
T.P.	4.78	177.47	1.85	172.69	
BM N.E.B.P.			0.32	177.15	Sterne & Willow

Willow



70' St
18' Cbs
85' 1/4 S

20

X section Russell St.

Willow To N.W'ly End 70' St 18' Cbs 85' 1/4 S

B.M. S.W. B.P. 9.56	170.92		161.36 corrected 161.33 (?)	Willow & Russell
0+00 = W.L. Willow				
S.L.		9.0	161.9	
+10.5 on Cb		9.64	161.28	✓
Gutter on paving		10.25	160.67	✓
Cb Line " "		10.29	160.63	
1/4 " "		10.33	160.59	
℄ " "		10.46	160.46	
1/4 " "		10.77	160.15	
Cb Line " " +7.5		11.13	159.79	
Gutter Lip of Cb basin		11.54	159.38	✓
Cb on 43' R. Rt.		10.58	160.34	✓
N.L.		10.1	160.8	
0+10				
N.L.		9.7	161.2	
Cb		10.5	160.4	
1/4		10.1	160.8	
℄		9.8	161.1	
1/4		9.8	161.1	
Cb.		9.2	161.7	
S.L.		8.5	162.4	
0+25				
S.L.		7.9	163.0	
Cb.		8.6	162.3	

	+	170.92	−	Elev
1/4			9.7	161.2
℄			9.7	161.2
1/4			9.8	161.1
Cb			10.1	160.8
N.L.			10.0	160.9
		0+75		
N.L.			8.8	162.1
Cb.			9.2	161.7
1/4			8.6	162.3
℄			8.3	162.6
1/4			8.1	162.8
Cb			7.1	163.8
S.L.			7.0	163.9
		1+00		
S.L.			5.3	165.6
Cb.			6.4	164.5
1/4			7.2	163.7
℄			7.2	163.7
1/4			7.4	163.5
Cb			8.0	162.9
N.L.			8.7	162.2
		1+50		
N.L.			6.2	164.7
Cb.			6.1	164.8
1/4			5.6	165.3

	+	170.92	−	Elev
℄			5.3	165.6
1/4			5.2	165.7
Cb			4.7	166.2
S.L.			4.2	166.7
		2+00		
S.L.			2.7	168.2
Cb.			3.2	167.7
1/4			3.7	167.2
℄			3.7	167.2
1/4			4.0	166.9
Cb.			4.8	166.1
N.L.			4.8	166.1
		2+50		
N.L.			2.3	168.6
Cb.			2.2	168.7
1/4			1.4	169.5
℄			1.0	169.9
1/4			0.6	170.3
T.P.	7.77	178.14	0.55	170.37
Cb.			7.3	170.8
S.L.			5.8	172.3
		2+75		
S.L.			5.7	172.4
Cb.			5.9	172.2
1/4			6.4	171.7

	+	π	−	Elev
		178.14		
℄			6.6	171.5
1/4			7.2	170.9
Cb			7.7	170.4
N.L.			7.7	170.4
		3+00: E.L. Plvm		70 St 18 Cbs 85 1/4
N.L.			6.4	171.7
Cb			6.6	171.5
1/4			6.4	171.7
℄			6.3	171.8
1/4			6.3	171.8
Cb			6.0	172.1
S.L.			4.5	173.6
		E Cb Plvm		
S.L.			3.9	174.2
Cb			5.6	172.5
1/4			6.1	172.0
℄			6.1	172.0
1/4			6.1	172.0
Cb			6.2	171.9
N.L.			5.4	172.7
		E 1/4		
N.L.			5.1	173.0
Cb			5.7	172.4
1/4			5.8	172.3
℄			5.9	172.1

	+	π	−	Elev
		178.14		
1/4			5.9	172.1
Cb			5.5	172.6
S.L.			4.2	173.9
		℄		
S.L.			4.2	173.9
Cb			5.4	172.7
1/4			5.7	172.4
℄			5.6	172.5
1/4			5.6	172.5
Cb			5.5	172.6
N.L.			4.7	173.4
		W 1/4		
N.L.			4.4	173.7
Cb			5.3	172.8
1/4			5.4	172.7
℄			5.7	172.4
1/4			5.7	172.4
Cb			5.5	172.6
S.L.			4.4	173.7
		W Cb		
S.L.			4.2	173.9
Cb			5.4	172.7
1/4			5.5	172.6
℄			5.5	172.6
1/4			5.5	172.6

178.14

	+	⊼	−	Elev
Cb.			5.2	172.9
N.L.			4.6	173.5
		0+00 = W.L. P/VM		
N.L.			4.6	173.5
Cb			5.7	172.4
1/4			5.2	172.9
℄			5.0	173.1
1/4			5.1	173.0
Cb			4.5	173.6
S.L.			4.1	174.0
		0+70		
S.L.			5.1	173.0
Cb.			3.9	174.2
1/4			4.9	173.2
℄			4.9	173.2
1/4			5.0	173.1
Cb			5.6	172.5
N.L.			5.9	172.2
		0+55 = Edge of 15' concrete apron		
		driveway to Garage 18' back of Edge		
N.L. −18		to driveway	5.81	172.33
N.L.			6.05	172.09
Cb.			5.5	172.6
1/4			5.5	172.6
℄			5.5	172.6

178.14

	+	⊼	−	Elev
1/4			6.1	172.0
Cb.			6.7	171.4
S.L.			7.7	170.4
		0+70 = W.L. P/ Apron on N		
−10			9.2	168.9
S.L.			8.6	169.5
Cb			7.9	170.2
1/4			7.1	171.0
℄			6.4	171.7
1/4			6.2	171.9
Cb.			5.9	172.2
N.L. 7 on Apron			6.07	172.07
+18			5.82	172.32 ✓
		0+80 = ℄ 3.5' Cemt S.W. on N 0.4 in St.		
N.L.			6.06	172.08
		1+00		
N.L.			6.1	172.0
+14			6.9	171.2
+17			8.2	169.9
Cb.			8.2	169.9
1/4			8.3	168.8
℄			8.6	169.5
1/4			9.4	168.7
Cb.			10.3	167.8
S.L.			10.8	167.3
+20			13.6	164.5

	+	H.I.	−	Elev
		178.14		
		1+25		
S.L. -35			17.0	161.1
S.L.			15.5	162.6
Cb.			12.9	165.2
1/4			11.3	166.8
℄			10.5	167.6
1/4			10.2	167.9
Cb.			10.1	168.0
+6			8.8	169.3
N.L.			8.0	170.1
		1+50		
N.L.			9.6	168.5
+10			10.7	167.4
Cb.			11.8	166.3
1/4			12.3	165.8
℄			12.7	165.4
T.P.	1.65	167.42	12.37	165.77
1/4			3.0	164.4
+5			4.6	162.8
Cb			5.0	162.4
S.L.			7.3	160.1
+30			12.8	154.6
		1+75		
−30			16.4	151.0
S.L.			11.8	155.6
Cb.			8.6	158.8

	+	H.I.	−	Elev
		167.42		
+5			7.7	159.7
1/4			6.4	161.0
+4			5.0	162.4
℄			4.5	162.9
1/4			4.0	163.5
Cb			3.3	164.1
+8			1.6	165.8
N.L.			0.5	166.9
	179654 S 44 N	to M 6.15		on S = W End Russell St
N.L.			3.0	164.4
+9			3.9	163.5
Cb.			5.5	161.9
1/4			6.3	161.1
℄			7.3	160.1
1/4			9.6	157.8
Cb.			10.9	156.5
S.L.			14.5	152.9
+30			21.2	146.2
		2+25		
−30			26.6	140.8
S.L. projected W.			19.3	148.1
Cb.	"	"	15.9	151.5
1/4	"	"	14.0	153.4
℄	"	"	13.1	154.3
1/4			11.7	155.7

	+	167.42 ⊼	−	Elev
Cb.	Projected W		9.9	157.5
N.L.	"	"	7.0	160.4
T.P.	8.32	174.09	1.65	165.77
T.P.	4.32	176.41	2.00	172.09

-90' 5" 18' 16.5 8.5 1/4 5

Xsection Plum, Russell to Udahl

0+00 = N.L. Russell

W.L.			2.9	173.5
Cb			2.9	173.5
1/4			2.7	173.7
℄			3.0	173.4
1/4			3.3	173.1
Cb			3.6	172.8
E.L.			4.6	171.8
		0+25		
E.L.			4.1	172.3
Cb			3.0	173.4
1/4			2.8	173.6
℄			2.5	173.9
1/4			2.4	174.0
Cb			2.7	173.7
+8			1.8	174.6
W.L.			2.2	174.2
		0+50		
W.L.			2.7	173.7

Plotted. Oct. 29-'29

	+	176.41 ⊼	−	Elev
+10			2.6	173.8
Cb.			2.9	173.5
1/4			2.6	173.8
℄			2.5	173.9
1/4			2.8	173.6
Cb			2.7	173.7
E.L.			4.6	171.8
		0+75		
−10			6.7	169.7
E.L.			5.8	160.6
Cb			4.6	161.8
1/4			4.4	162.0
℄			3.8	162.6
1/4			3.9	162.5
Cb			4.1	162.3
W.L.			3.8	162.6
		1+00		
W.L.			6.1	160.3
Cb.			6.5	169.9
1/4			6.2	170.2
℄			6.3	170.1
1/4			6.9	169.5
Cb.			7.4	169.0
E.L.			8.2	168.2
+10			8.7	167.7

	+	176.41 ±	−	Elev
		1+25		
−10			10.0	166.4
E.L.			9.5	166.9
Cb			8.9	167.5
1/4			8.7	167.7
℄			8.1	168.3
1/4			8.0	168.4
Cb.			8.4	168.0
+6.			7.5	168.9
W.L.			7.1	169.3
		1+50		
W.L.			8.7	167.7
+12			9.0	167.4
Cb.			9.7	166.7
1/4			9.3	167.1
℄			9.5	166.9
1/4			9.9	166.5
Cb			9.5	166.9
E.L.			10.3	166.1
+10			11.1	165.3
		1+75		
−10			10.3	166.1
E.L.			10.7	165.7
Cb.			11.5	164.9
1/4			11.9	164.5

	+	176.41 ±	−	Elev
℄			11.2	165.2
1/4			11.0	165.4
Cb			11.5	164.9
+2			10.8	165.6
W.L.			10.5	165.9 ✓
		2+00 = S.L. Storm St		
W.L.			11.2	165.2
Cb			13.2	163.2
1/4			13.1	163.3
℄			13.4	163.0
1/4			13.7	162.7
Cb.			12.3	164.1
E.L.			10.8	165.6
T.P.	6.96	172.38	11.09	165.32
		0+00 = N.L. Storm		
−10			10.8	161.5
E.L.			10.7	161.6
Cb			10.6	161.7
1/4			10.3	162.0
℄			10.4	161.9
1/4			10.4	161.9
Cb			10.3	162.0
W.L.			9.9	162.4
+10			9.4	162.4

SW cor Hub Storm St Plum

	+	172.28 +	−	Elev
		0+25		
−10			10.1	162.2
W.L.			10.3	162.0
Cb			10.1	162.2
1/4			9.6	162.7
℄			9.8	162.5
1/4			10.1	162.2
Cb			9.6	162.7
E.L.			8.7	163.6
+10			9.2	163.1
		0+50		
−10			9.0	163.3
E.L.			9.0	163.3
Cb			9.3	163.0
1/4			9.4	162.9
℄			8.9	162.4
1/4			8.7	163.6
Cb			9.2	163.1
+8.			8.5	163.8
W.L.			9.1	163.2
+10			9.8	162.5
		0+75		
−10			8.7	163.6
W.L.			7.8	164.5
+10			7.5	164.8
Cb			8.4	163.9

	+	172.28 +	−	Elev
1/4			8.1	164.3
℄			7.7	164.6
1/4			8.2	164.1
Cb			7.1	165.2
E.L.			7.4	164.9
+10			7.3	165.0
		1+00		
−10			5.2	167.1
E.L.			5.5	166.8
Cb			6.1	166.2
1/4			7.0	165.3
℄			6.9	165.4
1/4			7.0	165.3
Cb			7.4	164.9
W.L.			7.6	164.7
+10			7.6	164.7
		1+25		
−10			6.9	165.4
WL			6.3	166.0
Cb			6.3	166.0
1/4			5.6	166.7
℄			5.5	166.8
1/4			5.3	167.0
+5			5.3	167.0
+6			3.5	168.8

	+	172.38 ↑	−	Elev
Cb			3.5	168.8
E.L.			4.0	168.3
+ 10			3.3	169.0
		1+50		
E.L-10			1.1	172.2
E.L.			2.4	169.9
Cb			3.6	168.7
+5			4.5	167.8
1/4			4.3	168.0
℄			4.3	168.0
1/4			4.5	167.8
Cb.			5.1	167.2
+3			4.8	167.5
W.L.			4.6	167.7
+10			4.6	167.7
		1+75		
−10			4.5	167.8
W.L.			4.6	167.7
Cb			4.0	168.3
1/4			3.3	169.0
℄			3.1	169.2
1/4			3.2	169.1
Cb.			3.0	169.3
E.L.			0.7	171.6
T.P.	12.41	183.63	1.06	171.22

	+	183.63 ↑	−	Elev
		2+00 = S.L. Jennyson		
E.L.			11.1	172.5
Cb.			12.2	171.4
1/4			12.6	171.0
℄			12.4	171.2
W.L.			12.7	170.9
Cb			13.0	170.6
W.L.			12.8	170.8
		0+00 = N.L. Jennyson		
W.L.			11.8	171.8
Cb.			11.7	171.9
1/4			11.3	172.3
℄			11.1	172.5
1/4			10.5	173.1
Cb			10.7	172.9
E.L.			9.6	174.0
		0+75		
E.L.			6.1	177.5
Cb.			8.3	175.3
1/4			9.0	174.6
℄			9.9	173.7
1/4			10.5	173.1
Cb			10.6	173.0
W.L.			10.7	172.9
		1+25		
W.L.			9.1	173.9

	+	π	−	Elev
		183.63		
Cb			8.4	175.2
1/4			8.0	175.6
℄			7.6	176.0
1/4			6.9	176.7
Cb.			5.5	178.1
E.L.			3.4	180.2
T.P.	12.64	195.52	0.75	182.88
		0+50		
E.L.			11.2	184.3
Cb.			14.3	181.2
1/4			15.4	180.1
℄			15.3	180.2
1/4			15.8	179.7
Cb			16.2	179.3
Cb+10			18.7	176.8
W.L.			19.9	175.6
W.L+10			19.9	175.6
		0+75		
W.L-10			17.8	177.7
W.L			17.2	178.3
W.L+13			15.0	180.5
W Cb			12.9	182.6
+2			11.8	183.7
1/4			11.6	183.9
℄			11.0	184.5

	+	π	−	Elev
		195.52		
1/4			10.2	185.3
Cb.			9.2	186.3
E.L.			6.8	188.7
1+00				
E.L.			4.9	190.6
+15			5.8	189.7
Cb			5.7	189.8
1/4			6.7	189.3
℄			7.0	188.5
1/4			7.0	188.5
+5			7.1	188.4
Cb.			8.4	187.1
+8			12.9	182.6
W.L.			14.0	181.5
+10			15.5	180.0
+20			16.2	179.3
		1+25		
−20			12.7	182.8
−6			11.4	184.1
W.L.			8.5	187.0
+14			4.2	191.3
Cb			4.2	191.3
1/4			4.3	191.2
℄			4.3	191.2
1/4			4.1	191.4

1955.52

	+	x	−	Elev
Cb			3.7	191.8
E.L.			3.5	192.0
		1+50		
E.L.			2.1	193.4
Cb.			2.2	193.3
1/4			3.4	192.1
℄			3.3	192.2
1/4			3.2	192.3
Cb.			3.3	192.2
+8			2.9	192.6
W.L.			4.8	190.7
+10			6.6	188.9
		1+75		
-10			4.9	190.6
W.L.			3.8	191.7
Cb.			3.2	192.3
1/4			2.6	192.9
℄			2.6	192.9
1/4			2.6	192.9
Cb			2.2	193.3
+5			1.6	193.9
E.L.			1.3	194.2
		1+95		
E.L.			0.7	194.8
+13			1.1	194.4

1955.52

	+	x	−	Elev
Cb			3.0	192.5
1/4			3.6	191.9
℄			3.8	191.7
1/4			3.6	191.9
Cb			3.7	191.8
W.L.			3.5	192.0
		2+00 - S.L. Udahl (paved)		
W.L.			3.3	192.2
+9.5 on end of 43' R. Ret.			3.35	192.17
Cut. on print			3.97	191.45
Cb Line projected "			3.42	191.90
1/4 " "			3.57	191.95
℄ " "			3.62	191.90
1/4			3.78	191.74
Cb Line " "			3.96	191.56
+9 Gutter			4.16	191.36
End Cb of 43' R. Ret			3.54	191.98
+15 inside edge of Walk			3.28	192.24
E.L.			1.9	193.6
		5 Cb Line of Udahl on Print		
-35 B.C. Ret. on Print			2.76	192.96
EL Plan projected.			2.97	192.55
Cb		"	3.21	192.31
1/4			3.23	192.29
℄			3.16	192.36
1/4			3.21	192.31

	+	↑	−	Elev	
		195.52			
Cb			3.38	192.14	
W.L. projected			3.94	191.58	
+25 P.C. Ret on Prmt			5.82	189.70	
Sec A Around S.W. Ret of Udahl					
P.C. on Udahl			5.19	190.33	
+10 on arc			4.33	191.19	
+20 " "			3.68	191.84	
+30 " "			3.34	192.18	
+40 = "end"			3.35	192.17	
Sec B Around S.E. Ret Udahl					
P.C. on Udahl			1.89	193.63	
+10 on Arc			2.15	193.37	
+20 " "			2.44	193.08	
+30 " "			2.94	192.58	
+40 " " = End			3.54	191.98	
T.P.	2.47	197.24	0.75	194.77	
B.M. S.W. B.P.			10.03	187.21	Willow & Udahl
				187.16	Corrected
				diff .05	Elev

60' St
10' Cbs
10' 1/4s

X section Tennyson St

From intersection of Ely Line of Sterne St & Sly Line of Tennyson Pl. & W Ly Line of Willow. See Notes pp 1.—7 this Book

31

T.P.	6.31	138.76		132.45	Nail in Bank ∠ of Sterne p 7
0+00 = Ely Line of Sterne St					
Same as Last Section, p 7.					
N.L.			11.2	127.6	
+5			11.50	127.26	
Cb			11.66	127.10	
Gut			12.5	126.3	
1/4			12.7	126.1	
℄			12.4	126.4	
1/4			13.0	125.8	
Gut			13.3	125.5	
Cb Top P.C. 10R Ret			12.83	125.93	
+5 = edge of walk			12.56	126.20	
S.L.			12.4	126.4	
0+25					
S.L.			7.9	130.9	
+3			8.9	129.9	
+5 = edge of walk			9.06	129.70	
Cb.			9.13	129.63	
Gut			10.0	128.8	
1/4			9.5	129.3	
℄			8.5	130.3	
1/4			8.6	130.2	
G.			9.1	129.7	

Plotted 10/14/29/CBH

138.76

	+	↑	−	Elev
Cb Top			7.92	130.84
+4			7.6	131.2
N.L.			5.2	133.6
	0+50			
N.L.			0.7	138.1
+8			4.2	134.6
Cb Top			4.55	134.21
G			5.8	133.0
+4			5.2	133.6
1/4			5.2	133.6
℄			5.1	133.7
1/4			5.8	133.0
+8			6.4	132.4
G			7.0	131.8
Cb Top			5.69	133.07
+5 edge of walk			5.43	133.33
+6			5.4	133.4
S.L.			3.8	135.0
	0+55 to 0+75			
	Cb on S. broken down			
	0+75.			
S.L.			0.2	138.6
+4			1.7	137.1
+5 edge of Walk			1.88	136.88
+7			2.1	136.7

Bank on both sides of St has slough shown on the S. walk as shown by Roger. Ty lines between Cb's

138.76

	+	↑	−	Elev
Cb Line (cb broken out			3.8	135.0
G.			3.8	135.0
+3			2.5	136.3
1/4			2.1	136.7
℄			1.6	137.2
1/4			1.8	137.0
G			1.9	136.9
Cb Top			1.12	137.64
+2			0.7	138.1
T.P.	11.87	149.79	0.84	137.92
N.L.			8.3	141.5
	1+00			
N.L.			5.4	144.4
+7			8.19	141.60
Cb Top			8.50	141.29
G.			9.2	140.6
+5			9.8	140.0
1/4			9.4	140.4
℄			9.4	140.4
1/4			9.8	140.0
G			10.6	139.2
Cb Top			9.55	140.24
+4			9.5	140.3
S.L.			7.3	142.5

149.79

	+	π	−	Elev
		1+75		
S.L.			4.1	145.7
+7			6.3	143.5
CbTop			6.31	143.48
G			7.9	141.9
+2			6.9	142.9
1/4			6.3	143.5
℄			6.3	143.5
1/4			6.1	143.7
+6			6.2	143.6
G			6.4	143.4
Cb Tob			5.77	144.52
+7			4.4	145.4
N.L.			3.0	146.8
		1+50		
N.L.			0.9	148.9
+5 edge of walk			2.77	147.57
Cb Top			2.44	147.35
G			4.4	145.4
+4			3.2	146.6
1/4			3.2	146.6
℄			3.2	146.6
1/4			3.4	146.4
+7			3.6	146.2
G			4.8	145.0

149.79

	+	π	−	Elev.
Cb Tob			3.50	146.29
+6			3.1	146.7
S.L.			1.8	148.0
T.P.	12.17	160.70	1.26	148.53
		1+75		
S.L.			10.4	150.3
+3			11.6	149.1
Cb Tob			11.80	148.99
G.			12.6	148.1
+4			12.1	148.6
1/4			11.7	149.0
℄			11.3	149.4
1/4			11.3	149.4
+7			11.4	149.3
G			12.0	148.7
Cb Tob			10.77	149.93
+9			10.6	150.1
N.L.			9.6	151.1
		2+00		
N.L.			8.2	152.5
+1			8.4	152.3
Cb Tob			8.51	152.19
G			9.3	151.4
1/4			9.0	151.7
℄			8.9	151.8

	+	160.70	−	Elev
1/4			9.8	151.4
+6			9.9	150.5
G			10.8	149.9
Cb Top			9.55	151.15
+8			9.4	151.3
S.L.			8.5	152.2
		2+25		
S.L.			6.5	154.2
+2			7.5	153.2
Cb Top			7.70	153.00
G			8.3	152.4
1/4			7.7	153.0
℄			7.5	153.2
1/4			7.4	153.3
G			7.5	153.2
Cb Top			6.80	153.90
N.L.			6.4	154.3
		2+50		
N.L.			4.8	155.9
Cb Top			5.22	155.48
Cut			5.8	154.9
1/4			5.9	154.8
℄			6.0	154.7
1/4			6.1	154.6
+8			6.9	153.8

	+	160.70	−	Elev
G			6.5	154.2
Cb Top			6.70	154.00
+9			5.9	154.8
S.L.			4.8	155.9
2+75				
S.L.			4.4	156.3
+1			4.8	155.9
Cb Top			5.09	155.61
G			5.5	155.2
+4			5.5	155.2
1/4			5.0	155.7
℄			4.7	156.0
1/4			4.7	156.0
+5			4.9	155.8
G			4.7	156.0
Cb Top			4.12	156.58
4.9			4.0	156.7
N.L.			3.7	157.0
3+00				
N.L.			2.8	157.9
+2			3.0	157.7
Cb Top			3.24	157.46
G			4.0	156.7
1/4			3.7	157.0
℄			3.9	156.8

160.70

	+	↗	−	Elev
1/4			4.1	156.6
G			4.8	155.9
Cb Top			4.11	156.59
+9			3.8	156.9
S.L.			3.4	157.3
		3+25		
S.L.			2.8	157.9
+1			3.0	157.7
Cb Top			3.28	157.42
G			4.0	156.7
1/4			3.2	157.5
℄			2.9	157.8
1/4			2.8	157.9
G			2.9	157.8
Cb Top			2.48	158.22
+9			2.3	158.4
N.L.			2.0	158.7
		3+50		
N.L.			1.3	159.4
+1			1.6	159.1
Cb			1.73	158.97
G			2.3	158.4
1/4			2.1	158.6
℄			2.0	158.7
1/4			2.3	158.4

	+	↗	−	Elev
T.P.	9.63	168.59	1.74	158.96
G			10.7	157.9
Cb Top			10.37	158.22
+9			10.1	158.5
S.L.			9.8	158.8
		3+78 15' on N to 3+79 on S = W.L. Clove St		
		And ⌀ in Tennyson		
S.L.			8.9	159.7
+1			9.3	159.3
Cb			9.42	159.17
G			9.8	158.8
1/4			9.6	159.0
℄			8.9	159.7
1/4			9.0	159.6
G			9.2	159.4
Cb			8.74	159.88
+8			8.5	160.1
N.L.			8.2	160.4
		+35 = old ℄ Clove St = N and S. Line		
		No Cbs or 1/4's taken on this intersection		
		no Cbs, walks & Grading Go across at		
		no change in Grade. Street 65' wide.		
		at this station		
N.L.			7.0	161.6
+10.8 = Cb Top			7.67	160.92

	+	π	−	Elev
		168.59		
G			8.7	159.9
1/4			7.9	160.7
℄			7.8	160.8
1/4			8.2	160.4
G.			8.8	159.8
Cb Top			8.48	160.09
+ 7			8.3	160.3
S.L.			8.0	160.6
	+ 70 = Old S.L. Clove = 0+00			
		70' St 10' Cbs 12.5 1/4s		
S.L.			7.0	161.6
+ 1			7.3	161.3
Cb Top			7.55	161.04
Gut			8.0	160.6
1/4			7.1	161.5
℄			6.8	161.9
1/4			6.8	161.8
G			7.0	161.6
Cb Top			6.64	161.95
+			6.3	162.3
N.L.			5.7	162.9
		0+50		
N.L.			5.2	163.4
Cb			5.43	163.16
G			5.8	162.8

	+	π	−	Elev
		168.59		
1/4			5.5	163.1
℄			5.7	162.9
1/4			5.9	162.7
G			6.6	162.0
Cb Top			6.30	162.29
S.L.			6.0	162.6
	1+07.4 = End of Cbs & Walks			Subdivision Line
S.L.			4.8	163.8
+ 1			4.6	164.0
Cb Top Cb			4.79	163.80
G			5.1	163.5
1/4			4.9	163.7
℄			4.4	164.2
1/4			4.4	164.2
G			4.3	164.3
Cb			4.15	164.44
N.L.			4.0	164.6
T.P.	11.44	176.09	3.94	164.65
	1+25 = 70' St. 18' Cbs 8.5 1/4s			
N.L.			10.8	165.3
Cb.			11.3	164.8
1/4			11.2	164.9
℄			11.2	164.9
1/4			11.2	164.9
Cb.			11.7	164.4

17+09

	+	▲	−	Elev
S.L.			11.8	164.3
		1+50		
S.L.			10.7	165.4
+10			11.2	164.9
Cb.			11.1	165.0
1/4			10.6	165.5
℄			10.3	165.8
1/4			10.4	165.7
Cb			10.5	165.6
+9			10.4	165.7
N.L.			9.9	166.2
		2+00		
N.L.			7.9	168.2
+9			8.6	167.5
Cb.			8.7	167.4
1/4			8.5	167.6
℄			8.4	167.7
1/4			8.7	167.4
Cb			9.1	167.0
+8			9.3	166.8
S.L.			9.0	167.1
		2+50		
S.L.			6.8	169.3
+10			7.4	168.7
Cb			7.1	169.0

17+09

	+	▲	−	Elev
1/4			6.7	169.4
℄			6.4	169.7
1/4			6.6	169.5
Cb			6.8	169.3
+8			6.5	169.6
N.L.			5.6	170.5
		2+75		
N.L.			5.0	171.1
+10			5.6	170.5
Cb.			5.8	170.3
1/4			5.7	170.4
℄			5.6	170.5
1/4			5.9	170.2
Cb			6.1	170.0
+8			6.5	169.6
S.L.			5.9	170.2
		3+00 = W.L. P/V in 70 ft Cb. 8.5 ft ±0		
S.L.			5.0	171.1
+10			5.4	170.7
Cb			5.3	170.8
1/4			5.2	170.9
℄			4.8	171.3
1/4			4.7	171.4
Cb			4.9	171.2
+8			4.8	171.3
N.L.			4.2	171.9

	+	⊼	−	Elev
		176.09		
	W. Cb. Plum St.			
N.L.			4.0	172.1
Cb			4.5	171.6
1/4			4.3	171.8
℄			4.4	171.7
1/4			4.5	171.6
Cb			4.6	171.5
S.L.			5.3	170.8
	W 1/4 Plum			
S.L.			5.1	171.0
Cb			4.4	171.7
1/4			4.0	172.1
℄			4.3	171.8
1/4			4.0	172.1
Cb			4.2	171.9
N.L.			3.7	172.4
T.P.	12.39	184.82	3.66	172.43
	℄ Plum			
N.L.			12.0	172.8
Cb			12.9	171.9
1/4			12.7	172.1
℄			12.6	172.2
1/4			12.6	172.2
Cb.			13.2	171.6
S.L.			13.3	171.5

	+	⊼	−	Elev
		184.82		
	E 1/4 Plum			
S.L.			13.4	171.4
Cb			13.0	171.8
1/4			12.5	172.3
℄			12.5	172.3
1/4			12.5	172.3
Cb			12.8	172.0
N.L.			11.7	173.1
	E Cb Plum			
N.L.			12.0	172.8
Cb			12.5	172.3
1/4			12.3	172.5
℄			12.3	172.5
1/4			12.5	172.3
Cb			12.8	172.0
S.L.			13.1	171.7
	E.L. Plum = 0+00			
S.L.			12.3	172.5
Cb			12.2	172.6
1/4			12.0	172.8
℄			11.8	173.0
1/4			11.8	173.0
Cb			11.8	173.0
N.L.			11.2	173.6

184.82

	+	⊼	−	Elev
		0+75		
N.L.			6.1	178.7
+6			8.9	175.9
Cb			9.8	175.0
1/4			10.0	174.8
℄			10.0	174.8
1/4			10.5	174.3
Cb			10.7	174.1
S.L.			9.7	175.1
		0+75		
S.L.			5.0	179.8
Cb.			6.0	178.8
1/4			6.0	178.8
℄			5.4	179.4
1/4			5.5	179.3
Cb			5.3	179.5
+12			4.5	180.3
N.L.			0.0	184.8
T.P.	12.37	196.01	1.18	183.64
		1+25		
N.L.			6.2	189.8
+10			10.9	185.1
Cb			11.6	184.4
1/4			11.6	184.4
℄			11.4	184.6

196.01

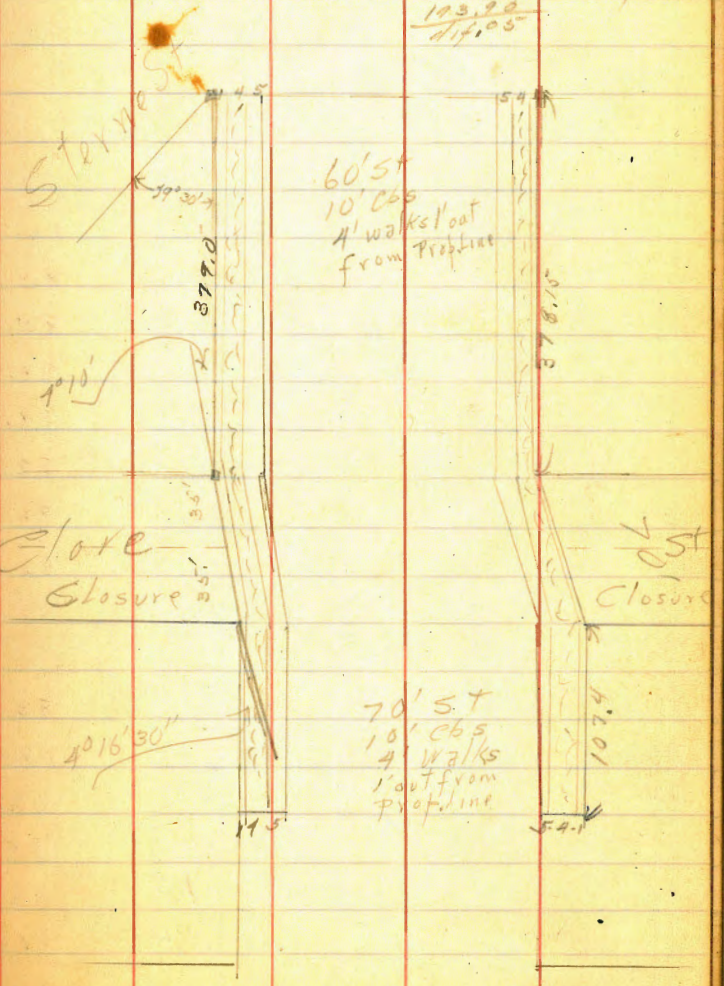
	+	⊼	−	Elev
1/4			11.7	184.3
Cb			11.8	184.2
S.L.			11.5	184.5
		1+75		
S.L.			6.3	189.7
Cb			7.2	188.8
1/4			7.0	189.0
℄			6.6	189.4
1/4			6.7	189.3
Cb			7.1	188.9
+11			6.3	189.7
N.L.			2.7	193.3
		2+00		
N.L.			1.4	194.6
+7			4.2	191.8
Cb			4.7	191.3
1/4			4.8	191.2
℄			4.6	191.4
1/4			4.9	191.1
Cb			5.1	190.9
S.L.			4.5	191.5
		2+75		
S.L.			3.1	192.9
Cb			4.1	191.9
1/4			3.9	192.1

196.01

	+	↗	−	Elev
℄			3.4	192.6
1/4			3.7	192.3
CL			3.9	192.1
+ 11			3.2	192.8
N.L.			0.6	195.4
	2+75			
N.L.	0.2			
+ 9			2.2	193.8
CL			2.6	193.4
1/4			2.5	193.5
℄			2.3	193.7
1/4			2.3	193.7
CL			2.4	193.6
+ 13			1.8	194.2
S.L.			0.1	195.9
	3+00 = W.L. Willow Paved			
S.L.			1.8	194.2
+10.5 = End 13' R CL			1.81	194.20
G			2.63	193.38
CL Line			2.43	193.58
1/4			2.24	193.77
℄			2.21	193.80
1/4			2.25	193.76
CL Line			2.34	193.67
+ 7.5 Gutter			2.61	193.40

196.01

	+	↗	−	Elev
CL end of 13' R Rt			1.81	194.20
N.L.			1.6	194.4
S.W.B.P.			2.06	193.95
			193.90	Willow & Tennyson
			14.05	



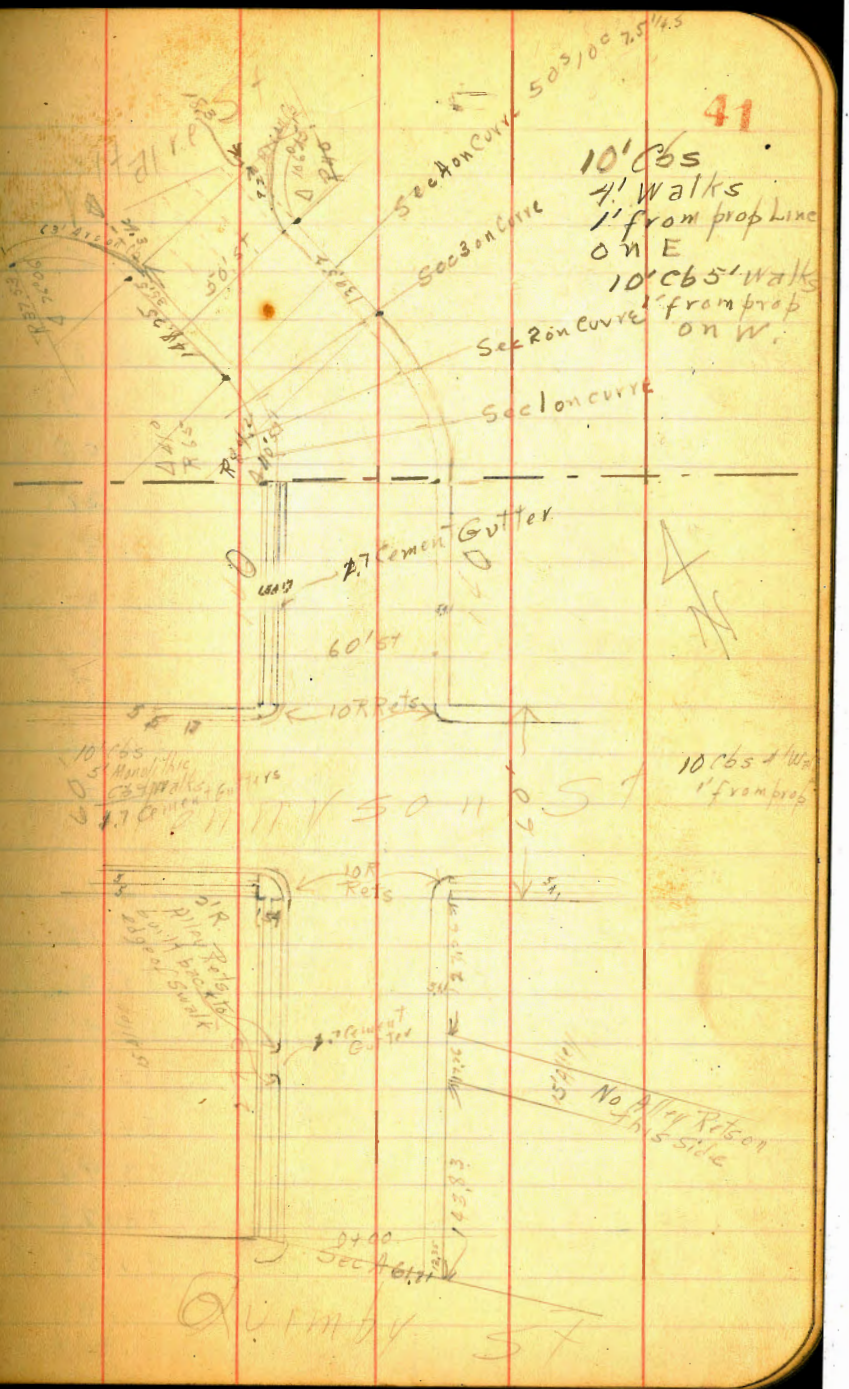
Plum St

Section Capistrano St
Voltaire to Quimby.

B.P.S.M.	7.07	103.72		96.65
T.P.	3.51	105.38	1.85	101.87
T.P.	0.31	93.03	12.66	92.72

Sec A diagonal on Nt. Quimby St.

W.L.	11.5	81.5
+ 10.3 = C.B. Dirt / C.B. Top	11.3	81.7
	11.95	81.081
Gutter	12.75	80.28
+ 1.1 = Edge of Gutter	12.65	80.38
1/4 (10.3)	11.5	81.5
℄	11.2	81.8
1/4	11.0	82.0
G.	11.1	81.9
C.B. Top	10.91	82.082
E.L.	10.8	82.2
0+00 = P.C. Reton W.		
E.L.	10.0	83.0
C.B.	10.28	82.75
G	10.6	82.4
1/4	10.0	83.0
℄	10.0	82.0
1/4	11.4	81.6
+ 8.3	12.59	80.44
G	12.71	80.32



93.03

	+	H	−	Elev
Cb Top			11.92	81.11
Cb Line dirt			11.3	81.7
W.L.			11.5	81.5
		0+25		
W.L.			9.9	83.1
Cb Top			10.16	82.87
G.			10.98	82.05
+1.7			10.83	82.21
1/4			10.1	82.9
℄			9.4	83.6
1/4			9.2	83.8
G.			9.2	83.8
Cb Top			8.77	84.26
E.L.			8.5	84.5
		0+50		
E.			6.9	86.1
Cb in driveway			7.88	85.15
G.			8.0	85.0
1/4			7.6	85.4
℄			7.9	85.1
1/4			8.5	84.5
+8.3			9.09	83.94
G.			9.25	83.78
Cb			8.45	84.58
W.L.			8.0	85.0

93.03

	+	H	−	Elev
		1+00		
W.L.			4.6	88.4
Cb			5.00	88.03
G.			5.76	87.27
+1.7			5.59	87.44
1/4			5.2	87.8
℄			4.6	88.4
1/4			4.3	88.7
G			4.2	88.8
Cb			3.91	89.12
E.L.			3.61	89.42
		1+30 = SL Alleyon N		
E.L.			1.2	91.8
+1			1.7	91.3
Cb			2.08	90.95
G			2.3	90.7
1/4			2.4	90.6
℄			2.6	90.4
1/4			3.2	89.8
+8.3			3.53	89.50
G.			3.68	89.35
Cb Top Alley Ref			3.92	90.11
+4 = edge of Walk end Ref			2.82	90.21
+9 " " "			3.63	90.40
W.L.			2.6	90.4

93.03

	+	↑	−	Elev
	1+45 = N.L. Alley on W.			
W.L.			1.3	91.7
+1			1.60	91.43
+6			1.90	91.13
Cb Top Alley Ret			1.85	91.18
G.			2.62	90.41
+1.7			2.40	90.63
1/4			1.7	91.3
℄			1.6	91.4
1/4			1.3	91.7
G			0.8	92.2
Cb			1.18	91.95
+9			0.72	92.31
E.L.			0.0	93.0
T.P.	11.80	104.52	0.31	92.72
	1+75			
E.L.			9.3	95.2
+5 on edge of Walk			9.74	94.78
Cb Line			9.8	94.7
G			11.2	93.3
+3			10.4	94.1
1/4			10.5	94.0
℄			10.6	93.9
1/4			10.9	93.6
+8.3			11.28	93.24

Cb from E Broken down from 5th St. 1 x 1 x 0 Tenny son Walk may be saved.

104.52

	+	↑	−	Elev
G.			11.43	93.09
Cb			10.65	93.87
W.L.			10.1	94.4
	2+00			
W.L.			8.1	96.4
Cb			8.34	96.18
G			9.10	95.37
+1.7			9.01	95.51
1/4			8.8	95.7
℄			8.4	96.1
1/4			8.4	96.1
G & Cb Line			8.0	96.5
+5 on Walk			7.36	97.16
E.L.			7.0	97.5
	2+25			
E.L.			11.5	100.0
+5 on Walk			5.01	99.51
Cb			5.3	99.2
G			5.8	98.7
1/4			5.7	98.8
℄			6.0	98.5
1/4			6.5	98.0
+8.3			6.75	97.77
G			6.87	97.65
Cb			6.06	98.46
W.L.			5.8	98.7

	+	π (104.52)	−	Elev
2 + 75 = S.L. Tennyson				
W.L.			1.2	103.3
Cb			1.44	103.08
G.			2.28	102.24
+ 1.7			2.16	102.36
1/4			1.7	102.8
℄			1.3	103.2
1/4			1.3	103.2
G			1.0	103.5
Cb Broken down			1.1	103.4
+ 5 on walk		walk & Ret Broken down	0.38	104.14
E.L.			0.0	104.5
Shot on base of F.H.P.C of Ret 0.99				103.53
T.P.	11.49	115.02	0.99	103.53
0 + 00 = N.L. Tennyson				
E.L.			8.3	106.7
Cb Top			9.30	105.72
G			9.5	105.5
1/4			9.6	105.4
℄			10.0	105.0
1/4			10.50	104.52
+ 8.3			10.90	104.12
G			11.06	103.96
Cb Top			10.28	104.74
W.L.			10.1	104.9

	+	π (115.02)	−	Elev
0 + 35				
W.			5.9	109.1
Cb Top			6.26	108.76
G			7.07	107.95
+ 1.7			6.92	108.10
1/4			6.5	108.5
℄			6.4	108.6
1/4			6.1	108.9
G			6.0	109.0
Cb			5.30	109.72
E			5.0	110.0
0 + 65				
E			1.5	113.5
+ 5 on Walk			1.74	113.28
Cb Line			2.2	112.8
1/4			2.4	112.6
℄			2.7	112.3
1/4			2.8	112.2
+ 8.3			3.45	111.57
G			3.60	111.42
Cb			2.82	112.20
W.			2.6	112.4
T.P.	12.83	127.66	0.19	114.83
0 + 90				
W			12.5	115.2

Cb from Sta 0+35 to Sta 1+30 broken & undermined. 4' walk may be saved

	+	127.66 π	−	Elev	
Cb				12.70	~~115.0~~ 114.96
G				13.51	114.15
+1.3				13.38	114.28
1/4				12.6	115.1
℄				12.4	115.3
1/4				12.3	115.4
G = Cb line				12.3	115.4
+5 on dirt				12.1	115.6
on walk				11.31	116.35
E.L.				11.1	116.6
		1+15			
E.L.				6.2	121.5
+4				8.3	119.4
+5 on walk				8.40	119.26
+5 " dirt				9.2	118.5
Cb L & G.				9.2	118.5
1/4				9.1	118.6
℄				9.3	118.4
1/4				9.7	118.0
+8.3				10.61	117.05
G.				10.76	116.90
Cb				9.93	117.73
W.				9.7	118.0
		1+30 = Brk in Cb on E			
W				8.1	119.6

	+	127.66 π	−	Elev	
Cb				8.33	119.33
G				9.15	118.51
+1.7				8.98	118.68
1/4				8.0	119.7
℄				7.5	120.1
1/4				7.3	120.4
G				7.7	120.0
Cb Top				6.82	120.84
+2				8.0	119.7
+5 on Walk				6.64	121.02
+8				6.6	121.1
E.L.				5.4	122.3

1+40 = end of Gutter on E & beginning of Curves. St Narrows from 60' st. 10' Cbs at this station to 50' st 10' Cbs at E.c. on West See sketch

E.L.				5.0	122.7
+1				5.8	121.9
+5 on walk				5.86	121.80
+8				6.6	121.1
Cb Top				6.03	121.63
G				6.9	120.8
1/4				6.4	121.3
℄				6.5	121.2
1/4				7.0	120.7

127.66

	+	π	−	Elev
+ 8.3 =	End of 1.1 Cement Gutter		7.84	119.82
G =	" " " "		8.04	119.62
Cb. Top			7.17	120.49
W.L.			6.9	120.8
	Sec. 1 on Curve 59' St 10 Cbs 9.75 1/4s			
W.L.			6.1	121.6
Cb Top			6.24	121.42
G			7.1	120.6
1/4			5.9	121.8
℄			5.2	122.5
1/4			5.4	122.3
G			5.3	122.4
Cb			4.49	123.17
E			4.35	123.31
	Sec 2 on Curve 56.4 St 10 Cbs 9.1 1/4s			
E			2.9	124.8
Cb. Top			3.26	124.40
G			4.2	123.5
1/4			4.4	123.3
℄			4.4	123.3
1/4			5.1	122.6
G			6.2	121.5
Cb Top			5.37	122.29
W.			5.17	122.49

127.66

	+	π	−	Elev
	Sec 3 on Curve = 52.3 St 10' Cbs 8.08 1/4s			
W			4.40	123.26
Cb			4.48	123.18
G			5.2	122.5
1/4			4.4	123.3
℄			3.8	123.9
1/4			3.5	124.2
G			3.2	124.5
Cb			2.47	125.19
E			2.2	125.5
	Sec 4 on Curve = P.C on W=0+00 50' St 10' Cbs 7.5 1/4s			
E.L.			1.68	125.98
Cb			1.92	125.74
G			2.7	125.0
1/4			3.0	124.7
℄			3.4	124.3
1/4			3.9	123.8
G.			4.5	123.2
Cb.			3.95	123.71
W.L.			3.9	123.8
	0+37			
W.			3.4	124.3
Cb			3.55	124.11
G			3.9	123.8

	+	↑	−	Elev
		107.66		
1/4			3.3	124.4
℄			2.8	124.9
1/4			2.4	125.3
G			2.2	125.5
Cb			1.46	126.20
E			1.3	126.4
	0+87			
E			1.0	126.7
Cb			1.28	126.38
G			3.0	125.7
1/4			2.2	125.5
℄			2.5	125.2
1/4			2.1	124.6
G			2.9	123.8
Cb			3.39	124.27
W.			2.3	125.4
T.P.	3.39	128.56	2.49	125.17
	1+12.5 = P.C. on W E			
W.			4.5	124.1
Cb			4.57	123.99
G			5.0	123.6
1/4			4.2	124.4
℄			3.2	125.4
1/4			3.0	125.6
G			2.7	125.9
C				

	+	↑	−	Elev
		128.56		
Cb P.C Ret			2.13	126.43
E			1.8	126.8
	1+48 = P.C. on W. Rdway 46.7 bet Cbs.			
E. Cb. on Ret			0.42	128.14
G			1.1	127.5
+16.7 = Cb line projected			2.8	125.8
1/4 projected			3.4	125.2
℄ "			4.2	124.4
1/4 "			5.0	123.6
G "			5.4	123.2
Cb "			5.27	123.29
W.L. "			5.4	123.2
T.P. 11.08		136.25	3.39	125.17
S.L. Voltaire on diagonal 75' bet Cbs				
Prof P.C. on W +29.3 to +18.3 on E.L. projected				
W. Cb on Ret (cb sunken)			15.92	120.33
G			16.3	120.0
+10			14.8	121.5
+20			13.5	122.8
+30			12.0	124.3
+40			10.5	125.8
+50			9.3	127.0
+60			8.1	128.2
+70			6.4	129.9
+75 G			5.8	130.5
E Cb on Ret			5.59	130.97

136.75

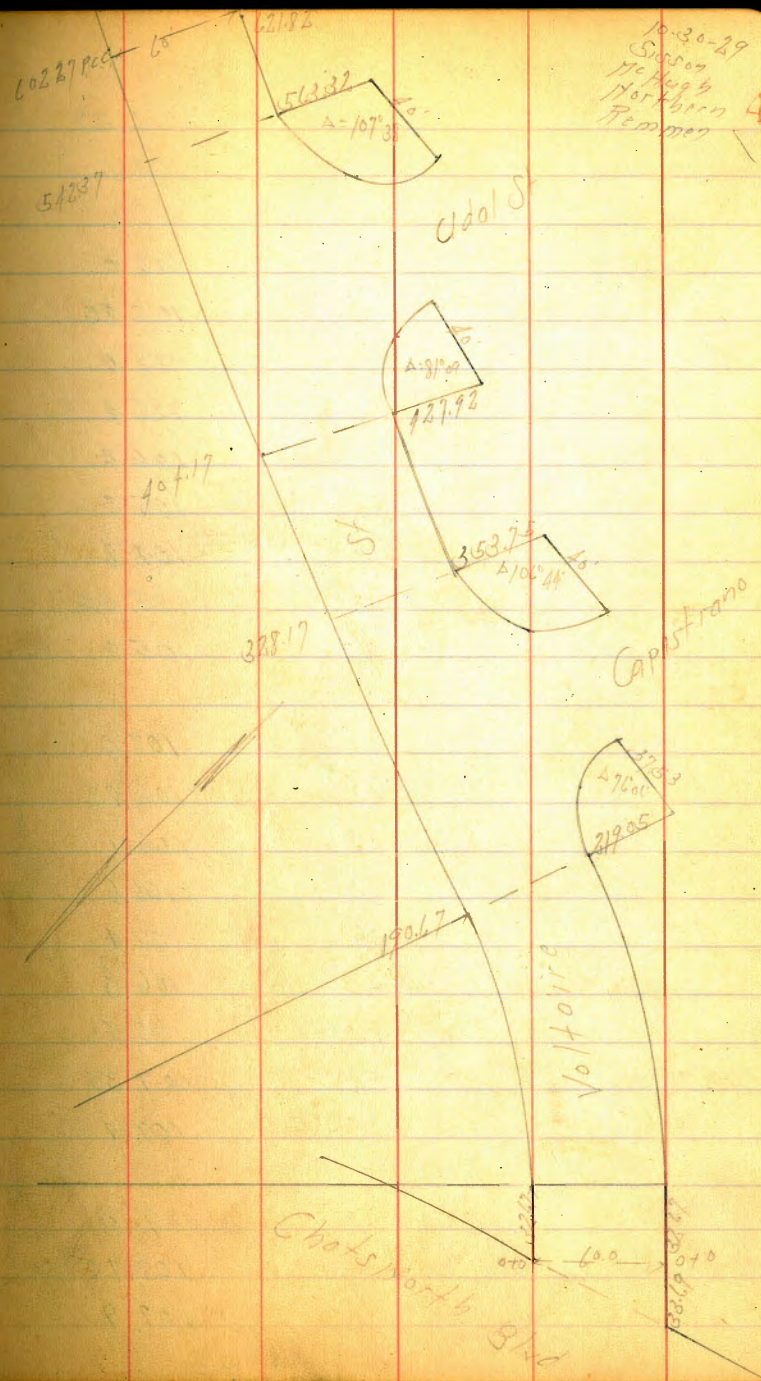
	+	−	Elev Capistrano & Voltaire
Sec A round S.E. Ref			
P.C. on Voltaire		0.18	136.07
+11 on Arc		1.56	134.69
+9 " "		3.04	133.21
" "		4.53	131.72
" " "		6.02	130.23
" " "		7.47	128.78
" " "		8.46	127.79
" " "		9.32	126.93
" " "		9.72	126.53
" " "		9.83	126.42
P.C. on Capistrano		9.83	126.42
T.P.	3.75	11.08	125.17
Sec A round S.W. Ref			Capistrano & Voltaire
P.C on Capistrano		5.65	123.27
+9 on Arc.		6.11	122.81
" " "		6.70	122.22
" " "	} Cb broken down		
" " "			
" " "			
" " "		11.30	117.62
P.C on Voltaire		12.10	116.82
T.P.		9.83	119.09

Voltaire St. Cross Section
Chatsworth to Clover

60' Wide
10' Cbs
10' Qts

BM	11.45	110.93		99.48 SWBP Chatsworth & Voltaire
		EL Chatsworth		68.42 Cbs 11.6 Qts
N			9.6	101.3
Cb Top & Ground			10.04	100.89
1/4			9.9	101.0
℄			9.6	101.3
1/4			10.5	100.4
Cb Top & Ground			11.02	99.91
S			11.0	99.9
		EL Chatsworth on N 33.69 E of EL on S		60' Wide
S			8.8	102.1
Cb Top			9.14	101.79
Gutter			9.4	101.5
1/4			9.1	101.8
℄			8.7	102.2
1/4			9.1	101.8
Cb Top & Ground			9.93	101.00
N			9.6	101.3
		32.67 E on N = PC 32.67 E on S = 66.36		
N			7.1	103.8
Cb Top & Ground			7.56	103.37
1/4			7.2	103.7
℄			6.7	104.2
1/4			6.8	104.1
Gutter			7.0	103.9

PLOTTED 11/1/29 CAH



Voltaire

		110.93						110.93	
Cb Top			6.66	104.27	¼			2.6	108.3
S			6.4	104.5	℄			1.9	109.0
		52.42 E on N			¼			2.6	108.3
		65.97 E on S							
S			4.9	106.0	Gutter			3.2	107.7
Cb Top			5.13	105.80	Cb Top			2.60	108.33
Gutter			5.9	105.0			111.47 E on N		
¼			5.32	105.6	N		125.87 " " S	2.8	108.6
℄			4.7	106.2					
¼			5.6	105.3	N			0.6	110.3
Gutter			6.1	104.8	Cb Top			0.89	110.04
Cb Top			5.93	105.00	Gutter			1.4	109.5
		72.17 E on N			¼			0.9	110.0
N		79.27 " " S	5.7	105.2	℄			0.4	110.5
					¼			1.1	109.8
N			3.9	107.0	Gutter			1.3	109.6
Cb Top			4.31	106.62	Cb Top			0.62	110.31
Gutter			4.8	106.1	S			0.5	110.4
¼			4.3	106.6	TP	11.9°	122.63	0.20	110.73
℄			3.5	107.4			131.42 E on N		
¼			4.1	106.8			149.17 " " S		
Gutter			4.4	106.5	S			10.7	111.9
Cb Top			3.60	107.33	Cb Top			10.86	111.77
S			3.5	107.4	Gutter			11.4	111.2
		91.42 E on N			¼			11.2	111.4
		102.57 " " S						10.6	112.0
S			1.9	109.0	℄			10.8	111.8
Cb Top			2.18	108.75	¼			11.3	111.3
Gutter			3.0	107.9	Gutter			10.87	111.76
					Cb Top				

Voltaire

		122.63		
N		10.6	112.0	
	151.17' E on N 172.47 " " S			
N		8.9	113.7	
Cb Top		9.10	113.53	
Gutter		10.5	112.1	
1/4		8.9	113.7	
℄		8.8	113.8	
1/4		9.4	113.2	
Gutter		9.8	112.8	
Cb Top		9.39	113.24	
S		9.2	113.4	
	170.92' E on N 195.77' E on S			
S		7.5	115.1	
Cb Top		7.72	114.91	
Gutter		8.2	114.4	
1/4		7.6	115.0	
℄		7.1	115.5	
1/4		7.4	115.2	
Gutter		7.6	115.0	
Cb Top		7.24	115.39	
N		6.9	115.7	
	190.67' E on N = PC on N 219.05' E on S = PC on S			
N		4.9	117.7	
Cb Top		5.21	117.42	
Gutter		5.6	117.0	
1/4		5.4	117.2	

		122.63		
℄		5.2	117.4	51
1/4		5.9	116.6	
Gutter		6.1	116.5	
Cb Top		5.82	116.81	
S		5.5	117.1	
	213.59' E on N 241.50' E on S			
S		2.9	119.7	
+45 = Existing Cb		3.38	119.25	
Cb		3.8	118.8	
1/4		3.7	118.9	
℄		2.9	119.7	
1/4		3.1	119.5	
Gutter		3.2	119.4	
Cb Top		2.59	120.04	
N		2.4	120.2	
TP	123.4	134.63	0.34	122.29
	236.50' E on N 263.95 " " S			
N		11.4	123.2	
Cb Top		11.69	122.94	
Gutter		12.2	122.4	
1/4		12.4	122.2	
℄		12.1	122.5	
1/4		12.5	122.1	
Cb		12.7	121.9	
S		12.7	121.9	
	259.42' E on N 286.40' E on S			
S		9.4	125.2	

Voltaire

13463

Cb	9.4	125.2	
¼	9.4	125.2	
℄	9.1	125.5	
¼	9.1	125.5	
Gutter	8.8	125.8	
Cb Top	8.20	126.43	
N	8.1	126.5	
			283.34 E on N
			308.85 E on S
N	11	130.0	
Cb Top	11.3	130.00	
Gutter	5.3	129.3	
¼	5.6	129.0	
℄	5.1	129.0	
¼	5.9	128.7	
Cb	6.0	128.6	
S	6.5	128.1	
			805.26 E on N
			331.30 N on S
S	2.5	132.1	
+45 = Existing Cb Top	2.25	132.38	
+5	2.7	131.9	
Cb	2.6	132.0	
¼	2.3	132.3	
℄	2.1	132.5	
¼	2.0	132.6	
Gutter	1.9	132.7	
Cb Top	1.19	133.44	

13463

N	1.0	133.6	
TP = 133.6	146.40	0.59	134.04
			338.17 E on N = FC on S
N = 353.75 N on S		9.2	137.2
Cb Top		9.11	136.96
Gutter		10.2	136.2
¼		10.3	136.1
℄		10.3	136.1
¼		10.5	135.9
Gutter		10.6	135.8
Cb Top		10.35	136.05
S		10.2	136.2
			353.50 E on N
			378.49 E on S
S	6.2	140.2	
Cb Top	6.11	139.96	
Gutter	6.9	139.5	
¼	6.9	139.5	
℄	6.5	139.9	
¼	6.1	140.0	
Gutter	6.3	140.1	
Cb Top	5.10	140.80	
N	5.8	141.1	
			378.83 E on N
			403.19 E on S
N	1.6	144.8	
Cb Top	1.71	144.69	
Gutter	2.2	144.2	
¼	2.5	143.9	

Voltaire

146.40

℄			25	143.9	
¼			27	143.7	
Gutter			32	143.2	
Cb Top			253	143.87	
S			28	144.1	
PP	12.57	158.77	020	146.20	
		404.17' E on N			
		427.42 E on S	= PC of Obl on S		
S			10.8	148.0	
Cb Top			11.05	147.72	
Gutter			11.6	147.2	
¼			11.2	147.6	
℄			10.8	148.0	
¼			10.7	148.1	
Gutter			10.8	148.0	
Cb Top			10.14	148.63	
N			9.9	148.9	
		427.20' E on N			
		450.49 " " S			
N			6.6	152.2	
Cb Top			6.84	151.93	
Gutter			7.5	151.3	
¼			7.5	151.3	
℄			7.7	151.1	
¼			8.1	150.7	
Cb			8.4	150.4	
+55 = Ex Int of Cb Top			8.19	150.58	
S			8.0	150.8	

158.77

	South 1st Return of Udal L-91.6 to Back 179				
N Face			11.05	147.72	
1			8.83	149.94	
2			7.18	151.59	
3			6.30	152.47	
4 = S End			5.92	152.85	
	South East Return of Udal L-94 to Back 236				
S End			11.1	154.11	
1			9.35	154.42	
2			8.12	155.15	
3			7.91	155.86	
4 = E End			7.15	156.62	
		450.23' E on N			
		473.66 " " S			
S			6.0	152.77	
Cb			5.9	152.9	
¼			5.5	153.3	
℄			5.2	153.6	
¼			5.1	153.7	
Gutter			4.9	153.9	
Cb Top			4.19	154.48	
N			4.1	154.7	
		473.24' E on N			
		495.63 " " S			
N			2.51	156.3	
Cb Top			2.75	156.02	
Gutter			3.4	155.4	
¼			3.8	155.0	

Voltaire

158.77

℄		3.6	155.2
¼		4.0	154.8
Cb		4.3	154.5
S		4.4	154.4
	491.29 E on N 512.20 " " S		
S		4.2	154.6
Cb		3.6	155.2
¼		3.2	155.6
℄		2.6	156.2
¼		3.0	155.8
Gutter		2.7	156.1
Cb Top		2.13	156.64
N		1.9	156.9
	519.32 E on N 540.77 " " S		
N		1.7	157.1
Cb Top		1.93	156.84
Gutter		2.4	156.4
¼		2.6	156.2
℄		2.5	156.3
¼		2.9	155.9
Cb		3.5	155.3
155 = Existing Cb		2.83	155.94
S		2.8	156.0
	542.37 E on N 563.32 " " S = EC of Oakdale		
S		2.0	156.8
Cb Top		2.15	156.67

158.77

54

Gutter		2.7	156.1
¼		2.6	156.2
℄		2.2	156.6
¼		2.3	156.5
Gutter		2.0	156.8
Cb Top		1.70	157.07
N		1.5	157.3
	562.34 E on N 582.82 " " S		
N		1.2	157.5
Cb Top		1.56	157.21
Gutter		1.9	156.9
¼		2.0	156.8
℄		1.8	157.0
¼		2.3	156.5
Gutter		2.4	156.4
Cb Top		1.85	156.95
S		1.7	157.1
	582.37 E on N 602.32 " " S		
S		1.4	157.4
Cb Top		1.55	157.22
Gutter		2.0	156.8
¼		1.9	156.9
℄		1.4	157.4
¼		1.7	157.1
Gutter		1.7	157.1
Cb Top		1.80	157.47

Voltaire

		158.77		
H			1.1	158.7
	602.27' E on N 621.82' E on S - PCC			
H			0.5	158.3
Cb Top			0.96	157.81
Gutter			1.3	157.5
1/4			1.3	157.5
1/2			1.0	157.8
1/4			1.4	157.4
Gutter			1.6	157.2
Cb Top			1.12	157.65
S			0.9	157.9
TP	11.89	170.43	0.23	158.54
	629.41' E on N 645.72' " " S			
S			11.8	158.6
Cb Top			12.09	158.34
Gutter			12.6	157.8
1/4			12.4	158.0
1/2			12.1	158.3
1/4			12.4	158.0
Gutter			12.4	158.0
Cb Top			12.00	158.43
H			11.7	158.7
	656.55' E on N 669.62' " " S			
H			11.1	159.3
Cb Top			11.24	159.19
Gutter			11.8	158.6

		170.43		
1/4			11.8	158.6
1/2			11.5	158.9
1/4			11.7	158.7
Gutter			11.8	158.6
Cb Top			11.30	159.23
S			11.0	159.4
	683.69' E on N 693.52' " " S			
S			10.1	160.3
Cb Top			10.33	160.10
Gutter			10.9	159.5
1/4			10.8	159.6
1/2			10.7	159.7
1/4			10.9	159.5
Gutter			11.0	159.4
Cb Top			10.37	160.06
H			10.2	160.2
	710.83' E on N 717.42' " " S			
H			9.2	161.2
Cb Top			9.41	161.02
Gutter			10.0	160.4
1/4			10.0	160.4
1/2			9.8	160.6
1/4			10.0	160.4
Gutter			10.2	160.2
Cb			9.46	160.97
S			9.3	161.1

Voltaire

17043

737.93 E on N
741.32 " S

S		8.4	1620
Cb. Top		8.58	161.85
Gutter		9.2	161.2
"		9.0	161.4
"		8.8	161.6
"		9.0	161.4
Gutter		8.9	161.5
Cb Top		8.47	161.96
N		8.3	162.1
	765.11 E on N		
	765.22 " S = EC - S.E.L. Pontage		
-10		5.8 = Face of Curb + Rail	164.6
N		7.5	162.9
Cb Top		7.74	162.69
Gutter		7.7	162.7
"		7.8	162.6
"		7.3	163.1
"		7.6	162.8
Gutter		8.0	162.4
Cb Top		7.7	162.72
S		7.6	162.8
	25' E of E.L. Pontage		
S		6.1	164.3
Cb		6.1	164.3
"		5.8	164.6
"		5.8	164.6
"		5.8	164.6

17043

Cb			5.3	1651
N			4.1	1663
		50' E		70' Wide 38.1 RM
N			3.4	1680
Cb			2.9	167.5
"			3.5	1669
"			3.5	166.9
"			3.9	1665
Cb			4.1	166.3
S			4.7	165.7
		75' E		70' Wide 37.9 RM
S			2.2	1682
Cb			1.9	168.5
"			1.6	168.8
"			1.0	169.4
"			1.3	1691
Cb			0.4	1700
"			0.4	170.0
"	12.30	18335	0.38	170.05
		100' E		70' Wide 38.3 RM
N			9.1	173.7
Cb			10.1	172.7
"			12.1	171.3
"			12.0	171.3
"			12.1	170.7
Cb			12.2	170.1

Voltaire

		183.35					183.25		
S			13.6	169.7	H			2.7	180.6
			70' Wd. NCb/Pt					70' Wd. NCb/Pt	
	125' E		324 RM SCb/Pt	171.91		205.6' E		324 RM SCb/Pt	
S			13.2	171.1	H			0.0	183.3
Cb			11.2	172.1	Hub			1.2	182.1
¼			10.4	173.0	Cb			2.2	181.1
¼			9.9	173.4	¼			2.4	181.0
¼			10.2	173.1	¼			2.6	180.7
Cb			9.4	173.9	¼			2.9	180.4
Hub			8.6	174.7	Cb			3.0	180.3
H			8.6	174.7	S			5.4	178.0
			70' Wd. NCb/Pt						50' Roadway
	150' E		358 RM SCb/Pt			230.6' E = H.M.L. Close			125 Gtr
H			5.6	177.7	S			1.9	181.4
Cb			7.2	176.1	+10 - Ex. Shrub, Cb & Walk			2.15	181.20
¼			7.8	175.5	Gutter on Paving			2.67	180.68
¼			7.4	176.0	¼ " "			2.00	181.35
¼			8.1	175.2	¼ " "			1.47	181.88
Cb			9.1	174.2	¼ " "			1.19	181.16
S			10.2	173.1	Gutter " "			0.91	182.41
			70' Wd. NCb/Pt		Cb Top			0.49	182.86
	175' E		349 RM SCb/Pt		H			0.0	183.4
S			7.2	175.7	TP	0.44	171.18	12.61	170.74
Cb			6.6	176.7	BM			9.60	161.58
¼			5.7	177.6					
¼			5.1	178.2					
¼			5.2	178.1	BM	2.10	11889		11679
Cb			4.8	178.5	TP	1.05	109.96	9.98	108.91
Hub			3.3	180.0	BM			10.48	99.48

57

Chats worthy + Zola 161.50

SW B.P. Chats worthy Voltaire

SW B.P. Chats worthy Voltaire

70' wide Chatsworth Blvd X Sec 10-8-29 Mills.

Macaulay to Voltaire

B.M.	13.02	131.01		117.99	S.W. Chatsworth + La Cresta
T.P.	5.73	136.20	0.54	130.47	
	Chatsworth	70' wide. 10' cb on S. 14' cb. on N.	3' cmt gutter on N. 20' Pavmt		
	103.7' S. of S. Line Macaulay = N. Line Arlington Drive				
W. Line on N. End cmt. Return			2.22	133.78	
07' W. of W. cb. Line - W. cmt cb			2.91	133.29	on 14' Radius Return
W. cb. Line gutter Pavmt.			3.67	132.53	
+3 = E. Edge cmt gutter			3.67	132.53	
+11 = W. Edge strip Pavmt.			3.50	132.70	
℄ Pavmt			3.34	132.86	
+10 E. Edge strip Pavmt.			3.44	132.76	
12' E. of Pavmt			4.9	131.3	
13' E. " "			3.8	132.4	
15' " " " = S. cb.			3.9	132.3	
E. Line			4.3	131.9	
+5			4.5	131.7	
	50' S. of M				
E-5			8.0	128.2	
E. Line			7.3	128.9	
cb			7.7	128.5	
+2			7.9	128.3	
+3			8.5	127.7	
+15 = E. Edge Pavmt			6.87	129.33	
℄			6.80	129.40	
+10 = W. Edge Pavmt.			6.94	129.26	
+4			6.6	129.6	

Existing Curb Plotted 11/20-29 - G.B.H.

Chatsworth

136.20

+8 = E. Edge 3' cmt. gutter	7.03	~~128.17~~ 129.17
+11 cmt. gutter	7.28	128.92
W. cmt. cb	6.47	129.73
W. Line	6.1	130.1
S. Line Macaulay	50' wide 1.0' cbs 7.5' 14s	
W.	8.4	127.8
+4	9.6	126.6
W. cmt. cb.	9.70	126.50
cmt. gutter	10.44	125.76
+3 = E. Edge cmt. gutter	10.29	125.91
+7	9.7	125.5
+11 = W. edge Pavmt	10.02	126.18
℄ "	9.84	126.36
+10 = E " "	10.00	126.20
+12	12.0	124.2
+13	10.8	125.4
cb	10.7	125.5
E	11.0	125.2
+5	11.2	125.0
S. cb		
E-5	12.0	124.2
E	12.2	124.0
cb	12.5	123.7
+15 = E. Pavmt.	10.54	125.66
℄ "	10.43	125.77
+10 = W. "	10.59	125.61
+8 = ground	10.4	125.8

58

136.20

S. cl. Macaulay (con)

+4 = E. Edge cmt. gutter	11.01	125	19
+11 cmt. gutter	11.07	125	13
cmt. cl	10.32	125	88
+10	10.2	126	0
W	9.0	127	2
S. 1/4			
W.	9.4	126	8
+4	10.5	125	7
cmt. cl	10.80	125	40
" gutter	11.71	124	49
+3 = E. cmt. gutter	11.44	124	76
+3 on ground.	10.8	125	4
+11 = W. pavm't.	11.03	125	17
℄ "	10.88	125	32
E. "	11.03	125	17
cl	12.5	123	7
E	12.7	123	5
+5	12.6	123	6
4.5 E. of S. 1/4 = S. End cmt. walk on W.			
W. cmt. cl	11.11	125	09
+5 = E. Edge walk	11.08	125	12
+10 = W " "	10.94	125	26
+12	10.6	125	6
+14 W. Line	9.9	126	3

From this station N. cmt. gutter on W 1 s. 5' wide

136.20

℄

Chatsworth

E-5	13.1	123	1
E	12.9	123	3
cl	12.5	123	7
+15 = E. Pavm't	11.48	124	72
℄ "	11.35	124	85
+10 = W "	11.47	124	73
+6 ground	11.4	124	8
+6 = E. Edge cmt gutter	11.82	124	38
gutter ground.	11.7	124	5
cmt. gutter	12.30	123	90
W. cmt. cl	11.32	124	88
T.P. 1.48	125.84	11.84	124.36
N. 1/4			
N. cmt. cl.	1.48	124	36
gutter ground	2.45	123	39
cmt. gutter	1.9	123	9
+5 = E. cmt. gutter	1.97	123	87
+5 ground.	1.5	124	3
+11 = W. Pavm't.	1.56	124	28
℄ "	1.38	124	46
+10 = E. "	1.52	124	32
+15 = cl.	2.5	123	3
E.	2.8	123	0
+5	3.0	122	8

125.84

N. el

E-	2.0	123.8
+4	3.3	122.5
el	2.9	122.9
+15 = E. Pavmt	1.89	123.95
℄ "	1.79	124.05
+10 W "	1.97	123.87
+6 ground	1.9	123.9
+6 E. cmt. gutter	2.45	123.39
+11 " "	2.94	122.91
+11 = gutter dirt	2.2	123.6
+11 = W. cmt. el	1.95	123.89
00 = N. line Macawlay		
W. cmt. el	2.64	123.20
gutter dirt	2.8	123.0
cmt. gutter	3.63	122.21
+5 = E. edge gutter	3.15	122.69
+5 dirt	2.6	123.2
+11 = W. edge pavmt	2.54	123.30
℄ "	2.40	123.44
+10 = E " "	2.45	123.39
+12 = W. edge 3' cmt. gutter	3.10	122.74
+15 = E " " "	3.31	122.53
+15 E. cmt. el S. End.	2.35	123.49
+2.5 = W. edge cmt. walk	2.24	123.56
+7.5 = E " "	2.15	123.69
E. Line	2.0	123.8

From above Station W. cmt. gutter on E. 5' wide

125.84

41.4 N.

Chatsworth

60

E. cmt. el	4.54	121.28
cmt. gutter	5.56	120.28
+3 = W. edge gutter	5.33	120.51
+9	4.9	120.9
+15 = E. edge pavmt	4.82	121.02
℄ "	4.77	121.07
+10 = W " "	4.90	120.94
+6 = E. " cmt gutter	5.85	119.99
+6 dirt	5.3	120.5
+11 cmt. gutter	6.21	119.63
+11 W. cmt. el.	5.23	120.61
82.8 N. = S. line La Cresta Drive {60' wide, 10' cls		
Intersection Paved W. of 20' Pavmt.		
W. cmt. el	7.89	117.95
cmt. gutter to S.	8.78	117.06
gutter pavmt. & ground	8.44	117.40
+5 E. Edge cmt. gutter to S.	8.39	117.45
+5 Pavmt to W. & ground	7.98	117.86
+11 W. edge Strip Pavmt.	7.29	118.55
℄ "	7.12	118.72
+10 E " " "	7.26	118.58
+6	7.2	118.6
+12 = W. edge cmt. gutter	7.49	118.35
+15 " "	7.68	118.16
+15 E. cmt. el	6.73	119.11

125.84
℄ La Cresta

E. cmt. cb		8.30	117.54	
cmt. gutter		9.27	116.57	
+3 W. edge gutter		9.02	116.82	
+15 = E. edge parmt.		8.62	117.22	
℄ "		8.46	117.38	
W. edge 20' Strip Parmt		8.63	117.21	
00 = N. Line La Cresta Drive				
From La Cresta N. 70' Wide 10' cbs W. + E.				
20' Parmt. in Center 5' cmt gutter on W. 3' Gutter on East				
W. cmt. cb		10.05	115.79	
gutter parmt.		10.77	115.07	
W. edge cmt gutter to N.		11.07	114.77	
+5 cmt. gutter & parmt.		10.51	115.33	
+15 W. edge Strip parmt		9.94	115.90	
℄ " "		9.82	116.02	
+10 E. " " "		9.92	115.92	
+12 W. edge cmt. gutter		10.58	115.26	
+15 E " " "		10.84	115.00	
+15 E. cmt. cb.		9.86.	115.98	
T.P.	0.78	113.60	13.02	112.82
		52.5 N.		
E. cmt. cb			0.34	113.26
cmt. gutter			1.32	112.28
+3 = W. edge cmt. gutter			1.06	112.54
+15 = E. parmt.			0.41	113.19
℄ "			0.32	113.28

113.60 Chatsworth.

W. Parmt.	0.45	113.15
+10 = E. edge cmt. gutter	0.97	112.63
+15 = W. " " "	1.38	112.22
+15 = W. cmt. cb	0.43	113.17
105' N = S. Line Alley.		
W. line dirt	2.4	111.2
" " cmt cb Alley Return	2.93	110.67
+8 ground + W. edge cmt gutter	3.80	109.80
W. cmt. cb	3.15	110.45
gutter	4.24	109.36
+5 E. cmt-gutter	3.81	109.79
+15 W. parmt	3.27	110.33
℄ "	3.16	110.44
E "	3.15	110.45
+12 W. cmt. gutter	3.94	109.64
" " "	4.19	109.41
E. cmt. cb.	3.18	110.42
125' N. = N. Line Alley		
E. cmt. cb	4.23	109.37
cmt. gutter	5.22	108.38
+3 W cmt. gutter	4.99	108.61
+15 E. Parmt.	4.27	109.33
℄ "	4.13	109.47
W "	4.27	109.33
+5	4.2	109.4
+10 = E. cmt	4.87	108.73

113.60
125' N. (con)

cmt. gutter	5.25	108.35
W. cmt. cb	4.31	109.29
+2 ground & W. cmt gutter	4.91	108.69
N. Line cmt. cb. Ret.	4.13	109.47
" " ground	3.5	110.1
150' N.		
W. cmt. cb	5.64	107.96
cmt. gutter	6.63	106.97
+5 = E. cmt. gutter	6.20	107.40
W. Pavmt	5.61	107.99
℄ "	5.51	108.09
E. "	5.61	107.99
+12 W. cmt. gutter	6.31	107.29
" "	6.57	107.03
E. cmt. cb	5.61	107.99
200' N		
E. cmt. cb	8.30	105.30
cmt. gutter	9.26	104.34
+3. W. cmt. gutter	8.98	104.62
+15 E. pavmt	8.25	105.35
℄ "	8.16	105.44
W. "	8.31	105.29
+5	8.5	105.1
+10 E. cmt. gutter	8.89	104.71
~ " "	9.37	104.23
W. cmt. cb	8.38	105.22

113.60
250' N

W. cmt. cb		11.01	102.59
" gutter		12.00	101.60
+5 W " "		11.57	102.03
+10		10.9	102.7
+15 W pavmt		10.97	102.63
℄ "		10.80	102.80
E. "		10.91	102.69
+12 W. cmt. gutter		11.51	101.09
" "		11.78	101.82
E. cmt. cb		10.93	102.67
T.P. 1.06	101.73	12.93	100.67
300' N. = S. Line Olyphant			60' wide, 10' cbs, 10' 4s
E. cmt. cb		1.75	99.98
" gutter		2.47	99.26
+3 W " "		2.16	99.57
+15 = E. Pavmt		1.64	100.09
℄ "		1.45	100.28
W. "		1.60	100.13
+5		1.80	99.93
+10 = E. cmt. gutter		2.26	99.47
" "		2.64	99.09
W. cmt. cb		1.68	100.05
	W. cb		
W. cmt. cb		2.05	99.68
" gutter		3.05	98.68
+5 = E " "		2.66	99.07
+10		2.1	99.6

101.73

W. el. Olyphant

W. Line Pavm't.	1.99	99.74
℄ " "	1.84	99.89
℄ " "	2.03	99.70
E. el. Line	2.2	99.5
The 3' gutter on E. of Chatsworth follows Return into Olyphant		
el + 1.7 W. edge cmt. gutter around Return	2.33	99.40
5. Line cmt. gutter	2.76	98.97
" " " el.	1.76	99.97
" " 3' N. of S. el. = outer edge cmt gutter	2.57	99.16
W. ¼		
E	2.5	99.2
el	2.3	99.4
E. pavm't.	2.41	99.32
℄ "	2.24	99.49
W "	2.39	99.34
+ 5	2.4	99.3
+ 10 = E. cmt. gutter	3.00	98.73
" "	3.41	98.32
W " el.	2.41	99.32
℄		
W. cmt. el.	2.77	98.96
" gutter	3.77	97.96
+ 5.3 " "	3.35	98.38
+ 10	2.8	98.9
W. Pavm't.	2.75	98.98
℄ "	2.60	99.13

101.73

Chatsworth,

E. Pavm't.	2.73	99.00
el.	2.6	99.1
E	2.7	99.0
N ½		
E	3.6	98.1
el	3.3	98.4
E. pavm't	3.08	98.65
℄ "	2.90	98.83
W "	3.11	98.62
+ 5	3.0	98.7
+ 10 = E. cmt. gutter	3.71	98.02
+ 15 W " "	4.11	97.62
+ 15 W. " el	3.12	98.61
N. el.		
W. cmt. el	3.46	98.27
" gutter	4.45	97.28
+ 5 = E " "	4.03	97.70
+ 10	3.3	98.4
W. Pavm't	3.49	98.24
℄ "	3.32	98.41
E. "	3.41	98.32
el.	4.1	97.6
3' cmt. gutter on E. follows Return around into Olyphant		
el + 1.7 = W. side cmt. gutter around Return	4.48	97.25
5. Line cmt. gutter	4.73	97.00
" " " el	3.78	97.95
" " 3.5. of N. el. = outer edge cmt gutter	4.50	97.23

101.73

00 = N. line Oliphant

E. cmt. el	3.77	97	96
" gutter	4.75	96	98
+3 = W. " "	4.47	97	23
E. pavmt	3.79	97	94
℄ "	3.71	98	02
W "	3.83	97	90
+5	3.7	98	0
+10 = E. cmt. gutter	4.38	97	35
" "	4.83	96	90
W. cmt. el	3.85	97	88
350' N			
W. cmt. el	5.93	95	80
" gutter	6.90	94	83
+5 = E " "	6.44	95	29
+10	5.8	95	9
+15 = W. pavmt.	5.83	95	90
℄ "	5.64	96	07
E "	5.82	95	91
+12 = W. cmt. gutter	6.62	95	11
" "	6.90	94	83
E. cmt. el.	5.92	95	81
100' N.			
E. cmt. el	8.03	93	70
" gutter	9.00	92	73
+3 = W " "	8.74	92	99
E. pavmt.	8.44	93	65

101.73 chatsworth. 64

℄ Pavmt	7.90	93	83
W "	8.00	93	73
+5	8.0	93	7
+10 = E. cmt. gutter	8.54	93	19
" "	8.95	92	78
W " el	7.95	93	78
150' N			
W. cmt. el	10.14	91	59
" gutter	11.12	90	61
+5 = E. " "	10.62	91	11
+10	10.2	91	5
+15 = W. Pavmt.	10.26	91	47
℄ "	10.04	91	69
E. "	10.19	91	54
+12 = W. edge cmt. gutter	10.79	90	94
" "	11.11	90	62
E. cmt. el	10.12	91	61
200' N			
E. cmt. el.	12.21	89	52
" gutter	13.10	88	63
+3 = W " "	12.78	88	95
E. Pavmt	12.24	89	49
℄ "	12.07	89	66
W "	12.16	89	57
+5	12.2	89	5
+10 = E. cmt. gutter	12.74	88	99

101.73

200' N. (con)

cmt. gutter			13.16	88.57
W. cmt. eb			12.24	89.49
T.P.	0.37	89.11	12.99	88.74

250 N.

W. cmt. eb			1.67	87.44
" gutter			2.62	86.49
+5=E " "			2.14	86.97
+10			1.6	87.5
W. pavmt			1.62	87.49
℄ "			1.47	87.64
E. "			1.45	87.46
+12= W. cmt. gutter			2.09	87.02
E " "			2.41	86.70
E. cmt. eb			1.68	87.43

275' N. = S. Line Wawona Drive { 60' wide / 30' eks / 30' ½ }

E. cmt. eb.			2.69	86.42
" gutter.			3.35	85.76
+3= W " "			3.06	86.05
+3			2.6	86.5
E. pavmt			2.63	86.48
℄ "			2.48	86.63
W. "			2.60	86.51
+5			2.6	86.5
+10 = E. side cmt. gutter			3.18	85.93
" "			3.66	85.45
W. cmt. eb.			2.68	86.43

89.11

Chatsworth

65

Intersection W. of Pavmt See Book P

For existing cmt gutter Now Covered with dirt

W. eb. Line

W. Line cmt. eb.	2.63	86.48	
" " dirt gutter	3.3	85.8	
" eb. line	3.5	85.6	
W side Pavmt	2.96	86.15	
℄ "	2.83	86.28	
E " "	2.98	86.13	
E. eb. line	2.9	86.2	
3' cmt gutter on E. follows Return into Wawona			
eb + 17 = W. side cmt. gutter	3.16	85.95	
E line cmt. eb	2.67	86.44	
" " " gutter	3.59	85.52	
" " 3' N. of eb. = N. hip cmt gutter	3.35	85.76	

N. ½

E	3.3	85.8	
eb	3.1	86.0	
E. Line pavmt	3.33	85.78	
℄ "	3.19	85.92	
W " "	3.37	85.74	
eb	3.8	85.3	
W.	3.6	85.5	

89.11

℄ Wawona.

W.	3.9	85.2
cb	4.1	85.0
W. Line pavmt.	3.70	85.41
℄ "	3.58	85.53
E " "	3.72	85.39
cb	3.5	85.6
E	3.7	85.4
N. 1/4		
E	4.5	84.6
cb	4.0	85.1
E. Line Pavmt.	4.04	85.07
℄ "	3.91	85.20
W. " "	3.97	85.14
cb	4.4	84.7
W.	4.5	84.6
E. cb. Line		
W Line cmt. cb	4.62	84.49
" " dirt gutter	4.8	84.3
cb	4.8	84.3
W. Line Pavmt.	4.29	84.82
℄ "	4.17	84.94
E " "	4.36	84.75
cb.	5.0	84.1
3.' gutter on E. follows Return into Wawona		
+1.7 = W. Lip cmt. gutter	5.13	83.98
.5. Line cmt. cb	4.67	84.44

89.11

Chatsworth.

66

5. Line cmt. gutter	5.63	83.48
" " 3.' S. of above = outer Lip of gutter	5.26	83.85
00 = N. Line Wawona.		
E. cmt. cb.	4.67	84.44
" gutter	5.64	83.47
+3 = W " "	5.28	83.83
E. Line Pavmt	4.64	84.47
℄ "	4.48	84.63
W " "	4.61	84.50
+10 = E. edge cmt. gutter	5.14	83.97
cmt. gutter	5.55	83.56
W. cmt. cb.	4.60	84.51
6.5' N.		
W. cmt. cb	5.95	83.16
" gutter	6.93	82.18
+5 = ℄ "	6.47	82.64
+10	6.1	83.0
W. Line Pavmt	4.08	83.03
℄ "	5.92	83.19
E " "	6.07	83.04
+12 = W. cmt gutter	6.82	82.29
" "	7.15	81.96
E. cmt. cb.	6.20	82.91

89.11

130' N. = S. Line Alley

E. cmt. el	7.70	81.41
" gutter	8.68	80.43
+3 = W "	8.43.	80.68
E. Line Pavmt.	7.52	81.59
℄ "	7.32	81.79
W " "	7.45	81.66
+10 = E. edge cmt. gutter	7.85	81.26
+15 = " " "	8.22	80.89
W. cmt. el	7.18	81.93
+2' = W. edge cmt. gutter + ground	7.80	81.31
W. Line cmt. Alley el. Ret	6.92	82.19
" " ground.	6.6.	82.5

145' N. = N. Line Alley

W. Line ground	7.0	82.1
" " cmt. el. Return	7.27	81.84
+8 = W. edge cmt. gutter + dirt	8.15	80.96
W. cmt. el.	7.56	81.55
" gutter	8.57	80.54
+5 = E. edge cmt gutter	8.19	80.92
W " Pavmt.	7.85	81.26
℄ "	7.69	81.42
E " "	7.84	81.27
+12 = W " cmt. gutter	8.77	80.34
+15 = E " " "	9.06	80.05
+15 = E. cmt. el	8.08	81.03

89.11

210' N.

Chatsworth.

E. cmt. el	9.62	79.49
" gutter	10.55	78.56
+3 = W " "	10.24	78.87
+15 = E. edge Pavmt.	9.28	79.83
℄ "	9.16	79.95
W " "	9.27	79.84
+5	9.2	79.9
+10 = E. Edge cmt. gutter	9.46	79.65
+15 = " " " "	9.78	79.33
+15 = W. cmt. el.	8.83	80.28
T.P. 3.69	81.90	10.90 78.21

255' N. = S. End. Pavmt. on W. side Chatsworth

in Intersection of Poe St.

W. cmt. el	2.46	79.44
" gutter to S. + Pavmt. to N.	3.39	78.51
+5 = E. side cmt gutter to S. ½ Pavmt to N.	3.10	78.80
+10. dirt to S.	2.8	79.1
+15 = W. edge Pavmt.	3.01	78.89
℄ "	2.92	78.98
E " "	3.06	78.84
+12 = W. edge cmt. gutter	4.10	77.80
" "	4.35	77.55
E. cmt. el.	3.39	78.51

81.90

259.5' N. = S (W) End. 15' el. inlet on W.

W. cmt. cb	2.55	79.45
W. gutter S (W) End. Lip of el. inlet	3.52	78.38
270' N = S. End catch Basin. on E.		
E. cmt. cb.	3.70	78.20
gutter S.E. cor. catch Basin	4.73	77.17
+2.5 SW. " " "	4.58	77.32
+3 = W. edge cmt. gutter	4.37	77.53
+5	3.9	78.0
+15 = E. Edge pavmt.	3.37	78.53
275' N. = S. Line Poe St. {60' wide, 10' cbs, 10' 1/4s}		
E. cmt. cb.	3.84	78.06
gutter on N.E. cor catch Basin	3.91	77.99
+2.5 N.W. " " "	3.83	78.07
+15 = E. Line pavmt.	3.46	78.44
S. cb. Line		
E. Line cmt. cb.	3.99	77.91
" " " gutter W. End	5.02	76.88 No cmt. gutter around Return
3' N. of above = outer Lip. cmt. gutter	4.73	77.17
E. cb.	4.2	77.7
+15 = E. Line Pavmt.	3.64	78.26
S. 1/4		
E. Line	4.5	77.4
E. cb	4.0	77.9
+15 = E. Line Pavmt	3.78	78.12

81.90 chatsworth

68

℄ Poe St.

E. Line	4.4	77.5
E. cb.	4.1	77.8
+15 = E. Line pavmt.	4.00	77.9
N. 1/4		
E. Line	5.0	76.9
E. cb	4.5	77.4
+15 = E. Line pavmt	4.17	77.73
N. cb.		
S. Line cmt. cb	4.97	76.93
" " " gutter	5.97	75.93
3' S. of above = outer Lip cmt. gutter	5.67	76.23
3' cmt. gutter follows Return. into Poe St.		
+8.3 = W. edge cmt. gutter	5.55	76.35
E. cb. Line	5.3	76.6
+15 = E. Line pavmt.	4.33	77.57
00 = N. Line Poe St. N. End Pavmt N. 1/2 of Chatsworth		
E. cmt. cb.	4.92	76.98
cmt. gutter	5.89	76.01
+3 = W. edge cmt. gutter	5.58	76.32
+15 = E. edge pavmt.	4.44	77.46
℄ "	4.27	77.63
W. " "	4.38	77.52
+15 = E. edge cmt. gutter to E.	4.57	77.33 on pavmt
gutter pavmt.	4.70	77.20
W. cmt. cb.	3.85	78.05

81.90

50' N. of Poc

W. cmt. eb	4.07	77 83
cmt. gutter	5.05	76 85
+5 = E. edge cmt. gutter	4.66	77 24
+15 = W. " parmt.	4.66	77 24
℄ "	4.57	77 33
E " "	4.64	77.26
+12 = W " cmt. gutter	6.13	75 77
+14 ground	5.6	76.3
41 "	6.38	75.52
E. cmt. eb.	5.40	76.50

100' N of Poc

E. cmt. eb	5.92	75.98
" gutter	6.86	75 04
+3 = W. edge cmt. gutter	6.65	75.25
+4. ground	6.0	75.9
+15 = E " parmt	4.84	77.06
℄ "	4.70	77 20
W " "	4.81	77 09
+10 = E " cmt. gutter	4.78	77 12
" "	5.14	76.76
W. cmt. eb.	4.21	77 69

134.5 N = S. Lin Wabaska Section at 90°.

W. cmt. eb	4.34	77 56
gutter	5.23	76 67
+5 E. edge cmt. gutter	4.88	77.02
+15 = W. " parmt	4.93	76.97
℄ "	4.92	76.98
E " "	5.03	76.87

81.90 Chautsworth.

+11	6.3	75 6
+12 = W. edge cmt. gutter	6.91	74 99
+15 = E " " "	7.19	74 71
E. cmt. eb.	6.24	75 66

141.5 N. = N. End cmt. gutter on E.

E cmt eb.	6.24	75.62
dirt gutter	6.4	75.5
cmt. gutter at S. E. cor catch basin	7.26	74 64
3.0 S W. " " "	7.00	74 90
+7 dirt	6.2	757
+15 = E. edge parmt.	5.08	76 82
℄ "	4.96	76.94
W " "	4.96	76.94

From W. edge Parmt. West. Intersection Taken in

X Sec. Wabaska Book Page

143.5 N

E. cmt. eb. + dirt	6.30	75 60 ✓
gutter on N.E. cor. catch Basin	7.26	74 64
+2.5 " NW " " "	7.00	74 90
+3 dirt	6.0	759
+15 = E. Edge parmt.	5.16	76.74
℄ "	5.00	76 90
W. " "	5.00	76.90

81.90

152' N. = N. End cmt. cb. on E

E. Line			5.5		76.4
N. End. East. cmt. cb.			6.38		75.52
dirt gutter			6.3		75.6
+3			6.3		75.6
+15 = E. Edge pavmt.			5.29		76.61
℄ "			5.03		76.87
W " "			4.98		76.92
T.P. B.M. E. cb	8.91	86.05	4.76	77.14 = 77.14	N. Line Wabaska

187.5 N. = S. End. cmt. cb. on E.

E. Line			7.5		78.5
S. End. E. cmt. cb. & ground.			8.99		77.06 ✓
+15 = E. Edge Pavmt.			9.34		76.71
℄ "			9.42		76.63
W " "			9.14		76.91

189.5 N. = S. End Catch Basin on E. cb

E. cmt. cb.			8.88		77.17
gutter on S.E. Cor catch Basin			9.02		77.03
+3' W = S.W. " " " & ground.			9.02		77.03
+15 = E. Edge pavmt.			9.29		76.76
℄ "			9.31		76.74
W " "			9.12		76.93

193.5 N. = N. End Catch Basin

E. cmt. cb.			8.69		77.36
gutter at N.E. cor catch basin			9.61		76.44
+1.75 W = N. Edge cmt. gutter to N			9.62		76.43
+3' W = N.W. cor. catch Basin			9.47		76.58
+4 ground			9.0		77.0

86.05

Chatsworth.

193.5
89.5
97.5

70

+15 = E. Edge pavmt.			9.10		76.95
℄ "			9.11		76.94
W " "			9.07		76.98

200' N

E. cmt. cb.			8.41		77.64
cmt gutter			9.34		76.71
+1.75 = W. edge cmt. gutter			9.20		76.85
+4 ground.			8.8		77.2
+15 = E. edge pavmt			8.88		77.17
℄ "			8.80		77.25
W " "			8.80		77.25

240' N. = N. End P.C. 13' Radius Return N.W. cor. { Chatsworth & Wabaska.

E. cmt. cb.			6.57		79.48
cmt. gutter			7.51		78.54
+1.75 = W. edge cmt. gutter			7.37		78.68
+4			7.0		79.0
+15 = E. Edge pavmt.			7.29		78.76
℄ "			7.18		78.87
W " "			7.32		78.73

Sewer being constructed bet cb + Pavmt

W. cmt. cb.			7.90		78.15

275.5 N. = S. Line Quimby { 60' Wide, 10' cbs, 10' yds.

W. cmt. cb.			5.98		80.07
+15 = W. Edge Pavmt			5.82		80.23
℄ "			5.64		80.41
E " "			5.71		80.34

86.05

S. line Quimby (con)

+11	5.3	80 7
+13.25 = W. edge cmt. gutter	5.67	80.38
" "	5.84	80.21
E. cmt. el.	4.86	81.19

1.75 cmt. gutter on E. follows Return into Quimby

S. el. Line

E. Line cmt. el.	4.81	81 24
" " " gutter	5.48	80 37
1.75 N. of above = outer Lip gutter	5.60	80.45
E +6.5 = W. edge cmt. gutter	5.58	80.47
el. Line	5.4	80.6
+5	5.0	81.0
+15 = E. Edge pavmt.	5.39	80.66
℄ "	5.29	80.76
W " "	5.44	80 61
W cmt. el	5.45	80.60

S. 1/4

W. cmt. el.	4.97	81 08
+15 = W. edge pavmt.	5.06	80.99
℄ "	4.88	81.17
E " "	5.03	81.02
+10	4.9	81.1
el. Line	5.2	80.8
E. "	5.0	81.0

86.05

℄

Chatsworth

E	4.9	81.1
el	5.0	81.0
+5	4.7	81.3
+15 = E. Edge pavmt	4.71	81.34
℄ "	4.55	81.50
W. " "	4.73	81.32
W. cmt. el.	4.49	81 56

N. 1/4

W. cmt. el.	3.98	82 07
+15 = W. Edge pavmt	4.39	81.66
℄ "	4.20	81.85
E " "	4.37	81.68
el	4.7	81.3
E	4.9	81.1

N el. Line

E. Line cmt. el.	3.83	82 22
" " " gutter	4.74	81 31
1.75 S. of Above = outer Edge gutter	4.64	81.41
+6.0 = W. Edge cmt. gutter	4.75	81.30

1.75 cmt. gutter on E. follows Return into Quimby

el. Line	4.5	81.5
+15 = E. Edge Pavmt.	4.07	81.98
℄ "	3.85	82.20
W " "	4.01	82.04
W. cmt. el.	3,50	82.55

84.05

(1) 00 = N. Line Quimby on East.

W. emt. el.		3.01	83 04
+15 = W. edge pavmt		3.67	82 38
℄ "		3.51	82 54
E " "		3.68	82 37
+13.25 = W. edge emt. gutter,		4.59	81. 46
emt. gutter		4.69	81.36
E " el.		3.78	82. 27

(2) 10' N.

E. emt. el		3.20	82. 85
" gutter		4.15	81 90
+1.75 = W "		3.99	82. 06
+15 = E. edge pavmt		3.17	82. 88
℄ "		3.03	83 02
W " "		3.20	82. 85
W. emt. el.		2.48	83. 57

(3) 50' N.

W. emt el		0.34	85. 71
+15 = W edge Pavmt.		0.88	85 17
℄ "		0.69	85 36
E " "		0.88	85 17
+13.25 = W " emt. gutter		1.51	84. 54
" "		1.67	84 38
E. emt el.		0.70	85 35
T.P.	12.16 98.12	0.03	86. 02

98.12. Chatsworth

(4) 100' N

E. emt. el		9.65	88 47
" gutter		10.62	87. 50
+2.75 = W. edge emt. gutter		10.49	87. 63
+15 = E. edge pavmt.		9.97	88 15
℄ "		9.84	88 28
W " "		10.01	88. 11
W. emt. el.		9.95	88. 16

(5) 153' N

W. emt. el		7.30	90. 82
+15 = W. Edge pavmt.		7.00	91 12
℄ "		6.76	91 36
E " "		6.87	91. 25
+13.25 W. edge gutter		7.19	90 93
emt gutter		7.33	90 79
E. emt. el		6.33	91. 79

(6) 173' N. = { P.C. Return curve into centralcma / S. edge Intersection Pavment on W. side strip pavmt

E. emt el		5.08	93 04
emt. gutter		6.06	92 06
+1.75 = W. edge. gutter		5.93	92 19
+15 = E. edge. pavm't.		5.78	92 34
℄ "		5.67	92 45
W " "		5.81	92 31
+7.5 on S. Edge pavmt		6.26	91 86
+15 = gutter on S. edge Intersection pavmt		6.84	91 28
W. emt. el.		6.23	91. 89

72

98.12

193' N.

E. cmt. cb	4.33	93 79
cmt. gutter	5.30	92 82
+1.75 = W. edge cmt. gutter	5.17	92 95
+15 = E. edge pavmt.	5.05	93 07
℄ strip "	4.85	93 27
W Edge +7.5 W Cb Line W Line part		93 06 / 92 81 / 92 54 / 92 28
224' N.		
E. cmt. cb	3.25	94 87
" gutter	4.22	93 90
+1.75 = W. edge gutter	4.09	94 03
+15 = E. " pavmt	4.00	94 12
℄ strip "	3.88	94 24
W Edge +7.5 Cb Line W Line		94 11 / 94 05 / 94 12 / 94 08
255' N.		
E. cmt. cb	2.15	95 97
" gutter	3.11	95 01
+1.75 = W. edge gutter	3.00	95 12
+15 = E. edge pavmt.	2.94	95 18
℄ "	2.87	95 25
W Edge +7.5 Cb Line W Line		95.20 / 95.09 / 95.11 / 95.10
275' N = S. Line Tennyson St		40' wide / 10' cbs / 10' 1/4s
E. cmt. cb	1.46	96 66
cmt. gutter	2.44	95 68
+1.75 = W. edge gutter	2.28	95 84
+15 = E. Edge pavmt	2.27	95 85
℄ "	2.21	95 91

98.12 Chatsworth

73

S. cb. Line

E. Line cmt. cb	1.48	96 64
" " " gutter	2.45	95 67
1.75 cmt. gutter on E. follows Return into Tennyson		
1.75 N. = outer Lip of gutter	2.30	95 82
S + 6.4 = W. edge cmt. gutter	2.27	95 85
E. cb Line	2.1	96.0
E. Line Pavmt.	2.08	96 04
℄ "	2.01	96 11
S. 1/4		
E. Line	1.9	96 2
E. cb. "	2.0	96.1
E " pavmt	1.98	96 14
℄ "	1.93	96 19
℄		
E. Line	1.6	96 5
E. cb. "	1.9	96 2
E " pavmt.	1.90	96 22
℄ "	1.82	96 30
N. 1/4		
E. Line	1.6	96 5
E. cb "	1.8	96 3
E " pavmt.	1.86	96 26
℄ "	1.76	96 36
N. cb. Line		
E. Line cmt. cb	0.95	97 17
" " " gutter	1.88	96 24
1.75 S. of above = outer Lip gutter	1.73	96 39

1.75 gutter on E follows Return into Tennison

98.12

N. el. Line Tennyson (con)

E + 2.5 = W. edge cmt gutter	1.78	96.34
E. el Line	1.6	965
℄ " Pavmt.	1.75	96.37
℄ "	1.64	96.48

(1) 00 = N. Line Tennyson Ave. { E. el. R = 358.10 ; Δ = 28-49-30

E. cmt. el	0.97	97.15
" gutter	1.96	96.22
+ 1.75 = W. edge cmt. gutter	1.82	96.30
+ 2 + 15 = E. " pavmt.	1.66	96.46
℄ "	1.54	96.58
W. edge strip "	1.73	96.39
+ 7.5 on pavmt	2.04	96.08
gutter "	2.51	96.61 95.61
W. cmt. el.	1.96	96.22

S.E. Chatsworth

T.P. B.M.	6.97	103.63	1.46 96.66 = 96.65 + Tennyson

end W el Line 51.26

(2) See A. Δ 7-12-22½ chd E. el. Line 45.01

Curb is 0.95 out of Line

0.95 E. of E. el. Line = E. cmt. el	6.07	97.56
cmt. gutter	7.04	96.59
E. el. Line on " "	6.98	96.65
" " " + 0.8 = W. edge 1.75 cmt. gutter	6.92	9671
" " " + 7.5 = E. Edge Pavmt.	6.91	96.72
℄ "	6.72	96.91
W. " "	6.83	96.80

(3) See B. Δ 14°-24'-45"

Curb is 0.55 out of Line

6.55 E. of E. el. Line = E. cmt. el.	6.00	9667
cmt. gutter	6.96	9667

103.63

Chatsworth Blvd.

T.R. 1.46

E. el Line on cmt. gutter	6.90	96.73
" " " + 1.20 = W. edge 1.75 gutter	6.82	9681
℄ " " + 2 dirt	6.4	97.2
" " " + 15 = E. Edge pavmt.	6.48	97.15
℄ "	6.36	97.27
W. " "	6.52	97.11

(4) See # E. Δ 21°-37'-07" E. el. OK

E. cmt. el & dirt on Roadway	5.86	97.77 Here
cmt. gutter	6.82	~~97.81~~ 96.81
+ 1.75 = W. edge cmt. gutter	6.69	9694
+ 2 dirt	6.1	97.5
+ 15 = E. edge pavmt.	6.13	97.50
℄ "	5.98	97.65
W. " "	6.09	97.54

Sec D Δ 23°-57'-24" = P.I. = N. End cmt. gutter on S.

E. cmt. el	5.81	97.82
gutter dirt	6.0	97.6
cmt. gutter	6.80	9683
+ 1.75 = W. edge cmt. gutter	6.78	9685
+ 2 dirt	6.0	97.6
+ 15 E. Edge pavmt.	5.97	97.66
℄ "	5.83	97.80
W. " "	5.96	97.67

(5)

E.C. 103.63 = 00

E. cmt. cb	5.36	98 27
dirt gutter	5.6	98 0
+15 = E. edge pavm't	5.39	~~97 24~~ 98.24
℄ "	5.33	98.30
W " "	5.42	98 21

53.5 (E) N

E. cmt. cb	4.64	98.99
dirt gutter	5.0	98 6
+15 = E. edge pavmt	4.83	98 80
℄ "	4.72	98.91

+35 W Cb — 98.82, 98.23

W. side chatsworth paved from S. Line Villa Drive North at 90° to chatsworth 107' N = S. Line Voltaire on E. { 68.81 wide, 11.47 cbs, 11.47 1/4s.

E. cmt cb + dirt in Rdw.	4.11	99.52
+15 = E. Line pavmt.	4.32	99.30
℄ "	4.13	99.50

+35 W Cb — 99.37, 99.82

S. cb. at 90° from chatsworth (118.47)

E. Line cmt. cb. + dirt	3.67	99 96
cb "	4.0	99.6
+15 = E. edge pavm't	4.14	99 49
℄ "	3.95	99 68

+35 W. Cb. — 99.52, 98.93

S. 1/4 (129.94)

E	3.0	100 6
E. cb	3.4	100 2
+15 = E. Line pavm't	3.98	99 65
℄ "	3.78	99 85

+35 W Cb — 99.69, 99.10, 99.24, 99.63

+15 Tp Cb

(141.41)

103.63 ℄

chatsworth

75

E	2.3	101.3
E. cb Line	2.9	100.7
+15 = E. Line pavm't	3.79	99 84
℄ "	3.61	100 02

+35 +42.5 Cb Line +7.4 Tp Cb — 99.85, 99.63, 99.30, 99.40, 100.02

N 1/4 (152.88)

E	2.5	101.1
E. cb Line	2.8	100.8
+15 = E. Line pavm't	3.57	100 06
℄ "	3.33	100 30

+35 +42.5 W Cb Line — 100.11, 99.88, 99.62

N. cb. Line (164.35)

E. Line on cb. Line to E. on dirt	2.4	101.2
1.47 N. of above = E. Line on 10' Rad. Return	2.70	100 93
E. cb. Line	3.0	100.6
+15 = E. edge pavm't	3.18	100.45
℄ "	2.97	100.66

+35 +42.5 W Got Tp Cb — 100.58, 100.56, 100.07, 100.96

N. Line Voltaire to E. Sec. at 90° to chatsworth (175.82)

E. cmt. cb.	2.37	101 26
gutter dirt	2.8	100.8
+15 = E. edge pavm't	2.57	101.06
℄ "	2.33	101 30

+35 +42.5 W Got T Cb — 101.18, 100.96, 100.59, 101.28

2.32 N = P.C. Δ = 24°30' E. cb. Radius (178.14)

E. cmt. cb	2.25	101.38

From Voltaire on E. to Voltaire to W. Sewer under construction on E. No readings for yardage

+15 = E. edge pavm't	2.44	101.19
℄ "	2.21	101 42

103.63

chd on W. cl. Line 34.94

See A Δ 2°-56'-45" chd. on E. cl. Line 37.51

E. emt. cl		0.16	103.	47
+15 = E. edge Pavm't.		0.19	103	44
℄ "		0.05	103.	58
T.P.	12.67	116.25	0.05	103.58

See B. Δ 5°-52'-30" (53,)

E. emt. cl		10.49	105	76
+15 = E. edge pavm't.		10.53	105.	72
℄ "		10.40	105	85

See C. Δ = 8°-49'-15" (50,)

E. emt. cl		8.20	108	05
+15 = E. Edge pavmt.		8.30	107.	95
℄ "		8.18	108.	07

See D Δ = 11°-46' (47,)

E. emt. cl		5.97	110.	28
+15 = E. Edge pavmt.		6.12	110.	13
℄ "		5.97	110	28

See E Δ = 14°-42'-45" (43)

E. emt. cl		3.54	112.	71
+15 = E. edge pavmt.		3.83	112.	42
℄ "		3.68	112	55

See F Δ = 17°-39'-30" (40,)

E. emt. cl		1.34	114	91
+15 = E. edge pavm't		1.66	114	59
℄ "		1.48	114.	77
T.P.	5.93	121.95	0.23	116.02

121.95

chatsworth

116.83

76

See G Δ = 20°-36'-15" (37,)

E. emt. cl		5.19	116	76
+15 = E. Line pavm't		5.25	116	70
℄ "		5.08	116.	87

This section Not on Radial Line. on S. Line Vollaire To West.

See H Δ = 23°-34'-00" = S. Line Vollaire produced from W = S. End. Full Width Pavmt. on E. cl.

E. emt. cl.		3.40	118.	55
gutter on pavmt to N.		3.76	118	19
+7.5'		3.53	118	42
+15 = E. Line strip pavmt. to S.		3.43	118	52
℄ Pavmt. on S. Line Voltaire		3.42	118.	53
chk on B.M. S.W. Chatsworth + Vollaire		5.14	116.81 = 116.83	

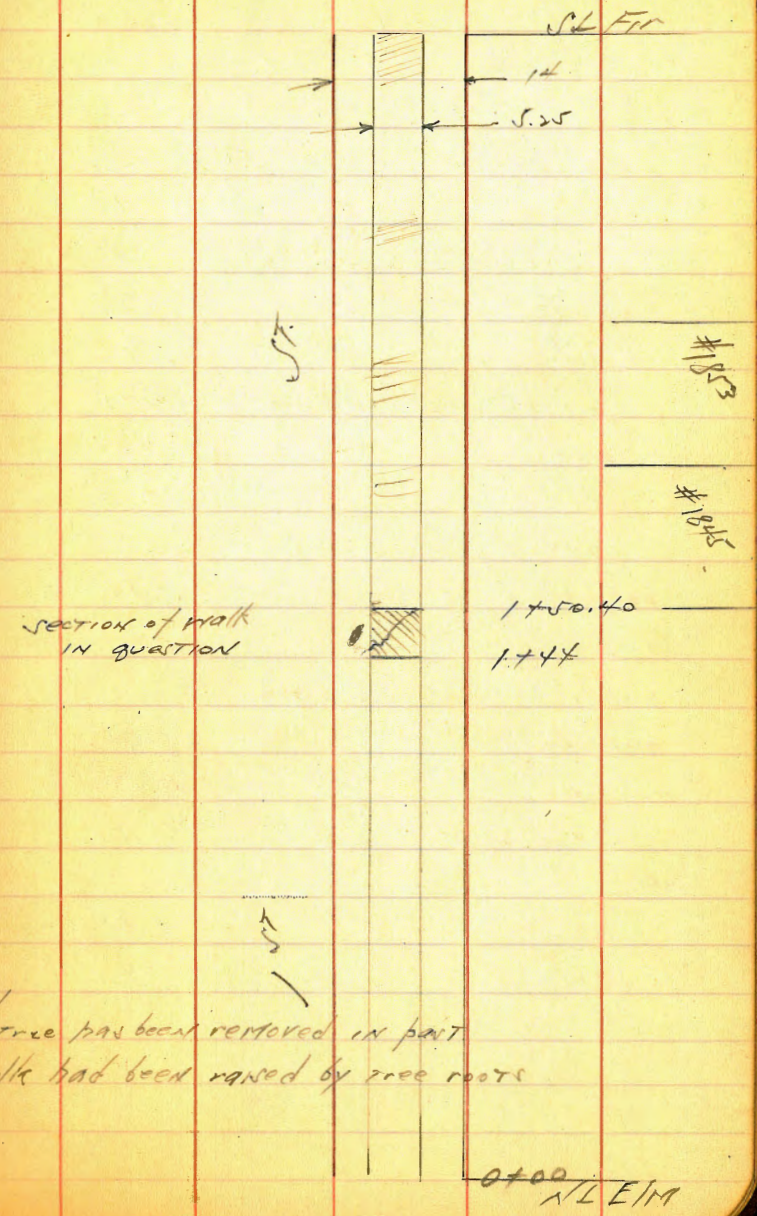
Levels on E Sidewalk on 1st St
betw. Elm & Fir Sts.

	1.27[illegible]	125.65	112.93
0+00 = NLE/M			
cb		12.70	
outside edge walk		12.58	
inside " "		12.46	
0+50			
cb		9.25	
outside		9.19	
inside		9.14	
1+00			
cb		5.74	
outside		5.61	
inside		5.53	
1+23.5			
cb		4.29	
outside		3.99	
inside		3.81	
1+44			
outside		2.56	
inside		2.48	
1+50.40			
outside		2.00	
inside		2.01	
1+50.45			
outside		2.08	
inside		2.00	

Moore
2/5/34

indexed
C.S.K.

77



Note! Tree has been removed in past
walk had been raised by tree roots

125.65

T.P.	10.7N	136.96	0.41	125.24
	2+00			
ob				9.17
outside				9.07
inside				8.97
	2+04 = SL new porch			
ouside				8.78
inside				8.66
	2+12.5 = NL new porch			
outside				8.24
inside				8.10
	2+44.5 = SL new porch			
outside				7.88
inside				7.77
2+49.3	= NL new porch			
outside				7.64
inside				7.47
	3+00.6			
ob				2.03
outside				1.89
inside				1.79

IMPROVED TABLES
AND
INFORMATION

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1½ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

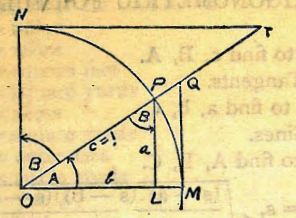


TABLE II

TRIGONOMETRIC FORMULÆ.

$\angle A = \angle MOP \qquad \angle B = \angle PON = \angle OPL$

$R = OB = c = 1$

$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$

$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$

$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$

$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$

$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$

$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$

$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B$ #

$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$

$\text{exsec } A = PQ = \text{coexsec } B$

$\text{coexsec } A = PT = \text{exsec } B$

$\sin \tfrac{1}{2} A = \sqrt{\frac{1 - \text{Cos } A}{2}} \qquad \cos \tfrac{1}{2} A = \sqrt{\frac{1 + \text{Cos } A}{2}}$

$\sin 2A = 2 \sin A \cos A \qquad \cos 2A = \cos^2 A - \sin^2 A$

Law of Sines $\frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C}$

Law of Cosines $c^2 = a^2 + b^2 - 2ab \cos C$

Law of Tangents $\frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$

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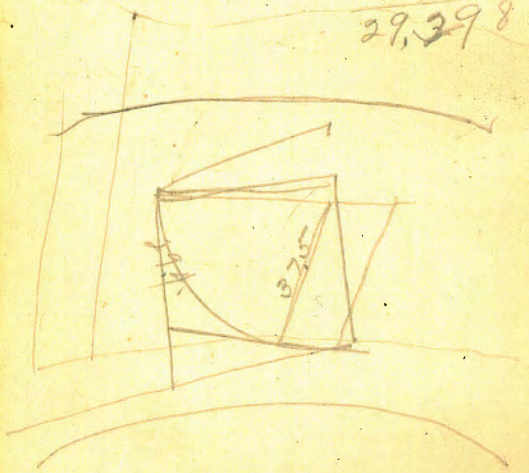
76.06
38.03

.7813
47.5
39065
54691
31255
37.11175

.7813
37.5
39065
54691
23439
29.39875



1875 S. End cl.
2900.

145
130
275

145
165
210
45

89.11
2.67
86.44

89.11
10.90
78.21

17.5
34.5
52.0

193
31
224
255

193
82.2
275.2

240
285.6

275
193
82