

1385

ATLANTIC ST.

EXTENSION

PASTS

LEVEL BOOK

No. 809F

MICROFILMED

DEC 23 1964

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

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Walker
W.D. BAS
Drebert
Mattoon
2-30

Cross Section ATLANTIC at Extension
120' wide from station 0+00 to Sta 36+00
thence 100' wide from 36+00 to Sta.

U.S.G.S. 511.
Sta 1600
Red Top Canyon

3.5A 22.85 19.31
L 80/1600 Ave = 0+00 Section Parallel to 80/1600 Ave

E-25	2.5	20.4
E	3.1	19.8
L	4.2	18.7
M	5.3	17.6
+25	5.8	17.1

0+585 = N edge Paving Section Parallel to Paving

-25' on Paving	6.02	16.83
M " "	5.46	17.39
L " "	4.35	18.50
E " "	3.12	19.73
+25 " "	2.51	20.34

0+25.85 = South edge Paving Section Parallel to Paving

-25 " "	2.51	20.34
E " "	3.11	19.74
L " "	4.31	18.54
M " "	4.88	17.97
+25 " "	6.01	16.84

0+36

-25	5.9	17.0
M	5.4	17.5
L	4.5	18.4
E	3.0	19.9
+25	2.3	20.6

22.85

0+40

-25	3.6	19.3
E	3.9	19.0
L	4.5	18.4
M	5.6	18.3
+25	6.1	16.8

0+50

-25'	5.0	17.9
M	4.8	18.1
L	4.2	18.7
E	2.1	20.8
+25	1.0	21.9

0+61.89 = A bit 8° 52' Section on Bisector.

-25	1.5	21.4
E	1.8	21.1
+15	2.3	20.6
+20	3.3	19.6
L on Hub.	5.05	17.80
M	6.0	16.9
+25	6.4	16.5

1+00

-25'	7.2	15.7
M	6.5	16.4
L	5.0	17.9
+35	3.9	19.0
+40	2.5	20.4

22.85

E	2.2	20.7
+25	2.0	20.9
1+50		
-25	2.4	20.5
E	2.4	20.5
+10	2.5	20.4
+15	4.1	19.8
♀	5.4	17.5
+15	6.3	16.6
+25	7.1	15.8
M	7.1	15.8
+25	7.2	15.7
2+00		
-25	7.2	15.7
M	7.1	15.8
+15	5.7	17.2
+22	6.8	16.1
+40	7.0	15.9
♀	5.1	17.8
+40	4.3	18.6
E	3.0	19.9
+25	2.4	20.5
2+50		
-25	2.5	20.4
E	3.3	19.6
+10	5.8	17.1

22.85

♀	6.4	16.5
+10	7.3	15.6
+22	6.1	16.8
+45	7.5	15.4
M	7.5	15.4
+25	7.9	15.0
3+00		
-25	7.9	15.0
M	8.0	14.9
+22	7.0	15.9
+28	6.3	16.6
♀	7.1	15.8
+40	6.2	16.7
E	4.2	18.7
5+25	3.1	19.8
3+50		
E-25	4.1	18.8
E	5.3	17.6
+5	6.6	16.3
♀	7.5	15.4
+22	7.0	15.9
+48	8.1	14.8
M	7.4	15.5
+10	7.6	15.3
+25	8.4	14.5
4+00		

2

22.85

18.93

-25		8.7	14.2
-13		8.3	14.6
-10		7.9	15.0
N		8.5	14.4
+25		7.7	15.2
+42		6.7	16.2
Σ		7.7	15.2
+10		6.3	16.6
E		6.9	16.0
+5		6.1	16.8
+25		5.0	17.9
T.P.	106	18.93	4.98
	4+50		17.87
-25		1.6	17.3
E		2.6	16.3
+15		3.5	15.4
+40		2.9	16.0
Σ		3.7	15.2
+24		4.0	14.9
N		4.9	14.0
+3		4.0	14.9
+12		4.7	14.2
+25		5.0	13.9
-25		5.6	13.3
-10		4.8	14.1

5+00.39 P.C. Lt. 19°35' & R=1933.7

sections in this
curve
on radial line

N		4.7	14.2 ³
+1		5.5	13.4
+10		4.1	14.8
Σ on Hub.		4.30	14.63
+5		3.7	15.2
+28		3.2	15.7
+37		4.2	14.7
E		3.4	15.5
+8		2.2	16.7
+25		3.2	16.7
	5+50		
-25		1.7	17.2
E		3.8	15.1
+10		4.3	14.6
+21		3.6	15.3
Σ		4.4	14.5
N		5.4	13.5
+25		5.9	13.0
	6+00 = beginning of Wall on West on side of line MAGNOLIA Ave.		
-25 on Wall		4.5	14.4
-25 Ground		5.5	13.4
N " "		4.8	14.1
" " Wall		3.8	15.1
+15		5.9	13.0
Σ		4.4	14.5
+25		4.0	14.9

18.93

E	4.5	14.4
+6	4.4	14.5
+13	2.9	16.0
+25	2.0	16.9
6+50		
-25	+1.5	20.4
-17	0.0	18.9
E	4.3	17.6
E	4.8	14.1
+31	5.9	13.0
+35	6.8	12.1
W	6.6	12.3
+4 - Base of cobble Wall	6.6	12.3
+5 - top " " "	4.7	14.2
7+00		
-6' on top cobble Wall	5.5	13.4
-6 Base " "	7.5	11.4
W	7.5	11.4
+13	7.5	11.4
+25	5.7	13.2
E	5.0	13.9
E	4.8	14.1
+20	+4.7	23.6
7+50		
-20	+6.2	25.1
E	4.8	14.1

18.93

E	5.1	13.8
+27	5.4	13.5
+40	7.9	11.0
W	7.7	11.2
+6 - Base Cobble Wall	7.6	11.3
+7 top " "	6.3	12.6
8+00		
-9 - top cobble Wall	6.6	12.3
-8 - Base " "	8.1	10.8
W	9.2	9.7
+10	8.6	10.3
+25	5.5	13.4
E	5.3	13.6
E	4.1	14.8
+20	+4.8	23.7
8+24 ^{on West} End Cobble Wall on top	6.4	12.5
8+50		
-10	4.2	14.7
E	4.6	14.3
E	5.7	13.2
+25	5.9	13.0
+38	9.2	9.7
W	9.3	9.6
+20	9.3	9.6
9+00		
-20	9.6	9.3

4

18.93

-3		9.7	9.2
W		10.1	8.8
+17		9.6	9.3
+34		5.7	13.2
2		5.8	13.1
+24		6.6	12.3
E		6.2	12.7
+15		1.4	17.5
	9+50		
-10		6.4	12.5
E		7.2	11.7
2		5.8	13.1
+22		6.8	12.1
+33		10.1	8.8
W		10.2	8.7
+20		10.2	8.7
T.P.	6.99 16.62 [✓]	9.30	9.63
	10+00		
-20		8.8	7.8
W		8.1	8.5
+25		8.1	8.5
+35		4.0	12.6
2		3.9	12.7
E		4.9	11.7
+10		5.8	10.8
	10+50		

16.62

5

-20		5.4	11.2
E		5.8	10.8
+20		6.3	10.3
2		4.1	12.5
+19		4.6	12.0
+20		7.1	9.5
+29		8.7	7.9
W		9.2	7.4
+1		8.5	8.1
+25		9.8	6.8
	11+00		
-25		10.6	6.0
-10		9.0	7.6
W		9.6	7.0
+25		9.2	7.4
+34		7.1	9.5
+40		4.6	12.0
2		4.3	12.3
+15		6.3	10.3
E		6.1	10.5
+20		6.0	10.6
	11+61.92 = E.C.		
-20		6.4	10.2
E		6.6	10.0
+15		6.8	9.8
+20		5.7	10.9

16.62

+40	6.3	10.3
$\frac{1}{2}$ on Hub.	4.56	12.06
+6	5.1	11.5
+15	9.1	7.5
+28	9.8	6.8
W	9.8	6.8
+25	11.6	5.0
12+00		
-25	11.8	4.8
-10	11.3	5.3
-15	10.0	6.6
+28	8.4	8.2
+30	9.4	7.2
+35	9.0	7.6
+45	5.2	11.4
$\frac{1}{2}$	4.6	12.0
+6	5.0	11.6
+10	6.3	10.3
+25	5.4	11.2
+30	7.1	9.5
E	6.7	9.9
+20	6.3	10.3
13+00		
-20	6.3	10.3
E	6.6	10.0
+40	6.8	9.8

16.62

6

+45	5.5	11.1
$\frac{1}{2}$	4.9	11.7
+6	5.9	10.7
+13	9.5	7.1
+26	10.4	6.2
W	8.1	8.5
+10	7.1	9.5
+15	12.3	4.3
+25	12.7	3.9
14+00		
-25	12.0	4.6
W	10.6	6.0
+35	9.1	7.5
+45	6.3	10.3
$\frac{1}{2}$	5.3	11.3
+6	6.1	11.5
+11	7.5	9.1
E	6.4	10.2
+20	6.1	10.5
15+00		
-20	7.2	9.4
E	7.4	9.2
+40	7.6	9.0
+45	6.1	10.5
$\frac{1}{2}$	5.6	11.0
+6	6.6	10.0

1662

+13		10.0	6.6	
W		10.8	5.8	
+10		11.0	5.6	
+25		12.1	4.5	
	16+00			
-25		11.5	5.1	
-10		10.5	6.1	
W		10.3	6.3	
+35		10.2	6.4	
+23		7.1	9.5	
L		6.1	10.5	
+7		6.9	9.7	
+11		8.0	8.6	
E		7.2	9.4	
+25		6.7	9.9	
TP	3.49	14.37 ^v	5.74	10.88
	17+00			
-25		3.8	10.6	
E		5.0	9.4	
+40		5.8	8.6	
L		4.3	10.1	
+6		4.8	9.6	
+16		7.6	6.8	
W		7.9	6.5	
+20		7.5	6.9	
	18+00			

1437

-25'		7.8	6.6
W		7.5	6.9
+35		7.3	7.1
+45		5.3	9.1
L		4.6	9.8
+10		5.1	9.3
E		4.5	9.9
+20		4.1	10.3
	19+00		
-20		4.4	10.0
E		5.3	9.1
+40		5.3	9.1
L		4.6	9.8
+6		5.3	9.1
+12		6.8	7.6
W		7.5	6.9
+25 on old RR. Bed		5.9	8.5
	19+50		
-25'		6.4	8.0
-10		5.1	9.3
W		6.1	8.3
+5		6.6	7.8
+30		5.9	8.5
+35		7.2	7.2
+43		5.5	8.9
L		4.8	9.6

14.37

+10	5.3	9.1
+13	5.1	8.8
E	5.3	9.1
+25	4.5	9.9
20+00		
-25	4.7	9.7
E	5.5	8.9
+40	5.6	8.8
2	4.8	9.6
+6	5.8	8.6
+10	7.6	6.8
+18	7.7	6.7
+37 on old RR Bed.	5.0	9.4
W " " " "	5.0	9.4
+25	8.0	6.4
20+75		
-25	9.2	5.2
W-3'	8.6	5.6
W	7.7	6.7
+5' on RR Bed.	6.2	8.2
+17 " " "	4.8	9.6
+30	5.4	9.0
+33	7.0	7.4
+40	7.5	6.9
+42	5.3	8.5
2	5.0	9.4

14.37

+10	5.7	8.7
+45	5.9	8.5
E	5.4	9.0
21+00		
-25	3.7	10.7
E	5.6	8.8
+5	6.0	8.4
+40	5.7	8.7
2	5.1	9.3
+28	4.9	9.5
+42	6.0	8.4
W	8.6	5.8
+25'	3.7	4.7
22+00		
-25	10.4	4.0
W	9.3	5.1
+20	8.5	5.9
+28	6.1	8.3
+38	5.0	9.4
2	5.3	9.1
+10	6.1	8.3
E	5.9	8.5
+8	5.7	8.7
+13	4.6	9.8
+25	4.2	10.2
23+00		

8

14.37

E-25'		4.5	9.9	
E		5.4	9.0	
+5		5.6	8.8	
+40		6.7	7.7	
L		5.3	9.1	
+10		6.0	8.4	
+20		8.3	6.1	
M		8.5	5.9	
+25		10.1	4.3	
T.P.	3.90	14.05	4.22	10.15
	24+00			
-25'		8.1	6.0	
M		7.2	6.9	
+20		7.4	6.7	
+35		6.7	7.4	
+42		5.6	8.5	
L		5.2	8.9	
+5		5.5	8.6	
+25		4.5	9.6	
E		4.8	9.3	
+20		3.0	11.1	
	25+00			
-25'		3.0	11.1	
E		3.0	11.1	
+5		3.9	10.2	
+30		4.2	9.9	

on Can. Merz
07 E
pp. 23+00

14.05

9

L		5.0	9.1
+23		5.9	8.2
+28		6.9	7.2
+43		6.3	7.8
M		6.9	7.2
+25'		7.8	6.3
	26+00		
-25'		6.5	7.6
-12		5.7	8.4
M		6.2	7.9
+7		5.7	8.4
+20		6.3	7.8
+25		5.1	9.0
+36		4.5	9.6
L		5.3	8.8
+10		5.2	8.9
+16		3.6	10.5
+41		3.7	10.4
E		3.4	10.7
+25		2.4	11.7
	26+39.17 = P.O.T.		
-24		1.4	12.7
E		2.8	11.3
+5		3.1	11.0
+33		3.9	10.2
+36		4.8	9.3

14.05

£ on Hub:	5.27	8.78
+15	5.3	8.8
+22	5.2	8.9
+28	6.3	7.9
W	6.7	7.4
+8	6.7	7.4
+25	7.0	7.1
27+00		
-25	7.1	7.0
-10	6.6	7.5
W	6.1	8.0
+10	5.6	8.5
+21	6.2	7.9
+35	4.8	9.3
+37	5.5	8.6
£	5.2	8.9
+13	5.0	9.1
+16	3.5	10.6
+54	2.9	11.2
+40	1.7	12.4
£	1.7	12.4
+25	1.7	12.4
28+00		
-15	0.7	13.4
£	2.2	11.9
+5	2.7	11.4

14.05

+25	2.3	11.8	10	
+33	2.7	11.4		
+38	4.8	9.3		
+43	5.8	8.3		
£	5.4	8.7		
+14	5.5	8.6		
+16	4.1	10.0		
+24	4.7	9.4		
+28	5.5	8.6		
+45	4.9	9.2		
W	5.2	8.9		
+25	6.3	7.8		
29+00				
-25	5.3	8.8		
-10	4.8	9.3		
W	4.3	9.8		
+10	3.9	10.2		
+24	4.6	9.5		
+35	2.6	11.5		
+40	5.7	8.4		
£	5.5	8.6		
+8	5.6	8.5		
+19	2.3	11.8		
£	1.8	12.3		
+25	+0.3	14.4		
T.P.	4.18	16.09	2.14	11.91

16.09

30+00

E-25	1.1	15.0
E	2.8	13.3
+33	3.5	12.6
+40	7.4	8.7
L	7.7	8.4
+10	7.7	8.4
+16	3.9	12.2
+30	6.0	10.1
W	5.5	10.6
+10	5.8	10.3

31+00

-25	7.0	9.1
W	6.1	10.0
+10	5.7	10.4
+20	6.0	10.1
+31	4.3	11.8
+35	4.7	11.4
+40	8.6	7.5
L	7.9	8.2
+6	8.4	7.7
+13	7.0	9.1
+20	3.5	12.6
E	2.8	13.3
+10	1.7	14.4

16.09

32+00

-10	3.0	13.1
E	4.7	11.4
+10	5.4	10.7
+33	4.8	11.3
+36	7.4	8.7
+44	8.5	7.6
L	7.9	8.2
+10	8.6	7.5
+15	5.0	11.1
+30	7.7	8.4
W	7.2	8.9
+25	8.4	7.7

33+00

-25	10.3	5.8
W	9.3	6.8
+20	9.7	6.4
+28	8.4	7.7
+35	7.9	8.2
+40	9.2	6.9
L	8.2	7.9
+6	8.8	7.3
+16	6.2	9.9
+38	7.0	9.1
E	6.3	9.8
+10	3.9	12.2

11

E			6.0	5.8
+7			7.5	4.3
+21			7.4	4.4
+35			7.8	4.0
+42			4.5	7.3
6 on Hub. PQT.			4.58	7.23
+7			5.2	6.6
+28			10.3	1.5
11			11.4	0.4
+10			11.4	0.4
TP	4.15	10.79	5.17	6.64 ^v
TP	4.42	10.63	4.58	6.21 ^v
TP	4.42	10.75	4.30	6.33 ^v
TP	4.81	10.72	4.84	5.91 ^v
TP	4.61	10.36	4.97	5.75 ^v
TP	4.67	10.33	4.70	5.66 ^v
TP	4.08	9.53	4.88	5.45 ^v
TP	7.29	12.29	4.53	5.00 ^v
TP	3.70	15.75	0.2A	12.05 ^v
Con Man. inside Santa Fe St. of Hwy 314 BR Jille Ho + Caspello Blvd.			4.30	11.45 ^v
TP	2.82	14.27	4.30	11.45 ^v
TP	5.30	13.48	6.09	8.18 ^v
TP	4.99	15.03	3.44	10.04 ^v
TP	1.83	12.27	4.59	10.44 ^v
TP	3.30	5.11	10.46	1.81 ^v
TP	3.57	2.32	6.36	-1.25 ^v

Note this line levels Cont Book 1985-21

				36+36			
				2.33		8.77	6.44
				-15			9.4
				11			-0.6
				+30			8.5
				+46			+0.3
				2			7.6
				+8			1.2
				+16			2.2
				E			6.6
				+10			1.7
							7.1
				-10			2.5
				2-5			6.3
				E			5.5
				2			3.8
				11			6.8
				+15			2.0
							36+41
				-15			1.8
				2-5			7.0
				E			2.3
				2			6.5
				11			4.9
				+15			4.4
							6.1
				-15			2.7
				11			8.8
				2			0.0
				E			9.8
				11			-1.0
				2			36+49
				-15			9.8
				11			-1.0
				2			9.9
				E			-1.1
				11			6.1
				+15			+2.7
				2			4.4
				-15			4.4
				11			2.1
				2			6.7
				+10			1.9
							6.9

EM on Com Mark
55' x 35' x 10
on P-12

29.57
11.5

36+52

-10	2.1	6.7
-5	3.9	4.9
E	4.1	4.7
+33	5.7	3.1
+41	2.3	6.5
2	2.9	5.9
+5	2.5	6.3
+17	7.3	1.5
Y	8.8	9.0
+15	9.8	-1.0

37+00

-15	9.0	-0.2
Y	9.1	-0.3
+20	8.7	10.1
+38	7.8	1.0
+44	2.8	6.0
2	2.0	6.8
+13	2.0	6.8
+20	5.1	3.7
E	1.0	4.8
+5	3.4	5.4
+10	0.8	8.0

37+50

-10	2.6	6.2
E	4.2	4.6

+28	4.7	4.1
+35	2.2	6.6
+44	1.8	7.0
2	2.3	6.5
+5	3.0	5.8
+15	6.9	1.9
+35	8.3	0.5
Y	8.2	0.6
+15	9.2	-0.4
+20	10.8	-2.0

38+00

-15	11.5	-2.7
Y	11.3	-2.5
+1	9.1	-0.3
+15	8.8	0.0
+42	6.5	2.3
2	2.8	6.0
+10	1.9	6.9
+20	2.2	6.6
+25	4.6	4.2
E	3.8	5.0
+10	2.5	6.3

38+50

-10	+1.8	10.6
-6	+0.9	9.7
E	3.7	5.1

+21		4.2	4.6
+27		2.3	6.5
+35		2.0	6.8
+44		3.0	5.8
L		6.3	2.5
+10		8.3	0.5
+30		5.6	-0.8
+32		11.1	-2.3
M		11.2	-2.4
+15		11.6	-2.8
	39+00		
-15		13.2	-4.4
M		11.8	-3.0
+25'		11.3	-2.5
+33		9.3	-0.5
L		7.5	+1.3
+12		2.8	+6.0
+20		2.1	+6.7
+32		2.4	+6.4
+37		3.7	+5.1
E		3.2	+5.6
+10		1.9	7.4
	39+50		
-10		1.7	7.1
E		2.8	6.0

+23		2.3	6.4
+33		3.6	5.2
+42		8.2	0.6
L		9.2	-0.4
+13		11.2	-2.4
+40		11.4	-2.6
M		12.6	-3.8
+15		13.3	-4.5
	40+00		
-15		13.3	-4.5
M		12.3	-3.5
+23		10.9	-2.1
L		10.7	-1.9
+15		8.8	0.0
+26		3.3	+5.5
+35		2.5	6.3
E		2.4	6.4
+10		1.5	7.3
	40+50		
-10		3.5	5.3
-5		3.6	5.2
E		2.7	6.1
+10		2.6	6.2
+17		3.2	5.6
+25		7.1	1.7
L		9.8	-1.0

M		12.6	-3.8
+15		13.0	-4.2
	41+00		
-15		13.3	-4.5
M		12.9	-4.1
L		10.0	-1.2
+20		9.8	-1.0
+33		6.6	+2.2
+41		3.9	5.4
E		2.6	6.2
+10		2.9	5.9
	41+50		
-10		2.8	6.0
E		3.4	5.4
+05'		5.5	3.3
+18'		5.6	3.2
+20'		10.0	-1.2
L		12.3	-3.5
+20		13.9	-5.1
M		14.1	-5.3
+15		14.1	-5.3
	42+00		
-15'		14.9	-6.1
M		14.9	-6.1
E		13.7	-4.9
+37		10.0	-1.2

+40		4.9	+3.9	
E		4.4	4.4	
+5		4.1	4.7	
+10		3.2	5.6	
	42+50			
-15		4.0	4.8	
E-10		6.7	2.1	
E		5.7	3.1	
+2		9.6	-0.8	
+9		11.4	-2.6	
+40		13.8	-5.0	
L		14.3	-5.5	
M		15.3	-6.5	
+15		15.2	-6.4	
	43+00			
-15'		15.4	-6.6	
M		15.4	-6.6	
L		15.6	-6.8	
+25		13.5	-4.7	
E		11.6	-2.8	
+10		10.8	-2.0	
+20		6.1	+2.7	
T.P	5.27	1.17	13.87	-4.10
	44+00			
-20		4.0	-2.8	
E		5.2	-4.0	

+15		6.7	-5.5
L		7.0	-5.8
M		7.8	-6.6
+20		7.9	-6.7
	45+00		
-20		8.0	-6.8
M		8.0	-6.8
L		7.3	-6.1
E		6.3	-5.1
+20		5.1	-3.9
	46+00		
-20		7.3	-6.0
E		7.3	-6.1
L		7.6	-6.4
M		8.0	-6.8
+20		8.1	-6.9
	47+00		
-20		8.2	-7.0
M		8.2	-7.0
L		7.9	-6.7
E		7.6	-6.4
+20		7.4	-6.2
	48+00		
-20		7.5	-6.3
E		7.8	-6.6
L		8.1	-6.9

M		8.3	-7.1
+20		8.3	-7.1
	48+59.21 = E.C.		
-20		8.3	-7.1
M		8.3	-7.1
L		8.1	-6.9
E		7.6	-6.4
+20		7.5	-6.3
	49+00		
-20		7.7	-6.5
E		8.0	-6.8
L		8.1	-6.9
M		8.2	-7.0
+20		8.3	-7.1
	50+00		
-20		8.3	-7.1
M		8.2	-7.0
L		8.2	-7.0
E		7.9	-6.7
+20		7.7	-6.5
	51+00		
-20		7.7	-6.5
E		7.8	-6.6
L		8.3	-7.1
M		8.3	-7.1
+20		8.4	-7.2

52+00

20			8.4	-7.2
N			8.3	-7.1
S			8.3	-7.1
E			7.9	-6.7
+20'			7.7	-6.5
T.P.	4.71	-0.26	6.14	-4.97

53+00

-20			6.4	-6.7
E			6.4	-6.7
S			6.5	-6.8
N			6.8	-7.1
+20			7.0	-7.3

54+00

-20			7.1	-7.4
N			7.1	-7.4
S			6.9	-7.2
E			6.7	-7.0
+20			6.5	-6.8

55+00

-20			7.0	-7.3
N			7.0	-7.3
S			6.7	-7.0
E			6.7	-7.0
+20			6.7	-7.0

56+00

-20'			6.4	-6.7
E			6.5	-6.8
S			6.7	-7.0
N			7.0	-7.3
+20			7.1	-7.4

57+00

-20'			7.0	-7.3
N			6.8	-7.1
S			6.6	-6.9
E			6.5	-6.8
+20			6.4	-6.7

58+00

-20			6.3	-6.6
E			6.3	-6.6
S			6.4	-6.7
N			6.5	-6.8
+20			6.7	-7.0

59+00

-20			6.8	-7.1
N			6.6	-6.9
S			6.4	-6.7
E			6.3	-6.6
+20			6.4	-6.7

32
59+65.84 = BC. RA

-20			6.1	-6.4
E			6.1	-6.4

L			6.3	-6.7
W			6.6	-6.9
+20'			6.7	-7.0
T.P	3.41	0.41	2.74	-3.00
T.P	3.92	1.00	3.33	-2.92
	60+00			
-20'			7.7	-6.7
W			7.7	-6.7
L			7.5	-6.5
E			7.3	-6.3
+20'			7.3	-6.3
	61+00			
-20'			6.5	-5.5
E			6.8	-5.8
L			7.5	-6.5
W			7.8	-6.8
+20'			7.9	-6.9
	62+00			
-20'			7.6	-6.6
W			7.5	-6.5
L			7.3	-6.3
E			7.0	-6.0
+20'			6.9	-5.9
	63+00			
-20'			6.9	-5.9
E			7.0	-6.0

on both on Bench
150 ft Lon 2'x2' plate
-A.M.H. tide 6.1100

L			7.2	-6.2
W			7.5	-6.5
+20'			7.7	-6.7
	64+00			
-20'			7.6	-6.6
W			7.5	-6.5
L			7.2	-6.2
E			6.7	-5.7
+20'			6.5	-5.5
	65+00			
-20'			7.5	-6.5
W			7.4	-6.4
L			7.1	-6.1
E			6.7	-5.7
+20'			6.5	-5.5
	66+00			
-20'			6.4	-5.4
E			6.6	-5.6
L			7.1	-6.1
W			7.4	-6.4
+20'			7.5	-6.5
	67+00			
-20'			7.4	-6.4
W			7.3	-6.3
L			6.9	-5.9
E			5.8	-4.8

+20		4.9	-3.9
	68+00		
-20'		4.3	-3.3
E		5.5	-4.5
L		6.8	-5.8
M		7.2	-6.2
+20		7.4	-6.4
	69+00		
-20'		7.3	-6.3
M		7.2	-6.2
L		6.7	-5.7
E		5.1	-4.1
+12		4.3	-3.3
+16		+1.9	+2.9
+10		+2.3	+3.3
	69+50		
-20		+2.4	+3.4
-11		+2.4	+3.4
-7		4.2	-3.2
E		4.7	-3.7
L		6.6	-5.6
M ₂₀		6.9	-5.9
	70+00	7.3	-6.3
-20		7.0	-6.0
M		6.6	-5.6
L			

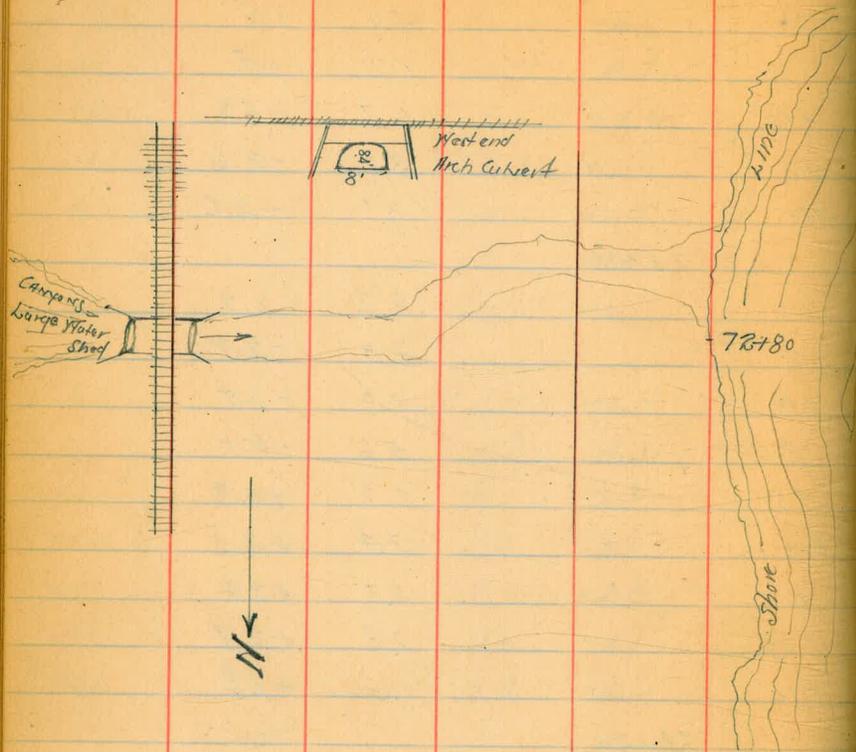
+40		4.2	-3.2
+45		+2.9	+3.9
E		+2.7	+3.7
+20		+2.7	+3.7
	70+50		
-20'		+2.6	+3.6
E		+2.6	+3.6
+20		+2.6	+3.6
+25		3.8	-2.8
L		5.4	-4.4
M		6.4	-5.4
+20		6.6	-5.6
TP	8.40	5.48	3.92
	71+00		
-20		10.7	-5.2
M		10.6	-5.1
L		8.6	-3.1
+5		2.6	+2.9
E		1.4	+3.1
+20		+1.0	+6.5
	71+10		
-20		+1.0	+6.5
E		1.3	+4.2
L		2.6	+2.9
+5		3.8	-3.3
M		10.3	-4.8

+20		10.5	-5.0
	71+50		
-20		10.3	-4.8
N		10.2	-4.7
+40		7.7	-2.2
+45		2.9	+2.6
L		2.6	+2.9
E		1.0	+4.5
+20		+1.2	+6.7
	72+100		
-20'		+1.0	+6.5
E		1.2	4.3
L		3.2	2.3
+10		3.5	2.0
+5		8.0	-2.5
N		9.6	-4.1
+20		9.7	-4.2
	72+150		
-20		9.0	-3.5
N		9.0	-3.5
+40		7.0	-1.5
+45		3.8	+1.7
L		3.7	+1.8
E		1.6	+3.9
+20		0.2	+5.3
	72+75		

-20		1.7	+3.8
E		2.1	3.4
L		4.0	1.5
+5		4.0	1.5
+10		6.7	-1.2
N		8.1	-2.6
+20		8.1	-2.6
	73+0.0		
-20'		8.2	-2.7
N		8.3	-2.8
+30		7.0	-1.5
L		5.6	-0.1
+5		5.2	+0.3
+10		3.4	+2.1
E		2.1	+3.4
+25		2.8	+2.7
+30		7.3	-1.8
	73+20		
-30		1.1	+4.4
-10		1.9	+3.6
-8		7.4	-1.9
E		7.4	-1.9
+10		7.4	-1.9
+20		5.6	-0.1
L		7.8	-2.3
N		7.8	-2.3

+20

8.3



73+35

-20	8.8	-3.3
M	8.4	-2.9
+35	7.6	-2.1
L	6.3	-0.8
+5	7.6	-2.1
+25	3.4	+2.1
E	2.1	+3.4

73+20

0.5 +5.0

22

73+50

-20	0.6	+4.9
E	2.7	+2.8
+20	3.7	+1.8
L	3.7	+1.8
+5	5.9	-0.4
+20	6.6	-1.1
+30	7.6	-2.1
M	8.7	-3.2
+20	9.0	+3.5

74+00

-20	9.6	-4.1
M	8.4	-2.9
+13	7.9	-2.4
+15	8.5	-3.0
L	7.1	-1.6
+5	4.8	+0.7
E	3.4	+2.1
+20	2.8	+2.7

74+50

-20	3.4	+2.1
E	4.3	+1.2
+38	5.5	0.0
+40	7.1	-1.6
L	8.0	-2.5

+13		8.4	-2.9
+15		7.9	-2.4
$\frac{1}{2}$		10.1	-4.6
+20		10.4	-4.9
	75+00		
-20		11.1	-5.6
$\frac{1}{2}$		11.1	-5.6
$\frac{1}{2}$		8.2	-2.7
+15		7.6	-2.1
+20		5.7	-0.2
E_0		4.7	+0.8
+20		3.9	+1.6
	75+50		
-20		4.9	+0.6
E_0		5.7	-0.2
+20		6.3	-0.8
+25		7.6	-2.1
$\frac{1}{2}$		9.3	-3.8
+10		10.4	-4.9
$\frac{1}{2}$		11.2	-5.7
+20		10.9	-5.4
	76+00		
-20		11.5	-6.0
$\frac{1}{2}$		11.3	-5.8
$\frac{1}{2}$		10.3	-4.8
+10		9.8	-4.3

+40		7.0	-1.5
E_0		6.0	-0.5
+20		5.5	-0.0
	77+00		
-20		6.0	-0.5
E_0		8.0	-2.5
+25		9.8	-4.3
$\frac{1}{2}$		11.2	-5.7
$\frac{1}{2}$		11.4	-5.9
+20		11.5	-6.0
	77+41.5 = E.C. = 78+44.0		
-20		11.1	-5.6
$\frac{1}{2}$		11.1	-5.6
$\frac{1}{2}$ on Hub.		10.81	-5.33
+30		10.3	-4.8
E_0		9.1	-3.6
+20		6.8	-1.3
T.P.	3.81	3.55	6.74 -1.26
	79+00		
-20		5.1	-2.4
E_0		6.8	-4.2
$\frac{1}{2}$		8.3	-5.7
$\frac{1}{2}$		8.6	-6.0
+20		8.7	-6.1
	80+00		
-20		8.7	-6.1

255

YI		85	-5.9
g		7.8	-5.2
E		7.0	-4.4
+10		6.7	-4.1
+20		5.4	-2.8
	81+00		
-20		6.4	-3.8
E		7.4	-4.8
g		7.5	-4.9
YI		8.4	-5.8
+20		8.4	-5.8
	82+00		
-20		8.4	-5.8
YI		8.0	-5.4
g		7.3	-4.7
E		6.8	-4.2
+20		6.7	-4.1
	83+00 - POT		
-20		5.6	-3.0
E		5.9	-3.3
g on Hdb.		6.67	-3.12
YI		7.8	-5.2
+20		8.1	-5.5
	84+00		
-20		8.2	-5.6
YI		7.9	-5.3

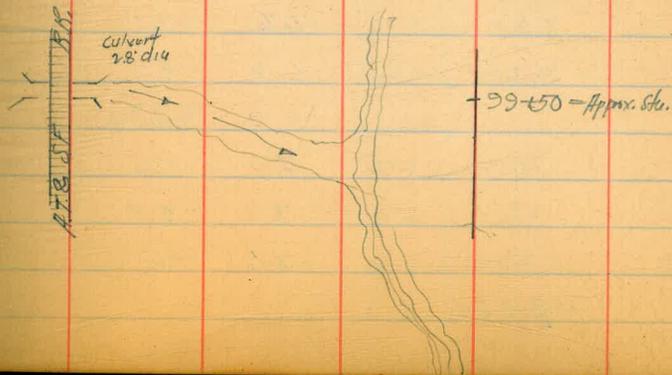
255

24

g			7.2	-4.6
E			6.6	-4.0
+20			6.4	-3.8
	85+00			
-20			7.5	-4.9
E			7.6	-5.0
g			8.0	-5.4
YI			8.9	-6.3
+20			8.9	-6.3
	86+00			
-20			9.1	-6.5
YI			9.0	-6.4
g			8.7	-6.1
E			8.4	-5.8
+20			8.4	-5.8
TP	4.10	0.20	6.45	-3.90
	87+00			
-20			6.4	-6.2
E			6.5	-6.3
g			6.5	-6.3
YI			6.8	-6.6
+20			6.7	-6.5
	88+00			
-20			6.7	-6.5
YI			6.7	-6.5
g			6.5	-6.5

E		6.2	-6.0
+20		6.2	-6.0
	89+00		
-20		6.2	-6.0
E		6.3	-6.1
L		6.5	-6.3
W		6.8	-6.6
+20		6.9	-6.7
	90+00		
-20		6.8	-6.6
W		6.8	-6.6
L		6.5	-6.3
E		6.3	-6.1
+20		6.2	-6.0
	91+00		
-20		6.2	-6.0
E		6.3	-6.1
L		6.5	-6.3
W		6.7	-6.5
+20		6.8	-6.6
	92+00		
-20		6.8	-6.6
W		6.8	-6.6
L		6.5	-6.3
E		6.3	-6.1
+20		6.2	-6.0

	95+00		
-20			6.4 -6.2
E			6.6 -6.4
L			6.8 -6.6
W			6.9 -6.7
T.P.	5.22	0.58	4.84 -4.64
	98+00		
-20			7.1 -6.5
W			7.0 -6.4
L			6.8 -6.2
E			6.8 -6.2
+20			6.5 -5.9
	101+00		
-20			6.6 -6.0
E			6.7 -6.1
L			7.0 -6.4
W			7.1 -6.5
+20			7.3 -6.7



-20	104+00		6.9	-6.3
N			6.9	-6.3
E			6.7	-6.1
E			6.0	-5.4
+20			4.9	-4.3
T.P	5.04	2.10	3.52	-2.94
	104+00			
-20			7.0	-4.9
E			7.6	-5.5
L			8.0	-5.9
N			8.3	-6.2
+20			8.5	-6.4
	106+00			
-20			8.5	-6.4
N			8.5	-6.4
E			8.2	-6.1
+40			7.7	-5.6
E			6.7	-4.6
+20			5.9	-3.8
	107+00			
-20			5.6	-3.5
-10			6.6	-4.5
E			6.9	-4.8
E			7.7	-5.6
N			8.0	-5.9
+20			8.1	-6.0
	108+00			

-20				7.9	-5.8
N				7.7	-5.6
E				7.5	-5.4
+30				7.0	-4.9
E				5.6	-3.5
+20				4.6	-2.5
	109+00				
-20				4.5	-2.4
E				4.9	-2.8
+10				5.7	-3.6
E				7.3	-5.2
N				7.8	-5.7
+20				8.1	-6.0
T.P	1.33	3.15	0.28	1.82	
	110+00				
-20				9.7	-6.5
N				9.5	-6.3
E				8.2	-5.0
+30				7.0	-3.8
E				5.5	-2.3
+20				5.7	-2.5
	111+00				
-20				5.0	-1.8
E				5.2	-2.0
+15				4.6	-1.4
+20				6.6	-3.4

on Proj Co South
Kennedy's
on old RR. Def.

315

+50	7.5	-4.3
L	8.4	-5.2
M	9.2	-6.0
+20	9.3	-6.1
111+64.34=PC.		
-20	9.3	-6.1
M	9.3	-6.1
Lo on Hub	8.19	-5.04
+25	6.4	-3.2
+30	5.4	-2.2
E	5.1	-1.9
+20	4.5	-1.3
112+00		
E-20	4.9	-1.7
E	5.2	-2.0
+22	5.5	-2.3
+25	6.6	-3.4
L	8.0	-4.8
M	9.6	-6.4
+20	9.6	-6.4
112+50		
-20	8.5	-5.2
M	8.5	-5.2
L	8.0	-4.8
+20	6.6	-3.4
+30	5.8	-2.6

315

27

E	6.0	-2.8
+20	5.5	-2.3
113+00		
-20	5.7	-2.5
E	6.0	-2.8
+35	5.9	-2.7
L	8.3	-5.1
+15	8.8	-5.6
+18	8.1	-4.9
M	8.2	-5.0
+20	8.6	-5.4
113+50		
-20	7.8	-4.6
M	7.2	-4.0
+10	7.0	-3.8
+12	5.9	-2.7
+30	6.0	-2.8
+35	6.9	-3.7
+40	8.7	-5.5
L	8.7	-5.5
+5	6.4	-3.2
E	5.9	-2.7
+20	5.5	-2.3
114+00		
-20	5.5	-2.3
E	5.8	-2.6

+28		5.7	-2.5
+35		8.4	-5.2
+45		9.2	-6.0
2		6.6	-3.4
+25		5.8	-2.6
11		5.8	-2.6
+20		7.0	-3.8
	114+50		
-20		6.0	-2.8
11		6.1	-2.9
+30		6.0	-2.8
+35		9.0	-5.8
2		8.8	-5.6
+5		6.0	-2.8
5		5.6	-2.4
+20		5.4	-2.2
	115+00		
-20		5.8	-2.6
5		5.8	-2.6
+35		5.9	-2.7
+40		9.3	-6.1
2		9.3	-6.1
+7		9.3	-6.1
+10		6.2	-3.0
11		5.7	-2.5
+20		7.0	-3.8

	115+25		
-20		5.7	-2.5
11		5.7	-2.5
+30		6.0	-2.8
+35		8.1	-4.9
+40		5.9	-2.7
2		5.5	-2.3
+20		5.8	-2.6
+25		9.0	-5.8
+35		8.7	-5.5
+40		6.1	-2.9
5		5.4	-2.2
+20		5.7	-2.5
	115+50		
-20		5.5	-2.3
5		6.5	-3.3
+1		7.9	-4.7
+15		9.3	-6.1
+20		5.4	-2.2
5		5.4	-2.2
+5		5.7	-2.5
+10		8.3	-5.1
+15		8.3	-5.1
+20		5.7	-2.5
11		5.7	-2.5
+20		6.0	-2.8

116+00

-20		5.9	-2.7
W		5.9	-2.7
Z		5.5	-2.3
+43		5.9	-2.7
+46		7.5	-4.2
E		5.8	-2.6
+20		5.3	-2.1
+75		5.0	-1.8
+80		8.2	-5.0
+90		8.2	-5.0
+95		5.0	-1.8

T.P. 840 5.78[✓] 5.77 -2.62 on P.I. Hub.

chk. on L. Hub 121+68.4 - FC. Book 1379-22 7.19

1.41
 1.43 = Hub
 0.02 = Error

Cont. in Book 1379-21

13.17

F		3.8	94
+30		3.6	96
	1292+0		
-20		3.6	96
F		3.7	95
$\frac{1}{2}$		4.1	91
H		4.4	88
+20		2.1	11.1
	1292+50		
-20		4.1	91
H		4.0	92
$\frac{1}{2}$		3.5	97
F		3.6	96
+20		3.6	96
	1293+0		
-20		3.7	95
F		3.9	93
$\frac{1}{2}$		3.7	95
H		3.8	94
+20		3.9	93
	1293+50		
-20		4.4	89
H		4.2	90
$\frac{1}{2}$		4.0	92
F		3.8	94
+20		3.9	93

13.17

31

	1294+0		
-20		3.8	94
F		3.9	93
$\frac{1}{2}$		4.2	90
H		4.2	90
+20		4.3	89
	1294+50		
-20		4.2	90
H		4.0	92
$\frac{1}{2}$		4.2	90
F		4.0	92
+20		4.0	92
	1295+0		
-20		3.9	93
F		3.9	93
$\frac{1}{2}$		4.2	90
H		4.2	90
+20		4.2	90
TP	4.67	13.00	4.34
	1295+50		8.93
-20		4.3	87
H		4.1	89
$\frac{1}{2}$		4.1	89
F		4.0	90
+20		3.7	93
	1296+0		

Top of MH
 1297-95

1300

-20		4.0	90
F		3.9	91
L		4.4	86
H		4.2	88
+20		4.3	87
	✓ 296+50		
-20		4.4	86
H		4.5	85
L		4.2	88
F		4.1	89
+20		4.0	90
	✓ 297+0		
-20		4.2	88
F		4.3	87
L		4.1	89
H		4.5	85
+20		4.4	86
	✓ 297+50		
-20		4.5	85
H		4.2	87
L		4.4	86
F		4.7	83
+20		4.1	89
	✓ 298+0		
-20		4.2	87
F		4.7	83

1300

32/230

L		4.5	85
H		4.7	83
+20		4.7	83
	✓ 298+50		
-20		4.8	82
H		4.7	83
L		4.7	83
F		4.5	85
+20		4.5	85
	✓ 299+0		
-20		4.5	85
F		4.4	86
L		4.3	87
H		4.5	85
+20		4.7	83
	✓ 299+4+23: FC		
-20		4.8	82
H		4.6	84
L		4.8	82
F		4.4	86
+20		4.4	86
	✓ 300+0		
-20		4.6	84
F		4.8	82
L		4.8	82
H		4.7	83

13.00

+20		5.0	80
	↓ 30170		
-20		4.8	82
H		4.8	82
L		4.7	83
F		4.3	87
+20		4.6	84
	↓ 30210		
-20		4.5	85
F		4.5	85
L		5.1	79
H		5.0	80
+20		5.0	80
	↓ 30370		
-20		4.6	84
H		4.4	86
L		4.5	85
F		4.8	82
+20		4.8	82
	↓ 30410		
-20		4.5	85
F		4.5	85
L		4.6	84
H		4.5	85
+20		4.5	85
	↓ 30570		

13.00

33

-20		5.0	80
H		5.0	80
L		4.6	84
F		4.8	82
+20		4.6	84
	↓ 30610		
-20		4.5	85
F		5.0	80
L		4.6	84
H		4.8	82
+20		5.2	78
TP	4.6	12.88	4.72
	↓ 30710		8.28
-20		5.3	86
H		5.0	89
L		4.6	83
F		4.7	82
+20		4.6	83
	↓ 30810		
-20		4.4	85
F		5.0	79
L		5.2	77
H		5.3	76
+20		5.3	76
	↓ 30910		
-20		5.4	75

12.88

H	47	82
L	52	77
F	48	81
120	47	82
1310+		
-20	48	81
F	51	78
L	51	78
H	55	74
120	54	75
1311+		
-20	52	77
H	52	77
L	46	83
F	49	80
120	47	82
1312+		
-20	45	84
F	45	84
L	43	86
H	46	83
+20	49	80
1313+		
-20	45	84
H	40	89
L	37	92

12.88

34

F	3.9	90
120	41	88
1314+		
-20	27	102
F	2.6	103
L	3.1	98
H	3.2	97
120	3.3	96
1315+		
-20	3.0	99
H	3.9	100
L	2.6	103
F	2.1	108
120	2.0	109
1315+56.25 P.S.T. = 2 Quince		
-20	1.7	112
F	2.0	109
L	2.5	104
H	2.6	103
120	2.6	103
TP	2.53	1035
3/16+0 See 1379 Page 67		

on 8 Feb
315+56.25 P.S.T.

HST Cross Section
California to Belt

80' wide
11' cb
3' 0"

5' Top of
Atlantic

35 4830
5000
50 B111
North
05607

BM 3.18 10.29 ✓

W.L. California

Belt

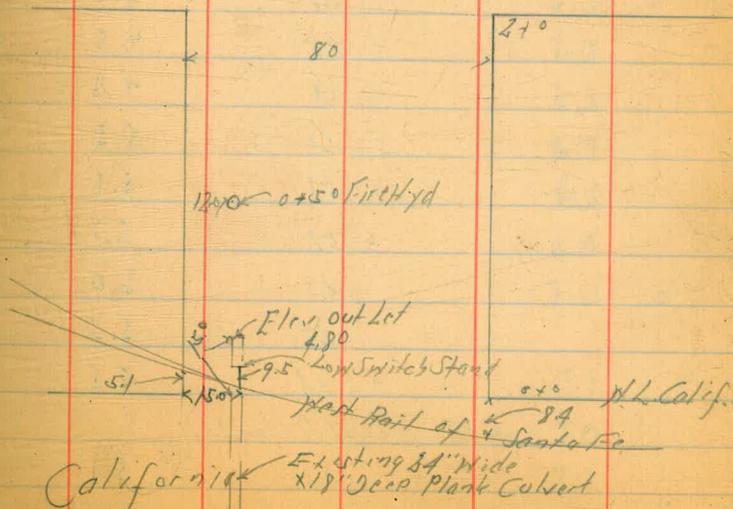
N	Top of 1st Rail	1.60	8.69
N	8.4' E of W.L.	2.1	8.2
cb		2.2	8.1
1/4		2.1	8.2
1/2		1.8	8.5
+10	Top of 1st Rail	1.95	8.34
1/4		2.1	7.9
cb		2.5	7.8
S		2.6	7.7
	Top 1st Rail	2.16	8.13

50' W of W.L. Calif

Atlantic

S		3.5	6.8
cb		3.7	6.6
1/4		3.9	6.4
1/2		5.7	4.6
1/4		5.7	4.6
1/2		3.8	6.5
1/4		2.5	6.8
1/2		2.5	6.8
1/4		3.3	7.0
cb		3.1	7.2
N		2.6	7.7

100' W



California Existing 84" wide x 12" Deep Plank Culvert

ASL	1029		
N	5.9	6.4	
cb	5.6	6.7	
1/4	4.5	5.8	
1/2	4.4	5.9	
1/4	4.6	5.7	
1/7	4.7	5.6	
1/8	5.8	4.5	
1/10	5.8	4.5	
1/11	4.0	6.3	
cb	3.7	6.6	
S	5.3	5.0	
150' N			
S	5.2	5.1	
cb	4.4	5.9	
1/4	4.7	5.6	
1/5	5.8	4.5	
1/6	5.8	4.5	
1/7	5.0	5.3	
1/4	5.2	5.1	
1/2	5.2	5.1	
1/4	4.3	6.0	
cb	4.8	5.5	
N	4.8	5.5	
200' N - E. of Atlantic			
N	5.2	5.1	
cb	5.0	5.3	

	1029		
1/4	5.2	5.1	
1/2	5.3	5.0	
1/4	5.4	4.9	
cb	5.9	4.4	
S	5.6	4.7	
W. of Atlantic			
S	4.0	6.3	
cb	4.6	5.7	
1/4	4.3	6.0	
1/2	4.8	5.5	
1/4	4.4	5.9	
cb	4.6	5.7	
N	4.6	5.7	
50' N of W. of Atlantic			
N	3.8	6.5	✓
cb	3.8	6.5	
1/4	3.8	6.5	
1/2	3.6	6.7	
1/4	3.8	6.5	
cb	3.9	6.4	
S	3.1	7.2	✓
100' N			
S	3.2	7.1	✓
cb	3.3	7.0	
1/4	3.0	7.3	
1/2	3.2	7.1	

1029

1/4	3.5	6.8	
cb	2.5	6.8	
H	3.6	6.7	✓

150' H

H	3.2	7.1	✓
cb	3.4	6.9	
1/4	3.1	7.2	
1/2	3.1	7.2	
1/4	3.0	7.3	
cb	3.3	7.0	
S	2.8	7.5	✓

200' H = East Line of Belt

S	2.9	7.4	✓
cb	2.8	7.5	
1/4	2.6	7.7	
1/2	2.3	8.0	
1/4	2.7	7.6	
cb	3.0	7.3	
H	3.0	7.3	✓

37

Asb St. Cross Section
California to Belt

80' wide
14' cbs
13' qts

38

BM 432 10.97 ✓

6.65 SE Top Hnd
Asb & Atlantic

11 1/2' California

5 cb Top	1.00	9.97
Gutter on Pavmg	2.29	8.68
1/4 " "	0.93	10.04
1/2 " "	0.69	10.28
1/4 " "	0.97	10.00
Gutter " "	1.70	9.27
11 cb Top	0.43	10.54

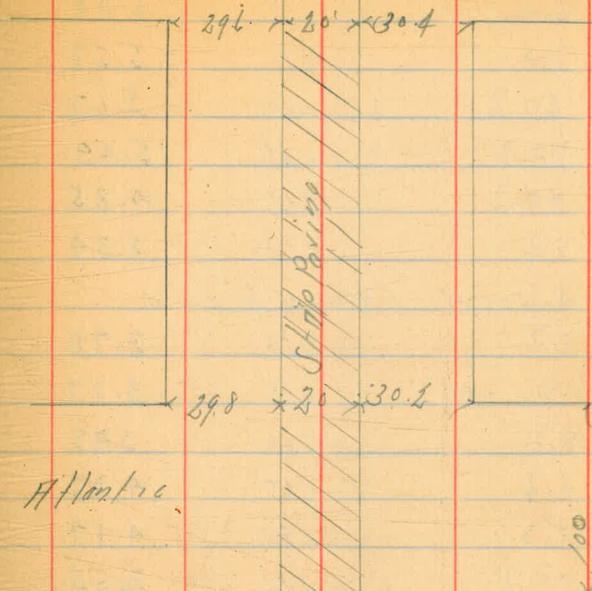
50' H

11 cb	2.18	8.85
Gutter on Pavmg	2.74	8.23
1/4 " "	2.47	8.50
1/2 " "	2.31	8.66
1/4 " "	2.48	8.49
Gutter " "	3.01	7.96
5 cb	2.53	8.44

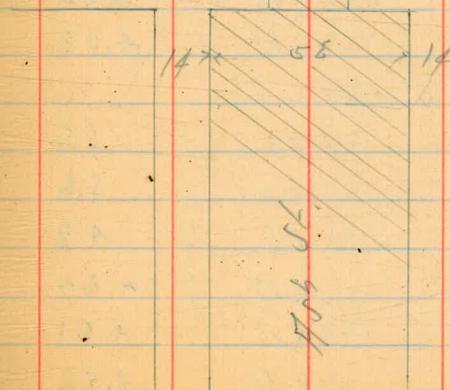
100' H

5 cb	4.09	6.88
Gutter on Pavmg	4.57	6.40
1/4 " "	4.03	6.94
1/2 " "	3.86	7.11
1/4 " "	3.97	7.00
Gutter " "	4.38	6.67
11 cb	3.74	7.23

Belt



Atlantic



California

150' W

H cb	5.84	5.63
Gutter on Pavings	5.91	5.08
1/4	5.40	5.57
1/2	5.30	5.67
1/4	5.48	5.49
Gutter	6.12	4.85
S cb	5.63	5.34

200' W - E Line of Atlantic

S cb	7.25	3.72
Gutter on Pavings	7.70	3.27
1/4	7.00	3.97
1/2	6.60	4.37
1/4	6.80	4.17
Gutter	7.46	3.55
H cb	6.94	4.03

W. Line of Atlantic

H	5.5	5.5
cb	5.4	5.6
1/4	6.2	4.8
1/3 - Edge Pavings	6.37	4.60
1/2	6.36	4.61
1/10 - Edge	6.45	4.52
1/4	6.5	4.5
cb	5.9	5.1
S	5.9	5.1

50' W of W. Atlantic

S	5.6	5.4
cb	5.5	6.5
1/4	6.2	4.8
1/3 - Edge Pavings	5.94	5.03
1/2	5.88	5.09
1/10 - Edge	5.88	5.09
1/4	5.8	5.2
cb	5.4	5.6
H	5.5	5.5

100' W

H	5.2	5.8
cb	5.8	5.8
1/4	5.3	5.7
1/3 - Edge Pavings	5.20	5.77
1/2	5.13	5.84
1/10 - Edge	5.16	5.81
1/4	5.5	5.5
cb	5.3	5.7
S	4.9	6.1

150' W

S	4.5	6.5
cb	4.3	6.7
1/4	4.7	6.3
1/3 - Edge Pavings	4.45	6.52
1/2	4.40	6.57

Asht

10.97

40

710 = Edge Pairing	4.45	6.52
74	4.7	6.3
06	4.6	6.4
74	4.5	6.5
20074 = E.L. of Bolt		
74	4.6	6.4
06	4.6	6.4
74	4.3	6.7
73 = Edge Pairing	4.08	6.89
74	4.00	6.97
710 = Edge	4.10	6.97
74	4.4	6.6
06	4.2	6.8
5	4.0	7.0

Beech St. Cross Section
California to Belt.

80' wide
11' cb
13' qtz

4-10-50

41

BM 7.92 15.39 7.47 SE Top Hyd
Beech Atlantic

H.L. California

S cb	3.80	11.59
Gutter on Paving	5.16	10.23
" " "	3.43	11.96
" " "	3.15	12.24
" " "	2.00	12.39
Gutter " "	4.30	11.09
H cb	2.90	12.49

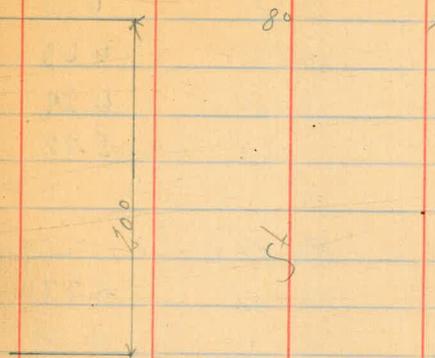
50' of H.L. Calif.

H cb	4.82	10.57
Gutter on Paving	5.62	9.77
" " "	5.15	10.24
" " "	5.31	10.18
" " "	5.61	9.78
Gutter " "	6.25	9.14
S cb	5.48	9.91

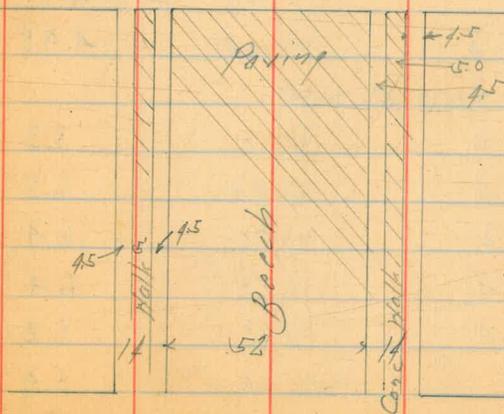
100' H

S cb	7.26	8.13
Gutter on Paving	7.97	7.42
" " "	7.25	8.14
" " "	6.97	6.742
" " "	6.98	8.41
Gutter " "	7.42	7.97
H cb	6.72	8.67

Belt



Atlantic



California

Beech St.

15.39

	150' H		
H cb		8.55	6.84
Gutter on Parings		9.21	6.18
1/4 " "		8.88	6.51
1/2 " "		8.76	6.63
1/4 " "		9.00	6.39
Gutter " "		9.67	5.72
S cb in Drive Way			

200' H = E.L. Atlantic = End Parings

S cb		10.62	4.77
Gutter on Parings		11.35	4.04
1/4 " "		10.71	4.68
1/2 " "		10.56	4.83
1/4 " "		10.56	4.83
Gutter " "		11.18	4.21
H cb		10.41	4.98

1/2 Atlantic

H		10.1	5.3
cb		8.9	6.5
1/4		9.0	6.4
1/2		9.0	6.4
1/4		9.2	6.2
cb		9.5	5.9
S		9.9	5.5

50' H of 1/2 Atlantic

S		9.3	6.1
---	--	-----	-----

15.39

42

cb		9.5	5.9
1/4		9.2	6.2
1/2		9.2	6.2
1/4		9.3	6.1
cb		9.4	6.0
H		9.6	5.8

100' H

H		9.2	6.2
cb		9.2	6.2
1/4		9.1	6.3
1/2		9.1	6.3
1/4		9.1	6.3
cb		8.9	6.5
S		8.6	6.8

150' H

S		9.0	6.4
cb		9.0	6.4
1/4		8.8	6.6
1/2		8.9	6.5
1/4		8.9	6.5
cb		9.1	6.3
H		9.2	6.2

200' H = E.L. Bell

H		9.2	6.2
cb		8.7	6.7
1/4		9.0	6.4

Beach St.

15.39

1/2
1/4
cb
s

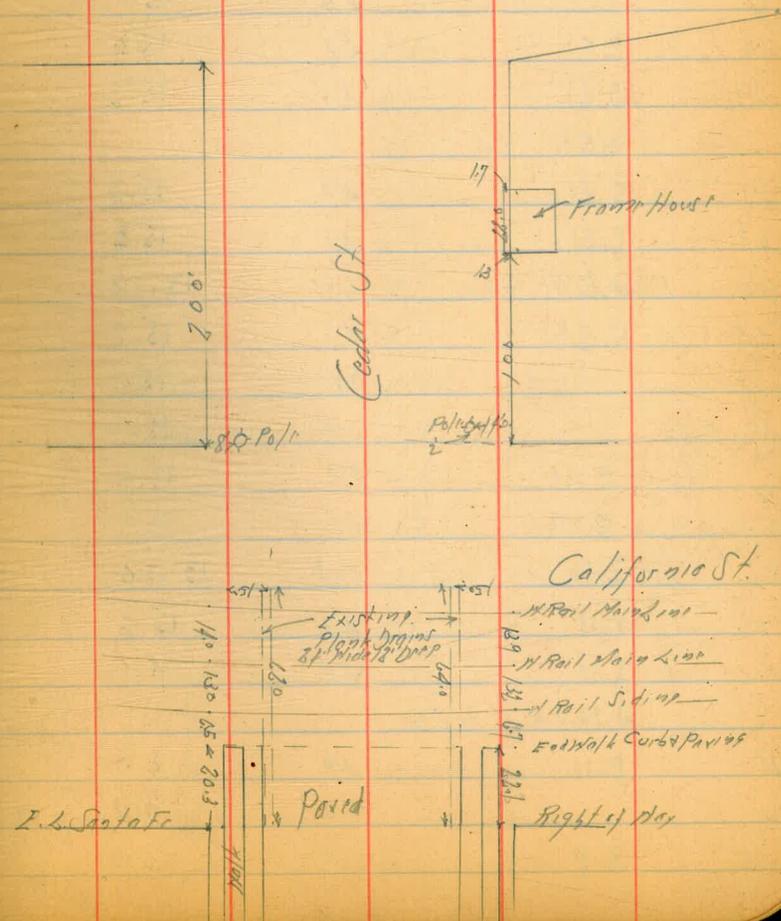
9.0
8.9
9.0
9.2

6.4
6.5
6.4
6.2

Cedar St. Cross Section
California to Atlantic

BM	11.55	19.28	7.73	SETOP H ₂ O Cedar St Atlantic
	E.L. Santa Fe Right of Way			
S cb		2.18	17.10	
Gutter on Paving		3.41	15.87	
1/4 " "		2.18	17.10	
1/2 " "		2.10	17.18	
1/4 " "		2.08	17.20	
Gutter " "		3.70	15.58	
H cb		2.02	17.26	
	22.1 H ₂ O E.L. 0.07 H 2.023 H ₂ O E.L. 0.07 S = End Paving Cbs & Walk			
H		3.3	16.0	
Cb + Paving		2.96	16.32	
1/4 on " "		2.96	16.32	
1/2 " "		2.96	16.32	
1/4 " "		2.99	16.29	
Cb + Paving		3.07	16.21	
S		3.3	16.0	
	50 ft of E.L.			
S Top Rail		3.34	15.94	
S		3.8	15.5	
Op		3.8	15.5	
1/4		3.3	16.0	
1/2 Top Rail + Dirt		3.23	16.05	
1/4 " " "		3.1	16.17	
Cb		3.1	15.7	

Atlantic



1928

H		3.6	15.7
H Top Rail		3.11	16.17
	64' W		
H		4.6	14.7
Cb		4.7	14.6
1/4		3.8	15.5
1/2		3.7	15.6
1/4		3.6	15.7
Cb		4.3	15.0
S		4.0	15.3
	65' W		
S		4.0	15.3
17		4.0	15.3
Cb - Flow Line Drain		6.10	13.18
15		4.1	15.2
1/2		3.6	15.7
1/2		3.7	15.6
1/2		3.9	15.4
1.4		4.1	15.2
Cb - Flow Line Drain		6.08	13.20
15		4.3	15.0
H		4.4	14.9
	75' W of EL		
H		4.9	14.4
Cb		6.0	13.3
15		6.3	13.0

1928

45

1/4		5.3	14.0
1/2		4.6	14.7
1/4		4.4	14.9
1.8		4.5	14.8
Cb		6.0	13.3
1.8		4.3	15.0
S		4.3	15.0
	100' W of EL = H.L. Calif.		
S		6.4	12.9
Cb		5.7	13.6
1/4		5.9	13.4
1/2		6.1	13.2
1/4		5.6	13.7
Cb		5.7	13.6
H		6.1	13.2
TP	5.15 12.88 ✓	11.55	7.73
	50' W of H.L. Calif.		
H		1.2	11.7
Cb		0.9	12.0
1/4		1.4	11.5
1/2		1.8	11.1
1/4		1.8	11.1
Cb		1.3	11.6
S		1.0	11.9
	90' W		
S		3.1	9.8

60' W - Concrete
0.9' S of H.L.

1.69

86' W - Concrete
1.3' S of H.L.

2.56

13.88

Cb	4.0	8.9	
1/4	4.0	8.9	91' W - Pale
2	3.2	9.7	115' of NL
1/4	3.1	9.8	
Cb	2.9	10.2	
11	2.8	10.1	
100' W			
11	4.1	8.8	
Cb	4.5	8.4	
1/4	4.6	8.3	
2	4.5	8.4	172' W - Bottom
1/4	4.3	8.6	175' of NL
Cb	4.5	8.4	547
S	3.6	9.3	
125' W			
S	4.5	8.4	128' W - Board
Cb	5.3	7.6	Walk
1/4	5.1	7.3	0.5' S of S.L.
2	5.7	7.2	427
1/4	6.3	6.6	137' W - 2
Cb	6.2	6.7	Garage Drift 17.1
11	5.9	7.0	0.5' S.L.
150' W			
11	6.4	6.5	1.70
Cb	6.7	6.2	
1/4	6.5	6.4	

13.88

46

2	6.7	6.2	
1/4	6.4	6.5	174' W - Pale
Cb	6.1	6.8	8' W of S.L.
S	5.3	7.6	167' W - Bottom
S on Board Walk	4.65	8.23	0.5' S.L.
175' W			
S	6.5	6.4	
Cb	6.3	6.6	
1/4	6.8	6.1	192' W - Pale
2	7.0	5.9	13' S of NL
1/4	6.8	6.1	
Cb	6.8	6.1	
11	6.6	6.3	
200' W = E.L. Atlantic			
11	7.3	5.6	
Cb	7.1	5.8	
1/4	7.3	5.6	
2	7.0	5.9	
1/4	7.0	5.9	
Cb	7.0	5.9	
S	7.1	5.8	

Flm St Cross Section
California St to Atlantic

80' 11" 1/2
14' 6 1/2"
13' 9 1/2"

47

BM 1309 19.37 ✓ 6.28 SE Top N/A
Flm St Atlantic

E.L. Santa Fe Right of Way

S	0.7	18.7
cb	0.7	18.7
1/4	0.6	18.8
1/2	1.1	18.3
3/4	1.6	17.8
cb	1.9	17.5
H	2.3	17.1

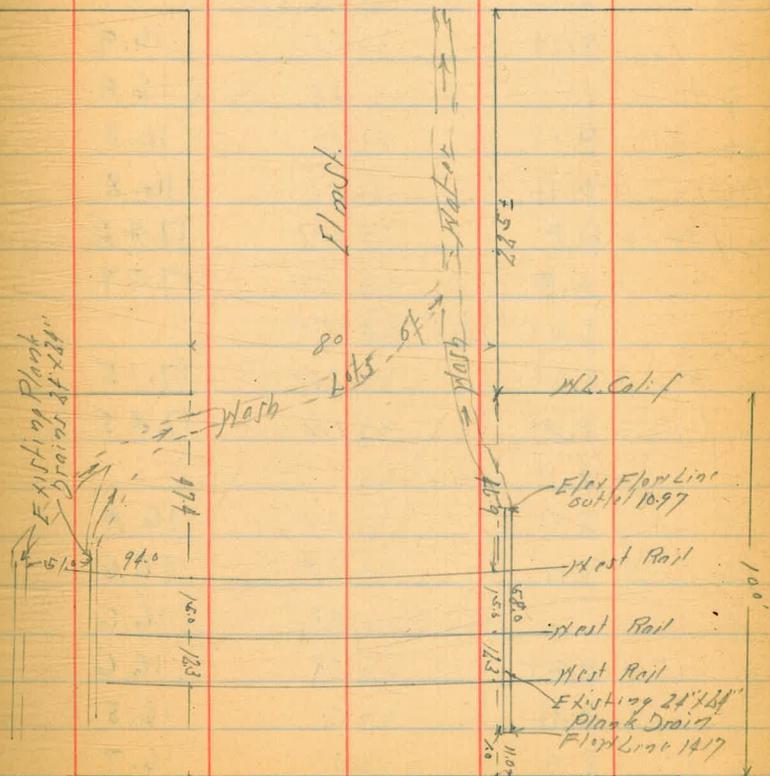
8' W of E.L. Santa Fe Right of Way

H	5.0	14.4
cb	2.7	16.7
1/4	2.3	17.1
1/2	1.5	17.9
3/4	1.5	17.9
cb	0.9	18.5
S	1.2	18.2

16' W

S	2.8	16.6
cb	2.7	16.7
1/4	2.7	16.7
1/2	1.6	16.8
3/4	2.7	16.7
cb	2.6	16.8
H	2.6	16.8

Atlantic



Elm St.

19.37

25.3 N. 0.5

25.6 N. on West Rail

H on Top Rail	1.21	18.16
S " " "	1.60	17.77
4' N		
H on Top Rail	1.48	17.89
H Dirt	2.2	17.2
Cb	2.3	17.1
1/4	2.4	17.0
2	2.5	16.9
1/4	2.5	16.9
Cb	2.6	16.8
S	2.6	16.8
S Top Rail	1.92	17.45
	1.60	17.77
58.1 N. 0.5 58.5 N. 0.2 N		
S Top Rail	2.22	17.15
H	1.92	17.45
59' N		
S	3.0	16.4
Cb	2.8	16.6
1/4	2.8	16.6
2	2.8	16.6
1/4	2.6	16.8
Cb	2.7	16.7
H	2.7	16.7

70' N

19.37

48

-10	6.9	12.5
H	8.4	11.0
Cb	6.7	12.7
1/4	6.7	12.7
2	7.2	12.2
1/4	7.2	17.2
Cb	6.8	12.6
S	7.6	11.8
+10	7.6	11.8
95' N		
-10	7.5	11.9
-5	8.0	11.4
S = Bottom West	9.8	9.6
Cb = " "	10.0	9.4
1/4	8.9	10.5
2	8.6	10.8
1/4	8.5	10.9
Cb	8.4	11.0
H	8.3	11.2
+10	8.3	11.1
100' N = H.L. California		
-10	8.5	10.9
H	8.4	11.0
Cb	8.6	10.8
1/4	8.7	10.7
2	8.7	10.7

E/m St

19.37

9.47

49

1/4	10.0	9.4
+8 = Bottom Wash	10.6	9.4
cb	9.7	9.7
S	8.7	10.7
+10	8.8	11.2

25' N of W.L. Coll

S	10.0	9.4
cb	10.1	9.3
1/4	10.3	9.1
1/2	9.8	9.6
+13 = Bottom Wash	12.1	7.3
1/4	10.4	9.0
cb	9.0	10.4
N	9.7	9.7

75' N

N	13.9	6.5
+10	12.0	7.4
+12 Bottom Wash	13.7	5.7
cb	12.8	7.2
1/4	11.3	8.1
1/2	11.2	8.2
1/4	12.1	7.3
cb	12.1	7.3
S	12.9	6.5
TP	12.61	6.76

2.71

2.47 ✓

125' N

S	3.7	5.8
cb	4.4	5.1
1/4	2.5	7.0
1/2	3.0	6.5
1/4	3.9	5.6
cb	2.7	6.8
+15 = Bottom Wash	4.1	5.4
+9	3.1	6.4
N	3.5	6.0
+11	5.0	4.5

175' N

N	4.4	5.1
+6	4.1	5.4
+10 Bottom Wash	4.6	4.9
cb	4.0	5.5
1/4	4.9	4.6
1/2	5.2	4.3
1/4	5.2	4.3
cb	5.0	4.5
S	5.0	4.5

225' N = E.L. H. Plantio

S	5.6	3.9
cb	5.4	4.1
1/4	5.6	3.9
1/2	5.5	4.0
1/4	5.2	4.3

150' N = Pol/c
13' N of S.L.

947

78

49

4.6

711 Bottom Wash

57

3.8

06

54

4.1

11

50

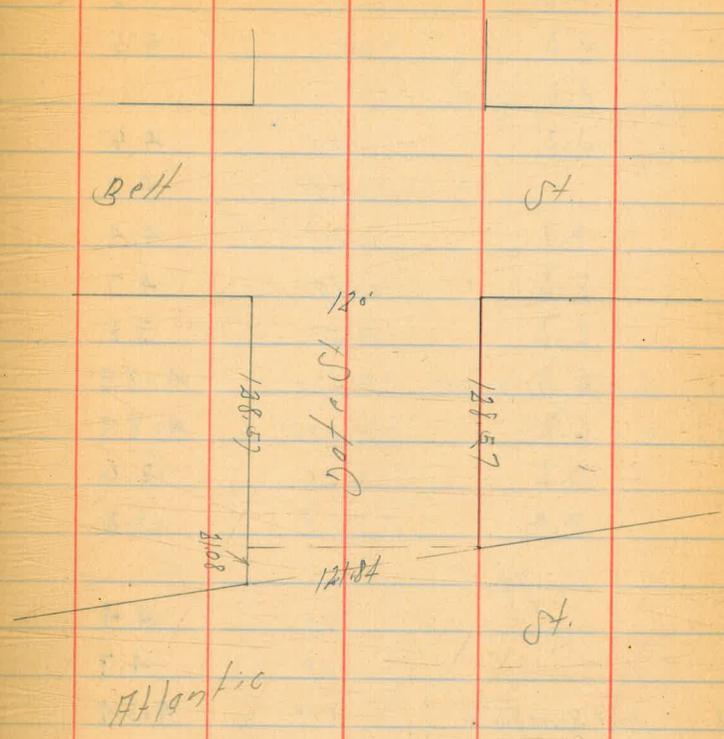
4.5

50

Date St Cross Section
Atlantic to Belt

120 W. side
20' CB
20' Q¹

BM	336	9.64 ✓	628	S.E. Top of H ₂ O
		W.L. Atlantic	121.84	side
H		6.9	2.7	
+10		4.4	5.2	
CB		5.2	4.4	
1/4		5.6	4.0	
1/2		4.2	5.4	
3/4		5.0	4.6	
CB		5.1	4.5	
S		5.1	4.5	
		W.L. Atlantic on N		
		20' N of W.L.	0.5	
S		4.8	4.8	
CB		4.8	4.8	
1/4		4.8	4.8	
1/2		4.2	5.4	
3/4		5.6	4.0	
+6	S Edge Board Walk	4.38	5.26	
+16	N Edge	4.60	5.04	
CB		5.2	4.4	
+10		4.3	5.3	
H		6.9	2.7	
		25' N of W.L. Atlantic on N		
H		4.9	4.7	
CB		6.5	3.1	
1/4		5.8	3.8	



9.64

L		4.6	5.0
1/4		4.8	4.8
cb		5.1	4.5
S		5.1	4.5
	50' W		
S		5.0	4.6
cb		5.4	4.2
1/4		5.2	4.4
L		4.9	4.7
1/4		5.8	3.8
122 - S Edge Board walk		4.25	4.89
112.2 N " " "		4.25	4.89
cb		7.0	2.6
N		7.8	1.8
	75' W		
N		5.2	4.4
cb		4.9	4.7
19 = End Board walk		5.10	4.54
119 - " " "		4.90	4.74
1/4		4.9	4.7
L		4.9	4.7
1/4		4.8	4.8
cb		5.1	4.5
S		4.9	4.7
	100' W		
S		4.9	4.7

9.64

52

cb		4.7	4.9
1/4		4.3	5.3
L		4.8	5.4
1/4		4.0	5.6
cb		4.0	5.6
N		4.0	5.6
	128.57' W = E. L. of Ball St.		
N		4.6	5.4
cb		4.4	5.2
1/4		4.3	5.3
L		4.3	5.3
1/4		4.3	5.3
cb		4.1	5.5
S		4.7	4.9

Grap St. Cross Section
California to Balt

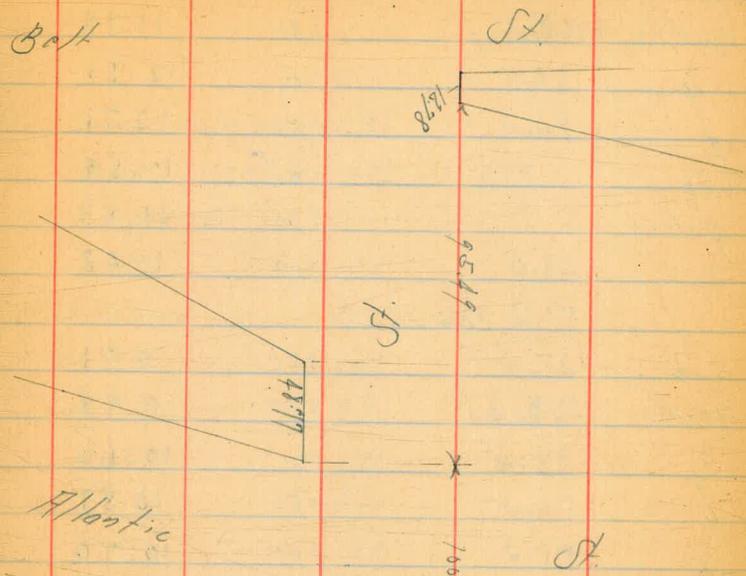
80' wide
8' 0" deep
13' 0" high

SE Top Kid
Grap & Atlantic

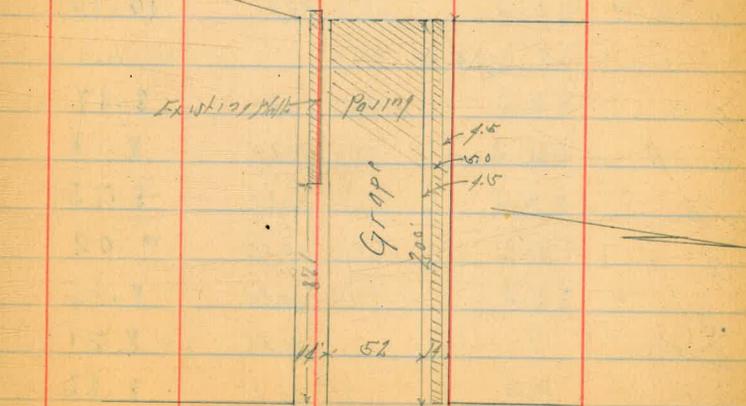
4-12-30
53

BM	10.88	19.67 ✓	8.79
	M.L. California		
S cb		1.69	17.98
Gutter on Pavement Outlet		3.12	16.55
"		1.66	18.01
"		1.65	18.02
"		1.71	17.96
Gutter " " Outlet		3.22	16.45
H cb		1.69	17.98
	SE Top of M.L. Calif		
H cb		3.56	16.11
Gutter on Pavement		4.26	15.41
"		3.59	16.08
"		3.42	16.25
"		3.56	16.11
Gutter " "		4.27	15.40
S cb		3.54	16.13
	50 ft		
S cb		5.42	14.25
Gutter on Pavement		6.20	13.47
"		5.42	14.25
"		5.27	14.40
"		5.42	14.25
Gutter " "		6.16	13.51
H cb		5.51	14.16

Balt



Atlantic



California

Grape St.

1967

75 W

H cb	729	12.38
Gutter on Paving	789	11.78
"	716	12.51
"	696	12.71
"	708	12.59
Gutter " "	784	11.83
SCB	719	12.48

100 W

SCB	896	10.71
Gutter on Paving	969	9.98
"	901	10.66
"	880	10.87
"	897	10.70
Gutter " "	964	10.03
H cb	897	10.70

125 W

H cb	1080	8.87
Gutter on Paving	1149	8.18
"	1092	8.75
"	1065	9.02
"	1082	8.85
Gutter " "	1146	8.21
SCB	1081	8.86

150 W

SCB	1249	7.18
-----	------	------

1967

54

Gutter on Paving	1203	6.64
"	1225	7.42
"	1215	7.52
"	1235	7.32
Gutter " " 12 Driveway	1292	6.69
TP	1.99 10.98 ✓	10.88 8.79
	175 W	

H cb	396	6.82
Gutter on Paving	461	6.17
"	402	6.76
"	383	6.95
"	392	6.86
Gutter " "	461	6.17
SCB	399	6.79

200 W: End of Atlantic - End of Paving Obs (W)

SCB	423	6.55 ✓
Gutter on Paving	493	5.85
"	430	6.48
"	414	6.64
"	434	6.44
Gutter " "	497	5.81
H cb	440	6.38 ✓

AL Atlantic

H	39	6.9
cb	50	5.8
"	46	6.2

Grape St.

10-78

S	45	6.3
1/4	47	6.1
cb	49	5.9
S	57	5.1

48.77' W of NE of FH/landfire

S	54	5.4
cb	52	5.6
1/4	48	6.0
S	49	5.9
1/4	48	6.0
cb	48	6.0
1/4	47	6.1

95.49' W

1/4	51	5.7	91.5' W of 1816
cb	49	5.9	11' W of SL
1/4	48	6.0	
S	47	6.1	
1/4	55	5.3	
cb	52	5.6	
S	57	5.1	

108.27' W of E.L. of Br/Hoy 1/4

S	58	5.0
cb	51	5.7
1/4	53	5.5
S	47	6.1
1/4	48	6.0

10-78

cb	51	5.7
1/4	47	6.1

55

Hartford St. Cross Section
California to Belt

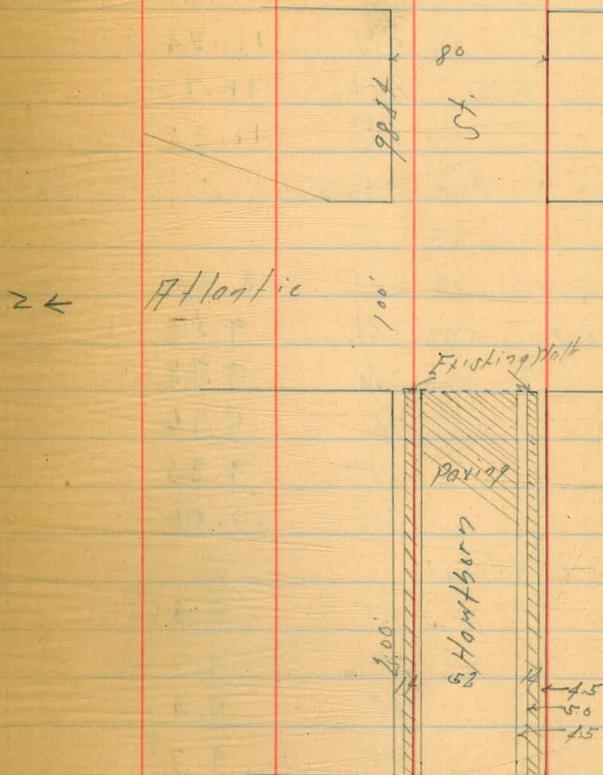
80' width
14' CB
13' QH

BM	843	17.22	879	SE Top of Grave & H. H. H. H.
N.L. California				
S cb		0.18	17.04	
Gutter on Paving Outlet		1.58	15.64	
1/4		0.26	16.96	
1/2		0.08	17.14	
3/4		0.30	16.92	
Gutter		0.83	16.39	
N cb		0.16	17.06	
50'				
N cb		1.95	15.27	
Gutter on Paving		2.64	14.58	
1/4		2.06	15.16	
1/2		1.96	15.26	
3/4		2.10	15.12	
Gutter		2.83	14.39	
S cb		2.04	15.18	
100'				
S cb		4.02	13.20	
Gutter on Paving		4.70	12.52	
1/4		3.91	13.28	
1/2		3.25	13.47	
3/4		3.87	13.35	
Gutter		4.40	12.82	
N cb		3.74	13.48	

56

2-12-31
Osborn
SE Bl'rs
Hartford
Osborn

Belt



California

Hartmann St.

1782

	150' N		
H cb		5.43	11.79
Gutter	on Paving	6.19	11.03
H	" "	5.67	11.55
S	" "	5.61	11.61
H	" "	5.88	11.34
Gutter	" "	6.50	10.72
S cb		5.87	11.35

200' N - E.L. of Atlantic - End Paving Certificate

S cb			
Gutter	on (conc) Driv	8.28	8.94
H	on Paving	7.68	9.54
S	" "	7.44	9.78
H	" "	7.46	9.76
Gutter	" "	7.87	9.35
H cb		7.16	10.06

N.L. of Atlantic

H		7.4	9.8
cb		7.5	9.7
H		7.8	9.4
S		7.5	9.7
H		7.6	9.6
cb		7.8	9.4
S		7.0	10.2

(50' N) of N.L. of Atlantic

S		7.8	9.4
---	--	-----	-----

1788

57

cb		8.2	8.9
H		8.5	8.7
S		8.1	9.1
H		8.6	8.6
cb		8.5	8.7
H		8.5	8.7
	982' N - E.L. of Belt		
H		9.1	8.1
cb		9.5	7.7
H		9.5	7.7
S		9.0	8.2
H		9.4	7.8
cb		9.4	7.8
S		8.9	8.3

Atlantic St. Grading

Prop Line Curb Prod Line
 8.00 790 783 780 785 795 753 820 830 852 865

Spruce

8.00 790 783 780 785 795 753 820 830 852 865

890 880 813 890 895 895 843 916 920 943 955

Redwood

910 900 833 890 895 895 863 930 940 963 975

970 960 893 890 895 895 938 1005 1015 1037 1050 1050

1030 1020 953 1018 1015 1048 1013 1080 1090

Quince

Prop 8 Curb 23 1/2 23 1/2 23 1/2 Curb 8 Prop

4-27-30
 S. Wilson
 J. O. ...
 North ...
 O. ...
 S. ...

BM 1403 215' of ...
 1403
 1403
 1415
 1420
 1425
 1439
 1334
 1290
 844
 441
 1285
 1217
 1068 HLT barn
 150' of ...
 1067
 90
 760

BM 1403 215' of ...
 1403
 1403
 1422
 1431 N.E. Cor.
 1437
 1365

Atlantic St. Grading

5-12-30

60

Thorn

790 783 780 775 765 755 750 740 730

8.52 8.65

799
526
131

790 783 780 775 765 755 750 740 730

8.52 8.65

890 883 870 865 855 845 840 830 820

9.42 9.55

Sassafras

890 883 870 865 855 845 840 830 820

9.42 9.55

835 830 825 820 815 810 805 800 795

805 790 783 770 765 755 750 740 730

8.52 8.65

Spruce

5.5 Sept. 10 1930
Sassafras & Co. 1st St
62.18 = 8.17
1.29 -
51.17 -
1.28 4 -
17.63 - TP
3.16 +
20.79 -
11.29
33.0 - TP
3.98 -
13.28 -
1.50 -
8.78 = TP
3.34 +
12.12 =
1.07 -
8.25 = TP NE Hub
Sassafras
& Atlantic

8M 10.04 NFBP
Horathy
+ 5.00
63

Horathy

SL

cb. 10.16

11.2506

10.50

9.40

9.70

10.00

Emory

SL

9.20

9.70

8.20

8.50

Bear

SL

Proposed Atlantic St Extension
At Barnett Ave

BM	0.32	28.05	27.73	BP Morgan Land Co From AT&T Viallet
TP	0.20	16.07	12.18	15.87
TP	0.75	8.39	8.43	7.64
BM	7.14	6.99	8.54	-0.15
		0.70		SX No 7 Barnett Atlantic

306 N. Ch Top 6.16

Gutter of Pavmg 6.81

Edge 5.95

253 E - Edge Pavmg 6.09

0.750 = BC

253 E - Edge Pavmg 5.97

Edge 6.19

306 N - Gutter of Pavmg 6.74

Edge Top Ch 6.13

0.775

311 N - Edge Top Ch 6.07

Gutter of Pavmg 6.74

Edge 6.26

346 E - Edge Pavmg 6.03

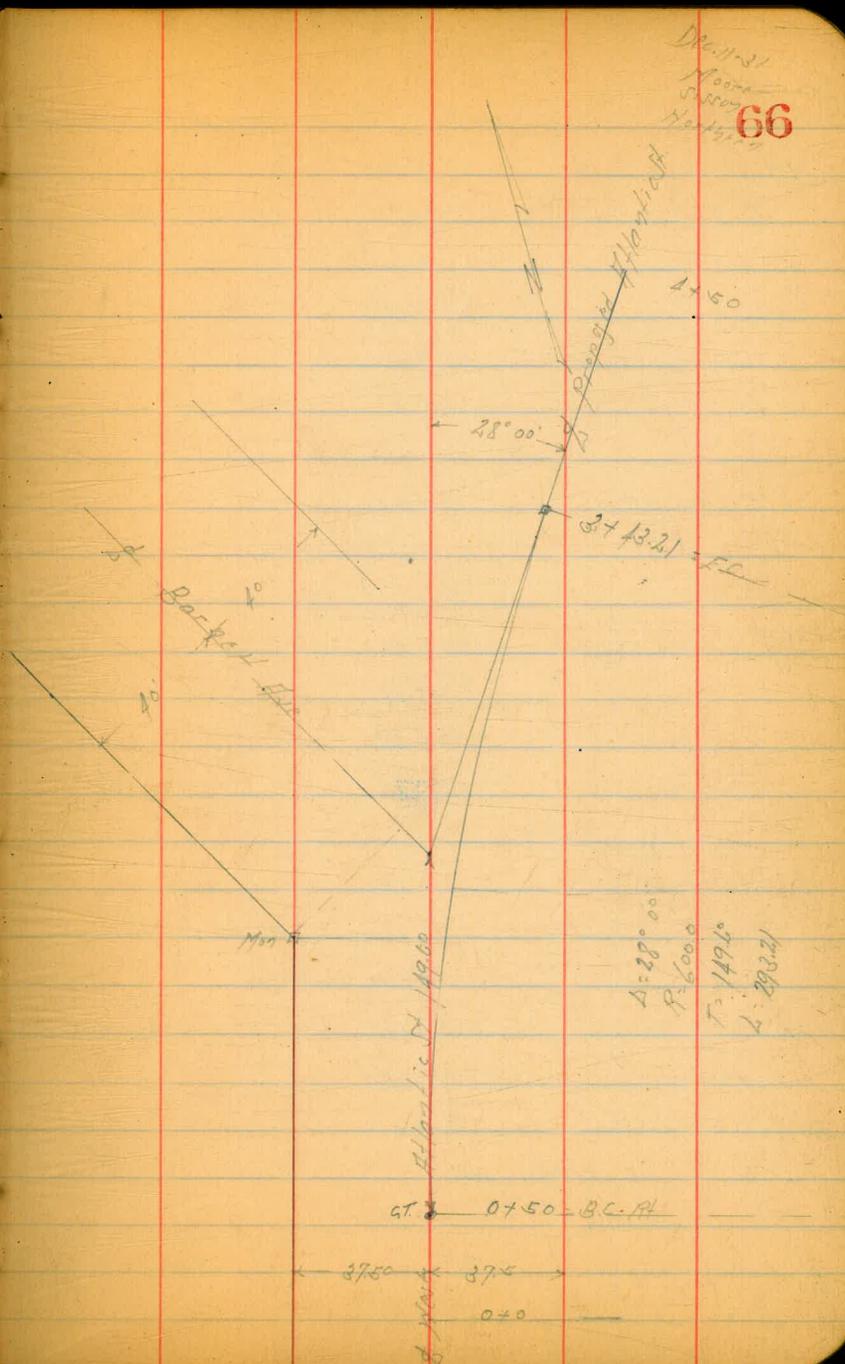
1.40

266 E - Edge Pavmg 6.16

Edge 6.21

326 N - Gutter of Pavmg 6.68

Edge Top Ch 6.04



6.99

1+25

354 W = Top Curb	6.00
Gutter on Pavmg	6.61
1/2 " " "	6.15
210 E = Edge "	6.25
Top Cb	5.60
10 E	6.2

1+50

456 E = Top W Rail	2.92
28 E	5.8
15.3 E = Top Cb	5.66
Gutter on Pavmg	6.24
1/2 " " "	5.88
398 W Gutter " "	6.54
Top Cb	5.94

1+75

540 W = Top Curb	5.79
Gutter on Pavmg	6.38
1/2 " " "	6.03
60 E = Gutter "	6.18
Top Cb	5.68
355 E = Top W Rail	2.38

1+86

305 E = Top W Rail	3.58
1/2 = Face on Top Cb.	5.61
Gutter on Pavmg	6.18

6.99

50 W on Pavmg

6.34

2+0

50 W on Pavmg	6.02
96 W = Gutter on Pavmg	6.18
Top Cb	5.60
1/2	4.8
32 E = Top W Rail	3.78
40 E	4.3
50 E	8.1

2+25

50 E	8.4
32 E	8.4
25 E	4.3
16.3 E = Top E Rail	4.05
8.3 E = " W "	4.05
1/2	4.6
345 W = Top Curb	5.64
Gutter on Pavmg	6.19

2+41.40 = 1/2 Track to S W

Top Rail	4.20
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2+51.17 = 1/2 Track to P

40 W	5.1
95 W = Top W Rail	4.27
1/2	4.3
21 E = Top E Rail	4.23
15 E	4.6

67

6.99

25 F	85
50 F	85
2175	
50' F	85
11' F	81
1/2	42
94 M = Top E Rail	418
28 M = Top M Rail	426
50 M	46
320	
50 M = Top M Rail	423
225 M = " E "	418
11 M	46
1/2	80
50' F	82
3125	
50' F	76
1/2	79
18 M	70
25 M	41
368 M = Top E Rail	415
615 M = " M "	420
374321 FC	
475 M = Top E Rail	422
35 M	42
25 M	76

6.99

1/2 of Hub	776
50 F	76
470	
50 F	79
1/2	77
50 M	76
4150	
50 M	72
1/2	79
50 F	85
M	489
57.5	613
0.86	
8 M	1555
4.20	

68

SE Top of
N. Harbor
N. Harbor
438

Top of Rail Levels
San Diego Electric R.R. At Atlantic St Extension

6.99

0 + 0 = 2741.50

62 SF = Spitch Point 3.70

100 SF 2.85

150 SF 1.48

200 SF 0.0

0 + 0 = 2741.40

21 SF = Spitch Point 4.30

50 SF 4.21

100 SF 4.20

150 SF 4.14

69

70

72

73

74

75

76

77

78

79

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill of side stake is located by the double entry method in left column and top row. The number in body

of table in same row and column gives distance from side stake to slope stake. If ground is not

IMPROVED TABLES
AND
INFORMATION

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given I may be found by dividing tangent (or external), opposite I by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

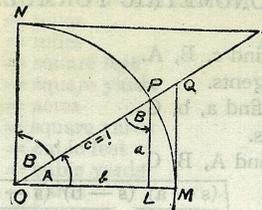


TABLE II

TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Sines} \quad \frac{\sin A}{a} = \frac{\sin B}{b} = \frac{\sin C}{c}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

$\frac{88}{114} = \frac{112}{66}$
 $\frac{66}{78}$

ENGINEERING DEPARTMENT,
SAN DIEGO.
CITY OF CALIFORNIA.

8.3
1.2
-7.1

0-3

6.8
0.3
-7.1