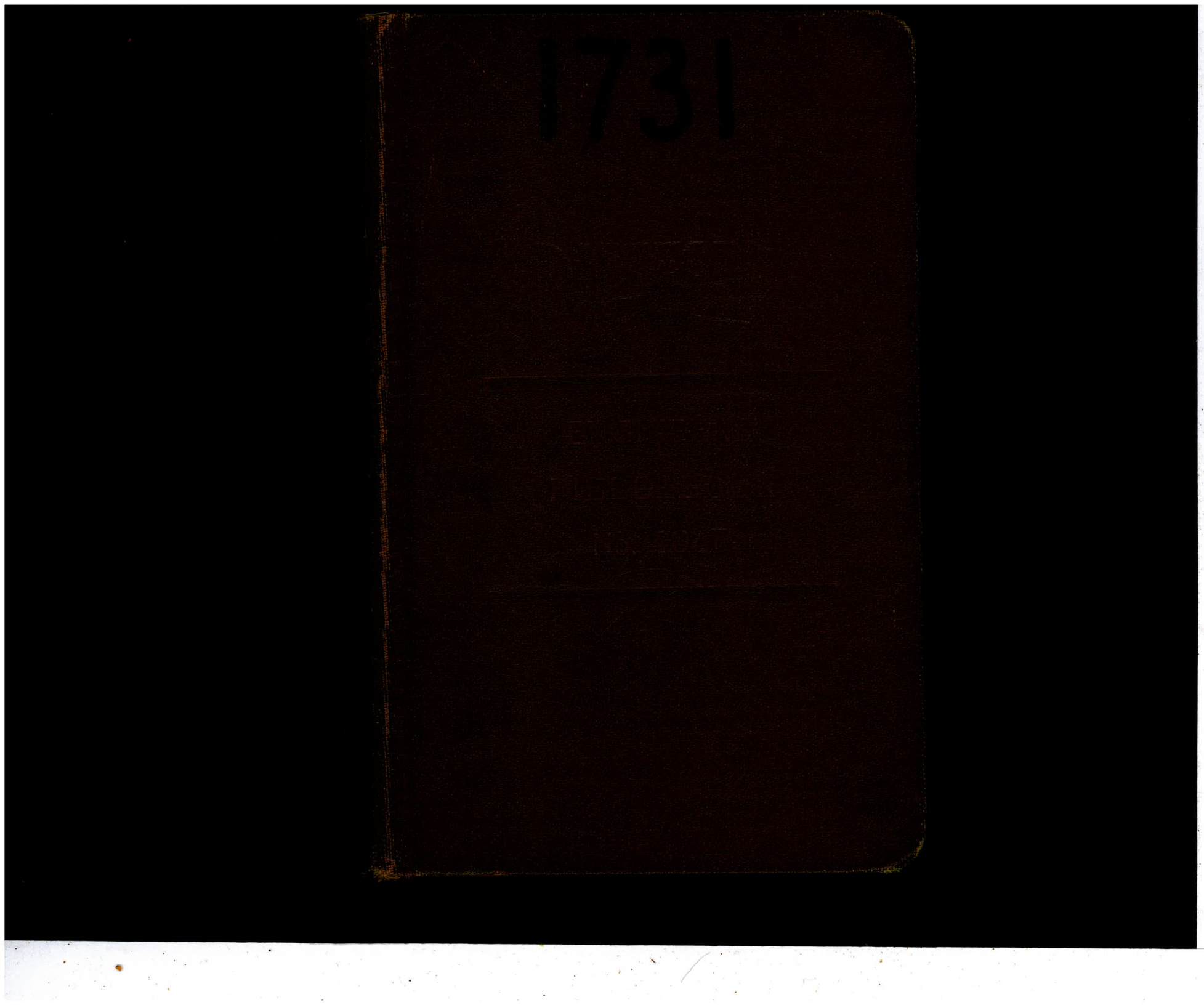
1731

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

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1731

CITY ENGINEER'S OFFICE

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Made in U. S. A.

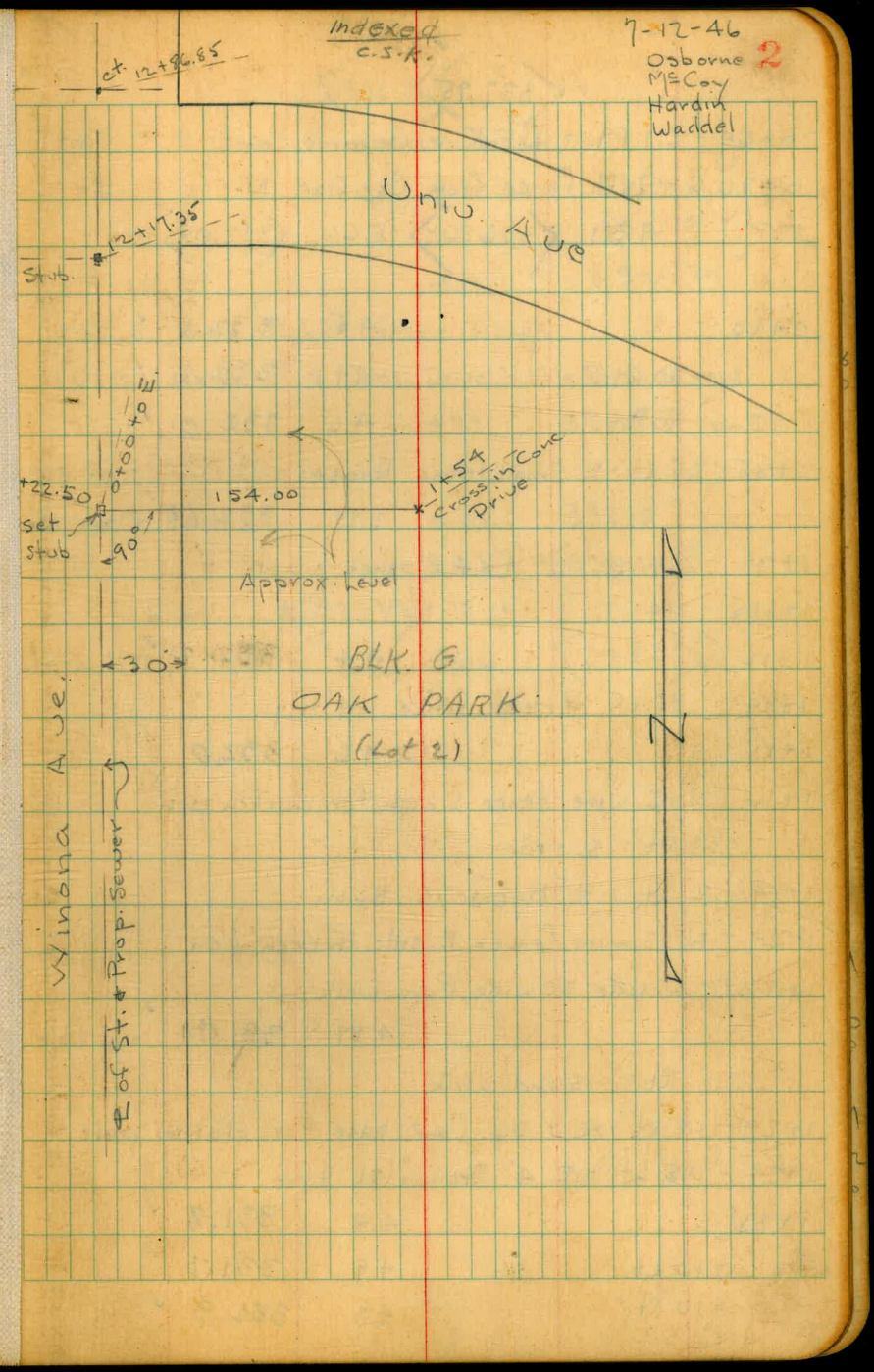
Beryl - Ingraham to Jewell 9

El Camino Del Teatro 20-39

" " " 40-59

Prop. Sewer Easement thru lot S. of Univ. Ave + E. of Prop. Sewer in ℄ of Winona Ave. - Refer to B. 1569-21 & (31)

B.M.	8.60	⟨337.75⟩	329.15 ✓	ct. N. of Univ. + ℄ Winona 1569-21
0+00 = Set stub = 11+22.50 on ℄ Winona				7/16/46
		4.46	333.29 ✓	on Stub.
0+28 - 3.5 Lt. = S.W.ly 2' Conc. walk				
		4.82	332.93 ✓	on walk
- 3.8 Rt. = N.W.ly 2' Conc. Drive				
		4.51	333.24 ✓	on Dr.
0+30 = E.L. Winona		4.8	333.0 ✓	
0+44 - 3.2 Lt. = S.W. Cor. Med. Stucco house				
		4.20	333.55 ✓	Floor elev.
0+50.2 = Latice fence bet. House & Gar.				
0+51 - 1.7 Rt. = N.W. Cor. Sing. Gar. Conc. floor & Strip drive				
		4.85	332.90 ✓	= Floor Gar.
4.3 Rt = N.ly. 2' Conc. Drive to Gar.				
		4.83	332.92 ✓	on Dr
0+53 - 0.6 Lt. = ℄ and S.ly. of 4'x2.5' Conc. Step to house				
		4.39	333.36 ✓	Top step
0+60 - Note - ground nearly level on both sides		5.2	332.5 ✓	
0+62 - 2.9 Lt. = S.E. Cor. House				
0+67 - 3' Lt. = ℄ 4"x4" Clothes post.				



(337.75) ✓

0+69 - 2.1 Rt. = N.E. Cor. Gararge			
0+70.6 = Lath fence from Cor. Gar. N.			
T.P.	4.51 (336.60) ✓	5.66	(332.09) ✓
0+80 - ℄		4.5	332.1 ✓
- 10 Rt.		4.1	332.5 ✓
- 10 Lt.		4.6	332.0 ✓
0+85 - 9.5 Lt. = ℄ Small frame House			
		3.99	332.61 ✓ Floor elev.
1+06 - 14 Rt. = ℄ 4"x4" Clothes post.			
1+11.5 - 14' " " " " " "			
1+12		4.4	332.2 ✓
1+14 = N.+S. Pickett fence - 4' high			
1+15		4.6	332.0 ✓
1+16 = N.+S. wire fence 5' high for chicken pen			
-3.3 Rt. = S. side			
1+19 - 2' Lt. = ℄ Hybiscus bush			
1+24 - N.+S. wire fence = E. side chicken pen			
1+26.8 = W. side 3.3 wide Conc. walk			
		4.89	331.71 ✓ on Edge
- 1' Rt. = = S. end walk			
1+29 - 1.8 Rt. = ℄ 1' Dia. Conc. base for clothes pole			
1+34 - 0.5' Lt. = ℄ 4" Ornamental tree			
1+35		4.8	331.8 ✓
- 10 Lt.		4.9	331.7 ✓
- 10 Rt.		4.3	332.3 ✓

(336.60) ✓

1+50 = ℄ Small Hybiscus bush		
1+52	4.3	332.3 ✓
- 10 Rt.	3.7	332.9 ✓
- 10 Lt.	4.4	332.2 ✓
1+52.8 = N.+S. Pickett fence 3' high		
1+53.3 = W. edge of 8' Conc. Drive - 11.6 Rt. to S. end.		
	4.73	331.87 ✓ on Dr.
1+54 = Chisel Cross in Conc.		
Drive = end.	4.73	331.87 ✓
T.P.	4.47	(332.13) ✓
5.69	(337.82) ✓	
check BM.	8.66	(329.16) ✓

X-Sect 20' Alley N. of Block 1 - Chalcedony Terrace - Set Tic points at Law & Ingraham & at Law & Jewell

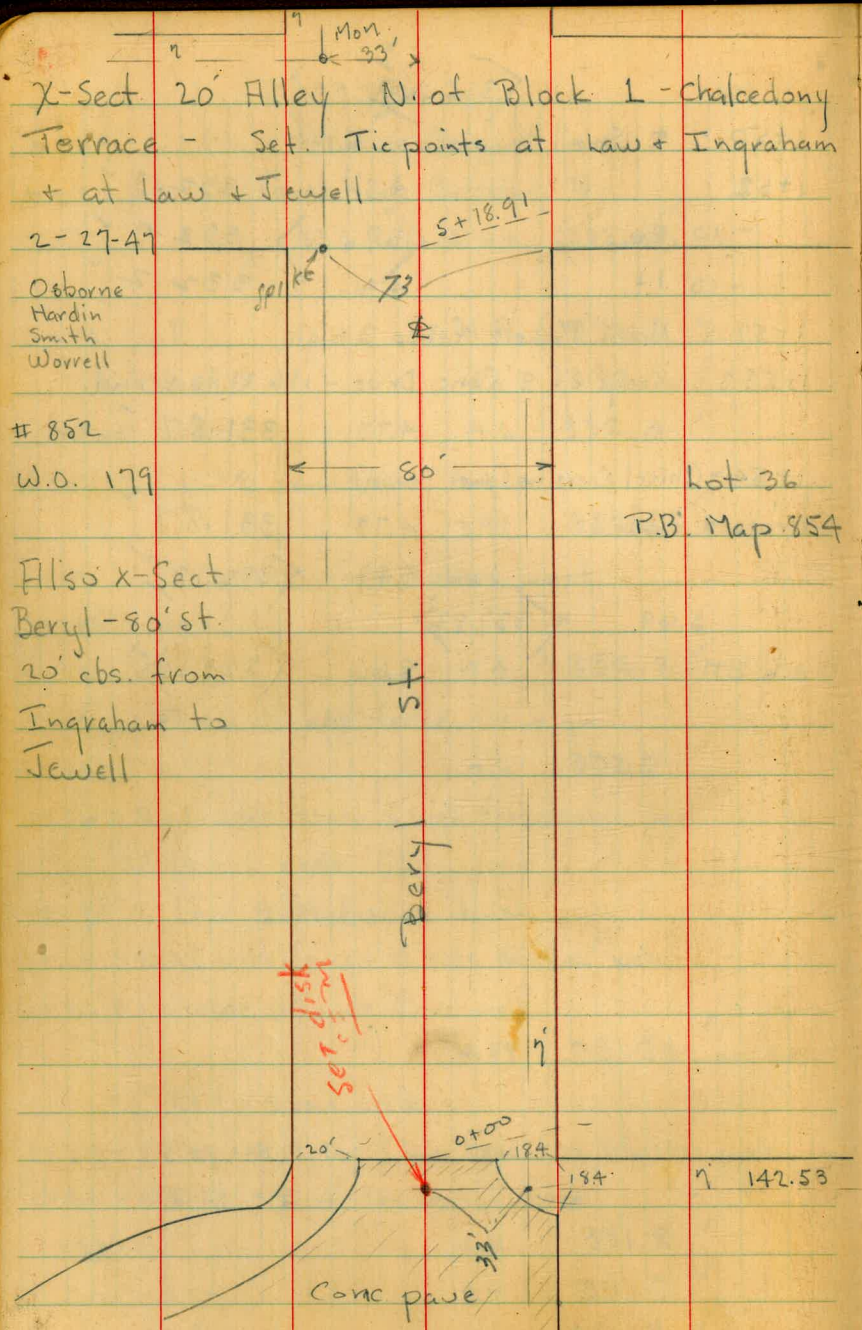
2-27-47

Osborne
Hardin
Smith
Worrell

852

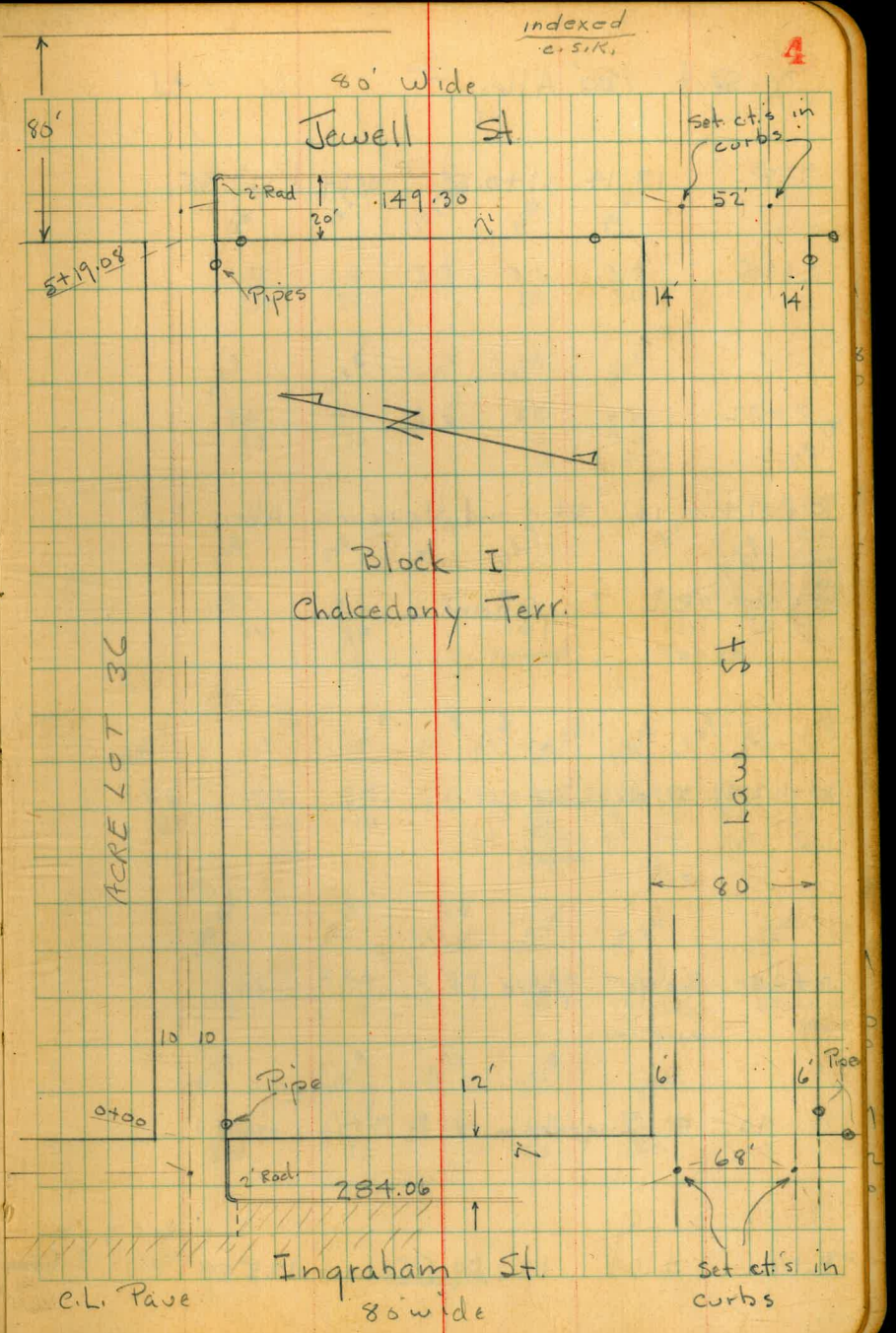
W.O. 179

Also X-Sect Beryl - 80' st. 20' cbs. from Ingraham to Jewell



indexed
C.S.R.

4



X-Sect. 20' Alley

T.P.	13.14	140.59	0.24	127.45	
0+25					
0+02					
0+01.4	10.1 Rt. = end New curb Alley Ret.				
0+00 =	E.L. Ingraham				
0-12 =	E. cb. Line				
0-20 =	Edge pave				
0-40 =	℄ Ingraham + H.C. paving				
B.M.	2.61	127.69		125.08	S.W. 7' ct. Beryl + Ingraham

Lt. = N. ℄ Rt. = S.

0+25	126.7 / 1.0 / 20	125.9 / 1.8 / 10	125.0 / 2.7	124.5 / 3.2 / 10	124.3 / 3.4 / 20					
0+02	124.7 / 3.0 / 20	123.5 / 4.2 / 10	123.2 / 4.5	121.9 / 5.8 / 10	121.1 / 6.6 / 20					
0+01.4										118.12 / 9.57 / 10.1 Top end.
0+00	124.4 / 3.3 / 20	123.1 / 4.6 / 10	120.9 / 6.8	118.7 / 9.0 / 10 ground	118.09 / 9.60 / 10.1 Top cb.	117.8 / 9.9 / 20				
0-12	124.2 / 3.5 / 50	122.9 / 4.8 / 20	121.9 / 5.8 / 10	120.3 / 7.4	117.4 / 10.3 / 10 gut.	117.94 / 9.75 / 10 Top cb. 2' Rad. Ret.	117.16 / 10.53 / 12 gut	117.89 / 9.80 / 12 Top P.C. Ret.	115.02 / 12.67 / 50 gut.	115.75 / 11.94 / 50 Top
0-20	120.64 / 7.05 / 50	118.35 / 9.34 / 10	117.72 / 9.97	117.25 / 10.44 / 10	117.24 / 10.45 / 12 = N. edge New pave	115.05 / 12.64 / 50 on New pave				
0-40	120.57 / 7.12 / 50	118.29 / 9.40 / 10	117.75 / 9.94	117.18 / 10.51 / 10	114.81 / 12.88 / 50					

127.69

2+60

2+39 - 12' Rt. = end Conc. wall

2+30 - 8.3 Rt. = ℄ P. pole

2+22 - 12' Rt = Beg. 6" Conc. wall - old foundation

T.P.	8.73	148.68	0.64	139.95

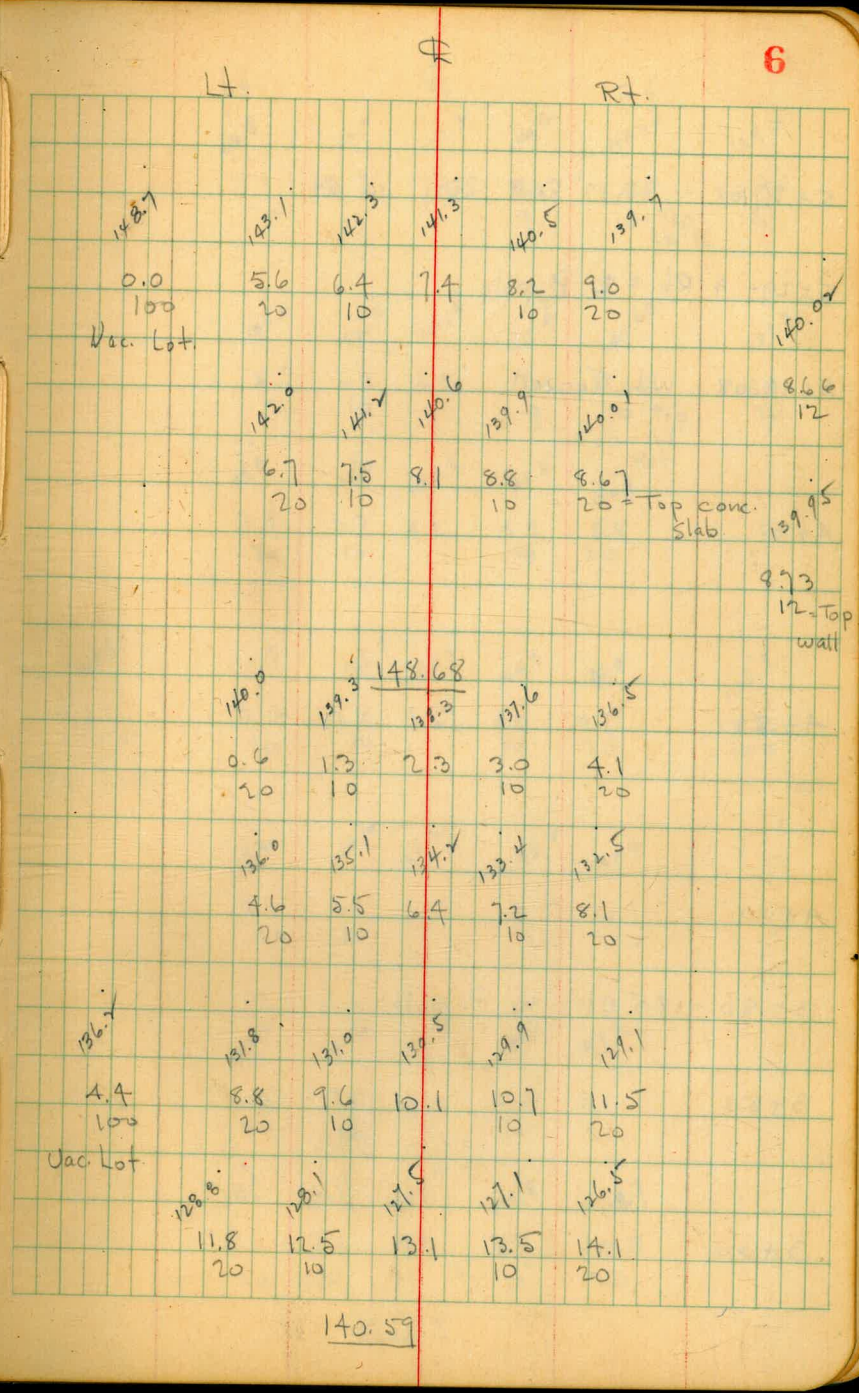
2+00

1+50

1+27-8.3 Rt. = ℄ P. pole

1+00

0+60



5+37.08 = P.C. 2° Rad. Ret. on Rt

5+29 - 9' Rt. = ℄ P. pole

5+19.08 = W.L. Jewell

4+80

4+50

4+00

3+80 - 8.5 Rt = ℄ P. pole

3+50

3+00

Lt.		℄		Rt.	
142.8	142.0	141.2	140.4	140.23	139.0
5.9 20	6.7 10	7.5	8.3 9	8.45 10=Top cb. PC.	9.7 20
143.0	142.4	141.9	141.4	140.63	139.8
5.7 20	6.3 10	6.8	7.3 9	8.05 10=Top cb.=end Ret.	8.9 20
145.8	145.0	144.5	143.8	142.9	
2.9 20	3.7 10	4.2	4.9 10	5.8 20	
148.8	146.7	145.9	145.2	144.7	135.5
+0.1 100 Vac. Lot.	2.0 20	2.8 10	3.5	4.0 10	4.7 20	13.2 100 Vac. Lot.
145.6	144.6	144.2		143.2	142.6
3.1 20	4.1 10	4.5		5.5 10	6.1 20
142.2	141.6	141.1		140.1	139.6
6.5 20	7.1 10	7.6		8.6 10	9.1 20
142.1	141.4	140.7		139.8	138.7
6.6 20	7.3 10	8.0		8.9 10	10.0 20

148.68

check starting B.M.		12.42	125.07	125.08
T.P.	1.87	137.49	13.06	135.62

End.

5+59.08 = ℄ Jewell = Sewer M.H.

5+39.08 = W. cb

144.2		141.4	140.66	139.7	136.6
4.5		7.3	8.02	9.0	12.1
50		10	on R.im M.H.	10	50

143.7	141.5	140.9	140.4	139.5	140.18	136.3	137.11
5.0	7.2	7.8	8.3	9.2	8.50	12.4	11.57
50	20	10		10	10	50	50
				gut.	Top on Ret.	gut.	Top cb.

148.68

X-Sect. Beryl - 80 st. 20' obs. from Ingraham to Jewell - Sketch - P.4

0+70

0+41 - 26' Rt. = ℄ 4" Olive

0+40

T.P. 12.44 149.66 0.12 137.22

0+10

0+02 - 2.34 Rt = ℄ P. pole

0+00 = E.L. Ingraham - edge Conc. pave

0 - 18.4 = end of cb. Ret. on Rt. at prop Line
Prob a 25' Rad

0 - 40 - on Conc. pave = ℄ Ingraham prod.

B.M. 12.26 137.34 125.08 Sw 7' ct. Beryl ℄ Ingraham

3-3-47
7.0.

Indexed
C.S.K.

Lt = N Rt = S

149.5	146.7	144.1	141.3	139.3	139.4	139.5	138.9	137.0		135.3
0.2	3.0	5.6	8.4	10.4	10.3	10.2	10.8	12.7		14.4
60	40	20	7	4		13	20	40		60

136.1	143.3	141.0	139.7	134.9	135.3	135.2	137.2	136.3	134.5	132.2
3.6	6.4	8.7	10.0	14.8	14.4	14.5	12.5	13.4	15.2	17.5
60	40	20	10	5		13	15	20	40	60

149.66

143.5	140.2	137.5	137.3	130.6	130.4	130.3	132.7	132.4	131.7	131.1
+6.2	+2.9	+0.2	0.0	6.7	6.9	7.0	4.6	4.9	5.6	6.2
60	40	20	16	7		10	15	20	40	50

140.1	129.7	128.74	127.95	128.13	128.09	127.74	127.11	127.67		128.1
+2.8	7.6	8.60	9.39	9.21	9.25	9.60	10.23	9.67		9.2
50	40	20	20	10		10	21.6	21.6		40
		Top end Ret	gut				9ut	Top end Ret		

127.83	127.33	127.64	127.58	127.23	126.72	125.51		126.09	
9.51	10.01	9.70	9.76	10.11	10.62	11.83		11.25	
23.7	23.7	10		10	20	40		40	
Top cb on Ret						gut		Top end cb.	

127.49	126.86	127.05	126.94		126.35	125.58		
9.87	10.48	10.29	10.42		10.99	11.76		
40	40	20			20	40 = edge Conc. Pave		
Top cb. on Ret	gut							

137.34

3+00

Beg.

2+94 - 40.8 = IN. edge of 12" Conc. wall

2+94 - 26.6 Rt. = ℄ 6" Olive stump

2+70

2+50 - 26' Rt. = ℄ 6" Olive

2+35

2+31 - 26' Rt. = ℄ 6" Olive

2+07 - 26.7 Rt. = ℄ 6" Olive

2+00

T.P. 11.80 160.92 0.54 149.12

1+58 - 27' Rt. = ℄ 3" Olive

1+50

1+00

℄

Lt. Rt.

163.7	160.9	158.8	157.2	156.1	156.0	155.4	154.6	153.4	153.90	152.5	150.1
+2.8	0.0	2.1	3.7	4.8	4.9	5.8	6.3	7.5	7.02	8.4	10.8
60	40	20	8	6		14	20	40	40.8 Top	40.8	60

153.54
7.38
40.8 Top wall

163.1	160.6	158.1	157.1	155.8	155.7	155.1	154.1	152.7	150.8	
+2.2	0.3	2.8	3.8	5.1	5.2	5.8	6.8	8.2	10.1	
60	40	20	8	6		14	20	40	60	

161.5	159.2	156.8	156.1	154.8	154.5	153.9	153.6	151.4	150.1	
+0.6	1.7	4.1	4.8	6.1	6.4	7.0	7.3	9.5	10.8	
60	40	20	9	6		15	20	40	60	

159.9	157.2	154.7	153.9	152.4	152.3	151.6	150.9	149.4	146.1	
1.0	3.7	6.2	7.0	8.5	8.6	9.3	10.0	11.5	12.8	
60	40	20	8	6		14	20	40	60	

160.92

156.4	154.1	151.7	150.6	147.4	147.5	147.1	146.5	145.2	143.9	
+6.7	+4.4	+2.0	+0.9	2.3	2.2	2.6	3.2	4.5	5.8	
60	40	20	7	5		15	20	40	60	

151.0	149.4	146.9	145.3	142.5	142.6	142.3	142.2	139.8	138.3	
+1.3	0.3	2.8	4.4	7.2	7.1	7.4	7.5	9.9	11.4	
60	40	20	8	4		15	20	40	60	

149.66

5+33 - 27' Rt. = ℄ 12" Olive

5+32 - 40.3 Rt = end Wedge of Conc. wall

5+18.91 = W.L. Jewell

5+09 - 28' Rt. = ℄ 12" Olive

4+85

4+69 - 40' Lt. = Beg ℄ 2' Hedge - 6' High

4+50

4+37 - 26' Rt. = ℄ 12" Olive

4+13 - 26.2 Rt. = ℄ 12" Olive

4+00

3+66 - 26.7 Rt. = ℄ 12" Olive

3+50

3+42 - 26' Rt. = ℄ 8" Olive

3+28 - 26' Rt = ℄ 6" Olive

Lt. ℄ Rt.

155.45

5.47 40.3 = Top end wall

167.2	165.3	162.8	160.6	158.4	158.1	157.1	155.6	154.3	155.39	152.3	150.1
+6.3	+4.4	+1.9	0.3	2.5	2.8	3.8	5.3	6.6	5.53	8.6	10.8
60	40	20	7	4		17	20	40	40.3 Top	41.3	60

169.42	166.2	164.4	160.9	158.8	157.3	157.2	156.4	155.1	153.8	155.15	152.1	150.5
+8.50	+5.3	+3.5	0.0	2.1	3.6	3.7	4.5	5.8	7.1	5.77	8.8	10.4
58 Floor House	55 ground at House	40	20	7	4		15	20	40	40.4 Top	41.4	60

165.6	163.2	159.9	157.9	156.7	156.5	155.9	154.1	153.9	154.96	152.7	151.1
+4.1	+2.3	1.0	3.0	4.2	4.4	5.0	6.8	7.0	5.96	8.2	9.8
60	40	20	8	5		16	20	40	40.4 Top	41.4	60

164.4	162.3	159.3	157.2	156.1	155.9	155.5	154.0	153.7	154.46	152.5	150.9
+ 3.5	+1.4	1.6	3.7	4.8	5.0	5.4	6.9	7.2	6.46	8.4	10.0
60	40	20	7	5		16	20	40	40.4 Top	41.4	60

164.6	162.2	159.1	157.2	155.8	155.7	155.5	154.5	153.2	154.03	151.7	149.7
+3.7	+1.3	1.8	3.7	5.1	5.2	5.4	6.4	7.7	6.89	9.2	11.2
60	40	20	8	6		14	20	40	40.6 Top wall	41.6	60

160.92

Continued on page 18

check Starting B.M.			10.93	125.10 ✓	125.08
	0.93	136.03	12.88	135.10	
T.P.	0.12	147.98	13.06	147.86	

End.

5+58.91 - ℄ Jewell - on Sewer M.H.

5+38.91 - W cb. Line Jewell

5+36 - 40' Lt. - End. E Hedge

168.6		165.4	162.7	160.4	159.01	158.3	156.9	153.3	147.2
+7.7	+4.5	+1.8	0.5	1.91	2.6	4.0	7.6	13.7	
80	40	20	10	MH	10	20	40	90	

167.4	166.3	163.4	161.9	159.1	158.6	157.4	157.0	153.5	150.8
+6.5	+5.4	+2.5	+1.0	1.8	2.3	3.5	3.9	7.4	10.1
60	40	20	11	5		17	20	40	60

160.92

Ingraham Street
Beryl st - South.

I.N.O. 25001

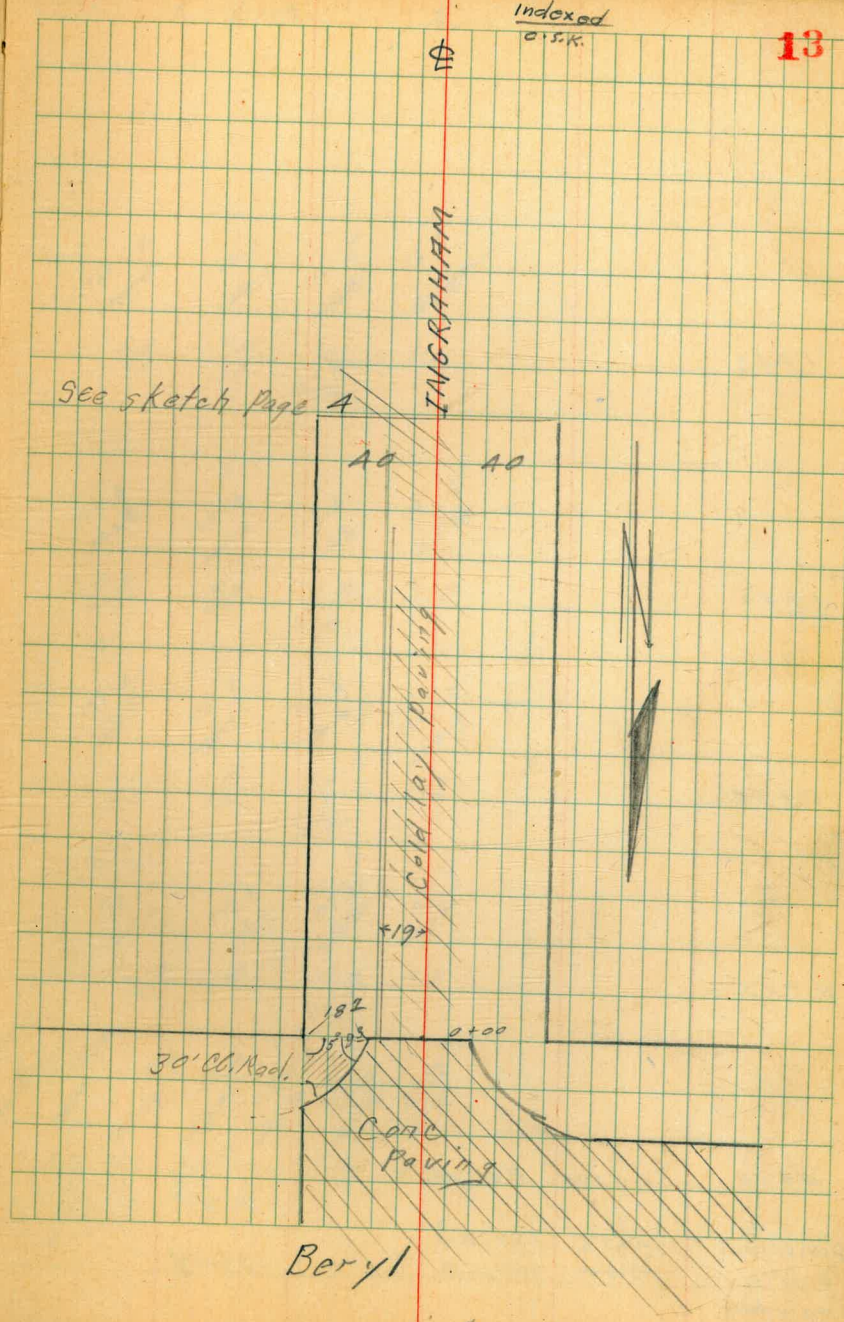
4-30-47

Sommermeyer
W. Moore
Meltan
Roberts

5-1-47 Notes Reduced Merry-

Indexed
O.S.K.

13



L = East. ℄

1+23				
1+00				
0+50				
0+05				
0+00 :	So. Line	Beryl.		
SW 7' Tack Beryl & Ingraham	4.56 ~~2.50~~	129.64 ~~127.58~~	—	125.08

123.4 ~~121.4~~	122.1 ~~120.1~~	118.5 ~~116.5~~	118.5 ~~116.5~~
6.2 / 40	7.5 / 23	11.1 / 19 E. Pav.	11.1
124.8 ~~122.8~~	123.0 ~~121.0~~	119.8 ~~117.8~~	119.8 ~~117.8~~
4.8 / 40	6.6 / 23	9.8 / 19 E. Pav	9.8
127.4 ~~125.4~~	126.1 ~~124.1~~	122.6 ~~120.6~~	122.7 ~~120.7~~
2.2 / 40	3.5 / 22	7.0 / 19 Edge Pav	6.9
131.1 ~~129.1~~	128.7 ~~126.7~~	125.2 ~~123.2~~	125.3 ~~123.3~~
+1.5 / 40	0.9 / 22	4.4 / 19 E Pav.	4.3
128.4 ~~126.4~~	127.34 ~~125.28~~	127.08 ~~125.02~~	126.10 ~~124.04~~
1.2 / 40	2.30 / 36 Edge Walk	2.56 / 31 Edge Walk	3.54 / 21.7 Top ℄
			4.14 / 21.7 Cut
			125.50 ~~123.44~~
			125.64 ~~123.58~~
			4.00 / 10
			125.57 ~~123.51~~
			4.07

1+48 on paving

1+47 30' Lt = E. Edge P. pole # 420.662 4

1+45

1+43

129.64

~~127.58~~

119.0	117.90	117.1	117.2	117.1	117.1
~~115.0~~	~~115.84~~	~~115.1~~	~~115.2~~	~~115.1~~	~~115.1~~
10.6	11.74	12.5	12.4	12.5	12.5
40	28 Topab	28	20	15.5	

119.9	117.4	117.2	117.2	
~~117.9~~	~~115.4~~	~~115.2~~	~~115.2~~	
9.7	12.2	12.4	12.4	
40	25	19 E.P.		

120.9	120.0	117.4	117.3
~~110.9~~	~~110.0~~	~~115.4~~	~~115.3~~
8.7	9.6	12.2	12.3
40	23	19 Edge pav	~~127.55~~ 129.64

Jewell St. Beryl South 150'

Alo sketch Needed. see page 4

W.O. 800.23

Lt. East ℄ Rt = West

1+18				
1+00				
0+50				
T.R	2.93	150.69	12.55	147.76
0+00 5				
0+00	30° Rt. = End of 1' wide East + West old Conc Wall.			
M.H. Rim R 12 Line G From Bottom	1.30	160.31	—	159.01

Indexed
C.S.K.

145.1	144.7	142.5	141.2	141.9	141.3	142.6	142.7	
5.6 / 40	6.0 / 36	8.2 / 31	9.5 / 22	8.8	7.4 / 17	8.1 / 18	8.0 / 40	
145.8	145.8	144.3	142.6	143.2	143.1	142.7	142.8	143.6	143.8
4.9 / 40	4.9 / 35	6.4 / 32	8.1 / 22	7.5 / 13	7.6	8.0 / 14	7.9 / 17	7.1 / 18	6.9 / 40
150.0	149.8	148.7	148.0	147.1	146.9	146.5	147.2	147.5	148.2
0.7 / 60	0.9 / 45	2.0 / 40	2.7 / 36	3.6 / 20	3.8 / 150.69	4.2 / 11	3.5 / 26	3.2 / 40	2.5 / 60
154.5		154.6	153.8	153.7			153.6		151.4
5.8 / 40		5.7 / 21	6.5 / 19	6.6			6.7 / 16		7.9 / 40
154.4		154.6	153.7	153.6	153.8	154.9	155.2		154.3
5.9 / 40		5.7 / 21	6.6 / 19	6.7	6.5 / 25	5.4 / 30	5.1 / 40 Top wall		6.0 / 40 Ord

160.31

Jewell St. Beryl South.

140.66
Check to M.H. Rim
Page 8 Line 7
~~From Bottom~~ 10.02 140.67 0.01

1+35

1+25

150.69

141.4 140.3 140.67 140.4 141.0 142.5

9.3/40 10.4/20 10.02 on M.H. 10.3/17 9.7/20 8.2/40

142.7 140.7 141.4 140.9 141.9 142.6

8.7/40 10.0/21 9.3 9.8/17 8.8/18 8.1/40

150.69

Beryl St. Cont. from Page 12

W.O. 80023

6+10 — over

Sommermeyer
W Moore
L Melton

5+98.91 = E. Line Jewell

Footings about 0.5 deep.

5+97 36' Lt. = start 10" wide faced rock wall

5+96

5+83

5+62

Rim M.H. Page 12 © Jewell & Beryl. 7.94 166.95 — 159.01

Stationing Continued from Page 12

Lt = N. ℄ Rt. = S

167.6	165.1	166.1	165.6	163.5	161.1	160.7	159.7	157.8	155.8	155.3
+0.7	+1.8	0.8	1.3	3.4	5.8	6.2	9.2	9.1	11.1	11.6
40	36.5 top wall	36.5 Ord.	25	14	6		15	21	34	40

167.6	165.1	166.1	165.6	163.5	161.0	160.6	159.7	157.8	155.9	154.5
+0.7	+1.8	0.8	1.3	3.4	5.9	6.3	9.2	9.1	11.0	12.4
40	36.5 wall top	36.5 Ord.	25	14	6		15	20	36	40

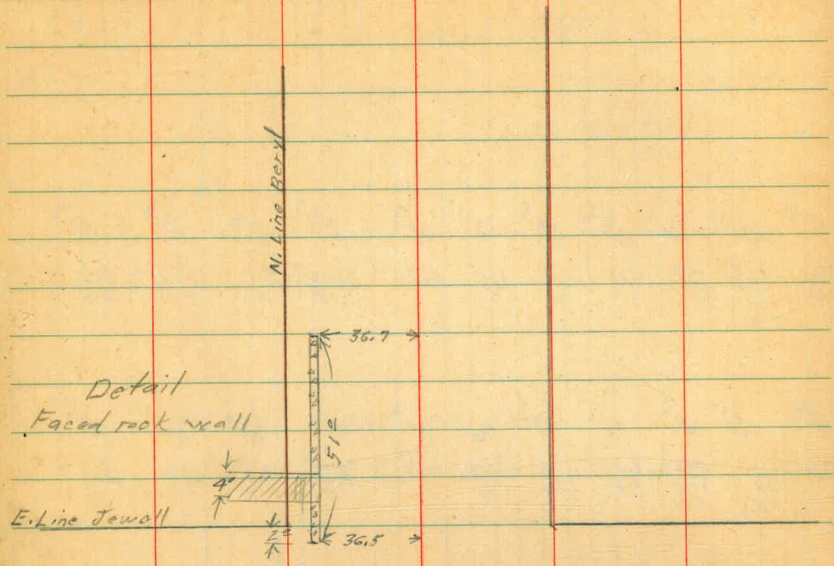
167.0	166.9	166.3	162.8	161.1	160.4
+0.1	0.0	0.6	4.1	5.8	6.5
40	35	24	10	6	

167.2	166.3	163.7	162.3	160.3	159.9	158.9	157.3	155.9	154.5
+0.3	0.6	3.2	4.6	6.6	7.0	8.0	9.6	11.0	12.4
40	35	16	8	5		15	22	38	40

167.0	166.1	165.1	162.4	159.7	158.9	158.2	155.9	153.6
+0.1	0.8	1.8	4.5	7.2	8.0	8.7	11.0	13.3
50	40	31	15	6		12	27	40

166.95

Beryl St. at Jewell



6+48 $36\frac{7}{}$ Lt. = End Faced rock wall

6+12^{3} = ℄ 4 wide steps in wall. (4 steps)

6+10

168.6 168.8 166.2 165.0 162.3 161.7 159.0 157.1 155.5

+1.7 +1.9 0.7 1.9 4.6 5.2 7.9 9.9 11.4

40 36.7 36.7 22 15 22 40 50

top wall Grd

166.8

0.1

36.5

Top Bottom step

168.7 168.8 166.0 165.4 161.4 161.0 160.1 158.1 159.6

+1.8 +1.9 0.9 1.5 5.5 5.9 6.8 8.8 12.3

40 36.5 36.5 25 5 15 21 40

top wall Grd

El. Camino del Teatro

Cross Sec. East of

Muirlands Dr.

Sommermeyer-

Melton 6-16-47

Sherman

W.O. 25001

Map # 2024

{M sheet 196
Doc. 355369
" 16663}

R. of S. 545 by R.E. 32

All distances chained

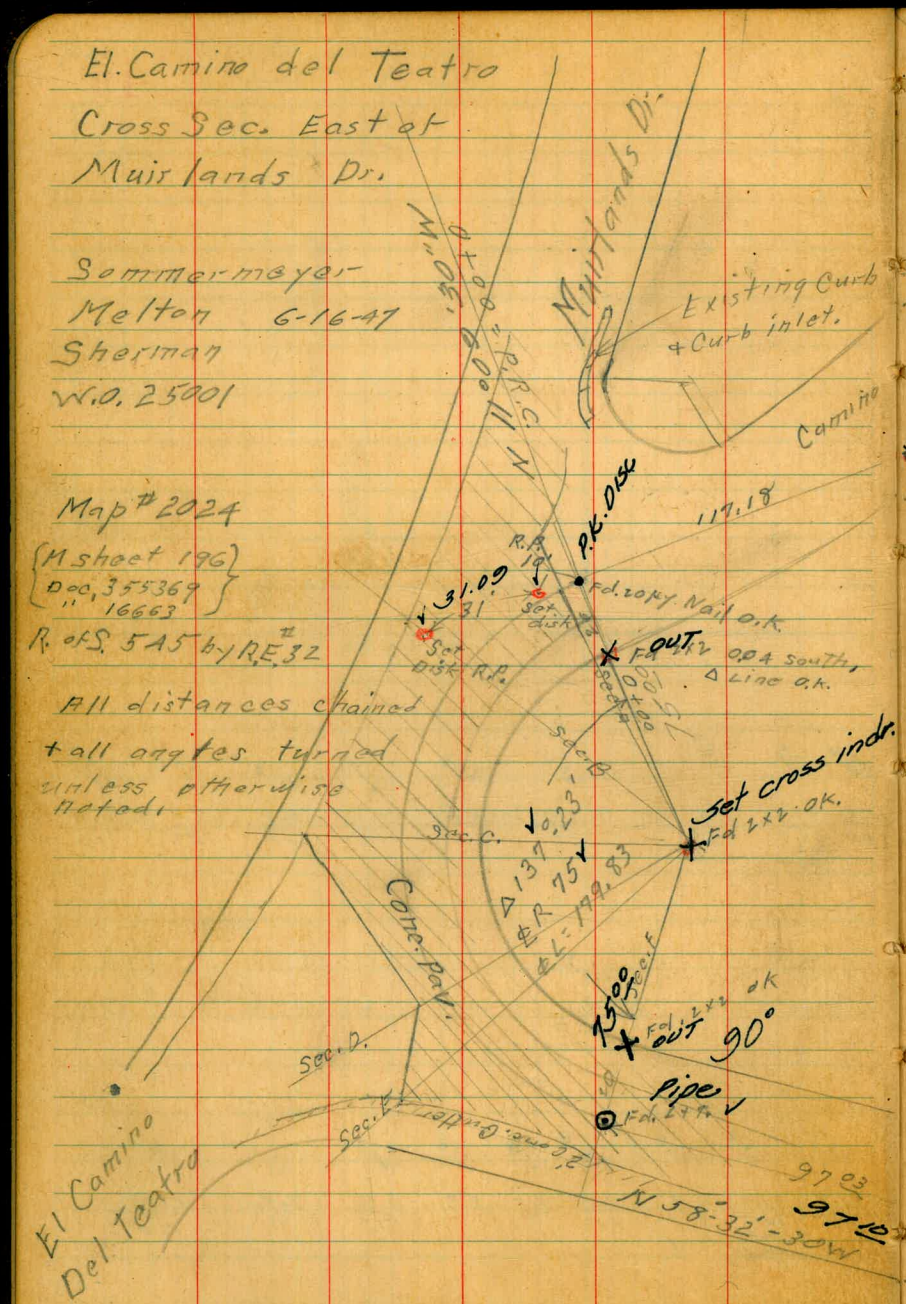
+ all angles turned

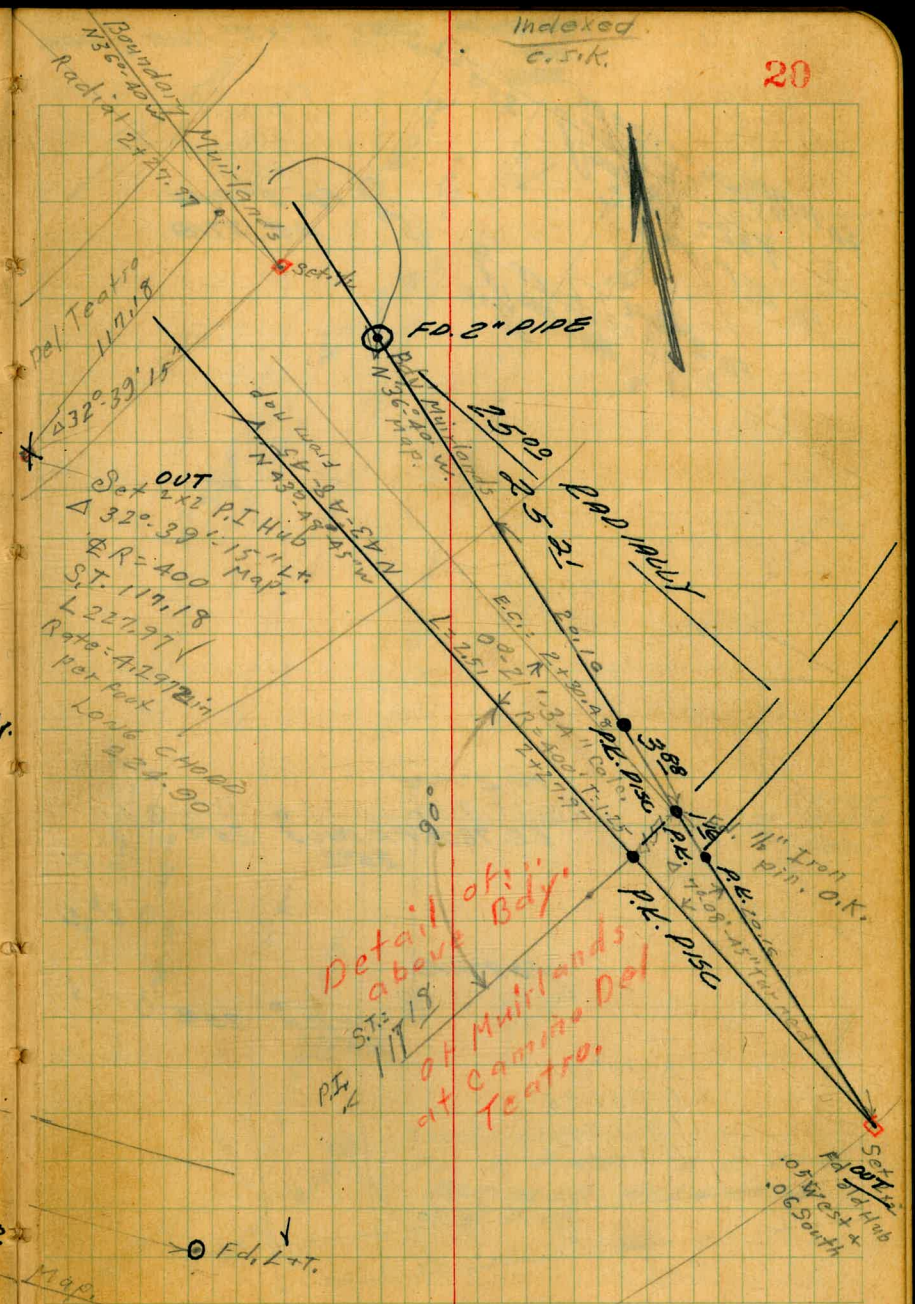
unless otherwise

noted.

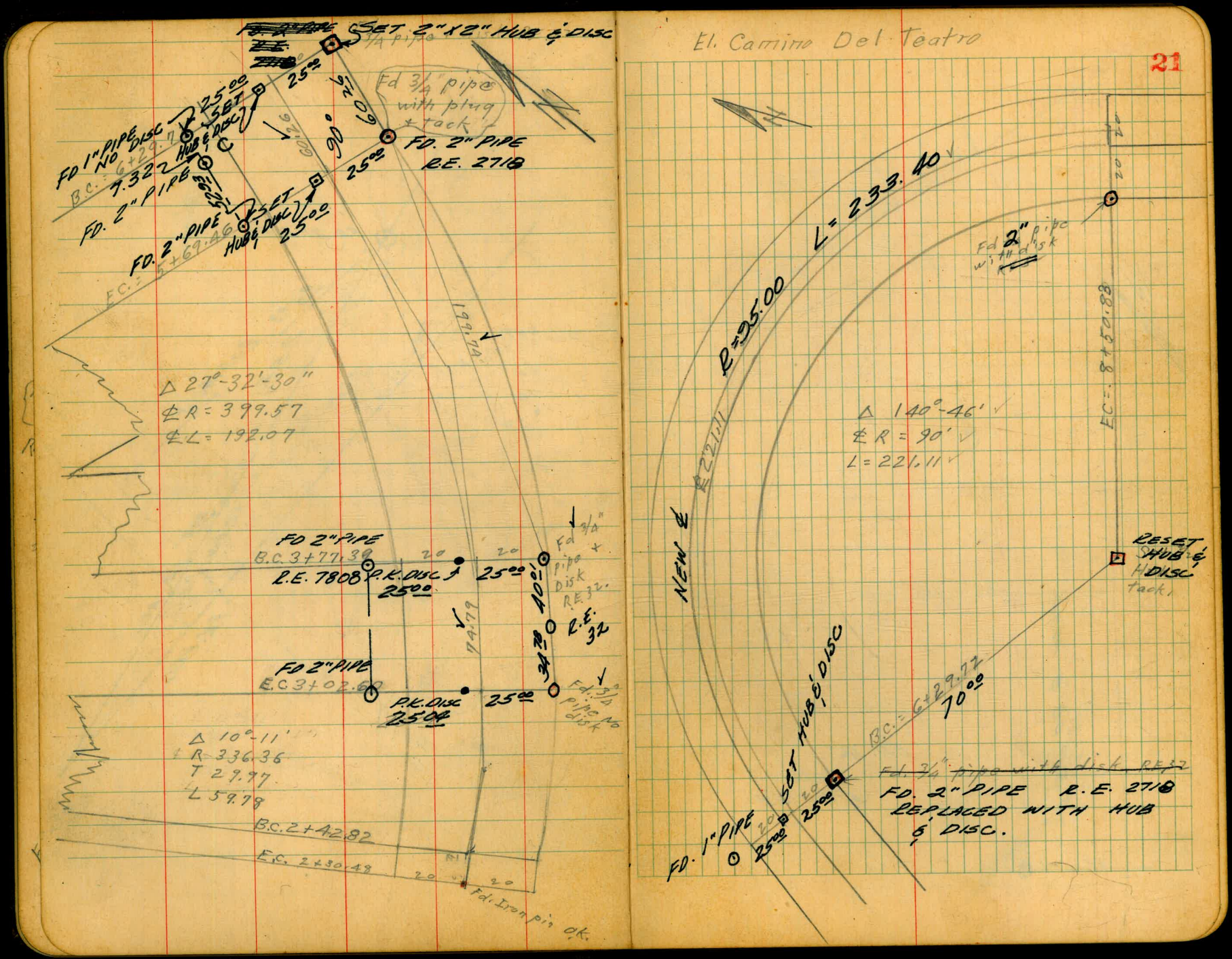
Indexed
C.S.K.

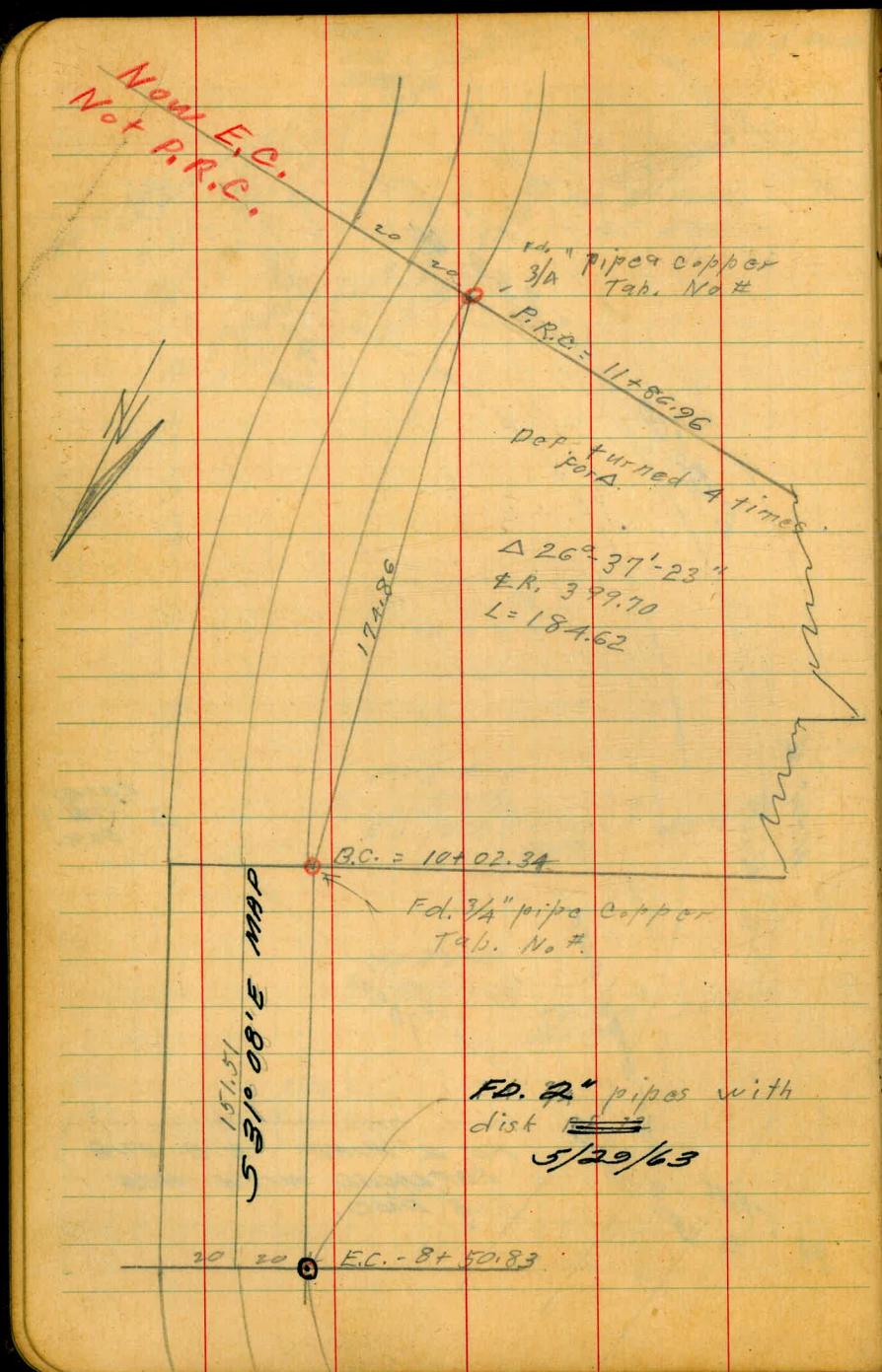
20

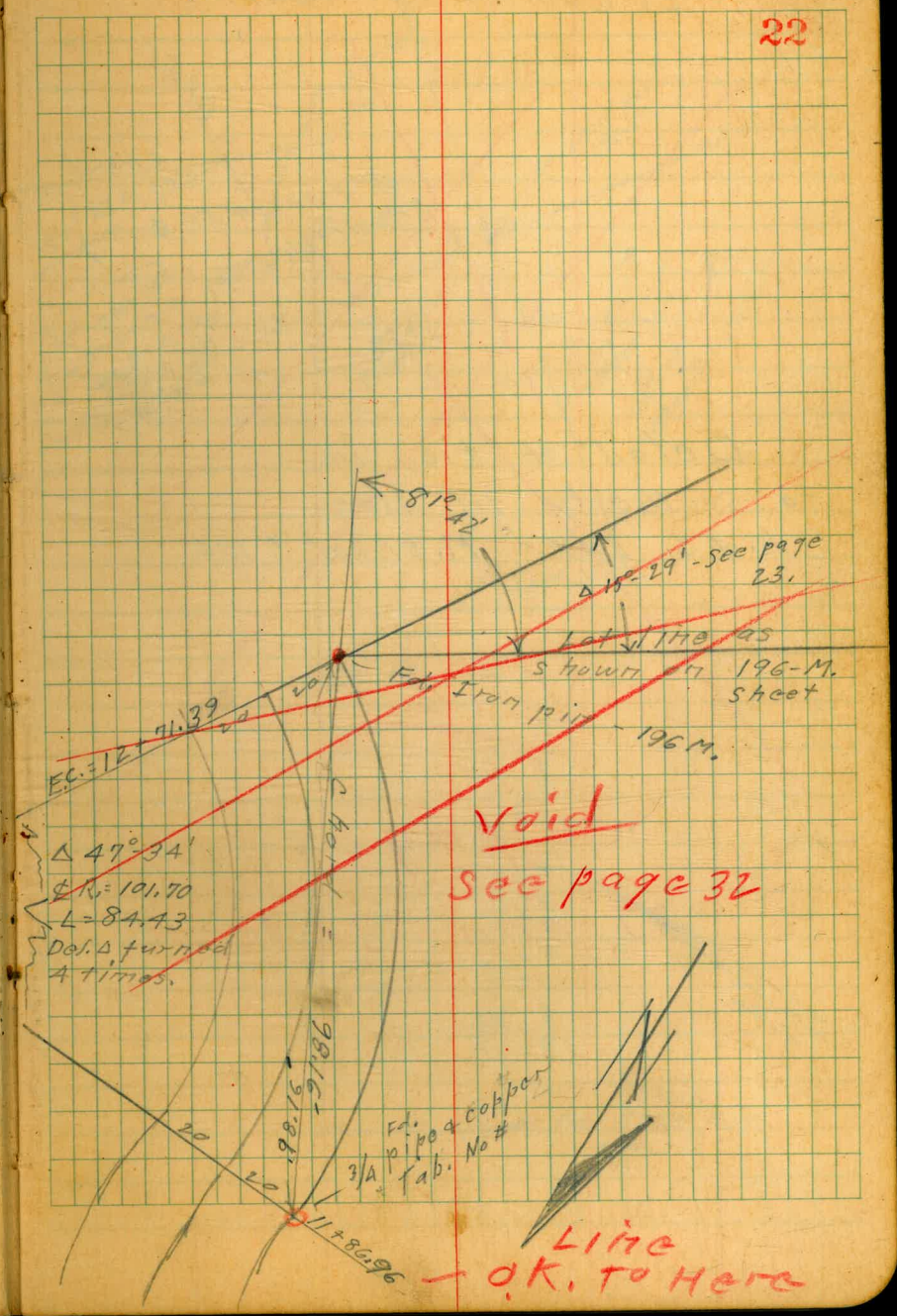




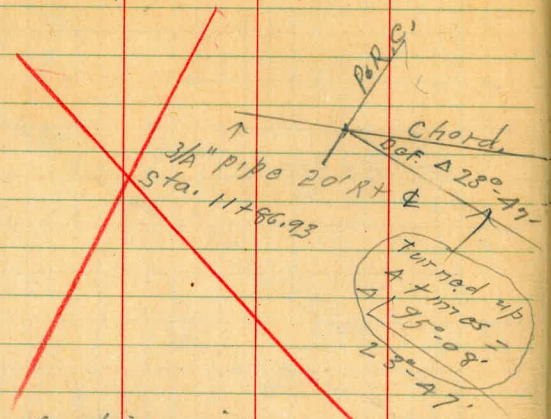
El. Camino Del Teatro




Now E.C.
Not P.R.C.
20
20
Fd. 3/4" pipe & copper Tab. No #
P.R.C. = 11+86.96
Def. turned 4 times for Δ.
Δ 26°-37'-23"
℄R. 399.70
L = 184.62
174.86
B.C. = 10+02.34
Fd. 3/4" pipe copper Tab. No #.
151.51
S 31° 08' E MAP
FD. 2" pipes with disk
5/29/63
20
20
E.C. - 8+50.83


81°42'
Δ 15°-29' - See page 23.
Lot line as shown on 196-M. sheet
Fd. Iron pin - 196 M.
E.C. = 12+71.39
20
20
Void
See page 32
Δ 47°-34'
℄R. = 101.70
L = 84.43
Def. Δ turned 4 times.
98.16
98.16
20
20
Fd. 3/4 pipe & copper Tab. No #
11+86.96
Line
O.K. to Here

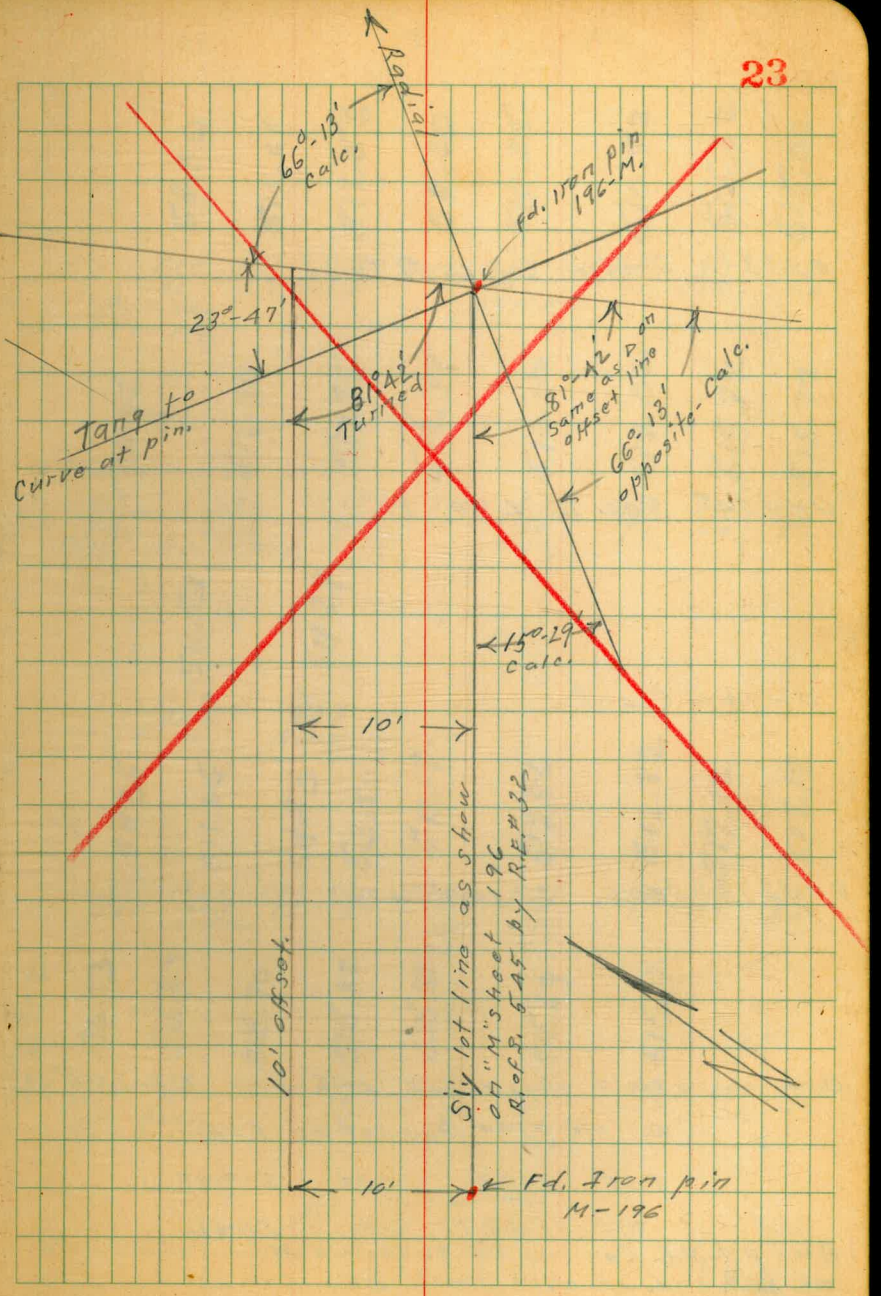
El Camino Del Teatro.



Detail of tie in
to Southerly lot line
R. of S. 545 - M. sheet # 196

Void

see pages
33 and 34 left.



0-73[7] Section "C" Δ 79°-25'

0-104[9] Sec. D. Δ 90°-15'

0-137[1] Cont

0-137[1] Sec. E. Δ 104°-45'

0- =Sec. "F" (Page 20) on Radial line Δ 137°-23'

Δ's off 0+00 Gun set on Radius point

9.25	518.32	0.70	509.07
9.15	509.77	—	500.62

B.M.= B.P. N.E. Camino Del Teatro & Muirlands Drive on North end of curb inlet. EL.= 500.62

Lt.					℄					Rt.				
					511.30		511.61	511.56	511.20	510.75	510.72	515.02	515.02	
					7.02 / 41 Δ in pav. Edge pav.		6.91 / 28	6.76 / 13	7.12	7.57 / 10 Edge pav.	7.6 / 12	3.3 / 19	3.3 / 20	
			511.62			512.30		512.75	512.37	512.00	512.02	515.72	515.72	
			6.7 / 39 Dirt			6.02 / 2.1.6 Δ in pav.		5.57 / 7	5.95	6.32 / 10 Edge pav.	6.3 / 11	2.6 / 17	2.6 / 20	
					511.53		511.29							
					6.79 / 46.7 top of		7.03 / 46.7 Gutter							
		511.35		511.65		511.83		513.20	513.17	512.87	512.82	517.12	517.12	
		6.97 / 345		6.67 / 32.2 End Par.		6.49 / 16		5.12 / 3	5.15	5.46 / 19 Edge pav	5.5 / 11	1.2 / 17	1.2 / 20	
517.52	516.13		515.84		515.70		515.82		515.81	515.69	515.72			
0.8 / 20	2.89 / 12 Curb Tot		2.48 / 12 Gutter		2.62 / 11		2.50 / 10 Edge Pav		2.51	2.63 / 19 Edge Pav.	2.6 / 12	+0.4 / 18	+0.4 / 20	

3' wide conc gutter

0+36 Def. 2°34' - 44' Lt. = End existing curb +

0+34 Continued

66' Lt = Ctr. 2x3^E Grate

0+34 (Def. = 2° 26' Lt) 60' Lt = Ctr. Curb inlet

0+00 = P.R.C. (Page 20)

0-6.9 Section A. Δ of 5°-30' End paving

2.07 509.79 10.60 507.72

0-52^7 Sec. B. (Page 20) Δ 40°-15' Transit set on Radius point. Δ^s off 0+00.

518.32

Lt.					℄			RT
501.92	501.09	502.09	503.09	503.19	505.39	505.69	508.99	509.39
7.87 / 44 top. el.	8.70 / 44 Gutter	7.7 / 43	6.7 / 30	6.6 / 22	4.4	4.1 / 12	0.8 / 17	0.4 / 20
		500.20	500.95	499.96				
12.6± / 66 Invert Aprox El.	9.59 / 66 on grate		8.84 / 60 top el.	9.83 / 60 Gutter				
		501.29	502.09	503.09	505.29			
	8.50 / 44 on con gutter		7.7 / 40	6.7 / 23	4.5			
501.79	503.08		503.82		504.79	505.39	509.09	509.19
8.00 / 58 Edge pav.	6.71 / 37 pav		5.97 / 20 Edge pav		5.0	4.4 / 11	0.7 / 18	0.6 / 20
			504.74		504.96	505.12	505.29	509.79	509.79
			5.05 / 10 Δ in pav		4.83	4.67 / 10 Edge pav	4.5 / 12	0.0 / 18	0.0 / 20
					509.79				
			508.00		508.15	508.09	508.12	510.72	510.72
			10.32 / 10 Edge pav		10.17	10.23 / 10 Edge pav	10.2 / 12	7.6 / 18	7.6 / 20

2+42.82 =	B.C. Lt.	Δ 9°-46'		
Iron Pipe 2+30.48	11.09	531.85	1.02	520.76
2+30.48	Bdry Muirlands		(Fd. Iron pin on ℄)	
2+00	14°-19.44'			
1+50	10°-44.55			
1+00	Def. 7°-09.70 Lt.			
T.P.	12.25	521.78	0.26	509.53
0+50	Def.	3°-35'		
		509.79		

Lt. ℄ Rt.

(2+42.82)		13.6/30 518.25	11.2/6 520.65	10.4/4 521.45	10.1 521.75	7.4/12 522.45	7.8/14 524.05	6.5/20 525.35	5.2/30 526.65
(2+30.48) 531.85		8.2/40 513.58	4.1/30 517.68	1.4/7 520.38	1.0 520.78	0.6/12 521.18	+1.5/16 523.3	+1.8/20 523.6	+2.9/30 524.7
(2+00)	10.6/60 510.18	10.0/42 511.78	7.2/36 514.58	6.8/30 514.98	4.2/11 517.58	4.0 517.78	3.9/12 517.88	0.7/18 521.08	0.5/20 521.28	+0.6/30
(1+50)	11.6/50 510.18	10.6/30 511.18	9.8/20 511.98	7.7/10 514.08	8.0/4 513.78	8.1 513.68	8.5/13 513.28	4.1/20 517.68	3.0/30 518.78
(1+00)	15.5/60 506.28	15.5/37 506.28	13.8/34 507.98	13.1/30 508.68	12.3 509.48	12.3/12 509.48	9.1/16 512.68	8.0/20 513.78	7.7/30 514.08
(0+50) 521.78	4.7/30 505.09	4.2/20 505.59	4.3/15 505.49	4.7/12 505.09	4.1 505.69	3.5/12 506.29	0.6/18 509.19	0.3/20 509.49	

509.79

		Lt.					℄				Rt.
4+40		515.25	517.85	518.95	520.75	521.55	522.25	523.95	525.05	527.15	
		16.6/50	14.0/30	12.9/23	11.1/10	10.3	9.6/13	7.9/14	6.8/20	4.7/30	
4+00		519.05	520.55	522.15	523.45	523.65	524.55	526.75	527.75		
		12.8/30	11.3/20	9.7/8	8.4/5	8.2	7.3/12	5.1/13	4.1/20		
3+77.39	= B.C. Lt.	517.35	520.25	523.95	525.15	525.15	526.05	528.15	529.45	530.75	
		14.5/50	11.6/30	7.9/8	6.7/5	6.7	5.8/12	3.7/13	2.4/20	1.1/30	
3+35		522.55	524.25	525.45	526.95	527.05	527.85	529.45	530.55	531.75	
		9.3/30	7.6/20	6.4/9	4.9/4	4.8	4.0/14	2.4/16	1.3/20	0.1/30	
3+02.60	= E.C.			522.15	524.45	526.45	527.25	528.85	530.45		
				9.7/30	7.4/15	5.4	4.6/13	3.0/20	1.4/30		
2+72.71	Mid curve	519.75	521.25	522.55	524.15	524.65	525.35	527.15	528.35		
		12.1/50	10.6/30	9.3/15	7.7/6	7.2	6.5/13	4.7/14	3.5/20		

531.85

Station					
6+64.72					
6+29.72	B.C. Rt.				
6+00					
T.P.	5.38	535.47	1.76	530.09	
	Pipe 20' Rt. of ℄ 5+69.46				
5+69.46	E.C.				
5+20					
4+80					
		531.85			

Lt. — ℄ — Rt.

535.47

Station										
6+64.72			521.07 14.4/30	524.07 11.4/15	526.37 9.1/5	526.77 8.7	527.27 8.2/13	529.27 6.2/14	530.47 5.0/20	
6+29.72		516.77 18.7/50	520.87 14.6/30	523.67 11.8/16	524.47 11.0/9	526.47 9.0	527.47 8.0/16	529.57 5.9/17	530.07 5.4/20	531.87 3.6/30
6+00	518.27 17.2/50	519.37 16.1/31	520.67 14.8/30	522.37 13.1/24	525.17 10.3/12	526.67 8.8	527.77 7.7/16	530.07 5.4/17	530.67 4.8/20	532.57 2.9/30
5+69.46	519.15 17.7/60	515.85 16.0/35	520.15 11.7/32	520.45 11.4/30	524.45 7.4/10	526.15 5.7	527.45 4.4/16	529.55 2.3/17	529.85 2.0/20	531.65 0.2/30
5+20				519.65 12.2/30	522.55 9.3/13	523.75 8.1	524.65 7.2/16	526.95 4.9/17	527.75 4.1/20	529.55 2.3/30
4+80				518.55 13.3/30	519.65 12.2/20	521.75 10.1	523.25 8.6/14	525.05 6.8/15	525.55 6.3/20	

9+00				
T.P.	8.59	550.12	1.55	541.53
8+50.83 E.C. pipe 20' Rt. ℄			1.55	
8+50.83	E.C.			
8+04.72				
7+69.72				
T.P.	7.68	543.08	0.07	535.40
7+34.72				
6+99.72				

535.47

Lt. ℄ Rt.

528.32 535.72 536.92 540.62 541.52 542.92 543.52 545.52 546.02 546.12

21.8/60 14.4/30 13.2/24 9.5/11 8.6/6 7.2 6.6/13 4.6/14 4.1/20 4.0/30

550.12

524.88 529.68 532.68 538.88 538.88 539.68 540.78 541.98 543.08

18.2/50 13.4/30 10.8/18 4.2/2 4.2 3.4/13 2.3/14 1.1/20 0.0/30

527.16 529.88 532.38 536.68 537.48 539.08 539.38 540.28

15.9/40 13.2/30 10.7/20 6.4 5.6/15 4.0/16 3.7/20 2.8/30

531.78 533.78 535.08 534.98 535.38 537.08 537.38

11.3/30 9.3/7 8.0/2 8.1 7.5/17 6.0/18 5.7/20

525.37 527.97 530.37 531.17 531.47 533.17 534.57 535.27

543.08

10.1/50 7.5/30 5.1/8 4.3 4.0/14 1.7/15 0.9/20 0.2/30

520.47 523.87 524.97 526.97 528.57 528.37 530.67 531.57

15.0/45 11.6/30 10.5/26 8.5/9 6.9/7 7.1 7.1/10 4.8/11 3.9/20

T.P.	4.58	561.25	2.35	556.67
11+40				
11+05				
10+70				
10+35				
10+02.34 = B.C. Rt.				
T.P.	10.01	559.02	1.11	549.01
9+50				
		550.12		

Lt. ℄ Rt.

Station						℄				
11+40	546.72	550.82	552.82	555.02		555.42	555.72	557.22	558.22	559.2 / 559.9
	12.3/50	8.2/30	6.2/20	4.0/12		3.6	3.3/6	1.8/8	0.8/12	+0.2/20, +0.9/30
11+05	548.62	550.32	551.22	552.62		553.12	553.22	555.22	557.82	559.6
	10.4/30	9.7/20	7.8/15	6.4/14		5.9	5.9/7	3.9/8	1.2/20	+0.6/30
10+70	543.22	546.02	548.02	548.62	550.42	551.12	551.32	554.12	556.12	548.02
	15.9/50	13.0/30	11.0/20	10.4/15	8.6/10	7.9	7.7/8	4.9/9	2.9/20	1.1/30
10+35	543.42	546.32	546.82	548.42	549.22	549.52	550.32	552.42	554.32	556.42
	15.6/30	13.7/20	12.2/13	10.6/9	9.8/5	9.5	8.7/11	6.6/12	4.7/20	2.6/30
10+02.34	537.02	541.52	543.72	546.22	547.92	548.32	549.52	551.22	552.42	554.92
	22.0/50	17.5/30	15.3/20	12.8/12	11.1/5	10.7	9.5/13	7.8/14	6.6/20	4.6/30
9+50	533.22	538.02	540.92	545.82		559.02 / 545.72	546.82	548.82	549.32	
	16.9/50	12.1/30	9.2/20	4.3/2		4.4	3.3/13	1.3/16	0.8/20	+0.6/30

orig B.M. =	Page 24 500.62		11.01	500.58	500.62
T.P.	1.25	511.59	13.26	510.34	
T.P.	0.50	523.60	12.96	523.10	
T.P.	0.86	536.06	12.67	535.20	
T.P.	0.71	547.87	12.45	547.16	
T.P. Iron Pin. 20' Rt. ℄ E.C. 12+71.39	3.38	559.61	5.02	556.23	B.M. #I

13+71.4 100' south. on Fwd. tangent.

12+71.39 End of curve.

12+35

12+00

11+86.97 P.R.C.

561.25

Lt. ℄ Rt

558.45

2.8

554.25 555.55 555.95 555.95 555.75 555.75 555.85 555.95 535.75

7.0/50 5.7/30 5.3/20 5.3/10 5.5/5 5.5 5.4/12 5.3/20 5.5/30

552.85 555.45 556.15 556.25 555.85 555.85 555.95 556.25 556.25

8.4/50 5.8/30 5.1/20 5.0/11 5.4/8 5.4 5.3/10 5.0/20 5.0/30

555.25 556.15 556.55 556.55 556.45 557.35 557.85 557.95

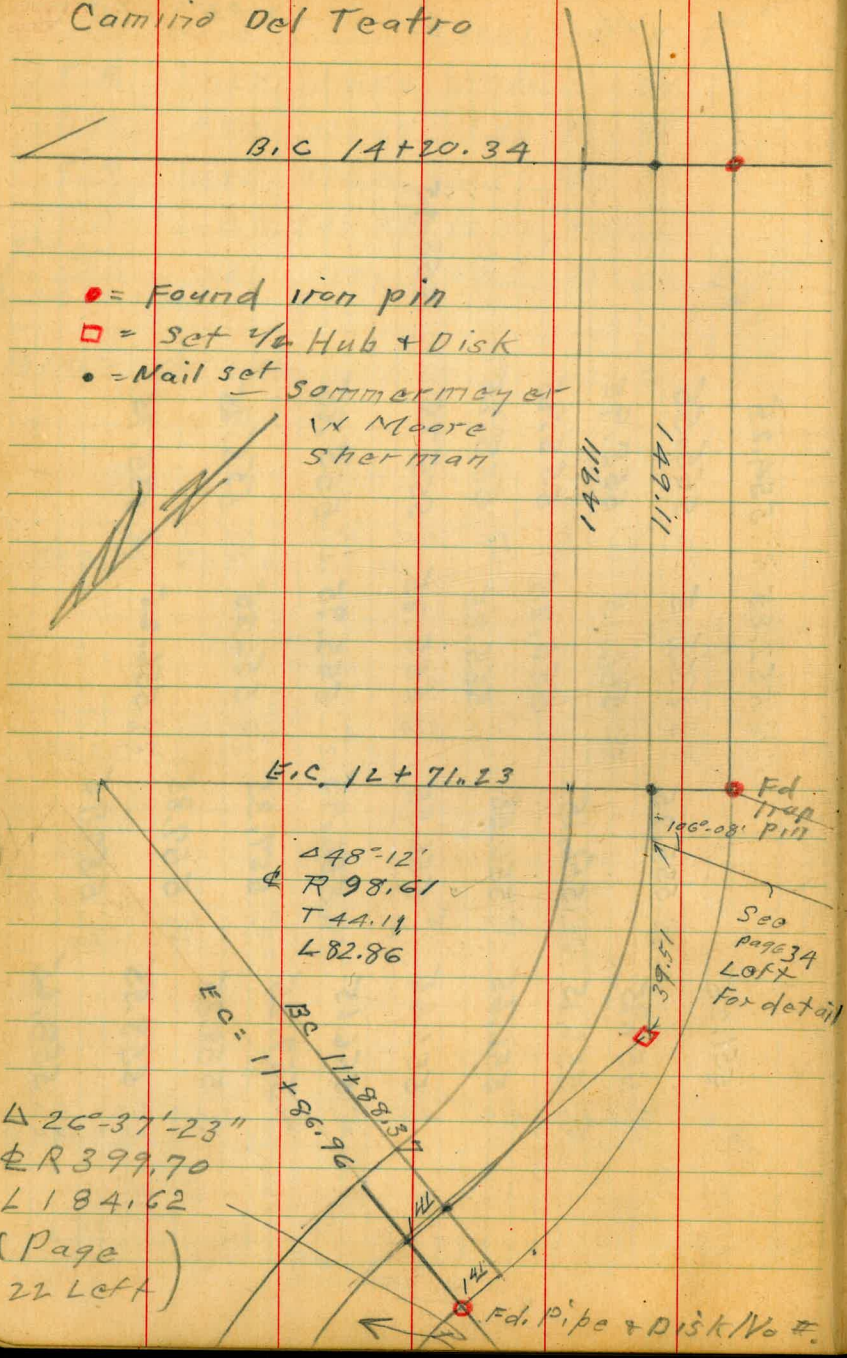
6.0/30 5.1/20 4.7/11 4.7 4.8/6 3.9/7 3.4/20 3.3/30

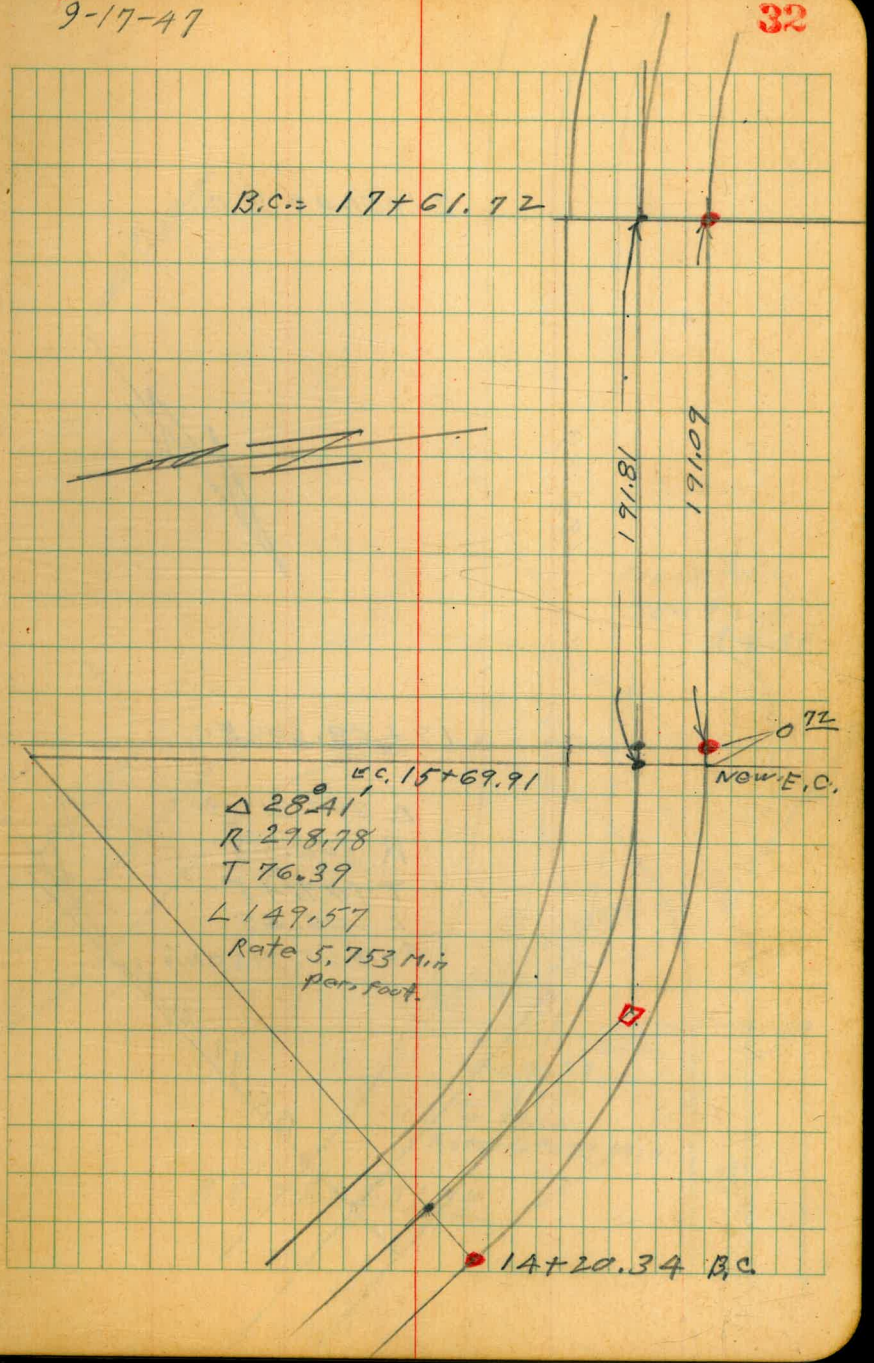
551.25 554.95 556.15 556.65 556.65 556.65 557.25 558.35 558.55 558.65

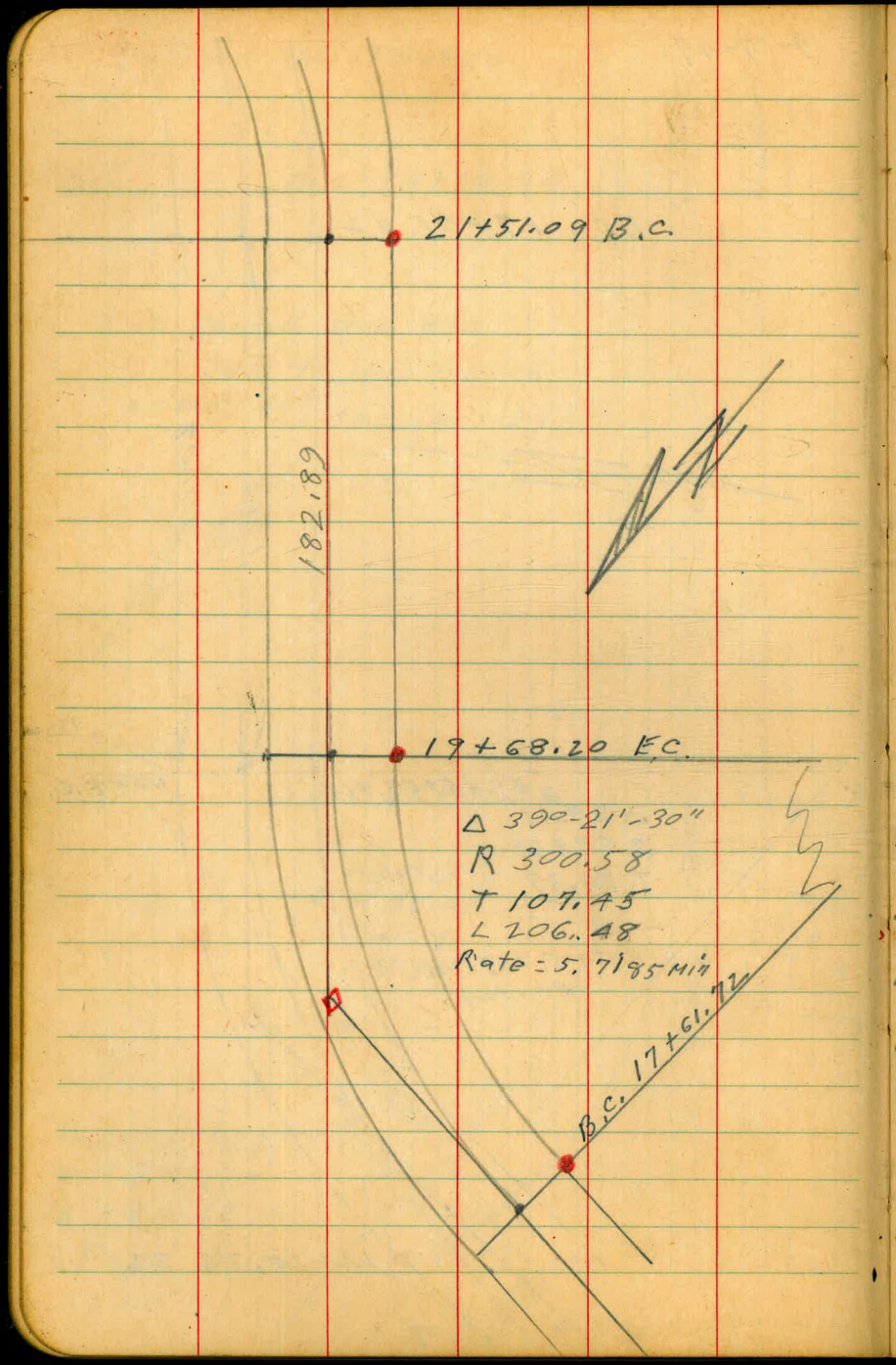
10.0/50 6.3/30 5.1/20 4.6/12 4.6 4.6/6 4.0/7 2.9/13 2.7/20 2.6/30

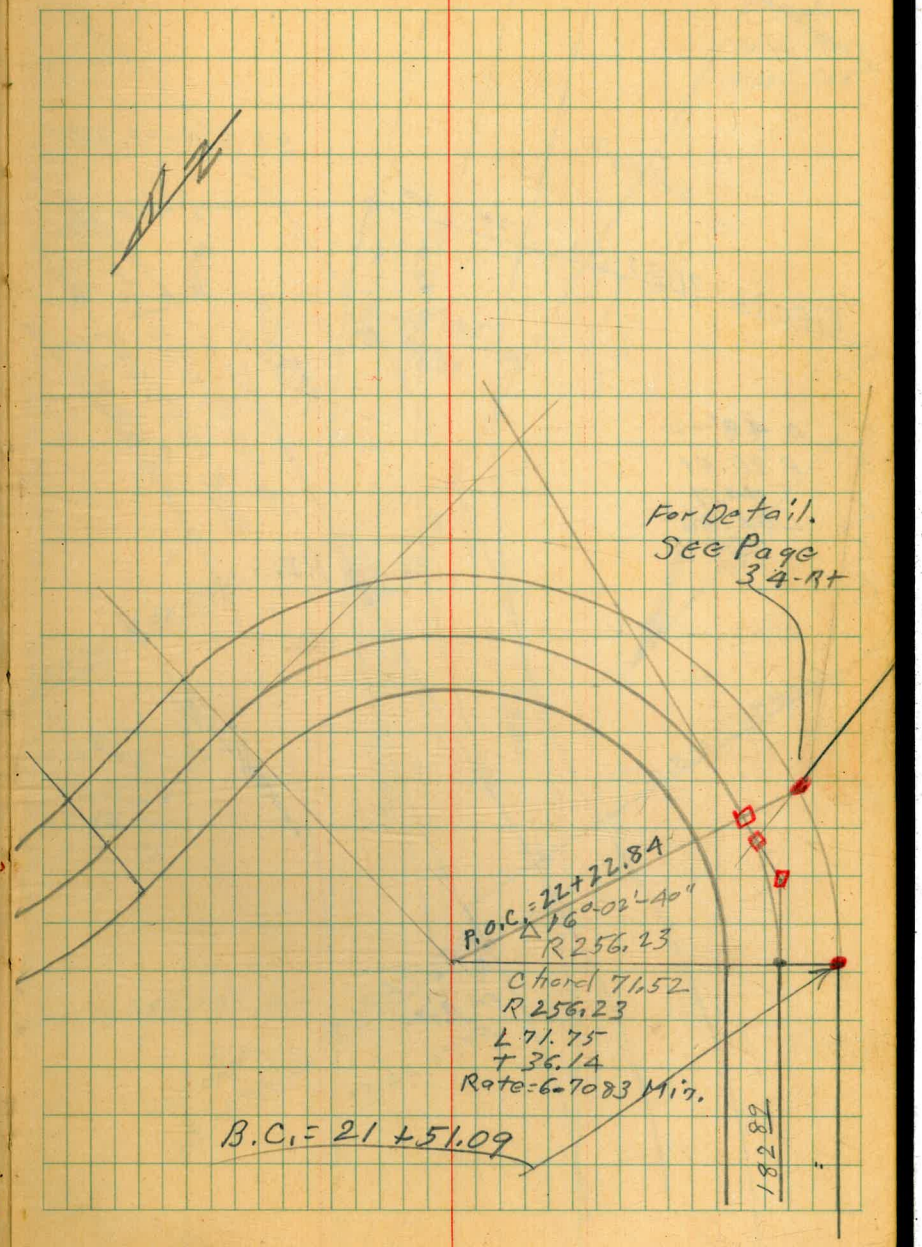
561.25

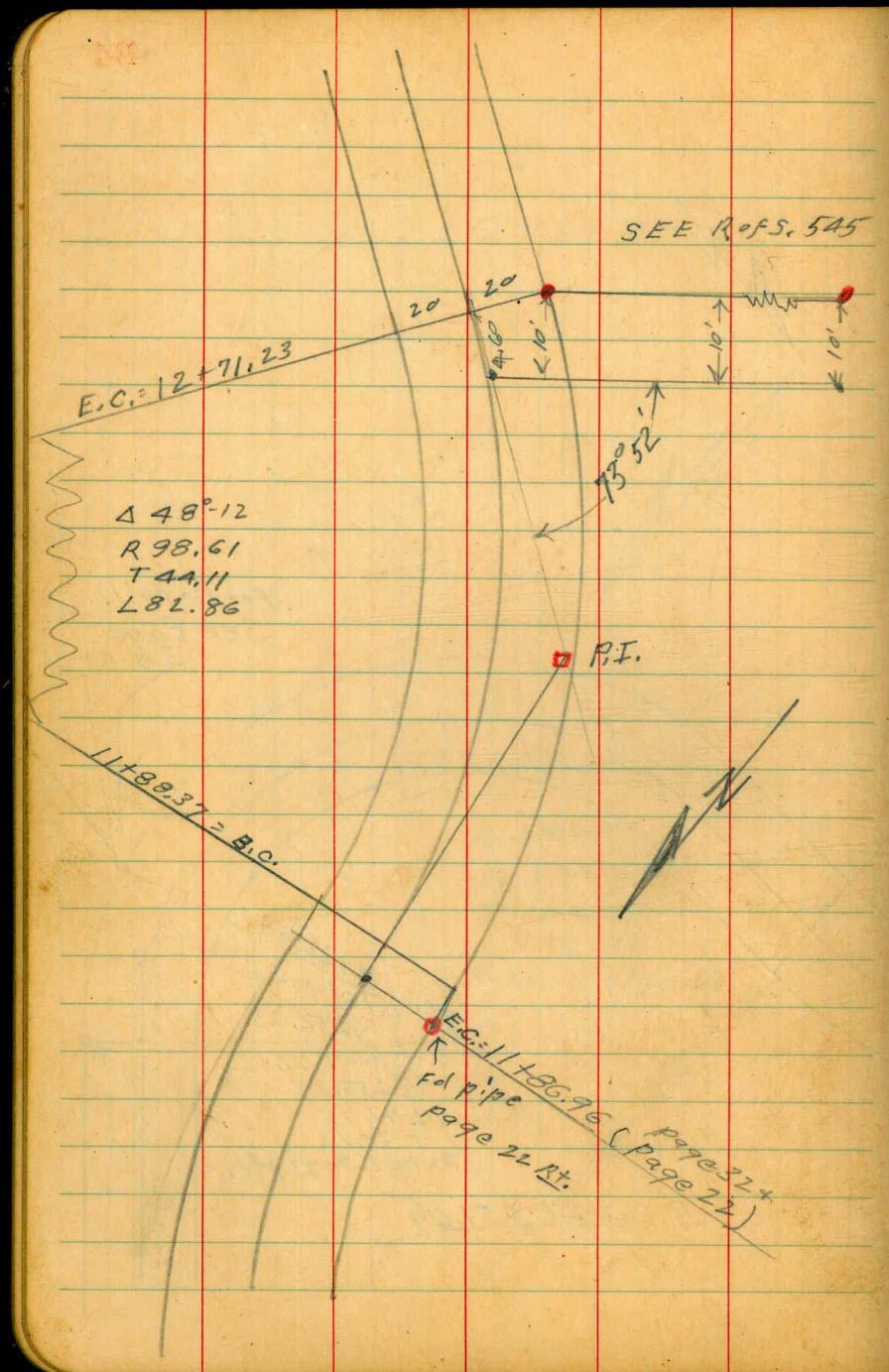
Camino Del Teatro

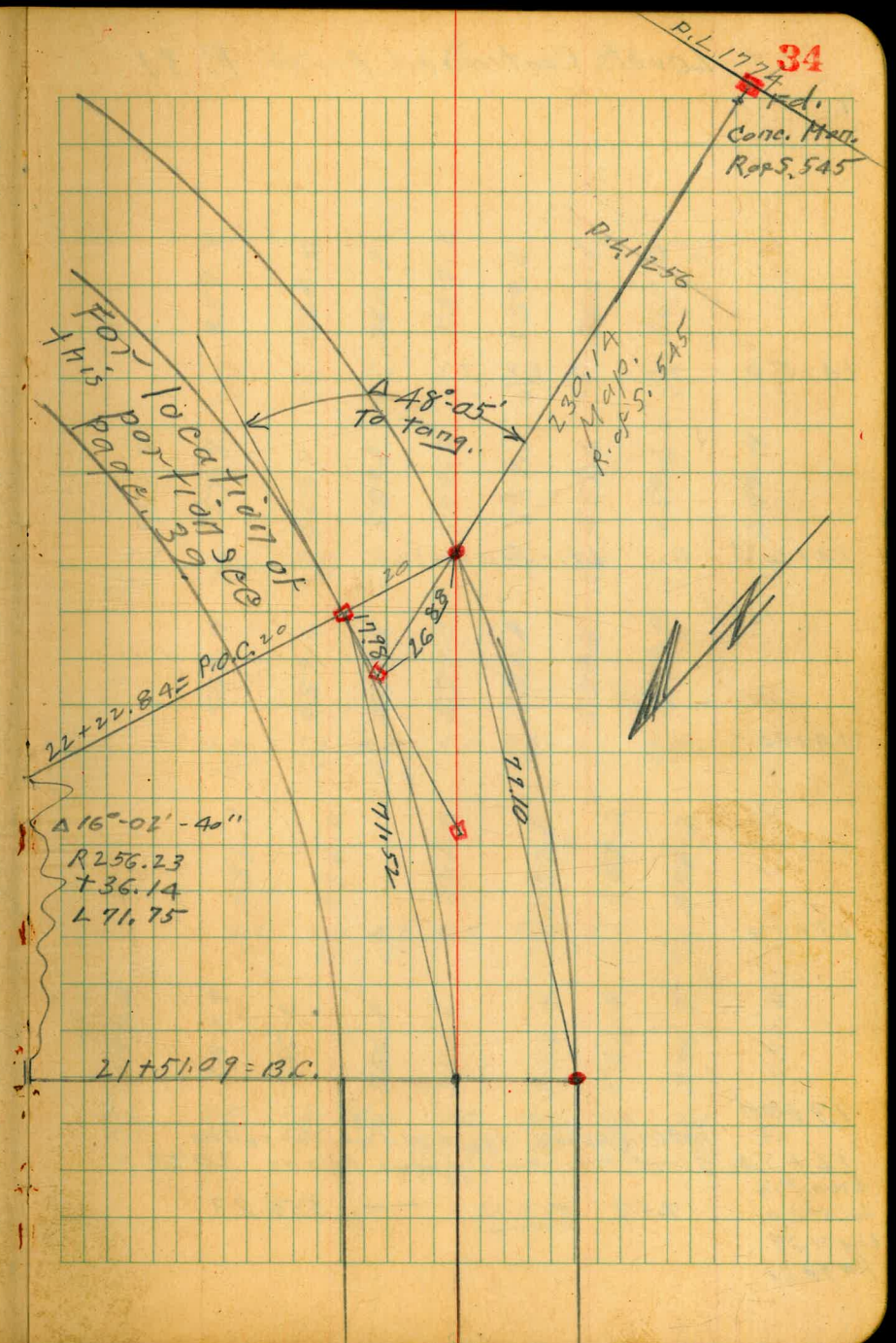





21+51.09 B.C.
182.89
19+68.20 E.C.
Δ 39°-21'-30"
R 300.58
T 107.45
L 206.48
Rate = 5.7185 Min
B.C. 17+61.72


For Detail
See Page
34-A+
P.O.C. = 22+22.84
Δ 16°-02'-40"
R 256.23
Chord 71.52
R 256.23
L 71.75
T 36.14
Rate = 6.7083 Min.
B.C. = 21+51.09
182.89


SEE R of S. 545
20
20
E.C.=12+71.23
4.60
10'
10'
10'
73°52'
Δ 48°-12
R 98.61
T 44.11
L 82.86
P.I.
11+88.37 = B.C.
E.C.=11+86.96 (page 32+ page 22)
Fd pipe page 22 Rt.


P.L. 1774
Fd. Conc. Mon. R of S. 545
P.L. 1256
230.14 Map. R of S. 545
Δ 48°-05' To tang.
For location of this portion see page 39.
20
17.98
26.88
22+22.84 = P.O.C. 20
Δ 16°-02'-40"
R 256.23
T 36.14
L 71.75
71.52
77.10
21+51.09 = B.C.

Levels Continued From P. 31

14+50					
14+20 34 = B.C Lt. - (Page 32)					
14+00					
13+50					
13+00					
12+74	19' Rt. (Aprox) Start old wire fence Start row Eucalyptus trees 20' Rt.				
Iron Pin 20' Rt. E.C. 12+71.39 Page 31	7.19	563.42	—	556.23	

Lt. ℄ Rt.

	559.9	560.0	560.1	559.6	559.6	560.1	560.2	
	3.5/30	3.4/20	3.3/8	3.8	3.8/8	3.3/9	3.2/20	
558.4	559.4	559.9	559.8	559.2	559.1	559.6	559.6	559.4
5.0/50	4.0/30	3.5/20	3.6/6	4.2	4.3/9	3.8/10	3.8/20	4.0/30
	559.4	559.6	559.4	559.0	558.8	559.3	559.4	
	4.0/30	3.8/20	4.0/7	4.4	4.6/11	4.1/12	4.0/20	
	558.1	558.2		558.0	557.8	558.2	558.2	
	5.3/30	5.2/20	4.9/5	5.4	5.6/10	5.2/11	5.2/20	
554.2	557.9	556.6	556.8	556.4	556.4	556.8	556.9	557.0
9.2/50	7.5/30	6.8/20	6.6/6	7.0	7.0/11	6.6/12	6.5/20	6.4/30
				563.42				

Camino Del Teatro

17+00				
16+50				
16+00				
15+69.91 = E.C.				
15+35				
T.P.	10.76	573.71	0.47	562.95
15+00		563.42		

	Lt.		℄		Rt.				
	556.7	560.6	563.8	567.3	569.0	569.9	571.5	573.0	
	17.0/50	13.1/30	9.9/20	6.4/3	4.7	3.8/19	2.2/15	0.7/20	
	555.2	561.6	564.0	567.4	568.6	569.6	570.9	572.1	573.2
	18.5/50	12.1/30	9.7/20	6.3/3	5.1	4.1/16	2.8/17	1.6/20	0.5/30
	560.7	562.4	564.0	565.5	566.2	566.4	567.3	568.1	569.1
	13.0/40	11.3/30	9.7/20	8.2/4	7.5/2	7.3	6.4/15	5.6/16	4.6/20
	560.1	562.3	563.4	564.2	564.9	564.7	565.5	566.4	567.1	567.7
	13.5/50	11.4/30	10.3/20	9.5/6	8.8/4	8.8	8.2/15	7.3/16	6.6/20	6.0/30
		561.5	562.3	563.0		563.0	563.3	563.6	564.5	565.0
		12.2/30	11.4/20	10.7/7	523.71	10.7	10.4/13	10.1/19	9.2/20	8.7/30
	559.6	561.0	561.4	561.4		561.1	561.3	561.7	562.0	562.3
	3.8/50	2.4/30	2.0/20	2.0/9		2.3	2.1/9	1.7/11	1.4/20	1.1/30
					563.42					

$19+68^{20}$	E.C.				
19+35					
19+00					
18+50					
18+00					
T. P.	5.71	576.36	3.06	570.65	
$17+61^{72}$	= B.C.	Rt.			
		573.71			

Station	Lt.	℄	Rt.
$19+68^{20}$	567.8 (8.6/50); 570.1 (6.3/30); 570.8 (5.6/20); 570.9 (5.5/10)	571.2 (5.2)	571.4 (5.0/11); 572.2 (4.2/12); 572.9 (3.5/20); 572.9 (3.5/30)
19+35	570.2 (6.2/50); 571.1 (5.3/30); 571.4 (5.0/20); 571.2 (5.2/8)	571.3 (5.1)	571.5 (4.9/11); 571.8 (4.6/12); 572.5 (3.9/20); 573.2 (3.2/30)
19+00	571.2 (5.2/30); 571.3 (5.1/20); 571.3 (5.1/7)	571.6 (4.8)	571.5 (4.9/13); 572.1 (4.3/14); 572.9 (3.5/20); 573.8 (2.6/30)
18+50	569.4 (7.0/50); 571.1 (5.3/30); 571.5 (4.9/20); 572.0 (4.4/7)	572.4 (4.0)	572.2 (4.2/13); 573.0 (3.4/14); 573.7 (2.7/20); 573.2 (3.2/30); 573.9 (2.5/50)
18+00	563.8 (12.6/50); 567.8 (8.6/30); 569.8 (6.6/20); 571.6 (4.8/5)	572.2 (4.2)	572.4 (4.0/13); 573.0 (3.4/15); 574.0 (2.4/20); 574.0 (2.4/30)
		576.36	
$17+61^{72}$	559.8 (13.9/50); 563.5 (10.2/30); 565.5 (8.2/10); 569.5 (4.2/4); 570.6 (3.1/2)	570.7 (3.0)	571.1 (2.6/14); 572.3 (1.4/15); 573.7 (0.0/20); 574.5 (+1.2/30)

573.71

Camino Del Teatro

Station					
~~E.R.~~ ℄ Hub 22+22.84	S.S.		5.23	570.72	Set B.M.

20⁵ Rt. = End Eucalyptus trees.

22+22⁸⁴ = P.O.C. (See page 34 Rt)

19⁵ Rt. = End wire fence

21+86⁹⁶ Mid. Curve

E.R. = edge of traveled road

21+51⁰⁹ = B.C. Lt. ("E.R." = edge of road)

21+00

T.P.	4.75	575.95	5.16	571.20

20+50

20+00

576.36

Station										
22+22.84	569.0 (6.9/50)	570.0 (5.9/35 E.R.)	570.0 (5.9/17 ER)	570.4 (5.5/15)	570.7 (5.2)	571.1 (4.8/20)				
21+86.96	568.1 (7.8/50)	570.0 (5.9/30)	570.0 (5.9/28 E.R.)	570.2 (5.7/10 ER)	570.7 (5.2)	571.4 (4.5/20)	571.5 (4.4/30)			
21+51.09	565.9 (10.0/50)	568.3 (7.6/30)	569.6 (6.3/20)	570.1 (5.8/18 ER)	570.7 (5.2 Edge Road)	571.1 (4.8/2)	571.8 (4.1/20)	571.9 (4.0/30)		
21+00	563.6 (12.3/50)	567.2 (8.7/30)	569.4 (6.5/20)	570.3 (5.6/13)	570.6 (5.3/10)	570.9 (5.0)	571.3 (4.6/6)	571.6 (4.3/7)	571.9 (4.0/20)	572.4 (3.5/30)
20+50	563.4 (13.0/50)	568.0 (8.4/30)	570.8 (6.6/20)	570.4 (6.0/12)	571.0 (5.4/10)	571.0 (5.4)	571.2 (5.2/7)	571.7 (4.7/8)	572.9 (3.5/20)	573.3 (3.1/30)
20+00	566.3 (10.1/50)	569.4 (7.0/30)	570.6 (5.8/20)	570.7 (5.7/11)	571.2 (5.2/9)	571.1 (5.3)	571.2 (5.2/10)	572.1 (4.3/11)	572.7 (3.7/20)	

575.95

	Azimuth	Dist	Level Reading Rod	EL.	
B=BC.	41°-51'Lt.	325	6.1		
P.O.C. A	42°-30'Lt	152	4.4		
At △#2	Set 180° on △#1 = 0°-00' Forward				
△#2: Rod 5 =		574.2		569.2	
E.C.	52°-43'	360	5.8	569.2	= △#2
P.O.C.	43°-34'Lt.	293	6.0		
P.O.C.	30°-34'Lt	201	6.5		
P.O.C.	25°-16'Lt	118	6.6		
P.O.C.	90°	23	5.7		
△#1	4.87	575.00		570.72	

0°-0' = Forward tang.

Transit at P.O.C. 22+22.84 Azimuth

Going on from sta 22+22.84 undedicated traveled road. on aprox. ℄ of 16' to 18' wide Above are stadia shots ↑

T.P.- Orig BM. Pg 35			7.63	556.22	556.23
T.P.	2.76	563.85	11.54	561.09	
T.P.	0.58	572.63	3.90	572.05	
		575.95			

the same elevation. shifted south at Aprox. at canyon ℄ can be This road follows S'ly. rim road.

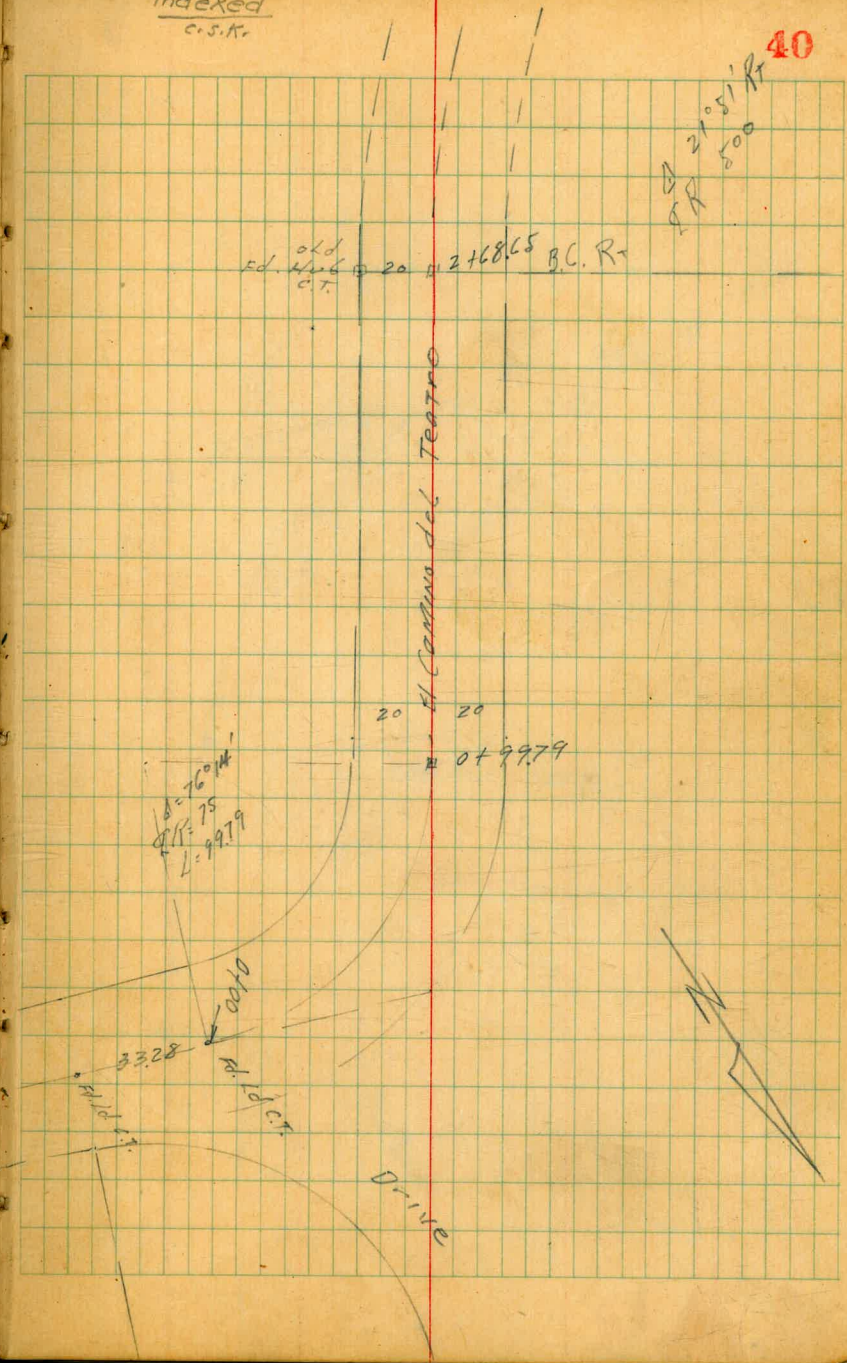
"E" = Junction with main soledad

"E"	16°-45'Lt	690	11.2	
Aprox EL D	31°-28'Lt	500	6.3	
"C"	39°-00'Lt.	420	7.1	

π=574.2

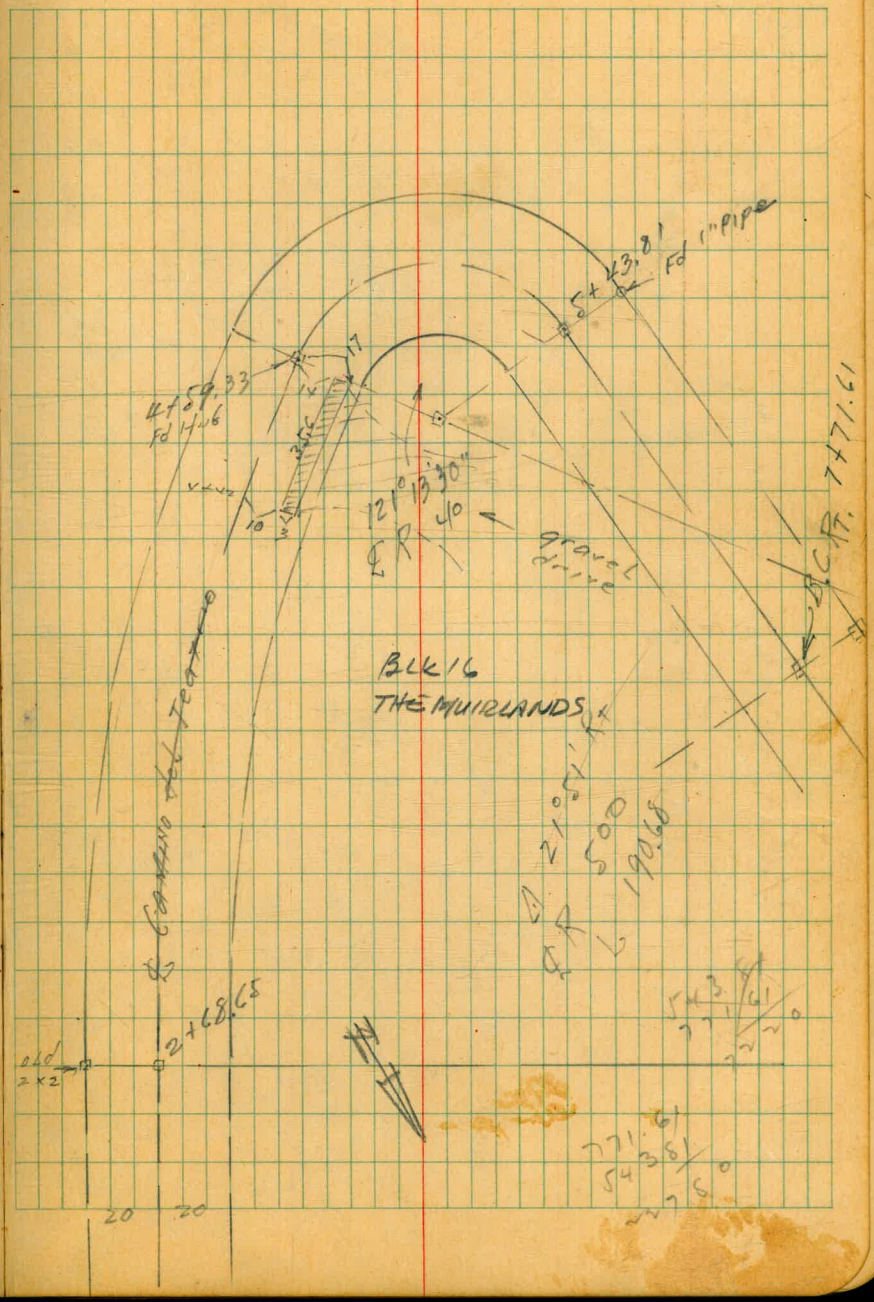
Xsec El Camino del Teatro
Muirlands Dr. to Muirlands Dr.
Wly side Blk 16, The Muirlands

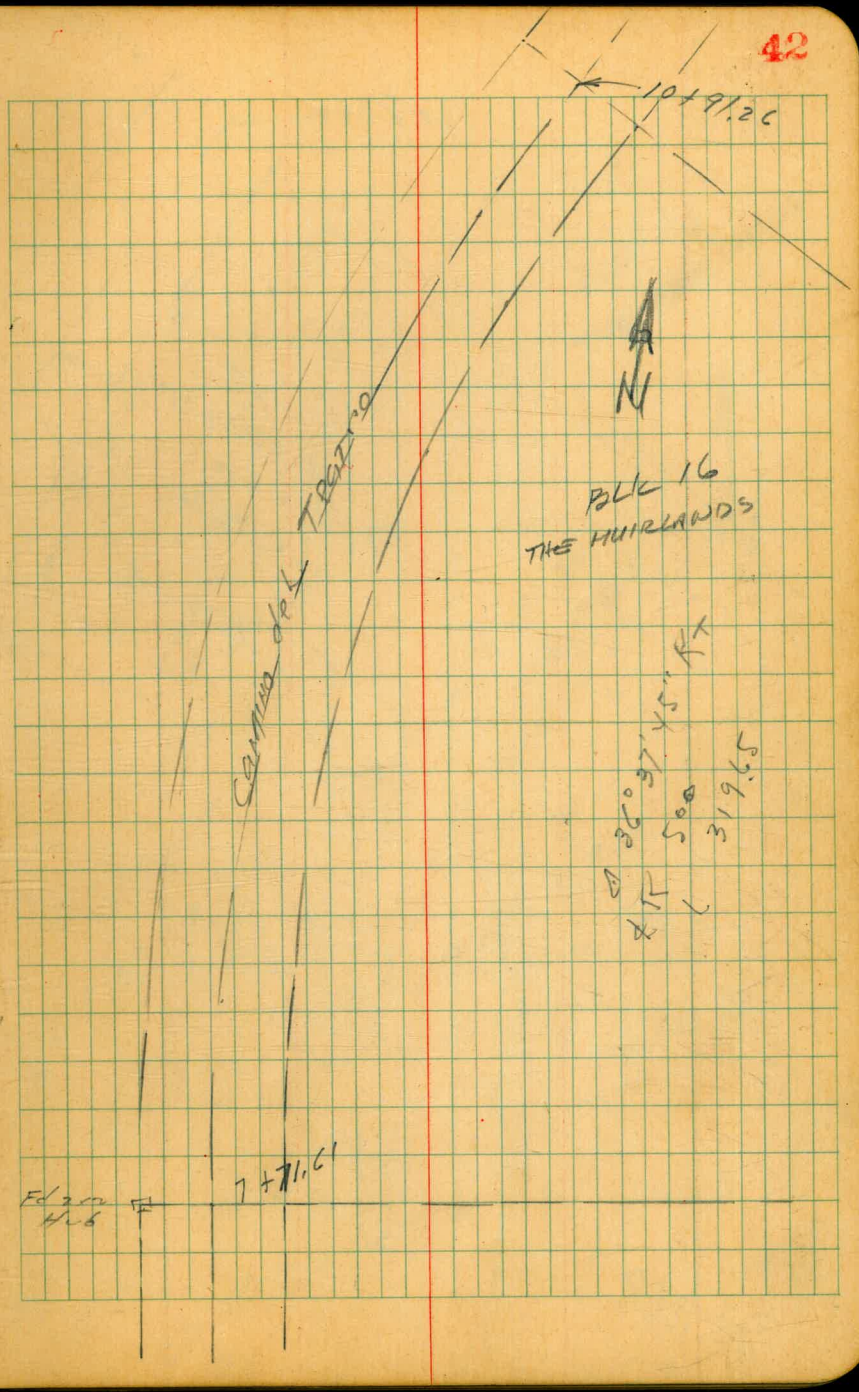
Indexed
C.S.K.

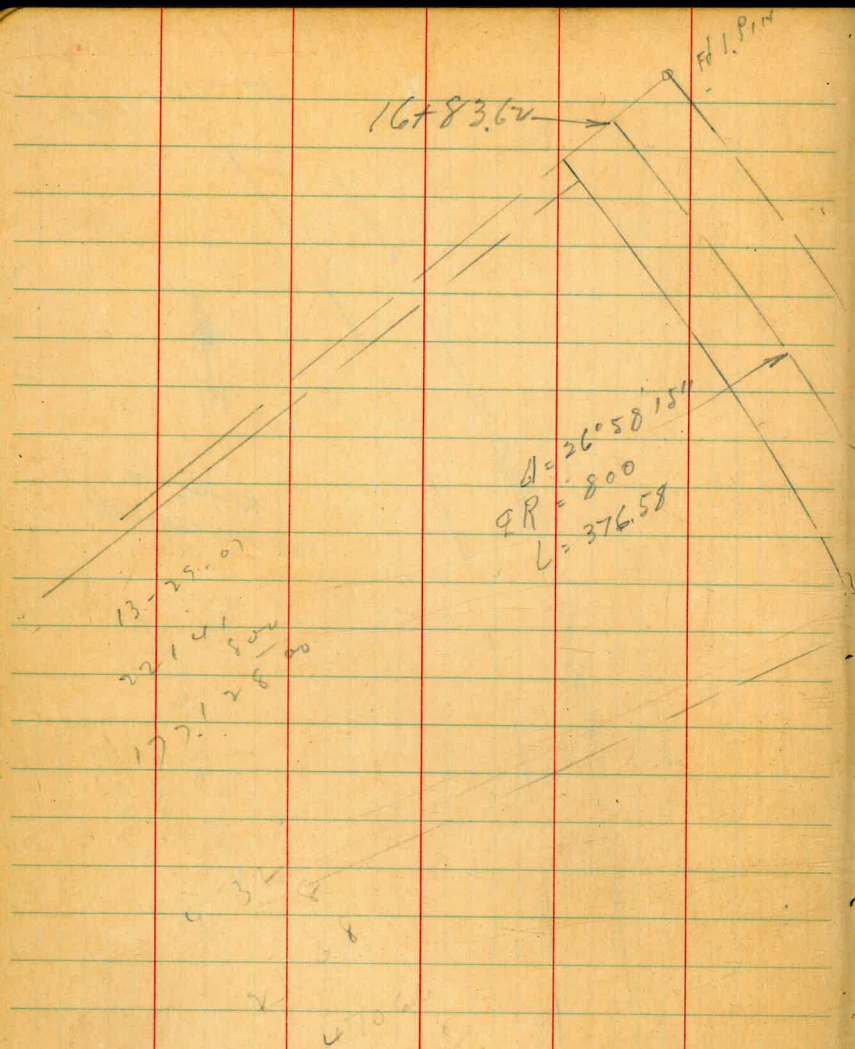


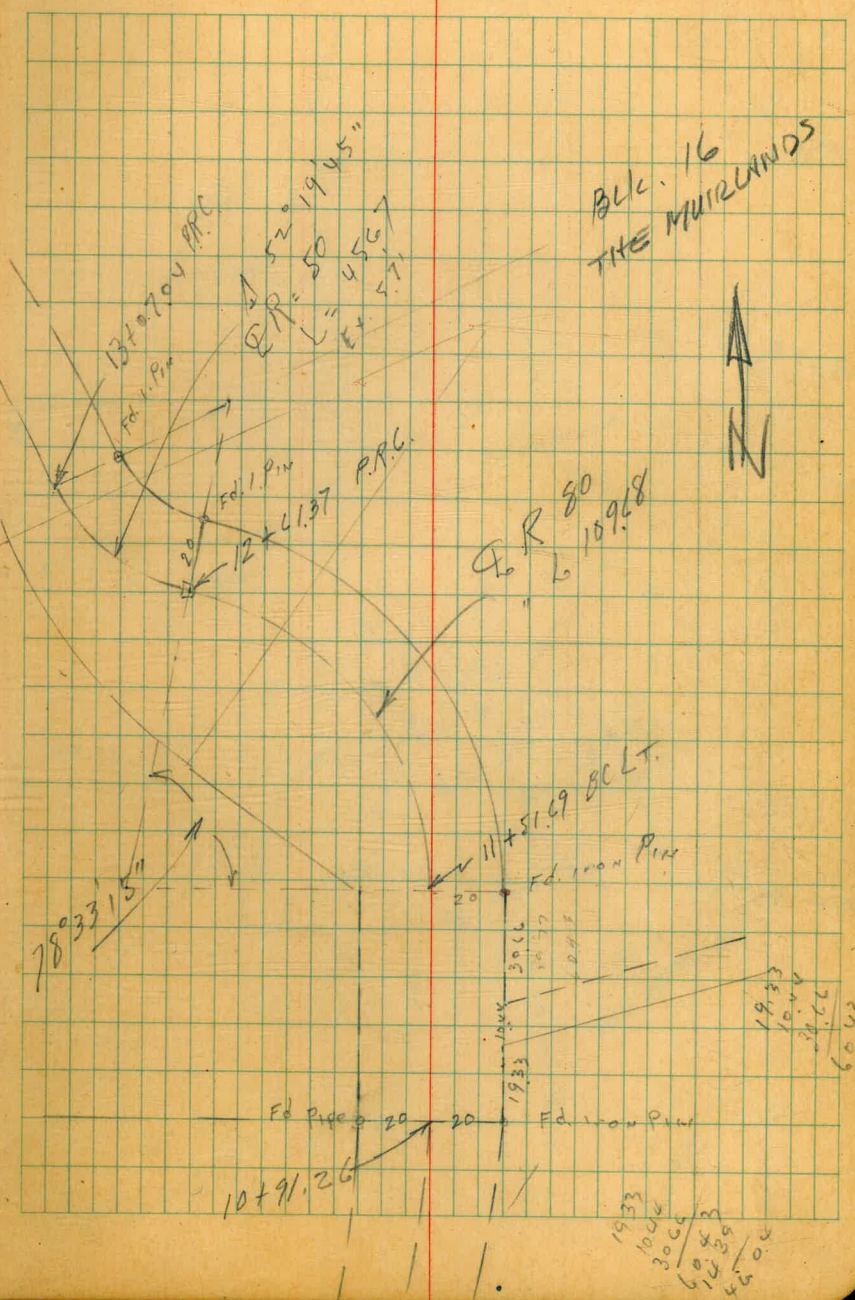
LA CUMBRA
DR

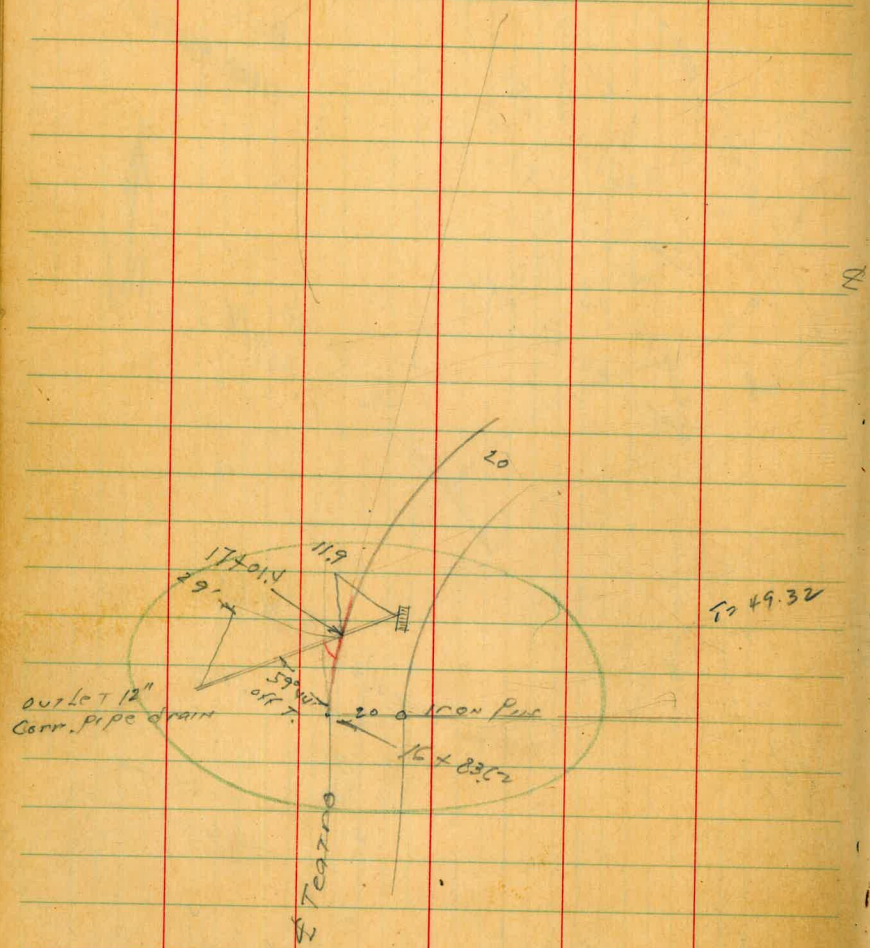
189.76
20
12.48
543.81
766.04

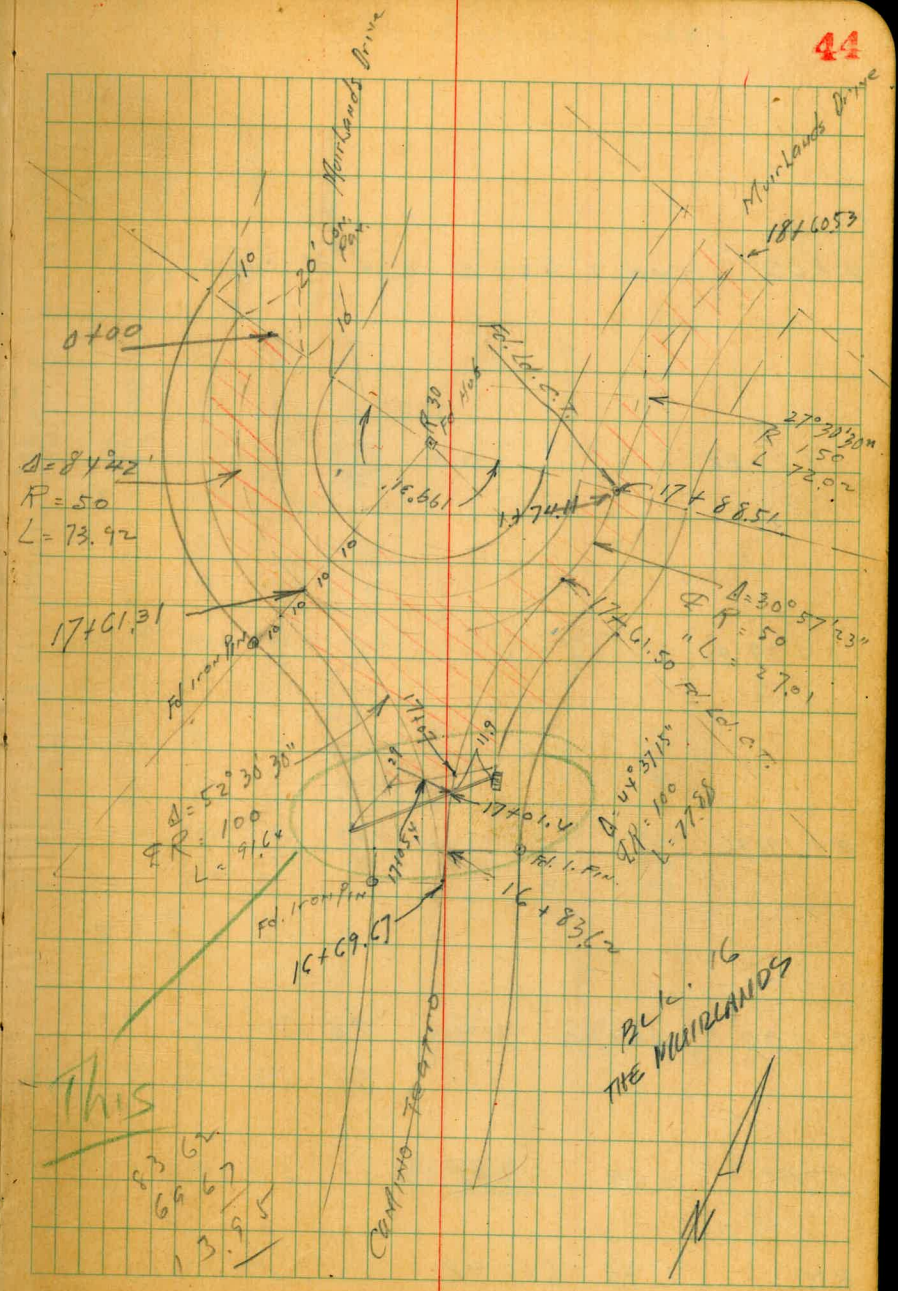



10+91.26
N
BLK 16
THE HUIRLANDS
Camino del Tranco
7+71.61


16+83.62
Fd I. Pin
Δ = 26°58'15"
℄R = 800
L = 376.58


BLK. 16
THE MUIRLANDS
N
13+07.04 P.R.C.
Δ 52°19'45"
℄R = 50
L = 45.67
Fd. I. Pin
12+41.37 P.R.C.
℄R 80
L 109.68
11+51.69 BC LT.
Fd. Iron Pin
78°33'15"
Fd Pipe
Fd. Iron Pin
10+91.26


20
17+01.4
11.9
29'
59°44'
off T.
20 Iron Pin
16+83.62
Outlet 12"
Corr. Pipe drain
℄ Teatro
T = 49.32


Muirlands Drive
Muirlands Drive
18+60.53
0+00
20' Con. Pan.
10
Fd. Ld. C.T.
R 30
Fd. Hub
27°30'30"
R 150
L 72.02
Δ = 84°42'
℄ R = 50
L = 73.92
16.661
1+74.11
17+88.51
Δ = 30°57'23"
℄ R = 50
L = 27.01
17+61.31
Fd. Iron Pin
17+61.50 Fd. Ld. C.T.
17+07
11.9
Δ = 52°30'30"
℄ R = 100
L = 91.64
17+01.4
Δ = 44°37'15"
℄ R = 100
L = 77.88
Fd. I. Pin
Fd. Iron Pin
16+69.67
16+83.62
Camino Teatro
Blk. 16
THE MUIRLANDS
This
83.62
69.67
13.95

Xsec. Camino del Teatro

0+66	end 2' Con gut. + 3" curb			
0+59.88				
0+39.92				
0+19.96				
0+00	Sketch p 40 B.C. LT.			
T.P.	3.69	514.98	0.69	511.29
B.M. P.24	11.36	511.98		500.62

Lt ℄ Rt

508.69	508.42	508.34	508.48				
6.29 / 9.8 3" cb	6.56 / 9.8 gut	6.64 / 8 gut	6.50 / 7 gut				
512.2	509.29	509.03	508.93	509.08	509.00	509.5	
2.9 / 20	5.69 / 10 3" cb	5.95 / 10 gut	6.05 / 8.8	5.90 / 7.8 gut.	6.0	5.5 / 20	
513.6	511.12	510.90	510.71	510.78	510.9	511.5	
1.4 / 20 Lawn	3.86 / 12 3" cb	4.08 / 12 gt	4.27 / 11 gut	4.20 / 10 edge con. gut.	4.1	3.5 / 20	
516.0	512.58	512.28	512.16	512.32	512.57	512.67	512.32
+1.0 / 20 Lawn	2.40 / 12 3" curb	2.70 / 12 gut	2.82 / 11 gut	2.66 / 10 edge pav	2.41 P	2.31 / 12 pav	2.66 / 20 pav
514.98	513.58	513.39	513.44	513.69	513.25	513.6	
0.0 / 20 on Brick drive	1.40 / 12 edge gut	1.59 / 10.6 in gut	1.54 / 10 edge pav	1.29 pav.	1.73 / 17.7 edge pav	1.4 / 20	

514.98

2+68.65 BC Rt				
T.P.	1.66	494.63	13.03	492.97
2+50				
2+00				
T.P.	0.90	506.00	9.88	505.10
1+50				
0+99.79 E.C.				
0+79.84				
		514.98		

Lt				℄			Rt
		$\frac{0.1}{20}$ 494.5	$\frac{3.5}{16}$ 491.1	3.0 491.6	$\frac{2.9}{12}$ 491.7	$\frac{5.6}{20}$ 489.0	$\frac{8.3}{25}$ 486.3
	$\frac{9.8}{20}$ 496.2	$\frac{9.9}{18}$ 496.1	$\frac{13.0}{15}$ 493.0	494.63 12.9 493.1	$\frac{12.7}{13}$ 493.3	$\frac{16.1}{20}$ 489.9	$\frac{16.9}{25}$ 489.1
	$\frac{5.0}{20}$ 501.0	$\frac{5.7}{16}$ 500.7	$\frac{9.0}{15}$ 497.0	8.8 497.2	$\frac{8.0}{15}$ 498.0	$\frac{9.3}{20}$ 496.7	$\frac{10.2}{25}$ 495.8
		$\frac{7.8}{20}$ 507.2	$\frac{13.3}{12}$ 501.7	506.00 13.3 501.7	$\frac{13.3}{17}$ 501.7	$\frac{13.6}{20}$ 501.4	$\frac{14.2}{25}$ 500.8
$\frac{4.4}{20}$ 510.6	$\frac{7.0}{13}$ 508.0	$\frac{8.8}{12}$ 506.2	$\frac{9.4}{8}$ 505.6	9.3 505.7	$\frac{9.6}{20}$ 505.4		
	$\frac{3.9}{20}$ 511.1	$\frac{6.0}{13}$ 509.0	$\frac{7.5}{10}$ 507.5	7.7 507.3	$\frac{7.2}{20}$ 507.8		
				514.98			

4+59.33	P.C.C.			
4+42	℄ gravel drive			
4+22.7	Beg. Con. gutter			
4+11.66				
T.P.	0.96	483.02	12.57	482.06
3+63.99				
3+16.32				
		494.63		

Lt ℄ Rt

479.1	475.5	475.5	476.9	476.0	474.45	474.3	474.45	474.6	474.8
3.9 / 20	7.5 / 15	7.5 / 10	6.1 / 9	7.0	8.57 / 14	8.70 / 15.5	8.57 / 17	8.4 / 20	8.2 / 25
						gutter			
					476.17	476.04	476.16	476.1	476.4
					6.85 / 11.6	6.98 / 13.1	6.86 / 14.6	6.9 / 20	6.6 / 30
					477.69	477.48	477.65		
					5.33 / 10	5.54 / 11.5	5.37 / 13		
		483.2	479.5	479.5	479.0	478.6	477.6	477.5	
		+ 0.2 / 20	3.5 / 12	3.5	4.0 / 9	4.4 / 12	5.4 / 20	5.5 / 25	
								Ivy Lawn	
486.33	486.8	483.0	483.6	483.02	482.9	483.4	482.4	478.5	
8.3 / 28	7.8 / 20	11.6 / 17	11.0		11.7 / 10	11.2 / 16	12.2 / 20	16.1 / 30	
	491.2	487.9	487.4		486.8	484.33	479.3		
	3.4 / 20	6.7 / 16	7.2		7.8 / 14	10.3 / 20	15.3 / 30		
			494.63						

T.P.	0.59	460.42	12.24	459.83
6+50				
6				
T.P.	0.74	472.07	11.69	471.33
5+43.81	E.C.			
5+22.69				
5+01.57				
4+80.45				
		483.02		

Lt				℄	Rt		
	452.6 19.5/30	456.3 15.8/20	460.3 11.8/14	460.3 11.8	459.7 12.4/13	461.9 10.2/14	465.6 6.5/20
457.8 14.3/30	461.3 10.8/20	462.3 9.8/17	465.2 6.9/14	464.9 7.2	464.5 7.6/13	468.5 3.6/18	468.5 3.6/20
				472.07			
465.1 17.9/25	466.7 16.3/20	470.3 12.7/16	471.0 12.0/12	469.8 13.2	469.0 14.0/15	471.0 12.0/20	472.5 10.5/25
	468.7 14.3/25	469.7 13.3/20	472.9 10.1/11	471.8 11.2	469.7 13.3/16	471.2 11.8/20	472.6 10.4/25
	470.2 12.8/27	471.9 11.1/20	474.1 8.9/13	473.2 9.8	471.3 11.7/17	472.4 10.6/20	473.1 9.9/25
476.1 6.9/34	476.8 6.2/20	474.4 8.6/15	475.9 7.1/10	474.7 8.3	472.5 10.5/15	473.1 9.9/20	473.7 9.3/25
				483.02			

Station				
9+31.42				
T.P.	0.65	436.85	12.51	436.20
8+78.15				
		Note! Last outs on Rt. = Top cut		
8+24.88				
T.P.	0.77	448.71	12.48 ~~12.49~~	447.94 ~~447.93~~
7+71.61	BC Rt			
7+50				
7+00				
		460.42		

Lt				℄	Rt		
425.9	429.6	434.1	435.5	435.7	435.8	439.6	447.1
11.0/35	7.3/26	2.8/20	1.4/19	1.2	1.1/14	+2.7/20	+10.2/29
				436.85			
429.4	433.1	437.8	440.4	440.2	439.7	445.2	448.7
19.3/35	15.6/27	10.9/20	8.3/17	8.5	9.0/14	3.5/20	0.0/25
	434.9	441.6	445.7	445.0	443.9	448.7	452.1
	13.8/35	7.1/20	3.0/14	3.7	4.8/16	0.0/20	+3.4/22
				448.71			
443.2	446.2	450.6		449.8	449.1	456.0	
17.2/30	14.2/20	9.8/12		10.6	11.3/15	4.4/20	
445.6	448.4	448.8	452.1	451.7	451.2	455.7	456.4
14.8/30	12.0/20	11.6/18	8.3/13	8.7	9.2/13	4.7/18	4.0/20
448.5	452.0	455.7		455.7	455.3	461.6	462.3
11.9/30	8.4/20	4.7/13		4.7	5.1/13	+1.2/20	+1.9/26
				460.42			

Station						
11+79.11						
11+51.69 BC Lt						
11+21						
10+91.2 C = EC.						
T.P.	1.17	425.50	12.52	424.33		
10+37.98						
9+84.7						
		436.85				

Lt			℄			Rt
	411.8 $\frac{13.7}{50}$	414.1 $\frac{11.4}{27}$	415.2 10.3	415.3 $\frac{10.2}{7}$	426.5 $\frac{+1.0}{20}$	429.0 $\frac{+3.5}{25}$
410.9 $\frac{14.6}{50}$	413.6 $\frac{11.9}{30}$	417.5 $\frac{8.0}{24}$	417.7 7.8	417.5 $\frac{8.0}{11}$		429.7 $\frac{+4.2}{20}$
	410.2 $\frac{15.3}{50}$	414.3 $\frac{11.2}{25}$	420.1 $\frac{5.4}{17}$	419.8 5.7	419.5 $\frac{6.0}{14}$	424.5 $\frac{1.0}{20}$	432.0 $\frac{+6.5}{30}$
	413.4 $\frac{12.1}{35}$	418.0 $\frac{7.5}{20}$	422.6 $\frac{2.9}{14}$	422.1 3.4	421.5 $\frac{4.0}{15}$	423.91 $\frac{1.59}{20}$ IRON PIN	434.2 $\frac{+8.7}{29}$
	415.7 $\frac{21.2}{35}$	423.3 $\frac{13.6}{20}$	427.8 $\frac{9.1}{15}$	425.50 426.7 10.2	426.1 $\frac{10.8}{13}$	428.2 $\frac{8.7}{14}$	431.5 $\frac{5.4}{20}$	437.9 $\frac{+1.0}{28}$
420.8 $\frac{16.1}{35}$	426.3 $\frac{10.6}{25}$	429.3 $\frac{7.6}{20}$	431.3 $\frac{5.6}{17}$	431.3 5.6	430.8 $\frac{6.1}{13}$	437.9 $\frac{+1.0}{20}$	441.2 $\frac{+4.3}{24}$
			436.85			

13+44.7				
13+07.04 P.R.C.				
12+84.7				
12+61.37 P.R.C.				
12+33.95				
T.P.	1.00	413.54	12.96	412.54
12+06.53				
		425.50		

Lt			℄			Rt
396.4 17.1/35	400.7 12.8/20	403.8 9.7/14	403.6 9.9	402.9 10.6/15	408.0 5.5/20	411.9 2.1/25
398.2 15.3/35	402.5 11.0/20	407.1 6.4/12	406.7 6.8	405.9 7.6/14	410.2 3.3/20	414.5 +1.0/24
399.7 13.8/40	402.1 10.4/25	408.7 4.8/15	408.5 5.0	407.8 5.7/17	413.8 +0.3/20	415.3 +1.8/23
400.7 12.8/50	402.5 11.0/39	409.5 4.0/26	410.0 3.5	410.0 3.5/12	417.5 +4.0/18	418.0 +4.5/20
	404.5 9.0/50	411.2 2.3/34	411.5 2.0	411.7 1.8/6	420.5 +7.0/18	420.8 +7.3/20
			413.54			
406.5 19.0/50		412.5 13.0/41	413.0 12.5	415.6 9.9/10	424.9 0.6/20	425.5 0.0/22
			425.50			

15+39 Sly edge con. dr. to dr. garage

15+33

T.P. 0.70 389.53 12.97 388.83

14+95.34

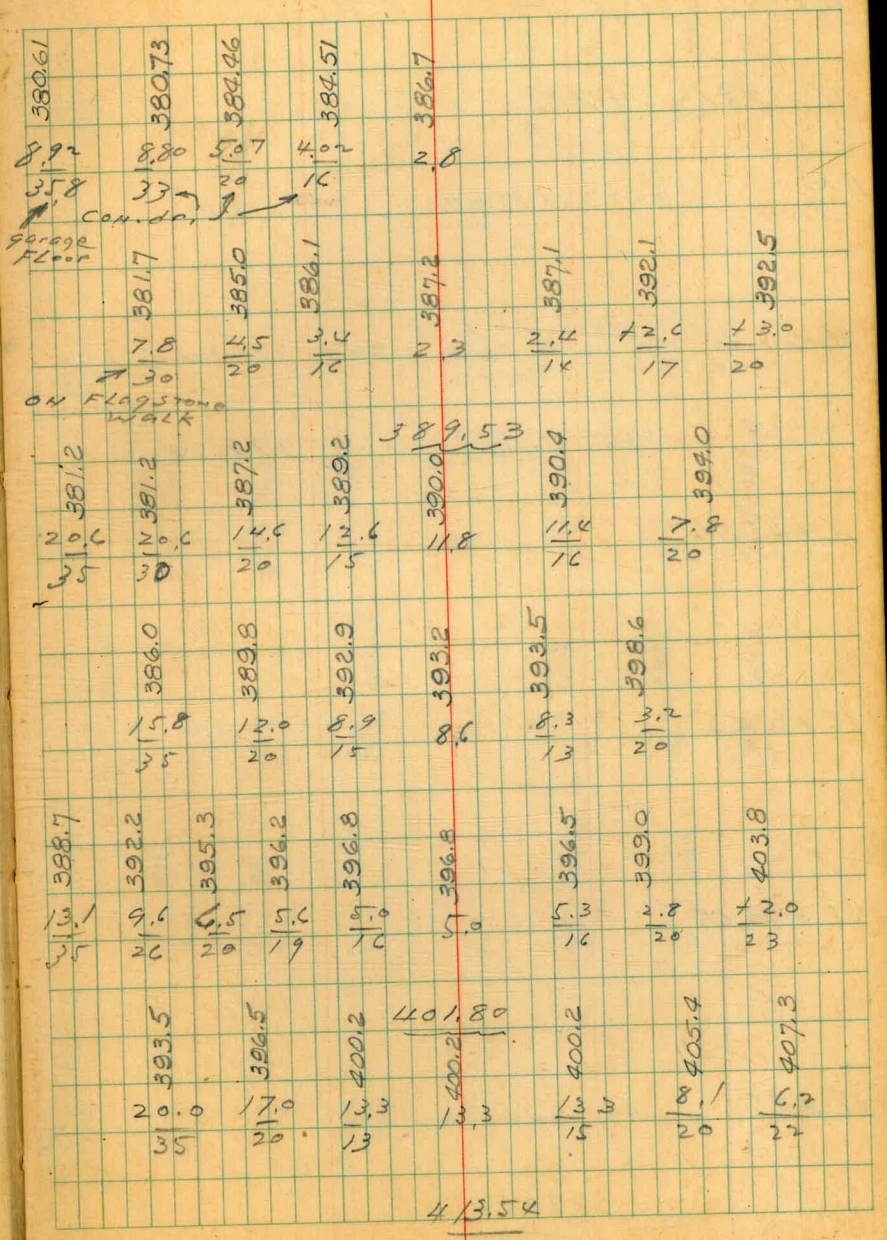
14+57.68

14+20.0N

T.P. 0.87 401.80 12.61 400.93

13+8N.36

413.54



16+92.6   15.7 Rt. = F. Hyd.

16+83.62   P.R.C.

B.M. Below   8.07   381.47   373.40

check to B.P. Base St. Lite. Muirlands Drive and Camino Teatro   8.07   373.32   373.40 / 0.08 error

T.P.   2.95   381.39   11.09   378.44

16+45.96

16+08.3

15+70.65

15+55   nly edge Con. dr.

389.53

Station	Lt				℄		Rt	
16+83.62	370.7 10.8/30	373.8 7.7/20	375.3 6.2/16	375.5 6.0/12	376.2 5.3	376.0 5.5/14	380.3 1.2/18	381.0 0.5/20
					381.47			
16+45.96	369.4 20.1/35	371.5 18.0/28	375.7 13.8/20	377.8 11.7/14	378.1 11.4	378.3 11.2/13	381.7 7.8/17	382.4 7.1/20
16+08.3	374.5 15.0/35	377.9 11.6/22	379.2 10.3/20	380.0 9.5/17	381.0 8.5	380.9 8.6/13	385.7 3.8/18	385.9 3.6/20
15+70.65	378.1 11.4/35	381.0 8.5/20	383.3 6.2/16		384.0 5.5	383.7 5.8/14	390.3 +0.8/20	
15+55	380.55 8.98/36.2 gar. floor	380.45 9.08/33.4	383.68 5.85/20	384.35 5.18/16.9	385.3 4.2			

drive

389.53

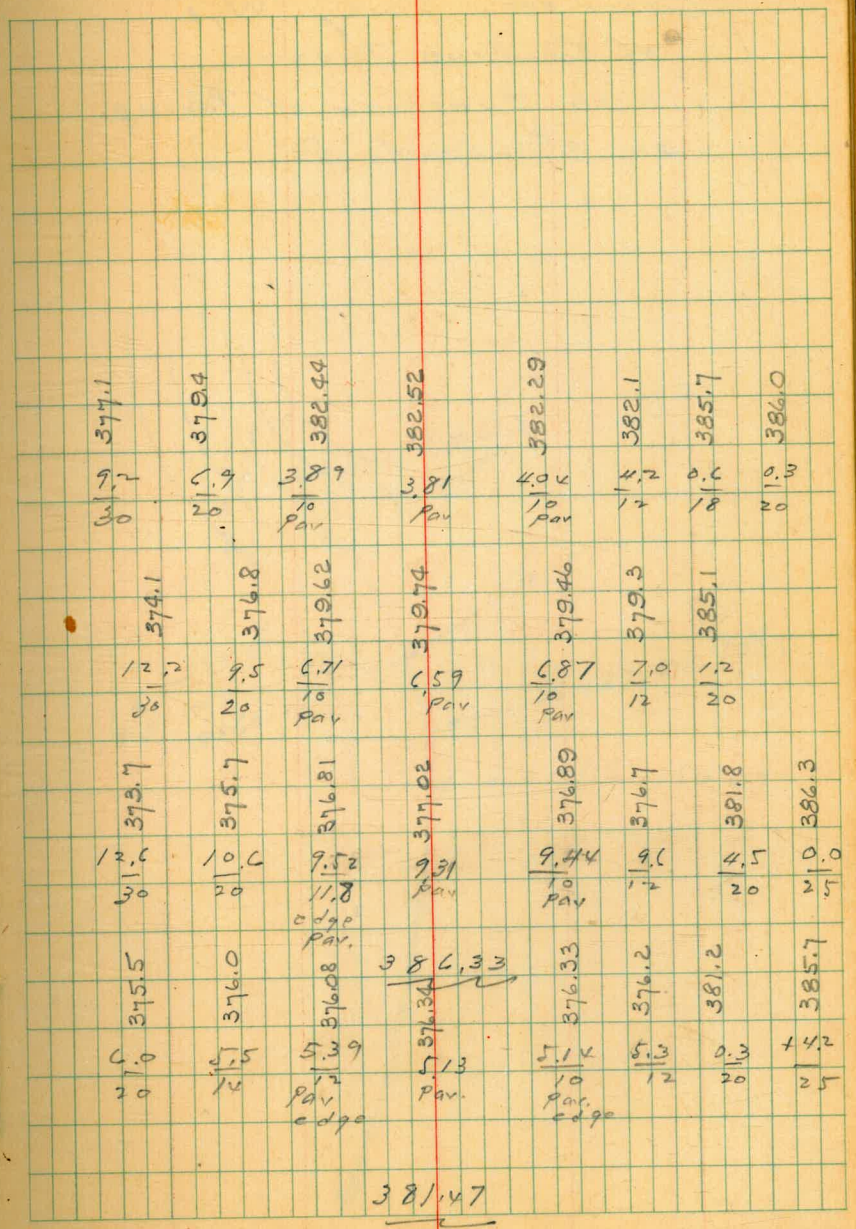
Station	Remarks	Lt			℄			Rt	
17+61.5	P.R.C.	7.0 / 20 — 374.5	6.5 / 14 — 375.0	6.37 / 12 Pav edge — 375.10	5.86 Pav — 375.61	5.80 / 10 Pav edge — 375.67	5.8 / 12 — 375.7	1.0 / 20 — 380.5	+4.0 / 25 — 385.5
17+42.03				8.18 / 20 Pav. — 373.29	6.71 Pav — 374.76	6.25 / 10 Pav edge — 375.22	6.2 / 12 — 375.3	+0.5 / 20 — 381.0	
17+22.56				8.23 / 20 Pav — 373.24	6.91 Pav — 374.56	6.30 / 10 Pav edge — 375.17	6.4 / 12 — 375.1	0.2 / 20 — 381.3	
17+07				8.14 / 24.7 Pav — 373.33	6.51 edge Pav — 374.96	6.3 / 13 — 375.2	5.0 / 14 — 376.5	+0.1 / 19 — 381.6	+0.1 / 20 — 381.6
17+03.02			7.80 / 19.7 Pav. — 373.67	6.86 / 7 Pav. — 374.61	6.4 — 375.1	6.1 / 13 — 375.4	0.1 / 19 — 381.4	0.3 / 20 — 381.2	
17+01.4	12" Corr. Iron drain Pipe See Sketch			12.73 / 29 — 368.74 F.L. outlet		6.34 / 11.9 — 375.13 grate	9.04 / 11.9 — 372.43 Bot. Box		

381.47

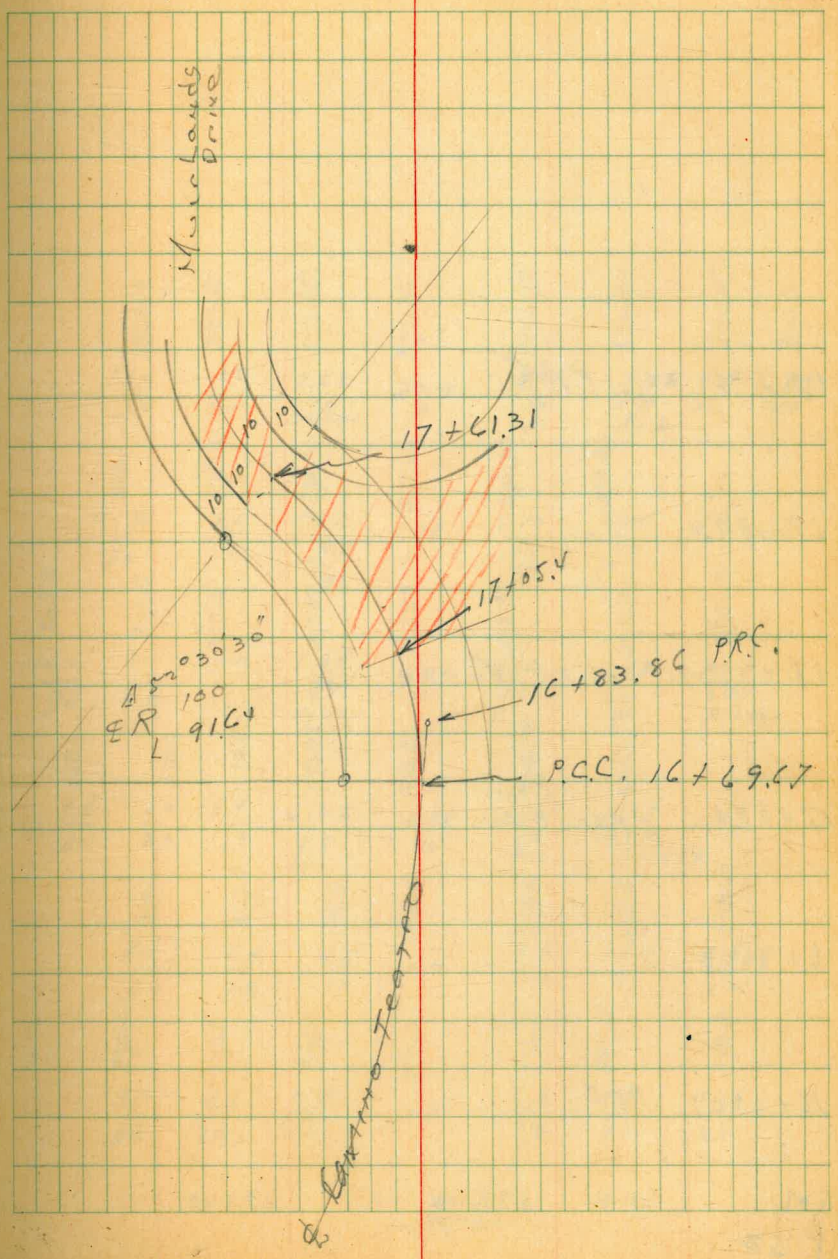
381.47

Check to BM		6.74	373.41	373.40
T.P.	3.44	380.15	9.62	376.71
18+60.53 PRC				
18+24.5 Ctr. Curve				
17+88.51 PRC				
T.P.	9.62	386.33	4.76	376.71
17+75 Ctr. Curve				
		381.47		

LT C RT



Cross Sec. Sw'ly Wye
of Camino Teatro
with Junction of Paving
on Muirlands Dr.



Swly Wye
CAMINO TEATRO

17 + 61.31 P.R.C.

17+38.4

17 + 15.49 C.T.R. Curve

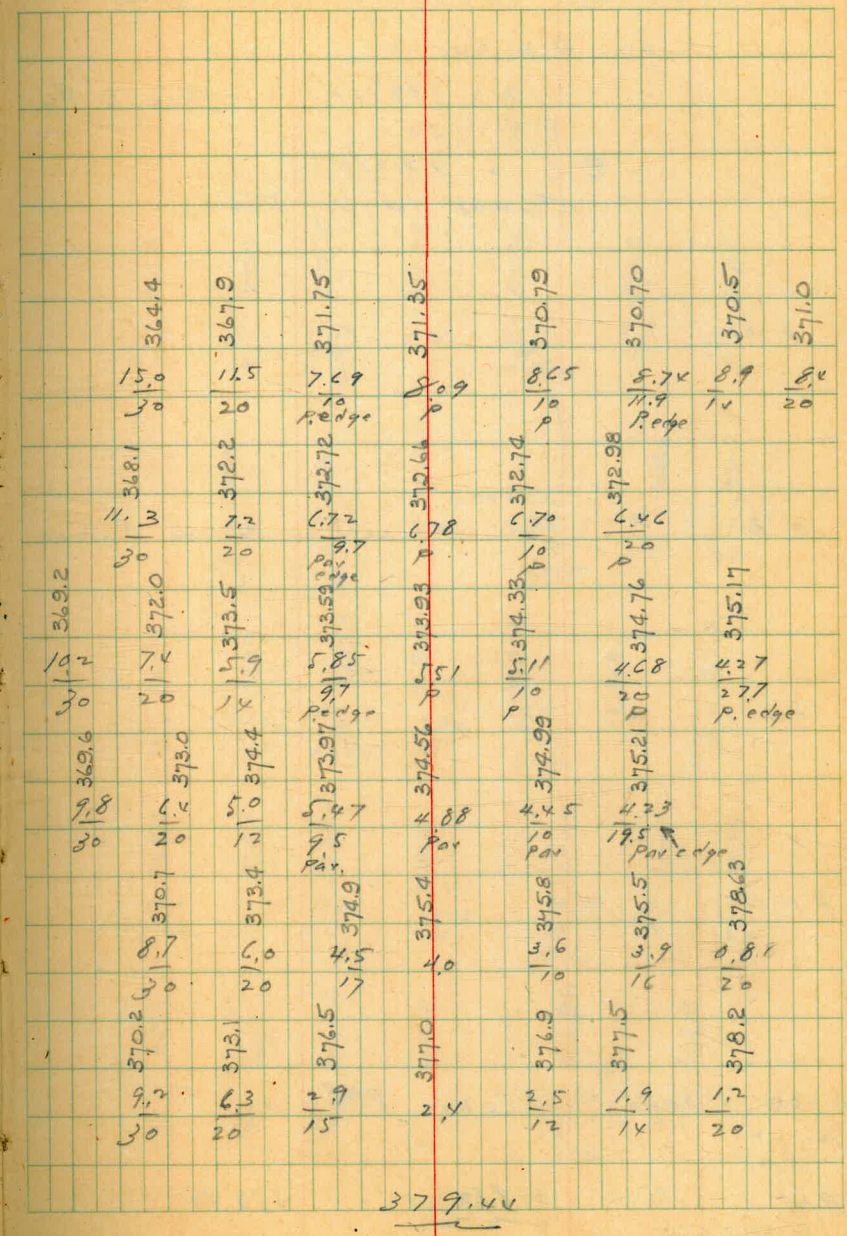
17+05.4 Conc. Edge Pav.

16+92.58

16+69.67 P.C.C.

B.M. Lot 379.44 373.40
P. 53

Lt = WLy



Levels on Muirlands Drive

on Big Curve

Δ = 199° 31' Sketch P. xx

℄R = 50

℄L = 174.11

Curve in 10 Parts

#4

#3

Note!
Pav. widened on inside Curve

#2

#1

0+00 = Lower end Curve PRC,

Sketch P. xx

B.M. P. 53 5.40 378.80 373.40

LT ℄ RT = Wily and SLY

370.4	370.4	370.30	371.09	371.46	370.3	367.5
8.4 / 10	8.4 / 15	8.4 / 11.8 P. edge	7.71	7.34 / 10 P. edge	8.4 / 15	N / 0 / 11.3
362.4	362.4	360.41	370.06	370.35	360.6	366.7
9.4 / 20	9.4	9.39 / 12 P. edge	8.74	8.45 / 10 P. edge	9.2 / 15	12.1 / 20
368.7	368.7	368.63	369.0	369.08	368.5	365.4
10.1 / 20	10.1 / 15	10.17 / 12 P. edge	9.80 P	9.72 / 10 P. edge	10.3 / 15	13.4 / 20
367.9	368.1	367.95	368.12	368.09	367.5	363.6
10.9 / 20	10.7 / 15	10.85 / 12 P. edge	10.68 P	10.71 / 9.8 P. edge	11.3 / 15	N / 0 / 15.2
367.1	367.2	367.02	367.12	366.94	366.4	362.6
11.7 / 20	11.6 / 15	11.78 / 11.8 P. edge	11.68 P	11.86 / 10 P. edge	12.4 / 16	16.2 / 20

378.80

#10 P.R.C. 1+74.11

#9

#8

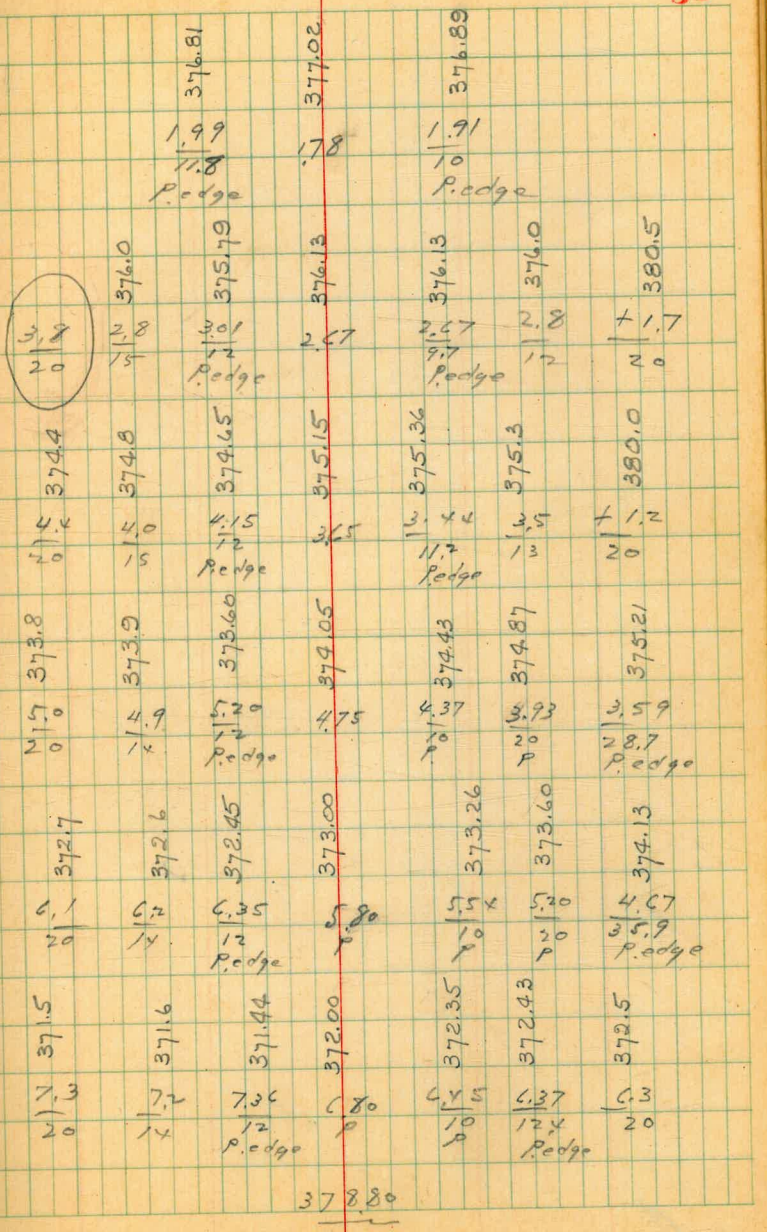
#7

#6

#5

378.80

L7 L8 L9



DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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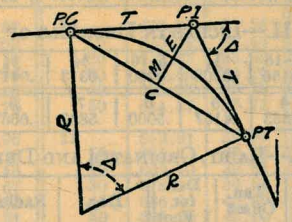

CURVE FORMULAS

Radius=R=$\frac{50}{\text{sin. } D/2}$ (1) Degree of Curve=D and sin. $\frac{D}{2}=\frac{50}{R}$ (2)

Tangent=T=R tan $\frac{\Delta}{2}$ (3) Length of Curve=L=$100\frac{\Delta}{D}$ (4)

Middle ordinate=M=R(1—cos. $\frac{\Delta}{2}$) (5)=R vers $\frac{\Delta}{2}$ (6)

External=E=T tan $\frac{\Delta}{4}$ (7)=R ÷ cos. $\frac{\Delta}{2}$—R (8)=R exsec $\frac{\Delta}{2}$ (9)

Long Chord=C=2 R sin. $\frac{\Delta}{2}$ (10) Δ=Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161+60.35 to find Sta. of P. C. and P. T. Δ=62° 10′ D=8° 20′. From Table IV for 1° curve T=3454.1 and ÷8⅓=414.49 ft. From Table V correction=.36 or T=414.85 ft. P. C.=Sta. P.I.—T=157 +45.50. Also from (4) L=746.00 and P. T.=Sta. P. C.+L=164+91.50.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance=158—Sta. P. C.=54.50, hence offset=7.27 $(54.50 \div 100)^2$=2.16 ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26)$=2.16 ft.

Deflections.—Deflection angle=½ D for 100 ft., ¼ D for 50 ft., etc. For c ft.=(in minutes) .3 x C x D° or=defl. for 1 ft. from Table III x C. For Sta. 158 of above curve=.3 x 54.5 x 8⅓=136.2′ or 2° 16.2′, or=2.50 x 54.5=136.2′ from Table III. For Sta. 159 deflection angle=2° 16.2′ +8° 20′ ÷2=6° 26.2′, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve E=960.6 for 8° 20′=960.6 ÷8⅓=115.27 and from Table V correction=.10 or E=115.37 ft. Or suppose Δ=32° and E is measured and found to be 42 ft. What is D? From Table IV E=230.9 and ÷42=5.5 or D=5° 30′.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20—16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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