X SECTIONS OVER.

WINDER ST. INDIA TO HANCOCK.

HANCOCK ST. WINDER-TO WITHERBY.

KURTZ ST. CALIFORNIA -HOELL

210

400

LEVEL

F.B. 210

210

Table showing the differ... latitude and departure in running 80 chains at any course from 1 to 60 minutes.

Minutes	Lks.	Minutes	Lks.	Minutes	Lks.
1	2 1/3	21	49	41	95 2/3
2	4 2/3	22	51 1/3	42	98
3	7	23	53 2/3	43	100 1/3
4	9 1/3	24	56	44	102 2/3
5	11 2/3	25	58 1/3	45	105
6	14	26	60 2/3	46	107 1/3
7	16 1/3	27	63	47	109 2/3
8	18 2/3	28	65 1/3	48	112
9	21	29	67 2/3	49	114 1/3
10	23 1/3	30	70	50	116 2/3
11	25 2/3	31	72 1/3	51	119
12	28	32	74 2/3	52	121 1/3
13	30 1/3	33	77	53	123 2/3
14	32 2/3	34	79 1/3	54	126
15	35	35	81 2/3	55	128 1/3
16	37 1/3	36	84	56	130 1/3
17	39 2/3	37	86 1/3	57	133
18	42	38	88 2/3	58	135 1/3
19	44 1/3	39	91	59	137 2/3
20	46 2/3	40	93 1/3	60	140

Return to City Engineers Office
City Hall, San Diego, Cal.

TABLE FOR RUNNING ON SLOPES.

In the following table the first column shows the angle, the second the number of links to be added to a chain on the slopes, to make one chain, horizontal measurement.

MICROFILMED
DEC 8 1964

Angle	Cor. in Links	Angle	Cor. in Links	Angle	Cor. in Links	Angle	Cor. in Links
o		o		o		o	
4	0.24	11	1.88	18	5.14	25	10.54
5	0.38	12	2.24	19	5.76	26	11.26
6	0.55	13	2.63	20	6.42	27	12.24
7	0.76	14	3.06	21	7.11	28	13.37
8	0.98	15	3.53	22	7.85	29	14.34
9	1.24	16	4.02	23	8.64	30	15.47
10	1.55	17	4.56	24	9.47	35	22.07

210

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City Hall, San Diego, Cal.

21.78
7.44
29.22
15
29.07
12.83
41.90
56
41.34
12.59
53.93
19
53.74
12.67
66.41
19
66.22
12.94
79.16
66
78.50
5.98
84.48

CROSS-SECTIONS OVER

WINDER ST. FROM

(COVERT WETMORE MOORE) INDIA TO HANCOCK ST.

NOV. 8, 1905

B.M.	7.44	29.22		21.78
	12.83	41.90	0.15	29.07
T.P. No 2	12.59	53.93	0.56	41.34
	12.67	66.41	0.19	53.74
	12.94	79.16	0.19	66.22
	5.98	84.48	0.66	78.50
B.M.	R.R. SPIKE IN PRONE POLE MARKED "C" AT EAST COR. OF INDIA AND WINDER.		1.07	83.41
	0 = S.W. LINE OF INDIA ST.			
N.L.			3.2	81.3
N.C.			3.5	81.0
N 1/4			3.9	80.6
1/2			4.1	80.4
S 1/4			4.5	80.0
S.C.			5.2	79.3
S.L.			5.8	78.7
	25 W. OF INDIA			
S.L.			7.5	77.0

CALIFORNIA & VINE
NE. COR. TEL. POLE
50' W. OF N.E. CO.

1

84.48

S.C	6.8	77.7
S 1/4	6.5	78.0
1/2	6.1	78.4
N 1/4	5.8	78.7
N.C	5.1	79.4
N.L	4.9	79.6
50 W. OF INDIA		
N.L	6.4	78.1
N.C	6.7	77.8
N 1/4	7.3	77.2
1/2	8.0	76.5
S 1/4	8.3	76.2
S.C.	8.6	75.9
S.L	9.1	75.4
75 W. OF INDIA		
S.L	11.7	72.8
S.C	11.2	73.3

84.48

S 1/4	10.4	74.1
1/2	9.8	74.7
N 1/4	9.3	75.2
N.C	8.6	75.9
N.L	8.1	76.4
100 W. OF INDIA		
N.L	9.9	74.6
N.C	10.6	73.9
N 1/4	10.9	73.6
1/2	12.0	72.5
S 1/4	11.9	72.6
S.C.	11.8	72.7
S.L.	12.4	72.1
125 W. OF INDIA		
S.L	13.7	70.8
S.C.	13.5	71.0
S 1/4	13.2	71.3

84.48
12.73
71.75
72.18

½			12.7	71.8	
N ¼			12.4	72.1	
N.C.			13.0	71.5	
N.L.			11.3	73.2	
	0.43	72.18	12.73	71.75	
	150° W. OF INDIA				
N.L			0.9	71.3	
N.C.			1.2	71.0	
N ¼			1.9	70.3	
½			1.9	70.3	
S ¼			2.4	69.8	
S.C.			3.0	69.2	
S.L			3.3	68.9	
	175 W OF INDIA				
S.L			4.5	67.4	
S C			4.4	67.8	
S ¼			4.3	67.9	

72.18

½			3.9	68.3	
N ¼			3.4	68.8	
N.C			3.4	68.9	
N.L			2.7	69.5	
	200 W. = E. L. ARCTIC				
N.L			5.1	67.1	
N.C			5.0	67.2	
N ¼			5.3	66.9	
½			5.C	66.6	
S ¼			5.7	66.5	
S.C			6.2	66.0	
S.L			6.3	65.9	
	14 W = E.C. ARCTIC.				
S.L			7.7	64.5	
S.C.			7.4	64.8	
S ¼			7.1	65.1	
½			6.9	65.3	

72.18

N. 1/4	6.7	65.5
N.C.	6.2	66.0
N.L.	5.6	66.6

E. 1/4 ARTIC.

N.L	7.0	65.2
N.C	7.4	64.8
N 1/4	7.6	64.6
1/2	8.1	64.1
S. 1/4	8.2	64.0
S.C.	8.5	63.7
S.L	9.0	63.2

1/2 ARTIC

S.L	10.2	62.0
S.C.	9.8	62.4
S. 1/4	9.3	62.9
1/2	9.3	62.9
N 1/4	8.2	64.0

72.15

N. C	8.0	64.2
N. L	7.8	64.4

W 1/4 ARTIC

N. L.	8.9	63.3
N.C	9.3	62.9
N. 1/4	9.0	63.2
1/2	9.9	62.3
S 1/4	9.2	63.0
S.C	9.9	62.3
S. L	10.8	61.4

W.C. ARTIC.

S. L	11.4	60.8
S. C	11.2	61.0
S 1/4	10.3	61.9
1/2	10.7	61.5
N 1/4	9.8	62.4
N C	9.6	62.6

		72.18		
		59.30		
N.L		9.4	62.8	
75 W. = W.L. ARCTIC.				
N.L		10.7	61.5	
N.C		10.4	61.8	
N.¼		10.9	61.3	
30 S		11.9	60.3	
½		11.9	60.3	
50 S		11.8	60.4	
S ¼		11.7	60.8	
S.C		12.1	60.1	
S.L		12.3	59.9	
25 W. OF ARCTIC				
N.L.		12.4	59.8	
N.C		12.6	59.6	
N ¼		12.6	59.6	
0.0	59.30	12.58	59.30	
32-S		0.5	58.8	

		59.30		
½		0.7	58.6	
50-S		1.0	58.3	
S ¼		0.5	58.8	
S.C		0.7	58.6	
S.L.		1.3	58.0	
50 W. OF ARCTIC.				
S.L.		2.8	56.5	
S.C.		2.8	56.5	
S ¼		2.2	57.1	
48-S		2.9	56.4	
½		2.3	57.0	
31-S		2.1	57.2	
N ¼		1.6	57.7	
N.C.		1.6	57.7	
N.L.		1.2	58.1	
75 W. OF ARCTIC.				
N.L		3.0	56.3	

59.30

N.C.	3.3	56.0
N 1/4	3.5	55.8
31-S	4.3	55.0
1/2	4.2	55.1
49-S	4.4	54.9
S 1/4	3.7	55.6
S.C.	4.6	54.7
S.L.	4.6	54.7

100 W. OF ARCTIC.

S.L.	6.4	52.9
S.C.	6.3	53.0
S 1/4	5.9	53.4
48-S	6.6	52.7
1/2	6.2	53.1
30-S	6.2	53.1
N 1/4	5.3	54.0
N.C.	4.8	54.5

59.30

N.L.	4.8	54.5

125 WEST OF ARCTIC

N.L.	6.5	52.8
N.C.	6.7	52.6
N 1/4	7.0	52.3
30-S	7.9	51.4
1/2	7.8	51.5
48-S	8.1	51.2
S 1/4	7.4	51.9
S.C.	7.4	51.9
S.L.	8.1	51.2

150 W. OF ARCTIC

S.L.	10.0	49.3
S.C.	9.5	49.8
S. 1/4	9.5	49.8
1/2	9.6	49.7

59.30

30-S		9.C	49.7	
N 1/4		8.9	50.4	
N.C.		8.7	50.6	
N.L.		8.6	50.7	
	175 W. OF ARCTIC.			
N.L.		10.2	49.1	
N.C.		10.5	48.8	
N. 1/4		10.8	48.5	
28-S		11.6	47.7	
1/2		11.6	49.7	
S 1/4		11.5	47.8	
S.C.		11.5	47.8	
S.L		13.0	46.3	
	200 W. OF ARCTIC = E.L. CALIF.			
S.L		12.6	46.7	
75-S		13.0	46.3	
71-S		14.7	44.6	

59.30
+L.79
46.53
.21
46.74

S.C			14.1	45.2
S 1/4			13.5	45.8
1/2			13.1	46.2
N 1/4			12.8	46.5
N.C			12.1	47.2
N.L			12.2	47.1
	0.21	46.74	12.77	46.53
	H-W E.C.	CALIF.		
N.L			0.5	47.2
N.C			0.6	47.1
N 1/4			0.9	45.8
1/2			1.4	45.3
S 1/4			1.7	45.0
S.C			1.4	45.3
S.L			0.9	45.8
	20' W.			44.4
S.L			2.3	

		40.74 3.82 42.92		
S.C			1.9	44.8
S 1/4			1.9	44.8
1/2			1.5	45.2
N 1/4			1.0	45.7
N.C			0.6	46.1
N.L			0.5	46.2
	E. L. OF HANCOCK.			
N.L			3.4	43.3
N.C			2.4	44.3
N 1/4			1.9	44.8
1/2			2.0	44.7
S 1/4			2.7	44.0
S C			2.3	44.4
S.L			2.3	44.4
CK. ON T.P. No 2			5.40	41.34
B.M.	SPIKE IN PHONE POLE. NORTH. COR OF WINDERS AND HANCOCK		3.82	42.92

X SECTIONS OVER HANCOCK ST. FROM WINDER — WITHERB

8

B.M.	3.82	40.74		42.92
	B.L. OF WINDERS.			
E.L.			2.3	44.4
E.C			2.6	44.1
E 1/4			3.4	43.3
1/2			4.2	42.5
W 1/4			5.2	41.5
W.C			5.9	40.8
W.L			7.3	39.4
	S.C WINDERS			
W.L			7.7	39.0
W.C			6.3	40.4
W 1/4			5.5	41.2
1/2			4.6	42.1
E 1/4			3.4	43.3
E C			2.3	44.4
E.L			2.7	44.0

46.74

S 1/4 OF WINDERS.

E.L	2.0	44.7
E.C	2.6	44.1
E 1/4	3.4	43.3
1/2	4.8	41.9
W 1/4	6.1	40.6
W C	7.0	39.7
W.L	8.1	38.6

1/2 WINDERS

W.L	8.3	38.4
W.C	7.3	39.4
W 1/4	5.3	41.4
1/2	4.0	42.7
E 1/4	4.2	42.5
E C	3.1	43.6
E.L	2.0	44.7

N 1/4 OF WINDERS

46.74

E.L	2.5	44.2
E.C	4.1	42.6
E 1/4	4.5	42.2
1/2	6.0	40.7
W 1/4	5.7	41.0
W.C	6.9	39.8
W.L	8.3	38.4

N.C. WINDER ST.

W.L	8.3	38.4
W.C	6.9	39.8
W 1/4	7.2	39.5
32.E	C.8	39.9
1/2	4.2	42.5
E 1/4	5.0	41.7
E C	4.8	41.9
E L	3.4	43.3

N.L. WINDER ST.

E.L	3.4	43.3

AC.74

E.C	4.7	42.0
E 1/4	5.1	41.6
1/2	4.5	42.2
30 E	5.1 5.1	41.6
24-E	7.1	39.6
W.C	8.1	38.6
W.L	8.3	38.4
S.L OF STORY ST.		
W.L	8.4	38.3
W.C	6.9	39.8
W 1/4	7.1	39.6
30-E	4.C	42.1
1/2	4.5	42.2
E.1/4	5.0	41.7
E.C	4.8	41.9
E.C	4.0	42.7
S.C STORY		

AC.74

E.L	4.1	42.6
E.C	4.9	41.8
E.1/4	4.8	41.9
1/2	5.1	41.6
W 1/4	5.1	41.6
22-E	7.1	39.6
W.C	8.2	38.5
W.L	8.1	38.6
S 1/4 STORY		
W.L	8.4	38.3
W.C	7.C	39.1
22-E	6.C	40.1
W 1/4	4.9	41.8
1/2	5.9	40.8
E.1/4	5.1	41.6
E C	4.9	41.8
E.L	4.1	42.6

46.74

1/2 STORY

E. L	4.2	42.5
E. C	5.1	41.6
E. 1/4	5.3	41.4
46-E	4.5	42.2
1/2	5.6	41.1
W 1/4	5.1	41.6
22-E	6.5	40.2
W. C	7.7	39.0
W. L	9.0	37.7

N 1/4 STORY

W. L	9.1	37.6
W. C	7.8	38.9
23-E	6.9	39.8
W 1/4	5.2	41.5
1/2	6.1	40.6
E 1/4	4.6	42.1

46.74

E. C	5.2	41.5
E. L	4.2	42.5

N. C. STORY

E. L	4.2	42.5
E. C.	5.2	41.5
E 1/4	4.8	41.9
45 E	4.6	42.1
42-E	5.7	41.0
1/2	6.0	40.7
30-E	5.3	41.4
W 1/4	5.4	41.3
22-E	7.1	39.6
W C	7.7	39.0
W L	8.9	37.8

N. L. STORY.

W. L	8.7	38.0
W. C	7.8	38.9

4C.74

22-E.	7.3	39.4
W 1/4	5.6	41.1
33-E.	6.5	40.2
1/2	6.0	40.7
E 1/4	4.7	42.0
E.C.	5.2	41.5
E.L	4.2	42.5
25 N. OF STORY.		
E.L	4.4	42.3
E.C	5.0	41.7
E 1/4	5.5	41.2
42-E	5.2	41.5
1/2	6.3	40.4
W 1/4	5.7	41.0
22-E	7.2	39.5
W.C	7.7	39.0
W.L	8.8	37.9

4C.74

50 N. OF STORY		
W.L	8.7	38.0
W.C	7.5	39.2
W 1/4	6.2	40.5
32 E	7.1	39.6
1/2	6.6	40.1
E 1/4	5.7	40.8
E.C	5.2	41.5
E.L	4.8	41.9
75 N. OF STORY		
E.L	5.0	41.7
E.C	5.6	41.1
E 1/4	5.7	41.0
1/2	7.1	39.6
31 E	7.2	39.5
W 1/4	6.5	40.2
W.C	7.7	39.0

46.74

W. L	8.8	37.9
100 N. OF STORY.		
W. L	8.7	38.0
W. C	8.1	38.6
W 1/4	7.5	39.2
1/2	7.3	39.4
E 1/4	6.9	40.7
E C	6.0	40.7
E. L	5.5	41.2
12[illegible] N. OF STORY.		
E. L	5.8	40.9
E. C	6.2	40.5
E 1/4	6.5	40.2
A2-E	6.8	39.9
1/2	7.8	38.9
32-E	7.1	39.6
W 1/4	7.9	39.0

46.74

W. C	8.1	38.6
W. L	8.7	38.0
150 N. OF STORY		
W. L	8.6	38.1
W. C	8.3	38.4
W. 1/4	7.7	39.0
32 E	7.4	39.3
1/2	8.1	38.6
43-E	7.0	39.7
E 1/4	6.7	40.0
E. C	6.4	40.3
E. L	6.0	40.7
175 N. OF STORY		
E. L	6.1	40.6
E. C	6.3	40.4
E 1/4	6.4	40.3
1/2	8.3	38.4

AC.74

W.¼	5.0	38.7
W.C	7.8	38.9
W.L	8.3	38.4

200 N. OF STORY.

W.L	8.8	37.9
W.C	7.9	38.8
24-E	7.3	39.4
½	8.5	38.2
E ¼	6.3	40.4
E.C	6.4	40.3
E.L	5.7	41.0

225 N. OF STORY.

E.L	5.8	40.9
E.C	6.5	40.2
E ¼	6.3	40.4
½	9.0	37.7
24-E	7.2	39.5

W.C	7.8	38.9
W.L	8.6	38.1

250 N. OF STORY.

W.L	8.6	38.1
W.C	7.9	38.8
24-E	7.6	39.1
½	9.3	37.4
E ¼	6.5	40.2
E.C	6.9	39.8
E.L	5.9	40.8

275 N. OF STORY.

E.L	6.1	40.6
63-E	6.2	40.5
E.C	7.1	39.6
E ¼	6.9	39.8
½	9.5	37.2
W ¼	7.7	39.0

		46.74 10.20 36.54 2.53 39.07		
W.C			8.3	38.5
W.L			8.8	37.9
	300 N. OF STORY = S.L HARASTHY.			
W.L			9.5	37.2
W.C			8.9	37.8
W 1/4			8.3	38.4
1/2			10.2	36.5
E 1/4			8.1	38.6
E C			7.3	39.4
E L			6.8	39.9
	2.53	39.07	10.20	36.54
E.L	S. C. HARASTHY.			
E. L			0.0	39.1
E.C			0.0	39.1
E 1/4			1.5	37.6
1/2			2.0	37.1
W. 1/4			0.9	38.2

		39.07		
W.C			1.5	37.6
W.L			2.2	36.9
	S 1/4 HARASTHY.			
W.L			2.5	36.6
W.C			1.7	37.2
24-E			1.3	37.8
1/2			2.3	36.8
E 1/4			1.7	37.4
E.C			0.0	39.1
E.L			4.2	34.9
	1/2 HARASTHY.			
E.L			6.3	32.8
E.C			2.7	36.4
56-E			0.7	38.4
~~50~~ E 1/4			0.7	38.4
48-E			1.8	37.3
1/2			2.6	36.5

39.07

W 1/4	2.1	37.0
W.C	2.3	36.8
W.L	2.5	36.3
N. 1/4 HARASTHY.		
W.L	2.7	36.4
W.C	2.2	36.9
W 1/4	2.6	36.5
1/2	2.9	36.2
E 1/4	2.6	36.5
E.C	6.5	32.6
E.L	5.0	34.1
N.C. HARASTHY.		
E.L	2.4	36.7
E.C	5.9	33.2
E 1/4	7.2	31.9
1/2	4.5	34.6
W 1/4	3.6	35.5

39.07

W.C	3.1	36.0
W.L	3.3	35.8
N.L. HARATHY.		
W.L	6.1	33.0
W.C	6.5	32.6
24-E	6.3	32.8
1/2	8.2	30.9
4C-E	7.8	31.3
E 1/4	5.8	33.3
EC	4.3	34.8
69E	1.0	38.1
E.L	0.8	38.3
25 N OF HARATHY		
E.L	1.1	38.0
E.C	1.9	37.2
E 1/4	2.9	36.2
1/2	3.6	35.5

39.07

W 1/4	3.4	35.7	
W.C	4.8	34.3	
W.L	8.0	31.1	
13 NORTH OF HARATHY.			
W.L	9.1	30.0	
W.C	8.8	30.3	
W 1/4	8.3	30.8	
1/2	4.1	35.0	
E 1/4	2.7	36.4	
E C	1.7	37.4	
E.L	0.8	38.3	
28 NORTH OF HARATHY			
E.L	0.7	38.4	
E.C	1.9	37.2	
E 1/4	3.1	36.0	
1/2	3.8	35.3	
W 1/4	3.6	35.5	

39.07
C.V.
32.62

W C	4.1	35.0	
W.L	5.4	33.7	
B.M. { R.R. SPIKE IN 6"X6" POST IN WING OF SMALL CULVERT 50' W OF N.W. COR. HANCOCK & HARATHY.	6.45	32.62	
50 N. OF HARATHY.			
W.L	5.4	33.7	
W.C	3.8	35.3	
W 1/4	4.5	34.6	
1/2	4.6	34.5	
E 1/4	2.9	36.2	
E.C	2.5	36.6	
E.L	1.8	37.3	
75 N. OF HARATHY			
E.L	2.7	36.4	
E.C	3.4	35.7	
E 1/4	4.1	35.0	
1/2	5.3	33.8	

		39.07		
W 1/4			5.2	33.9
W. C			5.7	33.4
W. L			5.5	33.6
	100 N. OF HARATHY.			
W. L			6.8	32.3
W. C			5.4	33.7
W 1/4			5.3	33.8
1/2			5.9	33.2
E 1/4			4.0	35.1
E. C			4.2	34.9
E. L			3.6	35.5
	125 - N. OF HARATHY			
E. L			4.0	35.1
E. C			4.7	34.4
E 1/4			5.2	33.9
1/2			6.4	32.7
W 1/4			5.7	33.4

		39.07		
		3.95		
		35.12		
W. C		35.44	5.7	33.4
W. L			7.4	31.7
	150 N. OF HARATH.			
W. L			7.5	31.6
W. C			6.9	32.2
W 1/4			6.4	32.7
1/2			7.0	32.1
E 1/4			5.3	33.8
E. C			5.1	34.0
E. L			4.7	34.4
	0.32	35.44	3.95	35.12
	175 N. OF HARASTHY			
E. L			0.9	34.5
E. C			1.7	33.7
E 1/4			1.9	33.5
1/2			3.7	31.7
W 1/4			3.2	32.2

35.44

W.C	3.9	31.5
W.L	4.9	30.5
200 N. OF HARASTHY.		
W.L	5.2	30.2
W.C.	4.4	31.0
W. 1/4	3.7	31.7
1/2	4.0	31.4
E 1/4	2.2	33.2
E.C	1.8	33.6
E.L	0.8	34.6
225 N. OF HARASTHY		
E.L	1.6	33.8
E.C	2.4	33.0
E 1/4	3.1	32.8
1/2	4.6	30.8
W 1/4	4.2	31.2
W.C	5.4	30.0

35.44.

W.L	6.1	29.3
250 N. OF HARASTHY.		
W.L	6.5	28.9
W.C	5.8	29.6
W 1/4	5.3	30.1
1/2	5.2	30.2
E 1/4	3.3	32.1
E C	3.3	32.1
E L	2.4	33.0
275 N. OF HARASTHY		
E.L	2.6	32.8
E C	3.9	31.5
E. 1/4	4.2	31.2
1/2	5.8	29.6
W 1/4	6.1	29.3
W.C	6.6	28.8
W.L	7.2	28.2

300 N. OF HARASTHY = S. L. CLAYTON.

W. L	7.6	27.8
W. C	6.9	28.5
W. 1/4	6.3	29.1
1/2	6.1	29.3
E 1/4	4.6	30.8
E C	4.3	31.1
E. L	3.0	32.4

14 = S. C CLAYTON

E. L	3.6	31.8
E. C	4.6	30.8
E 1/4	5.3	30.1
1/2	6.4	29.0
W 1/4	6.7	28.7
W C	7.2	28.2
W. L	8.0	27.4

27 = S 1/4 CLAYTON

W. L	8.3	27.1
W. C	7.3	28.1
W 1/4	6.7	28.7
1/2	6.6	28.8
E 1/4	5.8	29.6
E. C	4.9	30.5
E L	3.9	31.5

40 = 1/2 CLAYTON

E. L	4.3	31.1
E. C	5.5	29.9
E 1/4	5.8	29.6
1/2	6.8	28.6
W 1/4	6.7	28.7
W. C	7.7	27.7
W L	8.6	26.8

53 N. = N. 1/4 CLAYTON.

W. L	8.9	26.5

35.44

W. C			7.5	27.6	
W 1/4			7.0	28.4	
1/2			7.0	28.4	
E 1/4			6.1	29.3	
E C.			5.8	29.6	
E. L			4.5	30.9	
	60 =	N. C.	CLAYTON.		
E. L			4.6	30.8	
E C.			6.1	29.3	
E 1/4			6.8	28.6	
1/2			7.1	28.3	
W 1/4			7.2	28.2	
W C			8.2	27.2	
W. L			9.3	26.1	
	80 =	N. L.	CLAYTON.		
W. L			9.7	25.7	
W. C			9.0	26.4	

35.44

W. 1/4			7.7	27.7	
1/2			7.2	28.2	
E 1/4			7.2	28.2	
E C.			6.6	28.8	
E. L			5.2	30.2	
	25	N. OF	CLAYTON.		
E. L			5.9	29.5	
E. C			7.0	28.4	
E 1/4			7.3	28.1	
1/2			7.6	27.8	
W 1/4			8.5	26.9	
W. C			9.5	25.6	
W. L			10.1	25.3	
	50	N. OF	CLAYTON		
W. L			10.6	24.8	
W. C			10.0	25.4	
W. 1/4			9.0	26.4	

35.44

1/2	7.8	27.6
E 1/4	7.5	27.9
E C	7.4	28.0
E. L	5.9	29.5
75 N. OF CLAYTON.		
E. L	6.0	29.4
E. C.	7.2	28.2
E 1/4	7.4	28.0
1/2	7.9	27.5
28-E	8.3	27.1
21-E	9.9	25.5
W. C	10.3	25.1
W. L	10.9	24.5
100 N. OF CLAYTON		
W. L	11.1	24.3
W. C	10.3	25.1
22-E	10.0	25.4

35.44

29-E	8.3	27.1
1/2	8.1	27.3
E 1/4	7.6	27.8
E. C	6.9	28.5
E. L	5.6	29.8
125 N OF CLAYTON		
E. L	5.5	29.9
E. C	6.2	29.2
E 1/4	7.2	28.2
1/2	8.1	27.3
29-E	8.1	27.3
23-E	9.6	25.8
W. C	10.4	25.0
W. L	12.3	23.1
150 N. OF CLAYTON.		
W. L	13.8	21.6
W. C	11.4	24.0

35.44

21-E	10.9	24.5
27-E	8.3	27.1
½	8.3	27.1
E ¼	7.4	28.0
50-E	6.2	29.2
E.C.	5.2	30.2
E.L.	4.9	30.5
175 N. OF CLAYTON		
E.L.	3.8	31.6
E.C.	3.8	31.6
55-E	4.4	31.0
46-E	7.7	27.7
½	8.3	27.1
27-E	8.0	26.8
21-E	11.4	24.0
W.C.	12.1	23.3
W.L.	13.4	22.0

35.44

200 N. OF CLAYTON		
W.L.	13.3	22.1
W.C.	12.1	23.3
33-E	10.8	24.6
28-E	8.5	26.9
½	8.5	26.9
E ¼	7.8	27.6
57-E	6.0	29.4
64-E	3.8	31.6
E.L.	3.2	32.2
225 N. OF CLAYTON		
E.L.	4.5	30.9
E.C.	5.7	29.7
E ¼	7.5	27.6
½	8.6	26.8
29-E	8.5	26.9
22-E	10.8	24.6

35.44

W.C.	11.5	23.9
W.L	12.6	22.8
250 N. OF CLAYTON		
W.L	12.3	23.1
W.C	11.1	24.3
24-E	10.2	25.2
29-E	8.8	26.6
1/2	8.5	26.9
E 1/4	7.6	27.8
E.C.	6.2	29.2
E.L	5.0	30.4
275 - N. OF CLAYTON		
E.L	5.6	29.8
E.C.	6.5	28.9
E 1/4	7.6	27.8
1/2	8.3	27.1
29-E	8.4	27.0

35.44

23-E	9.8	25.6
W.C	10.5	24.9
W.L	11.7	23.7
300 N. OF CLAYTON = S.L. SUTHERLAND		
W.L	11.2	24.2
W.C	10.5	24.9
25-E	9.4	26.0
29-E	8.4	27.0
1/2	8.3	27.1
E 1/4	7.9	27.5
E.C	6.4	29.0
E.L	5.7	29.7
14 = S.C. SUTHERLAND		
E.L	6.1	29.3
E.C	6.5	28.9
E 1/4	7.7	27.7
1/2	8.2	27.2

35.44

28-E	8.4	27.0
24-E.	9.3	26.1
W.C	10.2	25.2
W.L	11.1	24.1

27. = S. 1/4 SUTHERLAND.

W.L	10.9	24.5
W.C	9.8	25.6
W 1/4	8.8	26.6
1/2	8.2	27.2
E 1/4	7.7	27.7
E.C	6.6	28.8
E.L	5.9	29.5

40 = 1/2 SUTHERLAND

E.L	6.1	29.3
E.C	6.9	28.5
E 1/4	7.6	27.8
1/2	8.2	27.2

35.44.

W 1/4	9.0	26.4
W.C	9.7	25.7
W.L	10.7	24.7

53 N. = N 1/4 SUTHERLAND.

W.L	10.6	24.8
W.C	9.6	25.8
W 1/4	8.9	26.5
1/2	8.4	27.0
E 1/4	7.7	27.7
E.C	7.0	28.4
E.L	6.2	29.2

66 = N.C. SUTHERLAND

E.L	6.2	29.2
E.C	7.0	28.4
E 1/4	7.7	27.7
1/2	8.4	27.0
W. 1/4	8.7	26.7

35.44
9.82
25.62
5.15
30.77

W. C		9.5	25.9
W. L		10.6	24.8
	8.0 = M. L.		
W. L		10.4	25.0
W. C		9.4	26.0
W 1/4		8.8	26.6
1/2		8.5	26.9
E 1/4		7.5	27.9
E. C.		6.C	28.8
E. L.	SPIKE IN F.P. AT NW	6.3	29.1
B.M.	COR. { SUTHERLAND HANCOCK	9.82	25.62
	5.15 30.77	9.82	25.62
	25 N. OF SUTHERLAND		
E. L		1.6	29.2
E. C		1.7	29.1
E 1/4		2.5	28.3
1/2		3.7	27.1

30.77

W. 1/4		4.0	26.8
W. C		4.6	26.2
W. L		5.1	25.7
	50 N. OF SUTHERLAND		
W. L		4.8	26.0
W. C		4.3	26.5
W 1/4		3.9	26.9
1/2		3.4	27.4
E 1/4		2.6	28.2
E. C		1.7	29.1
E. L		1.4	29.4
	75 N. OF SUTHERLAND		
E. L		1.3	29.5
E. C		1.6	29.2
E 1/4		2.3	28.5
1/2		3.3	27.5
W. 1/4		3.9	26.9

30.77

W.C	4.8	26.0
W.L	5.3	25.5
100 N. OF SUTHERLAND.		
W.L	4.2	26.6
W.C	3.5	27.3
W.¼	3.0	27.5
½	3.1	27.7
E ¼	2.9	27.9
E C	2.0	28.8
E L	1.3	29.5
125 N. OF SUTHERLAND.		
E.L	1.2	29.6
E.C	1.1	29.7
E¼	2.0	28.8
½	2.8	28.0
W ¼	3.1	27.7
W C	3.8	27.0

30.77

W.L	4.5	26.3
150 N. OF SUTHERLAND.		
W.L	2.6	28.2
W.C	2.7	28.1
W ¼	2.6	28.2
½	2.6	28.2
E ¼	1.8	29.0
E.C	0.7	30.1
E.L	1.3	29.5
175 N. OF SUTHERLAND		
E.L	1.2	29.6
E.C	0.6	30.2
E¼	1.1	29.7
½	2.5	28.3
W¼	2.2	28.6
W.C	2.7	28.1
W.L	2.8	28.0

30.77

200 N. OF SUTHERLAND.

W.L	2.4	28.4
W.C	2.5	28.3
W 1/4	2.0	28.8
1/2	2.4	28.4
E 1/4	1.8	29.0
E.C	1.2	29.6
E.L	1.7	29.1

225 N. OF SUTHERLAND.

E.L	2.3	28.5
E.C	2.2	28.6
E 1/4	2.7	28.1
1/2	2.7	28.1
W 1/4	2.6	28.2
W C	3.0	27.8
W.L	2.7	28.1

250 N. OF SUTHERLAND

30.77

W.L	3.8	27.0
W.C	3.9	26.9
W 1/4	2.7	28.1
1/2	2.9	27.9
E 1/4	3.4	27.4
E C	2.9	27.9
E L	3.2	27.6

275 N. OF SUTHERLAND.

E.L	3.9	26.9
E.C	3.8	27.0
E.1/4	3.8	27.0
1/2	3.5	27.3
W. 1/4	3.6	27.2
W.C	4.4	26.4
W.L	4.5	26.3

300 N. OF SUTHERLAND = S.L. NOELL

W.L	5.2	25.6

30.77

W.C		5.3	25.5
W 1/4		4.2	26.6
1/2		4.4	26.4
E 1/4		4.1	26.7
E C		4.2	26.6
E.L		4.0	26.8
B.M.	~~RR~~ SPIKE IN F.P. AT S.W. COR. NOELL HANCOCK	4.34	26.43

14 = S.C NOELL

E.L.		4.2	26.6
E.C		4.8	26.0
E. 1/4		4.7	26.1
1/2		4.7	26.1
28-E		4.5	26.3
18 E		7.5	23.3
W.C		7.1	23.7
9-E		5.3	25.5
W.L		5.7	25.1

30.77

27 = S 1/4 NOELL

W.L		6.2	24.6
W.C		8.0	22.8
18-E		8.0	22.8
28 1/E		5.3	25.5
1/2		5.7	25.1
E 1/4		4.8	26.0
E C		5.0	25.8
E.L		4.5	26.3

40 = 1/2 NOELL

E.L		4.7	26.1
E.C		5.1	25.7
E 1/4		4.9	25.9
1/2		5.9	24.9
W 1/4		5.8	25.0
W.C		7.4	23.4

30.77

W. L	8.9	21.9
53 = N ¼ NOELL		
W. L	7.7	23.1
W. C	6.1	24.7
W. ¼	6.7	24.1
½	5.9	24.9
E ¼	5.0	25.8
E C	5.0	25.8
E. L	5.0	25.8
66 = N. C. NOELL		
E. L	5.0	25.8
E. C	5.3	25.5
E ¼	5.2	25.6
½	5.7	25.1
W ¼	5.7	25.1
W. C	7.0	23.8
W. L	6.8	24.0

30.77

80 = N. L. NOELL		
W. L	7.5	23.3
W. C	7.3	23.5
W. ¼	6.0	24.8
½	5.4	25.4
E ¼	5.2	25.6
E C	5.2	25.6
E. L	5.0	25.8
25 N. OF NOELL		
E. L	5.0	25.8
E C	5.2	25.6
E ¼	5.3	25.5
½	5.1	25.7
W ¼	6.6	24.2
W. C	7.0	23.8
W. L	7.7	23.1
50 N. OF NOELL		

30.77

W.L	7.8	23.0
W.C	6.9	23.9
22-E	6.8	24.0
28 E	5.7	25.1
1/2	5.2	25.6
E 1/4	5.4	25.4
E C	5.4	25.4
E.L	4.6	26.2
75 N. OF NOELL		
E.L	4.4	26.4
E.C	5.5	25.3
E.1/4	5.4	25.4
1/2	5.7	25.1
W. 1/4	6.4	24.4
W.C	7.2	23.6
W.L	7.8	23.0
100 N. OF NOELL		
W.L	7.9	22.9

30.77

31

W.C	7.4	23.4
W 1/4	6.3	24.5
1/2	5.8	25.0
E 1/4	5.5	25.3
E.C	5.4	25.4
E.L	4.2	26.6
125 N. OF NOELL		
E.L	4.4	26.4
E.C	5.3	25.5
E.1/4	5.3	25.5
1/2	5.6	25.2
W. 1/4	6.4	24.4
W.C	7.2	23.6
W.L	8.1	22.7
150 N OF NOELL		
W.L	8.1	22.7
W.C	7.0	23.8

30.77

W. 1/4	5.7	25.1
1/2	5.5	25.3
E 1/4	5.2	25.6
E. C	4.8	26.0
E. L	3.2	27.6
175 - N. OF NOELL		
E. L	3.0	27.8
E. C	4.9	25.9
E 1/4	5.1	25.7
1/2	5.2	25.6
W 1/4	5.6	25.2
21-E	6.4	24.4
W. C	6.8	24.0
W. L	7.9	22.9
200 N. OF NOELL		
W. L	7.8	23.0
W. C	6.6	24.2

30.77

21-E.	6.2	24.6
W 1/4	5.4	25.4
1/2	5.2	25.6
E 1/4	5.0	25.8
E. C.	4.6	26.2
C9-E	3.1	27.7
E. L	2.4	28.4
225 N. OF NOELL		
E. L	2.5	28.3
E. C	4.2	26.6
E 1/4	4.9	25.9
1/2	5.1	25.7
W 1/4	5.4	25.4
21-E	6.3	24.5
W 1/4	7.0	23.8
W. L	7.7	23.1
250 N. OF NOELL		

30.77

W. L	7.5	23.3
W. C	6.7	24.1
22-E	6.1	24.7
W. 1/4	4.8	26.0
1/2	4.4	26.4
E 1/4	5.0	25.8
E. C.	4.0	26.8
E. L.	2.9	27.9

275 N. OF NOELL

E. L	2.7	28.1
E C	3.8	27.0
E 1/4	5.0	25.8
1/2	4.7	26.1
W 1/4	5.2	25.6
21-E	6.1	24.7
W. C	6.5	24.3
W. L	7.2	23.6

30.77

300 N. OF NOELL = S. L. ESTUDILLO

W. L	7.9	22.9
W. C	7.0	23.8
21-E	6.5	24.3
W 1/4	5.5	25.3
1/2	4.8	26.0
E 1/4	4.8	26.0
E. C	3.7	26.9
E. L	2.4	28.4

14 = S. C. ESTUDILLO

E. L	2.4	28.4
E. C	3.6	27.2
5C-E	4.8	26.0
E 1/4	4.8	26.0
1/2	4.8	26.0
W 1/4	5.3	25.5
21-E	6.7	24.1

	30.77		
W. C	7.3	23.5	
W. L	8.1	22.7	
27 = S 1/4 ESTUDILLO			
W. L	8.1	22.7	
W. C	7.1	23.7	
21-E	6.4	24.4	
W. 1/4	5.1	23.7	
1/2	4.8	26.0	
E 1/4	4.8	26.0	
57-E	4.8	26.0	
E.C	3.C	27.2	
E.L	2.7	28.1	
40 = 1/2 ESTUDILLO			
E.L	2.C	28.2	
E.C	3.3	27.5	
55-E	4.7	26.1	
E 1/4	4.7	26.1	

		30.77 2.21 28.56 1.91 30.47		
1/2			5.0	25.8
W 1/4			5.1	25.7
21-E			6.4	24.4
W.C.			7.0	23.8
W.L			7.9	22.9
B.M.	SPIKE IN PHONE POLE, AT N.E. COR ESTUDILLO HANCOCK		2.21	28.56
	1.91	30.47	2.21	28.56
53 = N 1/4 ESTUDILLO				
W.L			7.7	22.8
W.C			6.7	23.8
21-E			6.0	24.5
W.1/4			4.7	25.8
1/2			4.7	25.8
E.1/4			4.3	26.2
55-E			4.1	26.4
E.C			3.0	27.5
E.L			1.7	28.8

30.47

66 = N. C. ESTUDILLO

E. L	1.6	28.9
E. C	2.7	27.8
55-E	4.3	26.2
E 1/4	4.5	26.0
1/2	4.6	25.9
W 1/4	4.6	25.9
21-E	5.8	24.7
W. C	6.3	24.2
W. L	7.1	23.4

80 = N. L ESTUDILLO

W. L	7.1	23.4
W. C	5.9	24.6
W 1/4	4.8	25.7
1/2	4.5	26.0
E 1/4	4.2	26.3
53-E	4.1	26.4

30.47

E C	2.6	27.9
E. L	1.4	29.1

25 N. OF ESTUDILLO

E. L	1.2	29.3
E. C	2.6	27.9
E 1/4	3.9	26.6
1/2	4.5	26.0
W 1/4	4.9	25.6
W C	6.0	24.5
W. L	6.8	23.7

50 N. OF ESTUDILLO

W. L	7.0	23.5
W. C	5.5	25.0
W 1/4	4.4	26.1
1/2	4.1	26.4
E 1/4	3.9	26.6
E C	2.1	28.4

30.47

E. L	0.7	29.8
75 N. OF ESTUDILLO		
E. L	0.2	30.3
E. C	1.2	29.3
55-E	2.9	27.6
E 1/4	3.5	27.0
1/2	4.3	26.2
W 1/4	4.4	26.1
W. C	4.9	25.6
W. L	6.3	24.2
100 N. OF ESTUDILLO		
W. L	6.0	24.5
W. C	5.3	25.2
W 1/4	4.4	26.1
1/2	3.7	26.8
E 1/4	2.6	27.9
E. C	0.8	29.7

30.47

E. L	+ 0.2	30.3
125 N. OF ESTUDILLO		
E. L	0.0	30.5
E. C	0.9	29.6
E. 1/4	2.5	28.0
1/2	3.3	27.2
W 1/4	4.0	26.5
W. C	4.6	25.9
W. L	5.4	25.1
150 N. OF ESTUDILLO		
W. L	5.3	25.2
W. C	4.3	26.2
W 1/4	4.0	26.5
1/2	3.5	27.0
E 1/4	2.8	27.7
E. C	0.9	29.6
E. L	0.0	30.5

30.47

175 N. OF ESTUDILLO

E.L	+ 0.3	30.2
E.C	1.0	29.5
E.¼	2.3	28.2
½	3.5	27.0
W.¼	3.9	26.6
W.C	4.0	26.5
W.L	5.0	25.5

200 N. OF ESTUDILLO

W.L	4.7	25.8
W.C	3.9	26.6
W.¼	3.9	26.6
½	3.2	27.3
E.¼	2.2	28.3
E.C	1.0	29.5
E.L	0.0	30.5

225 N. OF ESTUDILLO

30.47

E.L	0.3	30.2
E.C	1.0	29.5
E.¼	2.7	27.8
½	3.3	27.2
W.¼	4.0	26.5
W.C	4.0	26.5
W.L	5.0	25.5

250 N. OF ESTUDILLO

W.L	5.3	25.2
W.C	4.3	26.2
W.¼	4.1	26.4
½	3.5	27.0
E.¼	2.4	28.1
E.C	1.3	29.2
E.L	0.4	30.1

275 N. OF ESTUDILLO

E.L	0.5	30.0

		30.47					30.47		
W.C			1.3	29.2		E.L		0.9	29.6
55-E			1.6	28.9		E.C		2.0	28.5
44-E			3.5	27.0		53-E		2.5	28.0
1/2			3.7	26.8		46 E		4.3	26.2
W 1/4			4.3	26.2		1/2		4.7	25.8
W C			4.8	25.7		W 1/4		5.0	25.5
W.L			5.7	24.8		W C		5.C	24.9
	300 N. OF ESTUDILLO = S. L. WRIGHT					W.L		6.7	23.8
W.L			6.4	24.1			27 = S 1/4 WRIGHT.		
W.C			5.3	25.2		W.L		6.7	23.8
W 1/4			4.7	25.8		W.C		5.6	24.9
1/2			4.4	26.1		W.1/4		5.2	25.3
45-E			3.9	26.6		1/2		5.0	25.5
55-E			2.1	28.4		E 1/4		4.3	26.2
EC			1.7	28.8		5C-E		2.C	27.9
E.L			0.7	29.8		E C		2.3	28.2
	74 = S.C WRIGHT					E.L		1.1	29.4

30.47

40 = ½ WRIGHT.

E.L	1.6	28.9
E.C	2.6	27.9
5C-E	3.0	27.5
5AE.	4.4	26.1
E¼	4.C	25.9
½	5.3	25.2
W¼	5.4	25.1
W C	5.7	24.8
W.L	7.0	23.5

53 = N ¼ WRIGHT

W.L	7.1	23.4
W.C	6.1	24.4
W¼	5.6	24.9
½	5.5	25.0
E¼	4.C	25.9
55-E	3.4	27.1

30.47

E C	3.1	27.4
E.L	2.0	28.5

CC = N.C. WRIGHT

E.L	2.2	28.3
E.C	3.5	27.0
54-E	3.9	26.6
55-E	4.C	25.9
E¼	4.7	25.8
½	5.8	24.7
W¼	5.5	25.0
W C	6.3	24.2
W.L	7.5	23.0

50 = N. L. WRIGHT

W.L	7.8	22.7
W.C	6.5	24.0
W¼	5.9	24.6
½	6.0	24.5

30.47
2.98
27.49

30.47

30.47
2.13
28.34
28.63
.29 - CK

E 1/4			5.1	25.4
E C			3.7	26.8
E. L			2.7	27.8
B.M.	R.R. SPIKE IN PHONE POST AT N.E. COR.	WRIGHT HANCOCK	2.98	27.49
	25 N. - WRIGHT			
E. L			3.5	27.0
E. C			4.6	25.9
E 1/4			5.8	24.7
1/2			6.5	24.0
W 1/4			6.7	23.8
W C			7.5	23.0
W. L			8.6	21.9
	50 N. - WRIGHT			
W. L			8.8	21.7
W. C			8.0	22.5
W. 1/4			7.1	23.4
1/2			6.8	23.7

30.47

E 1/4			6.4	24.1
E C			5.8	24.7
E. L			4.5	26.0
	75 N. - WRIGHT			
E. L			4.5	26.0
E. C			6.1	24.4
E 1/4			6.9	23.6
1/2			7.1	23.4
W 1/4			7.7	22.8
W C			8.4	22.1
W. L			9.4	21.1
	100 N. - WRIGHT			
W. L			9.8	20.7
W. C			9.0	21.5
W 1/4			8.4	22.1
1/2			7.6	22.9
E 1/4			7.5	23.0

3047

E.C	6.7	23.8
E.L	5.5	25.0

125 - N. - WRIGHT

E.L	6.2	24.3
E.C	7.3	23.2
E. 1/4	7.8	22.7
1/2	8.3	22.2
W 1/4	9.1	21.4
W C	9.7	20.8
W.L	10.4	20.1

150 N - WRIGHT

W.L	11.0	19.5
W.C	10.2	20.3
W. 1/4	9.3	21.2
1/2	8.9	21.6
E 1/4	7.9	22.6
E.C	7.7	22.8

3047

E.L	6.8	23.7

175 - N. - WRIGHT

E.L	7.3	23.2
E.C	7.8	22.7
E. 1/4	8.4	22.1
1/2	9.3	21.2
W. 1/4	9.9	20.6
W.C	10.7	19.8
W.L	11.5	19.0

200 - N. - WRIGHT

W.L	12.0	18.5
W.C	11.3	19.2
W. 1/4	10.3	20.2
1 1/2	9.6	20.9
E 1/4	8.7	21.8
E C	7.8	22.7
E.L	7.6	23.9

	0.02	23.02	7.47	23.00
	225 N. – WRIGHT			
E.L			0.5	22.5
E.C			1.1	21.9
E.¼			2.0	21.0
½			2.5	20.5
W ¼			3.4	19.6
W C			4.1	18.9
W L			5.0	18.0
	250 N – WRIGHT			
W.L			5.7	17.3
W.C.			4.7	18.3
W.¼			4.0	19.0
½			3.1	19.9
E ¼			2.3	20.7
EC			1.6	21.4
E.L			0.5	22.5
	275 N. WRIGHT			

		23.02		
E.L			1.1	21.9
E.C			2.1	20.9
E ¼			2.6	20.4
½			3.5	19.5
W ¼			4.5	18.5
W C			5.4	17.6
W.L			6.1	16.9
	300 N – WRIGHT = S.L BANDINI			
W.L			6.7	16.3
W.C			5.8	17.2
W.¼			5.1	17.9
½			4.1	18.9
E ¼			3.3	19.7
EC			2.6	20.4
E.L			1.6	21.4
	14 = S.C – BANDINI			
E.L			1.9	21.1

23.02

E.C.	2.9	20.1
E.¼	3.7	19.3
½	4.1	18.9
W¼	5.2	17.8
W C	5.9	17.1
W. L	6.9	16.1

27 = S ¼ BANDINI

W L	7.1	15.9
W. C	6.3	16.7
W. ¼	5.C	17.4
½	4.7	18.2
E ¼	3.9	19.1
E C	3.1	19.9
E L	2.3	20.7

40 = ½ - BANDINI

E L	2.6	20.4
E C	3. C	19.4

23.02

E¼	4.2	18.8
½	4.9	18.1
W¼	5.8	17.2
W. C	6.5	16.5
W. L	7.5	15.5

53 = N ¼ BANDINI

W. L	7.7	15.3
W. C	7.0	16.0
W. ¼	6.2	16.8
½	5.3	17.7
E ¼	4. C	18.4
E C	3.9	19.1
E L.	3.0	20.0

66 = N. C. BANDINI

E L	3.3	19.7
E. C.	4.1	18.9
E ¼	5.0	18.0

23.02

1/2	5.5	17.5	
W 1/4	6.5	16.5	
W C	7.2	15.8	
W. L	8.1	14.9	
50 = N. L. BANDINI			
W. L	8.3	14.7	
W. C	7.5	15.5	
W. 1/4	6.8	16.2	
1/2	5.9	17.1	
E 1/4	5.4	17.6	
EC	4.4	18.6	
E L	3.6	19.4	
25 N. - BANDINA			
E. L	4.2	18.8	
E. C.	5.2	17.8	
E. 1/4	6.1	16.9	
1/2	6.4	16.6	

23.02

W 1/4	7.4	15.6	
W. C	8.0	15.0	
W. L	8.7	14.3	
50 N. - BANDINI			
W. L.	9.4	13.6	
W. C	8.6	14.4	
W 1/4	7.9	15.1	
1/2	7.2	15.8	
E 1/4	6.5	16.5	
E C	5.7	17.3	
E. L	4.6	18.4	
75 N. - BANDINI			
E. L	5.5	17.5	
E. C	6.3	16.7	
E 1/4	7.1	15.9	
r 1/2	7.6	15.4	
W 1/4	8.4	14.6	

23.02

W.C		9.1	13.9
W.L		9.6	13.4
B.M	AR. SPIKE IN PHONE POST NEAR COR. BANDINI & HANCOCK	3.64	19.38
	100 N. - BANDINI		
W.L		9.9	13.1
W.C		9.5	13.5
W.1/4		8.8	14.2
1/2		7.9	15.1
E 1/4		7.5	15.5
E C		6.8	16.2
E L		6.1	16.9
	125 N. - BANDINI		
E.L		6.4	16.6
E.C		7.3	15.7
E.1/4		8.4	14.6
1/2		8.9	14.1
W.1/4		9.4	13.6

23.02

W.C		10.0	13.0
W.L		10.9	12.3
	150 N BANDINI		
W.L		11.8	11.2
W.C		10.5	12.5
W.1/4		9.7	13.3
1/2		9.1	13.9
E 1/4		8.6	14.3
E C		8.0	15.0
E.L		7.1	15.9
	175 - N. - BANDINI		
E.L		7.9	15.1
E.C		8.7	14.3
E 1/4		9.2	13.8
1/2		9.4	13.6
W 1/4		10.2	12.8
W C		11.5	11.5

		23.02 5.90 14 11.2 14.88		
W.L			11.7	11.3
	200 N - BANDINI			
W.L			12.3	10.7
W.C			11.4	11.6
W 1/4			11.1	11.9
1/2			10.7	12.3
E 1/4			9.6	13.4
E C.			9.1	13.9
E.L			8.4	14.6
AT STA	20.76	14.88	8.90	14 12
	225 N OF BANDINI			
E.L			0.8	14.1
E.C			1.2	13.7
E.1/4			2.6	12.3
1/2			2.8	12.1
W 1/4			3.3	11.6
W C			4.3	10.6

		14.88		
W.L			4.8	10.1
	250 N. OF BANDINI			
W.L			4.7	10.2
W.C			4.3	10.6
W 1/4			3.6	11.3
1/2			3.2	11.7
E 1/4			2.6	12.3
E C.			2.2	12.7
E.L			0.7	14.2
	275 N. OF BANDINI			
E.L			1.8	13.1
E.C			2.1	12.8
E.1/4			3.0	11.9
1/2			3.6	11.3
W.1/4			4.2	10.7
W.C			4.6	10.3
W.L			5.1	9.8

14.88

300 N OF BANDINI = S.L COUTS.

W.L	4.9	10.0
W.C	4.6	10.3
W 1/4	4.1	10.8
1/2	3.7	11.2
E 1/4	3.1	11.8
E C	2.4	12.5
E L	1.9	13.0

14 = S.C COUTS

E. L	1.5	13.4
E. C	2.5	12.4
E 1/4	3.5	11.4
1/2	3.7	11.2
W.1/4	4.3	10.6
W. C	4.7	10.2
W. L	4.9	10.0

27 = S 1/4 COUTS

14.88

W. L	5.0	9.9
W. C	4.6	10.3
W. 1/4	4.5	10.4
1/2	3.9	11.0
E 1/4	3.5	11.4
E C	2.9	12.0
E L	1.7	13.2

40 = 1/2 COUTS

E.L.	1.9	13.0
E.C	3.1	11.8
E 1/4	3.4	11.5
1/2	3.9	11.0
W 1/4	4.3	10.6
W. C	4.6	10.3
W L	5.0	9.9

53 = N 1/4 COUTS.

W. L	5.0	9.9

14.88

W.C			4.6	10.3
W.¼			4.2	10.7
½			4.0	10.9
E¼			3.3	11.6
E.C			2.9	12.0
E.L			2.3	12.6
	66 =	N.C.	COUTS.	
E.L.			2.4	12.5
E.C.			2.9	12.0
E¼			3.6	11.3
½			3.9	11.0
W.¼			4.1	10.8
W.C			4.6	10.3
W.L			5.1	9.8
	80 =	N.L.	COUTS	
W.L			5.1	9.8
W.C			4.6	10.3

14.88

W¼			4.1	10.8
½			3.8	11.1
E¼			3.6	11.3
E.C			2.9	12.0
E.L			2.3	12.6
	25 N.	OF	COUTS.	
E.L.			2.4	12.5
E.C			3.2	11.7
E.¼			3.4	11.5
½			3.8	11.1
W.¼			4.3	10.6
W.C			4.6	10.3
W.L			5.1	9.8
	50 N.	OF	COUTS	
W.L.			5.0	9.9
W.C			4.5	10.4
W¼			4.3	10.6

14.88

½		3.9	11.0
E ¼		3.4	11.5
E C		2.8	12.1
E L		2.6	12.3
75 N. OF COUTS.			
E L		2.6	12.3
E C		2.9	12.0
E ¼		3.5	11.4
½		3.9	11.0
W ¼		4.4	10.5
W C		4.7	10.2
W L		5.0	9.9
100 N. OF COUTS.			
W L		5.0	9.9
W C		4.7	10.2
W ¼		4.3	10.6
½		3.7	11.2

14.88

E ¼		3.4	11.5
E C		3.2	11.7
E L		2.2	12.7
125 N. OF COUTS.			
E L		2.3	12.6
E C		3.0	11.9
E ¼		3.6	11.3
½		3.9	11.0
W ¼		4.2	10.7
W C		4.4	10.5
W L		4.9	10.0
150 N OF COUTS.			
W L		5.1	9.8
W C		4.5	10.4
W ¼		4.0	10.9
½		3.9	11.0
E ¼		3.6	11.3

14.88

E C.	2.9	12.0
E L.	2.5	12.4
175 N. OF COUTS.		
E L	2.4	12.5
E C.	3.0	11.9
E 1/4	3.5	11.4
1/2	4.0	10.9
W. 1/4	4.2	10.7
W. C.	4.3	10.6
W L.	5.1	9.8
200 N. OF COUTS.		
W. L.	4.9	10.0
W. C.	4.8	10.1
W. 1/4	4.6	10.3
1/2	3.9	11.0
E 1/4	3.5	11.4
E C	3.0	11.9

14.88

E. L.	2.5	12.4
225 N. OF COUTS.		
E L.	2.6	12.3
E. C.	3.1	11.8
E. 1/4.	3.5	11.4
F 1/2.	4.0	10.9
W. 1/4.	4.3	10.6
W C.	4.7	10.0
W. L	5.3	9 6
250 N. OF COUTS.		
W. L	5.1	9.8
W. C.	5.0	9.9
W 1/4	4.7	10.2
1/2	3.9	11.0
E 1/4	3.5	11.4
E C.	3.2	11.7
E L	2.6	12.3

14.88

275 N. OF COUTS.

E.L	2.6	12.3
E.C	3.2	11.7
E 1/4	3.6	11.3
1/2	4.3	10.6
W 1/4	4.7	10.2
W C	4.8	10.1
W L	5.3	9.6

300 N. OF COUTS.

W.L	5.2	9.7
W.C	4.8	10.1
W 1/4	4.4	10.5
1/2	4.2	10.7
E 1/4	4.0	10.9
E C	3.3	11.6
E. L	2.7	12.2

325 N. OF COUTS

14.88

E.L	2.9	12.0
E.C	3.5	11.4
E. 1/4	3.9	11.0
1/2	4.3	10.6
W 1/4	4.6	10.3
W C	4.9	10.0
W L	5.8	9.1

350 N. OF COUTS.

W.L	6.0	8.9
W.C	5.2	9.7
W 1/4	4.9	10.0
1/2	4.6	10.3
E 1/4	3.9	11.0
E C	3.8	11.1
E L	3.2	11.7

355.5 N. OF COUTS

E.L	3.3	11.6

		14.88		
E.C			3.8	11.1
E.1/4			4.0	10.9
1/2			4.6	10.3
W.1/4			5.0	9.9
W.C			5.4	9.5
W.L			6.2	8.7
	365.5 – 355.5 N. =		S.L.	WITHERBY.
W.L			7.1	7.8
W.C			5.9	9.0
W.1/4			5.1	9.8
1/2	ON HUB. 10.25 / 10.25 / CO-CK.		4.63	10.25
E.1/4			4.1	10.8
E.C			3.8	11.1
E.L			3.3	11.6
B.M.	SPIKE IN PHONE POLE / S.E. COR WITHERBY. / HANCOCK		2.77	12.11
	7.91	20.02	2.77	12.11
B.M.	NAIL & STAPLE IN PHONE POLE. 100 E. ON WITHERBY. / B.S. & P.R.R. 24.51 G.D. / 18.75 C.D. / 5.76 DIF. TO 5.82 GOV. 5.77 GEOL.		1.27	18.75

CROSS-SECTIONS OVER
KURTZ ST. (1ST)
CALIFORNIA – NOELL {COVERT, WETMORE, MOORE}
NOV. 16, 1905

B.M.	7.75	29.73		21.78	CALIFORNIA-VINE 50' W. OF NO. COR SPIKE IN POLE
B.M.	ON PLUG AT CENTER KURTZ AND WEST LINE OF CALIFORNIA		3.53	26.20	
	WEST LINE OF CALIFORNIA.				
E.L.			2.8		26.9
E.C			2.5		27.2
E.1/4			2.7		27.0
1/2			3.4		26.3
W.1/4			3.9		25.8
W.C			4.2		25.5
W.L.			4.6		25.1
	189.34	SOUTH OF BEAN			
W.L			6.0		23.7
W.C			4.6		25.1
W.1/4			4.1		25.6
1/2			3.3		26.4
E.1/4			3.2		26.5

29.73

E C	2.5	27.2
E. L	2.8	26.9
175 S. – BEAN.		
E. L	2.0	27.7
E. C	2.6	27.1
E ¼	3.3	26.4
½	4.0	25.7
W ¼	4.1	25.6
W. C	4.6	25.1
W. L	6.2	23.5
150 S – BEAN		
W. L	6.1	23.6
W. C	4.6	25.1
W. ¼	4.1	25.6
½	3.5	26.2
E ¼	2.8	26.9
E C.	2.5	27.2

29.73

E. L	1.9	27.8
125 S – BEAN.		
E. L	1.4	28.3
E. C	2.4	27.3
E ¼	2.9	26.8
½	3.6	26.1
W. ¼	4.1	25.6
W. C	4.3	25.4
W L	5.9	23.8
100 S – BEAN		
W. L	5.1	24.6
W. C	4.6	25.1
W. ¼	3.8	25.9
½	3.2	26.5
E ¼	2.7	27.0
E. C.	1.9	27.8
E L	1.3	28.4

29.73

75 S. - BEAN.

E.L	1.2	28.5
E.C	1.9	27.8
E 1/4	2.6	27.1
1/2	3.2	26.5
W 1/4	3,9	25.8
W.C	4.5	25.2
W.L	4.8	24.9

50 S - BEAN.

W.L	5.6	24.1
W.C	4,7	25.0
W 1/4	4.2	25.5
1/2	3.3	26.4
E 1/4	2.5	27.2
EC	1.8	27.9
E.L	1,1	28.6

25 S. - BEAN.

29.73

E.L	1.1	28.6
E.C	2.0	27.7
E 1/4	2.7	27.0
1/2	3.4	26.3
W. 1/4	4.1	25.6
W.C	5.2	24.5
W.L	5.6	24.1

0 = S.L. BEAN

W.L	5.9	23.8
W.C	4.5	25.7
W 1/4	4.3	25.4
1/2	3.3	26.4
E 1/4	2.6	27.1
E.C	2.0	27.7
E.L	1.1	28.6

14 = S.C. BEAN

E.L	1.1	28.6

		29.73			
EC.			1.7		28.0
E. 1/4			2.6		27.1
~~1/2~~			3.7		26.0
W. 1/4			3.7		26.0
W. C.			4.5		25.2
W. L			5.9		23.8
	27 =	S 1/4	BEAN.		
W. L.			5.5		24.2
W. C			4.5		25.2
W. 1/4			3.6		26.1
1/2			3.1		26.6
E. 1/4			2.2		27.5
EC			1.8		27.9
E L			1.0		28.7
	40 =	1/2	BEAN.		
E L.			0.6		29.1
EC.			1.5		28.2

		29.73 2.80 26.93 4.31 31.24			
E 1/4			2.4		~~28.8~~ 27.3
1/2			2.8		~~28.4~~ 26.9
W. 1/4			3.4		~~27.8~~ 26.3
W. C			4.8		~~26.4~~ 24.9
W. L			5.6		24.1
ON CENTER PLUG	4.31	31.24	2.80	26.93	
	53 =	N. 1/4	BEAN.		
W. L.			7.1		24.1
W. C			6.2		25.0
W 1/4			4.8		26.4
1/2			4.0		27.2
E 1/4			3.7		27.5
E C			2.9		28.3
E L.			2.0		29.2
	66 =	N. C.	BEAN.		
E. L.			2.0		29.2
E. C.			3.2		28.0
E. 1/4			3.4		27.8

31.24

1/2.	3.9	27.3
W 1/4.	5.1	26.1
W.C.	6.3	24.9
W.L.	7.2	24.0
80 = N.L. BEAN.		
W.L.	7.0	24.2
W.C.	5.7	25.5
W 1/4.	5.2	26.0
1/2.	4.0	27.2
E 1/4.	3.2	28.0
E.C.	3.0	28.2
E.L.	2.0	29.0
25 N. OF BEAN.		
E.L.	2.0	29.2
E.C.	2.5	28.7
E 1/4	3.2	28.0
1/2	4.2	27.0

31.24

W.1/4.	4.7	26.5
W.C.	5.3	25.9
W.L.	6.9	24.3
50 N. - BEAN.		
W.L.	6.4	24.8
W.C.	5.1	26.1
W.1/4.	4.1	27.1
1/2.	3.9	27.3
E 1/4.	3.2	28.0
E.C.	2.6	28.6
E.L.	1.8	29.4
75 N. OF BEAN.		
E.L.	1.7	29.5
E.C.	2.5	28.7
E. 1/4	3.4	27.8
1/2.	3.6	27.6
W. 1/4	4.0	27.2

31.24

W. C.	5.8	25 4
W. L.	6.5	24. 7
100 N. - BEAN.		
W. L.	6.0	25.2
W. C.	6,5	24. 7
W. 1/4	5.2	26.0
1/2.	3, 8	27 .4
E 1/4.	3.2	28.0
EC.	2.9	28 3
E L.	1, 9	29 3
125 N. - BEAN.		
E. L.	2. 2	29.0
E.C	2,7	28. 5
E 1/4.	3, 4	27. 8
1/2.	4.6	26. 6
W. 1/4	5. 3	25 9
W. C	6. 5	24. 7

31.24

W. L.	5.6	25 .6
150 N. - BEAN		
W. L	7.0	24.2
W. C.	5.6	25 6
W. 1/4.	6.3	24 9
1/2.	4.2	27. 0
E 1/4.	3.8	27. 4
E. C.	2, 6	28. 6
E. L.	2. 6	28 .6
175 N. - BEAN.		
E. L.	2. 7	28. 5
E. C.	3. 3	27. 9
E 1/4.	3. 8	27 .4
1/2.	5. 6	25 .6
W. 1/4.	5. 7	25 3
W. C	5. 8	25 4
W. L	7. 1	24. 1

31.24

200 N. - BEAN.

W. L.	7.4	23 8
W. C.	6.7	24 5
W. 1/4.	5.8	25. 4
1/2.	5.6	25 6
E 1/4.	5.6	25.6
E C.	4.1	27.1
E. L.	3.2	28.0

225 N. - BEAN

E. L.	3.9	27.3
E. C.	5.6	25 6
E 1/4.	5.6	25 6
1/2.	6.3	24. 9
W. 1/4.	6.5	24 7
W. C.	6.8	24. 4
W. L.	7.2	24 0

250 N. - BEAN.

31.24.

W. L.	7.9	23.3
W. C.	7.3	23 9
W. 1/4.	6.7	24.5
1/2.	6.2	25.0
E 1/4.	5.6	25.6
E. C.	5.6	25 6
E. L.	3.9	27.3

275 N. OF BEAN

E. L.	5.0	26.2
E. C.	5.1	26.1
E 1/4.	6.2	25.0
1/2.	6.4	24.8
W. 1/4.	7.1	24.1
W. C.	7.4	23.8
W. L.	7.9	23 3

298.7 N. - BEAN = S. L. STORY.

W. L.	8.0	23.2

31.24

W. C	7.4	23.8
W. 1/4	7.0	24.2
1/2	6.3	24.9
E 1/4	6.1	25.1
E. C	5.3	25.9
E. L	5.1	26.1
14 = S. C. STORY.		
E. L	4.8	26.4
E. C.	5.3	25.9
E. 1/4	6.0	25.2
1/2	6.7	24.5
W 1/4	7.0	24.2
W. C	7.5	23.7
W. L	7.9	23.3
27 = S 1/4 STORY.		
W. L	7.8	23.4
W. C	7.4	23.8

31.24

W. 1/4	6.8	24.4
1/2	6.4	24.8
E. 1/4	5.8	25.4
E. C.	5.7	25.5
E. L.	4.8	26.4
40 = 1/2 STORY.		
E. L	4.8	26.4
E. C	5.5	25.7
E 1/4	5.8	25.4
1/2	6.2	25.0
W. 1/4	6.5	24.7
W. C	7.1	24.1
W. L	7.6	23.6
53 = N 1/4 STORY.		
W. L.	7.6	23.6
W. C.	7.1	24.1
W 1/4	6.7	24.5

31.24

1/2	6.2	25.0
E 1/4	5.9	25 3
E.C	5.2	26.0
E.L	4.5	26 7
66 = N. C. STORY		
E.L	4.8	26 4
E.C.	4.9	26 3
E. 1/4	5.5	25. 7
1/2.	5.9	25 3
W.1/4.	6.5	24 7
W. C.	6. 8	24 .4
W. L.	7. 4	23 8
80 = N. L. STORY.		
W. L.	7.4	23 .8
W. C	6.5	24 7
W 1/4	6.0	25.2
1/2	5. 6	25 .6

31.24

E. 1/4	4.9	26 3
E.C.	4.5	26 .4
E. L.	4.6.	26 6
25 N. - STORY.		
E.L	3..5	27 7
E.C	4.2	27. 0
E.1/4.	4.5	26 7
1/2.	5.1	26. 1
W. 1/4.	5.5	25 7
W. C.	6. 0	25. 0
W. L	6. 8	24.4
50 N. - STORY.		
W. L.	6. 2	25. 0
W. C.	5. 6	25, 6
W. 1/4	4.9	26 3
1/2	4.6	26. 6
E. 1/4	4.0	27.2

31.24

E.C.	3.6	27 6
E.L.	3.6	27.6
75 N. -STORY.		
E.L.	2.9	28 3
E.C.	3.3	27 .9
E 1/4	4.1	27.1
1/2	4.3	26 9
W. 1/4	4.8	26 4
W.C.	5.3	25 9
W.L.	5.9	25 .3
100 N. -STORY		
W.L.	5.3	25 9
W.C	4.6	26 6
W. 1/4	4.2	27.0
1/2	3.9	27 3
E 1/4	3.3	27. 9
EC	2.7	28 5

31.24

E.L.	2.4	28. 8
125 N. -STORY.		
E.L	2.1	29.1
E.C.	2.9	28. 3
E 1/4	2.7	28.3
1/2	3.3	27 9
W. 1/4	3.7	27 5
W.C	4.4	26.8
W.L	4.8	26 .4
150 N. STORY.		
W.L.	4.2	27.0
W.C	4.0	27.2
W. 1/4	3.3	27.9
1/2	2.8	28 .4
E 1/4	2.4	28 .8
EC	1.9	29 .3
E.L	1.5	29 .7

31.24

175 N. - STORY.

E. L.	1.2	30.0
E. C.	1.7	29 5
E. ¼	2.2	29.0
½	2.7	28.5
W. ¼	3.2	28.0
W. C.	3.7	27.5
W. L.	4.3	26.9

200 N. - STORY.

W. L.	4.0	27.2
W. C.	3.5	27.7
W. ¼	3.2	28.0
½	2.6	28.6
E. ¼	2.0	29.2
E. C.	1.7	29 5
E. L.	1.2	30.0

225 N. - STORY.

31.24

E. L.	1.6	29.6
E. C.	1.8	29.4
E. ¼	2.3	28.9
½	2.8	28 4
W. ¼	3.3	27 9
W. C.	3.7	27.5
W. L.	4.0	27.2

250 N. STORY.

W. L.	4.3	26.9
W. C.	4.1	27.1
W. ¼	3.7	27 5
½	3.1	28 1
E ¼	2.8	28 4
E C	2.5	28.7
E. L.	2.1	29 1

275 N. STORY

E. L.	2.5	28 7

31.24

E.C.	3.2	28.0
E 1/4	3.6	27.6
1/2	3.9	27.3
W. 1/4	4.5	26.7
W.C.	4.6	26.6
W.L	4.6	26.6
300 N-STORY. = S.L. HARASTHY.		
W.L.	5.6	25.6
W.C	5.2	26.0
W. 1/4	5.1	26.1
1/2	4.4	26.8
E 1/4	4.0	27.2
E.C.	3.5	27.7
E.L.	3.2	28.0
14 = S.C. HARASTHY.		
E.L	3.6	27.6
E.C	4.0	27.2

31.24

E 1/4	4.4	26.8
1/2	4.9	26.3
W 1/4	5.2	26.0
W.C	5.5	25.7
W.L	6.0	25.2
27 = S.C. HARASTHY		
W.L	6.3	24.9
W C	5.C	25.6
W 1/4	5.C	25.6
1/2	5.1	26.1
E 1/4	4.8	26.4
E C.	4.5	26.7
E.L	4.2	27.0
40 = 1/2 HARASTHY.		
E.L	4.4	26.8
E.C.	4.9	26.3
E. 1/4	5.1	26.1

60		31.24 5.80 25.44 .77 26.21			
½			5.5		25.7
W.¼			6.1		25.1
W.C.			6.2		25.0
74-W			6.6		24.6
W.L.			8.2		23.0
ON CENTER PLUG.	0.77	26.21	5.80	25.44	
53 = N. ¼ HARASTHY					
W.L.			5.3		20.9
73-W.			1.5		24.7
W. C.			1.4		24.8
W.¼			1.4		24.8
½			0.7		25.5
E.¼			0.6		25.6
E.C.			0.2		26.0
E.L.			0.0		26.2
66 = N.C. HARASTHY					
E.L.			0.2		26.0

		26.21			
E.C.			0.7		25.5
E.¼			0.9		25.3
½			1.3		24.9
W.¼			1.8		24.4
W.C.			2.0		24.2
72-W			2.0		24.2
W.L.			5.8		20.4
80 = N.L. HARASTHY					
W.L.			6.1		20.1
72-W			2.9		23.3
W.C.			2.4		23.8
W.¼			2.1		24.1
½			1.9		24.3
E.¼			1.5		24.7
E.C.			1.1		25.1
E.L.			0.6		25.6
25 N. = HARASTHY					

	26.21		
E.L	1.2		25.0
E.C	1.6		24.6
E 1/4	2.0		24.2
1/2	2.6		23.6
W 1/4	3.2		23.0
W C	3.5		22.7
71-W	3.4		22.8
W.L	7.0		19.2
50 N. - HARASTHY			
W.L	7.3		18.9
73-W	7.3		18.9
70-W	5.0		21.2
W.C	4.2		22.0
W 1/4	3.8		22.4
1/2	3.0		23.2
E 1/4	2.7		23.5
E C	2.3		23.9

	26.21		
E.L	1.9		24.3
75 - N. - HARASTHY			
E.L	1.9		24.3
E C	2.5		23.7
E 1/4	3.0		23.2
1/2	3.6		22.6
W. 1/4	4.3		21.9
W.C	4.6		21.6
69-W	5.6		20.6
72-W	7.3		18.9
W.L	7.2		19.0
85 - N - HARASTHY			
W.L	7.0		19.2
72-W	7.5		18.7
66-W	4.8		21.4
W C	4.3		21.9
W 1/4	4.3		21.9

	2C.21		
1/2	3.6	22.6	
E 1/4	3.2	23.0	
E C.	2.C	23.6	
9-W	2.5	23.7	
4-W	5.5	20.7	
E.L	5.4	20 8	
100 - N. - HARASTHY			
E.L	1.9	24 3	
7-W	3.3	22 9	
E. C	6.2	20.0	
23-W	2.5	23.4	
E 1/4	2.9	23 3	
1/2	3.3	22 9	
W 1/4	4.1	22.1	
W. C	4.6	21. 6	
71-W	7.4	18 8	
W. L	6.7	19. 5	

	2C.21		
	125 - N - HARASTHY		
W. L	6.7	19. 5	
70-W	7.8	18.4	
66-W	4.7	21 5	
W. C	4.5	21. 7	
W 1/4	4.0	22.2	
1/2	3.6	22. 6	
32-W	6.0	20.2	
E 1/4	6.5	19.7	
22-W	6.3	19 9	
17-W	3.9	22. 3	
E. C	3.6	22 6	
E. L	3.4	22.8	
150 N - HARASTHY			
E. L	4.4	21.8	
E. C	4.5	21. 7	
23-W	4.5	21 7	

26.21

28-W			7.5		18.7
33-W			6.7		19.5
1/2			4.6		21.6
W. 1/4			4.4		21.8
W. C			4.4		21.8
66-W			7.9		18.3
W. L			6.8		19.4
	175-N. - HARASTHY				
W. L	- ON. EAST RAIL		5.97		20.0
W. L			6.5		19.7
W. C.			8.5		17.7
60-W			6.2		20.0
W 1/4			5.5		20.7
1/2			5.4		20.8
35-W			7.2		19.0
E 1/4			8.1		18.1
21-W			5.5		20.7

26.21

E. C			5.1		21.1
E. L			5.1		21.1
	200 - N. - HARASTHY				
E. L			6.0		20.2
E. C			6.0		20.2
24-W			6.5		19.7
30-W			9.0		17.2
1/2			6.6		19.6
W. 1/4			7.2		19.0
56-W			7.2		19.0
W. C			8.9		17.3
W. L			6.2		20.0
	225 N. - HARASTHY				
W. L			6.3		19.9
67-W			7.2		19.0
W. C			9.3		16.9
W 1/4			9.1		17.1

		2C. 21 10. 34 15. 87			
47-W			9.7		16.5
1/2			8.2		18.0
E 1/4			6.9		19.3
E.C.			6.8		19.4
E.L.			7.2		19.0
	250 - N. - HARASTHY.				
E.L.			8.4		17.8
E.C.			8.3		17.9
E 1/4			8.9		17.3
31 W			9.9		16.3
1/2			9.4		16.8
W 1/4			10.0		16.2
53-W			10.8		15.4
65-W			7.3		18.9
W.L.			6.6		19.6
W.L.	ON WEST RAIL		6.30		19.9
B.M.	3.62	19.49	10.34	15.87	RESPIKE IN. TEL. POLE 50' SOUTH OF S.E. COR. OF KURTZ & CLAYTON

		19.49			
	275 N. - HARASTHY.				
W.L.			0.4		19.1
71-W			0.0		19.5
63-W			0.7		18.8
57-W			4.2		15.3
W. 1/4			3.8		15.7
1/2			3.9		15.6
E 1/4			4.1		14.4
E.C.			3.1		16.4
E.L.			2.7		16.8
	300 N. OF HARASTHY = S.L. CLAYTON				
E.L.			3.9		15.6
E.C.			3.7		15.8
E 1/4			5.0		14.5
1/2			4.8		14.7
42-W			5.8		13.7
W 1/4			4.7		14.8

19.49

54-W		4.3	15.2
62-W		0.9	18.6
69-W		0.0	19.5
W.L		0.9	18.6
	14 = S. C. CLAYTON.		
W.L		0.9	18.6
68-W		0.0	19.5
W.C		1.0	18.5
53-W		4.9	14.6
W 1/4		4.9	14.6
1/2		6.3	13.2
E 1/4		5.1	14.4
E.C		4.0	15.5
E.L		4.3	15.2
	27 = S 1/4 CLAYTON		
EL		4.7	14.8
E C		4.5	15.0

19.49

E 1/4		5.9	13.6
1/2		5.7	13.8
41-W		6.9	12.6
W. 1/4		5.0	14.5
53-W		4.8	14.7
W.C		1.0	18.5
68-W		0.1	19.4
W.L		0.9	18.6
	40 = 1/2 CLAYTON		
W.L		1.1	18.4
67-W		0.2	19.3
W.C		1.0	18.5
52-W		5.2	14.3
W 1/4		5.7	13.8
42-W		7.3	12.2
1/2		6.3	13.2
E 1/4		6.4	13.1

1949

E.C	5.3	14.2
E.L.	5.0	14.5
53 = N. 1/4 CLAYTON		
E.L	5.3	14.2
E.C	5.8	13.7
E 1/4	5.8	13.7
1/2	6.9	12.6
40-W	8.5	11.0
W 1/4	5.8	13.7
59-W	1.1	18.4
67-W	0.2	19.3
W.L	1.3	18.2
66 = N.C. CLAYTON		
W.L	1.5	17.7
66-W	0.3	19.2
58.W	1.3	18.2
W 1/4	6.3	13.2

1949

41-W	6.7	12.8
1/2	9.7	9.8
33-W	7.2	12.3
E 1/4	6.1	13.4
E.C	6.3	13.2
E.L	5.5	14.0
80 = N.L. CLAYTON.		
E.L	5.8	13.7
E.C.	7.0	12.5
E 1/4	6.7	12.8
32-W	7.4	12.1
1/2	9.2	10.3
40-W	7.1	12.4
47-W	6.9	12.6
57-W	1.4	18.1
65-W	0.4	19.1
73-W	1.4	18.1

1949.

W. L	2.9	16.6
25 N. OF CLAYTON.		
W. L	3.8	15.7
72-W	1.5	18.0
64-W	0.6	18.9
56 W	1.5	18.0
46-W	6.6	12.9
1/2	8.1	11.4
33-W	9.5	10.0
E 1/4	8.5	11.0
E. C	8.0	11.5
E. L	6.4	13.1
50 N. - CLAYTON		
E. L	6.1	13.4
7-W	6.6	12.9
10-W	8.0	11.5
E C	8.5	11.0

1949

E. 1/4	9.4	10.4
1/2	8.6	10.9
43-W	7.9	11 6
54-W	1.6	17 9.
W. C	0, 8	18.7
70-W	1, 8	17.7
W. L	4.3	15.2
75 - N. CLAYTON.		
W. L	5.3	14.2
69-W	1.9	17.6
W. C	0.7	18.8
62-W	1.7	17.8
41-W	7.5	12.0
1/2	8.4	11.1
E 1/4	9.8	9.7
E. C	8.8	10.7
E. L	6.4	13.1

1949

100 N. CLAYTON.

E. L	6.8	12.7
E. C.	8.0	11.5
E 1/4	9.8	9.7
31-W	10.4	9.1
1/2	8.3	11.2
52-W	2.0	17.5
59-W	0.9	18.6
67-W	2.0	17.5
W. L	5.6	13.9

125 N. CLAYTON.

W. L	7.0	12.5
66-W	2.1	17.4
58-W	0.9	18.6
50-W	1.9	17.6
1/2	7.5	12.0
E 1/4	9.2	10.3

1949

E. C	8.7	10.8
E. L	7.0	12.5

150 - N - CLAYTON

E. L	6.7	12.8
E. C	8.6	10.9
E. 1/4	8.8	10.7
1/2	7.8	11.7
W 1/4	1.9	17.6
57-W	1.0	18.5
64-W	2.1	17.4
W. L	8.5	11.0

175 N. - CLAYTON

W. L	9.6	9.9
63-W	2.6	16.9
55-W	1.2	18.3
47-W	2.2	17.3
1/2	8.4	11.1

19.49

E ¼	8.6	10.9
E.C	8.4	11.1
E.L	6.5	13.0
200 N. CLAYTON		
E.L	6.1	13.4
E.C	8.0	11.5
E ¼	8.5	11.0
38-W	8.1	11.4
45-W	2.2	17.3
53-W	1.2	18.3
W.C	2.3	17.2
W.L	9.7	9.8
225 N. CLAYTON		
W.L	9.2	10.3
69-W	8.2	11.3
59-W	2.3	17.2
52-W	1.3	18.2

19.49

43-W	2.5	17.0
36-W	7.4	12.1
E ¼	7.9	11.6
E.C	7.1	12.4
E.L	5.5	14.0
250-N. - CLAYTON.		
E.L	5.4	14.1
6-W	5.7	13.8
8-W	6.7	12.8
E.C	6.9	12.6
E ¼	7.5	12.0
35-W	7.3	12.2
43-W	2.6	16.9
51-W	1.4	18.1
58-W	2.3	17.2
67-W	8.2	11.3
W.L	9.1	10.4

19.49

275. N. CLAYTON

W. L	8.9	10.6
C7-W	8.4	11.1
57-W	2.5	17.0
W 1/4	1.6	17.9
41-W	2.4	17.1
34-W	6.8	12.7
E 1/4	6.8	12.7
E.C	6.8	12.7
8-W	6.2	13.3
E.L	5.2	14.3

300 = N. - CLAYTON = S.L. SOUTHERLAND

E.L	4.8	14.7
5-W	5.1	14.4
9-W	6.4	13.1
E.C	6.6	12.9
E 1/4	6.6	12.9

19.49

33-W	6.3	12.2
39-W	2.5	17.0
45-W	1.7	17.8
55-W	2.6	16.9
63-W	7.4	12.1
W.L	8.8	10.7

14 = S.C. - SOUTHERLAND.

W.L	8.9	10.6
W.C	7.2	12.3
54-W	2.5	17.0
47-W	1.7	17.8
39-W	2.7	16.8
34-W	6.0	13.5
E. 1/4	6.5	13.0
E.C	6.5	13.0
7-W	5.9	13.6
E.L	4.4	15.1

19.49

27 = S 1/4 SOUTHERLAND

E.L	4.1	15.4
4-W	4.2	15.3
E.C	6.2	13.3
E 1/4	6.6	12.9
33-W	5.7	13.8
38-W	2.7	16.8
46-W	1.8	17.7
54-W	2.8	16.7
59-W	6.5	13.0
W.L.	8.6	10.9

40 = 1/2 SOUTHERLAND

W.L	8.5	11.0
W.C	7.3	12.2
54-W	3.0	16.5
45-W	1.8	17.7
1/2	2.7	16.8

19.49.

32-W	5.9	13.6
E 1/4	6.1	13.4
E.C	6.2	13.3
5-W	4.0	15.5
E.L	3.8	15.7

53 = N. 1/4 - SOUTHERLAND

E.L	3.6	15.9
4-W	3.6	15.9
9-W	5.6	13.9
E.C.	5.9	13.6
E. 1/4	6.2	13.3
31-W	5.7	13.8
1/2	2.7	16.8
45-W	1.9	17.6
52-W	3.0	16.5
W.C	7.1	12.4
W.L	8.1	11.4

19.49

66 = N. C - SOUTHERLAND.

W.L		7.8		11.7
W.C		6.7		12.8
57-W		6.0		13.5
51-W		2.9		16.6
44-W		1.9		17.6
1/2		2.8	C	16.7
32-W		5.4		14.1
E 1/4		6.1		13.4
E C.		5.8		13.7
9-W		5.2		14.3
5-W		3.4		16.1
E L.		3.5		16.0

80 = N L. SOUTHERLAND.

E.L		3.5		16.0
10-W		4.9		14.6
E C		5.5		14.0

19.49
4.22
15.27
3.52
18.79

E. 1/4		5.4		14.1
32-W		4.8		14.7
35-W		3.1		16.4
44-W		1.9		17.6
52-W		3.1		15.4
57-W		5.8		13.7
W.C		5.9		13.6
W.L		7.7		11.8

SPIKE IN TEL. POLE. AT S.E COR. SOUTHERLAND & KURTZ.

B.M.	3.52	18.79	4.22	15.27

25 N. - SOUTHERLAND

W.L		5.4		13.4
W.C		4.6		14.2
54-W		4.4		14.4
50-W		2.6		16.2
42-W		1.4		17.4
34-W		2.4		16.4
30-W		3.6		15.2

15.7.9

E.¼		3,8	15.0
EC		3,8	15.0
E.L		3,2	15.6
	50 - N. - SOUTHERLAND		
E.L		2,0	16.8
E.C		2,5	16.3
E¼		3,2	14.6
30-W		3,8	15.0
33-W		2,2	16.6
40-W		1,5	17.3
W.¼		2.7	16.1
51-W		4,1	14.7
56-W		4,5	14.3
W.C		3,4	15.4
W.L		3.9	14.9
	75 N. - SOUTHERLAND		
W.L		2.4	16.4

15.7.9

W.C		2,3	16.5
54-W		4,0	14.8
47-W		2,9	15.9
39-W		1,7	17.1
32-W		2,5	16.3
28-W		3,7	15.1
23-W		1,3	17.5
E.C.		1,4	17.4
E.L.		1,5	17.3
	100 - N. - SOUTHERLAND		
E.L		1,6	17.2
EC		1,3	17.5
21-W		1,2	17.6
E.¼		3,7	15.1
30-W		2.8	16.0
½		1,8	17.0
45-W		1,9	16.9

18.79

51-w	4.1	14.7
54-w	2.5	16.3
W.C	3.2	15.6
W.L	3.4	15.4
125 - N. - SOUTHERLAND		
W.L	3.2	15.6
W.C	3.2	15.6
53-w	2.7	16.1
W 1/4	4.2	14.6
44-w	2.8	16.0
1/2	1.9	16.9
29-w	2.7	16.1
E 1/4	3.5	15.3
19-w	1.2	17.6
E C	1.1	17.7
E.L	0.9	17.9
150 N. - SOUTHERLAND		

18.79

E.L	0.1	18.7
7-w	1.5	17.3
E.C	0.8	18.0
18-w	1.1	17.7
25-w	3.C	15.2
27-w	2.8	16.0
1/2	1.9	16.9
42-w	2.8	16.0
W. 1/4	4.2	14.6
52-w	2.7	16.1
W.C.	3.3	15.5
W.L	3.8	15.0
175 N - SOUTHERLAND		
W.L	3.8	15.0
W.C	3.3	15.5
50-w	2.8	16.0
47-w	4.2	14.6

	18.79		
40-W		3.0	15.8
1/2			
~~34-W~~		2.6	16.3
34-W		2.1	16.7
E 1/4		3.1	15.7
22-W		3.6	15.2
17-W		1.0	17.8
E.C.		0.6	18.2
E.L.		0.6	18.2
	200 N. - SOUTHERLAND		
E L		0.9	17.9
E.C.		1.1	17.7
17-W		1.6	17.2
21-W		4.0	14.8
E 1/4		3.0	15.8
32-W		2.2	16.6
1/2		2.7	15.9
46-W		4.7	14.1

	18.79		
50-W		2.9	15.9
W.C.		3.7	15.1
W.L.		4.2	14.6
	225-N. SOUTHERLAND.		
W.L.		3.7	15.1
W.C.		3.8	15.0
48-W		2.9	15.9
45-W		4.7	14.1
1/2		3.2	15.6
31-W		2.5	16.3
25-W		3.1	15.7
18-W		4.0	14.8
14-W.		1.7	17.1
E L		1.5	17.3
	250-N - SOUTHERLAND		
E.L.		2.1	16.7
12-W		1.6	17.2

	18.79			
16-W		3.8		15.0
23-W		3.2		15.6
29-W		2.4		16.4
1/2		3.4		16.4
41-W		4.8		14.0
44-W		3.1		15.7
W.1/4		3.4		15.4
W.C		4.1		14.7
W.L		3.8		15.0
	275 N. OF SOUTHERLAND			
W.L		4.2		14.6
W.C		4.4		14.4
W 1/4		3.6		15.2
42-W		3.4		15.4
40-W		4.9		13.9
36-W		3.4		15.4
E 1/4		2.7		16.1

	18.79 − 84 = 17.95			
19-W		3.3		15.5
E.C		4.0		14.8
11-W		1.8		17.0
E.L		2.4		16.4
	300 N. − SOUTHERLAND = S.L. NOELL			
E.L		3.0		15.8
10-W		2.0		16.2
E.C		4.1		14.7
26-W		2.8		16.0
33-W		3.5		15.3
1/2		5.0		13.8
42-W		3.9		14.9
W. 1/4		4.1		14.7
W.C		4.5		14.3
W.L		5.0		13.8
B.M.	SPIKE IN TEL. POLE S.E. COR. & NOELL KURTZ	0.84	17.95	

BENCH MARKS

31.78 {CALIFORNIA & VINE SPIKE IN TEL. POLE 50'-W. OF N.E. COR.

53.41 {INDIA & WINDER - R.R. SP. IN PHONE POLE MARKED "C" S.EAST COR.

42.92 {WINDER & HANCOCK - N.E. COR. - SPIKE IN PHONE POLE

32.62 {HANASTY & HANCOCK - 50' W. OF N.W. COR. R.R. SPIKE IN 6"X6" POST IN NORTH WING OF SMALL CHURCH

25.62 {SOUTHERLAND & HANCOCK - N.W. COR. - SPIKE IN FENCE POST

26.43 {NOELL & HANCOCK - S.W. COR. - SPIKE IN FENCE POST

28.56 {ESTUDILLO & HANCOCK - N.E. COR - SPIKE IN PHONE POLE.

27.49 {WRIGHT & HANCOCK - N.E. COR - R.R. SPIKE IN PHONE POLE

17.38 {BANDINI & HANCOCK - N.E. COR - R.R. SPIKE IN PHONE POLE.

12.11 {WITHERBY & HANCOCK - S.E. COR - SPIKE IN PHONE POLE

15.84 {SPIKE IN TEL. POLE 50' S. OF S.E. COR CLAYTON & KURTZ

15.27 {SPIKE IN TEL. POLE AT S.E. COR. SUTHERLAND & KURTZ

{SPIKE IN TEL. POLE AT S.E. COR NOELL & KURTZ.

9 8 7 6 5 4 3 2 1 0 9

78 77 76 75 74 73 72 71 70 69

68 67 66 65 64 63 62 61 60 59

58 57 56 55 54 53 52 51 50 49

48 47 46 45

Degrees.

...ls,

210

Return to City Engineers Office
City Hall, San Diego, Cal.

TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100.00	0.44	100.00	0.87	99.99	1.31	89
1	99.98	1.75	99.98	2.18	99.97	2.62	99.95	3.05	88
2	99.94	3.49	99.92	3.93	99.91	4.36	99.88	4.80	87
3	99.86	5.23	99.84	5.67	99.81	6.10	99.79	6.54	86
4	99.76	6.98	99.73	7.41	99.69	7.85	99.66	8.28	85
5	99.62	8.72	99.58	9.15	99.54	9.58	99.50	10.02	84
6	99.45	10.45	99.41	10.89	99.36	11.32	99.31	11.75	83
7	99.25	12.19	99.20	12.62	99.14	13.05	99.09	13.49	82
8	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	15.64	98.70	16.07	98.63	16.50	98.56	16.93	80
10	98.48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98.16	19.08	98.08	19.51	97.99	19.94	97.90	20.36	78
12	97.81	20.79	97.72	21.22	97.63	21.64	97.53	22.07	77
13	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	24.19	96.92	24 62	96.81	25.04	96.70	25.46	75
15	96.59	25.88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	27.56	96.00	27.98	95.88	28 40	95.76	28.82	73
17	95.63	29.24	95.50	29.65	95.37	30.07	95.24	30.49	72
18	95.11	30.90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35.43	69
21	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38 67	67
23	92.05	39.07	91.88	39 47	91.71	39.87	91.53	40.27	66
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	43.84	89 69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	46.95	88.09	47.33	87.88	47.72	87.67	48.10	61
29	87.46	48.48	87.25	48.86	87.04	49.24	86.82	49.62	60
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	52 99	84.57	53.36	84.34	53.73	84.10	54.10	57
33	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	60.18	79.60	60 53	79.34	60.88	79.07	61.22	52
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	45
45	70.71	70.71							
Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees.
	DEGREES.		¾ DEGREE.		½ DEGREE.		¼ DEGREE.		

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