Waterline on Exchange
from Res. to Cave St.

X Section Prospect
Olive to Ravina

232

398

TRANCHES

F.B. 232

Table showing the difference of latitude and departure in running 80 chains at any course from 1 to 60 minutes.

Minutes	Lks.	Minutes	Lks.	Minutes	Lks.
1	2 1/3	21	49	41	95 2/3
2	4 2/3	22	51 1/3	42	98
3	7	23	53 2/3	43	100 1/3
4	9 1/3	24	56	44	102 2/3
5	11 2/3	25	58 1/3	45	105
6	14	26	60 2/3	46	107 1/3
7	16 1/3	27	63	47	109 2/3
8	18 2/3	28	65 1/3	48	112
9	21	29	67 2/3	49	114 1/3
10	23 1/3	30	70	50	116 2/3
11	25 2/3	31	72 1/3	51	119
12	28	32	74 2/3	52	121 1/3
13	30 1/3	33	77	53	123 2/3
14	32 2/3	34	79 1/3	54	126
15	35	35	81 2/3	55	128 1/3
16	37 1/3	36	84	56	130 1/3
17	39 2/3	37	86 1/3	57	133
18	42	38	88 2/3	58	135 1/3
19	44 1/3	39	91	59	137 2/3
20	46 2/3	40	93 1/3	60	140

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TABLE FOR RUNNING ON SLOPES.

In the following table the first column shows the angle, the second the number of links to be added to a chain on the slopes, to make one chain, horizontal measurement.

Angle	Cor. in Links	Angle	Cor. in Links	Angle	Cor. in Links	Angle	Cor. in Links
o		o		o		o	
4	0.24	11	[illegible]	18	5.14	25	10.54
5	0.38	12	2.[illegible]	19	5.76	26	11.26
6	0.55	13	2.63	20	6.42	27	12.24
7	0.76	14	3.06	21	7.11	28	13.37
8	0.98	15	3.53	22	7.85	29	14.34
9	1.24	16	4.02	23	8.64	30	15.47
10	1.55	17	4.56	24	9.47	35	22.07

MICROFILMED
DEC 8 1954

S. Cor. Cave & Exchange Hd. spk.
N.S round trac[illegible] 116.10

8 X 17.5 = 16.75

19.33 1/4 x 20'

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Water line from Exchange ^ Reservoir to Cave St. 2

April 11. 1906 Chiles Haslam Hawkins

Sta.		Grade	H.I.	Rod	Elev. cut.	
0,00	Valve at reservoir					
+50						
1 +00						
+50						
2 +00						
+28	So. line alley					
50' N						
100' N.						
150' N						
170' N	So. line College..	187.4	191.47	2.0	189.5	4.1
30' N		186.8		3.8	187.7	2.9
80' N	N. line College	184.4		8.9	182.6	0.2
50' N		181.4		12.52	178.95	0.0
100' N		178.3	180.16	3.8	176.4	0.1
150' N		175.2		6.0	174.2	1.0
200' N		172.2		7.8	172.4	2.2
250' N		169.3		9.6	170.6	3.3
300' N.	So. line State	166.4		12.82	167.34	2.9
30' N		165.3	168.80	2.6	166.2	2.9
80' N	N. line State	163.4		4.4	164.4	3.0

Sta.		Grade	H.I.	Rod	Elev.	cut
50' N	State	160.4	168.80	7.5	161.3	2.9
100' N		157.5		11.7	157.1	1.6
150' N		154.6	156.80	1.1	155.2	2.6
200' N		151.7		2.6	153.7	4.0
250' N		148.8		6.1	150.2	3.4
272.5' N	So. line Beach Road	147.5		8.2	148.1	2.6
	North line " "	144.5	144.64	2.6	141.9	0.0
50' N		140.6		5.4	139.1	0.5
100' "		136.6		8.6	135.9	1.3
150' "		132.7		11.74	132.80	2.1
200' "		129.1	133.31	3.6	129.7	2.6
250' "		127.0		6.3	127.0	2.0
300' "		125.0		8.4	124.9	1.9
350' "		123.0		10.2	123.1	2.2
400' "		121.0		12.0	121.3	2.4
450' "		119.0	124.36	4.6	119.8	2.8
500' "		117.0		5.7	118.7	3.7
550' "		115.0		7.3	117.1	4.1
615' "	Cross of Project					

Water line on College from Exchange to Magnolia ave.

April 11. 1906 { Childs Haslam Hawkins

Sta.		Grade	H.I.	Rod	Elev. cut	
0+00	= 10' East cen. Exchange	186.8	191.47	3.8	187.7	2.9
+50	West line Exchange	186.2		6.6	184.9	0.7
1+00		184.9		4.8	186.7	3.8
+50		183.5		6.1	185.4	3.9
2+00		182.2		6.8	184.7	4.5
+50		180.9		9.1	182.4	3.5
3+00		179.6		12.28	179.19	1.6
+50		177.0	179.45	3.0	176.4	1.4
4+00		174.0		7.3	172.1	0.1
+50		171.1		9.9	169.5	0.4
5+00		168.1		11.72	167.73	1.6
+50	East line Magnolia	165.2	168.95	4.0	164.9	1.7
+80	10' East of center "	163.7		5.3	163.6	1.9

X Sect. Prospect from Olive to Ravina (Child Haslam Hanley)

N. line Olive

April 13 1906

E. line	17+	73.20	3.4	69.8
			3.2	70.0
			3.6	69.6
C			3.7	69.5
			4.0	69.2
			4.0	69.2
W. line			4.5	68.6
	N. Cb			
W. line			4.5	68.7
W.			4.4	68.8
			4.0	68.2
C			3.9	69.3
			3.6	69.6
			3.4	69.8
E. line			3.3	69.9

X

N. 1/4

E. line		3.4	69.8
		3.5	69.7
		3.7	69.5
C		3.9	69.4
		3.9	69.3
		4.3	68.9
W. line		4.5	68.7
	Center		
W. line		4.3	68.9
		4.1	69.1
		3.9	69.3
C		3.8	69.4
		3.7	69.5
		3.7	69.5
E. line		3.6	69.6

X

So. 1/4

E. line	3.8	69.4	
	3.7	69.5	
	3.7	69.5	
C	3.8	69.4	
	4.0	69.2	
	4.1	69.1	
W. line	4.3	68.9	

So. C6

W. line	4.3	68.9	
	4.0	69.2	
	4.3	68.9	
C	3.9	69.3	
	3.8	69.4	
	3.8	69.4	
E. line	3.9	69.3	

So. line above

E. line	4.0	69.2
	4.0	69.2
	3.9	69.3
C	4.0	69.2
	4.3	68.9
	4.3	68.9
W. line	4.6	68.6

Sect. on AB Fig. 1.

W. line	4.6	68.6
	4.4	68.8
	4.3	68.9
C	4.1	68.1
	4.0	69.2
	4.0	69.2
E. line	4.0	69.2

		24' So. point B		
E. line			4.1	69.1
			4.2	69.0
			4.2	69.0
C			4.4	68.8
			4.4	68.8
			4.8	68.4
W. line			5.1	68.1
		50' So. point B		
W. line			5.7	67.5
			5.2	68.0
			4.3	68.9
C			4.1	69.1
			3.9	69.3
			4.5	68.7
E. line			4.5	68.7

Fig 1.

	75' So.		
E. line	4.6	68.6	
	4.8	68.4	
	4.8	68.4	
C	5.2	68.0	
	5.5	67.7	
	6.1	67.1	
W. line	6.6	66.6	
	100' So.		
W. line	7.4	65.8	
	7.0	66.2	
	6.4	66.8	
C	6.0	67.2	
	5.7	67.5	
	5.2	68.0	
E. line	5.0	68.2	

	120' So.		
E. line	5.6	67.6	
	5.9	67.3	
	6.3	66.9	
C	6.6	66.6	
	7.3	65.9	
	7.6	65.6	
W. line	8.2	65.0	
	140' So.		
W. line	9.0	64.2	
	8.1	65.1	
	8.0	65.2	
C	7.3	65.9	
	6.8	66.4	
	6.7	66.5	
E. line	6.3	66.9	

	160' So.		
E. line	6.5	66.7	
	7.5	65.7	
	7.8	65.2	
C	8.2	65.0	
	8.3	64.9	
	9.0	64.2	
W. line	10.3	62.9	
	180' So.		
W. line	11.6	61.6	
	9.8	63.4	
	9.3	63.9	
C	8.9	64.3	
	8.4	64.8	
	8.2	65.0	
E. line	7.9	65.3	

	205' So.		
E. line	8.6	64.6	
	9.0	64.2	
	9.7	63.5	
C	9.9	63.3	
	10.4	62.8	
	11.6	61.6	
W. line	14.1	59.1	
	230' So.		
W. line	17.7	55.5	
	14.4	58.8	
	12.5	60.7	
C	11.4	61.8	
	10.8	62.4	
	10.3	62.9	
E. line	9.3	63.9	

		H.I.			
		255' So.			
E. line		73.20	10.6	62.6	
			11.7	61.5	
			12.1	61.1	
C			13.2	60.0	
	H.I.	61.97	4.0	56.0	
			6.7	55.3	
W. line			10.1	51.9	
		280' So.			
W. line			13.4	48.6	
			10.5	51.5	
			7.7	54.3	
C			5.0	57.0	
			2.9	59.1	
	H.I.	73.20	13.0	60.20	
E. line			12.0	61.2	
	1.42	61.97	12.65	60.35	

	H.I. 61.97			
	305' So.			
E. line		2.7	59.3	
		3.8	58.2	
		5.1	56.9	
C		7.6	54.4	
		10.2	51.8	
		13.2	48.8	
W. line		16.7	45.3	
	330' So.			
W. line	H.I. 51.11	8.3	42.8	
		6.9	44.2	
	H.I. 61.97	14.1	47.9	
C		11.5	50.5	
		9.3	52.7	
		7.0	55.0	
E. line		4.7	57.3	

		355' So.		
E. line			6.8	55°.2
			10.4	51.6
			12.7	49.3
C	H.I	51,11	5.5	45°.6
			7.0	44,1
			8.0	43.1
W. line			9.2	41.9
		380' So.		
W. line			10.5	40.6
			9,2	41.9
			7,6	43.5°
C			6.9	44,2
			5.9	45.2
	H.I.	61,97	13.8	48.2
E. line			11.7	50.3

Fig. 2.

	405' So.			
E. line	H.E.	51.11	4.0	47.1
			5.7	45.4
			7.4	43.7
C			8.1	43.0
			9.2	41.9
			9.7	41.4
W. line			10.6	40.5
	430' So.			
W. line			10.2	40.9
			9.6	41.5
			9.1	42.0
C			8.3	42.8
			7.1	44.0
			7.0	44.1
E. line			6.1	45.0

	435' So		
E. line		9.7	41.4
		9.7	41.4
		7.4	43.7
C		8.1	43.0
		8.8	42.3
		9.2	41.9
W. line		9.9	41.2
	480' So.		
W. line		13.3	37.8
		12.6	38.5
		12.4	38.7
C		11.4	39.7
		11.5	39.6
		10.8	40.3
		[illegible]	
E. line		10.5	40.6

	497' So.		
E. line		11.2	39.9
		11.9	39.2
		13.3	37.8
C		13.5⁻	37.6
		13.5⁻	37.6
		14.1	37.0
W. line		16.5⁻	34.6
	20' So. E of Fig. 1		
W. line		16.6	34.5
		12.5⁻	38.6
		12.9	38.2
C		12.5⁻	38.6
		11.9	39.2
		12.1	39.0
E. line		11.9	39.2

	40' So. E. F.		
E. line		13.7	37.4
		13.8	37.3
		13.4	37.7
C		13.4	37.7
		13.4	37.7
		13.3	37.8
W. line		13.2	37.9
	60' So.		
W. line	A.I. 4117	2.8	38.4
		3.7	37.5⁻
		4.1	37.1
C		4.0	37.2
		4.3	36.9
		5.1	36.1
E. line		5.2	36.0

	80' So		
E line		7,7	33.5
		7,3	33.9
		5,3	35.9
C		2,6	38.6
		2,1	39.1
		3,2	38.0
W line		4.1	37.1
	15' So. joint		20 Fig 1
W. line		5,0	36.2
		5.7	35.5
		5.6	35.6
C		5,3	35.9
		6.4	34,8
		8.1	33.1
E line		9,6	31.6

	40' So.		
E line		10.8	30.4
		12,2	29.0
		13,3	27.9
C		13,3	27.9
		11.7	29.5
		11.0	30.2
W line		9.9	31.3
	65' So.		
W. line	N.I.31,82	5,3	26.5
		6,0	25.8
		6,5	25.3
C		6.3	25.5
		6,0	25.8
		4,7	27.1
E line		5,1	26.7

90' So.

E. line		9.6	22.2
		6.0	25.8
		7.0	24.8
C		9.0	22.8
		10.0	21.8
		9.5	22.3
W. line		8.0	23.8
	115' So.		
W. line		13.2	18.6
		13.2	18.6
		11.9	19.9
C		10.8	21.0
		9.5	22.3
		8.1	23.7
E. line		10.9	20.9

120' So.

E. line	11.7	20.1
	8.9	22.9
	10.1	21.7
C	11.3	20.5
	12.2	19.6
	13.4	18.4
W. line	19.8	12.0
	140' So.	
W. line	13.0	18.8
W.C +11	13.9	17.9
OB	18.5	13.3
OB+7'	16.5	15.3
1/4	12.3	19.5
C	12.0	19.8
	11.3	20.5
	11.0	20.8
E. line	14.9	16.9

North line Ravina

E. line		H.I.	14.9	16.9	
			17.4	14.4	
			16.2	15.6	
C			16.9	14.9	
			18.8	13.0	
			14.3	17.5	
W. line			13.0	18.8	
B.M.	11.49	30.29			18.80
	6' So. North line				
W. line			11.4	18.9	
			10.9	19.4	
			16.6	13.7	
C			15.8	14.5	
			15.9	14.4	
			14.7	15.6	
E. line			10.2	20.1	

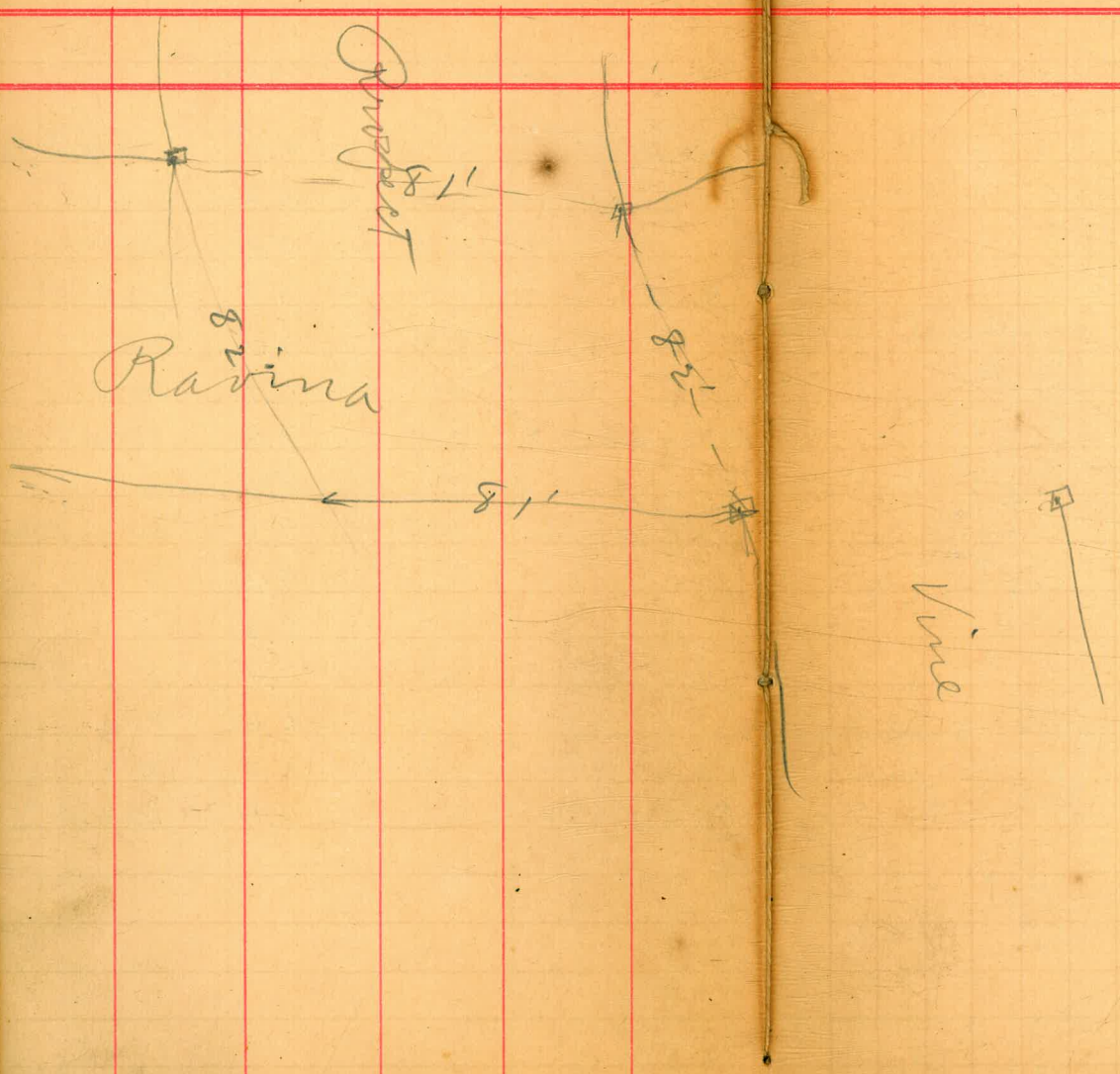
North Ch.

E. line	H.I.	5.3	25.0	
		6.9	23.4	
		6.8	23.5	
C		7.5	22.8	
		6.9	23.4	
		8.0	22.3	
W. line		10.0	20.3	
JP.	13.06	4323	0.12	30.17
	North 1/4			
W. line		14.1	29.1	
		11.5	31.7	
		9.4	33.8	
C		7.5	35.7	
		5.3	37.9	
		7.2	36.0	
E line		7.4	35.8	

43.23

	Center			
E line		3.9	39.3	
		4.0	39.2	
		4.1	39.1	
C		4.1	39.1	
		4.7	38.5	
		5.4	37.8	
W. line		7.7	35.5	
	So. ¼			
W. line		5.5	37.7	
		5.6	37.6	
		5.1	37.1	
C		4.7	38.5	
		4.3	38.9	
		3.4	39.8	
E. line		3.4	39.8	

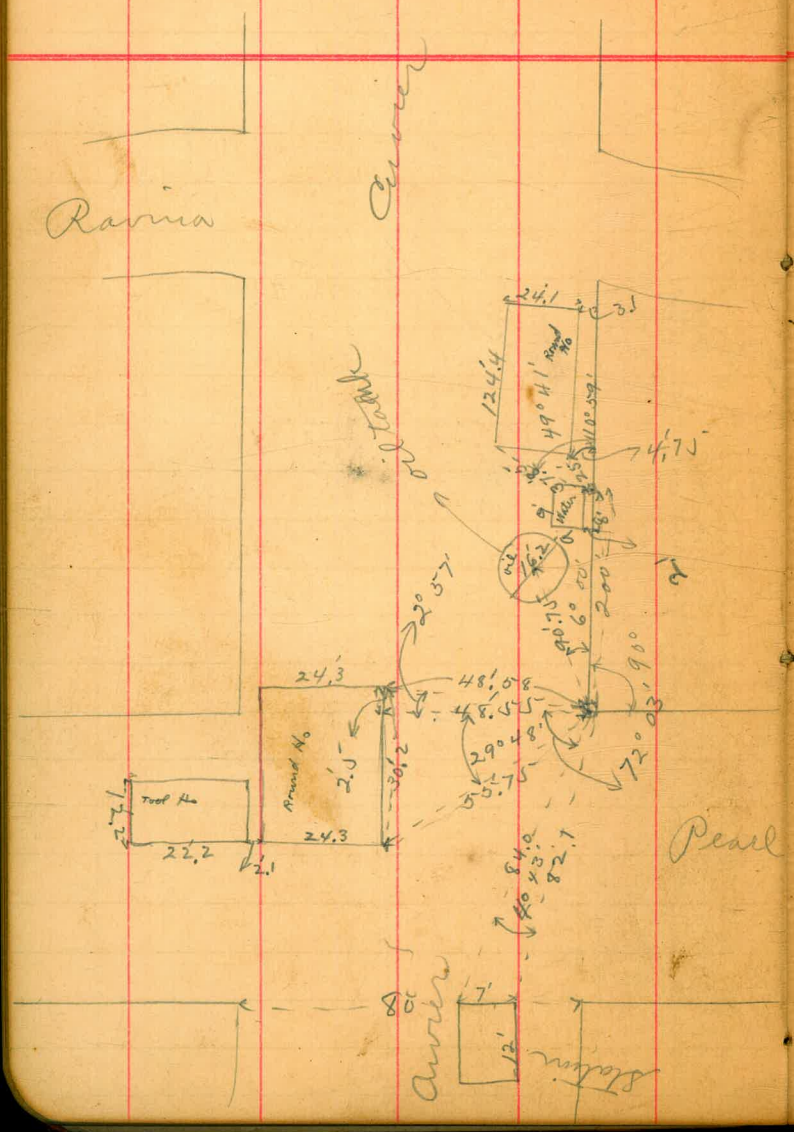
	So. Cb		
E line		4.5	38.7
		5.2	38.0
		5.5	37.7
C		5.7	37.5
		6.1	37.1
		6.9	36.3
W. line		7.6	35.6
	South line Ravina		
W. line		9.5	33.7
		9.0	34.2
		8.2	35.0
C		7.4	35.8
		6.6	36.6
		6.2	37.0
E. line		6.1	37.1


Rupert
8 1/
8 1/
Ravina
8 1/

Vine

POSTED

Location of Round House
La Jolla.



Location of Depot Lajolla.

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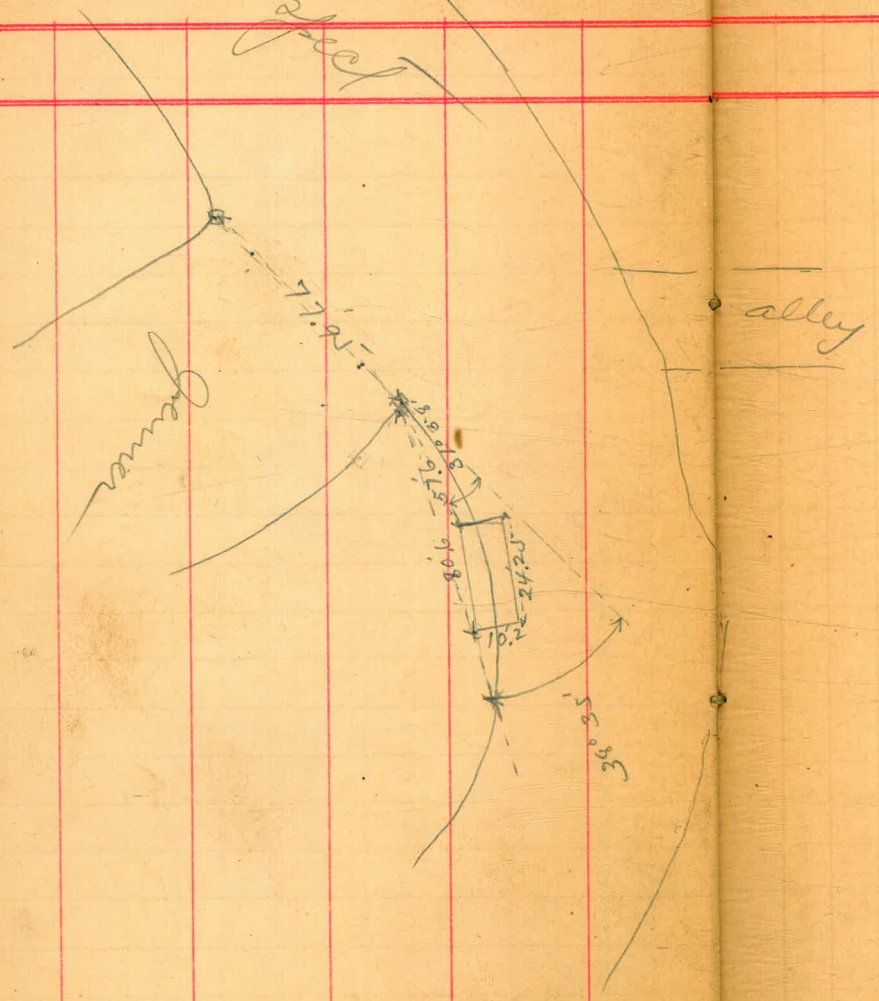

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May 27, 1907 { Childs, Evans, Barber }

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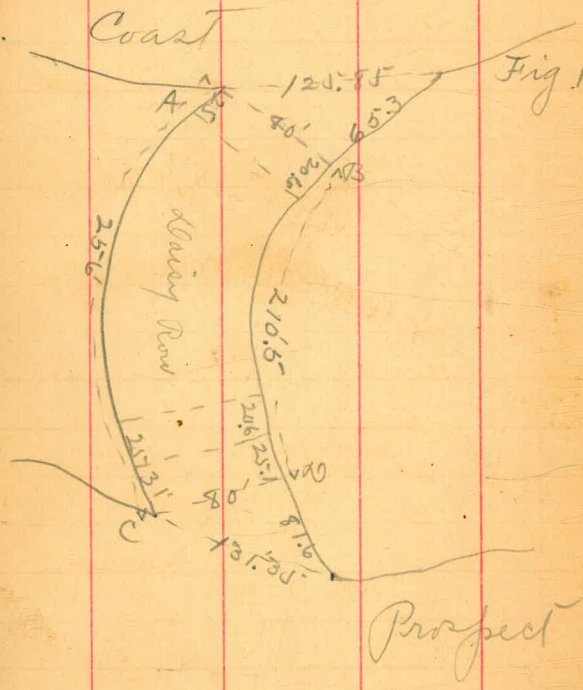
X section Dairy Row Coast to Prospect



87.82

	11.10	H.I. 87.82		76.72	
		W. line Prospect			
So line			4.9		
			5.2		
			4.8		
C			4.4		
			4.1		
			3.8		
N line			3.5		
		sect. on	C.D.	Fig. 1	
N. line			7.7		
			7.5		
			6.4		
C			5.4		
			5.2		
			5.3		
So line			4.9		

225' E. ~~Sect~~ AB Fig 1.

So line			6.2		
			7.3		
			7.5		
C			8.2		
			9.8		
			10.4		
N line			10.8		
		200' E.			
N line			13.7		
			13.3		
			12.4		
C			12.0		
			11.2		
			10.0		
So line			9.3		
		H.I.			
J.S.	0.05	75.26	12.61	75.21	

75.26

		175' E			
So line			−0.5	75.8	
			1.5		
			2.2		
C			2.9		
			3.5		
			3.8		
N line			4.5		
		150' E			
N. line			7.6		
			7.7		
			7.4		
C			7.1		
			6.3		
			4.7		
So. line			3.2		

POSTED

		125' E			
So line			6.1		
			7.6		
			10.9		
C			11.8		
			12.0		
			11.9		
N line			11.8		
		H.I.			
J.P.	2.20	65.07	12.39	62.87	
N.		100' E			
N line			5.3		
			0.6		
			5.5		
C			5.8		
			5.5		
			4.3		
So line			3.8		

6 4.07

		75° E			
So. line			9.7		
			9.7		
			10.1		
C			9.9		
			9.4		
			9.3		
N line			8.8		
		50° E			
N line			11.7		
			11.9		
			12.4		
C			12.6		
			13.1		
			13.7		
So. line			13.8		
J.P.	2.10	N.I. 54.79	12.38	52.69	

	25° E	
So. line		6.8
		6.1
		5.5
C		5.3
		4.6
		4.5
N line		4.0
	Sect. on A.B. Fig 1	
N line		5.6
		6.3
		6.7
C		7.3
		7.9
		8.3
So. line		8.8

POSTED

E. line Coast.

So. line 8.8

9.1

9.3

C 9.4

9.5

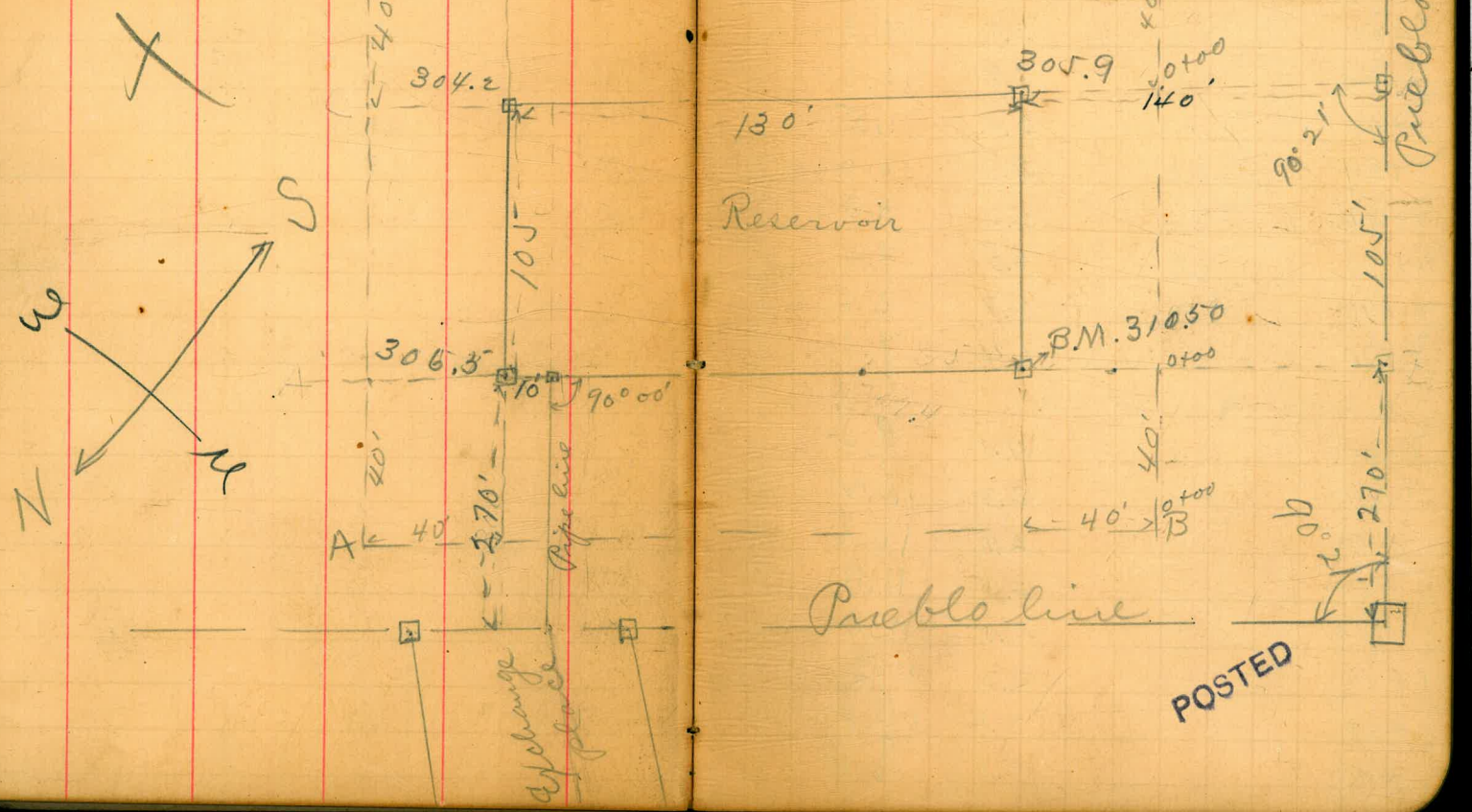
9.2

N. line 9.3

La Jolla Reservoir

location

Nov. 6, 1908 { Child
Barber
Rogers



POSTED

~~Feeds~~ X sect. Reservoir

H.I. 313.54

	N/ line A.B.	
40.+00	2.7	10.8
+20	1.6	11.9
+40	1.9	11.6
+60	2.2	11.3
+80	1.9	11.6
1+00	2.0	11.5
+20	3.5	10.0
+40	5.2	8.3
+70	6.5	7.0
+90	6.7	6.8
2+10	6.4	7.1
	20' So.	
0+00	4.1	9.4
+20	3.3	10.2
+40	2.9	10.6
+60	2.5	11.0
+80	2.5	11.0
1+00	2.2	11.3
+20	3.1	10.4
+40	5.1	8.4

Tafolla Nov. 11/08 { Childs, Barber, Rogers

note. West line is 0+00

B.M. 310.50

1+70	6.5	7.0
+90	6.2	7.3
2+00	5.9	7.6
	40' So. (No. line Reservoir)	
0+00	4.4	9.1
+20	3.2	10.3
+40	3.0	10.5
+60	3.3	10.2
+80	3.6	9.9
1+00	3.3	10.2
+20	3.9	9.6
+40	5.6	7.9
+70	7.0	306.50
+90	6.6	6.9
2+10	6.6	6.9

A.I. = 13.54

13.54

		60' Q.		
0+00			4.9	8.6
+20			3.7	9.8
+40			4.0	9.5
+60			4.0	9.5
+80			4.2	9.3
1+00			4.5	9.0
+20			5.2	8.3
+40			6.3	7.2
+70			7.6	5.9
+90			7.6	5.9
2+10			7.1	6.4
		80' Q.		
0+00			5.7	7.8
+20			5.2	8.3
+40			4.9	8.6
+60			4.5	9.0
+80			4.5	9.0
1+00			6.1	7.4
+20			6.5	7.0
+40			6.6	6.9
+70			8.0	5.5
1+90			7.9	5.6
2+10			7.4	6.1
		100' Q.		
0+00			5.0	8.5
+20			6.1	7.4
+40			5.6	7.9
+60			6.0	7.5
+80			6.0	7.5
1+00			7.0	6.5
+20			7.6	5.9
+40			8.1	5.4
+70			8.3	5.2
+90			8.2	5.3
2+10			7.7	5.8

313.54

		120' 20.			
0+00		6.0	4.5		
+20		6.7	6.8		
+40		6.3	4.2		
+60		7.1	6.4		
+80		7.1	6.4		
1+00		7.3	6.4		
+20		7.9	5.6		
+40		8.6	4.9		
+70		8.8	4.7		
+90		8.2	5.3		
2+10		7.2	6.3		
		145' 20 (Po. line Reservoir			
0+00		7.6	5.9		
+20		7.6	5.9		
+40		7.67	305.87		
+60		8.0	5.5		
+80		8.3	5.2		
1+00		8.9	4.6		
+20		9.2	4.3		
+40		9.3	4.2		

13.54

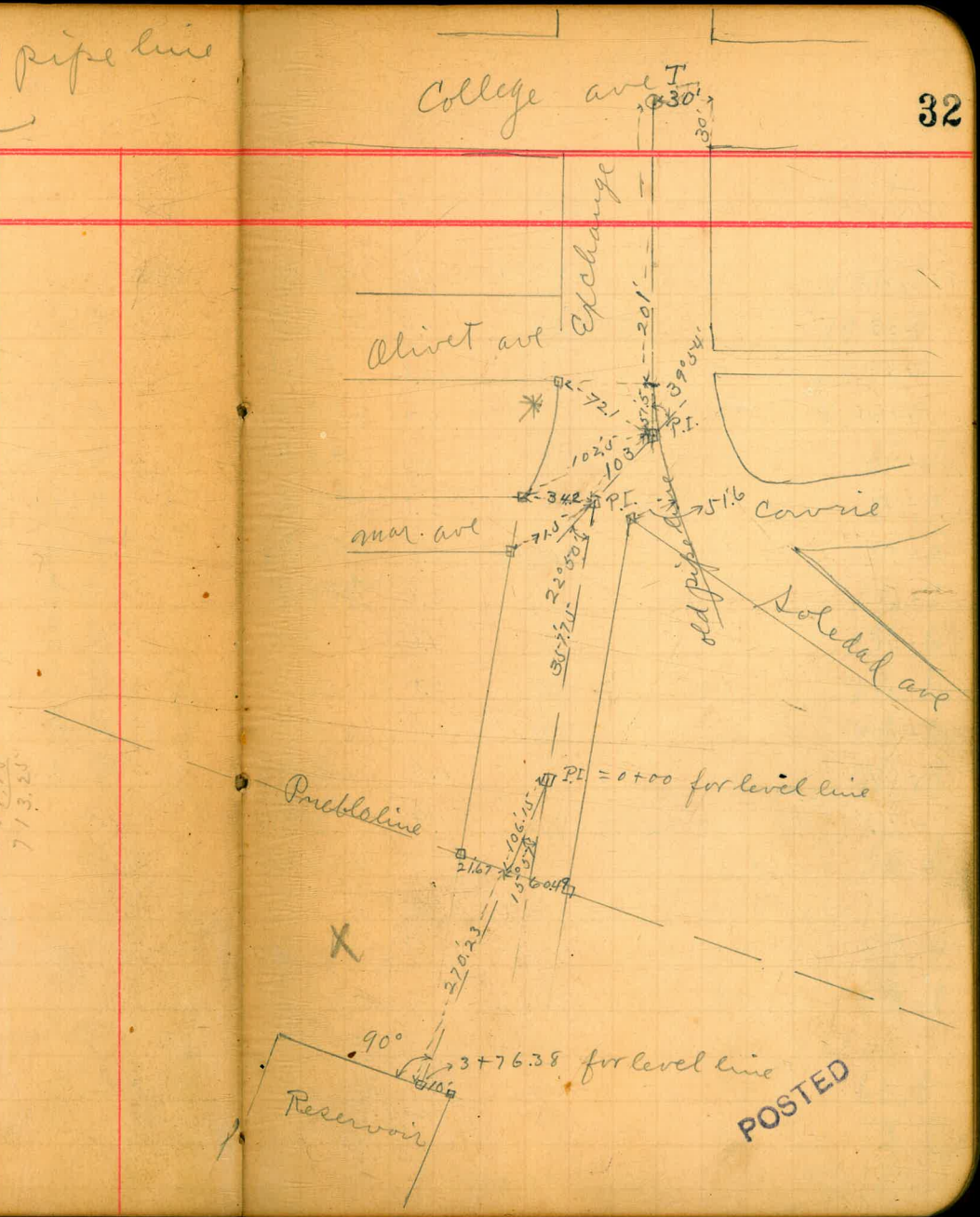
1+70	9.38	304.16	
+90	9.1	4.4	
2+10	8.6	4.9	
	165' 20		
0+00	7.7	5.8	
+20	8.1	5.4	
+40	8.1	5.4	
+60	8.5	5.0	
+80	8.8	4.7	
1+00	7.7	5.8	
+20	9.3	4.2	
+40	9.5	4.0	
+70	9.7	3.8	
+90	9.4	4.1	
2+10	8.8	4.7	

13.524

185' Rd. big C.D

0+00	8.8	4.7
+20	8.5	5.0
+40	8.2	5.3
+60	9.1	4.4
+80	9.5	4.0
1+00	9.1	4.4
+20	10.0	3.5
+40	9.9	3.6
+70	9.7	3.8
+90	9.9	3.6
2+10	8.3	5.2

Location of pipe line to Reservoir



levels on pipe line

Sta.			H.I.	Rod	Elev.
P.I. = 0+00			295.74	19.0	276.7
+22				17.4	278.3
+52				17.6	278.1
1+06.55				9.7	286.0
+21				5.4	290.3
+41				3.1	292.6
2+00			308.86	8.3	300.5
+60				3.8	305.0
+75				1.6	7.2
3+00				2.1	6.7
+40				1.1	7.7
+57				0.6	8.2
+ 76.38				1.9	6.9

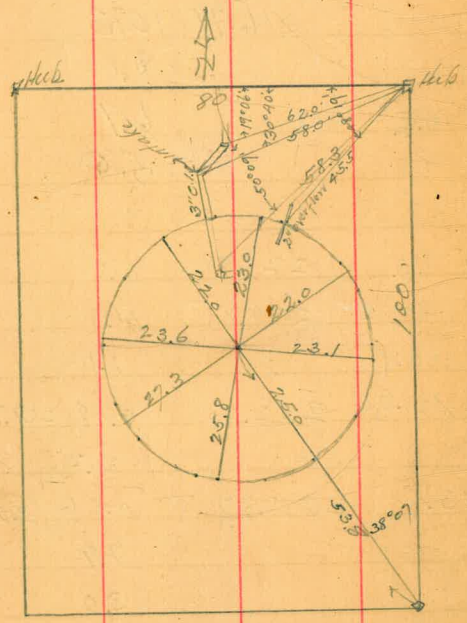
214.82
13.16 ✓
227.98
.32
227.66
12.27
239.95 ✓

Sta		H.I.	Rod	Elev.
0+00 T at College		195.35	8.5	186.8
+50		204.44	12.1	192.3
1+00			7.0	197.4
1+50			3.5	200.9
2+01		216.79	10.3	6.4
+14			8.0	8.7
2+52.5 P.I.			6.7	10.0
2+77.5			5.0	11.7
3+04			3.1	13.6
+55.5 P.I.		227.98	6.8	21.1
4+07		239.95	11.3	28.6
+50			1.1	38.8
J.P.	12.86	252.63	0.18	239.77
5+00			2.2	50.4
J.P.	13.00	265.37	0.26	252.37
5+50			7.9	57.4
6+00			3.0	62.3
J.P.	13.00	276.40	1.97	263.40
6+50			7.6	68.8
7+00			2.7	73.7
+13.25 = 0+00 opposite page				276.7

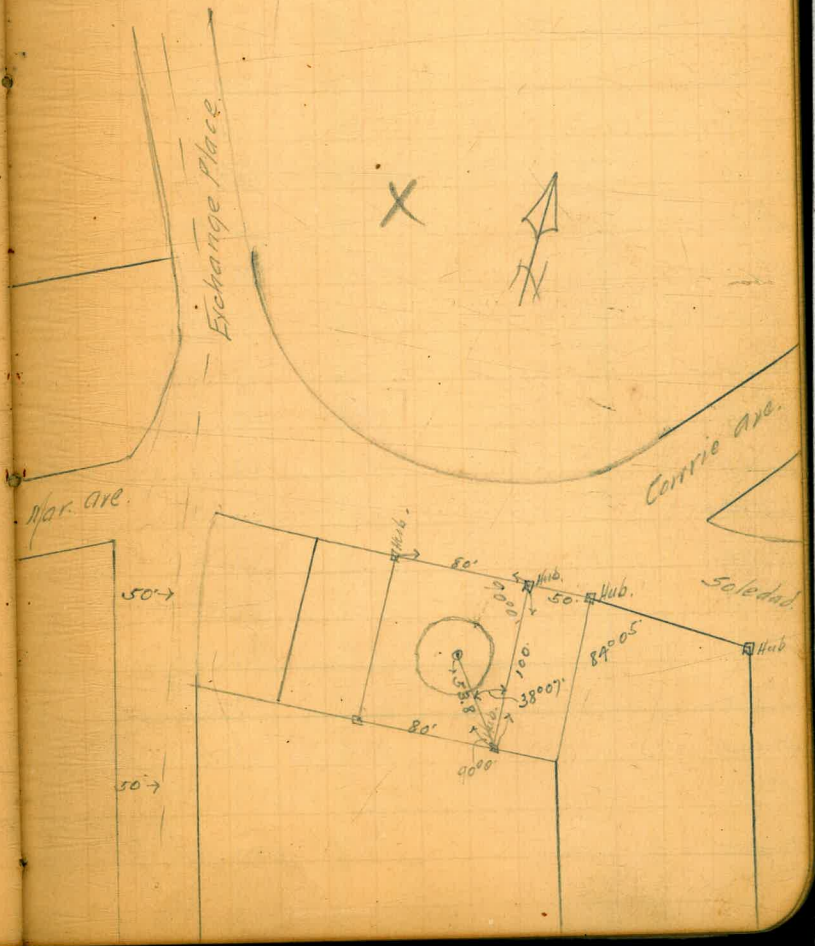
La Jolla Reservoir

12-22-08
Lockwood
Evans.
Brooks.

Distances on reservoir taken from
center in reservoir to inside edge
of concrete.



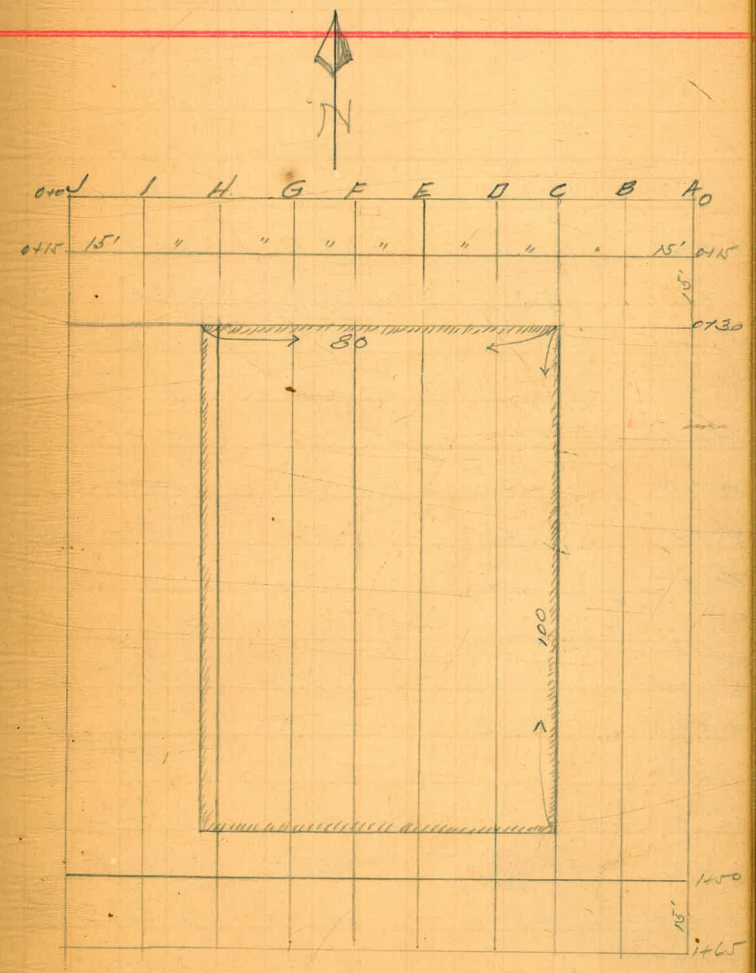
Location of reservoir
with reference to property
lines.



Exchange & Soledad Sts.

Sta.	12.83	H.I. 237.67		224.84	B.M.
	6.81	244.35	0.13	237.54	
A 0			8.1	236.2	
A 15			6.8	237.5	
A 30			6.4	237.9	
A+45			5.0	239.3	
A+60			4.7	239.6	
B 0			9.2	235.1	
B+15			7.6	236.7	
B+30			6.0	238.3	
B+45			4.4	239.9	
B+60			3.6	240.7	
C 0			9.8	234.5	
C+15			8.2	236.1	
C+30			6.0	238.3	
C+45			4.3	240.0	
D 0			11.2	233.1	
D+15			8.5	235.8	
D+30			6.4	237.9	
D+45			4.4	239.9	
E 0			12.7	231.6	
E+15			8.5	235.5	

Plan of x sections



La Jolla Rec.

		H.I.	—	
E+30		244.35	5.9	238.4
E+40			4.6	239.7
E+45			2.3	242.0
F 0			13.7	230.6
F+15			10.8	233.5
F+30			7.3	237.0
F+42			5.0	239.3
F+45			2.9	241.4
G 0			13.9	230.4
G+15			11.7	232.6
G+30			9.6	234.7
G+45			6.2	238.1
H 0			15.6	228.7
H+15			13.3	231.0
H+30			8.9	235.4
H+45			7.3	237.0
H+60			5.1	239.2
I 0			14.9	229.4
I+15			13.5	230.8
I+30			10.3	234.0
I+45			8.0	236.3
I+60			4.8	239.5
intake pipe			4.6	239.7

La Jolla Rec.

		H.I.	—	
J 0		244.35	18.0	226.3
J+15			15.5	228.8
J+30			13.7	230.6
J+45			9.2	235.1
J+60			7.3	237.0
J+75			4.0	240.3
T.P.	12.46	H.I. 254.96	1.85	242.50
A+75			14.3	240.6
A+90			12.5	242.4
A1+05		X	10.4	244.5
A1+20			8.5	246.4
A1+35			7.7	247.2
A1+50			6.0	248.9
B+75			12.7	242.2
B+90			10.2	244.7
B1+05			6.4	248.5
B1+20			5.2	249.7
B1+35			4.5	250.4
B1+50			1.6	253.3
C+55			13.6	241.3
C+60			11.6	243.3

La Jolla Res.

C+75		254.96	9.2	245.7
C+90	Bank Reservoir		6.4	248.5
C 1+05			5.6	249.3
C 1+20			3.6	251.3
C 1+35			0.9	254.0
D+60			8.4	246.5
D+75 N Edge reser.			5.8	249.1
E+60			7.3	247.6
E+64 N Edge reser.			6.2	248.7
F+60			7.5	247.4
F+66 N. Edge reser.			6.2	248.7
G+60			11.0	243.9
G+67			8.2	246.7
G+75			7.2	247.7
G+81 N edge Reser.			6.3	248.6
H+75			11.4	243.5
H+90			9.6	245.3
H 1+05			6.9	248.0
H 1+35			1.8	253.1
I+75			13.2	241.7
I+90			10.5	244.4

La Jolla Res.

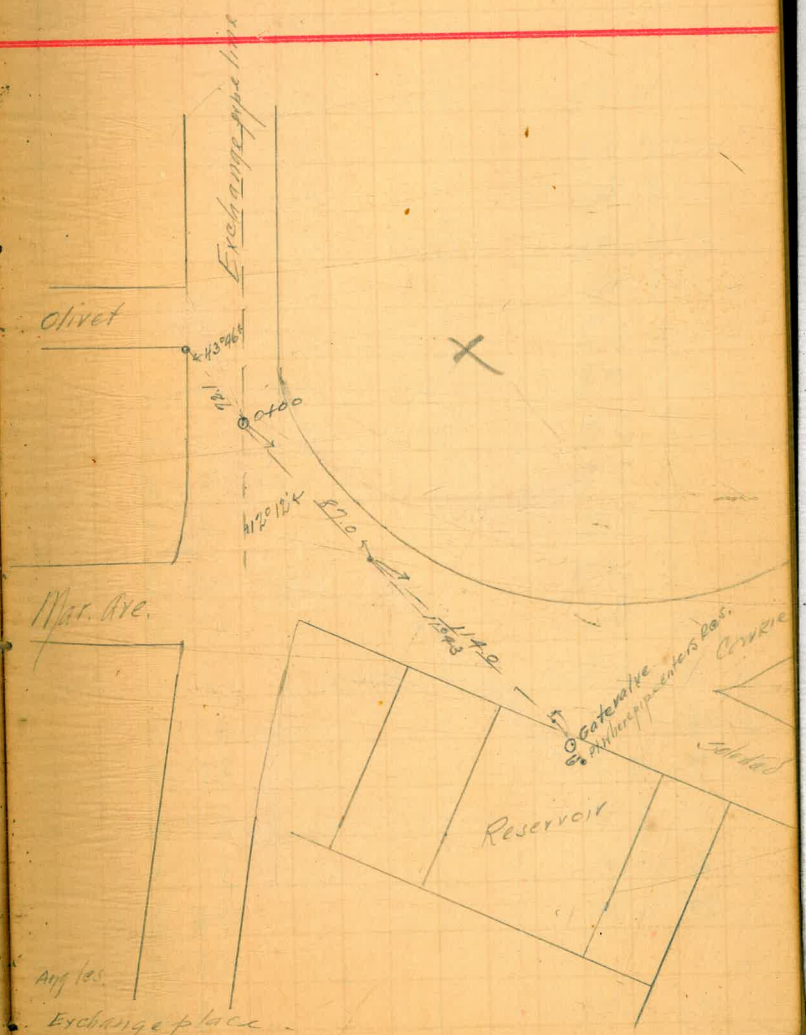
I 1+05		254.96	6.2	248.7
I 1+20			2.2	252.7
J+90			10.7	244.2
J 1+05			6.7	247.2
J 1+20			3.0	251.9
Bottom Res. near Ctr.			12.3	242.6
" " W. side			12.4±	242.5
Top of pipe at bend			3.15	251.8
D 1+11 S. side Res.			5.0	249.9
D 1+17			3.0	251.9
D 1+30			0.7	254.2
E 1+15 S side Reservoir			5.0	249.9
E 1+20			1.7	253.2
F 1+14 S side Reservoir			5.2	249.7
F 1+20			1.6	253.3
G 1+00 S side Res.			6.1	248.8
G 1+07			5.7	249.2
G 1+15			3.6	251.3
G 1+20			1.1	253.8
T.P.	12.80	266.59	11.7	253.79
C 1+50			8.5	258.1
C 1+65			6.2	260.4

La Jolla Res.

D. 1+35		Ht. 26659	10.6	256.0
D. 1+50			7.5	259.1
D 1+65			4.1	262.5
E. 1+35			9.4	257.2
E 1+50			6.6	260.0
E 1+65			2.6	264.0
F. 1+35			7.5	259.1
F. 1+50			5.1	261.5
F 1+65			2.5	264.1
G. 1+35			6.6	260.0
G. 1+50			3.9	262.7
G 1+65			1.9	264.7
H. 1+50			4.5	262.1
H 1+65			2.1	264.5
I 1+35			10.2	256.4
I 1+50			6.2	260.4
I 1+65			1.5	265.1
J 1+35			10.7	255.9
J 1+50			6.0	260.6
J 1+65			2.1	264.5
A 1+65			15.9	250.7
B 1+65			11.6	255.0

Location of Pipe Line La Jolla Res.

2+37			Pt. where pipe bends into res.
		36.0	
2+01.0			
		114.0	
0+87	11°93'L.		
		87.0	
0+00 =	12°12'L.		Pt. where line B.S. on pipe line



La Jolla Reservoir

Jan 6/09 { Childs, Barber, Rogers } 40

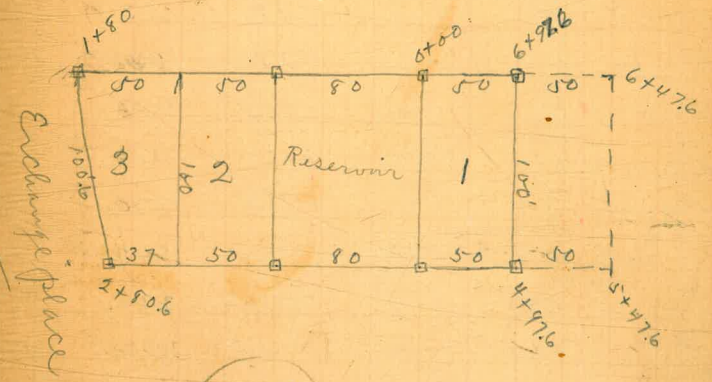
Sta		H.I.	Rod	Elev.
		250.41		
0+00	= N.E. cor. old Reservoir		12.3	238.1
+15			12.6	237.8
+30			12.1	238.3
+45		237.91	0.9	237.0
+60			3.0	234.9
+75			2.5	235.4
+90			3.9	234.0
1+05			6.9	231.0
+20			7.5	30.4
+35			7.4	30.5
+50			9.6	28.3
+65			12.0	N5.9
+80	cor. Exchange place BM		13.07	224.84 BM.
+95			10.7	27.N
2+10			6.6	31.3
+25		250.41	16.8	33.6
+40			13.3	37.1
+55			10.1	40.3
+70			5.4	45.0
+80.6	cor. Exchange		2.0	48.4
+85			0.9	49.5

Sta		H.I.	Rod	Elev.
3+00		259.04	7.8	51.N
+15			5.8	53.N
+30			4.7	54.3
+45			4.4	54.6
+60			4.2	54.8
+75			3.1	55.9
+90			1.4	57.6
4+05			2.2	56.8
+20			3.2	55.8
+35			4.9	54.1
+50			6.6	5N.3
+65			9.6	49.4
+80			13.0	46.0
+95		247.11	6.3	40.8
5+10			12.4	34.7
+24		229.10	0.6	N8.5
+25			2.6	N6.5
+84			4.4	N4.7
+40			7.3	N1.8
+47.6			7.6	N1.5

Tafolla Reservoir

Jan 6/09. { Childs. Barber Rogers

Sta		H.I.	Rod	Elev.
57+55		229.10	8.2	20.9
+70			9.4	19.7
+85			10.9	18.2
6+00			11.7	17.4
+15			12.6	16.5
+30			12.4	16.7
+45			12.8	16.3
+47.6			12.6	16.5
+60			7.4	21.7
+75		237.91	8.5	29.4
+90			3.7	34.2
7+05			1.2	36.7
+20		250.41	12.4	38.0
+35			12.1	38.3
+47.6	= 0+00 N.E. cor. of Reservoir		12.3	38.1



Bck. 79

X Recc. La Jolla Reservoir

E.

0+0 = 30' N. of ℄ St Line

Lockwood
Evans.
Brooks. } 1-12-09.

	12.95	237.79		224.84	B.M.
K. 0			12.9	224.9	
K + 15			10.4	227.4	
K + 30			7.4	230.4	
K + 45			4.8	233.0	
K + 60			1.1	236.7	
L 0			14.5	223.3	
L + 15			11.7	226.1	
L + 30			7.3	230.5	
L + 45			5.8	232.0	
L + 60			3.0	234.8	
M 0			14.9	222.9	
M. + 15			13.5	224.3	
M + 30			9.4	228.4	
M + 45			6.7	231.1	
M + 60			4.4	233.4	
N + 0			16.9	220.9	
N + 15			13.4	224.4	
N + 30			12.0	225.8	
N + 45			8.2	229.6	
N + 60			6.3	231.5	

0 0	237.29	17.5	220.3	
0 + 15		14.8	222.0	
0 + 30		12.9	224.9	
0 + 45		10.5	227.3	
0 + 60		6.7	231.1	
0 + 75		4.1	233.7	
P 0		18.0	219.8	
P + 15		15.7	222.1	
P + 30		14.1	223.7	
P + 45		11.5	226.3	
P + 60		7.5	230.3	
P + 75		4.4	233.4	
T.P.	12.73 250.26	0.26	237.53	
K + 75		10.6	239.7	
K + 90		7.3	243.0	
K 1 + 05		3.4	246.9	
L + 75		12.1	238.2	
L + 90		8.4	241.9	
L 1 + 05		5.3	245.0	
M. + 75		15.0	235.3	
M + 90		11.3	239.0	
M 1 + 05		6.3	244.0	
M 1 + 20		1.7	248.6	
N + 75		15.8	234.5	
N + 90		11.8	238.15	

Exec. Tajalla Reservoir

		250.26		
N 1+05			8.6	241.7
N 1+20			4.0	246.3
O+90			14.2	236.1
O 1+05			11.4	238.9
O 1+20			6.0	244.3
P+90			16.1	234.2
P 1+05			13.3	237.0
P 1+20			9.5	240.8
P 1+35			5.0	245.3
T.P.	12.57	262.49	0.34	249.92
K 1+05			15.2	247.3
K 1+20			11.3	251.2
K 1+35			7.2	255.3
K 1+50			3.1	259.4
L 1+20			13.0	249.5
L 1+35			8.2	254.3
L 1+50			4.1	258.4
M 1+35			9.9	252.6
M 1+50			5.8	256.7
M 1+65			1.9	260.6
M 1+35			12.0	250.5
N 1+50			7.7	254.8
N 1+65			4.2	258.3

O 1+35		262.49	14.5	248.0
O 1+50			11.2	251.3
O 1+65			8.0	254.5
O 1+80			7.0	255.5
O 1+95			7.7	254.8
P 1+50			15.3	247.2
P 1+65			14.5	248.0
P 1+80			13.6	248.9
P 1+95			12.8	249.7
P 2+10			11.9	250.6
T.P.	12.90	274.89	0.50	261.99
O 2+10			19.6	255.3
O 2+25			19.6	255.3
N 1+80			16.8	258.1
N 1+95			16.6	258.3
N 2+10			16.7	258.2
N 2+25			15.0	259.9
N 1+80			13.4	261.5
N 1+95			12.7	262.2
N 2+10			10.9	264.0
N 2+25			9.1	265.8
L 1+65			12.8	262.1
L 1+80			11.5	263.4

Exc. La Jolla Reservoir

I 1+95		274.89	9.7	265.2	G 1+80	274.89	7.9	267.0
I 2+10			7.5	267.4	G 1+95		5.4	269.5
I 2+25			6.0	268.9	G 2+10		2.5	272.4
K 1+65			11.6	263.3	G 2+25		1.5	273.4
K 1+80			7.2	265.7	F 1+80		8.3	266.6
K 1+95			7.7	267.2	F 1+95		4.9	270.0
K 2+10			5.7	269.2	F 2+10		3.0	271.9
K 2+25			5.0	269.9	F 2+25		1.5	273.4
J 1+80			8.0	266.9	E 1+80		8.8	266.1
J 1+95			5.0	269.9	E 1+95		6.2	268.7
J 2+10			4.0	270.9	E 2+10		3.1	271.2
J 2+25			3.6	271.3	E 2+25		0.8	274.1
D 1+80			7.0	267.9	D 1+80		9.8	265.1
D 1+95			4.0	270.9	D 1+95		7.1	267.8
D 2+10			2.9	272.0	D 2+10		4.7	270.2
D 2+25			2.8	272.1	D 2+25		0.8	274.1
H 1+80			7.3	267.6	C 1+80		12.7	262.2
H 1+95			4.4	269.5	C 1+95		10.3	264.6
H 2+10			3.0	271.9	C 2+10		8.0	266.9
H 2+25			2.3	272.6	C 2+25		5.6	269.3

x sec La Jolla Reservoir.

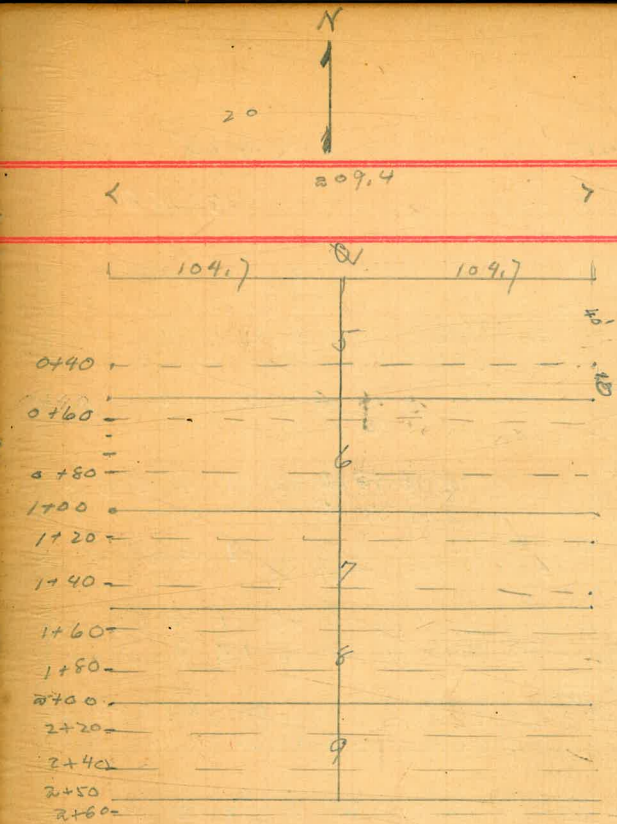
B. 1+80		274.89	17.0	259.9
B 1+95			15.3	259.6
B 2+10			12.3	262.6
B 2+25			9.6	265.3
T.P.	7.27	269.64	12.52	262.37
A 1+80			17.0	252.6
A 1+95			16.2	253.4
A 2+10			15.2	254.4
A 2+25			12.9	253.7

X

Contours La Jolla Reservoir

Lots 5, 6, 7, 8 & 9 Blk 7

			224.84	
12.63	237.47	0.61	236.86	
12.88	249.74	1.53	248.21	
13.03	261.24	0.88	260.36	
13.04	273.40	0.83	272.57	
11.07	283.88	1.01	282.87	TP
11.77	294.34			
12.22	294.79	0.19	294.60	
9.65	304.25	12.99	291.26	
0.26	291.52			
0.25	291.61	13.22	278.39	
0.47	278.86	12.89	265.97	
2.23	268.20	13.04	255.16	
3.73	258.89			



0+0 = Line dividing Lots 4 + 5

47

2+60

2+40

2+20

2+00

1+80

1+60

1+40

1+20

1+00

0+80

0+60

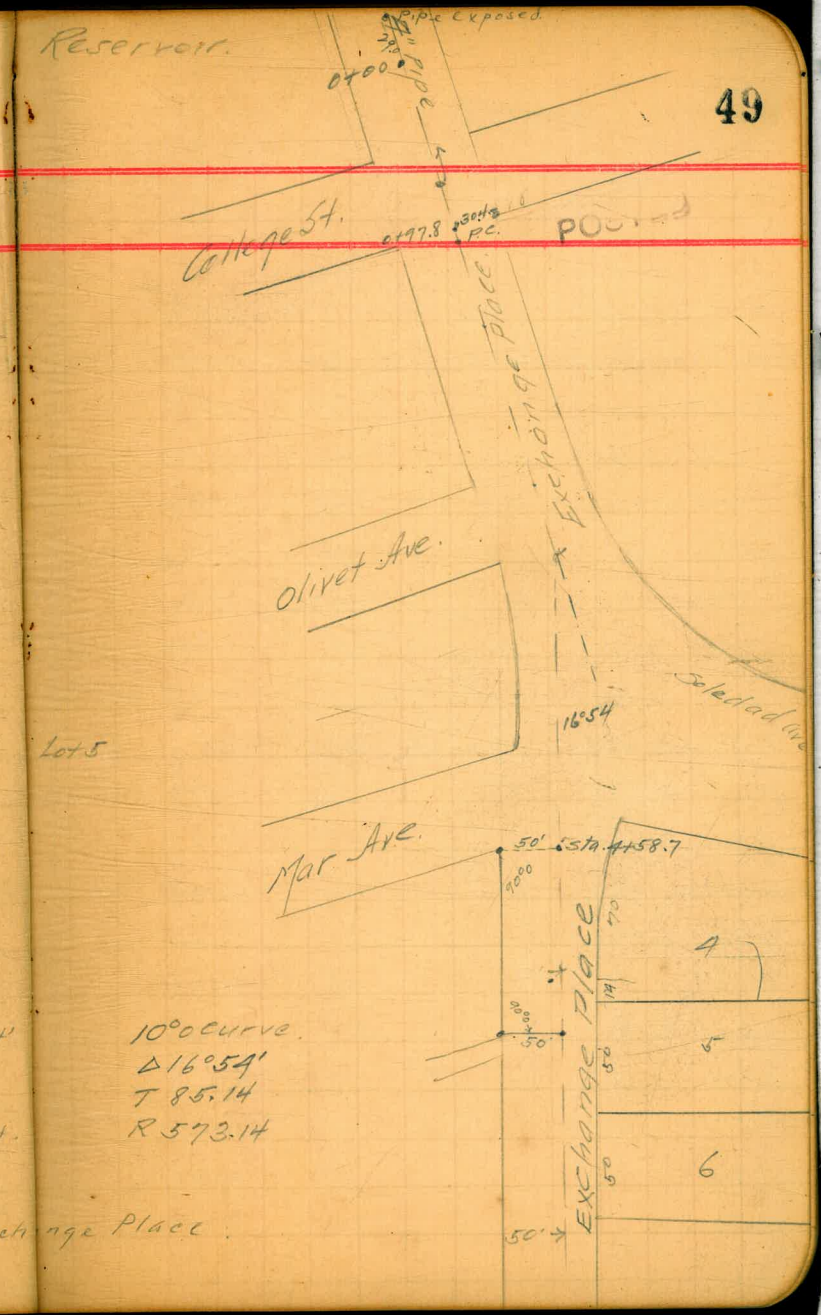
0+40

Survey of pipe Line La Jolla Reservoir.

POSTED

3-25-09
Lockwood
Evans
Taylor.

5+45	Pt. opp. apt. 14' W. of	Lot 5
4+58.7	Pt. of S side Mar Ave.	
1+69 Δ	P.T. LC. 169.0 T. 85.14 Δ 16°54' R. 573.14 P.C. 10° C to R.	10° curve. Δ 16°54' T 85.14 R 573.14
1+00 Δ	= S. Line College St.	
0+97.8	℄ pipe line	
0+00	Backsight on pipe line on Exchange Place.	



Levels on Pipe line on Exchange Place.

POSTED

Last location of Reservoir

	0.77	206.14	B.M. Ex. & Olivet	205.37
		196.0		
T.P.	1.91	195.99	12.06	194.08
Elev Pipe	29' W. of 0+00		16.4	179.6
0+00			13.8	182.2
+25			12.6	183.4
+50			8.6	187.4
+75			8.0	188.0
1+00			6.1	189.9
+25			3.0	193.0
+50			1.3	194.7
T.P.	12.64	207.75	0.88	195.11
1+75			10.3	197.4
2+00			8.5	199.2
2+25			5.9	201.8
2+50			4.0	203.7
2+69			2.6	205.1
2+75			2.2	205.5
3+00			0.9	206.8
T.P.	11.57	219.07	0.25	207.50
3+25			9.5	209.6
+50			7.0	212.1

POSTED

3+75		219.07	4.4	214.7
T.P.	12.77	231.14	0.70	218.37
4+00			11.0	220.1
+25			8.10	223.0
+50			3.7	227.4
+58.7			2.1	229.0
T.P.	12.76	243.50	0.40	230.74
4+75			10.5	233.0
5+00			4.3	239.2
T.P.	12.49	255.19	0.80	242.70
5+25			9.0	246.2
+50			4.4	250.8
T.P.	12.45	266.83	0.81	254.38
+75			12.6	254.2
Prop line inside 14' W. of Lot 5			5.7	261.1
25 W. Prop line 14' W. of Lot 5			2.5	264.3

POSTED

4-26-09

Levels NE Co. Exchange Place & Soledad

	12.90	237.74		224.84 BM
	12.28	249.87	0.15	237.59
	12.22	261.40	0.69	249.18
			0.23	261.17

B.M. = On Hub 50' S. of S.W. cor. of top of inner slope. Elev 278.82

May 27/09 { Schultz, Lawler, Taylor

278.82
0.58
279.40
265
11.95
267.45
3.80
271.25
265.0
6.25
2.05
4.2

278.82
0.97
279.79
12.54
267.25 J.P.
4.07
271.32
265.0
6.32

278.82
0.12
278.94
12.60
266.34 J.P.
396
270.30
4.75
5.55

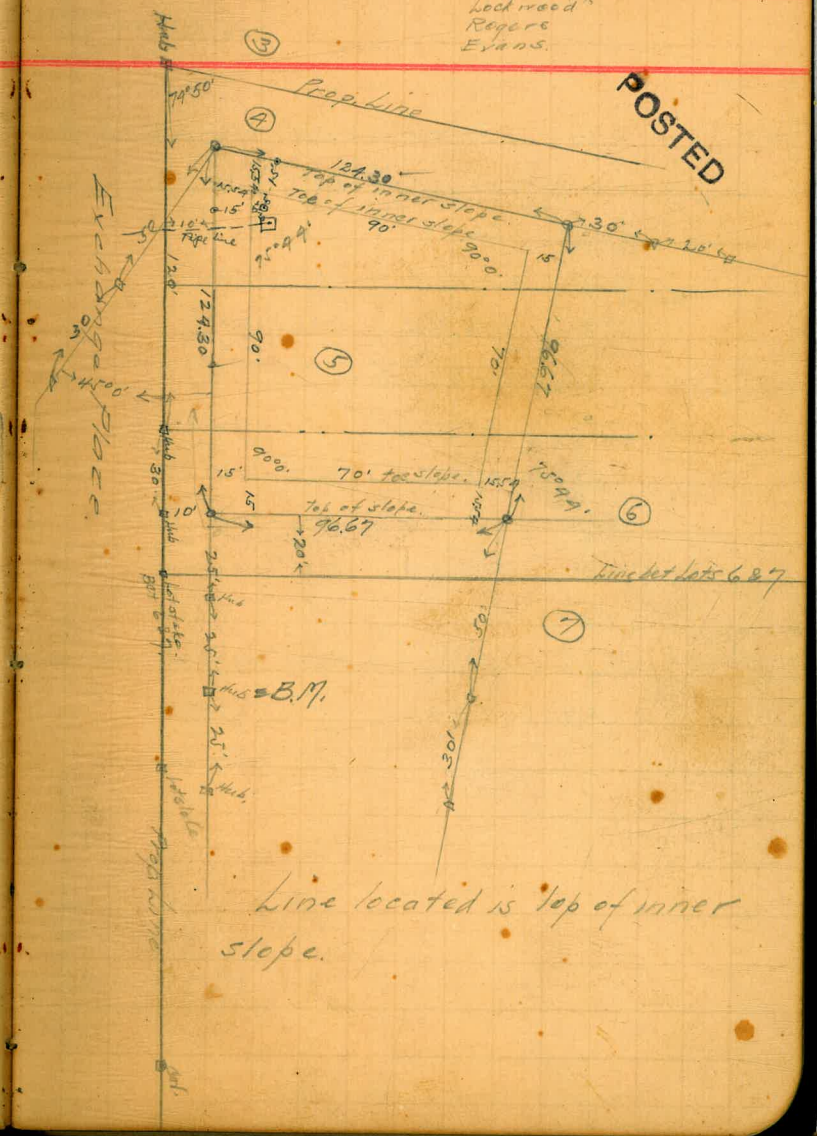
265
1.91
266.91
250
16.91
12.91
4.00

June 21/09

278.82
0.04
278.86
12.79
266.07 J.P.
0.61
266.68
13.03
253.65 J.P.
1.30
254.95
249.67
5.28

3.50
.33
249.67

Tie pts. - - - 4-26-09
La Jolla Reservoir 4-23-09
Lockwood
Rogers
Evans.



Line located is top of inner slope.

214.82
13.08
227.90
3.07
224.84

POSTED

52

	12.79	227.61		214.82 B.M.
T.P	11.97	238.99	0.39	227.22
	12.81	251.33	0.47	238.52
	12.30	263.47	0.16	251.17
	9.79	271.98	1.28	262.19
T.P.	6.78	278.46	0.30	271.68
	Check Levels			
	12.92	237.76		224.84
	11.70	249.32	0.14	237.62
	12.18	261.40	0.10	249.22
	12.27	273.44	0.23	261.17
	12.09	283.72	1.81	271.63
			4.90	278.82 = B.M.
T.P.	11.63	294.36	0.99	282.73
				292.79
			1.57	292.82

Elev Top of res. 265.00

E side
2.60 N side
256.47 0+68
F 8.53

1+20 0+50
261.27
F 3.73

1+00
9.70
266.28
F 2.72

N.W. cor.
12.20
253.78
F 5.22

E side N.E. cor.
2.60
269.38
.65
4.4

2+40
276.0
265
C. 11.0

South side
1.5
277.0
265
C 12.6

S.E. cor.
5.0
278.5
265
C 8.5

West side
0+50
9.3
269.2
65
C. 4.2

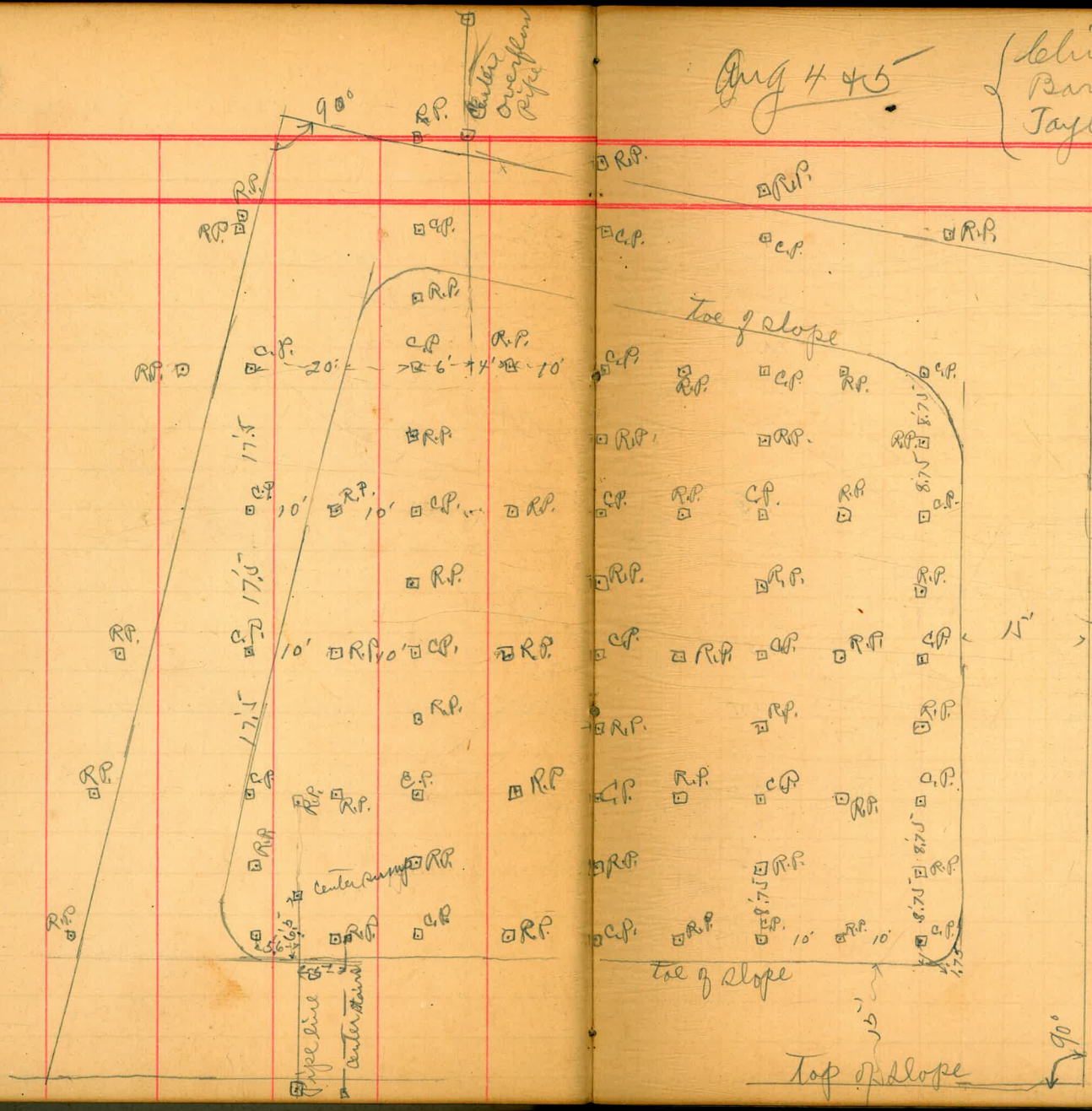
1+00
16.00
262.5
F 2.5

283.72
265
18.72
10.4
8.3

on Hub. 50' S. of S.W. cor. of inner slope

Aug 4 45

Shields
Barber
Taylor



X sect. State from West line of Exchange place.

Prospect to East line
Oct. 13/11
Childs
Taylor
Bidwell

			H.I.		
J.P.		12.85	161.57		148.72
	West line prospect.				
No. line				11.1	150.5
				11.4	
				11.1	
C				10.5	151.1
				10.3	
				9.5	
So. line				9.2	152.4
		2' west			
So. line 1' No.				5.8	155.8
				8.8	
				9.2	
				10.1	
C +11				10.0	151.6
				10.4	
				9.6	
				9.8	
No. line				9.3	152.3

	161.57		
	5' west		
No. line		9.2	152.4
+3'		8.7	
		10.1	
+2'		9.0	
		10.1	
C		9.9	151.7
		9.9	
		9.6	
+13		8.4	
So. line		4.2	157.4
	25' west		
So. line		4.0	157.6
+8'		4.0	
+10'		6.9	
C.		8.1	
		8.5	
C		8.5	153.1
+11		8.7	
		8.2	
+12'		8.9	
		8.1	
N. line		8.6	153.0

1961.57

50' west

Nolin +13	7.8	153.4	
	7.3		
	8.0		
	7.3		
C	7.1	154.5	
	7.1		
	6.5		
+4'	3.3		
So. line	2.8	158.8	

75' west.

So line +11	1.3	160.3	
	4.0		
	4.4		
	5.8		
C	6.1	155.5	
	7.0		
	7.7		
+2'	6.9		
N. line	7.8	153.8	

1961.57

100' west

Nolin	7.8	153.8	
	7.2		
	6.7		
C	5.4	156.2	
	5.2		
	4.4		
+2'	3.1		
So. line	0.9	160.7	

125' west

So. line	0.5	161.1	
	3.8		
	4.5		
C	4.7	156.9	
	5.6		
	6.5		
Nolin	7.4	154.2	

161.57

		150' west		
no. line		8.0	153.6	
		7.0		
		5.7		
c		5.0	156.6	
		4.5		
		3.3		
so. line		2.2	159.4	
		175' west		
so. line		1.8	159.8	
		3.0		
		4.0		
c		4.7	156.9	
		5.8		
		6.8		
no. line		7.5	154.1	

161.57

		200' west		
no. line		6.3	155.3	
		6.0		
		5.0		
c		4.1	157.5	
		3.4		
		2.6		
so. line		1.2	160.4	
		225' west		
so. line		0.7	160.9	
		2.2		
		2.8		
c		3.0	158.6	
		3.8		
		5.2		
no. line		5.9	155.9	

161.57

250' west

no.line			5.0	156.6
			4.3	
			3.3	158.3
c			2.5	159.1
			1.9	
so.cb.		K.I.	0.7	
J.P.	8.63	169.24	0.96	160.61
so.line			7.1	162.02

275' west

so.line			6.0	163.2
			7.5	
			8.9	
c			9.5	159.7
			10.7	
			11.4	
No.line			12.2	157.0

169.24

300' west

no.line	11.7	157.5
	10.9	
	9.8	
c	8.7	160.5
	8.0	
	6.7	
so.line	5.6	163.6

325' west

so.line	5.5	163.7
	6.7	
	7.6	
c	8.2	161.0
	9.1	
	10.2	
no.line	11.2	158.0

			350' west				400' west		
no.line				10.7	158.5	no.line		9.1	160.1
				9.8				8.1	
				8.6				7.1	
c				7.2	162.0	c		6.7	162.5
				7.1				6.6	
				6.2				5.6	
no.line				5.3	163.4	no.line		4.3	164.9
			375' west				425' west		
no.line				5.0	164.2	no.line		3.5	165.7
				5.7				4.7	
				6.4				5.8	
c				7.0	162.2	c		6.1	163.1
				8.3				6.8	
				9.2				7.2	
no.line				9.9	159.3	no.line		7.8	161.4

169.24

		450' west			
no. line			7.1	162.1	
			6.6		
			5.9		
c			5.5	163.7	
			4.8		
			3.8		
so. line			2.7	166.5	
		475' west			
so. line			1.8	167.4	
			2.4		
			2.5		
c			4.2	165.0	
			4.3		
			5.0		
no. line			5.7	163.5	

East line Exchange 481' on north
+500 on south

no. line	5.4	163.8
	4.6	
	4.0	
c	3.6	165.6
	2.6	
	2.2	
so. line	1.4	167.8

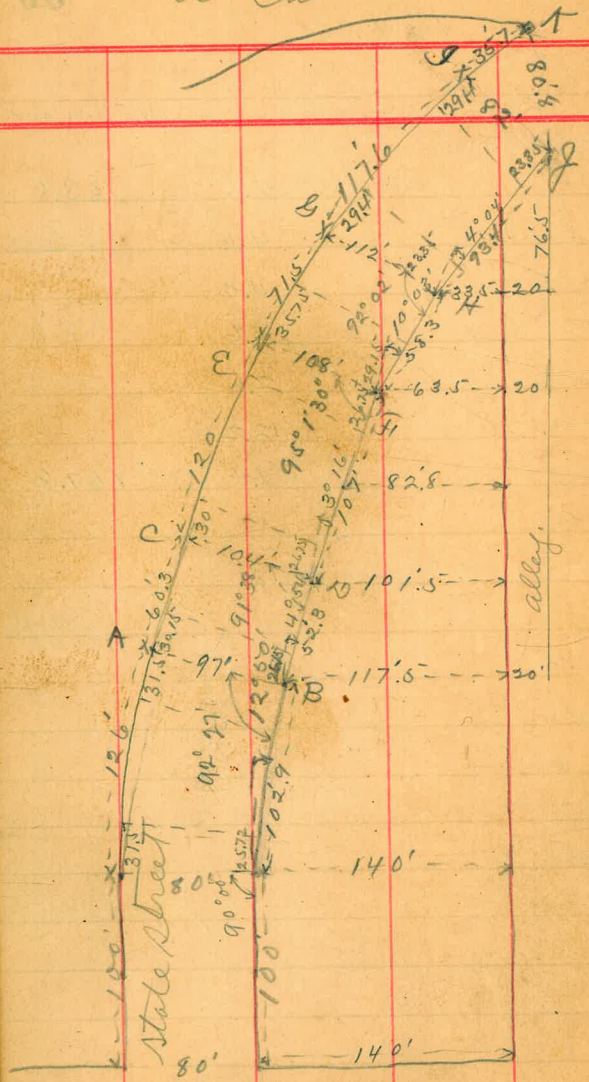
X sect. State Street from
to Cave.

Prospect

Dec. 4+5 11

Childs
Taylor
Bruker

60



15 2.11

		339	H.T. 15 2.11		148.72	B.M., State		
		East line prospect				50' east		
No. line				2.8	149 3	No. line +5'	5.1	147.0
							6.0	146.1
gutter				3.1			7.4	
				3.6				
				3.5			6.3	
C				2.8	149.3	C	5.9	146.2
gutter				2.0			5.6	
				0.7				
				0.10			5.4	
So. line				-0.2	15 2.3	So. line	3.4	148.7
		25' East.				75' east		
So. line				1.5	150.6	So. line +8'	5.6	146.5
				4.2			7.4	144.7
							7.2	
				3.9			7.1	
C				4.2	147.9	C	7.2	144.9
				4.7			7.5	
				5.9			9.0	145.6
C6+5'				3.6	148.5	+4	6.5	146.8
No. line				2.7	149.4	+12 No. line	3.3	
							0.9	146 2

15`2,11

100' East

no. line +5'			8.1 7.3	144.0 143.8
			9.1	
+4'			11.3	141.8
			10.1	
c			9.8	142.3
			9.6	
			9.7	
So. line			10.3	141.8
		125.72 east.		
So. line			12.7	139.4
			12.3	
			12.2	
c			12.4	139.7
No. 1/4			13.2	
		K.S.		
J.P.	1.78	141.80	12.09	140.02
cb			2.6	
No. line			4.8	137.0

141.80

151.44 East

no. line	13.3	128.5
	10.0	
+11	8.0	133.8
1/4	6.5	
+2	5.4	136.4
c	4.3	137.5
	4.1	
	4.3	
+12	4.6	
So. line	3.7	138.1

177.14 east

so. line	5.3	136.5
+8'	6.7	135.1
	6.3	
	6.2	
c	5.2	136.6
+6	8.2	
1/4	13.2	

141.80

202.9 east. Sect AB

C			10.8	131.0
			8.1	
/			7.9	
+10			8.2	
So. line			7.2	134.6

26.15 east AB

So line			8.7	133.1
+4'			10.1	
			9.9	
1/4			10.5	
+12			10.7	
C			14.8	129.0

Sect. C D

So. line			11.6	130.2
			11.8	
1/4			12.5	
I.P.	0.10	129.12 (H.S.)	12.78	129.02

177.14 east prospect

No. C6			4.6	
no. line			6.6	122.5

129.12

202.9 east (sect. AB)

~~No. line~~		
C6	13.2	116.9
1/4	9.4	

~~26.15 east AB~~

no. line		
C6		
1/4		

Sect. C D

1/4+14	2.3	
C	7.3	121.8

26.75 east C D

C	8.5	120.6
+8	8.4	
1/4	1.6	
	1.1	
So. line	1.2	127.9

H.I.
129.12

				10.19	118.93 T.P. on rock inroad above Burnthill
					sect. G.H.
		53.5' east C.20			
So. line			3.3	125.8	So. line 9.7 111.2
			3.1		9.7
1/4			3.5		10.1
+13			5.6		
C			9.5	119.6	C 11.5 107.4
		80.25' east C.20			H.I.
					T.P. 0.06 116.44 12.74 116.38
C			10.4	118.7	202.9 east (sect A.B.)
+4			8.1		
1/4			5.5		no. line 2.9 113.5
			4.8		26.15' East A.B.
So. line			5.0	124.1	no. line 8.6 107.8
		107' east C.20 = sect. E.F.			5.5°
So. line			6.6	122.5	1/4 2.5
			6.5		sect. C.20.
			7.2		
+15			9.0		no. line 11.8 104.6
C			12.8	116.3	CB 9.6
		29.15' east E.F.			CB+14 6.4
4' west cedar			14.5		1/4 4.7
C			11.3	117.8	
			8.6		
			8.2		
So. line			8.6	120.5	

116.44

	26.75 east C.20			
no. line			13.9	102.5
			10.1	
			6.1	
¼+10			3.7	112.7
	53.5 east C.20.			
Cb.			13.5	
¼			10.1	
	80.25 east C.20			
no. ¼			11.1	
J.P.	25.9	K.I. 106.07	12.96	103.48
	53.5 east C.20.			
no. line			5.8	100.3
	80.25 east C.20.			
no. line			5.8	100.3
Cb.			4.0	
	sect E.F.			
no. line			7.7	98.4
			5.2	
¼			2.5	

106.07

	29.15 east E.F.		
no. line		8.2	97.9
		6.5	
66+15		4.4	101.7
¼		2.5	
	sect G.K.		
no. line		6.2	99.9
		4.4	
no. ¼		−0.5	106.6
J.P.	Top stake prop. line	6.09	99.98

			H.I.		
J.R.		1.8 0	120.73		118.93
		23.35 east Sect. G.H.			
Do. line				2.3	118.4
				2.2	
				2.5	
	C			3.4	117.3
	C+6			4.6	116.1
	1/4			13.2	
				16.2	
No. line				18.6	102.1
		46.70 east G.H.			
No. line				15.3	105.4
				13.3	
	C6+14'			11.3	109.4
	1/4 C+9'			9.5	
				4.9	115.8
				4.0	
				3.4	
				3.5	
Do. line				3.7	117.0

120.73

70.05 east G.H.

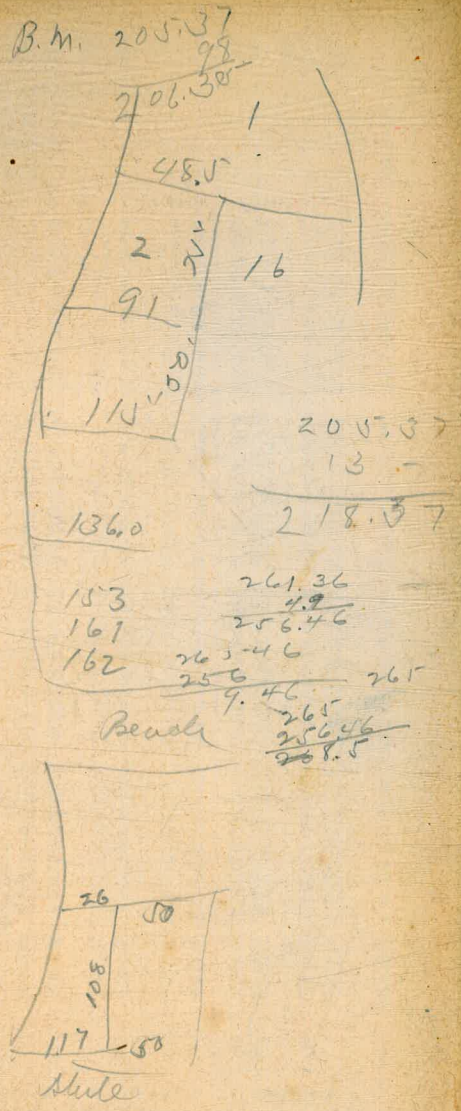
Do. line		3.7	117.0
		4.2	
		4.2	
	C	4.6	116.1
		5.8	
		9.9	
No. line		11.6	109.1
	Sect. F.J.		
No. line		6.7	114.0
		4.9	
		5.0	
	C	5.4	115.3
		5.0	
		5.2	
	C6+11	5.1	115.6
Do. line		1.1	119.6

120,73

sect. on J.K.

20. hrs		1.1	119.6
+4'		5.3	115.4
		5.5	
		5.6	
C		5.8	114.9
		6.6	
1/4 + 11		6.8	
		5.1	
10. hrs		3.48	117.2

				2FR27
0.43	283.00	11.70	27 1.30	
		8.20	274.60	
		1.00	276.00	
		5.00	278.00	
		2.50	280.50	
		1.20	281.70	



Return to City Engineers Office
City Hall, San Diego, Cal.

Return to City Engineers Office
City Hall, San Diego, Cal.

TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100.00	0.44	100.00	0.87	99.99	1.31	89
1	99.98	1.75	99.98	2.18	99.97	2.62	99.95	3.05	88
2	99.94	3.49	99.92	3.93	99.91	4.36	99.88	4.80	87
3	99.86	5.23	99.84	5.67	99.81	6.10	99.79	6.54	86
4	99.76	6.98	99.73	7.41	99.69	7.85	99.66	8.28	85
5	99.62	8.72	99.58	9.15	99.54	9.58	99.50	10.02	84
6	99.45	10.45	99.41	10.89	99.36	11.32	99.31	11.75	83
7	99.25	12.19	99.20	12.62	99.14	13.05	99.09	13.49	82
8	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	15.64	98.70	16.07	98.63	16.50	98.56	16.93	80
10	98.48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98.16	19.08	98.08	19.51	97.99	19.94	97.90	20.36	78
12	97.81	20.79	97.72	21.22	97.63	21.64	97.53	22.07	77
13	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	24.19	96.92	24 62	96.81	25.04	96.70	25.46	75
15	96.59	25.88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	27.56	96.00	27.98	95.88	28 40	95.76	28.82	73
17	95.63	29.24	95.50	29.65	95.37	30.07	95.24	30.49	72
18	95.11	30.90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35.43	69
21	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38 67	67
23	92.05	39.07	91.88	39 47	91.71	39.87	91.53	40.27	66
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	43.84	89 69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	46.95	88.09	47.33	87.88	47.72	87.67	48.10	61
29	87.46	48.48	87.25	48.86	87.04	49.24	86.82	49.62	60
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	52.99	84.57	53.36	84.34	53.73	84.10	54.10	57
33	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	60.18	79.60	60 53	79.34	60.88	79.07	61.22	52
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	45
45	70.71	70.71							
Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees.
	DEGREES.		¾ DEGREE.		½ DEGREE.		¼ DEGREE.		

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