

LEVEL BOOK

400

F.B.262

Return to City Engineers Office
City Hall, San Diego, Cal.
H. S. CROCKER COMPANY

**DRAWING MATERIALS AND
 SURVEYING INSTRUMENTS**

SAN FRANCISCO

TABLES FOR EXCAVATIONS AND EMBANKMENTS

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING

Roadway 18 Feet Wide. Side Slopes 1 to 1.
 For Single Track Excavation.

"Copyright, 1895, by Kueffel & Esser Co."

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	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

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Return to City Engineers Office
City Hall, San Diego, Cal.

262
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TABL

DE

	0
0	9.
1	10.
2	11.
3	12.
4	13.
5	14.
6	15.
7	16.
8	17.
9	18.
10	19.
11	20.
12	21.
13	22.
14	23.
15	24.
16	25.
17	26.
18	27.
19	28.
20	29.
21	30.
22	31.
23	32.
24	33.
25	34.
26	35.
27	36.
28	37.
29	38.
30	39.
31	40.
32	41.
33	42.
34	43.
35	44.
36	45.

76 26 SW Nagli - India Elee Pale
5404 SW Lammud
9178 NW Nutmeg Elee Pale
10161 SE Palm Fern
10162 SW Onim Elee Pale

Cross Section of Congress St. (Old Town) from Arista
St to Smith St.

POSTED

S.L. Arista St.

W	9.0	27.3
U	9.0	27.3
1/4	8.7	27.6
C	8.9	27.4
S.E. CH.		
1/4	11.7 → 11.5	24.6 24.8
U	13.6	22.7 23.6
E	8.9	27.4
S. Ch.		
E	9.1	26.9 23.1
4 W. E. L.	13.1	
U	14.1	22.2 22.7
4 W. U	13.6	
1/4	9.5	26.8
C	9.5	26.8
1/4	9.5	26.8
U	9.5	26.8
W	9.3	27.0

4.11 Streets 50 Wide

50-4

W	9.7	26.6
U	9.7	26.6
1/4	9.8	26.5
C	10.0	26.3
U	9.7 14.0	26.6 22.3
U	14.3	22.0
U.E. Ch	14.3	22.0
E	12.1	24.2
Ch Arista		
E	14.3	22.0
U	10.0	26.0
1/4	10.3	26.0
C	10.3	26.0
1/4	10.1	26.2
U	9.7	26.4
W	11.0	25.3

36.28
No 4 Arista

W	11.2	25.1
U	10.3	26.0
1/4	10.4	25.9
U	10.7	25.6
1/4	10.6	25.7
U	10.2	26.1
E	10.6	25.7
	No.	Ch.
E	11.0	25.3
U	10.8	25.5
1/4	10.9	25.4
U	11.1	25.2
1/4	10.9	25.4
U	10.9	25.4
W	11.1	25.2

Congress 07
No Line

2

W	11.5	24.8
U	11.7	24.6
1/4	11.6	24.7
U	11.7	24.6
1/4	11.8	24.5
U	11.4	24.9
E	11.9	24.4
T.P.	1.72	25.23
	12.77	23.51
	25.11.0	Arista
E	2.2	23.0
U	2.3	22.9
1/4	2.3	22.9
U	2.1	23.1
1/4	2.1	23.1
U	2.4	22.8
W	2.3	22.9

13.77, 25.11, 24.4 N, E Arista

25.23
50 N. Aristo

W	3.7	21.5
d	3.8	21.4
$\frac{1}{4}$	4.0	21.2
c	4.1	21.1
$\frac{1}{4}$	3.6	21.6
u	3.2	22.0
E	3.4	21.8

75 N₀

E	4.6	20.6
a	5.1	20.1
$\frac{1}{4}$	5.3	19.9
c	5.1	20.1
$\frac{1}{4}$	5.2	20.0
u	5.5	20.0
V	4.7	20.5

Congress St

3

100 N₀

W	6.1	19.1
u	6.4	18.8
$\frac{1}{4}$	6.4	18.8
c	6.3	18.9
$\frac{1}{4}$	6.4	18.8
u	6.4	18.8
E	6.4	18.8

125 N₀

E	7.8	17.4
u	7.8	17.4
$\frac{1}{4}$	7.7	17.5
c	7.6	17.6
$\frac{1}{4}$	8.2	17.0
u	8.0	17.2
W	7.1	18.1

155 No

157 No Aristo

W	8.7	16.5
U	9.1	16.1
$\frac{1}{2}$	9.2	16.0
C	9.1	16.1
$\frac{1}{4}$	9.0	16.2
U	8.7	16.3
E	8.7	16.4

156 No

E	10.0	15.2
U	9.5	15.7
$\frac{1}{4}$	9.6	15.6
C	11.2	14.0
$\frac{1}{4}$	9.5	15.7
U	9.2	15.8
W	9.4	15.8

Congress St

175 No

W	10.8	14.4
U	10.7	14.5
$\frac{1}{2}$	10.4	14.8
C	11.1	14.1
$\frac{1}{4}$	10.8	14.0
U	10.4	14.8
E	10.3	14.9

176 No

E	10.5	14.7
U	10.6	14.6
$\frac{1}{4}$	10.9	14.5
C	11.5	13.7
$\frac{1}{4}$	11.1	14.1
U	11.3	13.9
W	11.2	14.0

2523

250 N. Aristo

W	11.7	13.5
a	12.0	13.2
U	11.9	13.3
C	11.2	13.9
U	10.3	14.9
a	10.0	15.2
E	9.3	15.9

255 N.

E	7.0	17.9
a	8.0	17.2
U	8.5	16.7
C	9.4	15.8
U	10.2	15.0
a	10.9	14.3
W	11.8	13.4

Congroos St

250 N.

W	10.5	14.7
U	9.5	15.7
U	9.1	16.1
C	8.6	16.6
U	7.9	17.3
U	7.3	17.9
E	6.5	18.7

275 N.

E	5.1	20.6
U	4.9	20.3
U	5.6	19.6
C	6.1	19.1
U	6.5	18.7
a	6.9	18.3
W	8.1	17.1

25.13

300 $\frac{1}{10}$ = 5.2

Con de

N	7.3	17.9
u	6.6	18.6
u	5.9	19.3
o	5.3	19.9
u	4.8	20.4
u	4.6	20.6
E	4.4	20.8
E	4.4	20.8
u	4.7	20.5
u	5.4	19.8
o	5.8	19.4
u	6.1	19.1
u	6.3	18.9
N	6.9	18.5

5, u

Congress St

50' d

6

KI	6.8	18.4
u	6.1	18.8
u	6.2	19.0
o	5.9	19.3
u	5.5	19.7
u	5.2	20.0
E	4.4	20.8
E	4.8	20.4
u	5.6	19.6
u	5.8	19.4
o	6.1	19.1
u	6.4	18.8
u	6.5	18.7
N	7.0	18.2

u

25.23

No. 21 Condo

W	11.3	13.9
U	10.5	14.7
S' E W	7.2	18.0
W	6.4	18.8
C	6.2	19.0
W	6.3	18.9
U	5.8	19.4
E	5.7	20.0

No. 22

E	5.5	19.7
U	5.9	19.3
W	6.2	19.0
C	6.7	18.5
W	9.2	15.8
U	10.9	14.3
W	7.9	15.3

Congress St

No. 110 Condo

W	7.8	17.4
S' E W	11.7	14.5
U	9.3	15.9
W	{7.7 11.5	{17.5 18.5
C	6.6	18.6
W	6.5	18.7
U	6.0	19.2
E	5.8	19.4

No. 111

E	7.1	18.1
U	6.3	18.9
W	6.5	18.7
C	7.0	18.2
W	7.2	18.0
S' W W	{9.6 9.5	{17.6 15.5
U	10.3	14.9
S' W W	{9.8 9.5	{15.4 15.6
W	7.9	17.3

25.93

40 No. Condo

W	8.7	16.5
U	8.2	17.0
T	9.7	15.5
C	{ 8.0 7.0	15.8 18.2
S	6.6	18.6
CC	7.4	17.8
E	7.2	18.0

57 No. Condo

E	6.3	18.9
U	6.8	18.4
S	7.1	18.1
C	7.7	17.5
T	8.3	16.9
U	8.5	16.7
W	8.8	16.4

Congress

St.

8

75 No. Condo

W	9.1	15.8
U	7.9	17.3
T	7.6	17.6
C	7.5	17.7
S	7.3	17.9
U	6.9	18.3
E	6.5	18.7

101 No. Condo

E	6.4	18.8
U	7.0	18.2
S	7.2	18.0
C	7.3	17.9
T	7.5	17.7
U	8.2	17.0
W	9.3	15.9

125 No. Conde

W	16.6
U	17.3
S	17.9
C	18.1
Sy	18.2
U	18.4
E	19.0

157 No. Conde

E	19.1
U	18.8
S	18.4
C	18.4
Sy	18.2
U	18.2
W	17.5

Congress 9

175 No. Conde

W	18.4
U	18.5
S	18.7
C	18.8
Sy	18.8
U	18.8
E	19.0

200 No. Conde

E	19.9
U	19.1
S	19.0
C	19.0
Sy	19.2
U	19.5
W	19.2

25.23

225 No. Condo

VI	5.3	19.9
U	5.0	20.2
4	4.8	20.4
C	5.3	19.9
4	5.3	19.9
U	5.2	20.0
E	4.3	20.9

250 No. Condo

E	3.5	21.7
U	4.1	20.8
4	4.5	20.7
C	4.7	20.5
4	4.5	20.7
U	4.5	20.7
W	4.7	20.5

Congrow

10

275 No. Condo

VI	4.1	21.1
U	4.2	21.0
4	4.2	21.0
C	4.3	20.9
4	3.9	21.3
U	3.1	22.1
E	2.3	22.9

Ami Spill Gravel Pit S.W. Harney

TR 462 27.18 2.67 22.56

500 No. Condo S.L. Harney

W	5.2	22.0
U	5.5	21.7
4	5.7	21.5
U	5.8	21.4
4	5.3	21.9
U	4.8	22.4
E	4.0	23.2

22.18

So Cl Horney

E	5.4	22.8
U	4.7	22.5
$\frac{1}{4}$	5.1	22.1
C	5.2	22.0
$\frac{1}{4}$	5.2	22.0
U	5.2	22.0
W	4.9	22.3
58 $\frac{1}{4}$		
W	5.0	22.2
U	4.9	22.2
$\frac{1}{4}$	5.2	22.0
C	4.9	22.3
$\frac{1}{4}$	4.6	22.6
a	4.7	22.5
E	4.5	22.7

Congress St.

CTR

11

E	4.6	22.8
U	5.1	22.8
$\frac{1}{4}$	5.1	22.8
C	4.7	22.5
$\frac{1}{4}$	4.9	22.3
U	4.9	22.3
W	4.8	22.4
No. 1		
W	4.7	22.5
U	4.8	22.4
$\frac{1}{4}$	4.8	22.4
C	4.5	22.6
$\frac{1}{4}$	4.4	22.8
U	4.4	22.8
E	4.3	22.9

2218

	No. Ch	Harney	
E		3.4	22.8
U		4.2	23.0
Sy		3.7	20.5
C		4.1	23.1
Sy		4.5	22.7
U		4.7	22.5
W		4.6	22.6

N. Line

W		4.5	22.7
U		4.3	22.9
Sy		4.4	22.8
C		3.9	23.3
Sy		4.3	23.2
U		4.1	23.1
E		4.1	23.1

Congress St

to N.

E		3.2	24.0
U		3.3	23.9
Sy		3.3	23.9
C		3.7	23.5
Sy		4.0	23.2
U		3.8	23.4
W		3.1	24.1

100 N.

U		3.0	24.2
U		3.4	23.8
Sy		3.4	23.8
C		3.4	23.8
Sy		3.3	23.9
U		3.0	24.2
E		3.2	24.0

2715

150 No Harney

E	3.0	24.2
U	3.4	23.8
1/4	3.5	23.7
C	3.6	23.6
1/4	3.6	23.6
U	3.5	23.7
W	3.5	23.7

200 No Harney

W	3.6	23.6
U	3.9	23.3
1/4	3.8	23.4
C	3.8	23.4
1/4	3.8	23.4
U	3.7	23.5
E	3.6	23.5

BM Spk Pole 50' W. 15. W. Cor Twigg 2.96 24.22

Congress St

250 No Harney

E	4.7	22.5
U	4.8	22.4
1/4	4.8	22.4
C	4.8	22.4
1/4	5.8	22.4
U	4.6	22.6
W	4.3	22.9

300 No = S. L. Twigg

W	4.2	23.0
U	4.5	22.7
1/4	4.5	22.7
C	4.9	22.3
1/4	5.1	22.1
U	5.0	22.2
E	4.7	22.5

13

27.8

So. Ct. Tullig 5

E	5.2	22.0
U	5.2	22.0
$\frac{1}{4}$	5.3	21.9
C	5.2	22.0
$\frac{1}{4}$	5.0	22.2
U	4.9	22.3
H	4.7	22.5
	So. Ct.	
W	4.7	22.5
U	4.6	22.6
$\frac{1}{4}$	5.0	22.2
C	5.3	21.9
$\frac{1}{4}$	5.3	21.9
U	5.2	22.0
E	5.2	22.0

Congress St.

Ctr

14

E	5.1	21.8
U	5.3	21.9
$\frac{1}{4}$	5.1	21.8
C	5.1	21.8
$\frac{1}{4}$	5.2	22.0
U	4.5	22.7
H	4.8	22.4
	So. Ct.	
W	4.9	22.3
U	4.8	22.4
$\frac{1}{4}$	4.8	22.4
C	5.1	21.8
$\frac{1}{4}$	5.1	21.8
U	5.4	21.8
E	5.4	21.8

27.8
No. 10 Twigg's

E	5.6	21.6
U	5.6	21.6
$\frac{1}{4}$	5.7	21.5
C	5.5	21.7
$\frac{1}{4}$	5.6	21.8
U	5.1	22.1
W	5.0	22.2
N.L.		
W	4.9	22.3
U	5.0	22.2
$\frac{1}{4}$	5.1	22.1
C	5.7	21.5
$\frac{1}{4}$	5.8	21.4
U	5.5	21.7
E	5.5	21.7

Congress St.
5714 Twigg's

15

E	6.4	20.8
U	6.4	20.8
$\frac{1}{4}$	6.3	20.9
C	6.5	20.8
$\frac{1}{4}$	6.3	20.9
U	6.0	21.2
W	5.9	21.3
N.L.		
W	6.8	20.4
U	7.0	20.2
$\frac{1}{4}$	6.9	20.3
C	7.1	20.1
$\frac{1}{4}$	7.1	20.1
U	7.0	20.2
E	6.9	20.3

27.18
150 No Twigg's

E	7.7	19.5
U	8.0	19.2
4	7.7	19.5
C	7.6	19.6
4	7.6	19.6
U	7.5	19.7
W	7.1	19.1

200 No Twigg's

W	7.3	19.9
U	7.5	19.7
4	7.6	19.6
C	7.8	19.4
4	7.8	19.4
U	7.9	19.3
E	8.0	19.2

T.P. 4.65 24.07 7.76 19.42

Congress St.
250 No Twigg's

16

E	4.8	19.3
U	4.7	19.4
4	4.6	19.5
C	4.5	19.6
4	4.1	20.0
U	4.3	19.8
W	4.4	19.7

300 No S.L. Mason

W	4.0	20.1
U	4.4	19.7
4	4.2	19.7
C	4.6	19.5
4	4.7	19.4
U	4.9	19.2
E	4.8	19.3

2407
S. Ct. Mason

E	5.3	18.9
U	5.4	18.7
4	5.1	19.0
C	4.9	19.2
4	4.9	19.2
U	4.8	19.3
W	4.3	19.8
So 4		
W	4.5	19.6
U	5.0	19.1
4	4.8	19.3
C	5.1	19.0
4	5.3	18.8
U	5.3	18.8
E	5.4	18.7

Congress St.
CTR

17

E	5.1	19.0
U	5.2	18.9
4	5.1	19.0
C	5.0	19.1
4	4.9	19.2
U	4.8	19.3
W	4.4	19.7
No 4		
W	4.6	19.5
U	4.9	19.2
4	4.8	19.3
C	5.1	19.0
4	5.2	18.9
U	5.1	19.0
E	5.0	19.1

2407
No. of Mason

E	4.8	19.3
U	5.0	19.1
1/4	5.2	18.9
C	5.0	19.1
1/4	4.8	19.3
U	4.9	19.2
W	4.9	19.2

50 N.L. Mason

W	4.5	19.7
U	4.5	19.6
1/4	4.5	19.7
C	4.7	19.4
1/4	4.8	19.3
U	5.0	19.1
E	4.8	19.3

Congress St.
25 1/6 Mason

18

E	5.1	19.0
U	4.9	19.2
1/4	4.6	19.5
C	5.0	19.1
1/4	5.1	19.0
U	5.0	19.1
W	4.8	19.3

50 N. Mason

W	5.5	18.7
U	5.3	18.8
1/4	5.3	18.8
C	5.2	18.9
1/4	5.2	18.9
U	5.2	18.9
E	5.2	18.9

2107

75 N. Mason

E	5.2	18.9
U	5.0	19.1
$\frac{1}{4}$	5.0	19.1
C	5.0	19.1
$\frac{1}{4}$	4.9	19.2
U	4.7	19.4
W	4.8	19.3

106 N. Mason

W	5.8	18.3
U	5.7	18.4
$\frac{1}{4}$	5.8	18.3
C	5.7	18.4
$\frac{1}{4}$	5.7	18.4
U	5.7	18.2
E	5.5	18.6

Congress St.

19

125 N. Mason

E	6.0	18.1
U	5.5	18.6
$\frac{1}{4}$	5.2	18.9
C	5.5	18.6
$\frac{1}{4}$	5.8	18.3
U	6.2	17.9
W	6.3	17.8

157 N. Mason

W	7.0	17.1
U	7.1	17.0
$\frac{1}{4}$	6.9	17.2
C	6.4	17.7
$\frac{1}{4}$	6.4	17.7
U	6.1	18.0
E	6.3	17.8

T.P. 0.40 18.21 6.26 17.81

1821
175 No Mason

E	0.6	17.6
U	0.9	17.3
$\frac{1}{4}$	1.3	16.9
C	1.5	16.7
$\frac{1}{4}$	1.6	16.6
U	1.9	16.3
W	2.1	16.1

200 No Mason

W	3.0	15.2
U	2.8	15.4
$\frac{1}{4}$	2.4	15.8
C	2.1	16.1
$\frac{1}{4}$	1.8	16.4
U	1.5	16.7
E	1.0	17.2

Congress St.
225 No Mason

20

E	1.7	16.5
U	2.1	16.1
$\frac{1}{4}$	2.3	15.9
C	2.6	15.6
$\frac{1}{4}$	3.1	15.1
U	3.8	14.4
W	4.8	13.4

250 No Mason

W	6.0	12.2
U	5.2	13.0
$\frac{1}{4}$	4.0	14.2
C	3.3	14.9
$\frac{1}{4}$	2.3	15.9
U	2.2	16.0
E	1.7	16.5

18.21

275 N. Mason

E	2.1	16.1
Ch	2.2	16.0
4	2.7	15.5
0	3.2	15.0
4	4.4	13.8
Ch	5.6	12.6
W	6.2	12.0

300 N. S. L. Smith

W	6.8	11.4
Ch	5.5	12.7
4	4.5	13.7
C	3.8	14.4
4	3.1	15.1
Ch	2.7	15.5
L	2.3	15.9

B. M. Hub. Ch Congress + Smith 4.27 13.74

POSTED

21

Cross Section of 'A' St from 15th 192

POSTED

	12.19	85.82		7362-B.M. N.W
Tf.	12.90	97.90	9.82	85.00
		E. Line 15 th		
So		97.9	9.6	88.3
Cl.			10.1	87.5
4			10.0	87.9
0			9.7	88.2
1.4			9.9	88.0
Cl			8.08	87.1
			8.14	87.7
No			9.6	88.3
		6 E 15 th		
No			10.5	87.4
7.5 N.C			11.3	86.6
Cl.			11.7	86.2

5 } Davis
 11 } Moran
 47 } Thurman

	16 th B.		20 E 15 th	
No		97.9	8.5	89.4
Cl			10.8	87.1
4			15.0	82.9
C			15.1	82.8
4			15.1	82.8
Cl			16.5	81.4
So.			17.0	80.9
		25 E 15 th		
So			15.2	82.7
Cl.			13.2	84.7
4			12.3	85.6
C			11.9	86.0
4			10.9	87.0
Cl			9.4	88.5
No			8.0	89.9

97.90

50 E 15th

N _o	3.6	94.3
10 S _o N.L.	1.7	96.2
cl	2.4	95.5
W	3.1	94.8
5 S _o W	3.6	94.0
C	2.7	90.2
W	10.0	87.9
cl	11.3	86.6
S _o	12.5	85.4

75 E 15th

S _o	10.2	87.7
cl	9.1	88.8
W	6.5	91.4
C	2.2	95.7

100 E 15th

S _o	5.8	92.1
cl	2.0	92.9
W	2.4	95.5

23

TP 12.63[✓] 109.77[✓] 0.76 97.14[✓]75 E 15th

N _o W	109.8	9.7	100.1
cl		8.7	101.1
W N _o cl		8.6	101.2
N.L.		12.0	97.8

100 E 15th

N _o	8.6	101.2
5 S _o N.L.	8.0	101.8
cl	5.1	104.8
W	5.5	104.3
C	10.0	99.8

125 E 15th

S _o	12.1	97.7
cl	10.1	99.7
W	7.0	102.5
C	4.6	105.2
W	4.1	105.7
cl	3.4	106.4
N _o	2.5	107.3

109.77

107 E 15th

No	109.8	0.6	109.2
U		1.0	108.8
4		1.5	108.3
C		1.2	108.6
4		2.9	106.9
U		5.2	104.4
S.		8.0	101.8

175 E 15th

S.		4.6	105.2
3 N.		2.8	107.0
U		1.5	108.3
T.P.	7.97	116.88	0.86
4			108.91
C		7.0	109.9
W		6.6	110.3
U		6.4	110.5
		5.4	111.5
No		3.6	113.3

24

200 E = W.L. 16th

No	114.9	2.1	114.0
U		4.4	112.5
4		6.6	112.3
C		5.3	111.6
U		5.9	111.0
U		5.7	111.2
S.		7.8	109.1

W 16th

S.		6.9	110.0
U		4.5	110.1
4		6.1	110.8
U		5.9	111.0
4		5.2	111.3
U		5.1	111.8
N.		4.4	112.5

116.88

W 2/16th

N.	3.8	113.9
U	3.9	113.0
L	4.7	112.2
C	5.2	111.7
L	5.8	111.1
U	6.4	110.5
S.	7.5	109.4

Ch 16th

S.	6.7	110.2
U	5.5	111.4
L	4.7	112.2
C	4.2	112.7
L	3.5	113.4
U	2.9	114.0
N.	1.9	115.0

25

E 2/16th

N.	1.7	115.2
U	2.5	114.4
L	3.1	113.8
C	3.8	113.1
L	4.4	112.5
U	4.9	112.0
S.	5.9	111.0

E 16th

S.	{ 6.6	110.3
	{ 5.0	111.2
	{ 5.4	111.5
U	{ 4.3	112.6
L	{ 4.7	112.2
	{ 3.2	110.7
C	{ 2.9	110.0
	{ 2.4	114.5
L	{ 3.9	113.0
	{ 2.3	114.6
	{ 3.2	113.7
U	{ 1.9	115.0
	{ 2.3	114.6
N.	{ 1.8	115.1

T.P. 12.87 127.49 2.26 114.62

E L 16

N ₆	10.6	116.9
U	10.3	117.2
L ₄	10.0	117.5
C	11.5	116.1
L ₄	12.5	115.0
U	13.7	113.8
S ₁	14.3	113.2

TP 8.06 129.51 6.05 121.45

S' E 16

S ₁	13.5	116.0
U	10.8	118.7
L ₄	9.0	120.5
U	6.9	122.6
L ₄	6.2	124.3
U	4.1	125.4
N ₆	2.8	126.7

25 E 16

N ₆	19	127.6
U	33	126.2
L ₄	48	124.7
C	6.0	123.5
L ₄	8.1	121.4
U	9.9	119.6
S ₁	12.6	116.9

50 E 16

S ₁	12.7	116.8
U	10.1	119.4
L ₄	7.8	121.7
C	5.9	123.6
L ₄	4.1	125.4
U	2.1	127.4
N ₆	0.8	128.7

129.51

75 E 16th

16	1.2	128.3
U	2.2	127.1
U	4.5	125.0
C	6.2	123.3
U	8.9	120.6
U	11.2	118.3
S.	12.8	116.7

100 E 16th

S. U.	12.1	117.4
U	9.6	120.1
C	7.7	121.8
U	5.9	123.6
U	3.7	125.8
No	1.8	127.7

27

125 E 16th

16	3.0	126.5
U	5.8	123.7
U	8.1	121.4
C	10.2	119.3
U	12.1	117.4

150 E 16th

No	6.5	122.7
U	8.7	120.8
U	10.5	119.0
C	12.3	117.2

175 E 16th

No	7.9	121.6
U	9.8	119.7
U	12.2	117.3

200 E-W.D. 17th

No	11.6	117.9
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TP 0.27 117.09 126.9 116.82

117.09

150' E 16 th

S.L. 2.1 115.0

175' E 16 th

S.L. 3.4 113.9

Cb 1.7 115.4

150' E 16 th

S. 5.4 111.7

U 5.2 111.9

L 1.3 115.8

175' E 16 th

S. 6.8 110.3

U 5.1 112.0

L 3.5 113.6

C 1.9 115.2

28

207' E = W L 17 th

2.0 116.1

2.7 114.4

4.6 112.5

5.8 111.3

7.2 109.9

9.3 107.8

W Cl. 17 th

10.7 106.4

8.7 108.4

7.0 110.1

5.8 111.3

4.8 112.3

3.0 114.1

1.2 115.9

117.09

W 4/17th

No	2.1	114.3
U	5.4	112.7
4	6.9	111.2
C	7.3	109.8
4	8.4	108.7
Q	10.2	106.9
S	12.6	104.5
Chr 17 th		
S. Ch.	12.3	104.8
U	9.9	109.2
C	8.9	108.2
4	7.5	109.6
U	6.7	111.4
No	4.1	113.0

29

E 4/17th

No	4.9	112.2
U	6.1	111.0
4	8.6	108.5
C	10.7	106.4
4	12.0	105.1

E Ch 17th

No	6.1	111.0
U	7.8	109.3
4	10.2	106.8
C	12.8	104.3

E. L. 17th

No	7.7	109.4
U	10.5	106.6
4	13.0	104.1

SE 17th

No	10.9	106.2
----	------	-------

11 0.10 104.45 12.94 104.35

Ctr 17th

S.L. 1.6 101.9

E 17th

So 4.1 100.1

Cr 2.0 102.5

E. Cr. 17th

So 4 2.9 101.6

Cr 6.6 99.9

S.L. 6.0 98.5

E.L. 17th

Cr 2.6 101.9

4 5.1 99.4

Cr 5.7 98.6

So 9.3 96.2

25 E 17th

No. Cr 1.3 103.2

4 4.0 100.5

Cr 6.6 97.9

4 9.2 95.3

Cr 9.5 95.0

So 11.3 103.2

50 E 17th

S.L. 12.8 92.5

4 11.6 92.9

Cr 8.4 96.1

Cr 6.5 98.0

Cr 4.2 100.3

No 1.9 102.6

75 E 17th

No. 4.2 100.3

Cr 5.8 98.7

Cr 7.7 96.9

4 10.9 93.6

Cr

100' E 17th

No	5.2	99.3
U	8.4	96.1
1/4	10.5	94.0
C	12.2	92.3

125' E 17th

No	7.4	97.1
U	9.8	94.7
1/4	11.8	92.7

150' E 17th

No	10.4	94.1
U	11.9	92.6
1/4	13.2	91.3

175' E 17th

No	12.1	92.4
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TP	0.21	91.76	12.90	91.55
----	------	-------	-------	-------

50' E 17th

S.L.	1.0	90.8
------	-----	------

75' E 17th

S. 1/4	0.8	91.0
U	0.8	91.0
S.L.	2.7	89.1

100' E 17th

S. 1/4	1.8	90.0
U	1.8	90.0
S.L.	3.8	88.0

125' E 17th

S.L.	4.6	87.2
U	2.6	89.2
1/4	2.4	89.4
CR	0.7	91.1

200' E 17th

CR	2.2	89.6
1/4	3.4	88.4
U	4.1	87.7
S.	5.2	86.4

9176

175' E 17th

50	7.3	84.5
46	5.5	86.3
44	5.8	86.0
C	4.3	87.5
4	2.4	89.4
U	1.2	90.6

200' E. W. L. 18th

N _o	1.7	90.1
U	3.4	88.4
4	4.5	87.3
C	5.7	85.9
4	6.6	85.2
Q	6.2	85.6
7.5. a	→ 6.6	85.2
S	8.4	83.4

E. L. 18th

50	6.2	85.6
U	2.0	89.8
4	6.4	85.4
0	6.3	85.5
4	5.7	85.9
U	6.2	85.6
N _o	5.6	86.2

25' E 18th

N _o	6.3	85.5
U	6.5	85.3
4	6.6	85.2
C	6.7	85.1
U	6.7	85.1
U	6.7	84.9
U	6.4	83.4
U	6.7	84.9
U	6.7	85.1

T.P. 3.01 87.59 7.18 84.58

F7.57

50 E 18th

So	3.3	84.3
8 N. S. L.	3.7	83.9
U	5.0	82.6
4 N. U.	3.8	83.8
W	3.4	84.2
C	3.7	83.9
W	4.1	83.5
U	4.1	83.5
No	4.2	83.6

75 E 18th

No	6.9	80.7
U	6.9	80.7
W	6.0	81.6
C	4.5	83.1
W	5.0	82.6
9 S. W.	5.8	81.8
U	7.1	80.5
5 S. U.	6.8	81.8
So	4.8	82.8

100 E 18th

So	7.1	80.2
U	8.0	79.6
W	8.1	79.5
C	8.9	78.7
W	11.8	75.8
U	9.0	78.6
No	8.8	76.8

110 E 18th

No	9.2	78.4
2 N. U.	9.7	77.9
U	13.2	74.4
W	13.4	74.2
C	13.4	74.2
W	13.6	74.0
U	10.2	77.4
So	9.3	78.3

17.59
125 E 10th

S ₁	14.7	72.9
Cl	14.3	73.3
S ₂	14.2	73.4
C	13.8	73.8
S ₃	13.7	73.9
3 1/2 S ₄ a.	12.9	74.7
Cl	12.2	75.4
5 1/2 N. Cl.	10.4	77.2
N ₁	10.1	77.5

150 E 11th

N ₁	11.1	76.5
Cl	11.4	76.2
S ₁	12.4	75.2
C	13.4	74.2
S ₂	14.3	73.3
Cl	14.6	73.0
S ₃	15.0	72.6

175 E 11th ¹²⁰ POSTED 34

S ₁	14.8	72.8
Cl	14.9	72.7
S ₂	14.6	73.0
C	13.0	74.6
S ₃	11.6	76.0
Cl	10.5	77.1
N ₁	10.0	77.6

200 E 11th 114.19²⁰

N ₁	10.0	77.6
Cl	10.6	77.0
S ₁	11.6	76.0
C	12.6	75.0
S ₂	13.5	74.1
Cl	14.4	73.2
S ₃	14.8	72.8

Note - V-shaped culvert in middle of block
and about on Cl this will have to be extended across
of where graded. Is about 3' high & 4' across bottom

Cross Section of Redwood

POSTED

	13.78	205.15		
TR	14.53	216.48	1.20	203.95
TR	3.98	218.09	2.39	214.11
		W.L. Horton Ave		
N ₆			2.8	215.3
U			2.6	215.5
U			2.5	215.6
U			2.5	215.6
U			2.6	215.5
U			2.7	215.4
S ₆			3.0	215.1
		25° W		
S ₀			2.1	216.0
U			1.9	216.2
U			1.8	216.3
U			1.7	216.4
U			1.9	216.2
U			2.0	216.1
N ₆			2.4	215.7

50° W

	192.37	Bd. Hula Cr. H. Spruce N ₆		2.5	215.6
U				2.3	215.8
U				2.0	216.1
U				1.7	216.4
U				1.4	216.7
U				1.3	216.8
S ₆				1.4	216.7
				75° W	
S ₆				1.6	216.5
U				1.7	216.4
U				1.9	216.2
U				2.5	215.6
U				2.9	215.2
U				3.1	215.0
N ₆				3.4	214.7

21809
100 W of Horton

No	48	213.3
U	41	214.0
U	39	214.2
U	35	214.6
U	28	215.3
U	25	215.6
So	22	215.9

125 W

U	31	215.0
U	37	214.4
U	52	213.9
U	49	213.2
U	54	212.7
U	60	212.1
No	73	210.8

36

150 W

No	10.1	208.0
U	8.5	209.6
U	7.4	210.7
U	6.7	211.4
U	5.8	212.3
U	5.1	213.0
So	4.5	213.6

175 W

So	5.5	212.6		
U	6.5	211.6		
U	7.6	210.5		
U	8.7	209.4		
U	9.5	208.6		
U	10.9	207.2		
No	12.3	205.8		
TP	5.15	211.36	11.88	206.21

200 W of Horton E.L. Union

N.	7.5	203.9
U	5.9	205.9
U	5.3	206.1
U	4.3	207.1
U	2.8	208.6
U	1.6	209.8
S.	0.8	210.6

E of Union

S.	1.6	209.8
U	2.6	208.8
U	3.6	207.8
U	4.7	206.7
U	5.9	205.5
U	7.0	204.4
N.	8.6	202.8

E of

N.	10.1	201.3
U	8.2	203.2
U	6.8	204.6
U	5.8	205.6
U	4.7	206.7
U	3.5	207.9
S.	2.2	209.2

Ctr.

S.	3.1	208.3
U	4.2	207.2
U	5.6	205.5
U	6.6	204.8
U	7.6	203.8
U	9.4	202.0
N.	11.1	200.3

W. L. Union

No	11.3	200.1
U	9.8	201.6
U	7.9	203.5
U	6.9	204.5
U	6.3	205.1
U	5.2	206.2
S	4.0	207.4

W. L.

S	4.9	206.5
U	6.6	205.8
U	6.6	204.8
U	7.6	203.8
U	9.2	202.2
U	10.7	201.7
No	12.2	199.2

W. L. Union

No	12.3	199.1
U	10.9	200.5
U	9.7	201.7
U	8.2	203.2
U	7.1	204.3
U	6.5	204.9
S	5.3	206.1

25 W

S	6.9	205.5
U	6.6	204.6
U	7.0	204.0
U	8.2	203.2
U	9.0	202.4
U	9.8	201.6
No	11.5	199.9

4136

50 ml of Urion

11.	10.1	201.3
16	8.7	202.7
4	8.0	203.4
0	7.5	203.9
4	6.7	204.7
4	6.5	205.2
0	5.8	205.6

75 ml of Urion

5.	8.3	206.2
16	8.8	205.4
4	6.6	204.6
0	7.2	204.2
4	7.9	203.5
16	8.4	203.0
16	9.4	202.0

100 ml

39

16	10.5	200.9
16	9.5	201.9
4	8.2	203.2
0	7.6	203.8
4	7.0	204.4
4	6.0	205.4
5.	5.3	206.1

POSTED

125 ml

5.	6.6	204.8
16	7.2	204.2
4	8.0	203.4
0	9.0	202.4
4	9.8	201.6
4	11.1	200.3
16	14.3	199.1

21136

150 W of Union

50		8.4	203.0
4		9.4	202.0
4		10.3	201.1
C		11.1	200.3
No 4		12.5	198.6

175 W

50		10.3	201.1
4		11.7	199.7
4		12.6	198.6

TR	0.35	199.86	11.85	199.51
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150 W

No		3.0	196.9
4		1.9	198.0

175 W

No		6.3	193.6
4		4.4	195.5
4		3.0	196.9
C		2.1	197.8

200 W = E. L. State

No		8.6	191.3
4		7.0	192.9
4		4.5	195.4
C		3.5	196.4
4		2.9	197.0
4		1.9	198.0
50		0.5	199.4

E. C.

50		1.9	198.0
4		2.8	197.1
4		3.7	196.2
C		4.5	195.4
4		6.6	193.3
4		9.0	190.9
No		10.6	189.3

19986
EVI State

N.	12.0	187.9
U	10.1	189.8
U	8.2	191.7
U	5.9	194.0
U	4.6	195.3
U	3.7	196.2
5.	3.1	196.8
CH.		
5.	4.1	195.8
U	4.6	195.3
U	5.9	194.0
U	7.7	192.2
U	10.0	189.9
U	12.0	187.9

W U

5.	5.3	194.6
U	6.2	193.7
U	7.6	192.3
U	9.2	190.7
U	10.9	189.0
U	13.3	186.6

W CH

5.	7.0	192.9
U	8.2	191.7
U	9.4	190.5
U	10.5	189.4
U	12.3	187.6

W line State

5.	8.8	191.1
U	10.0	189.9
U	10.9	189.0
U	12.2	187.7
TP	10.4	188.02

		188.02	
No	Ctr State		
		2.3	185.7
	W L		
No		3.0	185.0
	W C.		
No		5.5	182.5
Ch.		3.7	184.3
	W. line State		
No		7.7	180.3
Ch.		5.5	182.5
L		2.9	185.1
	2.5 W		
So		0.6	187.4
Ch		1.7	186.3
L		3.0	185.0
C		4.5	183.5
L		7.3	180.3
Ch		9.9	178.1
No		12.0	176.0

		50 W	
No. Ch.			
		13.3	174.7
L		11.6	177.6
C		9.0	179.0
L		7.0	181.0
Ch		5.2	182.8
So		4.1	183.9
	75 W		
So		8.4	179.6
Ch.		9.6	177.4
L		11.4	176.6
C		12.8	175.2
TP.	0.18	175.57	14.63 175.39
	50 W of State		
No		2.9	172.7
	75 W		
No		8.4	167.2
Ch		5.5	170.2
L		4.6	173.0

175.57

100 W of State

No		12.5	163.1
U		10.5	165.1
U		8.3	167.3
c		6.5	170.1
4		3.7	171.9
U		2.7	172.9
S.		1.1	174.5

125 W

50		7.0	168.6	
U		9.0	166.6	
U		10.6	165.0	
c		11.8	163.8	
TP	0.48	163.32	12.83	162.74
U		1.3	162.0	
U		3.2	160.1	
No		4.5	158.8	

43

150 W

No		8.5	154.8
U		7.4	155.9
U		6.7	156.6
c		4.6	158.7
U		2.4	160.9
U		2.0	161.3
S.		0.6	162.7

175 W

S.		5.3	158.0
U		6.9	156.4
U		8.2	155.1
c		9.9	153.4
U		10.9	152.4
U		11.5	151.8
No		12.6	150.7

163.32

200 West State E.L. Columbia

50		10.7	152.6
Cl		11.8	151.5
H		12.6	150.7
T.P.	0.53	151.08	147.7
			150.55
U		1.6	149.5
U		2.1	149.0
Cl		3.0	148.1
No		4.7	146.4
	E Cl		
N.		2.0	144.1
Cl		3.0	146.1
U		4.3	146.8
c		3.7	147.4
4		3.1	148.0
Cl		2.4	148.7
50		1.5	149.6

E L

50		3.6	147.5
Cl		4.2	146.9
U		4.7	146.4
c		5.6	145.5
c		6.0	145.1
U		7.3	143.8
N.		9.0	142.1
	Cl		
N.		11.0	140.1
Cl		9.3	141.8
U		7.8	143.8
c		7.4	143.7
U		7.0	144.1
Cl		6.3	144.8
50		5.4	145.7

15/108

W. line

5.	7.5	143.6
4	8.4	142.7
4	8.9	142.2
0	9.2	141.9
4	9.7	141.4
W.	10.9	140.2
N.	12.3	138.8
W. line		
No. 26	13.1	138.0
4	11.6	139.5
0	11.0	140.1
4	10.0	141.1
4	9.5	141.6
5.	9.1	142.0
W. line Columbia		
5.	11.3	139.8
W.	11.4	139.7
4	12.2	138.9

TP 0.00 138.77

12.75

138.33

45

W. line

N.	1.9	136.9
W. line Columbia		
CH	1.2	137.6
4	2.2	136.6
4	2.0	135.8
N.	4.0	134.8
25 W		
N.	8.1	130.7
W.	7.8	131.0
4	6.6	132.2
0	5.3	133.5
4	4.5	134.3
W.	3.5	135.3
5.	3.6	135.2

STED

50 W of Col

So	7.7	131.1
Cl	8.6	130.2
u	9.5	129.3
c	9.8	129.0
4	11.2	127.6
Cl	12.0	126.8
+6	11.8	127.0
No.	11.3	127.5
	11.5	127.3

TR 1.46 127.65 12.60 126.17

75 W

No	4.6	123.0
+5	3.9	123.7
+7	4.4	123.2
Cl	4.8	122.8
u	4.2	123.4
c	2.8	124.8
4	2.3	125.3
Cl	1.5	126.2
So	0.6	127.0

100 W

So	4.8	122.8
Cl	5.5	122.1
u	6.2	121.4
c	6.7	120.9
4	8.1	119.2
Cl	8.7	118.9
+7	8.3	119.3
+9	7.5	118.1
No.	7.5	120.1

125 W

No.	11.7	115.9
+5	11.4	116.2
+7	12.3	115.3
Cl	12.4	115.2
u	11.3	116.3
c	10.9	116.7
4	9.8	117.8
Cl	9.9	117.9
+9	10.0	
No.	8.6	119.0
TR	0.34 115.21 12.76	114.87

150 W. of Columbia

S.	0.6	114.6
Cl	1.2	114.0
H	1.6	113.7
C	2.1	113.1
V	3.2	111.8
W	3.8	111.4
+ P	3.0	113.2
+ 1.0	2.2	113.0
100		

175 W

N.	5.8	109.4
+ 1.0	6.8	109.6
+ 5	6.7	108.5
Cl	7.6	107.7
U	6.8	108.4
C	6.2	109.0
H	5.5	109.7
Cl	5.6	109.6
S	4.6	110.6

188 W

S.	6.5	108.7
Cl	7.9	107.3
U	7.6	107.6
C	8.4	106.8
V	8.4	106.8
Cl	9.3	105.9
N	8.8	106.4

200 W. - E. line India

N.	11.5	103.7
H	11.2	104.0
Cl	10.2	105.0
+ 5	13.2	102.0
C	12.6	102.6
U	12.6	102.6
W	12.2	102.8
+ 4	12.5	102.7
+ 6	9.5	105.8
S	7.8	107.4

TT	0.37	103.01	12.57	102.64
CHK 829	S. W. India 7.00000	1.42	101.59	101.54

W. line India

S.		5.8	97.2
U		6.1	96.9
U		6.5	96.6
C		6.5	96.5
U		6.7	96.3
U		6.7	95.6
U		6.7	96.3
N.		6.8	96.2

9 W

Nb		12.5	90.5
U		12.1	90.9
U		11.4	91.6
C		10.8	92.2
U		10.4	92.6
U		10.3	92.7
S.		11.0	92.0

T.P? 0.66 91.57 12.10 90.91

14 W of India

S.		5.0	91.6
U		5.1	91.5
U		0.7	90.9
C		0.6	91.8
U		1.6	90.0
U		2.7	88.9
N.		3.5	88.1

25 W

Nb		5.5	86.1
U		5.0	86.6
U		4.9	86.7
U		4.0	87.6
U		4.0	87.6
U		3.5	88.1
S.		3.4	88.4

91.57

50 W of India

S.	8.1	83.5
U	8.1	83.5
4	8.5	83.1
c	9.2	82.4
4	9.3	82.3
U	9.3	82.3
No	9.6	82.0

75 W

No	12.3	78.3
U	13.0	78.6
4	12.4	79.2
c	12.1	78.7
4	12.4	79.2
U	12.1	79.5
S.	11.2	80.4

TIP	0.20	79.04	12.73	78.84
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49

100 W

S.	3.2	75.8
U	3.2	75.8
4	3.5	75.5
c	3.5	75.5
4	3.7	75.3
U	4.0	75.0
No	4.0	75.0

POSTED

125 W

No	6.5	72.5
U	6.4	72.6
4	6.6	72.4
c	6.4	72.6
4	6.2	72.8
U	5.9	73.1
S.	5.7	73.3

29.04
150 W of India

S.	8.5	70.5
U	1.7	70.3
4	9.0	70.0
U	8.7	70.3
4	8.4	70.6
U	8.3	70.1
N.	8.4	70.6

175 W

N.	11.8	67.2		
U	11.6	67.4		
4	11.2	67.8		
U	10.9	68.1		
4	11.2	67.8		
U	10.7	68.3		
S.	10.6	68.4		
T.P.	11.5	67.24	12.95	66.09

200 W = E.L. Arctic

50

S.	1.5	65.7
U	1.7	65.5
4	1.7	65.5
U	1.3	65.9
4	1.8	65.4
U	2.0	65.2
N.	1.5	65.8

E.L.

N.	2.8	64.4
U	3.3	63.9
U	2.9	64.3
U	2.5	64.7
U	2.7	64.5
U	2.2	64.0
S.	3.4	63.8

672

E 4 Arctic

S	3.9	63.3
U	3.2	64.0
L	2.9	64.3
C	2.8	64.4
U	3.2	64.0
U	3.4	63.8
No	4.0	63.2

30 W of E. Line

No	8.0	59.2
U	7.8	59.4
U	7.8	59.4
C	7.7	59.5
U	7.5	59.7
U	7.3	59.9
S	7.3	59.9

51

2' E of Rail = 33' W of E. L.

S	7.7	59.5
U	7.8	59.4
U	8.0	59.2
C	8.0	59.2
U	8.1	59.1
U	8.1	59.1
No	8.5	58.7

CH = Top of Rail

S	7.2	60.0
CH	7.6	59.6
No	8.06	59.18
S	2' W of Rail = 40' W of E L 7.9	59.3
U	8.0	59.2
U	8.1	59.1
C	8.1	59.1
U	8.3	58.9
U	8.3	58.9
No	8.7	58.5

67.22
N. W. of En. Line Arctic

N.	6.6	60.6
U	6.4	60.8
U	6.5	60.7
C	6.5	60.7
U	6.2	61.0
U	6.1	61.1
So.	6.4	60.8

W. L.

So.	6.8	60.4
U	6.9	60.3
U	7.0	70.2
C	7.0	60.2
U	6.9	60.3
U	6.8	60.4
N.	7.3	59.9

W. C.

N.	8.3	58.9
U	7.8	59.4
U	8.0	59.2
C	8.1	59.1
U	8.3	58.9
U	8.2	59.0
So.	8.2	59.0

W. line Arctic

So.	9.5	57.7
U	9.5	57.7
U	9.5	57.7
C	9.8	57.4
U	10.0	57.2
U	10.0	57.2
N.	10.1	57.1

155 W of Ardio

No	10.2	44.6
Ch	10.3	44.5
H	10.2	44.6
C	9.8	45.0
H	9.7	45.1
U	9.5	45.3
So	9.2	45.6

157 W

So	11.9	42.9
Ch	12.4	42.4
H	12.6	42.2
C	12.7	42.1
H	13.1	41.7
U	13.1	41.7
No	13.0	41.8

T.P. 0.08 42.52 12.37 42.44

175 W of E. line California

No	27	39.8
U	2.1	40.1
H	3.0	39.5
C	3.5	39.0
H	3.1	39.4
U	3.0	39.5
So	3.1	39.4

POSTED

Top of Rail on St. Fe' R.R. in California

So	11.75	30.77
Ch	11.95	30.57
No	12.15	30.38

Sections State from Redwood to Quince

10/24/07
 W. L. Williams
 Emery
 POSTED
 477 204.25 199.57
 Sl. Redwood.

TR.	477	204.25	199.57
E		4.9	199.4
cb		6.3	198.0
1/4		7.5	196.8
c		8.4	195.9
1/4		9.8	194.5
cb		11.4	192.9
W		13.2	191.1
	50	5.	
W		11.1	193.2
cb		9.6	194.7
1/4		8.0	196.3
c		6.7	197.6
1/4		5.4	198.9
cb		4.1	200.2
E		2.5	201.8

204.28
 100.5

E		2.6	201.7
cb		3.3	201.0
1/4		4.1	200.2
c		5.4	198.9
1/4		6.8	197.5
cb		8.3	196.0
W		9.9	194.4
	150	5.	
W		10.4	193.9
cb		9.1	195.2
1/4		8.0	196.3
c		7.1	197.2
1/4		6.4	197.9
cb		5.4	198.9
E		5.0	199.3

204.28
200' S.

E	9.2	195.1
cb	9.3	195.0
1/4	9.5	194.8
Cr	10.1	194.2
1/4	10.8	193.5
cb	11.3	193.0
W	12.3	192.0

105 192.53 12.50 191.48
225' S.

W	1.9	190.6
cb	0.8	191.7
1/4	0.3	192.2
cr	0.1	192.4
1/4	0.0	192.5
cb	+0.2	192.7
E	+0.1	192.6

56
250 192.53
S -

E	3.9	188.6
cb	3.9	189.1
1/4	2.5	190.0
C	2.4	190.1
1/4	2.4	190.1
cb	2.6	189.9
W	2.9	189.6

275' S.

W	3.6	186.9
cb	6.1	186.5
1/4	6.5	186.0
C	7.3	185.2
1/4	7.8	184.7
cb	8.8	183.7
E	9.2	183.3

19253

300' S = NW Quince

E	15.1	177.4
cb	15.2	177.3
1/4	13.7	176.8
c	12.3	180.2
1/4	11.5	181.0
cb	10.5	182.0
W	10.0	182.5
Bm. Spk in Phone pole NW Cor. Stake - Quince	12.18	180.35
	N cb. Quince	
W	0.8	179.8
cb	2.1	178.5
1/4	2.9	177.7
c	4.2	176.4
1/4	5.7	174.9
cb	6.2	174.4
E	6.7	173.9

18056

N 1/4

57

E	10.3	170.3
cb	9.6	171.0
1/4	8.8	171.8
c	8.0	172.6
1/4	6.5	174.1
cb	4.8	175.8
W	3.6	177.0
	Or,	
W	6.2	174.4
cb	7.7	172.9
1/4	9.5	171.1
c	10.8	169.8
1/4	11.3	169.3
cb	12.3	168.3
E	14.3	166.3

25.05

5 1/4

W		8.9	171.7
cb		10.5	170.1
1/4		12.6	168.0
T.P.	0.22	168.18/260	167.96
cr.		1.2	167.0
1/4		1.6	166.2
cb.		3.5	164.7
E		5.7	162.5
	5 cl.		
E		5.8	162.4
+P'		9.3	158.8
cb		7.8	160.4
1/4		5.7	162.5
c		4.4	163.8
1/4		3.0	165.2
cb.		2.4	165.8
W		+0.3	168.5 168.5

168.18

POSTED

58

SLINE

W		4.7	163.5
cb		5.5	162.7
1/4		6.9	161.3
c		8.2	160.0
1/4		9.3	158.9
cb		12.4	155.8
E		6.8	161.4

Elough
Foglar
my Pranga

Intersection of Durna
India to Union

21 (80)
B.M.
India + Union

113.88

59

1234 113.88 101.54

E line of India

S.L.	104	103.5
bl	107	103.2
"	103	103.5
"	105	103.4
"	106	103.3
bl	110	102.9
22	102	103.6
22	40	109.9
bl	50	108.9
"	43	109.5
"	46	109.3
"	53	108.4
bl	63	107.6
S.L.	36	110.3

S.L. +7

bl

"

b

"

bl

22

T.P.

25' E of

India

1244

125.60

57' E of

India

+20	115.9	111.9
2.0		111.9
2.0		112.0
1.9		112.5
14		111.9
2.0		111.5
1.4		114.9
+1.0	114.9	114.9
0.72	113.16	
6.7		118.9
8.3		117.3
8.3		117.3
8.0		117.6
8.7		116.9
7.5		118.3
5.6		120.0

	75'	<u>12560</u>	E of India	
SL			0.5	125.3
bl			3.0	122.6
y			3.6	122.0
b			3.0	122.6
y			3.0	122.6
bl			3.5	122.1
nl			2.6	123.0

	100'	<u>12601</u>	E of India	
TP	1217		176	12384
nl			87	127.3
bl			97	126.3
y			97	126.6
b			9.2	126.8
y			9.1	126.9
bl			9.2	126.8
SL			6.7	129.3

	125'	<u>13601</u>	E of India	<u>Quince 21</u>	60
SL			4.0		132.6
bl			4.5		131.5
y			4.2		131.7
b			4.3		131.7
y			4.2		131.8
bl			4.7		131.3
nl			4.7		131.3

	150'	<u>14846</u>	E of India	
nl			0.3	135.7
bl			1.0	135.0
y			0.7	135.3
b			0.3	135.7
y			0.4	135.6
bl			0.5	135.5
SL			0.0	136.0
TP	1267		0.4	135.77

	175'	14846	India	
SL			84	140.1
bl			84	140.1
y			85	140.0
b			85	140.0
y			80	140.5
bl			74	141.1
SL			70	141.5
	200'	E = W 2 of	Columbian (75)	
SL			34	145.1
bl			35	145.0
y			37	144.9
b			43	144.2
y			40	144.5
bl			40	144.5
SL			42	144.3

		14846	Quina	61
			W 60 of	Columbian
SL			13	147.2
bl			15	147.0
y			16	146.9
b			17	146.8
y			15	147.3
bl			10	147.6
SL			16	146.8
TP	1280	16082	0.44	148.02
			W 1/4 of	Columbian
SL			11.1	149.7
bl			11.0	149.8
y			11.0	149.8
b			11.3	149.5
y			10.9	149.9
bl			11.0	149.8
SL			11.0	149.8

16082

center of Columbia st		
SL	90	157.8
bl	86	152.2
y	82	152.6
b	78	153.0
t	78	153.0
bl	78	153.0
bl	85	152.3

E'ly of Columbia st

SL	53	155.5
bl	52	155.6
y	53	155.5
b	52	155.6
y	54	155.4
bl	56	155.2
SL	62	154.6

16082 2000

E'ly of Columbia			62
SL	33	157.5	
bl	33	157.5	
y	30	157.8	
b	22	158.6	
y	22	158.6	
bl	24	158.6	
SL	18	159.0	
TP	1250	171.67	1.65-159.17

E'ly of Columbia st

SL	100	161.7
bl	105	161.2
y	98	161.9
b	96	162.1
y	104	161.3
bl	108	160.9
SL	112	158.6

60

25'

171.67

E of

Columbia

SL	7.1	164.6
bl	.64	165.3
γ	4.9	166.8
δ	4.6	167.1
γ	4.8	166.9
bl	5.2	166.5
SL	5.9	165.8

50'

E of

Columbia

TR	1230	<u>181.41</u>	256	12811
SL			100	171.4
bl			9.3	172.1
γ			9.5	171.9
δ			9.1	172.3
γ			9.4	172.0
bl			10.8	170.6
SL			12.4	169.0

181.41

Dinner at

75'

E of

Columbia

63

SL	9.1	172.3
bl	7.3	174.1
γ	5.6	175.8
δ	4.1	177.3
γ	4.2	177.2
bl	4.7	176.7
SL	5.4	176.0

100'

E of

Columbia

SL	1.7	179.5
bl	1.8	179.6
γ	1.7	179.7
δ	2.6	178.8
γ	3.3	178.1
bl	5.0	176.4
SL	7.8	173.6

		18141		
20	125'	E of	Columbia	
SL			86	172.8
bl			66	174.8
y			42	177.2
b			23	179.1
TP	572	18544	165	172.6
y			48	180.7
bl			38	181.7
nd			34	182.1
	424	18520	322	18026
	150'	E of	Columbia	
nd			16	183.6
bl			30	182.2
y			51	180.1
b			80	177.2
y			109	175.2
bl			122	173.0
SL			147	170.5

		18520		64
	175'	E of	Columbia at	
SL			17.7	167.5
bl			13.8	171.4
y			11.0	174.2
b			8.8	176.4
y			5.4	179.8
bl			3.4	181.8
nd			1.5	183.7
	200' E - W of	State st	(75')	
nd			2.8	182.4
bl			5.4	179.8
y			8.2	177.0
b			10.8	174.4
y			13.3	172.9
TP	159	17603	10.76	174.4
bl			7.2	168.8
SL			12.5	163.5

		17605		
SL	Edin of State		14.5	161.5
bl			13.4	162.6
y			13.2	162.8
b			9.6	166.4
y			5.6	170.4
bl			2.0	174.0
TP	1153	185.97	15.9	174.44
nl			8.5	177.5
	25'	E of State		
nl			10.6	175.4
bl			12.1	174.9
y			12.4	174.6
b			14.5	171.5
y			16.3	169.7
bl			17.4	168.6
SL			19.0	167.0

		185.97		65
SL	50'	E of State	13.0	173.0
bl			11.5	174.5
y			10.0	176.0
b			8.5	177.5
y			7.3	178.7
bl			6.0	180.0
nl			4.0	182.0
	75'	E of State		
nl			6.0	180.0
bl			5.2	180.8
y			4.4	181.6
b			3.3	182.7
y			2.4	183.6
TP	11.95	195.06	2.86	183.11
bl			10.5	184.6
nl			9.8	185.3

	100'	19506	E of State st	
SL			5.0	190.1
bl			6.8	188.3
y			7.2	187.9
b			7.7	187.4
y			7.8	187.3
bl			8.7	186.4
SL			9.5	185.6
	125'		E of State st	
SL			3.6	191.5
bl			2.3	192.8
y			0.7	194.4
b			0.5	194.6
y			0.2	194.9
bl			0.0	195.1
SL			0.0	189.1
TP	12.40	20698	0.57	194.55

	150'	20698	E of State st	Quincy	66
SL			7.7		199.0
bl			8.0		199.0
y			8.5		198.5
b			8.8		198.2
y			9.8		197.2
bl			11.2		195.8
SL			12.3		194.7
	175'		E of State st		
SL			9.7		197.3
bl			8.3		198.7
y			6.9		200.1
b			5.4		201.6
y			4.7		202.3
bl			4.0		203.0
SL			4.2		202.8

	(198) \$	206.98	W Sun. Union (85)	
	200	E =		
n 2			14	205.6
u			15	205.5
y			28	204.2
b			31	203.9
y			40	203.0
ll			48	202.2
Sd			70	200.0
TP	780	213.98	080	206.8 85 H 2min
			384	210.94 224 min

Continued on Page 77

Cross-Section of State St. Kalmia to Laurel.
 1/25 Davis Drive Colgate

0.24 114.65 114.41 - 271 Sp. Fence
 5' W. Chain 20' (No.)
 1.24 102.90 12.99 101.66
 5.39 97.66 10.63 92.27

No. line Kalmia

E 4.5 93.2
 Cl 5.5 92.2
 W 6.8 90.9
 C 8.5 89.2
 W 10.2 87.5
 Cl 12.1 85.6
 W 13.6 84.1

POSTED

25' No

W 13.6 84.1
 Cl 13.0 84.7
 W 12.3 85.4
 W 10.9 86.8
 C 9.3 88.4
 W 7.5 92.2
 Cl 5.6 92.1
 E 4.1 93.6

50' No

E 3.9 93.8
 Cl 5.5 92.2
 W 7.2 90.5
 C 8.7 89.0
 W 10.3 87.4
 +3 11.4 86.3
 Cl 12.6 85.1
 W 13.4 84.3

75' No

W 13.1 84.6
 Cl 12.1 85.6
 +9 10.6 87.1
 +11 8.7 89.0
 W 8.6 89.1
 C 7.5 90.2
 W 6.4 91.3
 Cl 5.1 92.6
 E 3.9 93.8

100 No. of Kalmia

E	2.5	95.2
Cl	3.8	93.9
$\frac{1}{4}$	5.0	92.7
C	6.5	91.2
$\frac{1}{2}$	7.7	90.0
+6	8.3	89.4
+9	10.8	86.7
Cl.	11.8	85.9
W.	12.6	85.1

125' No

W	12.5	85.2
Cl	12.0	85.7
+7	7.7	90.0
$\frac{1}{4}$	7.1	90.6
C	6.0	91.7
$\frac{1}{2}$	4.3	93.4
Cl	2.9	94.8
E	1.7	96.0

150' No

E	1.8	95.9
Cl	2.4	95.3
$\frac{1}{4}$	4.2	93.5
C	6.6	91.1
$\frac{1}{2}$	7.6	90.1
+4	7.8	89.9
Cl.	12.8	84.9
W.	12.9	84.8

175' No

W	13.0	84.7
Cl.	14.1	83.6
+7	13.8	83.7
$\frac{1}{4}$	9.9	87.8
C	8.2	89.5
$\frac{1}{2}$	6.6	91.5
Cl	4.7	93.0
E	3.2	94.5

9766

200' No. of Kalmia

E		4.5	93.2
ct.		6.3	91.4
1/4		8.2	89.5
C		10.1	87.6
+8		12.1	85.6

225' No.

E		6.7	91.0
ct.		8.6	89.1
1/4		11.4	86.3
C		13.3	84.4

250' No.

E		9.6	88.1
ct.		11.2	86.5
T.P.	0.26	85.09	12.83
			84.83

70

200' No. Kalmia

W 1/4		1.4	83.7
+2		2.6	82.5
ct.		2.3	82.8
W.		2.8	82.3

225' No.

20' W. of W.L.		8.4	76.7
W.		5.3	79.8
ct.		4.7	80.4
1/4		4.0	81.1
+2		3.5	81.6

250' No.

25' W. of W.L.		12.6	72.5
W		8.8	76.3
ct.		7.1	78.0
1/4		5.0	80.1
+11		4.4	80.7
C		3.4	81.7
1/2		1.0	84.1

67

85.09

275' No. of Kalmia

E	1.1	84.0
Cl.	2.5	82.6
W	5.1	80.0
C	4.9	80.2
W	7.3	77.8
Cl.	9.7	75.4
W.	11.6	73.5

300' No. = S.L. Laurel

W	13.3	71.8
Cl.	12.1	73.0
W	10.9	74.2
C	8.4	76.7
W	5.8	79.3
Cl.	5.1	80.0
+9	4.6	80.5
+11	1.9	83.2
E	1.9	83.2
T.P.	0.35	74.13
	11.31	73.78

71

275' No. of Kalmia

25' W of W.L.	6.2	67.9
	S.L. Laurel	
25' W of W.L.	8.6	65.5

POSTED

ED

blought
700
Danga
cross-section of Laurel St (50')
W of Union to E of Columbia

	466	12092	11676	
	W. line of		Union	Ben 7000 ft at Columbia Union
SS			15	
bl			15	
"			17	
b			15	
b			19	
bl			32	
rd			50	
	25'	W of Union		
rd			103	
bl			89	
"			85	
b			70	
"			70	
bl			73	
SS			72	
TP	0.28	109.26	11.94	108.98

109.26 Laurel

	50'	W of Union	
SS			3.0
bl			2.3
"			4.2
b			4.8
"			6.3
bl			8.3
rd			10.2
	75'	W of Union	
rd			140
bl			137
"			122
b			10.3
"			9.3
bl			9.0
SS			7.5
TP	0.60	98.05	11.81
			97.45

65

	100'	98.05	w of Union st
SL			1.8
ll			2.7
"			4.3
b			5.3
"			6.4
ll			7.5
SL			8.9
	125'		w of Union
SL			12.7
ll			12.0
"			9.8
b			8.5
"			8.3
ll			8.0
SL			5.7

73

	150'	98.05	w of Union
SL			10.8
ll			11.3
"			11.2
b			12.8
TP	0.68	87.94	10.79
"			2.7
ll			3.6
SL			2.6
	137'		w of Union
ll			5.0
SL	158'		w of Union
			7.6
			7.6
			7.6
			7.6

175' 87.94 W of min

~~72 84
bl 80
" 81
l 79
" 78
bl 75
SR 74~~

175' W of min

SR 75
bl 74
" 72
l 76
" 81
bl 80
72 89

200' 87.94 W = C 2 of State St ^(75') **74**

~~SR 8.8
bl 9.2
" 9.4
l 9.2
" 10.2
bl 11.5
72 13.9
TP 11.08 7686~~

0.97 77.83 E 1/2 of S State St

~~72 67
bl 43
" 2.8
l 2.0
" 1.8
bl 2.0
SR 1.5~~

E 1/4 of State st

SE	4.0
NE	5.0
W	2.8
S	4.4
W	6.7
NE	7.6
SE	8.2
center of State st	
NE	10.4
NE	10.7
W	9.0
S	8.4
W	6.4
NE	5.5
SE	4.9

W 1/4 of State st

SE	6.3
NE	8.6
W	9.5
S	10.8
W	11.6
NE	13.4
NE	14.0
TP	16.6
W 1/4 of State st	
NE	69.22
NE	10.27
NE	67.52
NE	8.4
NE	7.3
W	6.4
S	4.5
W	4.5
NE	1.7
SE	0.9

69.22

Wd of	State	it
SL	7.9	64.3
U	6.6	62.6
1	8.0	61.2
1	9.1	60.1
1	10.3	58.9
U	10.4	59.0
22	10.4	58.8
TP	2,35- 6,55-	10.0 59.20

55

Cross-section of Quince St (80')

W of Union to W of Hartman

Bm SE cor. Union & Quince

	556	211.74	206.18
	W	S of	Union st (75')
SL		11.7	200.0
bl		10.6	201.1
4		9.4	202.3
6	POSTED	8.0	203.7
4		7.5	204.2
bl		6.6	205.1
7.2		6.2	205.5
	W of	Union st	
7.2		5.3	206.4
bl		6.0	205.7
4		6.5	205.2
6		7.2	204.5
4		8.0	203.7
bl		9.0	202.7
SL		10.4	201.3

211.74

W of Union st

77

SL	9.4	202.3
bl	8.3	203.4
4	7.0	204.4
6	6.3	205.4
4	5.6	206.1
bl	5.0	206.7
7.2	4.3	207.4
	Center of	Union
7.2	3.6	208.1
bl	3.9	207.8
4	4.5	207.2
6	5.2	206.5
4	6.7	205.5
bl	7.2	204.5
SL	8.3	203.4

POSTED

211.74

E 1/4 of Union

SL	75	204.2
bl	67	205.0
y	58	205.9
b	48	206.9
y	40	207.7
bl	33	208.4
SL	25	209.2

E bl of Union

SL	20	209.7
bl	27	209.0
y	30	208.7
b	39	207.8
y	50	206.7
bl	67	205.4
SL	69	204.8

211.74

E 1/4 of Union

SL	57	206.0
bl	54	206.3
y	47	207.0
b	38	207.9
y	30	208.7
bl	22	208.5
SL	08	210.9

25' E of Union

SL	07	211.0
bl	19	209.8
y	26	209.1
b	34	208.5
y	42	207.5
bl	52	206.5
SL	48	206.9

21174

	50'	E of	Number	at
SL			47	207.0
bl			50	206.7
"			44	207.3
l			31	208.6
"			25	209.2
l			16	210.1
nl			00	211.7
	75'	E of	Number	at
nl			00	211.7
bl			14	210.3
"			21	209.6
l			28	208.9
"			36	208.1
bl			49	206.8
SL			46	207.1

21174

79

	100'	E of	Number	at
SL			49	206.8
bl			51	206.6
"			42	207.5
l			32	208.5
"			23	209.4
bl			17	210.0
nl			07	211.0
	125'	E of	Number	at
nl			15	210.2
bl			29	208.8
"			36	208.1
l			45	207.2
"			53	206.4
bl			57	206.0
SL			57	206.0

21174

150' E of Anna st

Sl	Sl	7.3	204.4
b	ll	6.6	205.1
"	"	6.2	205.5
b	b	5.6	206.1
"	"	5.5	206.2
b	ll	4.3	208.4
2	2l	3.3	208.4

POSTED

175' E of Anna

2	2l	5.0	206.7
b	ll	5.4	206.3
"	"	6.0	205.7
b	b	7.0	204.7
"	"	7.8	203.9
ll	ll	9.0	202.7
Sl	Sl	11.2	202.5

21174

Luna

200' E = W of Hartson

2l	8.2	203.5		
ll	10.7	201.0		
<hr/>				
TP	4.73	205.22	11.25	200.49
1/4	6.2	199.0		
b	10.3	194.9		
"	12.5	192.7		
ll	13.5	191.7		
Sl	16.8	188.4		

Impudencia
Arista
Conde
Harney
Furgos
Mason
Smith

Return to City Engineers Office
City Hall, San Diego, Cal.

262

7.8
5.7
2.1
1.2

101.50

37.5
1.40
35.2

32.5
4.3
41.6

12
1.20

12.00
12.75
24.75

37.50
1.25
38.75

63.00
1.20

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

FOR SINGLE TRACK EMBANKMENT.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

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