F.B.319

Return to City Engineers Office
City Hall, San Diego, Cal.

H. S. CROCKER COMPANY

DRAWING MATERIALS AND SURVEYING INSTRUMENTS

SAN FRANCISCO

319

TABLES FOR EXCAVATIONS AND EMBANKMENTS

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING

Roadway 16 Feet Wide, Slopes 1½ to 1.

For Single Track Excavation.

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	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MICROFILMED
1964

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FROM
Lorinda Park Store

Cross-Section of Beryl Street from Broadway to the Ocean. 9/3/07 { Davis, Embry, Goliath

	1.10	132.15 ✓		131.05 BM Hub N.W. Bwdy	
		W.L. Bwdy			
No			1.1		131.1
U			2.9		
U			3.8		
C			4.6		127.6
U			5.2		
U			6.0		
So			7.0		125.2
		50 W			
So			8.9		123.3
U			7.3		
U			6.7		
C			5.9		126.3
U			5.3		
U			4.6		
No			3.4		128.8
		100 W			
No			4.8		127.4
U			6.0		
U			6.8		
C			7.4		124.8
U			8.1		
U			9.1		
So			10.6		121.6

POSTED

	150 W		
Beryl			
So		10.9	121.3
U		9.3	
U		8.6	
C		8.0	124.2
U		7.1	
U		6.5	
No		4.9	127.3
	200 W		
No		5.0	127.2
U		6.6	
U		7.1	
C		7.8	124.4
U		8.7	
U		9.5	
So		11.2	121.0
	250 W		
So		11.2	121.0
U		9.6	
U		8.9	
C		8.3	123.9
U		7.8	
U		7.2	
No		5.6	126.6

		132.15			
	300 W of Bwdy.				
No			6.5		125.7
W			8.1		
W			9.1		
C			9.9		122.3
W			9.9		
W			10.8		
So			12.4		119.8
		350 W			
So			13.6		118.6
W			12.4		
W			11.7		
C			11.3		120.9
W			10.5		
W			10.0		
No			9.1		123.1
		400 W			
No			11.0		121.2
W			12.0		
W			12.5		
C			13.0		119.2
T.P.	2.68	122.05 ✓	12.78	119.37 ✓	
W			3.4		
W			3.7		
So			4.6		117.5

Beryl Street

		121	
	450 W		
So		5.8	116.3
W		5.0	
W		4.3	
C		4.2	117.9
W		3.6	
W		3.2	
No		2.1	120.0
	411 W		
No		2.9	119.2
W		3.7	
W		4.2	
C		4.7	117.4
W		5.2	
W		5.4	
So		{6.5 {8.0 W.	115.6 114.1
	496 W		
So		7.6	114.5
W		6.8	
W		5.5	
C		4.7	118.4
W		4.2	
W		4.0	
No		3.1	119.0

122.05

500 W = E. Line of Haines

No	3.2	118.9
Ct	3.9	
L	4.7	
C	6.9	115.2
L	7.0	
Ct	7.2	
So	6.5	115.6

10 W of E. L

So	6.6	115.5
Ct	5.6	
L	5.2	
C	6.1	116.0
L	6.4	
Ct	6.2	
No	3.5	118.6
	500 W	116.7

15 W of E L

No	6.0	116.1
Ct	5.3	
L	4.4	
C	4.8	117.3
L	5.2	
Ct	5.7	
So	6.5	115.6

122.05

20 W of E L - E Ct

So	6.8	115.3
Ct	5.7	
L	5.2	
C	4.9	117.2
L	4.4	
Ct	4.1	
No	4.8	117.3

24 W of E L

No	3.5	118.6
Ct	4.1	
L	4.6	
C	4.9	117.2
L	5.2	
Ct	5.6	
So	6.8	115.3

30 W = E L

So	6.7	115.4
Ct	5.6	
L	5.1	
C	4.8	117.3
L	4.5	
Ct	3.9	
No	3.3	118.8

122.05

Ctr of Haines

N.	3.1	119.0
"	4.1	
"	4.5	
C	4.9	117.2
"	5.2	
"	5.8	
S.	6.7	115.4
W "		
S.	7.8	114.3
"	6.2	
"	5.8	
C	5.2	116.9
"	4.8	
"	4.1	
N.	3.3	118.8
W "		
N.	3.3	118.8
"	4.7	
"	5.0	
C	5.5	116.6
"	5.5	
"	5.9	
S.	6.8	115.3

Beryl Street

W line Haines

S.	6.4	115.7
"	6.3	
"	5.5	
C	4.9	117.2
"	4.6	
"	4.3	
N.	3.4	118.7
50 W.		
N.	3.8	118.3
"	5.0	
"	5.4	
C	5.2	116.9
"	5.4	
"	6.0	
S.	6.6	115.5
100 W		
S.	6.9	115.2
"	6.4	
"	6.1	
C	5.8	116.3
"	5.3	
"	4.9	
N.	4.4	117.7

122.05

150 W of Haines

No		4.4		117.7
Cl		5.2		
4		5.6		
c		6.0		116.1
4		6.2		
Cl		6.6		
So		7.3		114.8
	200 W			
So		8.1		114.0
Cl		7.4		
4		7.1		
c		6.7		115.4
4		6.1		
Cl		5.7		
No		4.8		117.3
	250 W			
No		5.4		116.7
Cl		6.3		
4		6.7		
c		7.2		114.9
4		7.7		
Cl		8.5		
So		9.2		112.9

	300 W			
So			90.0	112.1
Cl			9.2	
4			8.6	
c			7.9	114.2
4			7.6	
Cl			7.3	
No			6.2	115.9
	350 W			
No			6.8	115.3
Cl			7.7	
4			8.2	
c			8.8	113.3
4			9.2	
Cl			9.8	
So			10.7	111.4
	400 W			
So			11.0	111.1
Cl			10.0	
4			9.6	
c			9.1	113.0
4			8.5	
Cl			8.0	
No			7.2	114.9
TP	3.05	118.03	7.07	114.98

118.03

450 W of Haines

No	3.5	114.5
"	4.2	
"	4.7	
C	5.1	112.9
"	5.7	
"	6.2	
S.	7.1	100.9
	500 W- E.L. Gresham	
So	7.1	100.9
"	5.9	
"	5.5	
C	5.0	113.0
"	4.7	
"	4.4	
No	3.3	114.7
	E ct	
No	3.2	114.8
"	4.0	
"	4.4	
C	4.9	113.1
"	5.5	
"	5.8	
So	6.9	111.1

POSTED

Beryl Street.

E ½

So	6.8	111.2
"	5.9	
"	5.4	
C	4.9	113.1
"	4.5	
"	4.1	
No	3.1	114.9
	Ctr.	
No	2.9	115.1
"	4.1	
"	4.6	
C	4.9	113.1
"	5.5	
"	5.9	
So	6.8	111.2
	W ½	
So	6.8	111.2
"	6.0	
"	5.5	
C	4.8	113.2
"	4.4	
"	3.9	
No	2.8	115.2

POSTED

118.03

W. Ch. Gresham

No	2.9	115.1
Ch	3.7	
W	4.2	
C	4.7	113.3
W	5.2	
Ch	5.8	
S.	6.5	111.5

W. line Gresham

So	6.5	111.5
Ch	5.7	
W	5.3	
C	4.7	113.3
W	3.9	
Ch	3.5	
No	2.9	115.1

50' W

No	2.7	115.3
Ch	3.7	
W	4.2	
C	4.6	113.4
W	5.1	
Ch	5.8	
S.	6.6	111.4

100 W

So	6.6	111.4
Ch	6.1	
W	5.5	
C	4.9	113.1
W	4.4	
Ch	3.8	
No	2.8	115.2

150' W

No	2.8	115.2
Ch	3.9	
W	4.4	
C	4.9	113.1
W	5.4	
Ch	6.0	
S.	6.7	111.3

200 W.

S.	7.0	111.0
Ch	6.2	
W	5.5	
C	5.0	113.0
W	4.6	
Ch	4.1	
No	3.2	114.8

118.03

	350 W of Gresham		
No	3.3	114.7	
Ct	4.2		
H	4.7		
C	5.1	112.9	
H	5.5		
Ct	6.3		
So	7.0	111.0	
	300 W.		
So	7.0	111.0	
Ct	6.2		
H	5.7		
C	5.0	113.0	
H	4.6		
Ct	4.1		
No	3.2	114.8	
	350 W		
No	3.5	114.5	
Ct	4.5		
H	4.9		
C	5.4	112.6	
H	5.9		
Ct	6.4		
So	7.0	112.0	

Beryl Street.

	400 W		
So	7.4	110.6	
Ct	6.7		
H	6.1		
C	5.7	112.3	
H	5.4		
Ct	5.0		
No	4.2	113.8	
	450 W		
No	5.1	112.9	
Ct	5.8		
H	6.3		
C	6.6	111.4	
H	6.9		
H	7.3		
So	8.0	110.0	
	500 W. E.L. Fanuel		
So	8.8	109.2	
H	7.9		
H	7.3		
C	6.6	111.4	
H	6.3		
H	6.1		
No	5.3	112.7	
T.P 0.52	113.25 ✓	5.30	112.75 ✓

113.25

E Cl Fanuel

No	0.7	112.6
Cl	1.5	
Sp	1.8	
C	2.3	111.0
Sp	2.8	
Cl	3.3	
So	4.2	109.1

E Sp

So	4.4	108.9
Cl	3.5	
Sp	3.1	
C	2.6	110.7
Sp	2.2	
Cl	1.8	
No	1.1	112.2

Ctr.

No	1.0	112.3
Cl	1.8	
Sp	2.2	
C	2.6	110.7
Sp	3.0	
Cl	3.4	
So	4.3	109.0

W Sp

So	4.7	108.6
Cl	3.6	
Sp	3.1	
C	2.7	110.6
Sp	2.4	
Cl	2.0	
No	1.2	112.1

W Cl

No	1.0	112.3
Cl	1.8	
Sp	2.3	
C	2.7	110.6
Sp	3.1	
Cl	3.6	
So	4.5	108.8

W. line

So	4.7	108.6
Cl	3.7	
Sp	3.3	
C	2.9	110.4
Sp	2.5	
Cl	2.1	
No	1.4	111.9

113.25

50 W of Fanuel

No	2.4	110.9
Ct	3.0	
1/4	3.7	
C	3.9	109.4
1/4	4.3	
Ct	4.6	
So	5.3	108.0
100 W		
So	6.3	107.0
Ct	5.7	
1/4	5.2	
C	4.7	108.6
1/4	4.7	
Ct	4.5	
No	4.2	109.1
150 W		
No	5.9	107.4
Ct	6.2	
1/4	6.4	
C	6.6	106.7
1/4	6.7	
Ct	7.0	
So	7.7	105.6

Beryl Street

200 W		
So	8.6	104.7
Ct	8.0	
1/4	7.6	
C	7.4	105.9
1/4	7.2	
Ct	7.0	
No	6.6	106.7
250 W		
No	7.6	105.7
Ct	8.1	
1/4	8.3	
C	8.7	104.6
1/4	9.0	
Ct	9.2	
So	9.9	103.4
300 W		
So	10.3	103.0
Ct	9.9	
1/4	9.7	
C	9.3	104.0
1/4	9.1	
Ct	9.0	
No	8.6	104.7
T.P. 0.84 104.98 ✓	9.11	104.14 ✓

104.98

350 W of Kanuel

No	1.0	104.0	
Cl	1.5		
H	1.9		
O	2.2	102.8	
H	2.5		
Cl	2.8		
So	3.4	101.6	
400 W.			
So	1.0	101.0	
Cl	3.2		
H	2.8		
O	2.6	102.4	
H	2.1		
Cl	2.2		
No	1.7	103.3	
450 W			
No	2.6	102.4	
Cl	3.0		
H	3.3		
O	3.5	101.5	
H	3.8		
Cl	4.1		
So	4.8	100.2	

500 W. El. Everts.

So	5.1	99.9
Cl	4.6	
H	4.3	
O	3.9	101.1
H	3.6	
Cl	3.4	
No	3.0	102.0
E Cl.		
No	3.5	101.5
Cl	4.0	
H	4.3	
O	4.5	100.5
H	4.9	
Cl	5.1	
So	5.5	99.5
E H		
So	5.8	99.2
Cl	6.3	
H	6.0	
O	4.7	100.3
H	4.5	
Cl	4.2	
No	3.8	101.2

		104.98			
		Ctr Everts			
No			4.0		101.0
Ct			4.5		
4			4.7		
C			4.9		100.1
4			5.3		
Ct			5.5		
So			5.9		99.1
		W 1/2			
So			6.0		99.0
Ct			5.7		
4			5.4		
C			5.1		99.9
4			4.7		
Ct			4.7		
No			4.3		100.7
		W Ct.			
No			4.6		100.4
Ct			5.0		
4			5.2		
C			5.5		99.5
4			5.8		
Ct			5.9		
So			6.4		98.6

	Beryl Street.		
	W. line Everts.		
So		6.7	98.3
Ct		6.6	
4		6.4	
C.		6.2	98.8
4		5.9	
Ct		5.7	
No		5.2	99.8
	50 W.		
No		7.2	97.8
Ct		7.6	
4		7.6	
C		7.7	97.3
4		8.0	
Ct		8.3	
So		8.4	96.6
	100 W		
So		9.9	95.1
Ct		9.4	
4		9.3	
C		9.2	95.8
4		9.0	
Ct		8.8	
No		8.5	96.5

104.98

150 W of Everts

No			9.3		95.7
U			9.7		
L			9.9		
C			10.0		95.0
L			10.2		
U			10.6		
So			11.0		94.0
		200 W			
So			11.3		92.7
U			11.9		
L			11.6		
C			11.3		93.7
L			11.1		
U			10.8		
~~No~~			10.4		94.6
TP	0.55	94.12	11.41	93.57	
		250 W			
No			0.7		93.4
U			1.2		
L			1.5		
C			1.7		92.4
L			1.9		
U			2.2		
So			2.5		91.6

94.1

300 W

So		3.5	90.6
U		3.1	
L		2.7	
C	POSTED	2.5	91.6
L		2.4	
U		2.1	
No		1.7	92.4
	350 W		
No		3.6	90.5
U		4.3	
L		4.4	
C		4.6	89.5
L		4.8	
U		4.9	
So		5.2	88.9
	400 W		
So		7.3	86.8
U		7.5	
L		7.1	
C		6.8	87.3
L		6.4	
U		6.1	
No		5.2	88.9

94.12

450 W of Everts

No	6.0	88.1
Ct	7.2	
Lt	7.8	
C	8.4	85.7
Lt	9.0	
Ct	9.2	
So	9.6	84.5

500 W. El Dawes

So	10.9	83.2
Ct	10.2	83.9
Lt	9.7	
C	9.1	85.0
Lt	8.5	
Ct	8.0	
No	6.8	87.3

E Ct

No	7.2	86.9
	7.8 gate	86.3
Ct	8.1	
	8.8 "	
Lt	8.7	
	9.5 "	
C	9.3	84.8
	10.1 "	84.0
Lt	10.1	
	10.7 "	
Ct	10.6	
	11.2 "	
So	10.9	83.2
	11.7 "	82.4

Beryl Street

E Lt

So	11.2	82.9
Ct	10.6	
Lt	10.0	
C	9.4	84.7
Lt	8.8	
Ct	8.4	
No	7.3	86.8

Ctr

No	7.3	86.8
Ct	8.2	
Lt	8.8	
C	9.4	84.7
Lt	10.1	
Ct	10.5	
So	11.0	83.1

W Lt

So	11.3	82.8
Ct	10.7	
Lt	10.1	
C	9.5	84.6
Lt	9.0	
Ct	8.6	
No	7.7	86.4

94.12

W Ch Dawes

No		8.5 gutr 7.9	85.6 86.2
Ch		9.3 8.8 "	
W		10.1 " 9.3	
C		10.4 " 9.9	83.7 84.2
4		11.0 " 10.5	
Ch		11.6 " 10.9	
So		11.9 " 11.5	82.2 82.6
	W line		
So		11.8	82.3
Ch		11.2	
4		10.7	
C		10.1	84.0
4		9.6	
Ch		9.1	
No		8.2	85.9
	50 W		
No		9.4	84.7
Ch		10.0	
4		10.3	
C		10.7	83.4
W		11.1	
Ch		11.5	
So		12.3	81.8

		100 W		
So			12.8	81.3
Ch			12.2	
4			12.0	
C			11.6	82.5
4			11.1	
Ch			10.4	
No			10.4	83.7
T.P.	0.75	83.59	11.28	82.84
		100 W		
No			0.7	82.9
Ch			1.6	
4			1.8	
C			2.0	81.6
4			2.1	
Ch			2.6	
So			3.2	80.4
		200 W		
So			4.1	79.5
Ch			3.5	
4			3.2	
C			2.9	80.7
4			2.7	
Ch			2.5	
No			2.0	81.6

83.59

200 W of Dawes

No	3.4	80.2
U	3.7	
U	3.8	
C	3.7	79.9
U	3.1	
U	3.6	
So	4.7	78.9

300 W

So	5.7	77.9
U	5.2	
U	5.1	
C	4.9	78.7
U	4.8	
U	4.7	
No	4.5	79.1

350 W

No	4.9	78.7
U	5.2	
U	5.4	
C	5.7	78.0
U	6.0	
U	6.4	
So	7.4	76.2

Beryl Street

400 W

So	8.8	74.8
U	8.0	
U	7.2	
C	6.7	76.9
U	6.5	
U	6.2	
No	5.7	77.9

450 W

No	6.8	76.8
U	7.5	
U	7.9	
C	8.0	75.6
U	8.5	
U	8.9	
So	9.9	73.7

500 W EL Cass

So	10.8	72.8
U	10.1	
U	9.8	
U	9.3	74.3
U	9.0	
U	8.6	
No	8.2	75.4

T.P. 5.84	81.21	8.20	75.39 Hub N.E Cass
		0.51	80.70 Hub S.W Cass and Wilbur

8121

E Ct. Cass

No	6.6 / 7.1 gutr	74.6 / 74.1
U	7.0 / 7.6 "	
4	7.2 / 7.9 "	
C	7.5 / 8.1 "	73.7 / 73.1
4	7.8 / 8.4 "	
U	8.2 / 8.9 "	
So	9.1 / 9.6 "	72.1 / 71.6

E-W

So	8.9	72.3
U	8.3	
4	8.0	
C	7.7	73.5
4	7.4	
U	7.1	
No	6.5	74.7

Ctr

No	6.7	74.5
U	7.3	
4	7.6	
C	7.8	73.4
4	8.1	
U	8.4	
So	8.9	72.3

W-E

So	9.4	71.8
U	8.9	
4	8.7	
C	8.5	72.7
4	8.3	
U	8.2	
No	7.8	73.4

W Ct.

No	8.4 gutr / 8.0	72.8 / 73.2
U	8.6 " / 8.3	
4	8.8 " / 8.4	
C	9.0 " / 8.6	72.2 / 72.6
4	9.3 " / 9.0	
U	10.0 " / 9.3	
So	10.2 " / 9.9	71.0 / 71.3

W. line

So	9.7	71.5
U	9.2	
4	9.0	
C	8.8	72.4
4	8.6	
U	8.5	
No	8.2	73.0

81.21

50 W of Cross

No	8.7	72.5
"	8.9	
"	9.1	
"	9.3	71.9
"	9.5	
"	9.7	
So	10.2	71.0
100 W		
So	10.9	70.3
"	10.4	
"	10.2	
"	9.8	71.4
"	9.8	
"	9.5	
No	9.3	71.9
150 W		
No	9.8	71.4
"	10.1	
"	10.1	
"	10.2	71.0
"	10.7	
"	11.0	
So	11.8	69.4

Beryl Street.

200 W

So	12.0	69.2
"	11.4	
"	11.1	
"	10.8	70.4
"	10.6	
"	10.4	
No	10.1	71.1
250 W		
No	10.6	70.6
"	11.0	
"	11.2	
"	11.4	69.8
"	11.6	
"	11.9	
So	12.5	68.7
300 W		
So	12.9	68.3
"	12.5	
"	12.2	
"	11.9	69.3
"	11.7	
"	11.4	
No	11.0	70.2
T.P. 2.16	72.23	11.14	70.07

72.23

350 W of Cass

No		2.4		69.8
Ct		2.9		
4		3.2		
c		3.3		68.9
4		3.7		
Ct		3.8		
So		4.2		68.0
	400 W			
So		4.8		67.4
Ct		4.3		
4		4.0		
c		3.7		68.5
4		3.6		
Ct		3.3		
No		2.7		69.5
	450 W			
No		3.2		69.0
Ct		3.7		
4		4.1		
c		4.1		68.1
4		4.4		
Ct		4.8		
So		5.5		66.7
BM		5.41	66.82 Spk Pole S.E. Bay [illegible]	

500 W E.L. Bayard

So		5.7	66.5
Ct		5.3	
4		4.9	
c		4.7	67.5
4		4.5	
Ct		4.3	
No		3.4	68.8
	E Ct		
No		3.9	68.3
Ct		4.4	
4		4.7	
c		5.0	67.2
4		5.2	
Ct		5.5	
So		6.0	66.2
	E 4		
So		6.2	66.0
Ct		5.7	
4		5.4	
c		5.2	67.0
4		5.0	
Ct		4.7	
No		4.2	68.0

72.23

Ctr Bayard.

No	3.9	68.3
Ct	4.3	
1/4	4.7	
C	5.0	67.2
1/4	5.2	
Ct	5.5	
So	5.9	66.3

W 1/4

So	6.3	65.9
Ct	5.7	
1/4	5.3	
C	5.2	67.0
1/4	4.8	
Ct	4.6	
No	4.0	68.2

W Ct.

No	4.0	68.2
Ct	4.5	
1/4	4.8	
C	4.7	67.5
1/4	5.1	
Ct	5.6	
So	6.1	66.1

Beryl Street.

W line Bayard.

So	6.2	66.0
Ct	5.6	
1/4	5.2	
C	4.8	67.4
1/4	4.8	
Ct	4.6	
No	4.0	68.2

50 W

No	4.3	67.9
Ct	4.6	
1/4	5.0	
C	5.2	67.0
1/4	5.6	
Ct	5.8	
So	6.3	65.9

100 W

So	6.4	65.8
Ct	5.9	
1/4	5.7	
C	5.6	66.6
1/4	5.4	
Ct	5.1	
No	4.7	67.5

72.23

150 W of Bayard

No	5.0	67.2
"	5.4	
"	5.8	
C	6.0	66.2
"	6.2	
"	6.5	
So	6.7	65.5
	200 W	
So	7.8	64.4
"	7.3	
"	6.8	
C	6.7	65.5
"	6.7	
"	6.6	
No	6.1	66.1
	250 W	
No	7.2	65.0
"	7.6	
"	7.8	
C	8.1	64.1
"	8.3	
"	8.5	
So	9.0	63.2

300 W

So	9.8	62.4
"	9.4	
"	9.2	
C	8.9	63.3
"	8.7	
"	8.6	
No	8.2	64.0
	350 W	
No	8.9	63.3
"	9.5	
"	9.6	
C	10.0	62.2
"	10.1	
"	10.4	
So	10.8	61.4
	400 W	
So	12.0	60.2
"	11.5	
"	11.2	
C	11.1	61.1
"	10.8	
"	10.7	
No	10.3	61.9
T.P. 1.65	63.74	10.14	64.09

6374

	430 West Bayard			
No		2.9		60.8
W		3.2		
W		3.4		
C		3.6		60.1
W		3.8		
W		4.0		
So		4.5		59.2
	500 W. E.L. Allison			
So		4.8		58.9
W		4.4		
W		4.1		
C		3.8		59.9
W		3.8		
W		3.7		
No		3.4		60.3
	E Ch.			
No		3.3		60.4
W		3.5		
W		3.9		
C		4.2		59.6
W		4.4		
W		4.5		
So		4.8		58.9
BM.		4.18.	59.56	Spk. Pole SE Allison

Beryl Street. 6374

E ½

So		5.5	58.2
W		5.1	
W		4.7	
C		4.4	59.3
W		3.9	
W		3.6	
No		3.6	60.1
	2' E of Rail		
No		3.8	59.9
W		4.1	
W		4.2	
C		4.5	58.2
W		4.7	
W		4.9	
So		5.3	58.4
	2' W of Rail		
So		5.8	57.9
W		5.6	
W		5.4	
C		5.0	58.7
W		4.8	
W		4.8	
No		4.4	59.3
	Ctr. = Top Rail		
No		3.1	60.6
Ctr.		3.8	59.9
		4.45	59.29

63.74

W ¼ Allison

No	4.4	59.3
W	4.7	
W	5.0	
C	5.3	58.4
H	5.8	
W	5.8	
So	5.7	57.9

W Ct

So	6.2	57.5
W	6.1	
H	5.8	
C	5.8	57.9
H	4.4	
W	4.2	
No	3.8	59.9

W. line

No	4.1	59.6
W	4.6	
H	5.9	
C	6.1	57.6
H	6.4	
W	6.7	
So	7.0	56.7

40 N. of Allison

So	9.3	54.4
W	7.4	
H	6.8	
C	5.5	58.2
H	4.4	
W	4.2	
No	4.5	59.2

50 W

No	4.5	59.2
W	6.7	
H	6.7	
C	7.1	56.6
H	7.5	
W	7.9	
So	9.3	54.4

100 W

So	11.0	52.7
W	10.2	
H	9.6	
C	9.2	54.5
H	9.0	
W	8.7	
No	7.9	55.8

6374

150 W of Bayard

No			10.4		53.3
U			11.0		
L			11.1		
C			11.2		52.5
L			11.4		
U			11.6		
So			12.1		51.6
T.P.	229	53.72	12.31	51.43	
	200 W				
So			4.5		49.2
U			4.1		
L			3.8		
C			3.7		50.0
L			3.4		
U			3.2		
No			3.4		50.3
	250 W				
No			5.2		48.5
U			6.0		
L			6.0		
C			6.2		47.5
L			6.5		
U			6.7		
So			7.0		46.7

53.72

24

300 W

So			9.6		44.1
U			9.1		
L			8.6		
C			8.2		45.5
L			7.9		
U			7.6		
No			6.9		46.8
	350 W				
No			8.7		45.0
U			9.8		
L			10.2		
C			10.4		43.3
L			10.8		
U			11.2		
So			11.7		42.0
T.P.	201	48.32	12.41	41.31	
	400 W				
So			7.5		40.8
U			6.8		
L			6.3		
C			5.8		42.5
L			5.4		
U			5.0		
No			3.9		44.4

48.82

450 W=E.L Alley-So.

No	3.9	44.4
"	5.6	
"	6.2	
C	6.8	41.6
"	7.4	
"	7.8	
So	8.9	39.4

470 W=W.L Alley-So.

So	8.1	40.2
"	7.1	
"	6.6	
C	6.2	42.1
"	5.6	
"	5.0	
No	3.5	44.8

500 W=E.L. Alley-No

No	3.9	44.4
"	4.0	
"	4.3	
C	4.4	43.9
"	4.2	
"	5.8	
So	6.7	41.6

520 W=W.L. Alley So

So	6.6	41.7
"	6.1	
"	5.8	
C	5.5	42.8
"	5.2	
"	4.8	
No	3.8	44.5

570 W

No	6.6	41.7
"	7.2	
"	7.1	
C	7.4	40.9
"	6.9	
"	5.6	
So	6.4	41.9

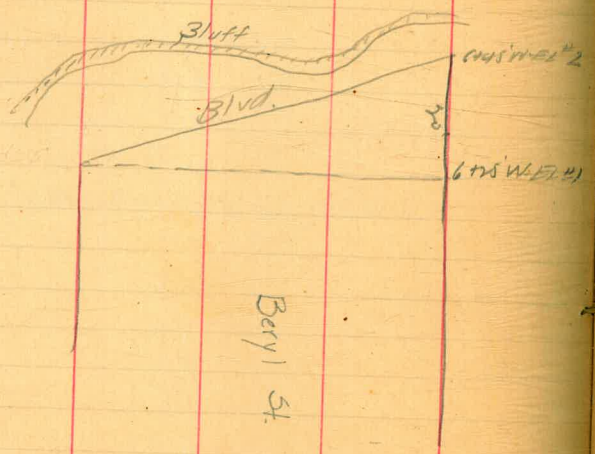
625 W=EL. Blvd. on So=EL #1

So	7.8	40.5
"	9.3	
"	9.6	
C	9.6	38.7
"	9.5	
"	9.2	
No	9.1	39.2

4.8-32

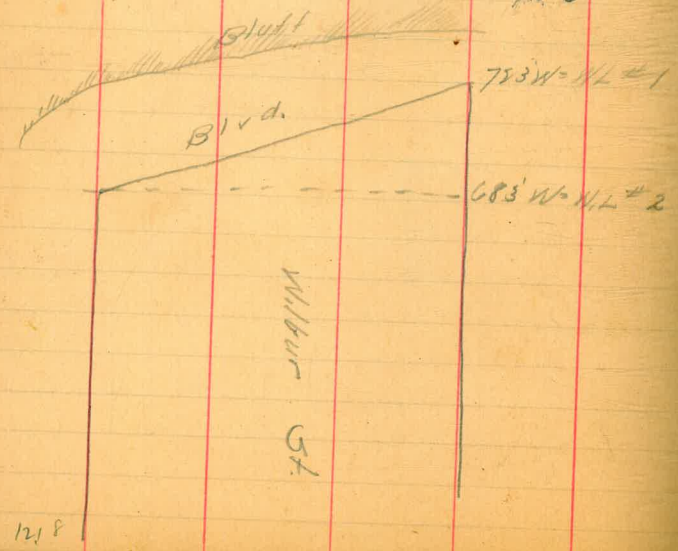
6+45 W on No. 8 6+25 W on So = WL Blvd #2

No	9.9	38.4
Ub	10.0	
L	9.9	
c	9.6	38.7
L	9.6	
Ub	9.3	
So	7.8	40.5



Cross-Section of Wilbur ~~St.~~ Ave Ocean to Broadway 9/24/07 { Emery Corbett

		48.32 ✓			
	4.53	40.26 ✓	12.59	35.73 ✓	
	E.L. Blvd #1 = 723' W of Allison on No = 683' W on So				
No			14.6		25.7
Ct			8.7		
4			5.4		
C			1.7		38.6
	683' W of Allison = E.L. Blvd #2				
No			7.7		32.6
Ct.			3.8		
4			1.2		
	670' W = W.L. Alley on No				
No			4.9		35.4
T.P.	12.48	52.34 ✓	0.40	39.86 ✓	



1218

	E.L. Blvd #1	
So 4	11.2	
Ct.	8.8	
So	8.4	43.9
	E.L. Blvd #2	
Ctr.	11.3	41.0
4	10.1	
Ct	8.5	
So	8.4	43.9
	670' W of Allison = W.L. Alley - No	
No. Ct.	11.2	
4	10.0	
C	9.4	42.9
4	8.4	
Ct.	7.5	
So	6.7	45.6
	650' W = E.L. Alley - No	
So	5.5	46.8
Ct	6.0	
4	6.6	
C	6.7	45.6
4	6.6	
Ct	7.5	
No	10.2	42.1

52.34

		618 W of Allison			
No			7.4		44.9
"			4.9		
"			3.6		
4 N. Ch			3.5		
Ch			{3.3-5		46.9
So L			3.4		49.0
"			3.3		
So			4.6		47.7
		600 W of Allison			
So			3.3		49.0
"			1.2		
"			1.2		
C			1.7		50.6
"			2.2		
"			2.6		
No			4.9		47.4
TP.	12.63	44.87	0.10	52.24	
		500 W			
No			13.2		51.7
"			11.8		
4			10.8		
C			9.5		55.4
4			8.0		
"			8.0		
So			10.8		54.1

6.49

		520 W. Rd. Away - So.	
So		7.7	57.2
"		6.2	
"		5.8	
C		6.7	58.2
"		7.4	
"		7.8	
No		8.2	56.7
		520 W. El. Away - So	
No		6.1	58.8
"		6.0	
"		6.0	
C		6.0	58.9
"		6.2	
"		6.5	
So		6.6	58.3
	450 W		
So		5.9	59.0
"		4.6	
"		4.6	
C		4.9	60.0
"		5.1	
"		4.8	
No		4.6	60.3

64.87

400 W of Allison

N.	3.3	61.6
"	3.7	
"	3.9	
C.	4.1	60.8
"	4.1	
"	4.3	
S.	4.8	60.1

350 W

S.	4.2	60.7
"	3.8	
"	3.7	
C	3.5	61.4
"	3.3	
"	3.0	
N.	2.9	62.0

300 W

N.	2.2	62.7
"	2.5	
"	2.8	
C	3.0	61.9
"	3.2	
"	3.4	
S.	3.9	61.0

250 W

S.	3.5	61.7
"	2.9	
"	2.6	
"	2.4	62.5
"	2.2	
"	2.0	
N.	1.7	63.2

200 W

N.	1.1	63.8
"	1.4	
"	1.5	
C	1.7	63.2
"	1.8	
"	2.0	
S.	2.4	62.5
1.1 gal	71.89	2.22 62.65

150 W

S.	8.7	63.2
"	8.4	
"	8.2	
C	8.1	63.8
"	7.9	
"	7.7	
N.	7.4	64.5

71.89

100 W of Allison

No.	6.6	65.3
"	6.9	
"	7.0	
"	7.1	64.8
"	7.2	
"	7.3	
So.	7.6	64.3

50'

So.	6.6	65.3
"	5.9	
"	5.8	
"	5.6	66.3
"	5.4	
"	5.2	
No	5.0	66.9

W. L. Allison

No.	4.4	67.5
"	4.7	
"	5.0	
"	5.0	66.9
"	5.4	
"	5.7	
So	6.2	65.7

Note- Intersection of Allison Cross Sections are taken across Allison instead of across Wilbur as they can be taken to a better advantage. Elevation of East Rail is taken as track is on a curve & said rail is the higher.

5.L Allison

W	6.2	65.7
9' E of W.L.	6.6	65.3
12' " "	8.3	63.6
17' " 2' W of Rail	7.7	64.2
Ch.	7.0	64.9
3' E of Ch. Top of E Rail.	6.7	65.2
6' E of Ch. 2' E of Rail	7.4	64.5
½	7.5	64.4
4' E of ½	5.9	66.0
Ch	5.2	66.7
3' E Ch.	3.9	68.0
½	5.5	66.4
Ch.	5.9	66.0
E.	5.6	66.3

50 Ch. Allison

E	5.3	66.6
Ch	5.3	
½	4.9	
4' E of Ch.	4.9	
Ch.	4.7	67.2
½	5.5	
3 W of ½	7.5	
3' E of Ch. 2' E of Rail	7.0	
1' E of Ch. Top of E Rail	6.3	
Ch	6.5	
14' E of W.L. 2' W of Rail.	7.2	
10' " " "	7.7	

71.89

S. Ch.		
6' E of W.L.	5.7	
W.L	5.7	66.2
S. ½ Allison		
W.	5.4	66.5
6' E of W.L.	6.0	
9' " "	7.4	
2' W of Rail = 13 E of W.L.	6.9	
Ch. Top of E. Rail	6.1	
2' E of " = 22 E of W.L	6.9	
6' E of Ch.	7.4	
½	5.3	
Ctr	4.4	67.5
2 E Ctr.	2.3	
½	4.7	
Ch	5.0	
E	5.0	66.9
Ctr Allison		
E	4.8	67.1
Ch	4.8	67.1
½	4.7	67.2
C	4.2	67.7
½	4.9	67.0
25 E of W.L.	7.2	64.7
Ch. 2' E of Rail	4.6	65.3
Top of E Rail.	5.94	65.95
11 E of W.L.	6.7	65.2
7 " "	7.5	64.4

5' E of W.L.	5.9	66.0
W.L.	5.0	66.9
No ½		
W.	5.0	66.9
3 E of W.L.	5.2	
6' " "	7.0	
10' " " = 2' W of Rail	6.5	
12' = Top of E Rail	5.75	
2' E "	6.5	
Ch	6.7	
½	4.5	
C	3.8	68.1
½	4.5	
Ch	4.6	
E.	4.6	67.3
N. Ch.		
E	4.3	67.6
Ch	4.3	
½	4.5	
C	3.5	68.4
½	4.4	
5. E of Ch.	4.5	
Ch	6.5	
2 E of Rail = 17' E of W.L	6.3	
Top of E Rail	5.55	
9 E of W.L = 2 W of Rail	6.4	

71.89

No Cl

7' E of W.L.	6.8	
3" " "	5.2	
W.L.	4.8	67.1
No line Allison		
W	4.4	67.5
2' E	6.1	65.8
7'0" = 2 W of Rail	6.2	65.7
Top of E. Rail = 12 E of W.L.	5.2	66.7
2' E of Rail	6.0	65.9
Cl.	5.9	66.0
3 E of Cl.	4.3	67.6
4	3.7	68.2
Ctr.	1.9	70.0
4	4.0	67.9
Cl	3.9	68.0
E	3.9	68.0
E.L Allison		
No	3.9	68.0
Cl	4.3	
4	4.6	
C	4.8	67.1
4	5.0	
Cl	5.2	
So	5.6	66.3

50 E of Allison

So	5.2	66.7
Cl	4.8	
4	4.5	
C	4.3	67.6
4	4.2	
Cl	4.0	
No	3.5	68.4
100' E		
No	3.2	68.7
Cl	3.9	
4	4.0	
C	4.3	67.6
4	4.4	
Cl	4.5	
So	4.9	67.0
150 E		
So	4.1	67.8
Cl	3.5	
4	3.0	
C	2.8	69.1
4	2.7	
Cl	2.6	
No	2.1	69.8

71.89

		200 E of Hilson			
No			1.4		70.5
U			1.9		
U			2.0		
C			2.3		69.6
U			2.6		
U			2.7		
S			3.5		68.4
		250 E			
So			1.6		70.3
U			1.4		
U			1.3		
C			1.0		70.9
U			0.9		
U			0.6		
No			0.4		71.5
T.P	10.13	81.41	0.61	71.28	
		300 E			
No			8.8		72.6
U			9.1		
U			9.1		
C			9.2		72.2
U			9.5		
U			9.7		
So			10.0		71.4

	350 E		
So		9.0	72.4
U		8.7	
U		8.3	
U		8.2	73.2
U		8.0	
U		7.8	
No		7.4	74.0
	400 E		
No		6.4	75.0
U		6.9	
U		7.2	
U		7.2	74.2
U		7.2	
U		7.0	
S		8.3	73.1
	450 E		
So		7.4	74.0
U		7.0	
U		6.7	
C		4.6	74.8
U		6.3	
U		6.1	
No		5.6	75.8

81.41

500 E - W.L. Boyard

No		4.9		76.5
Ut		5.5		
4		5.6		
C		6.0		75.4
4		6.1		
Ut		6.4		
So		6.8		74.6
	W. Ct.			
So		5.7		75.7
Ut		6.2		
4		5.9		
C		5.4		76.0
4		5.2		
Ut		4.8		
No		4.0		77.4
	A ½			
No		4.3		77.1
Ut		5.0		
4		5.3		
C		5.6		75.8
4		5.8		
Ut		6.1		
So		6.2		75.2

Ct.

So		5.8		75.6
Ut		5.5		
4		5.3		76.4
C		5.0		76.4
4		4.8		
Ut		4.5		
No		4.1		77.3
	E ½			
No		4.6 4.2 - E		76.8 77.2
Ut		5.1 4.8 "		
4		5.3 5.0 - E		
C		5.5 5.2 "		75.9 76.2
4		5.7 5.4 "		
Ut		6.0 5.6 "		
So		6.3 6.0 "		74.9 75.4
	Ct.			
So		6.1		75.3
Ut		5.6		
4		5.4		
C		5.0		76.4
4		4.7		
Ut		4.6		
No		4.2		77.2

81.41

E. line Bayard

No.	3.9	77.5
"	4.2	
"	4.5	
"	4.7	76.7
"	4.9	
"	5.3	
So.	5.8	75.6
50 E		
So.	5.6	75.8
"	4.8	
"	4.6	
"	4.4	77.0
"	4.3	
"	4.0	
No.	3.5	77.9
100 E		
No	3.0	78.4
"	3.6	
"	3.8	
"	4.0	77.4
"	4.4	
"	4.7	
So	5.2	76.2

150 E

So.	4.8	76.6
"	4.1	
"	3.8	
"	3.4	78.0
"	3.2	
"	3.0	
No	2.5	78.9
200 E		
No.	1.7	79.7
"	2.3	
"	2.6	
"	2.9	78.5
"	3.2	
"	3.5	
So	4.0	76.4
250 E		
So.	3.6	77.8
"	2.9	
"	2.6	
"	2.3	79.1
"	1.7	
"	1.5	
No	1.4	80.2

81.41

300 E of Bayard

No			1.0		80.4
Ut			1.4		
4			1.7		
C			2.0		79.4
4			2.4		
Ut			2.6		
So			3.2		78.2
		350 E			
So			2.9		78.5
Ut			2.4		
4			2.1		
C			1.7		79.7
4			1.1		
Ut			0.8		
No			0.5		80.9
TP	8.02	89.13	0.30	81.11	
		400 E			
No			7.9		81.2
Ut			8.4		
4			8.7		
C			9.1		80.0
4			9.3		
Ut			9.4		
So			10.1		79.0

450 E

So			9.1		80.0
Ut			8.6		
4			8.5		
C			8.0		81.1
4			7.6		
Ut			7.3		
No			7.0		82.1
		500 E = W.L. Cass			
No			6.4		82.7
Ut			6.9		
4			7.1		
C			7.3		81.8
4			7.5		
Ut			7.8		
So			8.4		80.7
VPM	10.65	91.35	8.43	8070	80.70
		W.Ct.			
So			10.3 10.7 gutr.		81.1 80.7
Ut			9.7 10.3 "		
4			9.5 10.0 "		
C			9.3 9.7 "		82.1 81.7
4			9.1 9.5 "		
Ut			8.8 9.2 "		
No			8.5 8.8 "		82.9 82.6

91.35

N ⊥ Cass

N.	8.3	83.1
U	9.0	
⊥	9.3	
O	9.6	81.8
⊥	9.9	
U	10.1	
S.	10.5	80.9

CH

S.	9.8	81.6
U	9.2	
⊥	8.9	
C	8.1	82.6
⊥	8.5	
U	8.3	
N.	7.7	83.7

E ⊥

N.	7.9	83.5
U	8.5	
⊥	8.7	
O	8.9	82.5
⊥	9.1	
U	9.2	
S.	9.8	81.6

E. U.

S.	10.0 gutr 10.0	81.0 81.4
U	10.2 " 9.5	
⊥	9.6	
O	9.0	82.4
⊥	8.8	
U	9.3 gutr 8.4	
N.	8.4 " 7.8	83.0 83.6

E line Cass

N.	8.5	82.9
U	8.7 9.3	
⊥	8.6	
C	8.6	82.8
⊥	9.4	
U	10.0 9.5	
S.	9.9	81.5

S. E

S.	9.7	82.2
U	8.7 9.3	
⊥	8.2	
O	7.6	83.8
⊥	8.1	
U	8.6 7.9	
N.	7.4	84.0

91.35

100 E of Cass

No		6.2	85.2
U		{6.7 / 7.5	
4		7.1	
c		6.6	84.8
4		7.0	
U		{8.4 / 7.3	
So		8.1	82.3

150 E

So		7.1	83.3
U		{6.6 / 7.4	
4		6.2	
c		5.5	85.9
4		5.9	
U		{6.3 / 5.6	
No		5.2	86.2

200 E

No		4.1	87.3
U		{4.5 / 5.6	
4		4.8	
c		4.5	86.9
4		5.4	
U		6.4 / 5.7	
So		6.3	85.1

250 E

So		5.6	85.8
U		{4.9 / 6.1	
4		4.3	
c		3.7	87.7
4		4.2	
U		{4.6 / 3.6	
No		3.1	88.3

300 E

No		2.2	89.2
U		{2.6 / 3.4	
4		3.2	
c		2.7	88.7
4		3.8	
U		{5.4 / 4.4	
So		5.1	86.3

350 E

So		4.5	86.9
U		{4.1 / 4.8	
4		3.6	
c		2.7	88.7
4		3.0	
U		{3.0 / 2.6	
No		1.6	89.9

T.P. 11.00 101.05 ✓ 1.30 90.05 ✓

101.055

400 E of Cass

No	10.6	90.4
U	11.6 / 12.3	
H	12.2	
C	11.7	89.3
H	12.8	
U	13.9 / 13.3	
So	13.5	87.5

450 E

So	12.2 / 12.0 / 13.3	88.8
U		
H	11.6	
C	10.7	90.3
H	11.2 / 11.9 / 10.7	
U		
No	10.1	90.9

500 E: W.L. Dawes.

No	8.6 / 9.2 / 10.3	92.4
U		
H	8.9	
C	Nil	92.6
H	9.3 / 10.8 / 9.6	
U		
So	9.4	91.6

W. Cl.

So	Nil	92.6
U	8.2 / 9.0	
H	8.1	
C	7.7	93.3
H	8.1	
U	8.4 / 7.9	
No	7.6 / 7.9	93.4
		93.1

W½

No	7.0	94.0
U	7.5	
H	7.2	
C	7.2	93.8
H	7.5	
U	7.9	
So	7.8	93.2

ctr

So	7.3	93.7
U	7.4	
H	6.7	
C	6.4	94.6
H	6.4	
U	6.6	
No	6.2	94.8

101.05

E 4 Dawes.

No		6.1	94.9
Cl		6.7	
4		6.3	
c		6.5	94.5
4		6.9	
Cl		7.3	
So		7.4	93.6
	E Cl		
So		{7.6 gutter 6.9	93.4 94.1
Cl		{6.7 7.4 "	
4		6.6	
c		6.0	95.0
4		6.1	
Cl		{6.4 5.7	
No		{5.5 6.1	95.5 94.9
	E. line		
No		4.7	96.3
Cl		{5.2 6.3	
4		5.4	
c		4.6	96.4
4		5.7	
Cl		{7.0 6.2	
So		6.5	94.5
Bm		4.71	96.34 Hub N.E. Dawes

50 E

So		5.6	95.4
Cl		{5.2 6.1	
4		4.7	
c		3.6	97.4
4		4.1	
Cl		{4.7 3.7	
No		3.2	97.8
	100 E		
No		2.0	99.0
Cl		{2.6 3.6	
4		3.2	
c		2.7	98.3
4		3.5	
Cl		{3.2 3.9	
So		4.4	96.6
	150 E		
So		3.3	97.7
Cl		{2.9 4.1	
4		2.5	
c		1.8	99.2
4		2.1	
Cl		{2.9 2.0	
No		1.4	99.6
T.P. 11.52	111.18 200' E	1.39	99.66
No		10.0	101.2
Cl		{10.9 11.4	
4		11.2	
c		10.9	
4		11.7	100.3
Cl		{12.9 12.0	
So		12.4	98.8

111.18

	250 E of Dawes				400 E		
No		7.7	103.5	So		6.8	104.4
U		{8.5 9.6		U		{6.1 6.9	
4		9.0		4		5.4	
C		8.6	102.6	C		4.7	106.5
4		9.8		4		5.1	
U		{11.4 10.1		U		{5.5 4.6	
So		10.4	100.8	No		4.2	107.0
	300 E				450 E		
So		9.2	102.0	No		2.6	108.6
U		{8.3 9.2		U		{3.4 4.2	
4		7.8		4		3.8	
C		6.9	104.3	C		3.4	107.8
4		7.5		4		4.5	
U		{8.3 7.1		U		{5.8 5.0	
No		6.5	104.7	So		5.6	105.6
	350 E				500 E = W.L. Everts.		
No		5.4	105.8	So		3.5	107.7
U		{5.8 7.0		U		{3.3 4.1	
4		6.2		4		2.7	
C		6.0	105.2	C		1.9	109.3
4		7.1		4		2.4	
U		{8.4 7.3		U		{2.3 1.6	
So		8.0	103.2	No		1.0	110.2
				BM. 10.48	120.68	0.98	Hub N.W. Everts 110.20

120.68

W/a Events

No	9.9	110.8
U	11.0	
H	11.2	
C	11.5	109.2
H	11.8	
U	13.0 / 12.5	
So	13.0	107.7

W/L

So	12.9	107.8
U	12.3	
H	11.6	
C	11.4	109.3
H	10.9	
U	10.5	
No	9.7	111.0

Ctr

No	9.4	111.3
U	10.3	
H	10.9	
C	11.3	109.4
H	11.6	
U	12.2	
So	12.9	107.8

E/L

So	12.6	108.1
U	12.0	
H	11.6	
C	11.2	109.5
H	10.7	
U	10.3	
No	9.9	111.8

E Ct

No	9.6	112.1
U	9.9	
H	10.6	
C	11.0	109.7
H	11.5	
U	11.8	
So	12.4	108.3

E line

So	12.1	108.6
U	11.6	
H	11.1	
C	10.8	109.9
H	10.3	
U	9.8	
No	9.7	112.0

120.68

50 E of Everts

No	8.3	112.4
W	9.8	
4	10.3	
C	10.5	110.2
4	11.0	
W	11.3	
So	11.6	109.1

100 E

So	10.9	109.8
W	10.5	
4	10.3	
C	9.9	110.8
4	9.6	
W	9.2	
No	8.0	112.7

150 E

No	7.0	113.7
W	8.2	
4	8.5	
C	9.0	111.7
4	9.1	
W	9.4	
So	9.9	110.8

200 E

So	8.1	112.6
W	7.4	
4	7.2	
C	6.9	115.8
4	6.5	
W	6.1	
No	4.7	116.0

250 E

No	3.4	117.3
W	4.2	
4	4.7	
C	5.1	115.6
4	5.4	
W	5.8	
So	6.6	114.1

300 E

So	5.6	115.1
W	4.8	
4	4.5	
C	4.0	116.7
4	3.7	
W	3.4	
No	2.4	118.3

120.68

350 E. + Everts

No			1.3		119.4
U			2.0		
4			2.4		
C			2.9		117.8
4			3.2		
U			3.4		
So			3.9		116.8
T.P.	12.23	130.77	2.14	118.54	
	400 E				
So			12.5		118.3
U			11.9		
4			11.5		
C			11.3		119.5
4			11.0		
U			10.6		
No			9.5		121.3
	450 E				
No			8.2		122.6
U			8.9		
4			9.0		
C			9.4		121.4
4			9.9		
U			10.2		
So			10.6		120.2

500 E = W.L. Fenuel

So		9.3	121.5
U		8.6	
4		8.1	
C		7.8	123.0
4		7.6	
U		7.3	
No		6.6	124.2
	W a		
No		6.0	124.8
U		6.6	
4		6.7	
C		7.0	123.8
4		7.3	
U		7.8	
So		8.6	122.2
	W 4		
So		8.6	122.2
U		7.6	
4		7.2	
C		6.9	123.9
4		6.7	
U		6.4	
No		5.9	124.9

130.77

Ctr. Tunnel

N.	5.4	125.4
"	5.8	
"	6.2	
"	6.5	124.3
"	6.8	
"	7.2	
So	8.0	122.8
	E 4	
So	7.8	123.0
"	7.0	
"	6.6	
"	6.3	124.5
"	5.9	
"	5.5	
No	4.9	125.9
	E 8	
No	4.6	126.2
"	5.4	
"	5.8	
"	6.2	124.6
"	6.6	
"	7.0	
So	8.1	122.7

E line

So	7.7	123.1
"	6.7	
"	6.4	
"	6.0	124.8
"	5.7	
"	5.2	
No	4.6	126.2
	50 E	
"	3.6	127.2
"	4.0	
"	4.3	
"	5.2	125.6
"	5.7	
"	6.1	
So	7.0	123.8
	100 E	
So	6.3	124.5
"	5.5	
"	5.1	
"	4.6	126.2
"	4.2	
"	3.7	
No	[illegible]	128.3

130.77

150 E of Fenvel

No			2.3		128.5
U			3.2		
H			3.6		
C			4.1		126.7
H			4.5		
U			4.9		
So			5.8		125.0
		200 E			
So			5.3		125.5
U			4.5		
H			3.9		
C			3.6		127.2
H			3.2		
U			2.8		
No			1.9		128.9
		250 E			
No			1.4		129.4
U			2.3		
H			2.6		
C			3.2		127.6
H			3.6		
U			4.0		
So		✓	4.4		126.4
T.P.	8.11	136.28	2.60	128.17	

136.0

300 E

So	9.5	126.8
U	8.9	
H	8.1	
C	7.8	128.5
H	7.4	
U	7.2	
No	6.4	129.9
	350 E	
No	6.3	130.0
U	6.6	
H	7.0	
C	7.4	128.9
H	7.9	
U	8.3	
So	9.1	127.2
	400 E	
So	8.8	127.5
U	7.9	
H	7.4	
C	7.1	129.2
H	6.9	
U	6.6	
No	5.2	131.1

136.28

	450 E. of Kanvel		
No		5.4	130.9
Ct		6.4	
W		7.2	
C		7.7	128.6
W		7.6	
Ct		7.9	
So		8.8	127.5
	570 E. W. L. Gresham		
So		9.0	127.3
Ct		7.5	
W		7.3	
C		7.1	129.2
W		6.5	
Ct		6.0	
No		5.0	131.3
	W Ct		
No		5.1	131.2
Ct		6.0	
W		6.3	
C		6.8	129.5
W		7.2	
Ct		7.3	
So		9.0	127.3

	W W		
So		8.8	127.5
Ct		7.8	
W		7.4	
C		7.0	129.3
W		6.4	
Ct		6.1	
No		5.2	131.1
	Ctr	5	
No		5.1	131.2
Ct		6.1	
W		6.6	
C		7.0	129.3
W		7.4	
Ct		7.9	
So		8.5	127.8
	E W		
So		8.6	127.7
Ct		7.6	
W		7.1	
C		6.6	129.7
W		6.2	
Ct		5.9	
No		5.1	131.2

136.28

E Cl. Gresham

No	5.0	131.3
Cl	6.0	
H	6.2	
C	4.6	129.7
H	7.1	
Cl	2.6	
So	8.5	127.8

E. line

S.	8.6	127.7
Cl	7.7	
H	7.3	
C	6.8	129.5
H	6.3	
Cl	5.7	
No	4.6	131.7

50 E

No	3.9	132.4
Cl	5.1	
H	5.7	
C	6.2	130.1
H	6.8	
Cl	7.4	
So	8.2	128.1

100 E

S.	7.5	128.8
Cl	6.3	
H	6.0	
C	5.7	130.6
H	5.2	
Cl	4.6	
No	3.7	132.6

150 E

No	3.5	132.8
Cl	5.2	
H	5.4	
C	5.5	130.8
H	6.0	
Cl	6.5	
So	7.6	128.7

200 E

S.	7.7	128.6
Cl	6.9	
H	6.2	
C	5.6	130.7
H	5.1	
Cl	4.6	
No	3.8	132.5

136.28

250 E of Graham

N.	3.9	132.4	
"	4.8		
"	5.1		
C	5.6	130.7	
"	6.3		
"	6.7		
S. 3.	7.8	128.5	

300 E

S.	8.0	128.3	
"	7.0		
"	6.5		
C	6.2	130.1	
"	5.6		
"	5.2		
N.	4.4	131.9	

350 E

N.	5.0	131.3	
"	6.0		
"	6.3		
C	6.7	129.6	
"	7.2		
"	7.5		
S.	8.3	128.0	

POSTED

400 E

S.	8.3	128.0	
"	7.5		
"	7.0		
C	6.5	129.8	
"	6.2		
"	5.7		
N.	5.0	131.3	

135.02 4.48 131.80

450 E

N.	3.8	131.2	
"	4.5		
"	4.9		
C	5.5	129.5	
"	5.8		
"	6.2		
S.	6.9	128.1	

458'

S.	6.9	128.1	
"	6.2		
"	5.9		
C	5.6	129.4	
"	5.3		
"	4.8		
1' S. of N.V.	3.9		
N.	5.6	129.4	

POSTED

135.02

470 E. of Gresham

No	5.6	129.4	
5 So	5.5		
11 "	4.4		
Ch	4.3		
4	5.0		
C	5.7	129.3	
"	6.2		
4	6.7		
5 O	7.2	127.8	
477 E			
So	7.4	127.6	
4	6.3		
4	5.7		
C	5.2	129.8	
4	4.4		
6	4.0		
135. of N.L.	4.9		
12 " " "	9.7		
5 " " "	8.2		
4 " " "	4.4		
No	4.2	130.8	

530 E = W.L. Haines

No	4.1	130.9
15 So	4.6	
19 "	6.8	
Ch "	7.7	
4 So Ch	11.1	
6 " "	4.3	
4	4.3	
C	5.0	130.0
4	5.6	
Ch	6.2	
5 O	6.9	128.1
W. Ch		
5 O	6.8	128.2
4	5.9	
4	5.1	
C	4.9	130.1
1 N. Ch	10.2	
6 " "	11.2	
6 " "	7.4	
4	6.3	
3 No 4	4.6	
Ch	4.6	
No	4.4	130.6

135.02

W ¼ Corner

No	4.5	130.5
Ch.	4.5	
¼	4.6	
3' S. ¼	4.9	
4' " "	7.3	
8 " "	8.7	
Ctr.	11.9	123.1
2' S. Ch	11.8	
3 " "	4.8	
¼	5.3	
Ch.	6.0	
S.	6.7	128.3
Ctr		
S.	6.5	128.5
Ch.	6.2	
¼	4.8	
1' No ¼	11.2	
Ctr.	6.5	128.5
2' 1½ Ctr	5.1	
¼	4.7	
Ch.	4.6	
No.	4.5	130.5

E ¼

No.	4.1	130.6
Ch.	4.7	
¼	4.7	
C	4.7	130.3
5' S.	5.2	
8 "	8.8	
¼	11.8	
4' S.	11.4	
5 "	5.0	
Ch.	4.8	
S.	6.0	129.0
E Ch.		
S.	6.1	128.9
6' S. Ch.	5.1	
5 " "	9.1	
2 " "	9.7	
Ch.	12.0	
2' S. ¼	10.8	
¼	4.9	
Ctr.	4.8	130.2
¼	4.8	
Ch.	4.7	
No	4.8	130.2

		135.02			
	3 E Ch.				
No			4.9		130.1
Ch			4.7		
4			4.8		
c			4.8		130.2
4			4.9		
Ch.			5.7		
1' So. Ch.			12.1		
So			6.1 West 12.9 East		128.9 122.1
	6' W of E line				
So			9.2 W. 5.3 E		125.8 129.7
6' No.			5.2		
Ch.			5.0		
4			4.9		
c	POSTED		4.9		130.1
4			4.8		
Ch			4.8		
No.			4.7		130.3
	E line				
No.			4.7		130.3
Ch			4.9		
4			4.8		
c			4.9		130.1
4			4.8		
Ch			5.0		
So.			5.1		129.9
BM.			5.06	129.96	Hub S E Hamlet
T.P.	5.60	139.66	0.96	134.06	
			8.61	131.05	131.05

BM. Hub N. W. Bridge & Bergh

Cross Section of Pacific Ave. Cass to the Ocean.

Note - for elevations in block bet Cass & Bayard the elevations for curb & ⊕ line will have to be figured from " along property lines, as street was partly excavated before elevations were taken, figure for straight slope from one side to the other.

Elevations on property lines on Pacific Ave - Cass to Bayard.

	North Ground Ele.	South Ground Ele
W. line Cass	-1.8	-4.3
50' W "	0.0	-3.0
100"	2.7	-0.2
150"	3.9	0.7
200	4.1	2.4
250	4.8	3.0
300	4.9	3.4
350	4.6	3.9
400	3.9	3.9
450	3.5	3.3
500 " E.L. Bayard.	3.3	3.2
2.17	6.15	3.98

W.L. Bayard.

No	4.1	2.1
U	3.8	2.4
U	3.8	2.4
C	3.8	2.4
U	3.8	2.4
U	3.8	2.4
So	4.1	2.1

50' W

So	4.3	1.9
U	4.4	1.8
U	4.4	1.8
C	4.3	1.9
U	4.5	1.7
U	4.4	1.8
No	4.8	1.4

100' W

N.	6.3	0.6
U	5.3	0.9
U	5.4	0.8
C	5.0	1.2
U	5.0	1.2
U	5.2	1.0
So	5.2	1.0

150' W

So	6.3	-0.1
U	6.4	0.0
U	6.2	0.0
C	5.9	0.3
U	6.4	0.0
U	5.8	0.4
No	5.9	0.3

Note Pacific Ave is 60' wide north 12' sidewalks from Cass to Allison, from Allison to Ocean is 100' wide north 20' sidewalks. Allison is 120' wide. See diagram P55

POSTED
POSTED

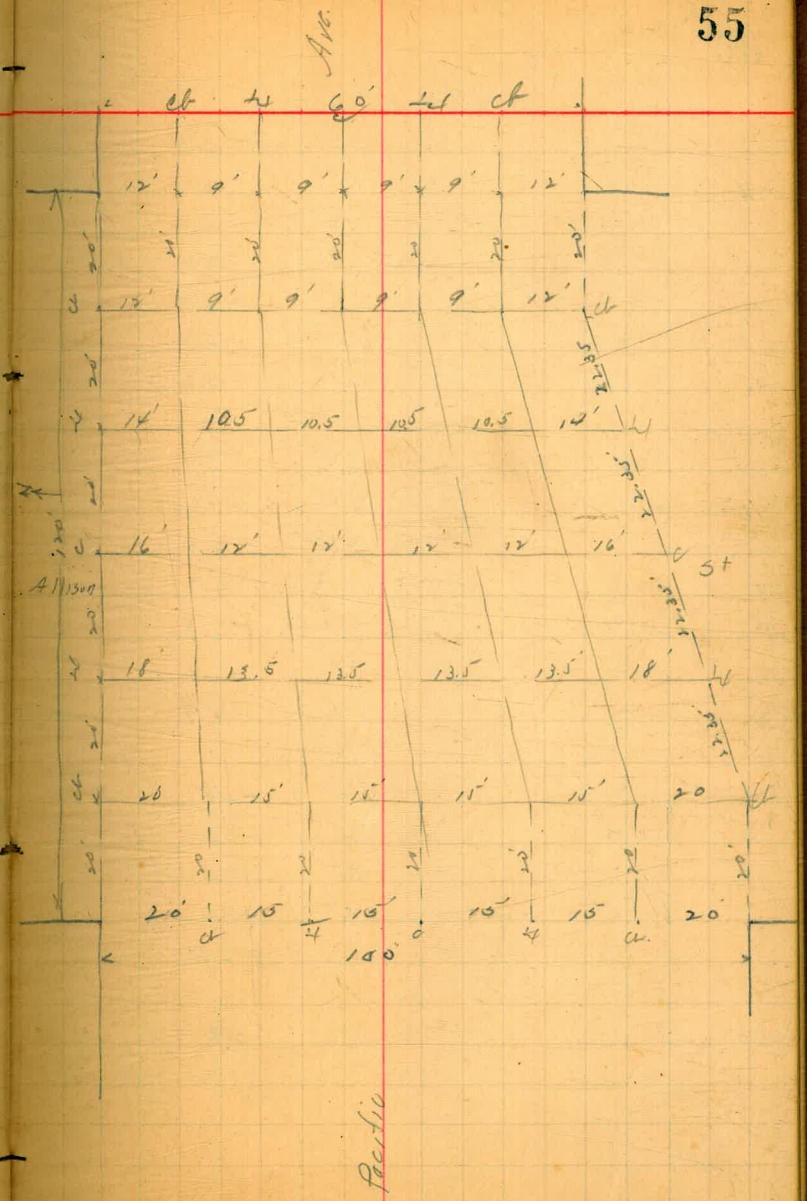
		6.15		
		200 W. of Bayard		
No			6.4	−0.2
"			6.4	−0.2
"			6.8	−0.6
C			6.4	−0.2
"			6.6	−0.4
"			6.7	−0.5
So			7.0	−0.8
		250 W		
S.			7.4	−1.2
"			7.4	−1.2
"			7.4	−1.2
C			7.1	−0.9
"			7.3	−1.1
"			6.8	−0.6
No			6.8	−0.6
		300 W		
N.			7.3	−1.1
"			7.7	−1.5
"			7.8	−1.6
C			7.8	−1.6
"			7.5	−1.3
"			7.5	−1.3
So			7.6	−1.4
T.R	1.34	1.81	5.68	0.47

	350 W	
S.	4.0	−2.2
"	3.9	−2.1
"	3.6	−1.8
C	4.2	−2.4
"	4.0	−2.2
"	3.9	−2.1
N.	3.7	−1.9
	400 W	
No	4.4	−2.6
"	4.5	−2.7
"	4.5	−2.7
C	4.5	−2.7
"	4.4	−2.6
"	4.4	−2.6
So	4.4	−2.6
	460 W. E. of Altura	
S.	5.2	−3.4
"	5.0	−3.2
"	5.2	−3.4
C	5.4	−3.6
"	5.5	−3.7
"	5.6	−3.8
N.	5.7	−3.9

1.81

E. ch Allison

N.	6.5	−4.7	
"	5.8	−4.0	
"	6.0	−4.2	
"	6.2	−4.4	
"	6.0	−4.2	
"	6.0	−4.2	
S.	6.0	−4.2	
	E ch		
S.	6.6	−4.8	
"	6.6	−4.8	
"	6.6	−4.8	
"	6.6	−4.8	
"	6.8	−5.0	
"	5.9	−4.1	
N.	6.6	.48	
	ch		
N.	6.5	−4.7	
"	6.4	−4.6	
"	6.7	−4.9	
"	7.0	−5.2	
S.	6.8	−5.0	
"	6.8	−5.0	
S.	6.9	−5.1	



1.81

	W^d Allison		
So		6.4	-4.6
U		6.7	-4.9
L		6.4	-4.6
C		6.6	-4.8
L		6.7	-4.9
U		6.8	-5.0
No		6.1	-4.3
	W Cu.		
No		5.5	-3.7
U		5.4	-3.6
L		6.4	-4.6
C		6.7	-4.9
L		6.7	-4.9
U		7.0	-5.2
So		6.7	-4.9
	W line Allison		
So		6.6	-4.8
1 So		6.3	-4.5
U		5.4	-3.6
L		5.1	-3.3
C		4.8	-3.0
L		4.6	-2.8
U		4.9	-3.1
No		4.7	-2.9

	15 W of Allison		
	East	6.3	-4.5
	West	5.5	-3.7
So		4.7	-2.9
U		4.7	-2.9
L		4.6	-2.8
C		4.6	-2.8
L		4.6	-2.8
U		4.7	-2.9
No			
	50 W		
No		4.2	-2.4
U		4.6	-2.8
L		4.4	-2.6
C		4.4	-2.6
L		4.3	-2.5
U		4.4	-2.6
So		4.5	-2.7
	100 W		
So		3.8	-2.0
U		3.8	-2.0
L		4.0	-2.2
C		4.0	-2.2
L		4.0	-2.2
U		3.5	-1.7
No		3.3	-1.5
T.P.	9.74 10.77	0.78	1.03

		10.77						
		150 W				800 W		
N.			10.6	0.2		S.	6.1	4.7
U			10.7	0.1		U	6.3	4.5
4			11.0	−0.2		4	6.5	4.3
C			11.2	−0.4		C	6.2	4.6
4			11.2	−0.4		4	6.3	4.5
U			11.5	−0.7		U	6.0	4.8
So			11.5	−0.7		No	6.0	4.8
		200 W				325 W		
So			9.8	1.0		N.	4.1	6.7
U			9.5	1.3		U	3.1	7.7
4			9.8	1.0		4	4.1	6.7
C			9.6	1.2		C	3.1	7.7
4			9.4	1.4		4	4.1	6.7
U			8.9	2.1		U	5.2	5.6
No			9.1	1.7		So	4.3	6.5
		250 W				350' W on North & 360' W on South Sides Ocean.		
N.			7.9	2.9		So	3.7	7.1
U			7.9	2.9		U	4.0	6.8
4			7.8	3.0		4	3.6	7.2
C			8.0	2.8		C	4.1	6.7
4			8.2	2.6		4	4.1	6.7
U			8.1	2.7		U.	25	8.3
So			8.1	2.7		S No U	1.9	8.9
						B " "	4.8	6.0
						No	3.2	7.6

POSTED

Cross - Section of Reed St - Bayard to Dawes for Scripps.

10/9/07 { Clam / Emery / Collett

	6.37	12.20		5.83 mm.	
		E.L. Bayard			
S.			7.2		5.0
U			6.9		5.3
H			6.8		
C			7.1		5.1
H			6.9		
U			7.0		
N.			6.8		5.4
		50 E			
N.			6.1		6.1
U			6.2		
H			6.1		
C			6.4		5.8
H			6.4		
U			6.4		
S.			6.5		5.7
		100 E			
S.			5.9		6.3
U			6.0		
H			5.9		
C			5.9		6.3
H			5.8		
U			5.7		
N.			5.7		6.5

	150 E		
N.		5.2	7.0
U		5.4	
H		5.2	
C		5.4	6.8
H		5.4	
U		5.5	
S.		5.7	6.5
	200 E		
S.		5.4	6.8
U		5.3	
H		5.2	
C		5.2	7.0
H		4.9	
U		4.7	
N.		5.1	7.1
	250 E		
N.		4.5	7.7
U		4.6	
H		4.5	
C		4.8	7.4
H		4.9	
U		5.0	
S.		5.1	7.1

12.20

300 E

S.			4.8		7.4
U			4.7		
4			4.5		
C			4.4		7.8
4			4.2		
U			4.1		
N.			4.1		8.1

350 E

N.			3.7		8.5
U			3.8		
4			4.1		
C			3.7		8.5
4			4.1		
U			4.1		
S.			4.3		7.9

400 E

S.			4.0		8.2
U			4.2		
4			4.0		
C			3.6		8.6
4			4.0		
U			3.6		
N.			3.5		8.7

450 E

N.			3.5		8.7
U			3.6		
4			3.8		
C			3.7		8.5
4			3.9		
U			3.8		
S.			4.1		8.1

500 E = W.L Cass

S.			4.0		8.2
U			3.8		
4			3.7		
C			3.5		8.7
4			3.5		
U			3.4		
N.			3.4		8.8
TP 6.58		14.75	4.03		8.17
		1x1 ch			
N.			58		9.0
			6.1 gutr		8.7
U			60	"	
			64	"	
4			59		
			64	"	
C			61		8.7
			67	"	8.1
4			63		
			69	"	
U			6.4		
			70	"	
S.			6.5		8.3
			72	"	7.6

14.75

W ¼ Cass.

S.	6.4	8.4
U	6.2	
4	5.8	
c	5.6	9.2
4	5.4	
U	5.6	
N.	5.5	9.3

Ctr.

N.	5.5	9.3
U	5.5	
4	5.4	
c	5.5	9.3
4	5.6	
U	5.8	
S.	5.8	9.0

E ¼

S.	6.4	8.4
U	6.4	
4	6.2	
c	6.0	8.8
4	6.1	
U	5.9	
N.	5.7	9.1

E Cl.

N.	6.7 gub 5.5	8.7 9.3
U	6.3 " 5.9 "	
4	6.4 " 5.9	
c	6.7 " 5.8	8.4 9.0
4	6.4 " 6.1	
U	6.6 " 6.1	
S.	6.8 " 6.1	8.0 8.7

E. line Cass

S.	6.2	8.6
U	6.0	
4	6.0	
c	5.7	9.1
4	5.8	
U	5.7	
N.	5.1	9.7

50 E

N.	4.7	10.1
U	5.3	
4	5.5	
c	5.4	9.4
4	5.4	
U	5.3	
S.	5.5	9.3

		14.75			
		100 E of Cass			
5.			5.1		9.7
4			4.9		
4			4.6		
4			4.8		10.0
4			4.7		
4			4.6		
16			4.0		10.8
		150 E			
No			4.1		10.7
4			4.3		10.5
4			4.2		10.6
4			4.0		10.8
4			4.2		10.6
4			4.8		10.0
50			5.2		9.6
TP	4.05	15.16	3.64	11.11	
		200 E			
5.			5.6		9.6
4			5.0		
4			4.8		
4			4.6		10.6
4			4.5		
4			4.5		
No			3.8		11.4

		15.2		
	250 E			
No		3.9		11.3
4		4.8		
4		5.0		
4		5.0		10.2
4		5.1		
4		5.2		
50		5.8		9.4
	300 E			
50		6.8		8.4
4		6.4		
4		6.2		
4		5.9		9.3
4		5.5		
4		5.2		
No		4.5		10.7
T.P. 4.76	13.97	5.95	9.21	
	350 E			
No		4.5		9.5
4		5.2		
4		5.5		
4		5.7		8.3
4		5.8		
4		6.1		
50		6.3		7.7

13-97

400 E of Cross

S.	5.6	8.4
W	5.5	
4	5.1	
C	5.1	8.9
4	5.0	
W	5.2	
No	4.2	9.8

450 E

S.	4.0	10.0
W	4.3	
4	4.5	
C	4.7	9.3
4	4.7	
W	5.0	
So	5.5	8.5

500 E. W.L. Davies

S.	4.9	9.1
W	4.5	
4	4.2	
C	4.2	9.8
4	4.0	
W	4.0	
No	3.5	10.5

Cross Section of Beryl St. Kendall to Morell

6 / 2 / 0 { Davis / Donnan / Colbath

	9.32	H.1 170.40		B.M. Hub 10 E.S.E. Cor Beryl 161.08	
		W.L. Lamont			
So			8.7	161.7	
cb			6.6		
1/4			6.2		
C			5.6	164.8	
+4			5.8		
+6			8.0		
1/4			8.0		
+9			7.8		
cb			5.6		
No			4.2	166.2	
		50' W. Lamont			
No			3.4	167.0	
cb			5.0		
1/4			5.3		
C			4.4	166.2	
1/4			5.0		
cb			5.5		
So			7.0	163.4	
		100' W			
So			7.5	162.9	
cb			6.1		
1/4			5.6		
C			4.6	165.8	
1/4			5.2		
cb			5.0		
No			1.8	168.6	

	150' W	
No	6.6	163.8
+4	7.2	
+8	5.3	
+15	5.7	
cb	7.1	
1/4	8.5	
C	8.3	162.1
1/4	8.5	
cb	8.5	
So	7.7	162.7
	163' W	
So	10.5	159.9
cb	10.1	
	200' W	
So	12.5	157.9
cb	11.1	
1/4	10.7	
C	10.3	160.1
1/4	9.6	
cb	9.3	
+5	6.5	
+12	6.3	
+17	7.9	
No	7.9	162.5

Beryl St

HS
170.40

250 W of Lamont

No			5.8	164.6
Ct			7.0	
¼			7.6	
C			8.1	162.3
¼			9.0	
Ct			9.5	
So			11.4	159.0
T.P.	11.81	175.25	6.96	163.44
		300 W		
So			13.3	162.0
Ct			11.4	
¼			11.0	
C			10.3	165.0
¼			9.4	
Ct			8.8	
No			6.6	168.7
		350 W		
No			4.1	171.2
Ct			6.3	
¼			7.1	
C			8.3	167.0
¼			9.1	
Ct			9.5	
So			11.4	163.9

400 W

So	9.9	165.4
Ct	7.8	
¼	7.3	
C	6.2	169.1
¼	4.9	
Ct	3.9	
No	1.9	173.4

450 W

No	0.5	174.8
Ct	2.2	
¼	3.3	
	3.7	
C	4.5	170.8
¼	5.2	
Ct	5.9	
So	8.0	167.3

500 W = E. line Kendall

So	8.5	166.8
Ct	6.2	
¼	5.1	
C	4.2	171.1
¼	3.1	
Ct	1.7	
No	+0.4	175.30

Beryl St

E. line Lamont

	7.60	168.68	BM	161.08
So		6.9	161.8	
cl		6.1	162.6	
¼		5.5	163.2	
C		5.0	163.7	
¼		4.7	164.0	
cl		4.1	164.6	
+10		3.0	165.7	
No		1.4	167.3	
	50 E			
No		1.6	167.1	
+10		4.9	163.8	
+16		5.3	163.4	
cl		4.5	164.2	
¼		5.4	163.3	
C		6.7	162.0	
¼		7.7	161.0	
cl		7.9	160.8	
So		9.1	159.6	
	100 E			
So		10.9	157.8	
cl		8.8	159.9	
¼		9.0	159.7	
C		8.4	160.3	
¼		7.9	160.8	
cl		7.2	161.5	
No		4.7	164.0	

	150 E	
No	5.4	163.3
cl	7.2	161.5
¼	8.4	160.3
C	9.3	159.4
¼	9.7	159.0
cl	9.4	159.3
So	11.6	157.1
	200 E	
So	11.3	157.4
cl	9.5	159.2
¼	9.5	159.2
C	9.0	159.7
¼	8.1	160.6
cl	7.5	161.2
No	5.7	163.0
	250 E	
No	6.2	162.5
cl	7.6	161.1
¼	7.8	160.9
C	8.1	160.6
¼	8.4	160.3
cl	9.1	159.6
So	10.1	158.6

Beryl St.

168.68

		300' E			
So			11.2		157.5
cl			10.4		
¼			9.6		
c			9.3		158.4
¼			8.5		
cl			7.9		
No			7.0		161.7
		350' E			
No			7.8		160.9
cl			9.5		
¼			10.2		
c			11.1		157.6
¼			11.8		
cl			12.5		
So			13.8		154.9
T.P.	3.91	161.31	11.28	157.40	
		400' E			
So			8.0		153.3
cl			6.4		
¼			5.7		
c			4.3		157.0
¼			2.9		
cl			2.3		
No			1.0		160.3

	450' E		
No		3.8	157.5
cl		5.7	
¼		6.1	
c		7.1	154.2
¼		7.6	
¼		7.9	
¼		9.0	
cl		8.8	
So		10.3	157.0
	500' E = W.L. Morell		
So		12.7	148.6
cl		11.8	
¼		10.5	
c		9.6	157.7
¼		8.6	
cl		7.9	
No		6.2	155.1

Cross Section of E ½ of 27th St
Market S to SL of Alley

60' wide
10' cbs

SEBP	275	144.86		1421	I St & 27th
TP	1.07	133.70	12.23	132.63	
S.L. Market=00			1337		
E			4.9	1288	✓
cb			5.3	1284	✓
1/4			5.5	1282	✓
e			6.1	1276	✓
0+5					
C			6.4	1273	✓
1/4			5.7	1280	✓
cb			4.7	1290	✓
E			4.2	1295	✓
0+20					
E			6.2	1275	✓
cb			6.2	1275	✓
1/4			6.7	1270	✓
C			6.0	1277	✓
0+30					
C			6.2	1275	✓
+5			6.9	1268	✓
1/4			9.6	1241	✓
cb			10.1	1236	✓
E			9.0	1247	✓
+5			7.9	1258	✓
T.P.	4.77	126.71	11.76	121.94	
0+42			1267		
-10			6.9	1198	✓
E			7.7	1190	✓

Moore
12/15/26

126.71

	1267		
cb	7.9	1188	✓
+5	8.0	1187	✓
1/4	5.8	1209	✓
C	0.0	1267	✓
0+55			
C	2.4	1243	✓
1/4	8.6	1181	✓
+5	11.6	1151	✓
cb	11.8	1149	✓
E	12.0	1147	✓
+10	12.4	1143	✓
+15	9.7	1170	✓
0+85			
-25	18.4	1083	✓
E	14.8	1119	✓
cb	13.0	1137	✓
1/4	8.9	1178	✓
C	1.9	1248	✓
1+03			
C	1.6	1251	✓
1/4	2.8	1239	✓
+2	3.8	1229	✓
cb	10.0	1167	✓
E	13.6	1131	✓
+25	17.0	1097	✓
1+11			
-25	17.6	1091	✓
-11	15.2	1115	✓
E	9.5	1172	✓

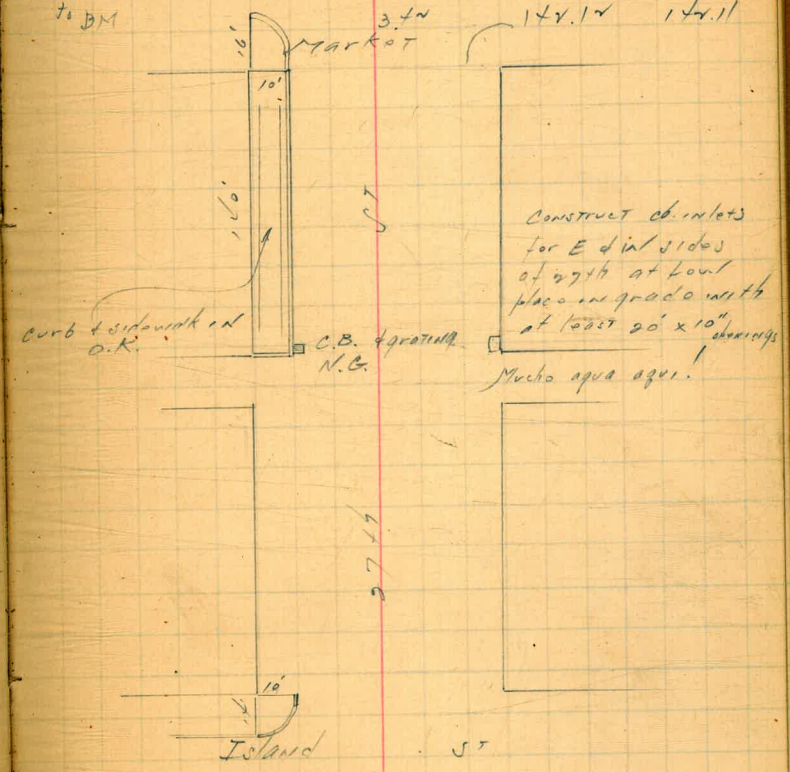
1267

1267

cb	4.5	1222 ✓
+4	2.5	1242 ✓
1/4	2.3	1244 ✓
c	1.7	1250 ✓
1+25		
c	1.6	1251 ✓
1/4	1.9	1248 ✓
cb	2.1	1246
+3	2.7	1240
E	6.8	1199
+17	16.8	1099
+25	17.6	1091
1+40		
−25	17.0	1097
−17	15.4	1113
E	5.8	1209
+4	2.7	1240
cb	1.7	1250
1/4	1.4	1253
c	1.2	1255
1+60 = st alley		
c	0.9	1258
1/4	1.2	1255
cb	1.3	1254
+9	1.1	1256
E	1.8	1249
+27	19.0	1077
+30	19.1	1076

1267

T.P.	11.59	137.36	0.94	125.77
check to BM	8.25	145.54	0.07	137.29
			3.42	142.12	142.11



NB
14' cbs north of Market

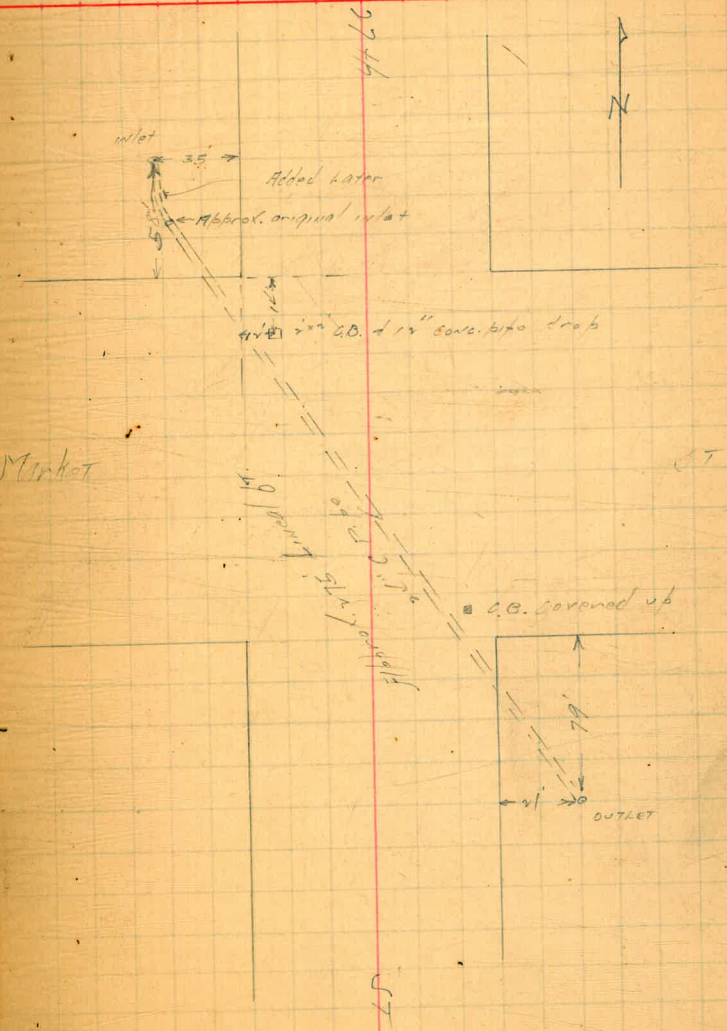
Location & Elev. of Culvert at 27th & Market

Moore 1/19/27

S.E.B.P.	1.03	143.14		142.11	27th & Ist
T.P.	5.46	135.62	12.95	130.16	
NEBP set			4.56	131.06	27th & Market
T.P.	9.55	132.02	13.15	122.47	
flowline of inlet			18.90	113.1 ✓	
T.P.	22.7	121.58	12.71	119.31	
flowline of outlet			16.03	105.6 ✓	

132.0
18.9
113.1

121.6
16.0
105.6



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City Hall, San Diego, Cal.

131.05 - Hub. N.W. cor Bwdy and Berry

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City Hall, San Diego, Cal.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

For Single Track Embankment.

Roadway 14 feet wide. Side Slopes $1\frac{1}{2}$ to 1.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	27
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

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