Return to City Engineers Office
City Hall, San Diego, Cal.

TRANSIT

398

F.B. 321

TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100

321

Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100.00	0.44	100.00	0.87	99.99	1.31	89
1	99.98	1.75	99.98	2.18	99.97	2.62	99.95	3.05	88
2	99.94	3.49	99.92	3.93	99.91	4.36	99.88	4.80	87
3	99.86	5.23	99.84	5.67	99.81	6.10	99.79	6.54	86
4	99.76	6.98	99.73	7.41	99.69	7.85	99.66	8.28	85
5	99.62	8.72	99.58	9.15	99.54	9.58	99.50	10.02	84
6	99.45	10.45	99.41	10.89	99.36	11.32	99.31	11.75	83
7	99.25	12.19	99.20	12.62	99.14	13.05	99.09	13.49	82
8	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	15.64	98.70	16.07	98.63	16.50	98.56	16.93	80
10	98.48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98.16	19.08	98.08	19.51	97.99	19.94	97.90	20.36	78
12	97.81	20.79	97.72	21.22	97.63	21.64	97.53	22.07	77
13	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	24.19	96.92	24.62	96.81	25.04	96.70	25.46	75
15	96.59	25.88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.82	73
17	95.63	29.24	95.50	29.65	95.37	30.07	95.24	30.49	72
18	95.11	30.90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35.43	69
21	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38.67	67
23	92.05	39.07	91.88	39.47	91.71	39.87	91.53	40.27	66
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	43.84	89.69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	46.95	88.09	47.33	87.88	47.72	87.67	48.10	61
29	87.46	48.48	87.25	48.86	87.04	49.24	86.82	49.62	60
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	52.99	84.57	53.36	84.34	53.73	84.10	54.10	57
33	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	52
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	45
45	70.71	70.71							
Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees
	DEGREES		¾ DEGREE.		½ DEGREE.		¼ DEGREE.		

Published by H. S. Crocker Company, Stationers, Drawing Materials, Mathematical Instruments, etc., San Francisco.

MICROFILMED
DEC 1964

Return to City Engineers Office
City Hall, San Diego, Cal.

Crocker Quality

TRANSIT BOOK

No._____

MANUFACTURED BY

H. S. CROCKER CO.

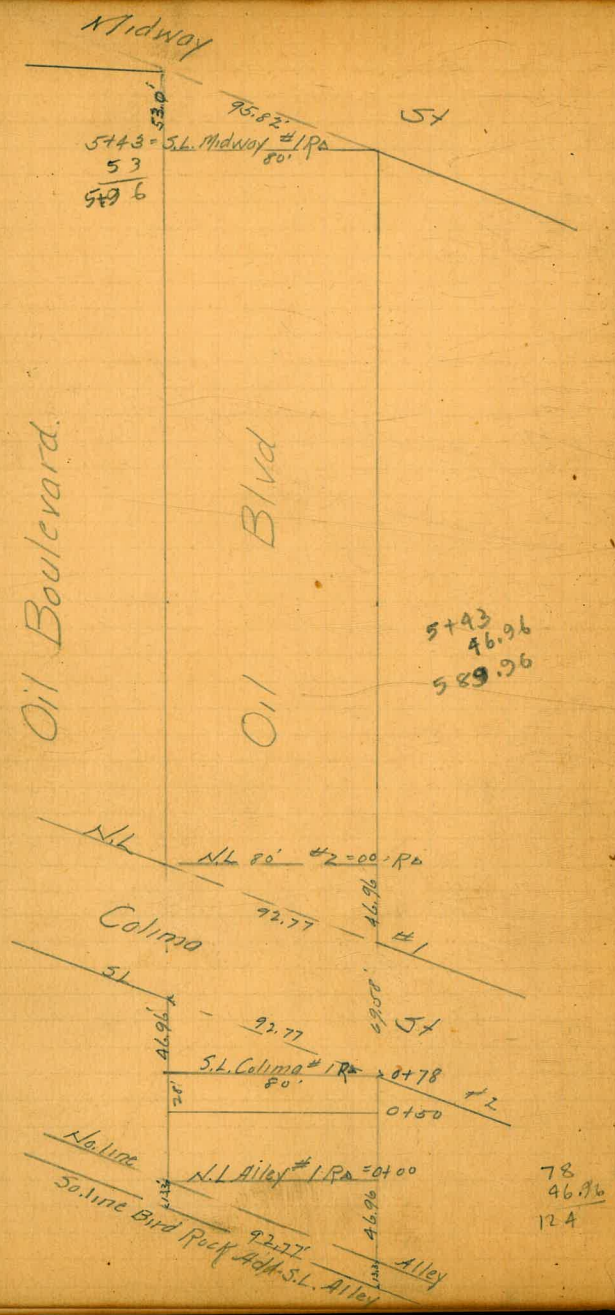
SAN FRANCISCO AND SACRAMENTO
CALIFORNIA

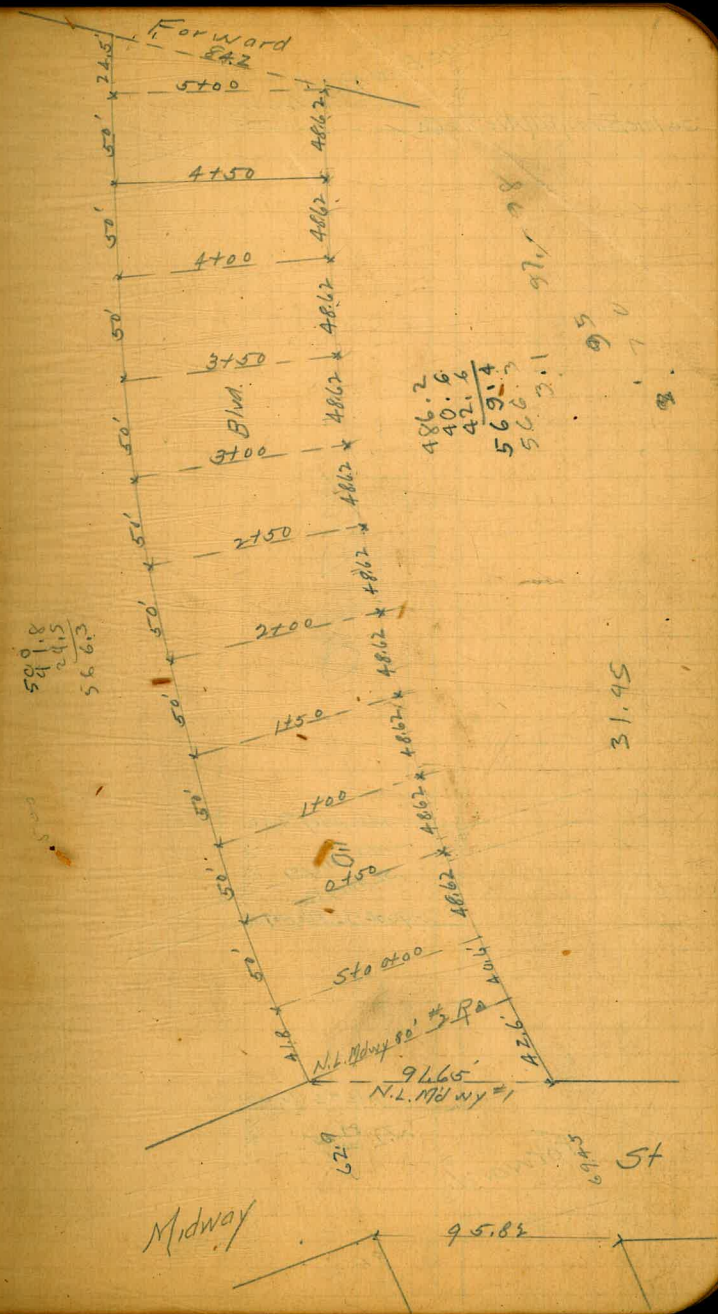
LORING & CO., AGENTS.
762 FIFTH STREET,
SAN DIEGO, CALIFORNIA

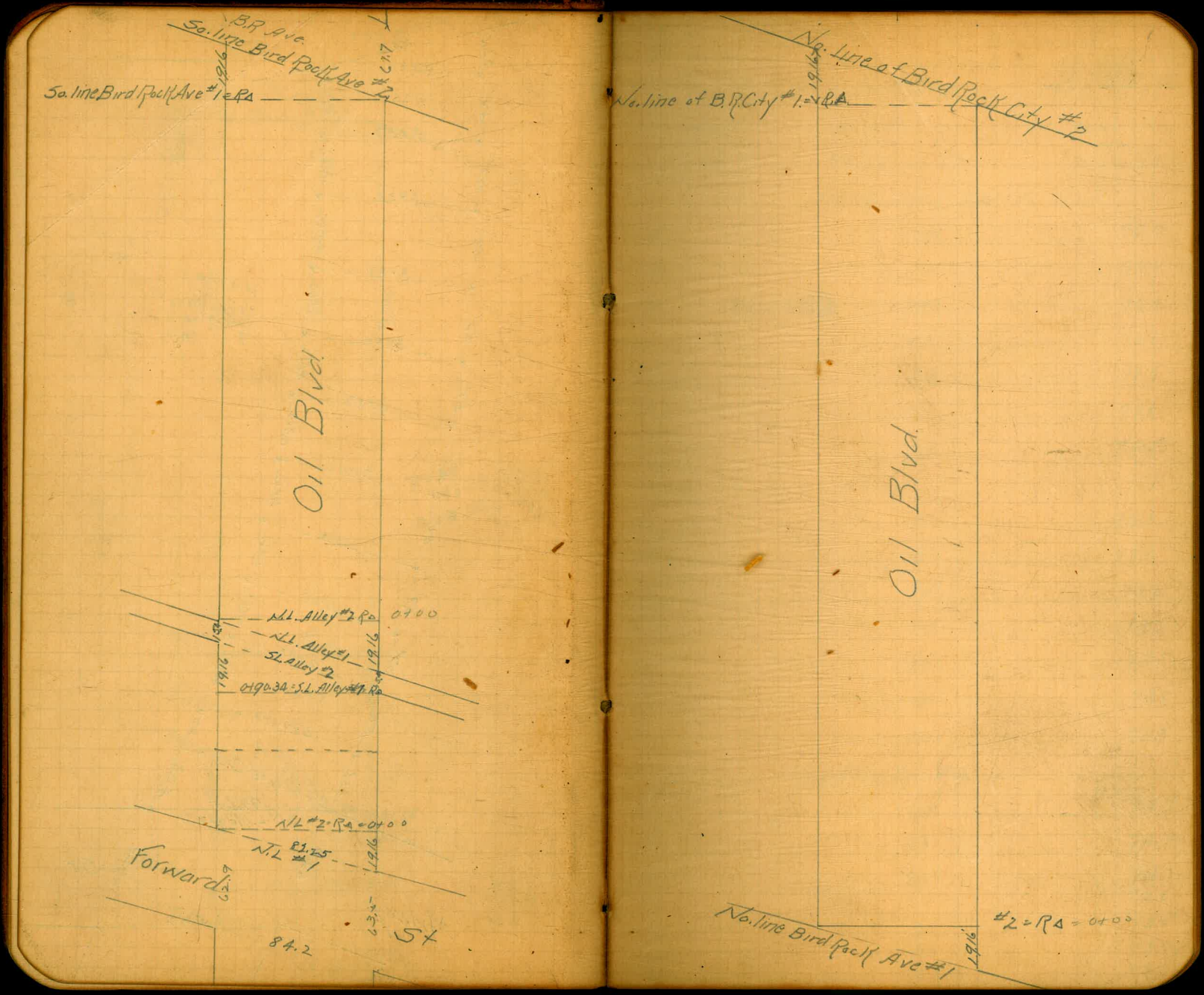
— Index —

Xsec Oil Blvd. entire length.	1
X sec Hodgman Bellevt.	14
X sec Colima	29
X sec Colima – Oil Blvd – Sun Ave	36
X-sec Midway Oil Blvd – West end	52
X sec Midway Oil Blvd – Sun	59

Sketch showing method of cross-sectioning






B.R Ave.
So. line Bird Rock Ave #1
So. line Bird Rock Ave #1 = R.A
Oil Blvd
N.L. Alley #2 R.A 0400
N.L. Alley #1
S.L. Alley #2
0490.34 = S.L. Alley #1 R.A
N.L #2 · R.A = 0400
N.L #1
Forward
84.2
St
No. Line of Bird Rock City #2
No. line of B.R. City #1 = R.A
Oil Blvd.
#2 = R.A = 0400
No. line Bird Rock Ave #1

Cross- Section of Oil Boulevard
from So. line of Bird Rock Add to 12/18/07 { Davis Donnan Collatt
No. line of Bird Rock City.

6.67	81.67		75.00
			Midway
11.16	81.16	11.67	7000 B.M.

S.L. Bird Rock Add = S.L. Alley

E	7.5	73.7
ct	7.6	73.6
1/4	7.8	73.4
c	8.1	73.1
1/4	8.3	72.9
ct	8.6	72.6
W	8.7	72.5

POSTED

N.L. Alley

W	8.1	73.1
ct	8.1	73.1
1/4	8.0	73.2
c	7.9	73.3
1/4	7.7	73.5
ct	7.4	73.8
E	7.3	73.9

N.L. Alley #1 = R△

E	6.5	74.7
ct	6.8	74.4
1/4	7.1	74.1
c	7.6	73.6
1/4	7.7	73.5
ct	8.0	73.2
W	8.1	73.1

8.1.16

N.L. Alley #2 (+50)

W	6.7	74.5
Ct	6.1	75.1
½	6.1	75.1
C	6.1	75.1
W	5.8	75.4
Ct	5.5	75.7
E	5.6	75.7

Alley #2 (+78) S.L. Colima #1

E	4.8	76.4
Ct	5.0	76.2
½	5.1	76.1
C	5.1	76.1
½	5.4	75.8
Ct	5.1	76.1
W	5.6	75.6

S.L. Colima #2

W	3.9	77.3
Ct	4.0	77.2
½	4.2	77.0
C	4.2	77.0
½	4.5	76.7
Ct	4.8	76.4
E	4.7	76.5

Oil Blvd.

8.1.16

No. line Colima #1

E	2.4	78.8
Ct	2.0	79.2
½	1.9	79.3
C	1.8	79.4
½	1.6	79.6
Ct	1.2	80.0
W	1.8	79.4
	1.78	B.M. Colima 79.38

POSTED

No. line Colima #2

W	1.8	79.4
Ct	1.0	80.2
½	1.2	80.0
C	1.3	79.9
½	1.0	80.2
Ct	0.8	80.4
E	1.1	80.1

50' No Col #2

E	1.3	79.9
Ct	1.3	79.9
½	1.0	80.2
C	1.5	79.7
½	1.4	79.8
Ct	1.5	79.7
W	1.8	79.4

8/1/16

100' No. Colima St

W	2.6	78.6
Ct	2.5	78.7
½	2.2	79.0
C	2.6	78.7
½	2.2	79.0
Ct	2.7	78.5
E	2.7	78.5

150' No.

E	3.7	77.5
Ct	3.7	77.5
½	3.7	77.5
C	3.7	77.5
¼	3.2	78.0
Ct	3.3	77.9
W	3.7	77.5

200' No.

W	4.7	76.5
Ct	4.7	76.5
½	4.7	76.5
C	4.6	76.6
¼	4.6	76.6
Ct	4.4	76.8
E	4.3	76.9

Oil Blvd. 8/1/16

250' No. of Colima St

E	4.9	76.3
Ct	5.0	76.2
½	5.0	76.2
C	5.3	75.9
¼	5.2	76.0
Ct	5.5	75.7
W	5.7	75.5

300' No.

W	6.3	74.9
Ct	6.2	75.0
½	5.9	75.3
C	6.0	75.2
¼	5.8	75.6
Ct	5.7	75.5
E	5.5	75.7

350' No.

E	6.5	74.7
Ct	6.8	74.4
½	7.1	74.1
C	7.5	73.7
¼	7.4	73.8
Ct	7.5	73.7
W	7.8	73.4

81.16

400' No. of Colima #2

W	9.0	72.2
Ct	8.9	72.3
½	8.5	72.7
C	8.6	72.7
½	7.7	73.5
Ct	7.7	73.5
E	7.3	73.9

450' No

E	8.3	72.9
Ct	8.5	72.7
½	8.6	72.6
C	9.2	72.0
½	9.4	71.8
Ct	10.0	71.2
W	10.4	70.8

500' No

W	11.6	69.6
Ct	11.3	69.9
½	10.9	70.3
C	10.8	70.4
½	9.9	71.3
Ct	9.7	71.5
E	9.3	71.9

01 Blvd

543' No of Colima #2 - St. Midway #1 Rd

E	9.9	71.3
Ct	10.5	70.7
½	10.6	70.6
C	11.9	69.3
½	12.0	69.2
Ct	13.0	68.2
W	13.4	67.8
TP 7.37	77.37	11.16 — 70.00

St. Midway #2

W	10.5	66.9
Ct	9.7	67.7
½	8.8	68.6
C	8.3	69.1
½	7.1	70.3
Ct	6.8	70.6
E	6.1	71.3

N.L. Midway #1

E	6.5	70.9
Ct	7.2	70.2
½	7.6	69.8
C	8.5	68.9
½	8.7	68.7
Ct	9.5	67.9
W	10.3	67.1

77.37

N.L. Midway #1 - P.I.

W	10.3	67.1
Ct	9.4	68.0
½	8.6	68.8
C	8.1	69.3
½	7.7	69.7
Ct	6.7	70.7
E	6.1	71.3

N.L #2 + 40.6 on E and 41.8 on W = 0.0

E	4.9	72.5
Ct	5.6	71.8
½	5.8	71.6
C	7.6	69.8
½	7.8	69.6
Ct	8.7	68.7
W.	9.9	67.5

0+50 on W. side = 0+48.62 on E side { Stations are from stored from W. Side

W	8.9	68.5
Ct	8.3	69.1
½	7.3	70.1
C	6.8	70.6
½	6.0	71.4
Ct	5.4	72.0
E	4.7	72.7

Oil Blvd.

77.37

4

1+00

E	3.5	73.9
Ct	4.3	73.1
½	4.7	72.7
C	5.8	71.6
½	5.9	71.5
Ct	6.4	71.0
W	7.1	70.3

1+50

W	5.8	71.6
Ct	5.2	72.2
½	4.8	72.6
C	4.7	72.7
½	4.0	73.4
Ct	3.3	74.1
E	2.8	74.6

2+00

E	2.0	75.4
Ct	2.8	74.6
½	2.9	74.5
C	3.9	73.5
½	4.1	73.3
Ct	4.2	73.2
W	4.9	72.5

77.37

2+50

W	4.1	73.3
CL	3.7	73.7
½	3.5	73.9
C	3.3	74.1
¼	2.3	75.1
CL	2.0	75.4
E	1.6	75.8

3+00

E	1.5	75.9
CL	1.9	75.5
¼	2.3	75.1
C	2.8	74.6
¼	3.2	74.2
CL	3.4	74.0
W	3.9	73.5

3+50

W	3.6	738
CL	3.0	74.4
½	2.7	74.7
C	2.1	75.3
¼	1.9	75.5
CL	1.5	757
E	1.1	76.3

Oil Blvd 77.37

4+00

E	1.1	76.3
CL	1.4	760
½	1.6	758
C	2.8	746
¼	2.9	745
CL	3.1	743
W	3.7	737

4+50

W	3.8	736
CL	3.2	742
¼	3.1	743
C	2.8	746
¼	1.9	755
CL	1.6	758
E	1.0	764

5+00 - 5L. Forward ½ = PP

E	09	76.5
CL	1.6	758
½	1.6	758
C	1.7	747
¼	1.7	747
CL	3.2	742
W	3.7	737

77.37

S.L. Forward #2

W			3.8	73.6
¼			3.1	74.3
½			2.7	74.7
C			2.9	74.5
½			1.5	75.9
¼			1.4	76.0
E			0.9	76.5
T.P.	434	80.79	0.92	76.45

N.L. Forward #1

E			4.4	76.4
¼			5.0	75.8
½			5.7	75.1
C			6.4	74.4
½			6.6	74.3
¼			7.0	73.8
W			7.5	73.3

N.L. Forward #2 Rd

W			7.5	73.3
¼			7.0	73.8
½			6.4	74.4
C			6.2	74.6
½			5.7	75.1
¼			5.0	75.8
E			4.6	76.2

Oil Blvd. 80.79

6

50 N. of N.L. #2

E			4.7	76.1
¼			5.7	75.1
½			5.7	75.1
C			6.6	74.3
½			6.7	74.1
¼			7.4	73.4
W			7.8	73.0

90.34 N. of N.L. #2 = S.L. Alley #1 = Rd

W			7.7	73.1
¼			7.6	73.2
½			6.8	74.0
C			6.5	74.3
½			5.7	75.1
¼			5.5	75.3
E			5.3	75.5

S.L. Alley #2

E			5.3	75.5
¼			5.5	75.3
½			5.6	75.2
C			6.5	74.3
½			6.7	74.1
¼			7.3	73.5
W			7.7	73.1

80.79

N.L. Alley #1

W	7.8	73.0
Ct	7.4	73.4
½	6.9	73.9
C	6.5	74.3
½	5.7	75.1
℄	5.6	75.2
E	5.3	75.5

5.91 80.91 75.00 B.M.

N.L Alley #2 = R₂ = 0+00

E	5.5	75.4
Ct	5.6	75.3
½	6.0	74.9
C	6.5	74.4
½	7.0	73.9
Ct	7.6	73.3
W	7.9	73.0

0+50

W	7.8	73.1
Ct	7.5	73.4
½	7.0	73.9
C	6.4	74.5
½	6.1	74.8
Ct	{6.3 5.7	{74.6 75.2
E	5.2	75.7

Oil Blvd

80.91

7

1+00

E	5.1	75.8
Ct	{5.6 5.1	{75.3 74.8
½	5.8	75.1
C	6.1	74.8
½	6.9	74.0
Ct	7.4	73.5
W	7.6	73.3

1+50

W	7.5	73.4
Ct	7.2	73.7
½	6.8	74.1
C	6.2	74.7
½	5.7	75.2
℄	{6.1 5.4	{74.8 75.5
E	4.9	76.0

2+00

E	5.0	75.9
Ct	{6.5 6.1	{75.4 74.8
½	5.9	75.0
C	6.3	74.6
½	6.8	74.1
Ct	7.4	73.5
W	7.8	73.1

8.0.91

2+50

W	9.2	71.7
Ct	7.8	73.1
¼	7.4	73.5
C	6.8	74.1
¼	6.2	74.7
Ct	6.1 5.2	74.8 75.7
E	4.9	76.0

2+75

E	4.7	76.2
Ct	6.2 6.8	74.7 74.1
¼	6.7	74.2
C	7.1	73.8
¼	7.5	73.4
Ct	7.8	73.1
W	9.6	71.3

3+00

W	8.3	72.6
Ct	7.1	73.8
¼	6.9	74.0
C	6.6	74.3
¼	6.6	74.3
Ct	7.5 7.0	73.4 73.9
E	5.7	75.2

Oil Blvd.

8091

3+50

E	3.9	77.0
Ct	4.3 5.0	76.6 75.9
¼	4.7	76.2
C	5.0	75.9
¼	5.4	75.5
Ct	5.5	75.4
W	5.7	75.2

4+00

W	5.0	75.9
Ct	4.9	76.0
¼	4.9	76.0
C	4.1	76.8
¼	4.2	76.7
Ct	4.5 3.7	76.4 77.2
E	3.5	77.4

4+50

E	2.9	78.0
Ct	3.2 3.8	77.7 77.1
¼	3.4	77.5
C	3.7	77.2
¼	4.1	76.8
Ct	4.2	76.7
W	4.4	76.5

80.91

5+00

W			3.8	77.1
Ct			3.6	77.3
½			3.5	77.4
C			3.4	77.5
½			2.9	78.0
Ct			{3.3 2.7	{77.6 78.2
E			2.4	78.5

5+39.1 = S.L. Bird Rock Ave #1 Rs

E			2.1	78.8
Ct			{2.5 3.2	{78.4 77.7
½			2.6	78.3
C			3.0	77.9
½			2.9	78.0
Ct			3.0	77.9
W			3.3	77.6

S.L. B.R. Ave #2

W			2.8	78.1
Ct			2.7	78.2
½			2.7	78.2
C			3.0	77.9
½			2.5	78.4
Ct			3.2 2.3	{77.7 78.6
E			2.1	78.8
T.P.	4.06	82.91	2.06	78.85 BM-BR Ave

82.91

Oil Blvd.

N.L. BR Ave #1

E	2.7	80.2
Ct	{2.3 3.0	{80.6 79.9
½	2.5	80.4
C	2.5	80.4
½	2.5	80.4
Ct	2.6	80.3
W	2.4	80.5

N.L. BR Ave #2 Rs = 0+00

W	2.4	80.5
Ct	2.5	80.4
½	2.3	80.6
C	2.1	80.8
½	2.2	80.7
Ct	{2.8 2.1	{80.1 80.8
E	2.0	80.9

0+50

E	1.4	81.5
Ct	{1.3 2.0	{81.6 80.9
½	1.0	81.9
C	1.5	81.4
½	1.8	81.1
Ct	2.0	80.9
W	1.7	81.2

8.2.91

1+00

W	2.7	80.2
W	2.5	80.4
W	2.2	80.7
C	1.5	81.4
W	1.7	81.2
W	2.2 / 1.6	80.7 / 81.3
E	1.2	81.7

1+50

E	1.7	81.2
W	2.2 / 2.7	80.7 / 80.2
W	2.6	80.3
C	2.7	80.2
W	3.4	79.5
W	3.8	79.1
W	4.2	78.7

2+00

W	4.7	78.2
W	4.3	78.6
W	3.8	79.1
C	3.1	79.8
W	3.0	79.9
W	3.1 / 2.6	79.8 / 80.3
E	2.1	80.8

BM SON. BR. AVE. 0.177 82.14

Oil Blvd 8.2.91

2+50

E	2.5	80.4
W	2.8 / 3.4	80.1 / 79.5
W	3.2	79.7
C	3.3	79.6
W	4.0	78.9
W	4.5	78.4
W	5.0	77.9

3+00

W	5.0	77.9
W	4.6	78.3
W	4.0	78.9
C	3.9	79.0
W	3.3	79.6
W	3.9 / 3.3	79.0 / 79.6
E	2.8	80.1

3+50

E	3.0	79.9
W	3.2 / 3.8	79.7 / 79.1
W	3.5	79.4
C	3.8	79.1
W	4.2	78.7
W	4.9	78.0
W	4.9	78.0

8.3.91

4+00

W	5.3	77.6
CL	5.1	77.8
¼	4.6	78.3
C	4.2	78.7
¼	3.8	79.1
CL	4.1 3.5	78.8 79.4
E	3.2	79.7

4+50

E	3.7	79.2
CL	4.2 4.8	78.7 78.1
¼	4.3	78.6
C	4.7	78.2
¼	5.0	77.9
CL	5.5	77.4
W	5.5	77.4

5+00

W	5.8	77.1
CL	5.4	77.5
¼	5.0	77.9
C	4.9	78.0
¼	4.6	78.3
CL	5.0 4.5	77.9 78.4
E	4.1	78.8

Oil Blvd.

8.2.91

11

5+50

E	4.2	78.7 78.3
CL	4.6 5.2	77.7
¼	4.7	78.2
C	5.0	77.9
¼	5.3	77.6
CL	5.8	77.1
W	5.8	77.1

5+80.64 N.L. BR City #1 P.I.

W	6.1	76.8
CL	5.7	77.2
¼	5.5	77.4
C	5.3	77.6
¼	5.1	77.8
CL	5.2 4.8	77.7 78.1
E	4.5	78.4

N.L. B.R. City #2

E	4.5	78.4
CL	4.8 5.3	78.1 77.6
¼	5.2	77.7
C	5.6	77.3
¼	5.6	77.3
CL	5.8	77.1
W	6.5	76.4

Brg. N.L. B.R. City 4.68 78.23

		83.91		
B.M. Stone Marked bet Akalone and Dolphin on E. line Goulath.			12.99 →	69.92
11.79	94.07		0.63	82.28 –
			2.31	91.76
12.92	106.32		0.67	93.40
12.95	119.08		0.19	106.13
			11.86	107.22
12.80	131.28		0.60	118.48
12.84	143.68		0.44	130.84
12.75	155.62		0.81	142.87

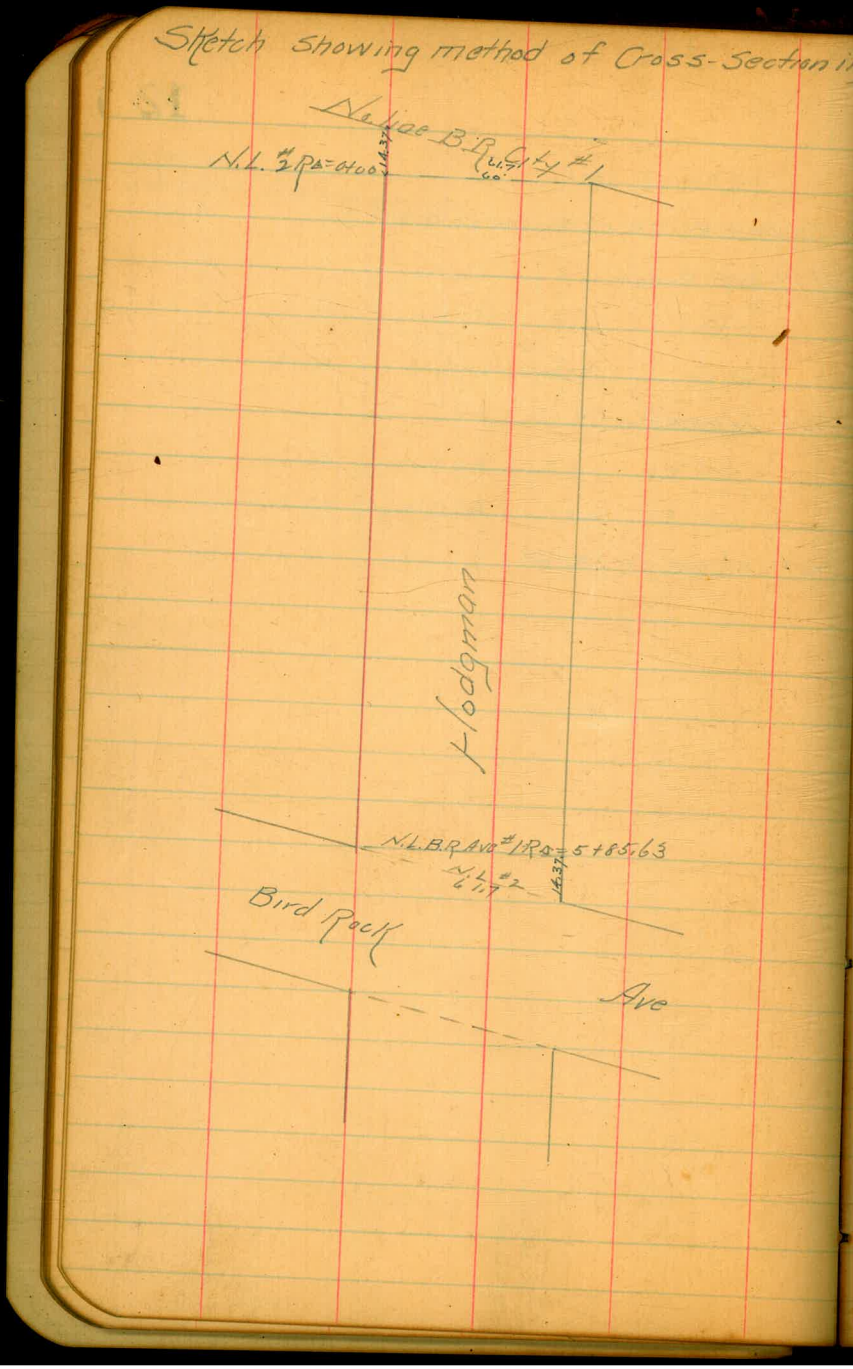
Marked Stone 40'N.W. of No. end Elect Arc.

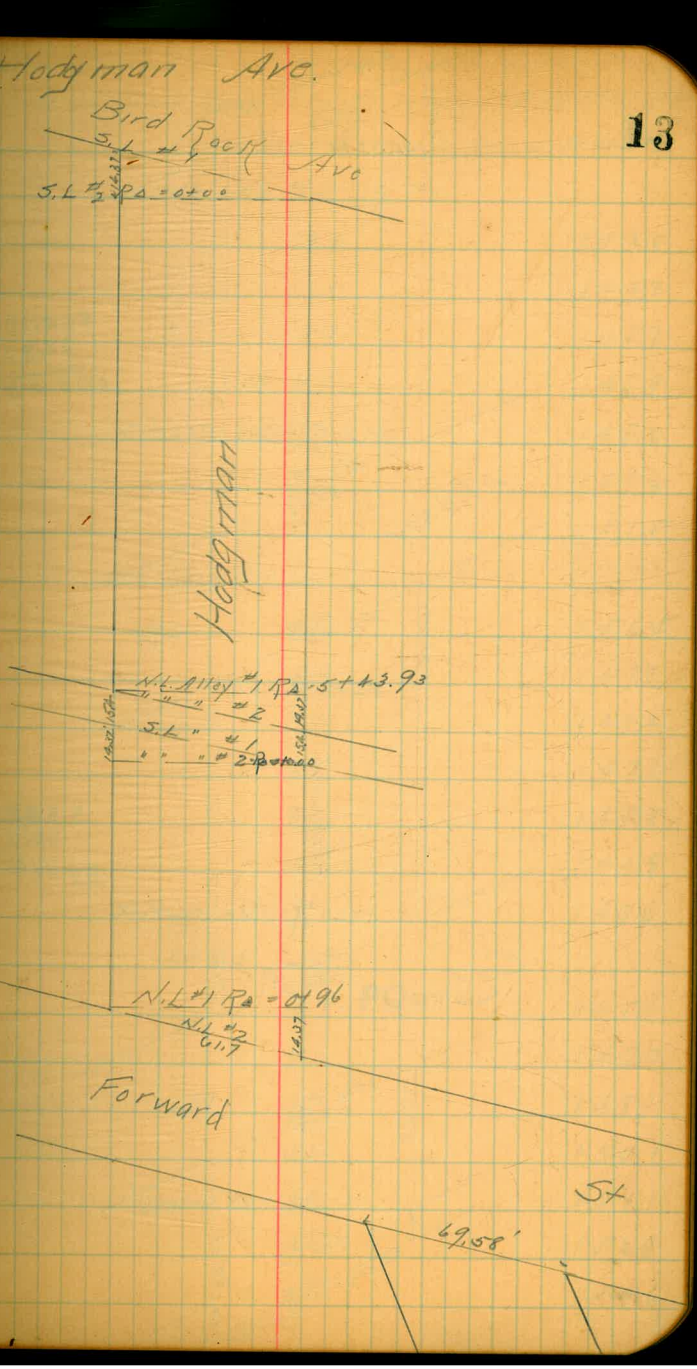
Hut. N. end Dodge

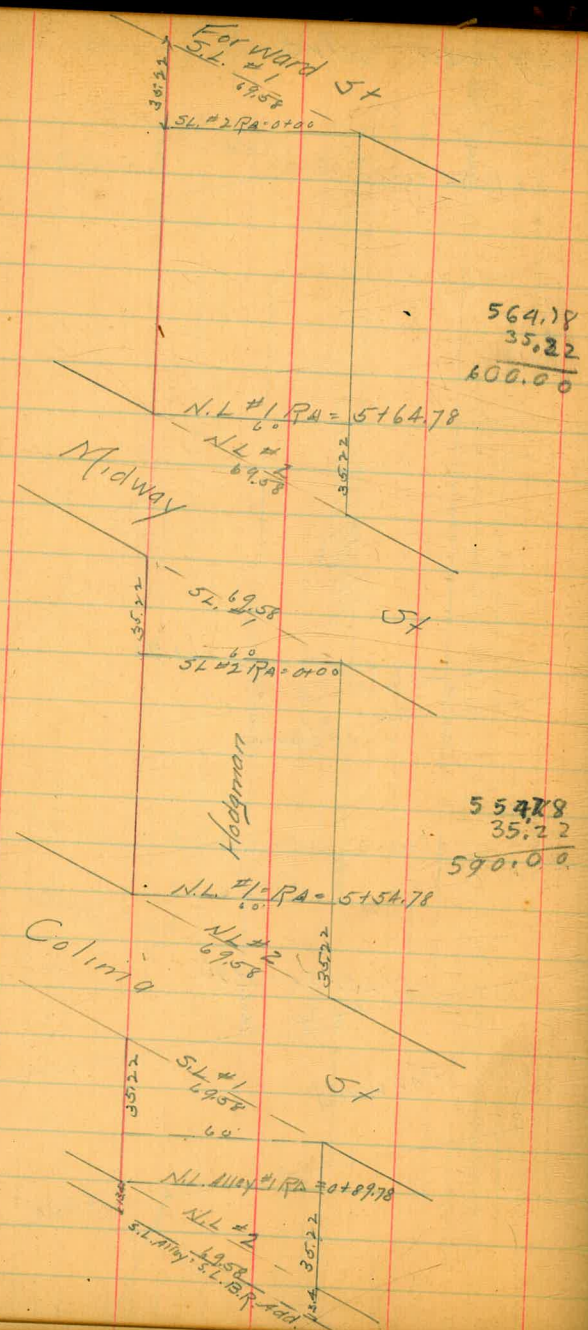
– Hut. N. end Burke

– Hut. N. end Hodgman.

Sketch showing method of Cross-Sectioning Hodgman Ave.







Cross-Section of Hodgman Ave. from
No. line of Bird Rock City to So line of Bird Rock Add.
155.62 12/19/07 Davis Donnan Collard

No line B.R. City #1

W	12.8	142.8
Cl	11.4	144.2
1/4	9.9	145.7
C	8.7	146.9
1/4	7.6	148.0
Cl	6.0	149.6
E	4.1	151.5

No. line B.R. City #2 = RA = 0+00

E	4.1	151.5
Cl	5.8	149.8
1/2	7.2	148.4
C	8.5	147.1
1/2	9.8	145.8
Cl	10.7	144.9
W	12.0	143.6

0+25

POSTED

W	9.7	145.9
Cl	8.6	147.0
1/2	7.5	148.1
C	5.5	150.1
1/2	4.5	151.1
Cl	2.8	152.8
E	1.0	154.6

		155.62		
		0+37		
E			0.0	155.6
C			2.6	153.6
W			3.0	152.6
C			4.4	151.2
W			5.8	149.8
C			7.2	148.4
W			8.6	147.0
		0+50		
W			8.5	147.1
C			7.3	148.3
W			6.0	149.6
C			4.2	151.4
W			2.8	152.8
C			1.9	153.7
E			1.0	154.6
T.P.	3.50	158.32	0.80	154.82
		0+75		
E			0.8	157.5
C			2.3	156.0
W			4.3	154.0
C			6.0	152.3
W			7.9	150.4
C			9.5	148.8
W			11.3	147.0

Hodgman Ave 158.32

	1+00	
W	10.5	147.8
C	9.1	149.2
W	7.4	150.9
C	5.4	152.9
W	3.9	154.4
C	2.1	156.2
E	0.4	157.9
	1+25	
E	0.7	157.6
C	2.2	156.1
W	4.8	153.5
C	5.9	152.4
W	7.6	150.7
C	9.1	149.2
W	10.6	147.8
	1+50	
W	11.0	147.3
C	9.7	148.6
W	8.0	150.3
C	6.1	152.2
W	5.3	153.0
C	3.7	154.6
E	P.V.I.	156.2

POSTED

158.32

		1+75		
E			2.5	155.8
Ct			4.1	154.2
½			6.0	152.3
C			7.2	151.1
½			8.9	149.4
Ct			10.7	147.6
W			11.9	146.4
		2+00		
W			14.1	144.2
Ct			12.3	146.0
½			10.8	147.5
C			8.8	149.5
½			6.9	151.4
Ct			5.5	152.8
E			3.9	154.4
		2+25		
E			5.6	152.7
Ct			7.1	151.2
½			8.8	149.5
C			10.2	148.1
½			12.2	146.1
T.P.	2.94	149.72	11.54	146.78
Ct			5.4	144.3
W			6.8	142.9

POSTED

149.72

Hodgman

	2+50	
W	8.6	141.1
Ct	7.3	142.4
½	5.6	144.1
C	3.8	145.9
½	2.6	147.1
Ct	1.0	148.7
E	+0.7	149.0
	2+75	
E	1.9	147.8
Ct	3.5	146.2
½	4.4	145.3
	5.0	144.7
C	6.2	143.5
½	7.8	141.9
Ct	9.5	140.2
W	11.0	138.7
	3+00	
W	13.0	136.7
Ct	12.2	137.5
½	10.9	138.8
C	9.0	140.7
½	7.7	142.0
Ct	7.5 / 6.5	142.2 / 143.2
E	5.1	144.6

POSTED

POSTED

		1+97.72		
		3+25		
E			7.6	142.1
Ck			9.3 10.3	140.4 139.4
Hub			10.9	138.8
C			12.0	137.7
TP.	2.28	139.79	12.21	137.58
Hub			3.6	136.3
Ck			4.9	134.9
W			5.9	133.9
		3+50		
W			8.7	131.1
Ck			7.3	132.5
Hub			6.2	133.6
C			4.7	135.1
Hub			3.6	136.2
Ck			3.0 2.1	136.8 137.7
E			0.6	139.5
		3+75		
E			2.8	137.5
Ck			4.3 5.2	135.5 134.6
Hub			6.1	133.7
C			7.0	132.8
Hub			8.8	131.0
Ck			9.7	130.1
W			10.7	129.1

Hodgman

	4+00	
W	12.8	127.0
Ck	12.0	127.8
Hub	10.5	129.0
C	9.3	130.5
Hub	7.5	132.3
Ck	6.5 5.7	133.3 134.1
E	3.9	135.9
	4+25	
E	4.6	135.2
Ck	6.6 7.3	133.2 132.5
Hub	8.3	131.5
C	10.3	129.5
Hub	11.7	128.1
Ck	12.7	127.1
W	13.2	126.6
	4+50	
W	12.2	127.6
Ck	11.9	128.0
Hub	11.7 12.2 11.4	128.1 127.6 128.4
C	10.1	129.7
Hub	8.7	131.1
Ck	7.3 6.8	132.5 133.0
E	4.4	135.4

139.79

4+75

E	6.1	133.7
CL	8.1 / 8.6	131.7 / 131.2
W	9.5	130.3
C	9.7	130.1
W +6 CL	10.5 / 11.7 / 10.9 / 11.0	129.3 / 128.4 / 128.9 / 128.9
W	11.6	128.2

5+00

W	11.0	128.8
CL +7	10.7 / 11.3	129.1 / 128.5
W	10.3	129.5
C	9.3	130.5
W	8.9	130.9
CL	9.4 / 8.8	130.4 / 131.0
E	8.1	131.7

5+25

E	7.9	131.9
CL	8.1 / 7.9	131.7 / 130.9
W	8.5	131.3
C	8.9	130.9
W +7 CL +8	9.6 / 10.3 / 9.7 / 9.7	130.2 / 129.5 / 130.1 / 130.1
W	9.5	130.3

Hodgman

5+50

W	9.1	130.7
CL +1	9.0	130.8
+3 W	8.9 / 9.4 / 8.6	130.9 / 130.4 / 131.2
CL	8.0	131.8
W	7.9	131.9
W	8.0 / 7.5	131.8 / 132.3
E	7.0	132.8

POSTED

5+75

E	6.8	134.0
CL	6.2 / 6.9	133.6 / 132.9
W	6.8	133.0
C	6.6	133.2
W +7 CL +8	7.1 / 8.2 / 7.5 / 7.5	132.7 / 131.6 / 132.3 / 132.3
W	7.7	132.1

5+85.63= N.L.B.R. Ave #1-RA

W	7.0	132.8
CL +1 +3 W	6.9 / 6.9 / 7.6 / 6.3	132.9 / 132.9 / 132.2 / 133.5
W	5.9	133.9
W	6.7	133.6
W	56.1 / 5.6	133.7 / 134.2
E	5.1	134.7

139.79

N.L.B.R. Ave #2

E		4.3	135.5
C		4.5	135.3
+2		6.4	134.4
W		6.7	134.1
C		5.5	134.3
W		6.0	133.8
+2		7.3	132.5
C		6.8	133.0
		6.8	133.0
W		7.0	132.8
T.P	11.85	144.63	7.01	132.78 N.L.B.R. Ave

S.L.B.R. Ave #1

W		8.3	136.3
C		7.4	137.2
+2		8.0	136.6
W		7.0	137.6
C		6.3	138.3
W		6.6	138.0
+8		6.9	137.7
C		6.1	138.5
E		6.1	138.5

S.L.BR. Ave #2: RA = 0+00

E		6.1	138.5
		6.1	138.5
C		6.7	137.9
W		6.2	138.4
C		6.0	138.6
W		6.9	137.7
+8		7.2	137.0
C		7.2	137.4
W		7.8	136.8

Hodgman

0+50

W		6.1	138.5
C		5.4	139.2
+2		5.8	138.8
C		4.9	139.7
C		4.3	140.3
W		4.1	140.5
C		4.3	140.3
		4.7	139.9
E		3.2	141.4

1+00

E		0.2	144.4
		0.6	144.0
C		1.2	143.4
W		1.1	143.5
C		1.1	143.5
W		1.8	142.8
+8		2.9	141.7
C		2.4	142.2
W		3.4	141.2
T.P.	4.24	149.91	0.96	143.67

1+50

W		6.8	143.1
C		6.0	143.9
+1		6.9	144.0
W		6.4	143.5
		5.5	144.4
C		4.3	145.6
W		3.2	146.7
C		3.3	146.6
		3.2	146.7
E		1.4	148.5

149.91

2+50

E	1.0	148.9
ib	1.4	148.5
	2.1	147.8
w	2.2	147.7
c	2.7	147.2
w	3.9	146.0
+7	5.0	144.9
+9	4.6	145.3
ob	4.6	145.3
W	5.1	144.8

2+50

W	6.6	143.3
ob	6.0	143.9
+2	5.9	144.0
w	6.4	143.5
	5.3	144.6
c	4.5	145.4
w	3.5	146.4
ob	3.4	146.5
	2.7	147.2
E	1.9	148.0

3+00

E	3.1	146.8
+8	3.8	146.1
ob	4.3	145.6
w	4.2	145.7
c	5.0	144.9
w	6.0	143.9
+7	7.0	142.9
+8	6.7	143.2
ob	6.8	143.1
W	7.5	142.4

149.91

Hodgman

20

3+50

W	8.1	141.8
ob	7.5	142.4
+2	7.3	142.6
+3	7.8	142.1
w	6.8	143.1
c	5.8	144.1
w	5.4	144.5
ob	5.3	144.6
	4.8	145.1
E	4.1	145.8

4+00

E	4.6	145.3
ob	5.3	144.6
	5.8	144.1
w	5.7	144.2
c	6.5	143.4
w	6.9	143.0
+7	8.1	141.8
+8	7.6	142.3
ob	7.8	142.1
W	8.4	141.5

4+50

W	9.3	140.6
ob	8.6	141.3
+2	8.5	141.4
+3	8.8	141.1
w	7.9	142.0
c	7.1	142.8
w	6.1	143.8
ob	6.6	143.3
+2	5.6	144.3
E	5.3	144.6

14991

5+00

E		
+8	6.0	143.9
	6.6	143.3
W	7.6	142.3
+3	6.7	143.2
W	7.1	142.8
C	7.9	142.0
W	8.6	141.3
+7	9.6	140.3
+8	9.0	140.9
CL	9.1	140.8
W	9.8	140.1

5+43.93 RA - N.L. Alley #1

W	10.9	139.0
CL	10.6	139.3
+7	10.5	139.4
W	11.2	138.7
	10.2	139.7
C	9.5	140.4
W	8.9	141.0
CL	9.6	140.3
	8.6	141.3
E	8.3	141.6

N.L. Alley #2

E	9.1	140.8
+8	9.3	140.6
CL	10.3	130.6
W	9.5	140.4
C	9.6	140.3
W	10.3	139.6
+8	11.4	138.5
CL	10.9	139.0
	10.7	139.2
W	10.9	139.0

T.P	2.19	141.14	10.96	138.95

Hodgman

Saline Alley #1

21

W	2.5	138.6
CL	2.3	138.8
+2	2.3	138.8
+3	3.3	137.8
W	2.1	139.0
C	1.5	139.6
W	1.5	139.6
CL	2.0	139.1
	1.3	139.8
E	0.9	140.2

S.L. Alley #2 RA - 0+00

E	0.9	140.2
CL	1.4	139.7
	2.3	138.8
W	1.7	139.4
C	1.8	139.3
W	2.5	138.6
+7	3.9	137.7
+8	3.0	138.1
CL	3.0	138.1
W	3.4	137.7

+50

W	5.7	135.4
CL	5.3	135.8
+2	5.3	135.8
+3	5.9	135.2
W	4.7	136.4
C	4.0	137.1
W	4.0	137.1
CL	4.6	136.5
	3.8	137.3
E	3.2	137.9

141.14

0+96 = N.L. Forward #1 RA

E	6.8	135.3
Ck	6.1	135.0
+1	6.1	135.0
+2	6.9	134.2
4L	6.1	135.0
C	6.3	134.8
4L	6.9	134.2
+8	7.9	133.2
Ck	7.3	133.8
W	8.0	133.1

N.L. Forward #2

W	8.0	133.1
Ck	7.4	133.7
+1	7.4	133.7
+3	7.9	133.2
4L	7.2	133.9
C	6.6	134.5
4L	6.8	134.3
+7	7.4	133.7
+8	6.7	134.4
Ck	6.6	134.5
E	6.4	134.7
B.M. N.E Forward.	6.36	134.78

S.L. Forward #1

W	6.9	134.2
+10	7.6	133.5
Ck	8.1	133.0
4L	7.3	133.8
C	6.7	134.4
4L	7.5	133.6
+7	8.0	133.1
+10	7.0	134.1
Ck	6.9	134.2
E	6.7	134.4

Hodgman

22

S.L. Forward #2 - RA = 0+00

E	6.7	134.4
Ck	7.1	134.0
+3	8.1	133.0
4L	7.8	133.3
C	7.2	133.9
4L	8.1	133.0
	9.1	132.0
Ck	8.4	132.7
W	8.8	132.3

0+50

W	10.9	130.2
	10.4	130.7
Ck	10.9	130.2
4L	9.8	131.3
C	8.8	132.3
4L	9.0	132.1
+7	9.6	131.5
+8	8.7	132.4
Ck	8.6	132.5
E	8.1	133.0

1+00

E	9.0	132.1
Ck	9.5	131.6
+2	9.6	131.5
+3	10.4	130.7
4L	10.1	131.0
C	9.7	131.4
4L	11.0	130.1
+8	12.1	129.0
Ck	11.4	129.7
W	11.8	129.3

141.14

1+50

W			12.3	128.8
Ck			11.8	129.3
+2			12.5	128.6
W			11.3	129.8
L			10.1	131.0
W			10.3	130.8
+8			10.8	130.3
Ck			9.8	131.3
E			9.2	131.9

2+00

E			9.2	131.9
Ck			9.7	131.4
+2			10.8	130.3
+7			10.4	130.7
C			10.5	130.6
W			11.4	129.7
+7			12.4	128.7
Ck +8			11.2	129.5
			11.6	129.5
W			12.4	128.7

2+50

W			12.8	128.3
Ck			12.4	128.7
+2			12.3	128.8
+3			13.3	127.8
W			12.0	129.1
C			11.1	130.0
W			11.1	130.0
+7			11.6	129.5
+8			11.7	130.4
Ck			10.6	130.5
E			10.0	131.1
T.P	0.19	130.88	10.45	130.69

Hodgman

23

3+00

E	0.5	130.4
Ck	1.1	129.8
+2	1.3	129.6
+3	2.0	128.9
W	1.7	129.2
C	1.9	129.0
W	2.9	128.0
+7	3.9	127.0
+8	3.5	127.4
Ck	3.6	127.3
W	4.3	126.6

3+50

W	5.4	125.5
Ck	4.7	126.2
+2	4.5	126.4
+3	5.0	125.9
W	3.9	127.0
C	3.2	127.7
W	3.9	127.0
+7	3.3	127.7
+8	2.5	128.4
Ck	2.2	128.7
E	1.7	129.2

4+00

E	2.7	128.2
Ck	3.5	127.4
+2	3.5	127.4
+3	4.3	126.6
W	3.8	127.1
C	4.0	126.9
W	5.7	125.7
+7	6.7	124.7
+8	5.5	125.4
Ck	5.8	126.1
W	6.3	124.6

130.88

4+50

W	6.8	124.1
U	6.3	124.6
+2	6.1	124.8
+3	7.0	123.9
U	5.8	125.1
C	4.9	126.0
U	4.7	126.2
+7	5.0	125.9
+8	4.1	126.8
C	4.1	126.8
E	3.5	127.4

5+00

E	4.4	126.5
U	4.9	126.0
+1	4.9	126.0
+3	5.8	125.1
U	5.7	125.2
C	5.7	125.2
U	6.5	124.4
+6	7.3	123.6
C +8	6.9	124.0
	7.0	123.9
WK	7.4	123.5

5+64.78 W.L. Midway #1 = RP

W	9.1	121.8
C	8.6	122.3
+2	8.4	122.5
U +3	8.9	122.0
	7.9	123.0
C	6.9	124.0
U	6.9	124.0
+7	6.9	124.0
C +8	6.2	124.7
	6.1	124.8
E	5.7	125.2

Hodgman

No. line Midway #2

E	6.6	124.3
U	6.9	124.0
+1	7.0	123.9
+3	7.8	123.1
U	7.3	123.6
C	7.4	123.5
U	8.3	122.6
+1	9.1	121.8
+2	8.6	122.3
C	8.3	122.6
W	9.1	

B.M. S.W. Midway 10.61 120.37

So. line Midway #1 120.3

W	10.6	
U	10.2	120.7
+3	10.3	120.6
+5	10.7	120.2
U	10.1	120.8
C	9.3	121.6
U	9.6	121.3
+6	10.4	120.5
+7	9.6	121.3
C	9.6	121.3
E	9.7	121.2

S.L. Midway #2 RP = 0+00

E	9.7	121.2
U	9.8	121.1
+2	9.7	121.2
U +3	10.8	120.1
C	10.1	120.8
U	10.8	120.1
	11.7	119.2
+7	11.1	119.8
C +8	10.3	120.6
W	10.7	120.2

130.88

0+50

W			12.9	118.0
C	+2		12.7	118.2
W	+3		12.6	118.3
			13.1	117.8
			12.4	118.5
C			11.8	119.1
W			11.7	119.2
	+7		12.5	118.4
	+8		11.6	119.3
C			11.1	119.8
E				
TP.	8.80	128.06	11.62	119.26
		1+00		
E			9.1	119.0
C			9.4	118.7
			10.2	117.9
W			9.7	118.4
C			9.5	118.6
W			10.5	117.6
	+6		11.6	116.5
C	+7		10.9	117.2
			10.8	117.3
W			11.0	117.1
		1+50		
W			12.7	116.4
C			11.7	116.4
W			11.0	117.1
C			10.3	117.8
W			10.3	117.8
C			10.7	117.4
E			10.5	117.6

Hodgman

25

2+00

E	7.4	120.7
	8.2	119.9
C	9.4	118.7
W	9.3	118.8
C	9.7	118.4
W	10.7	117.4
	11.5	116.6
C	10.7	117.4
	+3 10.6	117.5
W	11.1	117.0
	2+50	
W	11.3	116.8
C	10.6	117.5
	+2 10.7	117.4
	+4 11.3	116.8
W	10.3	117.8
C	9.4	118.7
W	8.7	119.4
	+8 9.0	119.1
C	+9 8.2	119.9
	8.0	120.1
E	7.5	120.6
	3+00	
E	8.2	119.9
	8.7	119.4
C	9.4	118.7
W	9.1	119.0
C	9.5	118.6
W	10.4	117.7
	11.5	116.6
C	+8 11.1	117.0
	11.2	116.9
W	11.7	116.4

126.06

3+50

W	11.8	116.3
C	11.2	116.9
+3	11.1	117.0
+3	11.7	116.4
W	10.5	117.6
C	9.9	118.2
W	9.6	118.6
+7	9.8	118.3
+8	9.1	119.0
C	9.0	119.1
E	8.5	119.6

4+00

E	8.5	119.6
C	9.0	119.1
+1	9.0	119.1
+2	9.3	118.8
W	9.5	118.6
C	9.7	118.4
W	10.8	117.3
+7	11.9	116.3
+8	11.3	116.8
C	11.4	116.7
NW	12.0	116.1

4+32

W	12.6	115.5
C	11.9	116.2
W	10.9	117.2
C	10.2	117.9
W	10.1	118.0
C	9.9	118.2
E	9.4	118.7

Hodgman

4+50

E	8.1	120.0
C	8.8	119.3
+1	8.9	119.2
+3	9.3	118.8
W	9.1	119.0
C	9.1	119.0
W	10.0	118.1
+7	10.8	117.3
+8	10.4	117.7
C	10.6	117.5
NW	11.7	116.4

POSTED

5+00

W	10.6	117.5
C	9.7	118.4
+2	9.5	118.6
+3	10.3	118.1
W	8.5	119.9
C	8.0	120.1
W	7.4	120.7
+7	7.7	120.4
+8	6.8	121.3
E	6.3	121.8

5+54.78 = N.L. Colima #1 Rd

E	5.0	123.1
C	5.4	122.7
+2	5.4	122.7
+3	6.3	121.8
W	6.0	122.1
C	6.9	121.2
W	7.9	120.2
+8	8.9	119.2
C	8.4	119.7
NW	9.0	119.1

158.06

No line Colima #2

W	9.0	119.1
Ch	8.2	119.9
+2	8.7	119.4
W	7.5	120.6
C	6.6	121.5
W	6.0	122.1
	5.9	122.2
+8	5.2	122.9
Ch +10	5.0	123.1
E	4.0	124.1
B.M. NE Colima	3.95	124.11

S.L. Colima #1

E.	2.7	125.4
Ch	3.2	124.9
	3.4	124.7
+2 +4 W	4.1	124.0
	3.9	124.2
C	4.2	123.9
W	5.2	122.9
	6.3	121.8
Ch	5.7	122.4
W	6.4	121.7

S.L. Colima #2 - R.P. = 0+00

W	6.0	122.1
Ch	5.1	123.0
W	4.3	123.8
C	3.7	124.4
W	3.4	124.7
	3.9	124.2
+7 Ch 8	3.1	125.0
	2.9	125.2
E	2.7	125.4

Hodgman

0+50

E	0.8	127.3
W	1.3	126.8
	1.4	126.7
+3 W	1.9	126.2
	1.8	126.3
C	2.2	125.9
W	3.1	125.0
	4.1	123.5
Ch	3.9	124.2
W	4.4	123.7

T.P. 4.67 131.95 0.78 127.28

0+89.78 - N.L. Alley #1 - R.P.

W	6.8	125.1
Ch	6.5	125.4
W	5.9	126.0
C	5.6	126.3
W	4.8	127.1
+5	4.8	127.1
+7	4.2	127.7
Ch	4.1	127.8
E	3.1	128.7

N.L. Alley #2

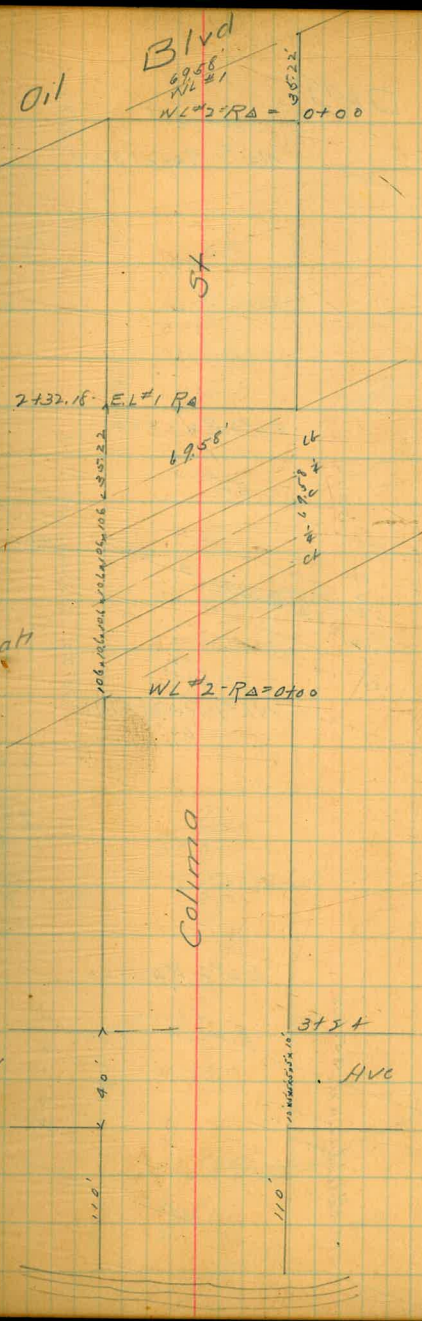
E	2.7	129.2
Ch	3.7	128.2
W	4.3	127.6
C	4.7	127.2
W	5.5	126.4
Ch	6.0	125.9
W	6.8	125.1

131.95

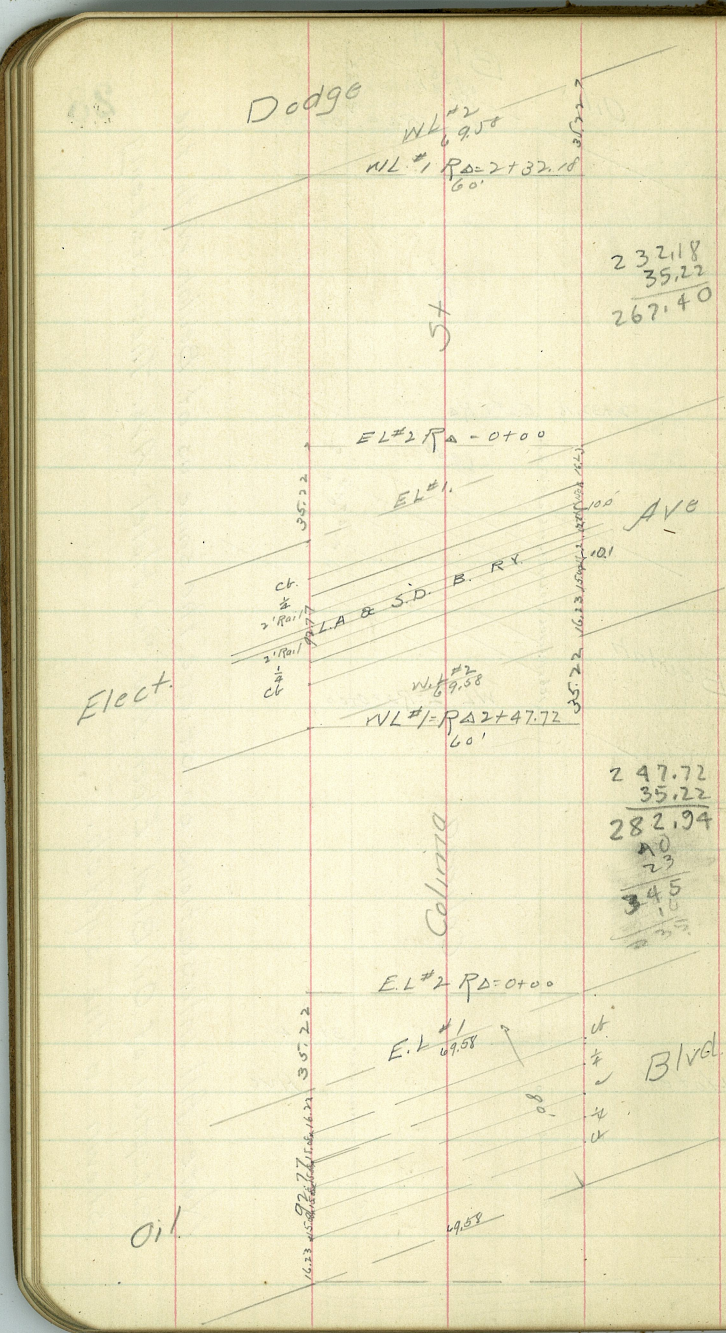
So. line Alley - S.L.B.R. Add.

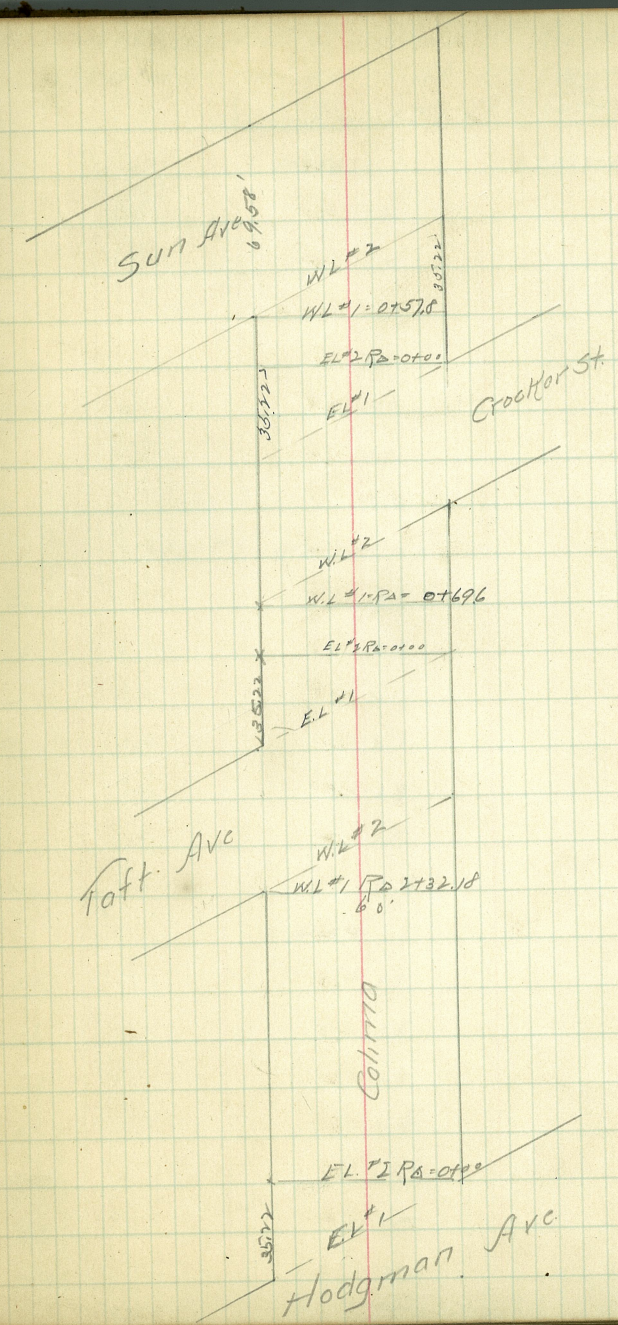
W	6.2	125.7
"	5.4	126.6
"	4.4	127.5
"	4.4	127.5
" +8	3.8	128.1
"	3.8	128.1
" +3	5.8	126.1
"	6.0	125.9
E	4.1	127.8

Sketch showing method of Cross-Sectioning Colima St.



Note- All intersections on St are the same as at Beulah with the exception of Oil Blvd. Elect Ave. and Hotel Ave. These Sts. being shown in the Sketch.


Dodge
WL #2
69.58
WL #1 RΔ=2+32.18
60'
35.22
232.18
35.22
267.40
St
EL #2 RΔ = 0+00
EL #1
35.22
Ave
L.A. & S.D. B. RY.
Elect.
WL #2
69.58
WL #1 = RΔ 2+47.72
60'
35.22
247.72
35.22
282.94
Colima
EL #2 RΔ = 0+00
EL #1
69.58
35.22
Blvd
Oil
69.58


Sun Ave
69.58'
WL #2
WL #1 = 0+57.8
35.22
EL #2 RΔ = 0+00
EL #1
Crocker St.
35.22
WL #2
WL #1 = RΔ = 0+69.6
EL #2 RΔ = 0+00
35.22
EL #1
Taft Ave
WL #2
WL #1 RΔ 2+32.18
60'
Colima
EL #2 RΔ = 0+00
EL #1
35.22
Hodgman Ave

Cross Section of Colima St from Oil Blvd. to West end of St. 12/20/07 { Davis Donnan Collatt

W.L. Oil Blvd #1

1.17 80.55 79.38 - BM.

No	1.2	79.4
ch	1.5	79.1
ch	1.7	78.9
c	2.3	78.3
ch	3.0	77.6
ch	3.1	77.5
So	3.3	77.3

WL #2 - RA = 0+00

So	3.6	77.0
ch	2.9	77.7
ch	2.1	78.5
c	2.1	78.5
ch	1.8	78.8
ch	1.5	79.1
No	1.2	79.4

0+50

No	1.7	78.9
ch	1.8	78.8
ch	2.0	78.6
c	2.4	78.2
ch	2.6	78.0
ch	3.0	77.6
So	3.2	77.4

80.55

1 + 0.0

So	3.4	77.2
Ch	2.8	77.8
N	2.2	78.4
C	2.0	78.6
Ni	1.8	78.8
U	2.1	78.5
No	2.2	78.4

1 + 5.0

No	2.7	77.9
U	2.7	77.9
Ni	2.7	77.9
C	2.7	77.9
Ni	3.1	77.5
U	3.0	77.6
So	3.3	77.3

2 + 0.0

So	4.2	76.4
Ch	4.3	76.3
Ni	4.5	76.1
C	4.2	76.4
Ni	3.7	76.9
U	3.9	76.7
No	3.7	76.9

Colima

2 + 32.8 = E.L. Beulah #1-Ra

No	5.3	75.3
U	5.0	75.6
N	4.8	75.8
C	4.9	75.7
N	5.4	75.2
U	5.7	74.9
So	5.7	74.9

E.L. Beulah #2

So	5.7	74.9
U	5.8	74.8
N	5.6	75.0
C	5.7	74.9
N	6.3	74.3
U	6.3	74.3
N	6.5	74.1
B.C. N.E. Beulah	6.48	74.07

E. Ch. Beulah

No	7.0	73.6
Ch	6.9	73.7
U	6.9	73.7
C	6.4	74.2
N	6.6	74.0
U	6.5	74.1
So	6.3	74.3

80.55

E¼ Beulah

So			7.3	73.3
ct			7.1	73.5
¼			7.4	73.2
c			7.9	72.7
¼			8.1	72.5
ct			8.4	72.2
No			9.2	71.4

Ctr Beulah

No			11.8	68.8
ct			11.1	69.5
¼			10.3	70.3
c			9.5	71.1
¼			9.3	71.3
ct			8.5	72.1
So			8.4	72.2

W¼ Beulah

So			10.3	70.3
ct			10.8	69.8
¼			11.5	69.1
c			12.3	68.3
¼			13.1	67.5
T.P.	0.92	68.61	12.86	67.69
ct			1.8	66.8
No			2.5	66.1

68.61

Colima

W Ct. Beulah

No			5.8	62.8
ct			5.0	63.6
¼			4.0	64.6
c			3.3	65.3
¼			2.2	66.4
ct			1.5	67.1
So			0.8	67.8

W.L. Beulah #1

So			3.8	64.8
ct			4.7	63.9
¼			5.7	62.9
c			6.4	62.2
¼			7.3	61.3
ct			7.9	60.7
No			9.0	59.6

W.L. Beulah #2 RΔ = 0+0.

No			9.0	59.6
ct			10.1	58.5
¼			10.7	57.9
c			11.3	57.3
¼			12.0	56.6
ct			12.5	56.1
TP	0.50	56.27	12.84	55.77
So			1.2	55.1

56.77

0+25

S.		7.7	48.6
W		7.0	49.3
W		6.7	49.6
C		6.1	√0.2
W		5.5	√0.8
E		4.7	√1.6
N		4.1	√2.2

0+50

N.		11.4	44.9
E		12.2	44.0
W		12.6	43.7
T.P.	0.49	43.91 12.85	43.42
C		1.0	42.9
W		1.8	42.1
W		2.6	41.3
S.		3.0	40.9

0+84

S.		8.4	35.√
E		8.0	35.9
W		7.7	36.2
O		7.5	36.4
W		7.7	36.2
W		7.8	36.1
N		7.5	36.4

43.91

Colima

1+24

N.	9.9	34.0
W	10.1	33.8
W	10.2	33.7
C	10.6	33.3
W	10.7	33.2
W	11.2	32.7
N	11.4	32.√

1+74

S.	12.4	31.√
W	12.2	31.7
W	12.0	31.9
C	11.8	32.1
W	11.5	32.4
W	11.√	32.7
N.	10.9	33.0

2+24

N	11.5	32.4
W	11.6	32.3
W	11.9	32.0
C	12.0	31.9
W	12.3	31.6
E	12.5	31.4
S.	12.7	31.2
T.P.	0.67 32.14	12.44 31.47

32.14

W Ck Hotel

So	3.1	29.0
"	2.9	29.2
W	2.7	29.4
C	2.5	29.6
E	2.3	29.8
"	2.2	29.9
No	2.1	30.0

W.L. Hotel = 0+00

N.	2.2	29.9
"	2.4	29.7
E	2.5	29.6
C	2.6	29.5
W	2.9	29.2
"	3.1	29.0
So	3.4	28.7

0+27

So	3.8	28.3
"	3.6	28.5
W	3.4	28.7
C	3.2	28.9
W	3.1	29.0
"	3.0	29.1
No	2.8	29.3

32.14

Colima

0+42

No	3.1	29.0
"	3.6	28.5
W	3.1	28.5
C	3.0	28.1
E	6.1	26.0
W	3.7	28.4
"	3.9	28.2
So	4.1	28.0

0+44

So	4.0	28.1
"	4.0	28.1
E	4.3	27.8
C	6.1	26.0
W	8.4	23.7
"	5.7	26.4
N.	4.8	27.3

0+59

N.	4.8	27.3
"	8.0	24.1
W	8.7	23.4
C	8.9	23.2
E	7.8	24.3
"	6.2	25.9
So	4.2	27.9

32.14

0+61

So	4.3	27.8
"	6.6	25.5
"	8.3	23.8
C	9.0	23.1
"	8.4	23.7
"	6.0	26.1
No	3.4	28.7

0+71

No	3.6	28.5
+3	5.0	27.1
"	5.0	27.1
"	5.7	26.4
+9	6.6	25.5
C	8.9	
"	10.1	22.0
+4	9.9	22.2
"	6.5	25.6
+5	4.5	27.6
So	4.4	27.7

0+91

So	7.5	24.6
"	7.7	24.4
"	7.8	24.3
+9	8.5	23.6
C	9.4	22.7
+2	12.0	20.1
"	9.6	22.5
"	8.6	23.5
No	9.3	22.8

32.14

Colima

1+10 = West Colima

No	11.9	20.2
"	10.1	22.0
"	11.3	20.8
+4	14.5	17.6
+8	14.4	17.7
C	13.0	19.1
+3	10.4	21.7
"	9.3	22.8
"	9.7	22.4
So	8.8	23.3

Cross Section of Colima St from Oil Blvd to E. line of Sun Ave 12/20/07 Laura Donna Collatto

W.L. Oil Blvd.

	6.72	86.10	79.38
So		6.7	79.4
"		7.0	79.1
"		7.3	78.8
"		7.8	78.3
"		8.5	77.6
Ct		8.6	77.5
So		8.8	77.3
	W. Ct.		
So		9.0	77.1
"		8.7	77.4
"		7.9	78.2
"		7.5	78.6
"		7.1	79.0
"		6.9	79.2
No		6.2	79.9
	W 1/4		
No		6.6	79.5
"		7.0	79.1
"		7.5	78.6
"		8.1	78.0
"		8.6	77.5
Ct		8.9	77.2
So		9.2	76.9

	Ct	
So	9.2	76.9
"	9.0	77.1
"	8.9	77.2
"	8.5	77.6
"	8.0	78.1
"	7.3	78.8
No	6.8	79.3
	E 1/4	
No	6.9	79.2
"	7.5	78.6
"	8.1	78.0
"	8.5	77.6
"	8.8	77.3
"	9.1	77.0
So	9.5	76.6
	E. Ct.	
So	9.7	76.4
"	9.4	76.7
"	9.0	77.1
"	8.4	77.7
"	8.2	77.9
Ct	7.6	78.5
No	6.9	79.2

86.10

E.L. Oil Blvd #1

No	7.4	78.7
"	7.6	78.5
"	8.1	78.0
"	8.6	77.5
"	9.0	77.1
"	9.4	76.7
So	9.7	76.4

E.L. Oil Blvd #2 RD = 0+00

So	9.7	76.4
"	9.3	76.6
"	9.1	77.0
"	8.9	77.2
"	8.7	77.4
"	8.3	77.8
No	7.8	78.3

0+50

No	8.0	78.1
"	8.6	77.5
"	9.2	76.9
"	9.4	76.7
"	9.6	76.5
"	9.7	76.4
So	9.8	76.3

Calimesa

1+00

So	9.3	76.8
"	9.1	77.0
"	8.9	77.2
"	8.7	77.4
"	8.5	77.6
"	8.2	77.9
No	8.2	77.9

1+50

No	7.3	78.8
"	7.6	78.5
"	7.7	78.4
"	8.1	78.0
"	8.2	77.9
"	8.5	77.6
So	8.8	77.3

2+00

So	7.9	78.2
"	7.6	78.9
"	7.4	78.7
"	7.4	78.7
"	7.4	78.7
"	7.2	78.9
No	6.7	79.4

86.10

2+47.72 = W.L. Elect Ave #1 - Rd

No	6.2	79.9
C	6.4	79.7
4	6.5	79.6
C	6.7	79.4
4	6.6	79.5
C	6.9	79.2
So	7.0	79.1

W.L. Elect Ave #2

So	6.6	79.5
C	6.6	79.5
4	6.6	79.5
C	6.5	79.6
4	6.4	79.7
C	6.3	79.8
No	6.2	79.9

W.C.L.

No	6.2	79.9
C	6.2	79.9
4	6.3	79.8
C	6.1	80.0
4	6.3	79.8
C	6.5	79.6
So	6.5	79.6

86.10

Colima

W.L. #1

So	5.2	80.5
C	5.5	80.6
4	5.6	80.5
C	5.9	80.2
4	5.8	80.3
C	5.7	80.4
No	5.6	80.5

W.L. #3 + 41.2 W of Rail

No	3.1	83.0
C	3.2	82.9
4	3.2	82.9
C	3.2	82.9
4	3.2	82.9
C	3.1	83.0
So	3.1	83.0

Ctr = Top Rail

So	2.51	83.59
Ctr	2.46	83.64
No	2.40	83.70

W.L. #2 + 51.5 = 2' E of Rail

So	3.2	82.9
C	3.2	82.9
4	3.2	82.9
C	3.2	82.9
4	3.2	82.9
C	3.1	83.0
No	3.0	83.1

86.10

E ¼ Elect. Ave

No	3.9	82.2
U	4.0	82.1
U	4.1	82.0
C	4.1	82.0
U	3.9	82.2
U	4.0	82.1
So	4.1	82.0

E. Ch.

So	4.1	82.0
U	4.0	82.1
U	3.7	82.4
C	3.6	82.5
U	3.7	82.4
U	3.7	82.4
No	3.4	82.7

E. Lima Elect Ave #1

No	3.0	83.1
Ch	3.1	83.0
U	3.1	83.0
C	3.2	82.9
U	3.3	82.8
U	3.5	82.6
So	3.5	82.6

B.M. N.E Elect Ave 2.97 83.13

Colima.

E.L #2 : RA = 0+00

So	3.5	82.6
	3.4	82.7
U	4.1	82.0
U	3.0	83.1
C	2.6	83.5
U	2.7	83.4
	3.2	82.9
U	2.5	83.6
No	2.2	83.9

0+50

No	1.1	85.0
	1.2	84.9
Ch	1.9	84.2
U	1.1	85.0
C	0.9	85.2
U	1.5	84.6
	2.2	83.7
	1.6	84.5
U	1.7	84.4
So	2.0	84.1

TP 11.98 97.86 0.22 85.99

1+00

So	12.1	85.8
	12.0	85.9
U	12.7	85.2
U	11.8	86.1
C	11.5	86.4
U	11.6	86.3
	11.9	86.0
U	11.4	86.5
No	11.1	86.8

97.86

1 + 50

No	9.4	88.5
cb	9.6 10.3	88.3 87.6
¼	9.6	88.3
c	9.4	88.5
¼	10.3	87.6
cb	11.2 10.6	86.7 87.3
So	10.4	87.5

2 + 00

So	8.7	89.2
cb	8.4 9.0	89.5 88.9
¼	8.2	89.7
c	7.7	90.2
¼	7.9	90.0
cb	8.5 7.7	89.4 90.2
No	7.7	90.2

2 + 32.18 W.L. Dodge #1 · Ra

No	6.5	91.4
cb	6.8 7.2	91.1 90.7
¼	6.8	91.1
c	6.3	91.6
¼	6.8	91.1
cb	7.6 7.0	90.3 90.9
So	7.5	90.4

Colima

97.86

W.L. Dodge #2

So	6.2	91.7
cb	6.4 6.9	91.5 91.0
¼	6.2	91.7
c	5.9	92.0
¼	6.3	91.6
cb	7.0 6.4	90.9 91.5
No	6.5	91.4

W. Cb

No	6.2 Gutr 6.5	91.7 91.4
cb	6.1 Gutr 6.5	91.8 91.4
¼	5.8	92.1
c	5.7	92.2
¼	5.6 Gutr 6.2	92.3 91.7
cb	5.8	92.1
So	5.7 Gutr 6.2	92.2

W ¼

So	5.0	92.9
cb	5.2 5.8	92.7 92.1
¼	5.1	92.8
c	5.2	92.7
¼	5.4	92.5
cb	6.1	91.8
No	5.9	92.0

POSTED

97.86

Ctr Dodge

N.	4.9	93.0
"	5.3	92.6
"	5.0	92.9
E	4.6	93.3
"	4.9	93.0
"	5.2	92.7
S.	4.6	93.3

E ¼

S.	4.1	93.8
"	4.8	93.1
"	4.1	93.8
E	4.3	93.6
"	4.4	93.5
"	4.3	93.6
N.	5.1	92.8

E. Ctr.

N.	4.2	93.7
	Contr 4.8	93.1
Ctr	4.2	93.7
	Contr 4.1	93.7
"	4.2	93.7
E	3.7	94.2
"	3.8	94.1
	Contr 4.6	93.3
Ctr	3.9	94.0
	3.5	94.4
S.	Contr 4.2	93.7

Colima

E. line Dodge #1

S.	3.1	94.8
"	3.4	94.5
	4.1	93.8
"	3.3	94.6
E	2.9	95.0
"	3.6	94.3
"	4.6	93.3
	3.9	94.0
N.	3.6	94.3

B.M. N.E. Dodge 3.65 — POSTED 94.21

E.L. Dodge - RA = 0+00

N.	2.5	95.4
"	2.6	95.3
	3.3	94.6
"	2.6	95.3
E	2.5	95.4
"	2.9	95.0
"	4.0	93.9
	3.1	94.8
S.	3.1	94.8

0 + 50

S.	1.2	96.7
"	1.0	96.9
	1.4	96.5
"	0.6	97.3
E	+0.1	98.0
"	0.2	97.7
"	0.8	97.1
	0.0	97.9
N.	0.0	97.9

TP	11.71	108.88	0.69	97.17
		1+00		
No			8.9	100.0
Ch			9.4	99.5
			10.2	98.7
4			9.4	99.5
C			9.1	99.8
4			9.7	99.2
Ch			10.5	98.4
			9.7	99.2
So			9.9	99.0
		1+50		
So			8.1	100.8
Ch			8.0	100.9
			8.7	100.2
4			7.9	101.0
C			7.6	101.3
4			7.7	101.2
Ch			8.6	100.3
+2			7.5	101.4
No			7.4	101.5
		2+00		
No			6.1	102.8
Ch			6.1	102.8
			6.9	102.0
4			5.7	103.2
C			5.6	103.3
4			5.6	103.3
Ch			6.8	102.1
			5.9	103.0
So			6.0	102.9

Colvina

42

2+32.18 = Rd. W.L. Burke #1

So	4.7	104.2
Ch	4.7	104.2
	5.3	103.4
4	4.8	1044
C	4.2	1047
4	4.5	1044
Ch	5.5	103.4
	4.7	104.2
No	4.8	104.1
W.L. #2		
No	4.8	104.1
Ch	4.4	104.5
	5.1	103.8
4	3.9	105.0
C	3.9	105.0
4	3.9	105.0
Ch	4.6	104.3
	4.0	104.9
So	3.9	105.0
W. Ch.		
So	8.5	105.4
Contr	4.4	104.5
Ch	3.7	105.2
Contr	4.3	104.6
4	3.5	105.4
C	3.5	1054
4	3.5	105.4
Guth	4.6	104.3
Ch	3.9	105.0
	4.2	104.6
Contr	5.2	103.7

108.88

N¼ Burke

No		3.6	105.3
		3.4	105.4
U	Gutr.	4.0	104.9
¼		2.9	106.0
C		2.8	106.1
¼		3.2	105.7
U		3.8	105.1
So		3.0	105.9

Ctr

So		2.2	106.7
		2.4	106.5
U		3.5	105.4
¼		2.5	106.4
C		2.5	106.4
¼		2.5	1064
CL	Gutr.	3.5	105.4
		3.1	105.8
No		2.8	106.1

E¼

No		2.9	106.0
U		3.0	105.9
¼		2.1	106.8
C		1.9	107.0
¼		2.2	106.7
U		2.5	106.4
So		2.2	106.7

Colma

E. Ct.

So		1.8	107.1
	Gutr.	3.6	106.3
U		2.0	106.9
	"	2.4	106.5
¼		1.8	107.1
C		1.7	107.2
¼		2.0	1069
	Gutr.	2.7	106.2
U		2.0	1069
No		2.3	106.6
	"	3.0	105.9

B.M. N.E Burke 1.62 107.26

E.L. Burke #1

No		1.6	107.3
		1.6	107.3
CL		2.1	106.8
¼		1.2	107.7
C		1.1	107.8
¼		1.1	1078
		1.8	107.1
CL		1.4	107.5
So		1.2	107.7

E.L #2 RP = 0+00

So		1.7	107.7
		1.0	107.9
CL		1.6	107.3
¼		0.4	108.5
C		0.1	108.8
¼		0.4	108.5
U		1.1	107.8
		0.4	108.5
No		0.2	108.7

T.P. 17.61 121.36 0.13 108.75

121.36

0+50

N.	10.1	111.3
	10.4	111.0
W	11.1	110.3
W	10.5	110.9
W	10.4	111.0
W	10.5	110.9
	11.3	110.1
W	10.4	111.0
S.	10.3	111.1

1+00

S.	8.1	113.3
	8.4	113.0
W	8.9	112.5
W	8.3	113.1
W	8.2	113.2
W	8.2	113.2
	9.4	112.0
W	8.8	112.6
	8.7	112.7
N.	9.3	112.1

1+50

N.	7.2	114.2
	6.7	114.7
W	7.2	114.2
W	6.4	115.0
W	6.1	115.3
W	6.2	115.2
	6.8	114.6
W	6.0	115.4
S.	6.1	115.3

121.36

Colima

44

2+00

S.	3.8	117.6
	3.6	117.8
W	4.2	117.2
W	3.7	117.7
W	3.7	117.7
W	4.1	117.3
	4.8	116.6
W	4.2	117.2
N.	4.3	117.1

2+37.18 - W.L. Hodgman #1 = RP

N.	2.3	119.1
	2.3	119.1
W	2.9	118.5
W	2.1	119.3
W	1.8	119.6
W	2.1	119.3
	2.6	118.8
W	2.1	119.3
S.	2.1	1193

TP 121.71 133.08 0.49 120.87

W.L #2

S.	11.4	121.7
	12.1	121.0
W	12.6	120.5
W	12.3	120.8
W	12.4	120.7
W	13.2	119.9
	14.3	118.8
W	13.6	119.5
N.	14.1	11

VBM N.E Hodgman 8.97 124.11 124.1

133.08

W. Ck. Hodgman

No		13.2	119.9
	Gutr	13.7	119.4
"		13.9	120.2
	"	13.3	119.8
"		12.4	120.7
"		11.8	121.3
"		11.7	121.4
"		11.7	121.4
	Gutr	11.4	121.7
So		10.7	122.4
	"	11.2	121.9

XV 1/4

So	10.2	122.9
"	10.5	122.6
"	10.8	122.3
"	11.1	122.0
"	11.7	121.4
"	12.2	120.9
No	12.5	120.6

Ctr.

No	11.6	121.5
"	11.6	121.5
"	11.2	121.9
"	10.5	122.6
"	10.1	123.0
"	9.7	123.4
So	9.2	123.9

133.08

45

Colma

E 1/4

So	8.9	124.2
"	9.3	123.8
"	9.6	123.5
"	9.9	123.2
"	10.5	122.6
"	10.7	122.4
No	10.9	122.2

E Ck.

	10.1	123.0
No	10.8	122.3
	9.9	123.2
"	10.3	122.8
"	9.7	123.4
"	9.2	123.7
"	9.0	124.1
"	8.7	124.4
So	8.2	124.9

E. line #1

So	7.7	125.4
	8.0	125.1
"	8.3	124.8
"	8.3	124.8
"	8.3	124.8
"	9.0	124.1
	9.7	123.4
"	9.0	124.1
No	9.0	124.1

POSTED

133.08

E.L. Hodgman #2 = RΔ = 0+00

N.			7.0	126.1
"			7.3	125.8
			7.8	125.3
"			7.2	125.9
"			7.0	126.1
"			7.5	125.6
"			8.1	125.0
			7.7	125.4
S.			7.7	125.4
		0+50		
S.			4.5	128.6
"			4.1	129.0
			4.9	128.2
"			3.5	129.6
"			3.3	129.8
"			3.3	129.8
"			4.0	129.1
			3.1	129.0
N.			3.0	130.4
TP	12.62	144.29	1.41	131.67
		1+00		
N.			10.4	133.9
"			10.8	133.5
			11.5	132.8
"			11.2	133.1
"			11.4	132.9
"			11.9	132.4
"			12.8	131.5
			12.4	131.9
S.			12.7	131.6

144.29

Colima

1+50

S.			8.7	135.6
"			8.3	136.0
			8.9	135.4
"			7.9	136.4
"			7.2	137.1
"			7.2	137.1
"			7.4	136.9
			6.7	137.6
N.			6.1	138.2
		2+00		
N.			1.6	142.7
"			1.8	142.5
			2.7	141.6
"			2.8	141.5
"			3.1	141.2
"			3.9	140.4
"			4.8	139.5
			4.4	139.9
S.			4.5	139.8
		2+32.18 = RΔ = W.L. Taft #1		
S.			1.5	142.8
"			1.3	143.0
			2.7	141.6
"			0.8	143.5
"			0.4	143.9
"			0.4	143.9
"			0.6	143.7
			0.0	144.3
N.			+0.1	144.4
TP	12.54	156.63	0.20	144.09

156.63

W. L. Taft #2

No	12.3	144.3
4+2	12.1	144.5
4	12.5	144.1
4	11.8	144.8
c	11.3	145.3
4	11.2	145.4
u	11.9	144.7
	11.3	145.3
So	11.0	145.6

W. Ch

So	10.0	146.6
ch	10.4	146.2
	10.7	145.9
4	10.3	146.3
c	10.5	146.1
4	10.7	145.9
u	11.7	144.9
	11.3	145.3
No	11.6	145.0
Cour	11.9	144.7

W 1/4

No	10.6	146.0
ch	10.3	146.3
4	9.7	146.9
c	9.3	147.3
4	9.3	147.3
u	10.1	146.5
	9.4	147.2
So	9.3	147.3

B.M. N.W. Taft. 13.27 144.36

Colima

C 1/4

47

So	8.7	147.9
	8.7	147.9
ch	9.3	147.3
4	8.4	148.2
c	8.3	148.3
4	8.4	148.2
+9	9.3	147.3
u	8.8	147.8
No	8.9	147.7

POSTED

E 1/4

No	8.1	148.5
ch	7.9	148.7
+4	8.3	148.3
4	7.4	149.2
c	7.3	149.3
u	7.7	148.9
	8.7	147.9
ch	7.9	148.7
So	8.0	148.6

E ch

So	7.3	149.3
+9	7.3	149.3
ch	7.8	148.8
4	7.0	149.6
c	6.5	150.1
4	6.6	150.0
+8	7.8	148.8
u	7.7	148.9
	7.1	149.5
No	7.3	149.3

1962.63

Eline Taft #1

No	6.6	1962.0
	6.3	1962.3
Ut	7.0	1496
+6	6.7	149.9
4	6.0	1962.6
C	5.9	1962.7
4	6.4	1962.2
Ut	7.1	149.96
+5	6.2	1962.4
So	6.4	1962.2

Eline #2 - RA = 0+00

So	6.4	1962.2
+7	6.3	1962.3
Ut	7.0	149.6
4	6.6	1961.0
C	5.2	1961.4
4	4.8	1961.8
+5	5.5	1961.1
Ut	5.5	1961.1
	4.4	1962.2
No	4.2	1962.4

0+50

No	1.6	1965.0
Ut	2.5	1964.1
4	2.7	1963.9
C	2.9	1963.7
4	3.2	1963.4
Ut	4.1	1962.5
+8	3.5	1963.1
So	4.0	1962.6

1962.63

Colima

0+696 RA = W.L. Crocker #1

So	3.5	1963.1
+7	2.9	1963.7
Ut	3.7	1962.9
+4	3.6	1963.0
4	2.6	1964.0
C	2.0	1964.6
4	2.0	1964.6
Ut	1.6	1965.0
No	0.9	1965.7

W.L. Crocker #2

No	0.9	1965.7
Ut	1.3	1965.3
+3	1.8	1964.8
4	1.5	1965.1
C	1.5	1965.1
4	1.6	1965.0
Ut	1.7	1964.9
+6	1.2	1965.4
So	2.0	1964.6

TP 12.54 167.96 1.21 1955.42

W. CA

So	12.5	1955.5
Ut	12.8	1955.2
4	12.4	1955.6
C	12.3	1955.7
Ut	12.5	1955.5
+10	12.3	1955.7
4	11.7	1956.3
No	11.9	1956.1

167.96

W ¼ Crocker

No.	11.1	1V6.9
	11.1	1V6.9
¼	11.9	1V6.1
¼	11.9	1V6.1
C	11.8	1V6.2
¼	11.9	1V6.1
¼	12.2	1V5.8
So.	11.6	1V6.4

C ¼

So.	11.1	1V6.9
¼	11.7	1V6.3
¼	11.5	1V6.5
C	11.2	1V6.8
¼	11.6	1V6.4
¼	11.4	1V6.6
	10.6	1V7.4
No.	10.2	1V7.8

E ¼

No.	10.1	1V7.9
+a	10.4	1V7.6
¼	10.9	1V7.1
¼	10.8	1V7.2
C	10.6	1V7.4
¼	10.6	1V7.4
¼	10.8	1V7.2
So.	10.6	1V7.4

Colima E Ct.

So.	10.0	1V8.0
¼	10.4	1V7.6
¼	10.0	1V8.0
C	10.1	1V7.9
¼	10.2	1V7.8
¼	10.0	1V8.0
No.	9.6	1V8.4

E. line Crocker #1

No.	8.9	1V9.1
¼	9.3	1V8.7
¼	9.6	1V8.4
C	9.3	1V8.7
¼	9.2	1V8.8
¼	9.3	1V8.7
So.	9.1	1V8.9

E.L. Crocker #2 Ra=0+00

So.	9.1	1V8.9
¼	8.6	1V9.4
¼	8.6	1V9.4
C	8.5	1V9.5
¼	8.3	1V9.7
¼	8.1	1V9.9
+7	7.7	160.3
No.	8.3	1V9.7

167.96

0+28

No	9.8	158.2
+5	6.4	161.6
4	6.3	161.7
4	6.5	161.5
c	6.5	161.5
4	6.9	161.1
4	6.6	1614
So	5.9	162.1

0+57.8 - W.L. Sum #1 - R4

So	3.4	164.6
4	3.3	164.7
4	3.8	164.2
c	3.4	164.6
4	3.8	164.2
4	3.7	1643
+6	3.5	164.5
No	6.6	161.5

W.L. Sum #2

No	6.6	161.5
+4	3.5	164.5
4	3.2	164.8
4	2.9	165.1
c	2.2	165.8
4	2.6	165.4
+8	2.5	165.5
4	1.9	166.1
So	1.3	166.7

Colma

W. Ck

So	0.8	167.2
	1.4	166.6
4	1.8	166.2
4	2.0	166.0
c	1.6	1664
4	2.0	166.0
4	2.0	166.0
+8	2.7	165.3
No	3.6	1644

W 1/4

No	1.7	1663
+2	1.0	167.0
4	1.0	167.0
4	1.2	166.8
c	1.1	166.9
4	1.5	166.5
+8	1.7	166.3
4	1.1	166.9
So	0.7	167.3

TP 39+ 171.80 0.10 167.86

Ctr

So	4.2	167.6
	4.4	167.4
4	5.0	166.8
4	5.1	166.7
c	4.2	167.6
4	4.3	167.5
+10	4.4	167.4
4	4.0	167.8
No	3.3	168.5

171.80

E ¼ Sum

No	3.3	168.5
ch	3.4	168.4
	3.9	167.9
¼	3.6	168.2
c	3.8	168.0
¼	4.6	167.2
	4.5	167.3
ch	3.8	168.0
So	3.7	168.1

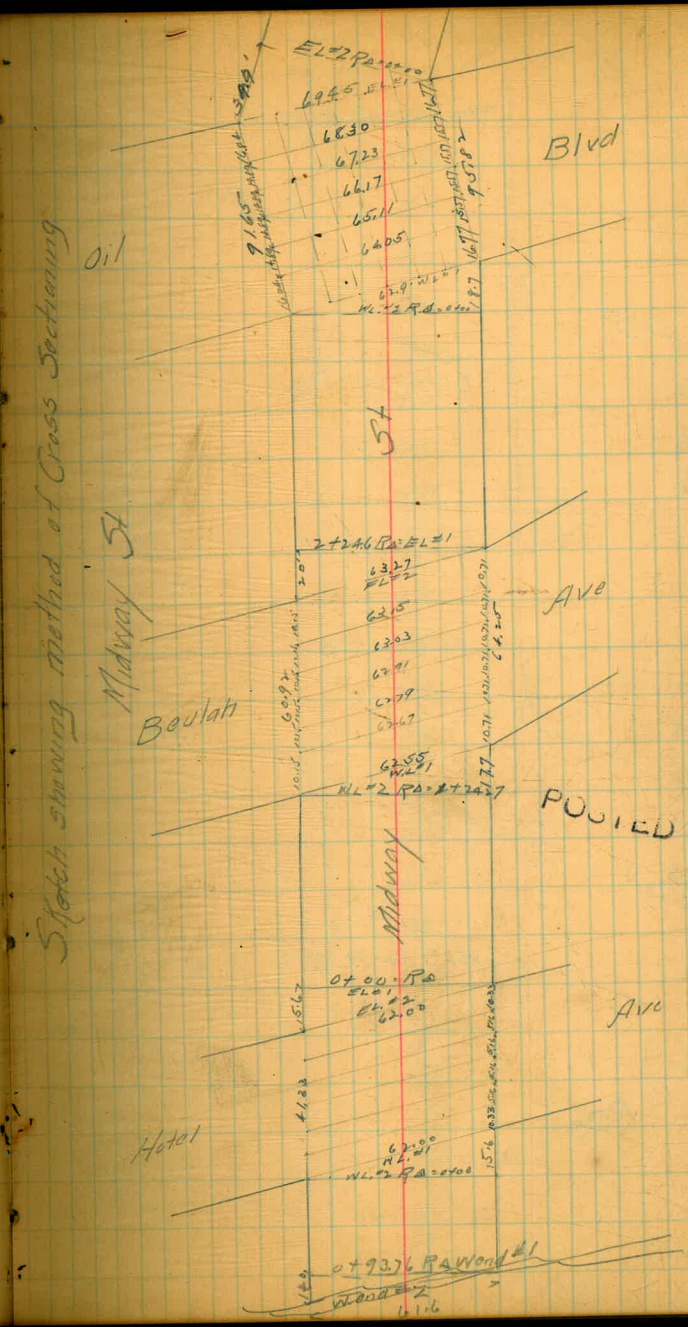
E ch

S.	3.1	168.7
ch	3.8	168.0
¼	3.6	168.2
c	3.1	168.7
¼	3.1	168.7
ch	3.3	168.5
+4	2.9	168.9
No	3.0	168.8

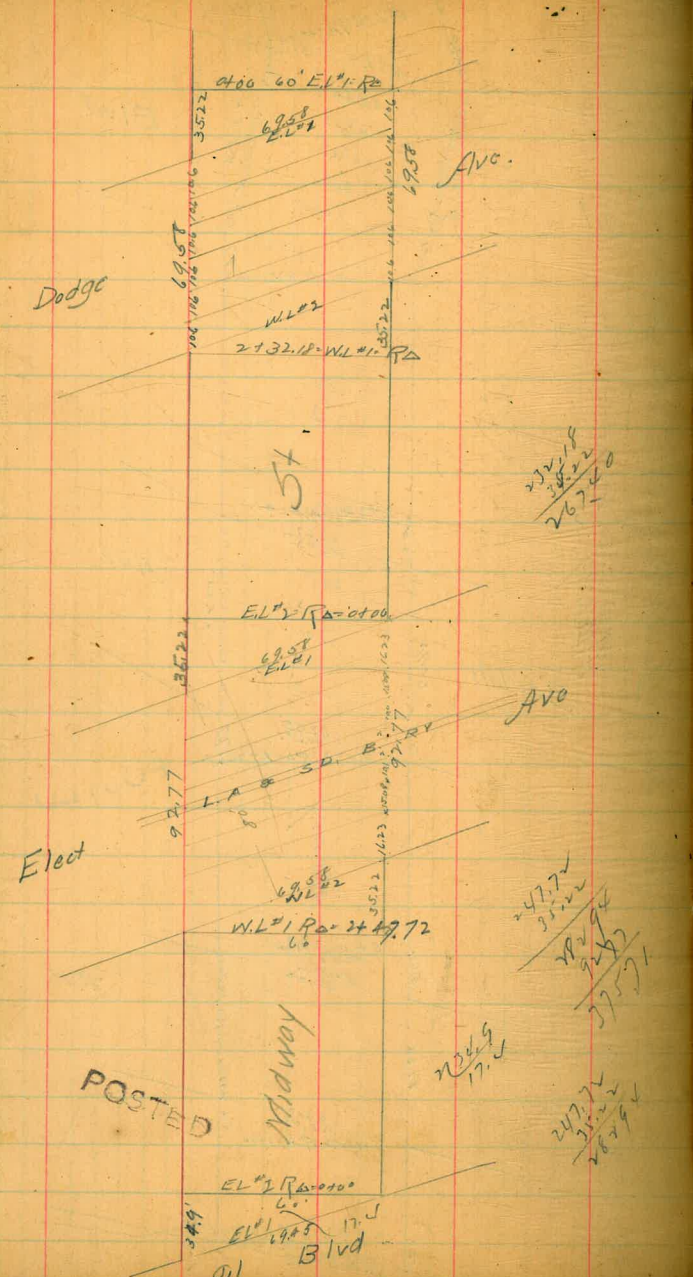
E. line of Sum

No	2.4	169.4
+8	2.3	169.5
ch	2.9	168.9
¼	2.4	169.4
c	2.7	169.1
¼	3.6	168.2
ch	3.3	168.5
So	3.0	168.8
B.M. S.E Sum	2.91	168.89

Sketch showing method of Cross Sectioning



Note- All intersections east of and including Dodge are the same.



Cross-Section of Midway St from W.L. Oil Blvd. to West end of St 12/20/07 {Davis Donnan Colton

W.L. Oil Blvd #1

	0.95	70.95	Oil Blvd 70.00 B.M.
So		4.0	67.0
cl		4.6	66.4
¼		4.5	66.5
c		4.4	66.6
¼		4.1	66.9
cl		4.0	67.0
No		3.9	67.1

W.L. Oil Blvd #2 RΔ = 0+00

No		3.9	67.1
cl		4.2	66.8
¼		4.6	66.4
c		4.8	66.2
¼		5.0	66.0
cl		5.3	65.7
So		5.2	65.8

0+25

So		6.2	64.8
cl		6.2	64.8
¼		6.3	64.7
c		6.2	64.8
¼		5.9	65.1
cl		5.6	65.4
No		5.2	65.8

PC

70.95

0+75

No		8.1	62.9
U		8.6	62.4
U		9.0	62.0
C		9.2	61.8
U		9.2	61.8
U		9.2	61.8
So		9.3	61.7

1+25

So		12.2	√8.8
U		12.4	√8.6
U		12.3	√8.7
C		12.2	√8.8
U		11.9	√9.1
U		11.3	√9.7
No		11.1	√9.9
T.R.	0.24	58.25	12.94	58.01

1+75

No		1.6	√6.7
U		2.5	√√.8
U		3.3	√√.0
C		3.4	√4.9
U		3.2	√√.1
U		3.0	√√.3
So		2.8	√√.√

POSTED

Midway √8.2√

2+246 = E.L. Bevlab #1 Rd

So	5.9	√2.4
U	6.1	√2.2
U	6.1	√2.2
C	6.0	√2.3
U	5.4	√2.9
U	4.7	√3.6
No	4.1	√4.2

E.L. 4.2

No	4.8	√3.√
U	5.4	√2.9
U	6.1	√2.2
U	6.6	√1.7
U	6.4	√1.9
U	6.3	√2.0
So	5.9	√2.4

E U

So	6.5	√1.8
U	6.8	√1.√
U	6.9	√1.4
C	7.2	√1.1
U	6.9	√1.√
U	6.4	√1.9
No	4.9	√3.4

POSTED

58.26

E¼ Beulah

No	57	√3.1
4	6.7	√1.6
4	7.6	√0.7
C	7.6	√0.7
¼	7.3	√1.0
4	7.3	√1.0
So	7.0	√1.3

Ctr

So	7.5	√0.8
4	7.7	√0.6
¼	7.9	√0.4
C	7.9	√0.4
¼	8.0	√0.3
4	7.1	√1.2
No	56	√2.7

W¼

No	5.7	√2.6
4	7.6	√0.7
¼	8.5	49.8
C	84	49.9
¼	8.3	√0.0
4	8.2	√0.1
So	8.1	√0.2

POST-D

√8.2√

Midway

W. Ctr.

So	8.7	49.6
4	8.5	49.√
¼	9.0	49.3
C	8.8	49√
¼	8.8	49.√
4	7.8	√0.√
No	6.0	√2.3

W. line Beulah #1

No	6.6	×57.7
4	8.4	49.9
¼	9.6	48.7
C	9.5	48.8
¼	9.4	48.9
4	9.5	49.0
So	9.3	49.0

BM. S.W. Beulah 9.26 48.99

115 So. 14 48.99

W.L #2 R.A. 1+24.7

So	2.1	48.0
4	2.1	48.0
¼	2.0	48.1
C	1.8	48.3
¼	1.7	48.4
4	0.4	49.7
No	+ 1.6	×51.7

POST-

50.14

1+00

No.	0.4	49.7
W	2.2	47.9
W	2.8	47.3
0	3.3	46.8
4	3.3	46.8
W	3.3	46.8
So	3.2	46.9

2+50

S.	5.6	44.5
W	5.4	44.7
W	5.3	44.8
C	5.2	44.9
W	5.5	44.6
W	4.9	45.2
No.	3.7	46.4

0+00 - EL. Hotel Pl. RD

No.	8.0	42.1
W	8.0	42.1
4	8.0	42.1
C	8.0	42.1
W	8.0	42.1
W	8.0	42.1
S.	8.1	42.0

Midway

E.L. 2

S.	8.1	42.0
W	8.1	42.0
4	8.2	41.9
C	8.5	41.6
W	8.7	414
W	8.7	414
No.	8.7	414

E. Ct

No.	9.4	40.7
W	9.4	40.7
W	9.3	40.8
C	9.1	41.0
4	9.0	41.1
W	8.8	41.3
So	8.7	41.4

E. 4

S.	9.0	41.1
W	9.1	41.0
W	9.2	40.9
C	9.4	40.7
W	9.6	40.5
W	9.6	40.5
No.	9.6	40.5

POSTED

50.14

Ctr Hotel Ave

No	9.9	40.2
Cl	9.8	40.3
4	9.8	40.3
C	9.6	40.5
4	9.5	40.6
Cl	9.4	40.7
So	9.3	40.8

W 1/4

So	9.6	40.5
Cl	9.7	40.4
4	9.9	40.2
C	10.0	40.1
4	10.1	40.0
Cl	10.1	40.0
No	10.2	39.9

Wd

No	10.5	39.6
Cl	10.5	39.6
4	10.4	39.7
C	10.2	39.9
4	10.2	39.9
Cl	10.0	40.1
So	9.9	40.2

USTL

50.14

Midway

W.L Hotel #1

So	10.3	39.8
Cl	10.4	39.7
4	10.4	39.7
C	10.6	39.5
4	10.8	39.3
Cl	11.1	39.0
No	11.2	38.9

T.P. 0.23 39.17 11.20 BM N.W Hotel 38.94

W.L #2 - R 0+00

No	0.2	39.0
Cl	0.2	39.0
4	0.1	39.1
C	0.1	39.1
4	0.0	39.2
Cl	0.0	39.2
So	0.0	39.2

0+31

So	1.5	37.7
Cl	1.5	37.7
4	1.4	37.8
C	1.4	37.8
4	1.4	37.8
Cl	1.3	37.9
No	1.5	37.7

PL

39.17

0+43

No	2.2	37.0
+8	2.5	36.7
+7	4.3	32.9
U	6.4	32.8
U	4.6	34.6
+4	3.5	35.7
+5	1.9	37.3
C	1.9	37.3
U	1.9	37.3
+2	2.1	37.1
+0	3.9	35.3
U	4.6	34.6
+8	3.9	35.3
So	2.4	36.8

0+60

So	7.7	31.5
+6	11.9	28.3
U	8.1	31.1
+3	9.7	29.5
U	2.6	36.6
C	2.6	36.7
U	2.9	36.3
U	8.3	30.9
+2	9.1	29.6
No	9.6	29.6

0+93.76 = W. End of 51st Pl RD

No	10.7	28.5
U	10.8	28.4
U	10.7	28.5
C	10.6	28.6
U	10.1	29.1
U	10.8	28.4
So	14.5	24.7

POSTED

Midway

W. End of 51st Pl

58

So	14.5	24.7
U	11.5	27.7
U	9.8	29.4
+8	9.6	29.6
C	10.5	28.7
+5	12.5	26.7
U	11.5	27.7
+8	11.7	27.5
U	15.4	23.8
No	20.0	19.2

POSTED

Cross. Section of Midway W.L. Oil Blvd. to Sun Ave 12/21/07 {Davis, Donnan, Coltrath

8.03 7.8.03 70.00 B.M.

W.L. Oil Blvd.

So	11.1	66.9
4	11.7	66.3
4	11.5	66.5
C	11.4	66.6
4	11.2	66.8
4	11.1	66.9
No	11.0	67.0

W Ct

No	10.2	67.8
4	10.4	67.6
4	10.5	67.5
C	10.7	67.3
4	10.9	67.1
4	10.4	67.6
So	10.3	67.7

W 1/4

So	9.4	68.6
4	9.5	68.5
4	9.4	68.6
C	9.4	68.6
4	9.5	68.5
4	9.5	68.5
No	9.4	68.6

POSTED

Ctr

No	9.2	68.8
4	9.3	68.7
4	9.2	68.8
C	9.2	68.8
4	9.1	68.9
4	9.0	69.0
So	9.0	69.0

E 1/4

So	7.8	70.2
4	8.0	70.0
4	8.3	69.7
C	8.3	69.7
4	8.2	69.8
4	8.2	69.8
No	8.2	69.8

E. Ct

No	7.9	70.1
4	7.9	70.1
4	8.0	70.0
C	7.9	70.1
4	7.9	70.1
4	7.6	70.4
So	7.5	70.5

POSTED

78.03

E.L. Oil Blvd #1

So.	6.7	71.3
"	7.0	71.0
"	7.2	70.8
"	7.2	71.8
"	7.3	70.7
"	7.3	70.7
No.	7.2	71.8

EL #2 RD = 0+00

No.	5.7	72.3
"	5.9	72.1
"	6.2	71.8
"	6.5	71.5
"	6.7	71.3
"	6.7	71.3
So	6.7	71.3

0+50

So	4.6	73.4
"	4.5	73.5
"	4.2	73.8
"	4.0	74.0
"	4.0	74.0
"	4.1	73.9
No.	3.8	74.2

Midway

1+00

No.	1.3	76.7
"	1.6	76.4
"	2.0	76.0
"	2.2	75.8
"	2.6	75.4
"	2.8	75.2
So	3.0	75.0

TP 11.94 89.02 0.95 77.08

1+50

So.	11.9	77.1
"	11.7	77.3
"	11.6	77.4
"	11.2	77.8
"	11.0	78.0
"	10.6	78.4
No.	10.3	78.7

2+00

No.	8.x	80.8
"	8.7	80.3
"	9.1	79.9
"	9.0	80.0
"	9.3	79.7
"	9.5	79.5
So	9.7	79.3

89.02

2+47.72 W.L. Elect Ave #1 Rail

So	8.2	80.8
Ch	8.0	81.0
4	7.9	81.1
C	7.9	81.1
4	7.6	81.4
W	7.3	81.7
N.	6.9	82.1

WL # 1

No	6.9	82.1
Ch	7.0	82.0
W	7.1	81.9
C	6.9	82.1
4	6.9	82.1
Ch	6.8	82.2
So	6.7	82.3

W Ch

So	6.0	83.0
Ch	6.1	82.9
4	6.1	82.9
C	6.1	82.9
W	6.1	82.9
Ch	6.3	82.7
N.	6.1	82.9

Midway

W 4

61

N.	5.4	83.6
Ch	5.7	83.3
4	6.0	83.0
C	5.6	83.4
4	5.7	83.3
W	5.9	83.1
So	5.6	83.4

WL # 2 + 41.4 = 2' W of Rail

So	3.3	85.7
Ch	3.4	85.6
W	3.3	85.7
C	3.3	85.7
4	3.1	85.9
Ch	3.1	85.9
No	3.0	86.0

POSTED

Ctr = Top Rail

So	2.79	86.20
Ctr	2.56	86.46
No	2.42	86.60

WL # 2 + 51.5 = 2' E of Rail

No	2.8	86.8
Ch	3.0	86.0
4	3.1	85.9
C	3.2	85.8
4	3.3	85.7
W	3.4	85.6
So	3.5	85.5

8902

E ¼ Elect. Ave

So.		3.0	86.0
Ch		3.2	85.8
"		2.5	86.5
"		2.2	86.8
"		2.3	86.7
"		2.3	86.7
No.		2.7	86.3

E Ch.

No.		1.9	87.1
"		2.1	86.9
"		2.1	86.9
"		1.9	87.1
"		2.1	86.9
"		3.0 / 3.5	86.0 / 86.6
So.		2.6	86.4

E.L # 1

So.		2.4	86.6
"		2.3 / 3.0	86.7 / 86.0
"		1.8	87.2
"		1.7	87.3
"		1.8	87.2
"		2.5 / 1.6	86.5 / 87.4
No.		1.4	87.6

POSTED

11.23 98.77 1.38 B.M. N.E. Elect 87.64

Midway

E.L Elect Ave ℄ R△=0+00

No.	10.6	88.4
"	10.9 / 11.6	89.1 / 87.4
"	11.2	87.8
"	11.1	87.9
"	11.7	87.3
"	12.8 / 12.0	86.2 / 87.0
So.	12.3	86.7

0+50

So.	11.4	87.6
"	11.1 / 11.7	87.9 / 87.3
"	10.6	88.4
"	9.8	89.2
"	9.9	89.1
"	10.3 / 9.6	88.7 / 89.4
No.	9.3	89.7

1+00

No.	7.7	91.3
"	8.0 / 8.8	91.0 / 90.2
"	8.3	90.7
"	8.3	90.7
"	8.8	90.2
"	10.0 / 9.4	89.0 / 89.6
So.	9.5	89.5

98.97

99°

1+50

S.	7.6	91.4
	7.4	91.6
W	8.1	90.9
W	6.9	92.1
C	6.3	92.7
W	6.2	92.7
W	6.8	92.2
	6.1	92.9
NW	5.6	93.4

2+00

N.	3.3	95.7
W	3.7	95.3
	4.6	94.4
W	3.9	95.1
C	3.7	95.3
W	4.2	94.8
W	5.6	93.4
	4.9	94.1
S.	5.3	93.7

2+33.1 P. W.L. Dodge #1 RP

S.	3.8	95.2
W	3.7	95.3
	4.1	94.9
W	2.9	96.1
C	2.3	96.7
W	2.4	96.6
W	3.1	95.9
	2.3	96.7
NW	2.2	96.8

Midway

W.L. Dodge #2

63

NW	2.2	96.8
W	2.0	97.0
	2.6	96.4
W	2.0	97.0
C	1.5	97.5
W	1.9	97.1
W	3.2	95.8
	2.3	96.7
SW	2.6	96.4

12 11 108.45

B.M. S.W. Dodge 2.63 96.34

W ch 108.5

	11.7	
S. Gutter	12.3	96.8
		96.2
"	11.9	96.6
	12.1	96.4
W	11.2	97.3
C	10.7	97.8
W	10.9	97.6
W	11.6	96.9
		97.4
NW Gutter	11.1	97.7
	11.4	

NW 1/4 108.5

NW	10.3	98.2
	10.8	97.7
	11.1	97.4
W	10.4	98.1
C	10.2	98.3
W	10.4	98.1
	11.4	97.1
W	11.0	97.5
SW	11.1	97.4

POSTED

108.45

Ctr Dodge

1085

So	10.8	97.7
ct	10.9	97.6
4	10.3	98.2
c	9.7	98.8
4	10.0	98.5
ct	10.6	97.9
+3	10.0	98.5
No	9.4	99.1

E 1/4

No	9.5	99.0
ct	10.0	98.5
4	9.7	98.8
c	9.6	98.9
4	10.0	98.5
ct	10.6	97.9
So	10.6	97.9

E ct.

So	10.3	98.2
ct	10.1 10.3	98.4 98.2
4	9.4	99.1
c	8.9	99.5
4	9.2	99.3
+8	9.6	98.9
ct	8.7	99.8
No	8.7	99.8

Midway

E. line Dodge #1

No	8.0	100.5
ct	8.2 9.0	100.3 99.5
4	8.7	99.8
c	8.6	99.9
4	9.0	99.5
ct	10.0	98.5
So	10.1	98.4

E.L. Dodge #2 - RD = 0+00

So	10.1	98.4
ct	9.6 10.0	98.9 98.5
4	8.8	99.7
c	8.0	100.5
4	7.9	100.6
ct	8.2 7.2	100.3 101.3
No	6.6	101.9

0+50

No	6.2	102.3
ct	6.8 7.5	101.7 101.0
4	6.5	102.0
c	6.8	101.7
4	7.4	101.1
ct	8.5	100.0
So	8.6	99.9

POSTED

108.45

1+00

So			6.9	101.6
Cb			7.2	101.3
4			6.2	102.3
c			5.1	103.4
4			5.1	103.4
Cb			5.7 4.9	102.8 103.6
No			4.5	104.0

1+50

No			2.8	105.7
Cb			3.1 3.7	105.4 104.8
4			3.4	105.1
c			3.0	105.5
4			3.9	104.6
Cb			5.0	103.5
So +2			4.4 4.7	104.1 103.8

2+00

No			2.4	106.1
+7			2.0	106.5
Cb			2.5	106.0
4			1.7	106.8
c			0.9	107.6
4			1.1	107.4
+8			1.7	106.8
Cb			0.8	107.7
So			0.6	107.9
T.P.	10.17	118.11	0.51	107.94

Midway

2+32.18 = W.L. Burke #1 RΔ

No	9.0	109.1
Cb	9.2 10.0	108.9 108.1
4	9.5	108.6
c	9.6	108.5
4	10.3	107.8
Cb	11.4 10.6	106.7 107.5
So	11.0	107.1

W.L # 2

So	9.9	108.2
Cb	9.8 10.3	108.3 107.8
4	9.5	108.6
c	8.8	109.3
4	9.2	108.9
+8	9.8	108.3
Cb	9.0	109.1
No	9.0	109.1

W Cb. POSTED 109.6

No	Gutr 8.5 9.1	109.0 109.4
Cb	" 8.7 9.3	108.8
4	8.8	109.3
c	8.6	109.5
4	9.2	108.9
Cb	9.8 9.3	108.3 108.8
So	9.4 10.2	108.7 107.9

118.11

W ¼ Burke

So	9.0	109.1
"	9.2	108.9
"	8.7	108.4
"	8.1	110.0
"	8.5	109.6
"	8.9	109.2
"	8.2	109.9
No	8.2	109.9

Ctr

No	7.5	110.6
"	7.7	110.4
"	8.3	109.8
"	7.8	110.3
"	7.6	110.5
"	8.2	109.9
"	8.4	109.7
So	8.3	109.8

E ¼

So	8.3	109.8
"	8.2	109.9
"	7.9	110.2
"	7.3	110.8
"	7.5	110.6
"	7.8	110.3
No	7.4	110.7

Midway

E.Ctr.

	6.5	111.6
Ctr	7.4	110.7
"	6.5	111.6
"	7.3	110.8
No		
"	6.8	111.3
"	6.7	111.4
"	7.4	110.7
"	7.9	110.2
"	7.3	110.8
"	7.6	110.5
So		

E.Line Burke #1

So	7.2	110.9
"	6.7	111.4
"	7.4	110.7
"	6.9	111.2
"	6.2	111.9
"	6.3	111.8
"	6.7	111.4
"	6.0	112.1
No	5.9	112.2

B.M.N.E Burke 5.86 112.25

E.L. Burke #1 RA-0+00

118.1

No	4.5	113.6
"	4.8	113.3
"	5.8	112.3
"	5.4	112.7
"	4.5	113.6
"	6.3	111.8
"	7.1	111.0
So	7.2	110.9

118.11

0+50 118.1

So			5.7	1124
Ct			5.0 5.7	113.1 112.4
Lt			4.9	113.2
o			4.0	1141
Lt			3.9	114.2
Ct			4.2 3.4	113.9 114.7
No			2.8	1153

1+00

No			1.4	1167
Ct			2.1 2.8	116.0 115.3
Lt			2.1	116.0
o			2.3	1158
Lt			3.2	114.9
Ct			4.2 3.7	113.9 114.4
So			3.9	1142
T.P.	12.12	128.26	1.97	116.14

1+50 128.3

So			12.4	1159
Ct			11.7 12.5	116.6 115.8
Lt			11.1	117.2
o			10.4	1179
Lt			10.3	118.0
Ct			10.9 9.9	117.4 118.4
No			9.7	1186

Midway

2+0 128.3

No			7.3	1210.8
Ct			7.8 8.7	120.5 119.6
Lt			8.6	119.7
o			8.4	1199
Lt			9.2	119.1
Ct			10.7 9.9	117.6 118.4
So			10.5	1178.6

2+32.18 = W.L. Hodgman #1 = RA

So			9.1	1192
Ct			8.6 9.1	119.7 119.2
Lt			8.3	120.0
o			7.5	1208
Lt			7.5	120.8
Ct			7.8 7.0	120.5 121.3
No			6.5	1218

W.L. #2

No			6.5	1218
Ct			6.8 7.6	121.5 120.7
Lt			7.1	121.2
o			7.0	1213
Lt			7.6	120.7
Ct			8.5 7.7	119.8 120.6
So			8.0	1203
Cr Hl.	128.29		8.02	120.24 ✓ 120.27

128.29

W. Ch. Hodgman

	1283	
So	7.6	120.9
	7.3	121.0
Ch	8.0	120.3
W	7.1	121.2
C	6.5	121.8
W	6.7	121.6
	6.9	121.4
Ch	6.2	121.1
No	6.0	121.3

E of W Ch.

	6.0	122.3
No	6.6	121.7
	6.3	122.0
W Ch.	6.8	121.5
	7.4	120.9
S. Ch	8.0	120.3
	7.6	120.7
So	8.2	120.1

W ½

So	7.5	120.8
Ch	7.3	121.0
W	7.0	121.3
C	6.3	122.0
W	6.3	122.0
Ch	6.1	122.2
No	6.6	122.7

Midway

Ctr 1283

No	4.8	123.5
Ch	6.5	121.8
W	6.0	122.3
C	6.0	122.3
E	6.6	121.7
	6.8	121.5
Ch	7.2	121.1
So	6.7	121.6

E ¼

So	7.1	121.2
Ch	6.8	121.5
W	6.4	121.9
	6.0	122.3
C	5.5	122.8
E	5.4	122.9
Ch	4.9	123.4
No		

E Ch

	4.3	124.0
No	5.1	123.2
	4.7	123.6
Ch	5.0	122.7
W	5.3	123.0
C	5.5	122.8
W	6.7	122.1
	7.7	121.1
Ch	6.6	121.2
	7.0	121.3
So	7.9	120.4

POSTED

128.29

1283

Eline Hodgman #1

So	7.1	1212
Ct	6.6	121.7
	7.2	121.1
¼	6.3	122.0
C	5.5	1228
¼	5.1	123.2
Ct	5.2	123.1
	4.6	123.7
No	4.0	1243

E.L. Hodgman #2 R△ = 0+00

1283

No	4.2	1241
Ct	4.6	123.7
	5.4	122.9
¼	4.9	123.4
C	5.1	1232
¼	6.2	122.1
Ct	7.0	121.3
	6.6	121.7
So	7.1	1212

0+50

So	6.2	1221
Ct	6.3	122.0
¼	5.2	123.1
C	4.3	1240
¼	4.2	123.1
Ct	5.0	123.3
	3.7	124.6
No	3.2	1251

Midway

1+00

1283

No	2.3	1260
Ct	2.9	125.4
	3.6	124.7
¼	3.2	125.1
C	3.5	1248
¼	4.4	123.9
Ct	4.8	123.5
So	5.1	1232

1+50

So	3.9	1244
Ct	3.5	124.8
¼	2.9	125.4
C	2.3	1260
¼	2.0	126.3
Ct	2.3	126.0
	1.2	127.1
+8	0.7	127.6

T.P. 10.68 137.91 1.06 137.9 127.23

+9 9.9

No 9.1 1288

2+00

No	9.6	1283
Ct	10.2	127.7
¼	10.4	127.7
C	10.5	1274
¼	11.0	126.9
Ct	11.3	126.6
So	11.5	1264

137.91

2+32.18 = W.L. Taft #1 - PI

So.	9.6	128.4
C.	9.1	128.8
¼	8.9	129.0
C	8.4	129.5
¼	8.8	129.1
C	8.6	129.3
N.	8.1	129.7
B.M. N.W Taft	8.26	129.66

W.L Taft #2

No.	8.2	129.7
C	7.8	130.1
¼	7.5	130.4
C	7.4	130.5
¼	6.8	131.1
C	7.0	130.9
So.	6.4	131.5

W Ct

So	4.8	133.1
C	5.9	132.0
¼	6.2	131.7
C	6.3	131.6
¼	6.6	131.3
C	6.7	131.2
No	6.6	131.3

Midway 137.9 70

W ¼

No	5.7	132.2
Ct	5.8	132.1
¼	5.5	132.4
C	5.2	132.7
¼	5.0	132.9
C	4.4	133.5
So	3.4	134.5

Ctr 137.9

So.	2.1	135.8
Ct	3.1	134.8
¼	3.8	134.1
C	4.1	133.8
¼	4.1	133.8
C	4.7	133.2
No.	4.5	133.4

E ¼

No	3.6	134.3
C	3.9	134.0
¼	3.3	134.6
C	3.3	134.6
¼	2.6	135.3
C	2.5	135.4
So	2.0	135.9

137.91

E. Ch. Taft 137.9

So.		1.1	136.8
+1°		1.4	136.5
Ch		1.7	136.2
H		1.8	136.1
C		1.6	136.3
H		1.9	136.0
Ch		2.3	135.6
		1.9	136.0
No		3.2	134.7

E. Line Taft #1

1379

No.		1.9	1360
+1.7		0.9	137.0
Ch		0.9	137.0
H		0.9	137.0
C		0.6	137.3
H		0.5	137.4
Ch		0.9	137.8
So		0.0	137
TP	11.92	149.81	0.02	137.89

EL #1 RA = 0708

1468

So.		11.9	1379
Ch		12.4	137.4
H		11.9	137.9
C		11.5	138.3
H		11.1	138.7
H		10.2	139.6
No.		9.5	1401

0708

1468

No.		3.3	1435
Ch		7.0	1428
+3		8.0	
H		7.7	1421
C		7.9	1419
H		8.5	1413
Ch		8.8	1410
So		9.2	1406
	1400		
So.		6.1	1437
Ch		5.9	1439
H		5.1	1447
C		4.3	1455
H		4.5	1453
H		4.0	1458
No.		3.3	1465
	1460		
No.		10.2	1580
Ch		0.7	1491
H		0.8	1490
C		1.0	1488
H		1.6	1482
H		2.4	1474
So.		2.8	1470
T.P	11.69	161.44	0.06	149.75

161.44

2+0.0 161 4

So	11.1	1503
+6	11.1	150.3
+7	11.8	149.6
Cb	11.3	150.1
¼	10.3	151.1
C	9.3	1541
¼	8.8	152.6
Cb	8.3	153.1
No	7.5	1539

2+32.18 = W.L. Sum #1 RA

No	5.9	1555
Cb	6.5	154.9
+3	7.7	153.7
¼	7.3	154.1
C	7.5	1539
¼	8.4	153.0
Cb	9.1	152.3
+3	9.9	
S. +4	8.9	1541
	9.3	
B.M. N.W. Sum.	5.86	155.58

W.L #2

So	8.3	1531
+8	8.1	153.3
+9	8.5	152.9
Cb	8.3	153.1
¼	7.3	154.1
C	6.6	1541
¼	6.6	154.8
+8	7.4	154.0
Cb	6.2	155.2
No	5.9	1555

Midway

W.Cb 161 4

No	5.2	1562
Cb	6.0	155.4
+2	6.0	155.4
+4	7.1	154.3
¼	6.1	1551
C	6.3	
¼	6.9	154.5
Cb	7.7	153.7
So	7.7	1537

W ¼

So	7.0	1544
Cb	7.0	154.4
¼	6.1	155.3
C	5.8	1556
¼	5.7	155.7
+8	6.8	154.6
+10	5.9	155.5
Cb	5.8	155.6
No	5.3	1561

Ctr

No	5.1	1563
Cb	5.1	156.3
+3	6.0	155.3
¼	5.1	156.3
C	5.0	1564
¼	5.6	155.8
Cb	6.5	154.9
+2	6.7	
+4	6.2	
So	6.4	1550

POSTED

161.44

E ¼ Sum 4

So		5.7	155.7
ch		5.6	155.8
¼		4.7	156.7
c		4.5	156.9
¼		4.7	156.7
ch +8		5.1 4.5	156.3 156.9
No		4.4	157.0
	E Ch.		
No		3.7	157.7
ch 12		3.6	157.8
¼ +3		3.8 4.6 3.6	157.6 156.8 157.8
c		3.5	157.9
¼		4.2	157.2
ch		5.1	156.3
So		5.1	156.3
	E. line Sum		
So		4.3	157.1
ch		4.3	157.1
¼		3.6	157.8
c		3.0	158.4
¼		2.9	158.5
ch +8 +10		3.7 3.6 2.6	157.7 158.8 158.8
No		2.6	158.8

POSTED

.587

80) 46.96

400

696

640

560

560

30°25'

Curve on Oil Blvd.

W. Side Def.
80' Sts.

0° 26½'
0° 53'
1° 19½'
1° 46'
2° 12½'
2° 39'
3° 05½'
3° 32'
3° 58½'
4° 25'
4° 51½'
5° 18'
5° 44½'
6° 11'

E. Side Def.

1° 49' C.
48.6' Sts
0° 26' = 44.23
0° 51½' 92.82'
1° 18'
1° 44½'
2° 11'
2° 37½'
3° 04'
3° 30½
3° 57'
4° 23½'
4° 50'
5° 16½
5° 43'

Distances from Block Cor to R.A Point on Streets east of Electric Ave in Bird Rock City are 80'Sts. 19.16 - 60'Sts 14.37

Bird Rock Add. 60'St - 35.22 - 80'- 46.96'

Published by H. S. CROCKER COMPANY, Stationers, Drawing Materials, and Mathematical Instruments, San Francisco.

Table showing the difference of latitude and departure in running 80 chains at any course from 1 to 60 minutes.

MINUTES.	LKS.	MINUTES.	LKS.	MINUTES.	LKS.
1	2⅓	21	49	41	95⅔
2	4⅔	22	51⅓	42	98
3	7	23	53⅔	43	100⅓
4	9⅓	24	56	44	102⅔
5	11⅔	25	58⅓	45	105
6	14	26	60⅔	46	107⅓
7	16⅓	27	63	47	109⅔
8	18⅔	28	65⅓	48	112
9	21	29	67⅔	49	114⅓
10	23⅓	30	70	50	116⅔
11	25⅔	31	72⅓	51	119
12	28	32	74⅔	52	121⅓
13	30⅓	33	77	53	123⅔
14	32⅔	34	79⅓	54	126
15	35	35	81⅔	55	128⅓
16	37⅓	36	84	56	130⅔
17	39⅔	37	86⅓	57	133
18	42	38	88⅔	58	135⅓
19	44⅓	39	91	59	137⅔
20	46⅔	40	93⅓	60	140

TABLE FOR RUNNING ON SLOPES.

In the following table the first column shows the angle, the second the number of links to be added to a chain on the slopes, to make one chain, horizontal measurement.

ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS
°		°		°		°	
4	0.24	11	1.88	18	5.14	25	10.54
5	0.38	12	2.24	19	5.76	26	11.26
6	0.55	13	2.63	20	6.42	27	12.24
7	0.76	14	3.06	21	7.11	28	13.37
8	0.98	15	3.53	22	7.85	29	14.34
9	1.24	16	4.02	23	8.64	30	15.47
10	1.55	17	4.56	24	9.47	35	22.07