

*Return to City Engineers Office
City Hall, San Diego, Cal.*

TRANSIT

398

F.B.323

TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		½ DEGREE.		¼ DEGREE.		¼ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0	99.98	1.75	100.00	0.44	100.00	0.87	99.99	1.31	89
1	99.94	3.49	99.98	2.18	99.97	2.62	99.95	3.05	88
2	99.86	5.23	99.92	3.93	99.91	4.36	99.88	4.80	87
3	99.86	6.98	99.84	5.67	99.81	6.10	99.79	6.54	86
4	99.76	8.72	99.73	7.41	99.69	7.85	99.66	8.28	85
5	99.62	10.45	99.58	9.15	99.54	9.58	99.50	10.02	84
6	99.45	12.19	99.41	10.89	99.36	11.32	99.31	11.75	83
7	99.25	13.92	99.20	12.62	99.14	13.05	99.09	13.49	82
8	99.03	15.64	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	17.36	98.70	16.07	98.63	16.50	98.56	16.93	80
10	98.48	19.08	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98.16	20.79	98.08	19.51	97.99	19.94	97.90	20.36	78
12	97.81	22.50	97.72	21.22	97.63	21.64	97.53	22.07	77
13	97.44	24.19	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	25.88	96.92	24.62	96.81	25.04	96.70	25.46	75
15	96.59	27.56	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	29.24	96.00	27.98	95.88	28.40	95.76	28.82	73
17	95.63	30.90	95.50	29.65	95.37	30.07	95.24	30.49	72
18	95.11	32.56	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	34.20	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	35.84	93.82	34.61	93.67	35.02	93.51	35.43	69
21	93.36	37.46	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	39.07	92.55	37.86	92.39	38.27	92.22	38.67	67
23	92.05	40.67	91.88	39.47	91.71	39.87	91.53	40.27	66
24	91.35	42.26	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	43.84	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	45.40	89.69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	46.95	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	48.48	88.09	47.33	87.88	47.72	87.67	48.10	61
29	87.46	50.00	87.25	48.86	87.04	49.24	86.82	49.62	60
30	86.60	51.50	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	52.99	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	54.46	84.57	53.36	84.34	53.73	84.10	54.10	57
33	83.87	55.92	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	57.36	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	58.78	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	60.18	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	61.57	79.60	60.53	79.34	60.88	79.07	61.22	52
38	78.80	62.94	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.77	64.28	77.41	63.27	77.16	63.61	76.88	63.94	50
40	76.66	65.61	76.25	64.61	76.04	64.99	75.76	65.28	49
41	75.47	66.91	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	68.20	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	69.47	72.84	68.54	72.54	68.84	72.24	69.15	46
44	71.93	70.71	71.63	69.83	71.33	70.09	71.02	70.40	45
45	70.71		70.71						
Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees.
Degrees.	DEGREES.		½ DEGREE.		¼ DEGREE.		¼ DEGREE.		Degrees.

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City Hall, San Diego, Cal.

Crocker Quality

TRANSIT BOOK



No. _____

MANUFACTURED BY

H. S. CROCKER CO.

SAN FRANCISCO AND SACRAMENTO
CALIFORNIA

FROM
LORING'S BOOK STORE
SAN DIEGO, CAL.

Cross-Section of El Cajon Ave. (Dand. 9. }
 Park Boulevard to City Limits. 57 }
 B.M. NE

	0.83	340.91	340.08 Univ Blvd.
		E. line P. Blvd = 0+00	
No		2.4	338.5
+3		2.0	338.9
ct		2.7	338.7
$\frac{1}{4}$		4.7	338.2
+20	POSTED	2.5	338.4
0		1.5	339.4
$\frac{1}{4}$		1.3	339.6
ct		0.6	340.3
50		0.4	340.5
		0+25	
50		2.2	338.7
+10		3.5	337.4
ct		3.3	337.6
$\frac{1}{4}$		3.2	337.7
C		3.2	337.7
+10		4.0	336.9
$\frac{1}{4}$		3.4	337.5
+12		4.7	336.2
+18		3.9	337.0
ct		4.6	336.3
+10		4.8	336.1
No		3.7	337.2

	0+50	
No	5.8	335.1
+5	6.2	334.7
ct	5.1	335.8
+10	5.0	335.9
+18	5.8	335.1
$\frac{1}{4}$	5.9	335.0
+20	6.2	334.7
C	4.7	336.2
$\frac{1}{4}$	4.8	336.1
ct	4.4	336.5
+14	4.8	336.1
50	4.1	336.8
	0+75	
50	4.4	336.5
+3	5.3	335.6
ct	5.4	335.5
$\frac{1}{4}$	5.6	335.3
C	5.7	335.2
+7	8.1	332.8
+10	8.4	332.5
+12	7.6	333.3
$\frac{1}{4}$	7.5	333.4
+6	7.7	333.2
+15	5.5	335.4
ct	6.4	334.5
No	7.4	333.5

340.91

1+00

No	11.0	329.9
U	9.4	331.5
+10	8.1	332.8
+19	11.2	329.7
+21	9.4	331.5
$\frac{1}{4}$	9.2	331.7
+15	9.3	331.6
+18	11.2	329.7
+21	10.7	330.2
C	8.5	332.4
+3	6.7	334.2
$\frac{1}{2}$	6.5	334.4
U	6.8	334.6
+17	5.8	335.1
S ₀	5.2	335.7
1+25		
S ₀	6.7	334.2
+13	8.3	332.6
U	8.6	332.3
+7	9.5	331.4
+15	8.7	332.2
$\frac{1}{2}$	9.1	331.8
+17.5	9.6	331.3
+23	10.2	330.7
C	11.7	329.2
+7	13.6	327.3
+9	13.3	327.6
+12	11.0	329.9
$\frac{1}{4}$	11.0	329.9
+3	10.9	330.0

El Cajon Ave.

2

1+50

S ₀	10.1	330.8
+9	12.2	328.7
U	12.1	328.8
+15	12.6	328.3
TP 0.11	328.08	12.74
1+25		
No $\frac{1}{2}$ +8	1.0	327.1
+12	1.0	327.1
+16	0.1	328.0
U	0.7	327.4
+5	1.1	327.0
No	1.5	326.6
1+50		
No	4.1	324.0
+15	3.8	324.3
U	3.1	325.0
+20	2.8	325.3
+25	+0.4	328.5
$\frac{1}{4}$	+0.4	328.5
+15	+0.5	328.6
+20	2.0	326.1
C	2.1	326.0
S ₀ $\frac{1}{2}$	0.8	327.3

32808

		1+66	
No		59	322.2
ck		57	3224
		1+70	
No		8.1	320.0
ck		6.6	321.5
		1+75	
No		8.6	319.5
+13		8.4	319.7
+16		7.7	320.4
ck		7.5	320.6
+16		6.1	322.0
+25		1.2	326.9
$\frac{1}{4}$		1.0	327.1
+15		0.9	327.2
+22		4.6	323.5
C		5.4	322.7
+13		5.2	322.9
+17		3.6	324.5
$\frac{1}{4}$		4.2	323.9
+12		4.4	323.7
ck		3.7	324.4
+8		3.0	325.1
So		1.1	327.0

2+00

So		4.2	323.9
+7		4.2	313.9
ck		6.6	321.5
+13		7.0	321.1
$\frac{1}{4}$		6.6	321.5
+14		8.5	319.6
C		8.0	320.1
+12		2.3	325.8
$\frac{1}{4}$		2.4	325.7
+13		2.4	325.7
+14		8.1	320.0
ck		7.5	320.6
+12		7.5	320.6
No		6.7	321.4
		2+25	
No		6.9	321.2
ck		7.7	320.4
+18		7.8	320.3
+24		3.9	324.2
$\frac{1}{2}$		4.0	324.1
+15		3.9	324.2
+25		9.3	318.8
C		9.6	318.5
+20		10.5	317.6
$\frac{1}{4}$		11.2	316.9
+6		13.5	314.6
+12		13.3	314.8
+17		11.3	316.8
ck		9.4	318.7
+4		8.4	319.7
+11		8.2	319.9
So		6.6	321.5

328.00

2150

So	10.1	318.0
+12	13.0	315.1
+18	15.5	312.6
Cl	15.0	313.1
r ³	12.6	315.5
$\frac{1}{4}$	10.8	317.3
+9	9.6	318.5
C	10.2	317.9
+5	9.9	318.2
+12	5.4	322.7
$\frac{1}{4}$	5.6	322.5
+3	5.8	322.3
+7	7.8	320.3
+17	8.2	319.9
Cl	7.7	320.4
No	6.7	321.4

2175

No	7.1	321.0
Cl	8.0	320.1
+5	8.2	319.9
$\frac{1}{4}$	7.0	321.1
+12	6.9	321.2
+18	10.0	318.1
C	10.2	317.9
$\frac{1}{4}$	11.0	317.1
+12	12.5	315.6
Cl	13.5	314.6
+5	14.1	314.0
+10	15.8	312.3
+14	15.8	312.3
So	13.6	314.5

El Cajon Ave

2190

So	14.8	313.3
+5	15.4	312.7
+12	14.3	313.8
Cl	14.1	314.0
$\frac{1}{4}$	12.0	316.1
C	10.3	317.8
+8	10.3	317.8
+13	7.7	320.4
$\frac{1}{2}$	7.9	320.2
Cl	8.3	319.8
No	7.6	320.5

2400 - N.L. Georgia

No	7.1	321.0
Cl	{ 7.6	320.5
	{ 8.3	319.8
$\frac{1}{4}$	8.3	319.8
C	8.3	319.8
$\frac{1}{2}$	9.1	319.0
+21	9.8	318.3
Cl	9.1	319.0
So	8.9	319.2

328.08

E.L. Georgia = 0100

So	10.4	317.7
Ch	10.6	317.5
+2	11.5	316.6
$\frac{1}{4}$	10.3	317.8
C	9.8	318.3
$\frac{1}{4}$	10.4	317.7
+26	10.2	317.9
Ch	9.1	319.0
No	8.8	319.3

0 + 07

No	10.9	317.2
+19	12.3	315.8
Ch	11.5	316.6
+20	10.4	317.7
$\frac{1}{4}$	10.8	317.3
+13	11.0	317.1
+20	14.1	314.0
C	14.9	313.2
$\frac{1}{4}$	14.9	313.2
Ch	14.4	313.7
	14.1	314.0

0 + 13

No	11.4	316.7
+15	13.2	315.1
Ch	12.1	316.0
+20	11.2	316.9
$\frac{1}{4}$	11.2	316.9
+13	11.6	316.5

T.P. 1.34 317.32 12.10 315.98

+20	4.5	312.8
C	5.1	312.2
+12	5.1	312.2
+16	6.7	310.6
$\frac{1}{4}$	7.8	309.5
+8	8.5	308.8
+17	7.3	310.0
Ch	7.5	309.8
So	6.5	310.8
10.50	5.8	311.5

0 + 25

10.50	5.7	311.6
So	6.1	311.2
Ch	6.1	311.2
+12	7.4	309.9
+23	9.1	308.2
$\frac{1}{4}$	8.2	309.1

317.32

0 + 25

50 $\frac{1}{4}$ + 6	8.0	309.3
+ 12	6.6	310.7
C	4.9	312.4
+ 8	4.3	313.0
+ 13	1.7	315.6
$\frac{1}{4}$	1.0	316.3
+ 0.5	1.5	315.8
+ 10	0.7	316.6
+ 18	2.4	314.9
U	2.4	314.9
No	1.9	315.4

0 + 50

No	2.6	314.7
U	2.7	314.6
+ 21	2.4	314.9
$\frac{1}{4}$	2.4	314.9
+ 13	2.6	314.7
+ 19	5.1	312.2
C	4.8	312.5
+ 8	5.1	312.2
+ 13	7.1	310.2
+ 17	6.6	310.7
+ 21	9.3	308.0
$\frac{1}{4}$	8.5	308.8
U	8.4	308.9

+ 7	7.3	310.0
50	6.2	311.1
10'50	5.9	311.4

0 + 75

10'50	5.6	311.7
50	6.0	311.3
+ 13	6.8	310.5
U	8.0	309.3
+ 7	10.1	307.2
+ 15	10.6	306.7
+ 25	11.0	306.3
$\frac{1}{4}$	9.3	308.0
+ 7	9.7	307.6
+ 13	8.7	308.6
+ 21	6.5	310.8
C	6.0	311.3
+ 10	5.5	311.8
+ 13	3.7	313.6
$\frac{1}{4}$	3.5	313.8
+ 4	3.5	313.8
+ 8	5.0	312.3
+ 13	4.1	313.2
U	3.7	313.6
No	2.7	314.6

317.32

1400

No.	2.5	314.8
+5	3.2	314.1
Ch.	3.5	313.8
+15	3.7	313.6
+20	5.6	311.7
+23	4.4	312.9
$\frac{1}{2}$	4.4	312.9
+14	4.6	312.7
+17	5.8	311.5
+23	6.2	311.1
C	7.4	309.9
+4	8.5	308.8
+9	9.1	308.2
+11	10.2	307.1
+19	11.9	305.4
$\frac{1}{2}$	12.6	304.7
+17	10.6	306.7
Ch.	9.4	307.9
So	7.3	310.0
No.	6.8	310.5

El Cajon Ave

1425

15'30	9.8	307.5
So	10.9	306.4
Ch.	11.6	305.7
+11	12.5	304.8
$\frac{1}{2}$	14.4	302.9
+8	12.3	305.0
+18	9.4	307.9
+26	8.4	308.9
C	7.8	309.5
+2	6.7	310.6
+12	6.6	311.7
$\frac{1}{2}$	5.6	311.7
+5	6.1	311.2
+10	3.9	313.4
Ch.	3.3	314.0
No	2.3	315.0

1450

No	2.4	314.9
Ch.	3.1	314.2
+18	3.7	313.6
+23	6.6	310.7
$\frac{1}{2}$	6.6	310.7
+15	6.6	310.7
+20	5.9	311.4

317.32

1+50

C	6.4	310.9
+20	10.9	306.4
$\frac{1}{4}$	10.6	306.7
+10	14.4	302.9
Ch.	14.5	302.8
+9	15.3	302.0
50	13.5	303.8
15'50	12.4	304.9

1+75

50 Ch.	12.4	304.9
+23	8.1	309.2
$\frac{1}{4}$	8.1	309.2
+14	8.4	308.9
+16	7.2	310.1
C	6.4	310.9
+11	6.8	311.5
+13	7.4	309.9
$\frac{1}{4}$	8.0	309.3
+5	7.5	309.8
+10	3.8	313.5
Ch.	3.1	314.2
No	2.6	314.7

2+00

No	3.1	314.2
Ch	4.2	313.1
+19	4.6	312.7
+25	8.9	308.4
$\frac{1}{4}$	9.0	308.3
+18	8.8	308.5
+21	7.0	310.3
C	7.3	310.0
+12	7.7	309.6
+17	9.1	308.2
+19	9.5	307.8
+22	8.7	308.6
Ch	9.3	308.0
+7	10.7	306.6
Ch.	12.5	304.8

2+25

10' No of 50 Ch.	12.9	304.4
$\frac{1}{4}$	11.6	305.7
+12	11.1	306.2
+14	9.7	307.6
C	9.6	307.7
+8	9.1	308.2
+11	9.7	307.6
$\frac{1}{4}$	10.1	307.2

317.32

2+25

No 4+3	9.7	307.6
+8	6.1	311.2
Ch	5.3	312.0
No	4.5	312.8

2+50

No	5.9	311.4
+5	6.7	310.6
Ch	7.4	309.9
+50	7.6	309.7
+52	10.2	307.1
$\frac{1}{4}$	11.0	306.3
C	11.2	306.1
+14	11.8	305.5

2+75

17 No. of 5. 4	12.9	304.4
C	13.0	304.3
A	11.9	305.4
+5	11.7	305.6
+8	10.1	307.2
Ch	10.1	307.2
No	8.5	308.8

3+00 = W.L. Florida

9

No	10.7	306.6
+11	11.9	305.4
Ch	12.1	305.2
+18	12.0	305.3
+21	13.2	304.1

N. Ch

No	11.0	306.3
+12	12.6	304.7
Ch	12.7	304.6
+18	12.8	304.5

T.P. 0.16	304.55	12.93	304.39
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15'50	+7.5	2.3	302.3
30.		4.0	300.6
+5		2.1	302.5

2+00

15'50	3.8	300.8
50	4.5	300.1
+1.	2.6	302.0

2+25

15'50	5.1	299.5
50	5.2	299.4
+1	4.0	300.6
Ch	1.7	302.9

304.55

2+50

20'S.	6.5	298.1
5'	7.0	297.6
4''	8.0	296.6
50	7.7	296.9
+3	5.0	299.6
Ch	3.0	301.6
+12	7.6	303.0
4	0.7	303.9

2+75

12' No. of 50 1/2	1.1	303.5
4	1.6	303.0
+3	1.4	303.2
Ch	3.8	300.8
+12	5.8	298.8
50	8.4	296.5
12'S0	11.3	293.3
13''	9.9	294.7
20''	8.9	295.7

3+00 = W.L. Florida

20'S0	10.5	294.1
15''	10.7	293.9
13''	11.5	293.1
9''	12.0	292.6
50	7.0	297.6

El Cajon Ave.

10

+5	5.9	298.7
Ch	4.5	300.1
4	2.4	302.2
+11	2.2	302.4
+13	1.5	303.1
C	1.4	303.2
1/4	0.7	303.9
+4	0.5	304.1

W. Ch

1/6 Ch + 21	1.0	303.6
4	1.5	303.1
C	2.0	302.6
1/4	2.5	302.1
Ch	5.3	299.3
50	6.3	298.3
+7' 50	6.5	298.1
14''	10.6	294.0
20''	11.0	293.6

Ch + 9

20'S0	8.7	296.4
50	6.0	298.6
Ch	6.1	298.5

304.55

W $\frac{1}{4}$ Florida

20' S.	9.0	295.6
S.	7.6	297.0
Ch	6.5	298.1
$\frac{1}{4}$	4.4	300.2
+5	4.7	299.9
C	2.8	301.8
$\frac{1}{4}$	1.7	302.9
Ch	0.8	303.8
No.	0.5	304.1

Ctr

No.	+0.1	304.7
Ch	0.6	304.0
$\frac{1}{4}$	2.2	302.4
C	3.0	301.6
$\frac{1}{4}$	4.8	299.8
Ch	6.2	298.4
S.	7.3	297.3
20' S.	8.4	296.2

E $\frac{1}{4}$

20' S.	8.8	295.8
S.	7.8	296.8
Ch	6.6	298.0
$\frac{1}{4}$	4.7	299.9
C	3.4	301.2

$\frac{1}{4}$	2.4	302.2
+5	2.3	302.3
+9	1.7	302.9
Ch	0.8	303.8
No.	0.6	304.0

E $\frac{1}{4}$ + +

No.	0.6	304.0
Ch	1.1	303.5

E Ch.

No.	2.9	301.7
Ch	3.4	301.2
+18	3.4	301.2
+22	2.5	302.1
$\frac{1}{4}$	2.7	301.9
+16	3.2	301.4
+19	3.9	300.7
C	4.9	299.7
+15	5.7	298.9
+20	4.8	299.8
$\frac{1}{4}$	5.6	299.0
Ch	8.0	296.6
S.	8.7	295.9
20' S.	9.7	294.9

30455

E. line Florida - 0400

20'S.	10.6	294.0
S.	9.6	295.0
Ch.	9.3	295.3
$\frac{1}{4}$	7.4	297.2
C	5.0	299.6
+12	3.4	301.2
$\frac{1}{4}$	2.8	301.8
+7	2.7	301.9
+11	5.2	299.4
Ch.	5.2	299.4
No	4.6	300.0

0425

15' No	7.6	297.0
No	8.0	296.6
Ch.	7.4	297.2
+12	7.2	297.4
+22	3.1	301.5
$\frac{1}{4}$	3.2	301.4
+15	3.4	301.2
+20	5.4	299.2
C	6.1	298.5
+6	8.1	296.5
$\frac{1}{4}$	9.6	295.0
Ch.	10.8	293.8

S.	11.1	293.5
20'S.	11.7	292.9

0445

20'S.	14.2	290.4
S.	13.6	291.0
Ch.	13.3	291.3
$\frac{1}{4}$	11.7	292.9
+19	11.1	293.5
C	6.3	298.3
+10	3.9	300.7
$\frac{1}{4}$	3.4	301.2
+5	3.5	301.1
+11	5.1	299.8
+12	10.5	294.1
Ch.	10.7	293.9
No	10.7	293.9
20'S.	9.7	294.9

0465

20' No	6.9	297.7
No	7.1	297.5
Ch.	7.9	296.5
+14	8.2	296.4
+22	3.8	300.8
$\frac{1}{4}$	3.9	300.7

304.55

0165

4+16	4.1	300.5
+20	5.7	298.9
C	7.0	297.6
+5	8.6	296.0
$\frac{1}{4}$	10.2	294.4
Ch	10.3	294.3
50	11.6	293.0
20'50	11.5	293.1
V.B.M.S.E Florida	8.07	296.48/296.46
	1+00	
15'50	9.6	295.0
50	9.7	294.9
+10	9.6	295.0
Ch	8.2	296.4
+12	7.5	297.1
$\frac{1}{4}$	9.0	295.6
C	7.8	296.8
+10	4.3	300.3
$\frac{1}{4}$	4.1	300.5
+6	3.8	300.8
+12	7.2	297.4
Ch	7.3	297.3
No	6.8	297.8
15'No	6.4	298.2

El Cajon Ave

18

1+25

15'No	6.3	298.3
No	6.3	298.3
Ch	6.8	297.8
+16	6.7	297.9
+22	4.0	300.6
$\frac{1}{4}$	4.3	300.3
+18	4.2	300.4
+25	6.9	297.7
C	7.0	297.6
+18	5.7	298.9
+24	8.0	296.6
$\frac{1}{4}$	8.5	296.1
Ch	9.7	294.9
50	9.4	295.2
15'50	10.6	294.0
	1+50	
10'50	8.3	296.3
50	8.1	296.5
Ch	8.2	296.4
$\frac{1}{4}$	8.0	296.6
C	6.8	297.8
+7	6.5	298.1
+11	4.1	300.5
$\frac{1}{2}$	4.0	300.6

1+50

$\frac{1}{2}$ +6	3.5	301.1
+11	6.5	298.1
+23	6.3	298.3
ck	5.5	299.1
+10	4.1	300.5
No	4.3	300.3
10 No	5.0	299.6
	1475	
10 No	5.0	299.6
No	4.7	299.9
ck	4.9	299.7
+17	5.2	299.4
+22	3.5	301.1
$\frac{1}{4}$	3.6	301.0
+15	3.6	301.0
+20	5.7	298.9
G	6.0	298.6
$\frac{1}{4}$	7.8	296.8
ck	7.8	296.8
So	8.8	295.8
10's.	9.1	295.5

2+00

10's.	8.0	296.6
So	7.9	296.7
ck	7.7	296.9
$\frac{1}{4}$	7.2	296.4
+3	6.9	297.7
+10	4.4	300.2
+14	5.6	299.0
✓	5.1	299.5
+7	5.0	299.6
+11	3.1	301.5
$\frac{1}{4}$	3.1	301.5
+7	3.2	301.4
+10	3.7	300.9
ck	3.5	301.1
+10	2.8	301.8
No	2.4	302.2
10 No	3.2	301.4
	2+25	
10 No	2.7	301.9
No	1.9	302.7
ck	2.5	302.1
+13	4.2	300.4
+20	3.7	300.9
+23	3.8	301.8

2+25

1/4	2.7	301.9
+17	2.8	301.8
C	3.4	301.2
+17	3.5	301.1
1/4	4.7	299.9
Ch	5.5	299.1
So	5.5	299.1
10 So	6.0	298.6

2+50

So	4.2	300.4
Ch	5.1	299.5
1/4	4.0	300.6
+10	3.0	301.6
C	3.7	300.9
+11	2.2	302.4
1/4	2.1	302.5
+15	2.4	302.2
+20	3.0	301.6
Ch	3.0	301.6
+12	1.7	302.9
No	2.6	302.0

2+75

No	1.0	303.6
+10	1.6	303.0
Ch	1.2	303.4
1/4	1.4	303.2
+16	1.6	303.0
+19	2.6	302.0
C	2.7	301.9
+11	2.6	302.0
1/4	3.6	301.0
Ch	4.7	299.9
So	4.6	300.0

3+100 WL Alakama.

So	4.2	300.4
Ch	3.9	300.7
1/4	3.0	301.6
+9	1.7	302.9
+14	2.0	302.6
+18	2.8	301.8
C	2.6	302.0
+11	0.8	303.8
1/4	0.2	304.4
+7	0.3	304.3
+15	1.4	303.2
Ch	1.4	303.2

TR 9.67 313.90 0.32 304.23

Ch 9 304.7

No 8.3 305.6

W. Ch. Alabama

No 8.5 305.4

Ch 9.5 304.4

+8 10.5 303.4

+16 10.4 303.5

+20 9.2 304.7

$\frac{1}{4}$ 9.1 304.8

+16 9.4 304.5

+20 10.6 303.3

C 11.4 302.5

+13 11.3 302.6

$\frac{1}{4}$ 12.2 301.7

Ch 12.7 301.2

So 12.0 300.9

W $\frac{1}{4}$

So 12.6 301.3

Ch 12.1 301.8

$\frac{1}{4}$ 12.2 301.7

+12 10.5 303.4

+19 11.3 302.6

C 10.4 303.5

+11 8.7 305.2

$\frac{1}{4}$ 8.5 305.4

+7 8.6 305.3

+11 9.8 304.1

Ch 9.9 304.0

No 9.5 304.4

Ch

No 8.2 305.7

Ch 9.4 305.5

+17 9.2 305.7

+20 7.9 306.0

$\frac{1}{4}$ 8.2 305.7

+17 8.2 305.7

+20 9.4 304.5

C 10.4 303.5

$\frac{1}{4}$ 11.6 302.3

Ch 11.6 302.3

So 12.8 301.1

E $\frac{1}{4}$

So 12.3 301.6

+10 10.8 303.1

Ch 10.2 303.7

+15 10.8 303.1

+20 11.4 302.5

$\frac{1}{4}$ 11.0 302.9

E 1/4

C	9.8	304.1
+6	9.4	304.5
+11	7.7	306.2
1/4	7.6	306.3
+7	7.6	306.3
+11	9.4	304.5
Ch	8.3	305.6
+10	7.3	306.6
No	7.1	306.8

E Ch.

No.	6.4	307.5
+15	7.2	306.7
Ch	8.1	305.8
+5	9.2	304.7
+15	9.1	304.8
+20	7.0	306.9
1/4	7.1	306.8
+16	7.1	306.8
+20	8.7	305.2
0	9.5	304.4
1/4	10.0	303.9
+6	10.9	303.0
+16	11.0	302.9
+22	10.3	303.6

Ch	10.3	303.6
+8	10.9	303.0
+15	11.8	302.1
So	12.0	301.9

E. line Alakama = 0+00

So	11.4	302.5
Ch	11.2	302.7
+19	10.4	303.5
1/4	9.2	304.7
+7	7.6	306.3
C	8.3	305.6
+8	7.8	306.1
+11	6.7	307.2
1/4	6.6	307.3
+7	6.7	307.2
+12	8.8	305.1
+20	9.2	304.7
Ch	7.8	306.1
No	6.0	317.9

0 + 15

No	6.9	307.0
Ch	8.1	305.8

313.90

0+25

No	5.2	308.7
+10	5.4	308.5
Ch	7.1	306.8
+6	7.7	306.2
+16	7.6	306.3
+21	5.5	308.4
$\frac{1}{4}$	5.5	308.4
+15	5.8	308.1
+17	6.3	307.6
C	7.1	306.8
$\frac{1}{4}$	8.5	305.4
+12	7.6	306.3
Ch	8.0	305.9
+10	9.0	304.9
+16	10.1	303.8
S.	10.1	303.8
0+50		
S.	8.9	305.0
Ch	8.7	305.2
+24	8.1	305.8
$\frac{1}{4}$	7.8	306.1
+7	6.2	307.7
C	6.4	307.5
+4	6.3	307.6

18

+12	4.8	309.1
$\frac{1}{4}$	4.6	309.3
+7	4.5	309.4
+10	6.3	307.6
Ch	6.4	307.5
+6	5.5	308.4
No	6.1	307.8

0+75

No	5.3	308.6
Ch	4.8	309.1
+19	3.5	310.4
$\frac{1}{4}$	3.7	310.2
+15	3.9	310.0
+18	5.2	308.7
C	5.5	308.4
$\frac{1}{4}$	7.1	306.8
Ch	7.3	306.6
+15	6.4	307.5
S.	7.1	306.8
7.12	7.12	306.781 306.74

CH M.
313.86

313.86

1+00

50	6.0	307.9
ck	4.9	309.0
+9	5.9	308.0
$\frac{1}{4}$	5.1	308.8
C	5.0	308.9
+7	4.5	309.4
+11	3.0	310.9
$\frac{1}{2}$	2.7	311.2
+6	2.8	311.1
+10	3.5	310.4
ck	3.5	310.4
No	2.5	311.4

1+25

No	0.9	313.0
ck	2.2	311.7
$\frac{1}{2}$	1.9	312.0
+16	2.0	311.9
+19	2.8	311.1
C	3.1	310.8
$\frac{1}{4}$	3.8	310.1
ck	4.7	309.2
50	5.5	308.4

$\frac{1}{9}$
 $\frac{1}{08}$ } Davis
Donnan
Colkath
Day

19

1+50

50	2.8	311.1	
+12	3.8	310.1	
ck	3.9	310.0	
$\frac{1}{4}$	1.8	312.1	
C	2.3	311.6	
+7	2.4	311.5	
+11	1.2	312.7	
$\frac{1}{4}$	0.7	313.2	
ck	1.7	312.2	
No	1.4	312.5	
TR 12.75	325.12	1.49	312.37

1+75

50	13.0	312.1
ck	12.5	312.6
+15	12.7	312.4
TR 5	12.5	312.6
$\frac{1}{4}$	12.1	313.0
C	12.2	312.9
+7	11.8	313.3
+10	11.3	313.8
$\frac{1}{4}$	11.1	314.0
+13	11.0	314.1
+17	9.7	315.4
ck	10.3	314.8

325.12

21

1+75

ck+1+	10.7	314.4
No	11+	313.7
2+00		
No	8.8	316.3
ck	9.3	315.8
$\frac{1}{4}$	10.0	315.1
c	10.0	315.1
$\frac{1}{4}$	9.6	315.5
+10	10.9	314.2
+20	9.1	316.0
ck	9.5	315.6
+10	10.8	314.3
So	9.6	315.6

2+25

So	7.6	317.5
+12	8.4	316.7
ck	8.5	316.6
$\frac{1}{4}$	7.9	317.2
c	7.9	317.2
$\frac{1}{4}$	8.2	316.9
ck	6.3	318.8
No	6.3	318.8

22

2+50

No	4.5	320.6
ck	5.4	319.7
#	7.0	318.1
+18	6.6	318.5
+20	6.1	319.0
c	6.1	319.0
$\frac{1}{4}$	6.8	318.3
+22	6.1	319.0
ck	6.7	318.4
+10	6.6	318.5
So	6.3	318.8

2+75

So	5.9	319.2
+5	5.1	320.0
ck	4.7	320.4
$\frac{1}{4}$	5.1	320.0
c	4.6	320.5
+8	4.7	320.4
+12	5.6	319.5
$\frac{1}{4}$	5.8	319.3
ck	4.4	320.7
No	4.3	320.8

3400-WL, Mississippi

N _o	39	321.2
Ch	46	320.5
$\frac{1}{4}$	51	320.0
C	45	320.6
$\frac{1}{4}$	48	320.3
+7	46	320.5
+12	39	321.2
Ch	47	320.4
S _o	57	319.4

W Ch

S _o	40	321.1
+10	48	320.3
Ch	41	321.0
+15	36	321.5
$\frac{1}{4}$	43	320.8
C	40	321.1
$\frac{1}{4}$	46	320.5
Ch	35	321.6
N _o	32	321.9

W $\frac{1}{4}$

N _o	28	322.3
Ch	32	321.9
$\frac{1}{4}$	41	321.0
C	36	321.5
$\frac{1}{4}$	40	321.1
+7	29	322.2
Ch	29	322.2
S _o	30	322.1

C Ch

S _o	30	322.1
Ch	25	322.6
+10	21	323.0
+13	30	322.1
$\frac{1}{4}$	37	321.4
C	27	322.4
+9	24	322.7
+12	34	321.7
$\frac{1}{4}$	34	321.7
+10	28	322.3
Ch	33	321.8
+16	29	322.2
N _o	22	322.9

337.34

0425

Cl	11.4	325.9
No	10.6	326.7
0450		
No	9.0	328.3
Cl	9.5	327.9
+17	10.0	327.3
+21	11.1	326.2
+4	11.5	325.8
+14	11.4	325.9
+20	9.2	328.1
C	9.0	328.3
$\frac{1}{2}$	9.7	327.6
Cl	10.5	326.8
S ₀	10.0	327.3

0475

S ₀	8.0	329.3
Cl	7.8	329.5
$\frac{1}{2}$	8.2	329.1
C	8.0	329.3
+8	8.1	329.2
+13	10.4	326.9
$\frac{1}{4}$	10.6	326.7
+5	10.1	327.2
+7	8.4	328.9

23

Cl	7.9	329.4
No	7.4	329.9
1700		
No	6.3	331.0
Cl	6.3	331.0
+19	6.7	330.6
+24	9.8	327.5
$\frac{1}{2}$	9.9	327.4
+14	9.4	327.9
+19	5.6	331.7
C	5.6	331.7
$\frac{1}{2}$	6.6	330.7
Cl	7.4	329.9
S ₀	7.0	330.3

1725

S ₀	4.7	332.6
Cl	4.6	332.7
$\frac{1}{2}$	4.8	332.5
C	4.6	332.7
+9	4.5	332.8
+12	9.0	328.3
$\frac{1}{4}$	9.5	327.8
+5	9.1	328.2
+7	6.1	331.2

337.34

1+25

ck	5.1	332.2
N _o	4.5	332.8
1+50		
N _o	3.9	333.4
ck	4.9	332.4
+20	4.5	332.8
+21	8.1	329.2
+23	8.7	328.6
$\frac{1}{4}$	9.1	328.2
+15	8.7	328.6
+17	3.8	333.5
C	4.3	333.6
$\frac{1}{4}$	4.4	332.9
+12	3.6	333.7
ck	4.8	332.5
S ₀	4.1	333.2

1+75

S ₀	2.7	334.6
ck	2.1	335.2
+20	3.0	334.3
$\frac{1}{4}$	2.1	335.2
C	2.8	334.5
+10	3.1	336.2
+12	7.9	329.4

21

+14	8.6	328.7
14	8.7	328.6
+13	8.3	329.0
+6	7.0	330.3
+8	3.4	333.9
ck	3.7	333.6
N _o	3.5	333.8

2+00

N _o	3.5	333.8
ck	3.3	334.0
+18	3.5	333.8
+20	6.4	330.9
+25	7.6	329.7
$\frac{1}{4}$	7.8	329.5
+14	7.9	329.4
+15	7.4	329.9
+19	2.5	334.8
C	2.3	335.0
$\frac{1}{4}$	2.2	335.1
ck	2.2	335.1
+11	1.8	335.5
S ₀	1.0	336.3

337.34

2+25

S.	2.0	335.3
Ch	0.6	336.7
+10	0.4	336.9
$\frac{1}{4}$	2.1	335.2
C	2.0	335.3
+9	2.6	334.7
+11	7.1	330.2
+12	7.5	329.8
$\frac{1}{4}$	7.9	329.4
+3	7.6	329.7
+7	6.1	331.2
+9	3.5	333.8
Ch	3.7	333.6
N.	3.3	334.0

3+50

N.	5.1	332.2
Ch	4.5	332.8
+17	3.8	333.5
+19	6.6	330.7
+22	7.7	329.6
$\frac{1}{4}$	8.3	329.0
+14	8.1	329.2
+16	7.5	329.8
+18	2.8	334.5

25

C	2.9	334.4
$\frac{1}{4}$	0.9	336.4
+1	2.1	335.2
Ch	2.0	335.3
S.	1.7	335.6

2+75

S.	0.3	337.0
Ch	1.8	335.5
$\frac{1}{4}$	3.4	333.9
C	4.0	333.3
+8.5	4.3	333.0
+10.5	7.6	329.7
+12	8.2	329.1
$\frac{1}{4}$	8.6	329.7
+5	7.9	329.4
+9	5.2	332.1
Ch	6.2	331.1
N.	6.0	331.3

3400 = W.L. Louisiana

No	7.6	329.7
ck	7.6	329.7
+19	7.5	329.8
+22	8.5	328.8
$\frac{1}{4}$	8.9	328.4
+17	8.4	328.9
+19	5.9	331.4
C	5.6	331.7
$\frac{1}{4}$	4.6	332.7
ck	4.2	333.1
So	2.6	334.7

W.ck

So	4.1	333.2
ck	5.1	332.2
$\frac{1}{4}$	6.1	331.2
C.	6.7	330.6
+8	7.1	330.2
+10	8.3	329.0
$\frac{1}{4}$	9.1	328.2
ck	8.9	328.4
No	9.2	328.1

W.ck

No	9.4	327.9
ck	9.4	327.9
+21	9.1	328.2
$\frac{1}{4}$	9.4	327.9
+15	9.0	328.3
+20	7.4	329.9
C	7.3	330.0
$\frac{1}{4}$	7.2	330.1
ck	6.5	330.8
So	5.9	331.4

Ck

So	7.0	330.3
ck	7.2	330.1
$\frac{1}{4}$	8.0	329.3
C	8.0	329.3
+8	8.1	329.2
+12	9.5	327.8
$\frac{1}{4}$	9.8	327.5
+7	9.3	328.0
ck	9.7	327.6
No	9.7	327.6

337.34

E 1/4 La.

N.	10.1	327.2
ck	10.0	327.3
1/4	10.1	327.2
C	9.1	328.2
1/4	9.8	327.5
ck	8.5	328.8
So	8.4	328.9

E ck.

So	9.8	327.5
ck	10.0	327.3
1/4	10.3	327.0
C	10.2	327.1
1/4	10.3	327.0
ck	10.3	327.0
No	10.4	326.9

E. line La. 0+00

N.	10.8	326.5
ck	10.7	326.6
1/4	10.4	326.9
C	10.8	326.5
1/4	10.9	326.4
ck	10.6	326.7
So	10.7	326.6

0+25

So	12.5	324.8
ck	12.2	325.1
1/4	11.9	325.4
C	11.5	325.8
1/4	11.0	326.3
+6	10.9	326.4
+10	12.0	325.3
ck	11.9	325.4
No	11.4	325.9

0+50

No	11.8	325.5
ck	12.3	325.0
+15	12.3	325.0
+21	11.3	326.0
1/4	11.2	326.1
+16	11.0	326.3
+21	12.2	325.1
C	12.7	324.6
1/4	12.4	324.9
T.P. 6.09	330.48 12.95	324.39
ck	6.5	324.0
+5	7.3	323.2
+10	7.3	323.2
So	5.9	324.6

27

0+75

So	7.3	323.2
Ch	7.4	323.1
$\frac{1}{4}$	7.7	322.8
C	6.6	323.9
+5	6.5	324.0
+11	4.2	326.3
$\frac{1}{4}$	4.3	326.2
+18	4.6	325.9
+20	5.5	325.0
Ch	6.0	324.5
N.	5.8	324.7

1+0.0

N.	6.4	324.1
Ch	6.6	323.9
+12	6.4	324.1
+20	4.4	326.1
$\frac{1}{4}$	4.7	325.8
+15	4.6	325.9
+21	6.8	323.7
C	7.3	323.2
$\frac{1}{4}$	7.7	322.8
Ch	7.3	323.2
So	8.8	321.7

1+25

So	8.4	322.1
Ch	9.0	321.5
+18	8.5	322.0
$\frac{1}{4}$	7.2	323.3
+9	6.4	324.1
+14	7.2	323.3
C	7.6	322.9
+6	7.5	323.0
+13	4.7	325.8
$\frac{1}{4}$	5.0	325.5
+7	4.8	325.7
+11	6.8	323.7
Ch	6.9	323.6
N.	6.5	324.0

1+50

N.	7.0	323.5
Ch	7.2	323.3
+14	6.8	323.7
+20	5.1	325.4
$\frac{1}{4}$	5.1	325.4
+13	4.9	325.6
+17	6.7	323.8
C	7.5	323.0
+18	6.8	323.7

330.48

1+50

1/4	8.2	322.3
Ch	9.0	321.5
So	9.2	321.3

1+75

So	8.6	321.9
Ch	8.2	322.3
+7	9.2	321.3
1/4	8.8	321.7
+8	7.7	322.8
+20	8.8	321.7
C	8.8	321.7
+5	8.7	321.8
+1A	5.0	325.5
1/4	5.0	325.5
+9	4.7	325.8
+19	7.4	323.1
Ch	7.3	323.2
1/6	7.7	322.8

1+93

So	10.0	320.5
Ch	9.5	321.0

29

2+00

1/4	8.2	322.3
Ch	8.0	322.5
+13	7.3	323.2
+20	4.4	326.1
1/4	4.7	325.8
+13	4.8	325.7
+24	9.2	321.3
C	9.4	321.1
1/4	10.1	320.4
Ch	10.1	320.4
+13	10.8	319.7
So	12.1	318.4

2+09

So	10.2	320.3
+7	11.4	319.1
+12	11.4	319.1
Ch	11.0	319.5

2+25

So	9.6	320.9
Ch	10.5	320.0
1/4	10.2	320.3
+6	9.1	321.4
C	9.5	321.0
+4	9.1	321.4

330.48

2+25

C+14	4.6	325.9
4	4.8	325.7
+8	4.7	325.8
+13	7.9	322.6
ck	8.5	322.0
No.	8.3	322.2

2+50

No.	7.9	322.6
+9	8.4	322.1
ck	8.5	322.0
+13	9.1	321.4
+20	4.5	326.0
4	4.7	325.8
+14	4.8	325.7
+25	8.5	322.0
0	8.7	321.8
4	9.4	321.1
ck	9.5	321.0
So	9.4	321.1

2+75

30

So.	7.6	322.9
ck	9.2	321.3
4	7.8	322.7
+7	7.3	323.2
+14	8.5	322.0
C	8.4	322.1
+5	8.1	322.4
+12	4.6	325.9
4	4.8	325.7
+5	4.6	325.9
+12	8.3	322.2
ck	8.2	322.3
No.	7.7	322.8

3400-WL. Texas

No.	7.2	323.3
ck	7.5	323.0
+13	7.5	323.0
+20	4.7	325.8
4	4.9	325.6
+16	4.8	325.7
+22	7.0	323.5
C	7.3	323.2
4	7.5	323.0
ck	8.5	322.0
So	8.6	321.9

W. Ct. Texas

50	83	322.2
Ch	80	322.5
$\frac{1}{4}$	77	322.8
C	74	323.1
+5	69	323.6
+10	54	325.1
$\frac{1}{4}$	52	325.3
+6	51	325.4
+11	72	323.3
Ch	74	323.1
No	73	323.2
W $\frac{1}{4}$		
No	64	324.1
Ch	61	324.4
$\frac{1}{4}$	52	325.3
C	60	324.5
$\frac{1}{4}$	64	324.1
Ch	70	323.5
So	75	323.0

Ct. r

50	73	323.2
Ch	68	323.7
$\frac{1}{4}$	62	324.3
C	54	325.1
$\frac{1}{4}$	51	325.4
Ch	56	324.9
No	61	324.4
E $\frac{1}{4}$		
No	60	324.5
Ch	54	325.1
$\frac{1}{4}$	50	325.5
C	52	325.3
$\frac{1}{4}$	62	324.3
Ch	68	323.7
50	72	323.3
E Ch		
50	73	323.2
Ch	69	323.6
$\frac{1}{4}$	64	324.1
C	52	325.3
$\frac{1}{4}$	48	325.7
+10	49	325.6
+15	57	324.8
Ch	62	324.3
No	64	324.1

E. 1170 Texas - 0100

No	54	325.1
4	59	324.6
+16	58	324.7
+21	47	325.8
$\frac{1}{4}$	45	326.0
+16	47	325.8
+20	53	325.2
C	54	325.1
$\frac{1}{4}$	59	324.6
4	66	323.9
So	69	323.6

0125

So	61	324.4
4	57	324.8
$\frac{1}{4}$	54	325.1
C	50	325.5
+7	49	325.6
+11	43	326.2
$\frac{1}{4}$	39	326.6
+12	50	325.5
4	42	326.3
+5	43	326.2
No	54	325.1

0150

No	58	324.7
4	50	325.5
+15	46	325.9
+18	38	326.7
$\frac{1}{4}$	33	327.2
+16	36	326.9
+20	43	326.2
C	44	326.1
$\frac{1}{4}$	49	325.6
4	52	325.3
So	53	325.2

0175

So	48	325.7
4	45	326.0
$\frac{1}{4}$	43	326.2
C	39	326.6
+7	39	326.6
+11	29	327.6
$\frac{1}{4}$	25	328.0
4	44	326.1
+5	49	325.6
No	48	325.7

1700

No.	35	327.0
+11	20	328.5
Ch	10	328.7
+10	30	327.5
+16	32	327.2
+20	21	328.4
U	19	328.6
+16	23	328.2
+19	32	327.3
C	35	327.0
$\frac{1}{4}$	37	326.8
Ch	41	326.4
S.	41	326.4

1125

S.	36	326.9
Ch	33	327.2
$\frac{1}{4}$	29	327.6
C	27	327.8
+6	25	328.0
+11	13	329.2
$\frac{1}{4}$	08	329.7
+8	13	329.2
+12	32	327.3
U	40	326.5
No	39	326.6

1750

No	19	328.6	
+5	26	327.9	
Ch	17	328.8	
+13	21	328.4	
T.P. 11.38	341.43	0.43	330.05
+20	10.7	330.7	
4	10.5	330.9	
+14	11.0	330.4	
+20	12.9	328.5	
C	13.1	328.3	
$\frac{1}{4}$	13.5	327.9	
U	13.6	327.8	
S.	14.0	327.4	

1175

S.	13.5	327.9
Ch	13.1	328.3
$\frac{1}{4}$	12.8	328.6
C	12.4	329.0
+6	12.0	329.4
+17	9.5	331.9
$\frac{1}{4}$	9.1	332.3
+7	9.3	332.1
+13	12.6	328.8
U	13.0	328.4
No	13.3	328.1

341.43

2400

No.	109	330.5
+12	12.2	329.2
Ch	117	329.7
+13	109	330.5
+19	8.3	333.1
$\frac{1}{4}$	81	333.3
+17	85	332.9
+24	111	330.3
0	118	329.6
$\frac{1}{4}$	122	329.2
Ch	126	328.8
So	129	328.5

2475

So	119	329.6
Ch	118	329.6
$\frac{1}{4}$	117	329.7
0	108	330.6
+5	10.5	330.9
+12	7.7	333.7
$\frac{1}{2}$	7.2	334.2
+8	7.2	334.2
+13	9.7	331.7
Ch	114	330.0
	117	330.7

34

2450

No.	9.5	331.9
+8	9.3	332.1
+16	8.2	333.2
Ch	80	333.4
+14	8.2	333.2
+20	6.5	334.9
$\frac{1}{4}$	6.2	335.2
+17	6.7	334.7
+23	9.3	332.1
0	9.8	331.6
$\frac{1}{4}$	10.3	331.1
Ch	104	331.0
So	10.9	330.5

2475

So	9.6	331.8
Ch	9.4	332.0
$\frac{1}{2}$	9.1	332.3
0	8.9	332.5
+5	8.6	332.8
+14	5.6	335.8
$\frac{1}{4}$	5.7	336.3
+7	5.3	336.1
+14	8.2	333.2
Ch	8.8	332.6
No	9.1	332.3

3100 = N.L. Arizona

No	7.3	334.1
ct	6.7	334.7
+12	6.9	334.5
+17	4.1	337.3
$\frac{1}{2}$	3.8	337.6
+15	4.4	337.0
+21	7.1	334.3
C	7.6	333.8
$\frac{1}{2}$	8.1	333.3
ct	8.2	333.2
S.	8.8	332.6

W/ct

S.	8.0	333.4
ct	7.6	333.8
$\frac{1}{2}$	7.4	334.0
C	6.9	334.6
+5	6.4	335.0
+12	3.3	338.1
$\frac{1}{4}$	3.0	338.4
+9	3.2	338.2
+15	5.6	335.8
ct	6.3	335.1
No	6.1	335.3

W/ct

No	5.7	335.7
ct	6.0	335.4
+12	5.8	335.6
18	3.4	338.0
$\frac{1}{2}$	2.1	339.3
+15	2.5	338.9
+23	5.3	336.1
C	6.1	335.3
$\frac{1}{2}$	6.7	334.7
ct	7.0	334.4
S.	7.1	334.3

POSTED

C/A

S.	6.4	335.0
ct	6.3	335.1
$\frac{1}{2}$	5.8	335.6
C	5.2	336.2
+4	4.9	336.5
+12	1.8	339.6
$\frac{1}{4}$	1.4	340.0
+8	1.8	339.6
+15	4.6	336.8
ct	3.7	337.7
No	4.4	337.0

E 1/2 Arizona

No	3.2	338.2
Ch	3.0	338.4
+12	3.1	338.3
+18	1.0	340.4
1/4	0.6	340.8
+15	1.0	340.4
+24	4.0	337.4
C	4.5	336.9
1/2	4.5	336.9
Ch	5.2	336.2
S.	6.3	336.1

E Ch.

S.	4.6	336.8
Ch	4.3	337.1
1/2	3.6	337.8
C	3.3	338.1
+3	3.0	338.4
+12	0.3	341.1
1/4	4.01	341.5
+9	0.2	341.2
+10	2.5	338.9
Ch	2.9	338.5
No	2.5	338.9

T.P. 11.28 351.50 1.21 340.22

E. line Arizona = 0400

No	11.2	340.2
Ch	10.9	340.6
+9	11.3	340.2
+16	9.4	342.1
1/4	9.2	342.3
+19	9.4	342.1
+24	12.0	339.5
C	12.3	339.2
1/4	12.4	339.1
Ch	13.4	338.1
S.	13.6	337.9

0+25

S.	10.9	340.6
Ch	11.2	340.3
1/4	10.9	340.6
C	10.7	340.8
+3	10.5	341.0
+11	7.5	344.0
1/4	7.2	344.3
+10	7.4	344.1
+16	9.6	341.9
Ch	9.5	342.0
No	9.8	341.7

	1+25	
$\frac{1}{4}+6$	12.0	351.4
+11	10.2	353.2
Ch	9.0	354.4
No.	9.9	353.5
	1+50	
No.	6.3	357.1
Ch	6.7	356.7
+17	6.9	356.5
+21	10.0	353.4
$\frac{1}{4}$	9.6	353.8
+16	9.9	353.5
+18	8.4	355.0
C	8.6	354.8
$\frac{1}{4}$	8.0	355.4
Ch	9.6	353.8
50	9.7	353.7
	1+75	
50	5.8	357.6
Ch	6.9	356.5
+7	6.4	357.0
$\frac{1}{4}$	3.7	359.7
C	5.2	358.2
+8	5.1	358.3
+11	8.5	354.9

$\frac{1}{4}$	8.0	355.4
+5	8.5	354.9
+8	4.7	358.7
Ch	5.3	358.1
No.	4.0	359.4
	1+88	
No.	1.8	361.6
Ch	3.8	359.6
	1+00	
No.	1.6	361.8
Ch	1.7	361.7
+19	1.1	362.3
+23	6.6	356.8
$\frac{1}{4}$	6.3	357.1
+15	6.7	356.7
+18	2.6	360.8
C	2.5	360.9
$\frac{1}{4}$	1.4	362.0
+10	3.2	360.2
Ch	4.0	359.4
No.	3.5	359.9
TP 9.0V	370.38	2.08
		311.36

370.38

2+25

50	8.1	362.3
Ch	7.8	362.6
+5	8.2	362.2
+20	6.3	364.1
$\frac{1}{4}$	6.2	364.2
+10	6.6	363.8
+13	7.3	363.1
C	7.2	363.2
+9	7.5	362.9
+12	11.5	358.9
$\frac{1}{4}$	11.3	359.1
+5	11.4	359.0
+8	6.6	363.8
Ch	6.2	364.2
No	6.7	363.7

2+50

No	4.4	366.0
Ch	4.3	366.1
+20	5.1	365.3
+23	9.2	361.2
$\frac{1}{4}$	9.1	361.3
+14	9.3	361.1
+17	5.5	364.9

39

C	4.9	365.5
+15	5.3	365.1
+21	4.2	366.2
$\frac{1}{4}$	4.7	365.7
Ch	5.4	365.0
50	5.9	364.5

2+75

50	4.3	366.1
Ch	4.3	366.1
+18	4.6	365.8
+23	2.9	367.5
$\frac{1}{4}$	3.0	367.4
C	3.3	367.1
+8	3.8	366.6
+15	7.8	362.6
$\frac{1}{4}$	7.6	362.8
+3	7.8	362.6
+7	7.8	367.6
Ch	7.9	367.5
No	7.7	367.7

2+25

50	8.1	362.3
Ch	7.8	362.6
+5	8.2	362.2
+20	6.3	364.1
$\frac{1}{4}$	6.2	364.2
+10	6.6	363.8
+13	7.3	363.1
C	7.2	363.2
+9	7.5	362.9
+12	11.5	358.9
$\frac{1}{4}$	11.3	359.1
+5	11.4	359.0
+8	6.6	363.8
Ch	6.2	364.2
No	6.7	363.7

2+50

No.	+4	366.0
Ch	+3	366.1
+20	5.1	365.3
+23	9.2	361.2
$\frac{1}{4}$	9.1	361.3
+14	9.3	361.1
+17	5.5	364.9

C	4.9	365.5
+15	5.3	365.1
+21	4.2	366.2
$\frac{1}{4}$	4.7	365.7
Ch	5.4	365.0
50	5.9	364.5

2+75

50	4.3	366.1
Ch	4.3	366.1
+18	4.6	365.8
+23	2.9	367.5
$\frac{1}{4}$	3.0	367.4
C	3.3	367.1
+8	3.8	366.6
+15	7.8	362.6
$\frac{1}{4}$	7.6	362.8
+3	7.8	362.6
+7	2.8	367.6
Ch	2.9	367.5
No	2.7	367.7

3400 Hamilton
W.L. California

No	1.5	368.9
Ch	2.2	368.2
+12	2.0	368.4
+14	1.1	369.3
+20	0.9	369.5
+23	6.0	364.4
$\frac{1}{4}$	6.1	364.3
+15	6.5	363.9
+19	3.0	367.4
C	3.0	367.4
$\frac{1}{4}$	2.5	367.9
+17	1.6	368.8
Ch	2.1	368.3
50	3.2	367.2
	W.L. Ch	
50	2.6	367.8
Ch	1.9	368.5
$\frac{1}{4}$	1.9	368.5
C	2.5	367.9
+9	2.5	367.9
+12	6.0	364.4
$\frac{1}{4}$	5.3	365.1
+5	5.4	365.0
+8	1.7	368.7

Ch	1.7	368.7
No	2.2	368.2
	W.L. Ch + 5	
No	2.4	368.0
Ch	3.0	367.4
$\frac{1}{4}$	5.2	365.2
	W $\frac{1}{4}$	
No	2.2	368.2
Ch	2.9	367.5
+12	4.8	365.6
$\frac{1}{4}$	4.9	365.5
+14	5.4	365.0
+17	2.3	368.1
C	2.3	368.1
+6	1.3	369.1
$\frac{1}{4}$	1.1	369.3
+17	0.7	369.7
Ch	1.4	369.0
50	2.2	368.2
	Ch	
50	2.1	368.3
Ch	0.9	369.5
+17	1.2	369.2
$\frac{1}{4}$	0.5	369.9
C	1.6	368.8

Chr Cal.

Chr+8		1.5	368.9
+11		4.6	365.8
$\frac{1}{4}$		4.3	366.1
+6		4.5	365.9
Ch		3.4	367.0
No		2.3	368.1
T.R	9.45	377.73	2.10 368.28
		E $\frac{1}{4}$	
No		6.2	371.5
Ch		6.3	371.4
+7		7.5	370.2
+16		6.2	371.5
+19		6.5	371.2
+22		11.3	366.4
$\frac{1}{4}$		11.1	366.6
+15		11.4	366.3
+18		7.4	370.3
C		8.1	369.6
$\frac{1}{4}$		7.0	370.7
+9		8.3	369.4
Ch		8.6	369.1
S.		9.1	368.6
CHK BM. S.E. Cal.		5.63	372.10 372.09

E. Ch.

S.		8.0	369.7
Ch		7.9	369.8
+6		8.2	369.5
$\frac{1}{4}$		6.1	371.6
C		7.5	370.2
+8		7.2	370.5
+11		10.9	366.8
$\frac{1}{4}$		10.7	367.0
+5		11.1	366.6
+9		7.3	370.4
+22		7.2	370.5
Ch		6.1	371.6
No			371.6
		^{6.1} Hamilton	
		E. line Cal = 0400	
No		6.9	370.8
Ch		7.1	370.6
+16		7.2	370.5
+21		10.1	367.6
$\frac{1}{4}$		10.1	367.6
+14		10.5	367.2
+17		8.5	369.2
C		7.3	370.4
2d		6.1	371.6
+15		6.9	370.8
Ch		5.8	371.9
S.		6.7	371.0

37773

0+25

So	6.7	371.0
Ch	7.0	370.7
$\frac{1}{4}$	6.8	371.9
C	6.8	370.9
+P	6.9	370.8
+12	9.6	368.1
$\frac{1}{2}$	9.1	368.6
+5	8.9	368.8
+8	5.1	372.6
Ch	6.4	371.3
No	5.5	372.2

0+50

No	5.4	372.3
Ch	5.6	372.1
+17	4.8	372.9
+21	8.5	369.2
$\frac{1}{4}$	8.8	369.5
+13	9.0	368.7
+17	5.7	372.0
C	5.0	372.7
+17	5.7	372.0
$\frac{1}{4}$	5.3	372.4
+19	4.6	373.1
Ch	5.2	372.5
+10	6.2	371.5
Si	6.0	371.7

 $\frac{1}{11}$
 $\frac{58}{58}$

 DAVIS
 Dorman
 Collett
 Day

7.45

379.54

563

372.10

4.2

0+75

So	7.6	371.9
Ch	7.6	371.9
+15	7.6	371.9
+22	6.1	373.4
$\frac{1}{2}$	6.9	372.6
C	7.0	372.5
+8	7.1	372.4
+13	10.0	369.5
$\frac{1}{4}$	9.4	370.1
+5	10.0	369.5
+9	6.4	373.1
+25	6.0	373.5
Ch	5.7	373.8
+8	4.6	374.9
No	6.5	373.0

1+00

No	6.2	373.3
Ch	6.2	373.3
+17	5.6	373.9
+21	9.1	370.4
$\frac{1}{4}$	8.9	370.6
+14	9.5	370.0
+18	6.4	372.9

379.54		
1400		
C	6.3	373.2
TR	6.4	373.1
$\frac{1}{4}$	3.9	375.6
CL	6.6	372.9
So	5.8	373.7
1425		
So	6.6	372.9
CL	6.4	373.1
+15	6.0	373.5
+19	4.8	374.7
$\frac{1}{4}$	5.2	374.3
C	5.5	374.0
+9	4.7	374.8
+13	9.0	370.5
$\frac{1}{2}$	8.1	371.4
+7	8.4	371.1
+9	5.5	374.0
CL	6.0	373.5
No	4.9	374.6
1450		
No	4.3	375.2
+10	3.8	375.7
CL	5.5	374.0
+18	5.4	374.1

+21	8.2	371.3
$\frac{1}{4}$	7.5	372.0
+14	8.5	371.0
+18	5.5	374.0
C	5.6	373.9
$\frac{1}{4}$	4.8	374.7
+17	6.0	373.5
CL	4.9	374.6
So	6.0	373.5
1475		
So	4.3	375.2
+8	5.6	373.9
CL	5.7	373.8
+14	5.4	374.1
+20	4.5	375.0
$\frac{1}{4}$	4.8	374.7
C	5.3	374.2
+9	5.4	374.1
+13	7.9	371.6
$\frac{1}{4}$	6.8	372.7
+7	5.7	373.8
+10	4.0	375.5
+15	4.8	374.7
CL	5.4	374.1
No	5.2	374.3

379.54

3400

No.	5.3	374.2
U	4.5	375.0
+17	5.0	374.5
+21	7.2	372.3
$\frac{1}{4}$	6.3	373.2
+14	7.3	372.2
+18	4.7	374.8
C	4.3	375.2
+14	5.1	374.4
+20	3.3	376.2
$\frac{1}{4}$	3.4	376.1
+8	3.2	376.3
U	5.6	373.9
So	5.4	374.1

2+25

So	4.4	375.1
+4	4.9	374.6
U	4.6	374.9
+5	5.3	374.2
$\frac{1}{4}$	4.1	375.4
C	4.8	374.7
+9	5.0	374.5
+12	6.7	372.8
$\frac{1}{4}$	6.2	373.3

44

+5	6.9	372.6
+10	5.2	374.3
U	4.9	374.6
No.	5.2	374.3

2+50

No	4.9	374.6
U	5.2	376.3
+13	5.2	374.3
+20	8.7	375.8
+22	6.1	373.4
$\frac{1}{4}$	5.7	373.8
+14	6.5	373.0
+17	4.9	374.6
C	4.8	374.7
$\frac{1}{4}$	4.5	375.0
U	5.0	374.5
So	5.2	374.3

2+75

So	5.1	374.4
U	5.0	374.5
$\frac{1}{4}$	4.8	374.7
C	4.2	375.3
+9	4.5	375.0
+11	5.9	373.6

379.54

2775

1/4	5.6	373.9
+5	6.1	373.4
+9	5.0	374.5
+14	5.0	374.5
Ch.	4.6	374.9
+5	4.2	375.3
No	5.0	374.5
30	5.0	374.5
+14	3.5	376.0
+16	4.8	374.7
Ch	5.2	374.3
37000 W.L. Oregon		
No	5.2	374.3
Ch	5.0	374.5
+20	5.2	374.3
+22	5.9	373.6
1/4	5.3	374.2
+14	5.8	373.7
+16	5.1	374.1
C	4.8	374.7
+7	4.8	374.7
+12	4.1	375.3
+20	5.2	374.8
1/4	4.9	374.6
Ch	4.9	374.6
30	5.0	374.5

2785

37000 W.L. Oregon

45

W.L. Ch

5.0	5.1	374.4
Ch	+9	374.6
1/4	5.0	374.5
C	5.1	374.4
+6	5.2	374.3
+10	5.7	373.8
1/4	5.2	374.3
+6	5.8	373.7
+9	5.0	374.5
+23	4.6	374.9
Ch.	4.4	375.1
No	3.5	376.0
Ch + 8		
No	3.0	376.5
Ch	4.3	375.2
+18	5.0	374.5
+21	5.7	373.8
1/4	5.3	374.2
Ch + 10		
No	5.2	374.3
Ch	5.6	374.0
+23	5.7	373.8
1/4	5.2	374.3

	W ₂	
No.	5.1	374.4
U	5.3	374.2
+20	5.5	374.0
+22	5.8	373.7
$\frac{1}{4}$	5.1	374.4
+14	5.6	373.9
+20	5.4	374.1
C	5.0	374.5
$\frac{1}{4}$	4.7	374.8
U	5.0	374.5
50	5.0	374.5
	Ch	
50	4.8	374.7
U	5.0	374.5
$\frac{1}{4}$	4.9	374.6
C	4.7	374.8
+7	4.8	374.7
+10	5.4	374.1
$\frac{1}{2}$	5.0	374.5
+2	5.1	374.4
+4	5.5	374.0
+7	4.9	374.6
U	4.7	374.8
No	4.5	375.0

	E _{1/4}	
H-	5.1	374.4
U	5.4	374.1
+21	5.0	374.5
+20	5.4	374.1
+25	4.8	374.7
$\frac{1}{4}$	4.8	374.7
+14	5.1	374.4
+17	4.4	375.1
C	4.4	375.1
$\frac{1}{4}$	4.6	374.9
+12	5.0	374.5
U	4.2	375.3
50	3.7	375.6
	E Ch.	
50	3.8	375.7
U	4.2	375.3
+3	4.5	375.0
+15	5.0	374.5
$\frac{1}{4}$	4.6	374.9
U	4.3	375.2
+8	4.2	375.3
+10	4.9	374.6
$\frac{1}{4}$	4.6	374.9

379.54

E Cl

1/4 + 6	5.1	374.4
+ 8	4.6	374.9
Cl	4.7	374.8
No	5.0	374.5

E line Oregon - 0 + 00

No	5.0	374.5
Cl	4.4	375.1
+ 19	4.1	375.4
+ 21	4.9	374.6
1/4	4.5	375.0
+ 14	4.5	374.7
+ 16	4.1	375.4
C	4.1	375.4
1/4	4.2	375.3
Cl	4.2	375.3
No	3.8	375.7

0 + 25

5.0	3.7	375.8
Cl	4.1	375.4
1/4	4.3	375.2
+ 10	4.9	374.6
+ 20	4.8	374.7
C	3.5	376.0
+ 3	3.6	375.9

47

+ 10	4.9	374.6
1/4	4.4	375.1
+ 6	5.0	374.5
Cl	4.8	374.7
No	3.9	375.6

0 + 50

No	4.5	375.0
Cl	4.6	374.9
+ 21	4.9	374.6
1/4	4.4	375.1
+ 14	4.5	375.0
+ 17	4.8	374.7
+ 20	4.3	375.2
C	3.8	375.7
+ 12	3.4	376.1
+ 18	4.6	374.9
+ 21	3.8	375.7
1/4	4.0	375.5
Cl	4.2	375.3
5.0	3.6	375.9

	0175	
50	32	376.3
4	38	375.7
+17	43	375.2
+22	33	376.2
4	30	376.5
+4	33	376.2
+6	40	376.5
C	46	374.9
+10	49	374.6
4	43	375.2
+6	47	374.8
4	44	375.1
No	34	376.1
	1700	
No	42	375.3
4	44	375.1
+20	47	374.8
4	42	375.3
+17	47	374.8
+20	42	375.3
C	38	375.7
+2	36	375.9
+10	20	377.5
+14	48	374.7

+16	48	374.7
+20	36	375.9
4	39	375.6
+2	40	375.5
+4	30	376.5
+8	36	375.9
4	38	375.7
50	27	376.8
	1725	
50	20	377.5
+3	28	376.7
4	31	376.4
4	38	375.7
+8	49	374.6
+14	40	375.5
C	42	375.3
+10	45	375.0
4	41	375.4
+9	47	374.8
+19	44	375.1
4	38	375.7
No	36	375.9

379.54

1+50

No	4.2	375.3
U	4.2	375.2
+20	4.7	374.8
$\frac{1}{4}$	4.1	375.4
+17	4.6	374.9
C	3.4	376.1
+15	4.0	375.5
$\frac{1}{4}$	3.2	376.3
U	2.7	376.8
50	2.1	377.4

1+75

50	2.7	376.8
U	3.3	376.2
+15	3.8	
$\frac{1}{4}$	3.5	376.0
C	3.8	375.7
+7	3.9	375.6
+10	4.3	375.2
$\frac{1}{4}$	4.0	375.5
+7	4.5	375.0
+13	3.9	375.6
U	4.2	375.3
No	4.3	375.2

49

2+00

No	4.0	375.5
U	4.1	375.4
+20	4.6	374.9
$\frac{1}{4}$	4.0	375.5
+17	4.0	375.0
C	4.3	375.2
$\frac{1}{4}$	3.7	375.8
U	4.0	375.5
50	3.3	376.2

2+25

50	3.3	376.2
U	4.5	375.0
+12	4.2	375.3
+20	3.2	376.3
$\frac{1}{4}$	3.4	376.1
C	4.3	375.2
+10	4.6	374.9
$\frac{1}{4}$	3.8	375.7
+7	4.4	375.1
+12	3.4	376.1
+16	4.0	375.5
U	4.4	375.1
No	4.0	375.5

379.54

Σ + 50

No		4.1	375.4
4		4.2	375.3
+19		4.5	375.0
4		4.0	375.6
+17		4.5	375.0
+19		4.1	375.4
C		4.0	375.6
+15		3.9	375.6
+20		3.2	376.3
4		3.4	376.1
+5		4.1	375.4
Ch		4.1	375.4
S.		3.2	376.3
TP	375	378.89	4.40 375.14
		Σ + 75	
S.		3.3	375.6
Ch		3.8	375.1
+19		4.0	374.9
4		3.2	375.7
+13		2.7	376.2
+24		3.3	375.6
C		3.5	375.4
+8		3.6	375.3
+11		4.1	374.8
+13		3.7	375.2

50

4		3.4	375.5
+9		3.9	375.0
+17		3.3	375.6
Ch		3.3	375.6
No		3.4	375.5

Σ + 100 = 112.14410

No		3.5	375.4
Ch		3.6	375.3
+17		3.5	375.4
+20		3.9	375.0
+23		3.6	375.3
4		3.5	375.4
+14		3.7	375.2
+17		4.0	374.9
15		3.6	375.3
✓		3.6	375.3
4		3.2	375.7
Ch		3.5	375.4
5		3.7	375.2

378.89.

W. Ch. W. 1/4

50	3.8	375.1.
U	3.3	375.6
1/4	3.7	375.2
V	3.5	375.4
+8	3.6	375.3
+10	3.9	375.0
+12	3.7	375.2
1/4	3.4	375.5
+7	4.0	374.9
+10	3.5	375.4
U	3.6	375.3
N ₀	3.5	375.4
	U + 10	
N ₀	3.6	375.3
U	3.5	375.4
+15	3.6	375.3
+20	4.0	374.9
1/4	3.5	375.4
	W 1/4	
N ₀	4.0	374.9
U	4.0	374.9
+19	4.0	374.9
1/4	3.5	375.4
+12	3.7	375.2

51

+16	4.0	374.9
+19	3.7	375.2
C	3.4	375.5
1/4	3.3	375.6
+11	3.9	375.0
U	3.0	375.9
+3	2.3	376.6
50	3.4	375.5
	Ctr	
50	3.5	375.4
U	3.6	375.3
+10	4.0	374.9
+28	2.7	376.2
1/4	3.0	375.9
C	3.5	375.4
+7	3.5	375.4
+10	4.0	374.9
+13	3.6	375.3
1/4	3.4	375.5
+5	3.6	375.3
+7	3.9	375.0
+10	3.5	375.4
U	3.1	375.8
N ₀	3.1	375.8

E L

No.	39	375.0
Ch	39	375.0
+15	39	375.0
+18	41	374.8
+21	36	375.3
$\frac{1}{2}$	34	375.5
+14	38	375.1
+19	34	375.5
C	32	375.7
$\frac{1}{4}$	27	376.2
Ch	38	375.1
So	30	375.9

E CL

So	25	376.4
Ch	39	375.0
+19	37	375.2
$\frac{1}{2}$	30	375.9
+5	33	375.6
+7	40	374.9
+10	35	375.4
C	33	375.0
+8	32	375.7
+10	39	375.0
$\frac{1}{2}$	36	375.3

+7	42	374.7
+10	35	375.4
Ch	36	375.3
No	36	375.3

E. line Idaho 0+00

No.	31	375.8
Ch	35	375.4
+16	36	375.3
+20	42	374.7
+22	39	375.0
$\frac{1}{4}$	37	375.2
+13	40	374.9
+15	24	376.5
C	26	376.3
+11	37	375.2
$\frac{1}{2}$	32	375.7
Ch	38	375.1
So	22	376.7

0+25

So	39	375.0
Ch	39	375.0
+8	38	375.1
$\frac{1}{2}$	27	376.2
+9	38	375.1

378.89

0+25

C	3.4	375.5
+9	3.5	375.4
+11	4.2	374.7
+2	3.8	375.1
+8	4.3	374.6
+10	3.7	375.2
Ch	3.6	375.3
No	3.6	375.3

0+50

No.	3.7	375.2
Ch	3.3	375.6
+18	3.6	375.3
+20	4.5	374.4
$\frac{1}{4}$	4.0	374.9
+14	4.3	374.6
+16	3.2	375.7
C	3.2	375.7
$\frac{1}{4}$	3.7	375.2
+5	3.6	375.3
+19	2.0	376.9
Ch	2.0	376.9
50	4.0	374.9

53

0+75

50	3.4	375.5
+7	4.0	374.9
Ch	3.3	375.6
+10	3.9	375.0
$\frac{1}{4}$	3.8	375.1
+8	2.9	376.0
+16	3.5	375.4
C	2.8	376.1
+9	3.0	375.9
+10	4.1	374.8
$\frac{1}{4}$	4.0	374.9
+7	4.5	374.4
+9	3.8	375.1
Ch	3.7	375.2
No	3.8	375.1

1+0.0

No.	3.7	375.2
Ch	3.6	375.3
+18	3.8	375.1
+20	4.9	374.0
$\frac{1}{4}$	4.3	374.6
+14	4.7	374.2
+16	4.0	374.9
C	3.9	375.0
$\frac{1}{4}$	3.6	375.3

	1+00		
Ct	1	4.1	374.8
So		4.1	374.8
	1+25		
So		3.9	375.0
U		4.1	374.8
$\frac{1}{4}$		3.4	375.5
r10		4.0	374.7
C		3.8	375.1
+8		4.1	374.8
+10		4.7	374.2
$\frac{1}{2}$		4.6	374.3
+7		5.1	373.8
+9		4.3	374.6
U.		3.7	375.2
No		3.7	375.2
	1+50		
		3.8	375.1
		4.1	374.8
+15		4.3	374.6
+19		4.2	374.7
+21		5.1	373.8
$\frac{1}{4}$		4.7	374.2
+14		4.8	374.1
+16		3.8	375.1

C		3.9	375.0
+10		3.4	375.5
+18		4.2	374.7
$\frac{1}{4}$		4.0	374.9
U		4.1	374.8
So		4.1	374.8
	1+75		
So		3.2	375.7
U		2.9	376.0
+15		4.5	374.4
$\frac{1}{2}$		4.2	374.7
C		4.0	374.9
+9		4.4	374.5
+10		5.1	373.8
$\frac{1}{4}$		4.9	374.0
+6		5.5	373.4
+7		4.8	374.1
+18		4.4	374.5
U.		4.0	374.9
No		4.1	374.8

2+10

N.	36	375.3
Cl	40	374.9
+19	47	374.2
+21	58	373.1
$\frac{1}{4}$	51	373.8
+14	52	373.7
+15	45	374.4
C	40	374.9
+20	43	374.6
+23	34	375.5
$\frac{1}{4}$	3.0	375.9
Cl	4.9	374.0
50	45	374.4

2+25

20	+1	374.8
+8	50	373.9
Cl	5.1	373.8
+20	5.1	373.8
$\frac{1}{4}$	4.7	374.2
+7	4.9	374.0
+14	4.0	374.9
C	4.4	374.5
+9	4.5	374.4
+11	5.6	373.3

$\frac{1}{4}$	5.3	373.6
+6	5.9	373.0
+7	5.3	373.6
Cl	4.7	374.2
26	4.9	374.0

2+50

N.	5.4	373.5
Cl	5.0	373.9
+13	5.2	373.7
+15	5.6	373.3
+20	5.5	373.4
+21	6.2	372.7
$\frac{1}{4}$	5.7	373.2
+16	5.8	373.1
+18	3.9	375.0
C	3.9	375.0
+2	4.0	374.9
+3	4.3	374.6
+14	4.5	374.4
+15	5.0	373.9
$\frac{1}{4}$	4.9	374.0
+22	5.4	373.5
Cl	5.0	373.9
+14	3.2	375.7
50	3.1	375.8

2175

So	54	373.5
Ch	55	373.4
+6	5.1	373.8
+20	5.3	373.6
$\frac{1}{4}$	4.9	374.0
C	5.3	373.6
+10	5.5	373.4
+12	6.3	372.6
$\frac{1}{4}$	6.2	372.7
+6	6.5	372.4
+8	5.8	373.1
Ch	5.2	373.7
No.	5.8	373.1

3700 W.L. Utah

No.	6.3	372.6
+6	6.6	372.3
+8	6.0	372.9
Ch	5.6	373.3
+20	6.1	372.8
+22	7.2	371.7
$\frac{1}{4}$	6.4	372.5
+15	6.8	372.1
+17	5.8	373.1
e	5.7	373.2
+22	4.7	374.2

$\frac{1}{4}$	5.4	373.5
Ch	6.1	372.8
So	6.0	372.9
	W L Ch	
So	6.1	372.8
Ch	6.2	372.7
+16	6.0	372.9
+21	5.6	373.3
$\frac{1}{4}$	5.6	373.3
C	6.1	372.8
+10	5.5	373.4
+12	7.0	371.9
$\frac{1}{4}$	6.5	372.4
+6	7.1	371.8
+7	6.2	372.7
Ch	6.5	372.4
No.	6.8	372.1
	W $\frac{1}{4}$	
No.	6.7	372.2
Ch	7.1	371.8
+19	6.4	372.3
+21	7.6	371.3
Ch	6.8	372.1
+14	7.3	371.6
+17	7.0	371.9

37889

W $\frac{1}{2}$

C	67	372.2
$\frac{1}{4}$	58	373.1
U	60	372.9
S.	60	372.9

Ctr

50	58	373.1
U	58	373.1
$\frac{1}{4}$	60	372.9
+11	65	372.4
+13	62	372.7
C	66	372.3
+9	69	372.0
+11	75	371.4
$\frac{1}{4}$	72	371.9
+6	77	371.2
+8	73	371.6
+11	68	372.1
U	71	371.8
No	73	371.6

v 1317 S.W. Utah

5.43 373.46 ✓ 373.45

57

E $\frac{1}{4}$

No	73	371.6
U	72	371.7
+20	75	371.4
+21	81	370.8
$\frac{1}{4}$	74	371.5
+16	78	371.1
+18	73	371.6
C	70	371.9
#	66	372.3
U	65	372.4
S.	63	372.6

E U

S.	70	371.9
+5	69	372.0
+15	58	373.1
U	60	372.9
+12	74	371.5
$\frac{1}{4}$	67	372.2
+6	60	372.9
+8	66	372.3
+11	58	373.1
+21	66	372.3
+24	74	371.5
C	73	371.6

POSTED

37d.8c

C+10	7.6	371.3
+12	8.0	370.9
+15	7.7	371.2
$\frac{1}{4}$	7.5	371.4
+7	8.2	370.7
+9	7.3	371.6
U	7.3	371.6
No	7.7	371.2

Eline Utah = 0 + 0

No	7.8	371.1
U	8.2	370.7
+19	7.8	371.1
+21	8.2	370.7
$\frac{1}{4}$	7.8	371.1
+15	8.2	370.7
+17	7.8	371.1
C	7.6	371.3
+2	7.8	371.1
+5	6.8	372.1
+20	6.1	372.8
$\frac{1}{4}$	7.3	371.6
+17	7.5	371.4
U	7.0	371.9
50	6.9	372.0

58

0+10

50	6.5	372.4
+15	7.9	371.0
U	7.5	371.4

0+25

50	8.3	370.6
+10	8.4	370.5
U	7.4	371.5
+10	6.7	372.2
+25	8.3	370.6
$\frac{1}{4}$	8.3	370.6
+17	7.4	371.5
C	8.0	370.9
+9	7.6	371.3
+11	8.6	370.3
$\frac{1}{4}$	8.2	370.7
+5	8.5	370.4
+7	8.9	370.0
+10	8.5	370.4
U	8.7	370.2
No	8.6	370.3

370.88

0150

No	90	369.9
ck	9.1	369.8
+20	87	370.2
+21	9.1	369.8
$\frac{1}{2}$	86	370.3
+14	89	370.0
+16	92	369.7
+17	87	370.2
0	87	370.2
+2	9.0	369.9
+13	7.7	371.2
$\frac{1}{2}$	82	370.7
+7	8.3	370.6
+12	77	371.2
ck	83	370.6
+8	83	370.6
So	68	372.1

0175

So	78	371.1
+11	89	370.0
ck	8.8	370.1
+20	89	370.0
$\frac{1}{2}$	8.2	370.7
+17	90	369.9

59

+22	84	370.5
C	9.1	369.8
+10	9.3	369.6
+12	9.6	369.3
$\frac{1}{2}$	9.0	369.9
ck	9.6	369.3
No	9.7	369.2

1+00

No	10.7	368.2
ck	10.3	368.6
+19	10.1	368.8
+22	9.5	369.4
$\frac{1}{2}$	9.2	369.7
+14	9.7	369.2
+16	10.0	369.9
+18	9.1	369.8
C	9.1	369.8
22	10.0	368.9
+6	9.2	369.7
+21	8.8	370.1
$\frac{1}{2}$	9.5	369.4
+7	9.8	369.1
ck	8.2	370.7
So	9.3	369.6

374.10

2+00

No.	6.2	367.9
Ch	5.8	368.3
+17	6.0	368.1
$\frac{1}{4}$	5.3	368.8
C	5.7	368.4
$\frac{1}{4}$	5.0	369.1
+22	5.6	368.5
Ch	5.0	369.1
+15	2.1	372.0
50	2.2	371.9

2+25

50	4.3	369.8
Ch	5.7	368.4
$\frac{1}{4}$	4.7	369.4
C	5.5	368.6
+8	5.6	368.5
+10	6.1	368.0
$\frac{1}{4}$	5.3	368.8
+5	5.6	368.5
+10	5.7	368.2
+13	5.7	368.4
Ch	5.7	368.2
140	6.2	367.9

61

2+50

No.	6.1	368.0
Ch	6.0	368.1
$\frac{1}{4}$	5.5	368.6
+15	6.0	368.1
+16	6.2	367.9
+19	5.6	368.5
C	5.6	368.5
$\frac{1}{4}$	5.2	368.9
Ch	5.5	368.6
50	3.1	371.0

2+75

50	5.1	369.0
+10	4.2	369.9
Ch	4.7	369.2
+7	5.6	368.5
$\frac{1}{4}$	5.0	369.1
C	5.2	368.9
+9	5.4	368.7
+10	6.3	367.8
$\frac{1}{4}$	5.6	368.5
Ch	6.0	368.1
No	6.3	367.8

POSTED

3700 = W.L. Kansas

No	63	367.8
u	60	368.1
+14	60	368.1
+18	66	367.5
+20	63	367.8
$\frac{1}{2}$	57	368.4
+14	58	368.3
+17	65	367.6
+19	53	368.8
C	48	369.3
$\frac{1}{4}$	54	368.7
ck	53	368.8
50	50	369.1

W. cl.

50	51	369.0
+10	48	369.3
+18	55	368.6
ck	55	368.6
$\frac{1}{2}$	58	368.3
C	54	368.7
+8	55	368.6
+9	64	367.7
+11	65	367.6

VBM. SW Kansas 446 369.64 369.64

+14	57	368.4
$\frac{1}{4}$	60	368.1
+9	66	367.5
ck	60	368.1
No	61	368.0
	W $\frac{1}{2}$	
No	67	367.4
u	65	367.6
$\frac{1}{4}$	60	368.1
+13	60	368.1
+16	66	367.5
+19	55	368.6
C	57	368.4
$\frac{1}{4}$	57	368.4
u	55	368.6
50	54	368.7
	C+	
50	56	368.5
ck	56	368.5
+15	53	368.8
$\frac{1}{4}$	58	368.3
C	56	368.5
+8	58	368.3

	CH		
C+11		66	367.5
+14		60	368.1
$\frac{1}{4}$		60	368.1
Ch		59	368.2
No		59	368.2
	E $\frac{1}{4}$		
No		67	367.4
Ch		68	367.3
$\frac{1}{4}$		62	367.9
+13		61	368.0
+16		66	367.5
+19		54	368.7
C		56	368.5
+15		64	367.7
$\frac{1}{4}$		65	368.6
+18		45	369.6
Ch		55	368.6
+7		59	368.2
50		59	368.2

	E CH		
50		6.1	368.0
Ch		59	368.2
$\frac{1}{4}$		58	368.3
C		6.1	368.0
+8		6.1	368.0
+10		6.7	367.4
+13		6.4	367.7
$\frac{1}{4}$		6.2	367.9
+6		6.6	367.5
Ch		6.5	367.6
No		6.7	367.4

E line Kansas = 0400

No		6.9	367.2
Ch		6.0	368.1
$\frac{1}{4}$		6.3	367.8
+13		6.5	367.6
+16		6.9	367.2
+18		6.5	367.6
C		6.3	367.8
+9		5.3	368.8
$\frac{1}{4}$		5.8	368.3
Ch		6.1	368.0
50		6.2	367.9

37410

0+25

S.	65	367.6
+9	64	367.7
ck	50	369.1
+8	43	369.8
+19	53	368.8
$\frac{1}{4}$	5.1	369.0
C	62	367.9
+8	67	367.4
+10	7.4	366.7
$\frac{1}{4}$	6.5	367.6
+7	6.9	367.2
+12	6.4	367.7
ck	6.5	367.6
No	6.8	367.3

0+50

No	6.7	367.4
ck	6.7	367.4
+14	6.9	367.2
+17	7.5	366.6
+19	7.3	366.8
$\frac{1}{4}$	6.8	367.3
+14	7.0	367.1
+16	7.4	366.7
+19	6.3	367.8

64

+22	5.7	368.4
C	5.7	368.4
$\frac{1}{4}$	5.9	368.2
+5	6.1	368.0
+8	6.7	367.4
ck	6.4	367.7
50	6.4	367.7

0+75

S.	6.6	367.5
+15	6.5	367.6
ck	5.7	368.4
+12	4.6	369.5
$\frac{1}{4}$	6.1	368.0
+9	6.7	367.4
+14	6.0	368.1
C	6.0	368.1
+8	6.4	367.7
+9	7.4	366.7
$\frac{1}{4}$	6.9	367.2
+7	7.6	366.5
+10	6.8	367.3
ck	6.8	367.3
No	7.2	366.9

374.10

1+00

No	6.8	367.3
ck	7.2	366.9
+15	7.1	367.0
+20	7.7	366.4
$\frac{1}{4}$	7.0	367.1
+14	7.3	366.8
+17	7.7	366.4
+20	6.8	367.3
C	6.3	367.8
+12	6.2	367.9
+17	7.2	366.9
+23	6.7	367.4
$\frac{1}{4}$	6.6	367.5
+12	7.2	366.9
ck	6.6	367.5
+10	5.6	368.5
So	6.0	368.1
1+25		
So	7.5	366.6
ck	7.4	366.7
+20	7.1	367.0
$\frac{1}{4}$	6.4	367.7
+8	7.6	366.5
+13	7.4	366.7
+16	6.4	367.7

65

C	6.8	367.3
+6	7.3	366.8
+10	8.0	366.1
+12	7.7	366.4
$\frac{1}{4}$	7.5	366.6
+9	8.0	366.1
ck	7.6	366.5
No	7.7	366.4
1+50		
No	8.3	365.8
ck	7.5	366.6
$\frac{1}{4}$	7.8	366.3
+18	8.2	365.9
+20	7.3	366.8
C	6.7	367.4
+9	6.1	368.0
+15	6.8	367.3
$\frac{1}{4}$	6.7	367.4
+7	6.7	367.4
+12	7.4	366.7
ck	6.9	367.2
+6	6.4	367.7
So	7.2	366.9

374.10

1+62

50	71	367.0
+15	58	368.3
Ch	6.1	368.0
+9	72	366.9
$\frac{1}{2}$	67	367.4

1+75

50	74	366.7
Ch	7.4	366.7
+15	7.6	366.5
$\frac{1}{2}$	69	367.2
+5	70	367.1
+9	75	366.6
+14	7.1	367.0
C	6.8	367.3
+7	6.9	367.2
+9	82	365.9
$\frac{1}{4}$	80	366.1
+16	84	365.7
+14	7.8	366.3
Ch	8.1	366.0
No	82	365.9

66

2+00

No	85	365.6
Ch	8.0	366.1
+13	8.3	365.8
+14	8.6	365.5
$\frac{1}{2}$	81	366.0
+14	8.1	366.0
+17	8.8	365.3
+20	7.7	366.4
C	7.9	366.2
+20	7.0	367.1
$\frac{1}{4}$	7.1	367.0
+17	7.8	366.3
Ch	6.0	368.1
+6	5.3	368.8
50	6.5	367.6
	2+25	
50	7.7	366.4
Ch	8.5	365.6
+17	8.2	365.9
+21	7.4	366.7
$\frac{1}{2}$	7.4	366.7
+19	7.4	366.7
+25	8.5	365.6
C	8.6	365.5

37410

	2+25	
U+10	9.0	365.1
$\frac{1}{4}$	8.5	365.6
U	9.0	365.1
N ₀	9.0	365.1
	2+50	
N ₀	8.4	365.7
U	9.2	364.9
+15	8.6	365.5
+20	8.9	365.2
$\frac{1}{2}$	8.5	365.6
+14	8.7	365.4
+17	9.2	364.9
+20	8.8	365.3
0	8.7	365.4
+3	8.9	365.2
+6	8.0	366.1
+15	8.5	365.6
$\frac{1}{2}$	6.9	367.2
+7	6.2	367.9
U	8.5	365.6
+12	8.6	365.5
S ₀	7.7	366.4

67

	2+75	
S ₀	7.2	366.9
+12	8.2	365.9
U	8.2	365.9
+18	9.1	365.0
+22	8.8	365.3
$\frac{1}{4}$	8.5	365.6
+5	8.9	365.2
+8	9.6	364.5
+15	9.6	364.5
+16	9.2	364.9
U	9.0	365.1
+8	9.2	364.9
+11	8.9	365.2
$\frac{1}{2}$	8.6	365.5
+7	9.3	364.8
+10	10.0	364.1
U	9.8	364.3
N ₀	10.0	364.1
	3+00 = W L 30 th	
N ₀	10.0	364.1
U	10.2	363.9
+19	10.0	364.1
+21	9.3	364.8
U	9.1	365.0

37410

W.L. 30th

+16	92	364.9
+17	88	365.3
0	88	365.3
+3	95	364.6
+15	10.1	364.0
+25	92	364.9
$\frac{1}{4}$	92	364.9
+8	96	364.5
U	74	366.7
50	85	365.6

W. C.

50	96	364.5
U	86	365.5
+15	80	366.1
$\frac{1}{4}$	87	365.4
+5	89	365.2
+7	98	364.3
+12	10.0	364.1
+14	95	364.6
U	92	364.9
+7	94	364.7
$\frac{1}{4}$	9.1	365.0
+7	89	365.2
13 th 30 th	6.78	367.32 ✓ 367.22

68

U	10.3	363.8
No	102	363.9

W. 4

No	10.1	364.0
U	10.3	363.8
+5	10.2	363.9
+10	9.3	364.8
$\frac{1}{4}$	9.1	365.0
0	9.5	364.6
+10	9.3	364.8
+18	9.0	365.1
$\frac{1}{4}$	9.1	365.0
+6	88	365.3
+9	9.4	364.7
+18	7.5	366.6
U	74	366.7
+12	84	365.7
50	95	364.6

C. 4

50	89	365.2
+10	68	367.3
U	7.1	367.0
+15	9.8	364.3
$\frac{1}{4}$	9.8	364.3

374.10

Ch

1/4 +7	9.8	364.3
+8	10.5	363.6
+12	11.0	363.1
+14	9.5	364.6
C	9.2	364.9
1/4	9.1	365.0
+7	9.5	364.6
+17	10.5	363.6
Ch	10.2	363.9
No	10.1	364.0
E 1/4 30 C		
No	10.1	364.0
Ch	10.3	363.8
+18	10.1	364.0
+19	9.7	364.4
1/4	9.1	365.0
+18	9.4	364.7
+21	9.2	364.9
+23	9.1	365.0
C	8.2	365.9
+5	8.7	365.4
+17	11.6	362.5
1/4	10.4	363.7
+2	10.1	364.0

69

+9	8.5	365.6
Ch	8.5	365.6
50	9.7	364.4
E Ch 30 th		
50	9.9	364.2
+7	9.5	364.6
+15	8.6	365.5
Ch	8.7	365.4
1/4	9.3	364.8
+12	8.8	365.3
C	9.2	364.9
+5	9.5	364.6
+18	8.9	365.2
1/4	9.2	364.9
+7	9.7	364.4
+8	10.1	364.0
Ch	10.3	363.8
No	10.3	363.8

374.10

E.L. 31th = 0+0.0

No		9.3	364.8	
Cl		10.2	363.9	
+18		10.0	364.1	
+21		9.3	364.8	
1/4		9.2	364.9	
+8		9.0	365.1	
C		9.7	364.4	
+15		10.2	363.9	
+24		9.7	364.4	
1/4		9.6	364.5	
+6		9.7	364.4	
+10		10.2	363.9	
+12		10.2	363.9	
+17		8.7	365.4	
Cl		9.2	364.9	
So		9.7	364.4	
T.P	6.89	370.25	10.24	363.86
So		0+25	5.4	364.9
+15			6.7	363.6
Cl			6.5	363.8
+23			6.3	365.0
1/4			5.9	364.4
+14			6.5	363.8
C			6.1	364.2

70

+20		5.2	365.1
1/4		5.2	365.1
+5		5.2	365.1
+8		6.2	364.1
Cl		6.5	363.8
No		6.3	364.0

0+50

No		5.0	365.3
+14		6.3	364.0
Cl		6.4	363.9
+19		6.2	364.1
+22		5.2	365.1
1/4		5.3	365.0
+14		5.2	365.1
C		5.7	364.6
+10		6.8	363.5
1/4		6.5	363.8
Cl		6.7	363.6
So		6.2	364.1

370.25

0 + 75

So	6.0	364.3
+4	6.6	363.7
U	6.2	364.1
$\frac{1}{4}$	6.3	364.0
C	6.0	364.3
+9	5.5	364.8
+20	5.7	364.9
$\frac{1}{4}$	5.3	365.0
+7	5.3	365.0
+9	5.8	364.5
+20	5.3	365.0
U	6.1	364.2
No	6.3	364.0
1 + 00		
No	6.1	364.2
U	6.2	364.1
+15	6.3	364.0
+20	5.2	365.1
$\frac{1}{4}$	5.2	365.1
+8	5.0	365.3
+18	5.7	364.6
C	6.5	363.8
$\frac{1}{4}$	6.3	364.0
U	6.6	363.7

71

+17	6.7	363.6
So	6.3	364.0
1 + 25		
So	6.8	363.5
U	6.8	363.5
+20	4.6	365.7
$\frac{1}{4}$	4.6	365.7
+7	5.2	365.1
+12	6.1	363.7
U	6.3	364.0
+10	5.3	365.0
+11	5.5	364.8
+21	5.3	365.0
$\frac{1}{4}$	5.5	364.8
U	6.2	364.1
+12	5.9	364.4
No	5.3	365.0
1 + 50		
No	5.8	364.5
U	5.9	364.4
+20	5.5	364.8
$\frac{1}{4}$	5.8	364.5
+7	6.0	364.3
C	6.3	364.0

370.25

1+50

1/4	6.5	363.8
Ch	6.9	363.4
So	6.4	363.9

1+75

So	6.4	363.9
Ch	6.3	364.0
1/4	6.5	363.8
+5	6.5	363.8
+14	6.0	364.3
+15	6.6	363.7
C	6.1	364.2
+7	5.7	364.6
+9	5.4	364.9
+20	5.2	365.1
1/4	5.4	364.9
+6	5.0	365.3
+20	4.6	365.7
Ch	5.0	365.3
No	5.7	364.6

2+0

No	5.6	364.7
Ch	6.0	364.3
+19	6.0	364.3
+21	5.1	365.2

72

+22	5.4	364.9
1/4	5.4	364.9
+7	5.3	365.0
C	5.7	364.6
+7	6.0	364.3
+12	6.4	363.9
+17	5.9	364.4
1/4	6.6	363.7
Ch	6.5	363.8
So	6.2	364.1

2+25

So	6.5	363.8
Ch	6.6	363.7
1/4	6.3	364.0
+5	6.3	364.0
+7	5.6	364.7
+12	6.3	364.0
C	5.4	364.9
+8	5.2	365.1
+10	5.4	364.9
+20	5.2	365.1
1/4	5.5	364.8
+8	6.0	364.3
Ch	6.1	364.2
No	5.9	364.4

370.25

2750

No	49	365.4
+9	56	364.7
ck	56	364.7
+19	59	364.4
+21	54	364.9
+23	56	364.7
$\frac{1}{2}$	54	364.9
+7	53	365.0
C	55	364.8
+14	60	364.3
+18	53	365.0
+21	60	364.3
$\frac{1}{2}$	63	364.0
ck	60	364.3
+10	66	363.7
So	61	363.6
	2775	
So	59	364.4
+19	47	365.6
ck	50	365.3
+15	64	363.9
$\frac{1}{4}$	62	364.1
C	59	364.4
+20	55	364.8

73

$\frac{1}{4}$	53	365.0
+8	49	365.4
ck	52	365.1
No	51	365.2
	8700 = W.L. 31 ^{1/2}	
No	47	365.6
ck	54	364.9
+14	56	364.7
+19	48	365.5
$\frac{1}{4}$	51	365.2
+16	51	365.2
+23	61	364.2
C	61	364.2
+4	61	364.2
+22	42	366.1
$\frac{1}{4}$	40	366.3
+14	64	363.9
ck	64	363.9
So	66	363.7

37025

W/C 31st

So	6.1	364.2
Ch	6.6	365.7
+18	6.5	363.8
$\frac{1}{4}$	5.1	365.2
+14	5.8	364.5
C	6.0	364.3
+7	5.7	364.6
+10	5.2	365.1
+21	5.0	365.3
$\frac{1}{4}$	4.9	365.4
+10	4.8	365.5
+12	5.2	365.1
Ch	5.0	365.3
No	4.7	365.6

KV $\frac{1}{2}$

No	5.0	365.3
Ch	4.8	365.5
+17	5.5	364.8
+23	5.0	365.3
$\frac{1}{4}$	5.1	365.2
+17	5.1	365.2
+22	5.7	364.6
C	5.7	364.4
+7	5.8	364.5

74

+12	6.2	364.1
+21	5.5	364.8
$\frac{1}{4}$	5.5	364.8
+5	6.2	364.1
Ch	6.0	364.3
So	6.8	363.5

C+V

So	6.3	364.0
Ch	3.3	367.0
+5	3.1	367.2
$\frac{1}{4}$	6.0	364.3
+14	6.2	364.1
+23	5.5	364.8
C	4.4	365.9
+3	4.0	366.3
+6	4.9	365.4
$\frac{1}{4}$	4.9	365.4
+9	5.4	364.9
Ch	4.5	365.8
No	5.0	365.3

Ch +7

So	5.8	364.5
Ch	2.5	367.8
+25	4.6	365.7

37025

C + 17

1/2	5.7	364.6
+18	6.0	364.3
0	4.3	366.0
+4	0.3	367.0
+9	4.4	365.9
1/2	4.6	365.7

C + 10

50	71	362.5
U	65	363.8
1/2	69	363.4
+5	65	363.8
+7	60	364.5
+22	54	364.9
0	45	365.8
+3	36	366.7
+7	44	365.9
1/2	47	365.6

E 1/2

50	69	363.4
U	61	364.2
1/2	66	363.7
+15	57	364.6
0	40	366.3
+4	33	367.0

75

77	42	366.1
1/2	47	365.6
U	50	365.3
1/6	53	365.0

1/2 + 4

1/6	51	365.2
U	54	364.9
1/2	48	365.5
+18	45	365.8
+23	0.2	367.1
0	0.5	366.8
+6	4.9	365.4
+19	56	364.7
+23	40	366.3
1/2	50	365.3
U	37	366.6
50	64	363.9

E U

36	65	363.8
U	65	363.8
+20	60	364.3
1/2	54	364.9
+7	50	365.3
+18	55	364.8

370.25

E ct.

C	4.7	365.6
$\frac{1}{2}$	5.0	365.3
ct.	5.6	364.7
+8	5.2	365.1
No	3.4	366.9

E. line 31 at 0+00

No	3.5	366.8
ct	3.4	364.9
+8	4.1	366.2
+11	4.9	365.4
$\frac{1}{2}$	5.0	365.3
C	5.3	365.0
$\frac{1}{4}$	5.7	364.6
ct	6.0	364.3
So	5.9	364.4

0+25

So	5.7	364.6
ct	5.7	364.6
$\frac{1}{2}$	5.7	364.6
+18	5.4	364.9
C	4.2	366.1
+8	3.9	366.4
+11	4.4	365.9
$\frac{1}{4}$	4.7	365.6
+10	4.3	366.0

76

+20	2.8	367.5
ct	3.9	366.4
+5	4.8	365.5
No	5.3	365.0

0+50

No	5.1	365.2
ct	5.4	364.9
+5	5.0	365.3
+10	3.3	367.0
+12	4.3	366.0
$\frac{1}{4}$	4.6	365.7
C	5.0	365.3
$\frac{1}{4}$	5.7	364.6
ct	5.9	364.4
So	5.7	364.6

0+65

No	2.2	367.7
ct	5.2	365.1

370.25

0175

S.	5.5	364.8
Ch	5.7	364.6
4	5.4	364.9
C	5.2	365.1
4	4.6	365.7
+7	4.4	365.9
+9	4.7	365.6
+13	4.6	365.7
+17	4.2	366.1
+20	4.9	365.4
U	5.0	365.3
+4	4.8	365.5
No	3.2	367.1

1120

No	4.4	365.9
+13	2.8	367.5
Ch	3.8	366.5
+5	4.4	365.9
+19	4.5	365.8
+20	4.1	366.2
4	4.4	365.9
+17	4.6	365.7
+22	5.0	365.3
C	5.1	365.2

77

+15	4.7	365.6
4	5.5	364.8
Ch	5.8	364.5
5.0	6.0	364.3

1107

No	4.2	366.1
+10	2.2	368.1
Ch	4.1	366.2

1125

5.0	6.0	364.3
U	5.6	364.7
4	3.4	364.9
C	5.2	365.1
+6	5.0	365.3
+9	4.3	366.0
4	4.2	366.1
+8	3.6	366.7
+10	4.3	366.0
+15	4.2	366.1
+19	3.3	367.0
U	4.1	365.7
No	4.6	365.7

POSTED

370.25

1450

No.	3.7	366.6
cl	4.5	365.8
+5	40	366.3
+20	34	366.9
7	39	366.4
+19	4.5	365.8
+21	5.0	365.3
c	5.2	365.1
7	5.2	365.1
a	5.6	364.7
So	5.7	364.6
TP	4.69	365.56

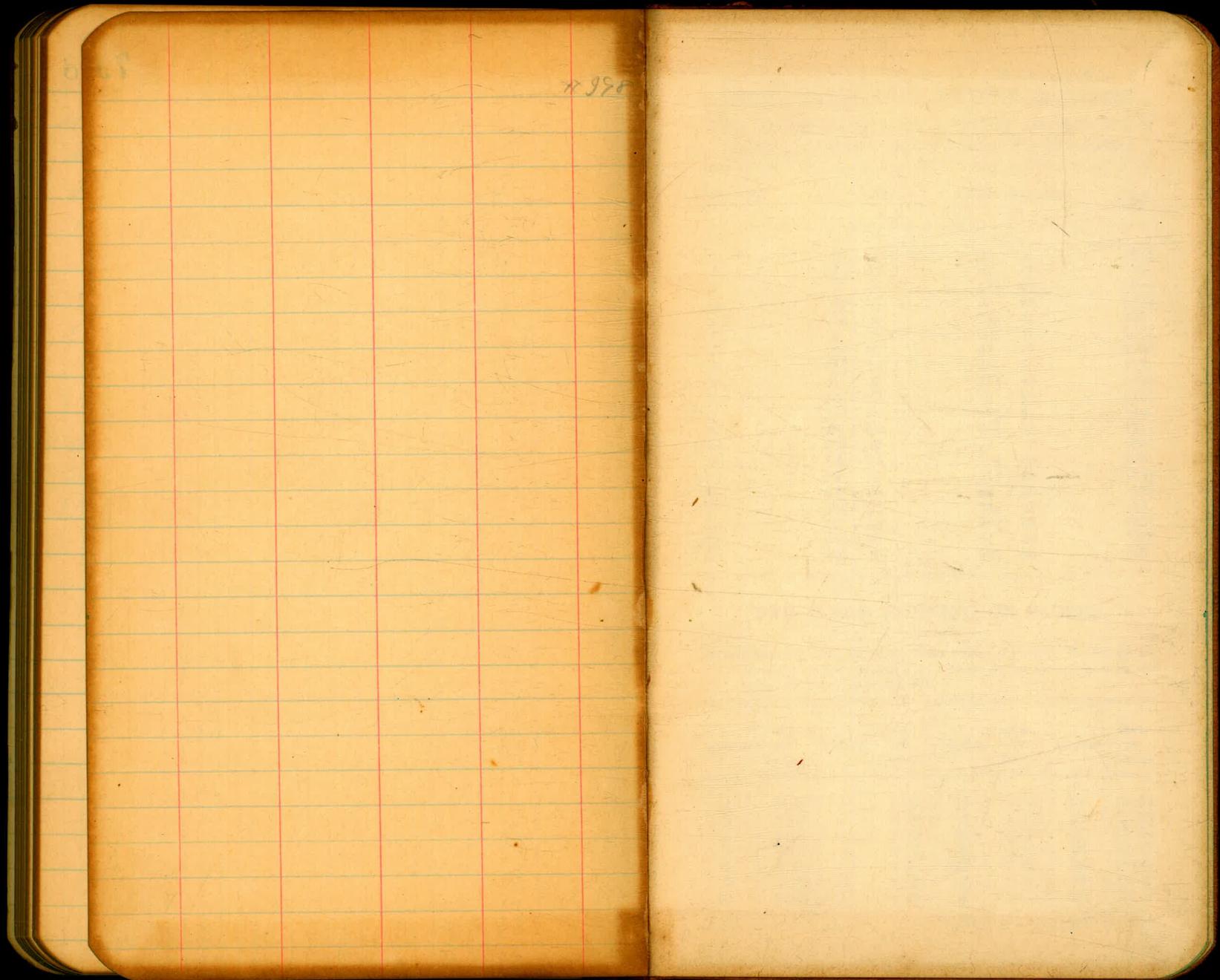
POSTED

Continued in book # 322

78

67

79



2367

296.46 - S. E Florida
 306.74 - " Alabama
 327.49 " " Miss.
 326.45 " " Texas
 339.97. " " Arizona
 372.69 " " Cal.
 376.51 " " Oregon
 384.61 Reservoir Top bell inlet pipe
 376.87 S. W Idaho
 373.45 " " Utah
 369.64 " " Kansas
 367.32 " " South

$$\begin{array}{r} 330.48 \\ 5.56 \\ \hline 324.92 \end{array}$$

Published by H. S. CROCKER COMPANY, Stationers, Drawing Materials, and Mathematical Instruments, San Francisco.

Table showing the difference of latitude and departure in running 80 chains at any course from 1 to 60 minutes.

MINUTES.	LKS.	MINUTES.	LKS.	MINUTES.	LKS.
1.....	2 $\frac{1}{2}$	21.....	49	41.....	95 $\frac{3}{4}$
2.....	4 $\frac{1}{2}$	22.....	51 $\frac{3}{4}$	42.....	98
3.....	7	23.....	53 $\frac{3}{4}$	43.....	100 $\frac{1}{2}$
4.....	9 $\frac{1}{2}$	24.....	56	44.....	102 $\frac{3}{4}$
5.....	11 $\frac{1}{2}$	25.....	58 $\frac{3}{4}$	45.....	105
6.....	14	26.....	60 $\frac{3}{4}$	46.....	107 $\frac{1}{2}$
7.....	16 $\frac{1}{2}$	27.....	63	47.....	109 $\frac{3}{4}$
8.....	18 $\frac{1}{2}$	28.....	65 $\frac{1}{2}$	48.....	112
9.....	21	29.....	67 $\frac{1}{2}$	49.....	114 $\frac{1}{2}$
10.....	23 $\frac{1}{2}$	30.....	70	50.....	116 $\frac{3}{4}$
11.....	25 $\frac{1}{2}$	31.....	72 $\frac{1}{2}$	51.....	119
12.....	28	32.....	74 $\frac{1}{2}$	52.....	121 $\frac{1}{2}$
13.....	30 $\frac{1}{2}$	33.....	77	53.....	123 $\frac{3}{4}$
14.....	32 $\frac{1}{2}$	34.....	79 $\frac{1}{2}$	54.....	126
15.....	35	35.....	81 $\frac{1}{2}$	55.....	128 $\frac{1}{2}$
16.....	37 $\frac{1}{2}$	36.....	84	56.....	130 $\frac{3}{4}$
17.....	39 $\frac{1}{2}$	37.....	86 $\frac{1}{2}$	57.....	133
18.....	42	38.....	88 $\frac{1}{2}$	58.....	135 $\frac{1}{2}$
19.....	44 $\frac{1}{2}$	39.....	91	59.....	137 $\frac{3}{4}$
20.....	46 $\frac{1}{2}$	40.....	93 $\frac{1}{2}$	60.....	140

TABLE FOR RUNNING ON SLOPES.

In the following table the first column shows the angle, the second the number of links to be added to a chain on the slopes, to make one chain, horizontal measurement.

ANGLE	COR. IN LINKS						
°		°		°		°	
4	0.24	11	1.88	18	5.14	25	10.54
5	0.38	12	2.24	19	5.76	26	11.26
6	0.55	13	2.63	20	6.42	27	12.24
7	0.76	14	3.06	21	7.11	28	13.37
8	0.98	15	3.53	22	7.85	29	14.34
9	1.24	16	4.02	23	8.64	30	15.47
10	1.55	17	4.56	24	9.47	35	22.07