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LEVEL BOOK

400

F.B. 341

FB #341

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EAGLE ST, WASHINGTON - 26-28
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X-SECTION

BLK. 22; UNIVERSITY HTS. - 29-
POND 31

H. S. CROCKER COMPANY

DRAWING MATERIALS AND SURVEYING INSTRUMENTS

SAN FRANCISCO

341

TABLES FOR EXCAVATIONS AND EMBANKMENTS

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING

Roadway 18 Feet Wide. Side Slopes 1 to 1.
For Single Track Excavation.

"Copyright, 1895, by Kueffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

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FROM
Loring's Book Store
SAN DIEGO, CAL.

X-Section Proposed extension of Front St from S.L. of Stocton to P.L. 100' N of Dickinson St
X-Section for 60' wide
B.M.: 290.33 40' E of 2nd on Lewis SPK tel pole

Dunkle
Shaw
Thomas
4/25/08

B.M	3.10	293.43		290.33	
	6.08	298.26	1.25	292.18	
		S.L. Stocton			
E			5.1		293.2
Crb			4.8		293.5
1/4			4.3		294.0
M			3.8		294.5
1/4			4.2		294.1
Crb			5.0		293.3
W			5.2		293.1
		S. Curb			
W			4.6		293.7
Crb			4.6		293.7
1/4			4.3		294.0
M			4.3		294.0
1/4			4.7		293.6
Crb			4.8		293.5
E.			5.0		293.3

POSTED

1

		S 1/4			
E			5.0		293.3
Crb			4.8		293.5
1/4			4.5		293.8
M			4.2		294.1
1/4			4.5		293.8
Crb			4.4		293.9
W			4.0		294.3
		Center			
W			3.8		294.5
Crb			4.3		294.0
1/4			3.6		294.7
M			3.6		294.7
1/4			4.0		294.3
Crb			4.7		293.6
E			5.0		293.3

POSTED

298.26

N 1/4

E	4.9	293.4
crb	4.5	293.8
1/4	3.4	294.9
M	2.8	295.5
1/4	3.0	295.3
crb	4.0	294.3
W	4.1	294.2

N curb

W	4.3	294.0
crb	3.7	294.6
1/4	2.6	295.7
M	2.6	295.7
1/4	3.0	295.3
crb	4.3	294.0
E	4.5	293.5

N.L. Stocton

E	4.5	293.5
crb	4.7	293.6
1/4	3.3	295.0
M	2.9	295.4
1/4	3.1	295.2
crb	3.9	294.4
W	4.2	294.1

0+25' N

W	4.0	294.3
crb	4.1	294.2
1/4	4.2	294.1
M	4.3	294.0
1/4	3.5	294.5
crb	3.3	295.0
E	3.6	294.7

		298.26			
		0+50'	N		
E			4.7		293.6
crb			4.6		293.7
1/4			4.7		293.6
M			4.3		294.0
1/4			3.6		294.7
crb			3.4		294.9
W			3.6		294.7
		0+75'			
W			2.3		296.0
crb			3.8		295.0
1/4			4.4		293.9
M			4.6		293.7
1/4			4.5		293.8
crb			4.5		293.8
E			4.9		293.4

		1+00			
E			4.9		293.4
crb			4.7		293.6
1/4			4.8		293.5
M			4.7		293.6
1/4			4.5		293.8
crb			4.4		293.9
W			4.4		293.7
		1+25			
W			4.3		294.0
crb			4.5		293.8
1/4			4.4		293.9
M			4.6		293.7
1/4			4.3		294.0
crb			4.5		293.8
E			4.8		293.5

		298.26			
		1+50			
E			5.5		292.8
crb			5.3		293.0
1/4			5.3		293.0
M			5.4		292.9
1/4			5.0		293.3
crb			4.8		293.5
W			4.5		293.8
		1+75			
W			6.2		292.1
crb			6.0		292.3
1/4			6.0		292.3
M			6.9		291.4
1/4			7.5		290.8
crb			7.5		290.8
E			8.2		290.1

		2+00			
E			9.7		289.6
crb			9.3		289.0
1/4			8.7		289.6
M			8.1		290.2
1/4			9.0		289.3
crb			8.3		290.0
W			7.0		291.3
		2+25			
W			10.9		287.4
crb			10.9		287.4
1/4			11.4		286.9
M			11.9		286.4
1/4			11.9		286.4
crb			12.0		286.3
E			12.0		286.3
T.P.	2.71	288.52	12.45	285.81	

288.52

2+50

E		7.3		281.2
crb		7.3		279.2
1/4		9.9		278.7
M		9.0		279.5
1/4		7.5		281.0
crb		5.9		282.6
W		4.4		284.1

2+75

W		9.0		279.5
crb		11.8		276.7
1/4		13.5		274.7
M		16.4		272.1
1/4		18.5		270.0
crb		18.7		269.8
E		18.7		269.8

2+90

E		26.8		261.7
crb		25.1		263.4
1/4		23.3		265.2
M		21.8		266.7
1/4		19.7		268.8
crb		17.9		270.6
W		16.2		272.5

3+00

E		25.4		263.1
crb		20.9		267.6
1/4		18.0		270.5
M		16.3		272.2
1/4		14.8		273.7
crb		13.5		275.0
W		13.6		274.9

		288.52			
		3+25			
W			2.5		286.0
Crb			2.5		286.0
1/4			3.5		285.0
M			7.7		280.8
1/4			10.7		277.8
Crb			14.1		274.4
E			20.2		266.3
		3+50			
E			12.2		296.3
Crb			12.6		275.9
1/4			8.2		280.3
M			2.5		286.0
1/4			2.1		286.4
Crb			1.8		286.7
W			0.9		287.6

		3+75			
W			1.9		286.6
Crb			1.9		286.6
1/4			1.8		286.7
M			2.2		286.3
1/4			2.3		286.2
Crb			2.3		286.2
E			2.7		285.8
		4+00			
E			1.1		287.4
Crb			1.1		287.4
1/4			1.6		286.9
M			1.6		286.9
1/4			1.3		287.2
Crb			1.2		287.3
W			1.9		287.1

		288.52			
		4+25			
W			1.1		287.4
crb			1.0		287.5
1/4			1.0		287.5
M			1.2		287.3
1/4			1.3		287.2
crb			0.7		287.8
E			0.1		288.4
T.P.	9.86	297.30	1.08	287.44	
		4+50			
E			9.3		288.0
crb			9.4		287.9
1/4			9.3		288.0
M			9.3		288.0
1/4			8.2		289.1
crb			7.8		289.5
W			7.7		289.6

297.30

S.L. Dickinson = 470' on E.L. & 471.15' on W.L.
x-section "A" see plot.

W			7.8		289.5
crb			8.4		288.9
1/4			8.8		288.5
M			8.9		288.4
1/4			8.9		288.9
crb			8.7		288.6
E			8.9		288.4
		S. curb			
E			8.6		288.7
crb			8.3		289.0
1/4			8.4		288.9
M			8.7		288.6
1/4			8.8		288.5
crb			8.9		288.4
W			8.6		288.7

297.30

S 1/4 Dickinson

W		8.2	289.1
crb		8.4	288.9
1/4		8.4	288.9
M		8.5	288.8
1/4		8.4	288.9
crb		8.3	289.0
E		8.3	289.0

center

E	POSTED	8.0	289.3
crb		8.2	289.1
1/4		8.1	289.2
M		8.2	289.1
1/4		8.2	289.1
crb		8.2	289.1
W		8.1	289.2

N 1/4

W		7.9	289.4
crb		7.9	289.4
1/4		8.0	289.3
M		8.0	289.3
1/4		7.5	289.8
crb	POSTED	7.6	289.7
E		8.0	289.3

N curb

E		7.6	289.7
crb		7.1	290.2
1/4		6.9	290.4
M		7.2	290.1
1/4		7.6	289.7
crb		7.3	290.0
W		7.5	289.8

297.30

N.E. DICKINSON

W	6.9	290.4
crb	6.9	290.4
1/4	6.5	290.8
M	6.4	290.9
1/4	6.3	291.0
crb	6.7	290.6
E	7.0	290.3

0 + 25' N

E	5.4	291.9
crb	5.5	291.8
1/4	5.5	291.8
M	5.4	291.9
1/4	5.2	292.1
crb	5.4	291.9
W	5.3	292.0

0 + 50 N

W	3.9	293.4
crb	4.1	293.2
1/4	4.3	293.0
M	4.3	293.0
1/4	4.4	292.9
crb	4.5	292.8
E	4.4	292.9

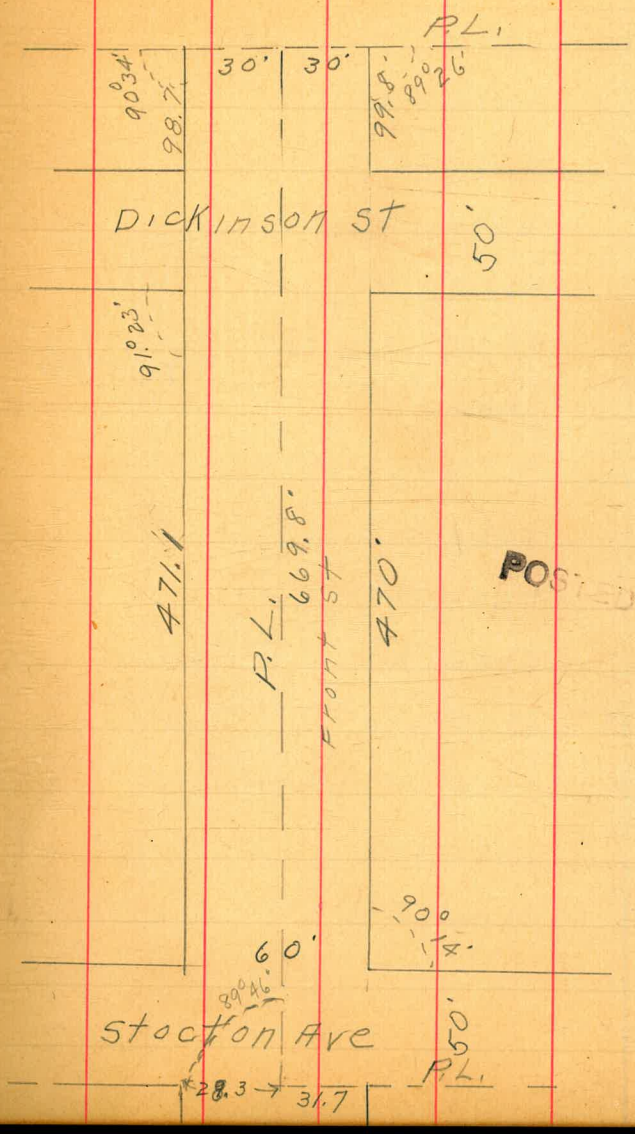
0 + 75

E	3.8	293.5
crb	3.7	293.6
1/4	3.8	293.5
M	3.8	293.5
1/4	3.5	293.8
crb	3.7	293.6
W	3.7	293.6

297.30

P.L. N. of Dickinson = 99.8 on E.L. & 98.7 on W.L.
X-section "B" see plot

W	3.4	293.9
crb	3.3	294.0
"4	3.4	293.9
M	3.5	293.8
"4	3.6	293.7
crb	3.4	293.9
E	3.6	293.7



X-Section on Goldfinch St Sutter Dunkle
To N. P. L. of Lot 112 2 Shaw
80' St Lambert

B.M. 269.54 S.E. Cor Goldfinch & Gem Tel pole					
B.M.	3.09	272.63		269.54	
T.P.	0.70	267.99	5.34	267.29	
N. L. Sutter St					
E			7.9	260.1	
Crb			7.4	260.6	
1/4			7.6	260.4	
M			7.8	260.2	
1/4			8.0	260.0	
Crb			8.3	259.7	
W			8.5	259.5	
0+25' N					
W			8.2	259.8	
Crb			7.9	260.1	
1/4			7.6	260.4	
M			7.5	260.5	
1/4			7.3	260.7	
Crb			7.4	260.6	
E			7.3	260.7	

POSTED

0+50					
E			6.7	261.3	
Crb			6.0	262.0	
1/4			6.5	261.5	
M			6.5	261.5	
1/4			7.2	260.8	
Crb			7.1	260.9	
W			7.1	260.9	
0+75					
W			7.2	260.8	
Crb			7.3	260.7	
1/4			7.0	261.0	
M			6.8	261.2	
1/4			6.7	261.3	
Crb			6.8	261.2	
E			6.9	261.1	

	267.99		
	1+00		
E		6.3	261.7
crb		6.4	261.6
1/4		6.9	261.1
M		6.6	261.4
1/4		6.7	261.3
crb		6.9	261.1
W		6.8	261.2
	1+25		
W		6.4	261.6
crb		6.7	261.3
1/4		6.5	261.5
M		6.3	261.7
1/4		6.4	261.6
Crb		6.6	261.4
E		6.3	261.7

	1+50		
E		7.4	260.6
Crb		6.8	261.2
1/4		6.4	261.6
M		6.5	261.5
1/4		6.3	261.7
crb		6.3	261.7
W		6.0	262.0
	1+75		
W		5.8	262.2
crb		6.0	262.0
1/4		6.4	261.6
M		6.4	261.6
1/4		6.3	261.7
Crb		6.6	261.4
E		6.9	261.1

	267.99		
	2+00		
E		6.9	261.1
crb		5.9	262.1
℄		6.3	261.7
M		6.4	261.6
℄		6.2	261.8
crb		5.8	262.2
W		5.4	262.6
	2+25		
W		5.4	262.6
crb		5.8	262.2
℄		6.2	261.8
CM		6.2	261.8
℄		7.1	260.9
crb		7.2	260.9
E		7.3	260.7

POSTED

	2+50		
E		7.4	260.6
crb		7.2	260.8
℄		6.5	261.5
M		6.0	262.0
℄		6.3	261.7
crb		5.9	262.1
W		5.4	262.6
	2+75		
W		5.2	262.8
crb		6.1	261.9
℄		6.5	261.5
M		6.7	261.3
℄		7.3	260.7
crb		8.0	260.0
E		7.8	260.2

267.99

3+00 = S.L. Bush St 80' st

E	8.0	260.0
crb	8.0	260.0
1/4	7.4	260.6
M	6.9	261.1
1/4	6.8	261.2
crb	6.5	261.5
W	5.5	262.5
S. curb		
W	6.6	261.4
crb	6.8	261.2
1/4	6.9	261.1
M	6.7	261.3
1/4	7.5	260.5
crb	8.2	259.8
E	8.6	259.4

S 1/4

E	8.5	259.5
crb	8.3	259.7
1/4	7.9	260.1
M	7.3	260.7
1/4	7.3	260.7
crb	7.0	261.0
W	6.7	261.3
center Bush		
W	5.6	262.4
crb	5.8	262.2
1/4	7.0	261.0
M	7.7	260.3
1/4	8.0	260.0
crb	8.1	259.9
E	8.2	259.8

267.99

N 1/4

E.	8.3	259.7	
crb	8.3	259.7	
1/4	8.2	259.8	
M	7.9	260.1	
1/4	7.4	261.6	
crb	6.0	262.0	
W	6.0	262.0	

N. Curb

W	7.0	261.0	
Crb	7.4	260.6	
1/4	7.5	260.5	
M	8.0	260.0	
1/4	8.5	259.5	
Crb	8.7	259.3	
E	9.2	258.8	

N. L. Bush 6+

E	9.4	258.6	
crb	9.0	259.0	
1/4	8.7	259.3	
M	7.3	260.7	
1/4	6.7	261.3	POSTED
Crb	6.8	261.2	
W	7.0	261.0	

0+25 N

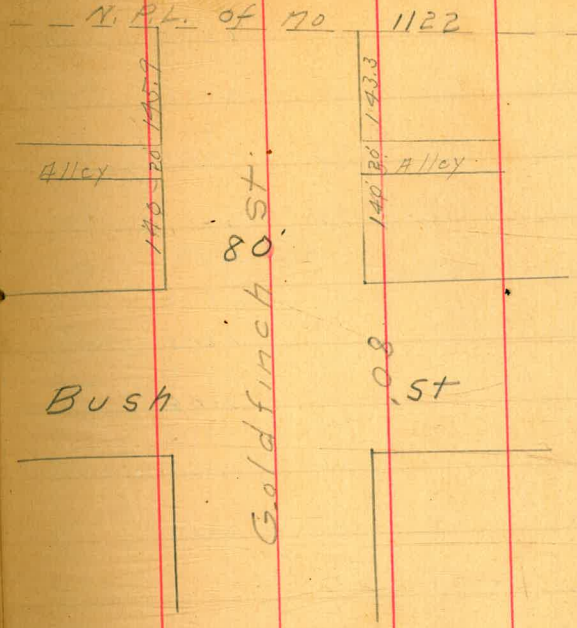
W	6.9	261.1	
Crb	8.1	259.9	
1/4	8.5	259.5	
M	8.8	259.2	
1/4	9.2	258.8	
Crb	9.8	258.2	
E.	10.0	258.0	

		267.99		
	0+50			
E			10.1	257.9
crb			9.4	258.6
1/4			8.3	259.7
M			8.0	260.0
1/4			8.2	259.8
crb			7.6	260.4
W			6.0	262.0
	0+75			
W			7.4	260.6
crb			7.7	260.3
1/4			7.3	260.7
M			7.3	260.7
1/4			7.8	260.2
crb			9.1	258.9
E			9.6	258.4

	1+00			
E			8.7	259.3
crb			9.2	258.8
1/4			8.8	259.2
M			7.3	260.7
1/4			6.5	261.5
crb			6.4	261.6
W			7.1	260.9
	1+25			
W			7.5	260.5
crb			7.6	260.4
1/4			7.9	260.1
M			8.3	259.7
1/4			8.0	260.0
crb			7.8	260.2
E			8.6	259.4
T. P.	7.13	270.32	4.80	263.19

	270.32		
	1+50		
E		10.0	260.3
crb		9.0	261.3
1/4		9.2	261.1
M		9.8	260.5
1/4		9.5	260.8
crb		7.9	262.4
W		8.3	262.0
	1+75		
W		9.5	260.8
crb		9.8	260.5
1/4		10.0	260.3
M		10.0	260.3
1/4		9.6	260.7
crb		9.3	261.0
E.		10.2	260.1

POSTED



POSTED

	270.32		
	2+00		
E		9.7	260.6
crd.		10.1	260.2
1/4		9.9	260.4
M		8.3	261.5
1/4		8.7	261.6
crb		9.6	260.7
W		9.6	260.7
	2+25		
W		9.1	261.2
crb		9.5	260.8
1/4		9.5	260.8
M		9.7	260.6
1/4		9.7	260.6
crb		9.2	261.1
E.		9.0	261.3
	2+50		
E.		8.3	262.0
crb		8.6	261.7
1/4		9.2	261.1
M		9.4	260.9
1/4		9.3	261.0
crb		9.4	260.9
W		9.2	261.1

	2+75		
W		8.9	261.4
crb		9.0	261.3
1/4		8.8	261.5
M		8.5	261.8
1/4	POSTED	8.3	262.0
crb		6.9	263.4
E		7.9	262.4
3+03.3 on E.L. & 305.9 on W.L. See Plot Page 17			
E		7.5	262.8
crb		7.8	262.5
1/4	POSTED	7.6	262.7
M		7.0	263.3
1/4		7.4	262.9
crb		8.4	261.9
W		8.7	261.6

POSTED

X-section India St N.L. Harasthy to S.L. McKee 5/9/08 Dunkle Shaw Thomas

B.M. SPK trolley pole India & Chamber 68.35

	+R	H.I.	-R	
B.M.	11.96	80.31		68.35
	8.95	87.09	2.17	78.14
	3.05	80.04	10.10	76.99

N.L. Winder ST.

E.L.			0.8	79.2
crb			2.1	77.9
1/4			4.0	76.0
M			6.0	74.0
1/4			7.6	72.4
crb			8.5	71.5
W.L.			9.2	70.8

POSTED

80.04

0+25' N

W			10.9	69.1
Crb			9.8	70.2
1/4			8.8	71.2
M			7.6	72.4
1/4			5.6	74.4
Crb			3.1	76.9
E			1.8	78.2

POSTED

0+50

E			4.4	75.6
Crb			6.3	73.7
1/4			8.6	71.4
M			10.4	69.6
1/4			11.0	69.0
Crb			11.7	68.3
W			12.3	67.7

		80.04		
		0+75 N		
W			11.6	68.4
crb			11.7	68.3
1/4			11.4	68.6
M			16.9	63.1
1/4			15.8	64.2
crb			15.5	64.5
E			10.9	69.1
		1+00		
E			8.4	71.6
crb			7.7	72.3
1/4			7.5	72.5
M			7.3	72.7
1/4			6.7	73.3
crb			6.4	73.6
W			5.7	74.3
T. P.	12.15	91.60	0.59	79.45

		91.60		
		1+25		
W			10.0	81.6
Crb			10.5	91.1
1/4			12.0	79.6
M			13.9	77.7
1/4			14.9	76.7
Crb			16.1	75.5
E			17.2	74.4
		1+50		
E			11.7	79.9
Crb			9.0	82.6
1/4			7.3	84.3
M			4.8	86.8
1/4			4.4	87.2
Crb			3.3	88.3
W,			1.8	89.8
T. P.	12.47	103.76	0.31	91.29

POSTED

		103.76		
		1+75 N		
W			3.6	100.2
crb			4.8	99.0
1/4			6.5	97.3
M			7.0	96.8
1/4			8.6	95.2
crb			11.3	92.5
E.			13.4	90.4
T.P.	12.40	116.03	0.13	103.63
		2+00		
		116.03		
E			14.6	1014
crb			12.5	103.5
1/4			11.1	1049
M			10.3	1057
1/4			9.0	107.0
crb			8.7	107.3
W			9.4	106.6

		116.03		
		2+25		
W			5.0	111.0
crb			3.7	112.3
1/4			2.6	113.4
M			2.3	113.7
1/4			2.9	113.1
crb			3.2	112.8
E			4.7	111.3
T.P.	12.08	127.65	0.46	115.57
		2+43 N		
E.			9.4	118.3
crb			8.7	119.0
1/4			9.1	118.6
M			9.8	117.9
1/4			11.2	116.5
crb			12.6	115.1
W.			14.0	113.7

POSTED

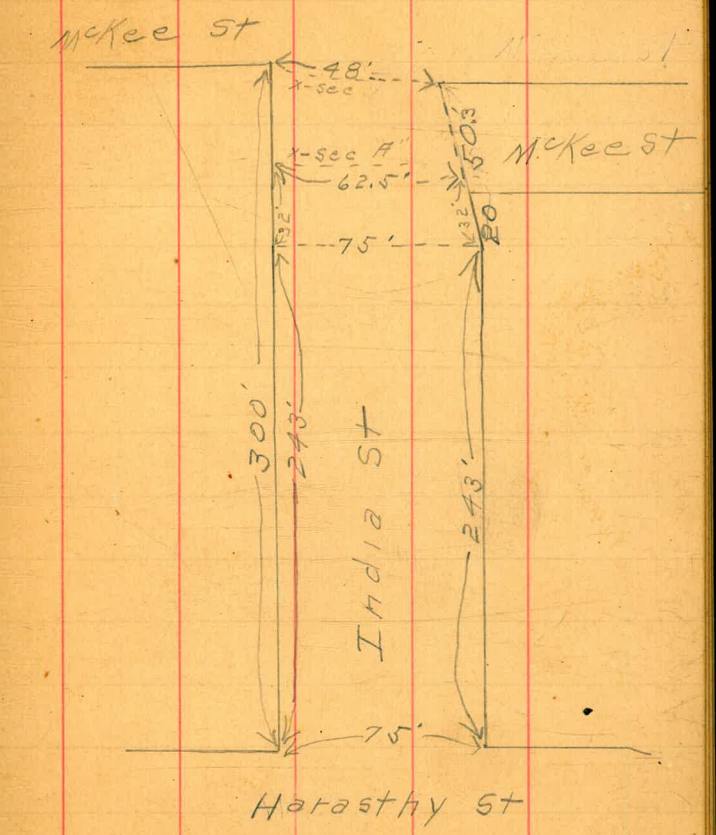
127.65

X-section A 2+75' see Plot Page 22

W	11.0	116.7
+10	9.5	118.2
+20	8.2	119.5
+30	6.6	121.1
+40	5.1	122.6
+50	4.1	123.6
+62.5=E.L.	2.5	125.2

section "B" S.L. McKee see Plot Page 22

W	8.9	118.8
+10	7.2	120.5
+20	5.6	122.1
+30	4.2	123.5
+40	2.9	124.8
+48=E.L.	1.7	126.0



POSTED

Survey of Pond of water situated 5/14/08 Dunkle
south of Adams St between Shaw
Florida & Alabama. Thomas

Note All angles turned to right.

Angle	Distance	Notes.
At S.E. Cor Florida & Adams		
0 0 = S.W. Cor Alabama & Adams.		
1 11° 28"	233'	Present water edge
2 19.46"	213	" " "
3 28°40"	211	
4 36° 21"	196	" " "
5 44° 34"	195	
6 53° 32"	178	" " "
7 54° 43"	163'	
8 61° 38"	151'	" "
9 65° 51"	132	
10 70° 03"	108	" " "
11 74° 21"	82	
12 69° 15"	77	" " "
13 54°06"	94	
14 31°46"	134	" " "
15 24°47"	167	" " "
16 11°02"	213	" " "
17 11° 22"	237	Former water edge
18 21° 18"	231	" " "
19 31° 19"	217	
20 38°47"	211	" " "
21 45°02"	207	" " "
22 49°49"	193	" " "
23 56°04"	175	" " "
24 62°40"	163	" " "
25 66°58"	149'	" " "
26 70°43"	120'	" " "

POSTED

Angle	Dist	Notes
27 78° 33"	86'	Former water Edge
28 69° 15"	77'	" " "
29 54°06"	94'	" " "
30 31°46"	134	" " "
31 24°47"	167	" " "
32 11° 02"	213'	" " "
89°50"	25'	S.W. Cor Lot 1
" "	50'	" " " " 2
" "	75'	" " " " 3
" "	100	" " " " 4
" "	125	" " " " 5
" "	150	" " " " 6

POSTED

Levels for extension of Sewer in alley bet Webster and Clay.

	+	H.I	−	6/6/08 { Davis Colbert Donnan Elev
	2.04	77.41 ✓		75.37 - B.M. Spk in pile S.W. 30th & Clay
0+00 = Bottom F.T.			6.14	71.0
0+00 = " " "			2.1	75.3
+06			3.0	74.4
+66.6 - 13 line 30th			3.3	74.1
1			3.5	73.9
+09			3.0	74.4
+19.6			4.3	73.1
+70			4.5	72.9
2			5.4	72.0
+40			3.8	73.6
3			4.1	73.3
+73			4.5	72.9
4			3.4	74.0
+20			5.3	72.1
+55			5.2	72.2
TP	5.85	75.93 ✓	7.33	70.08 ✓

Couldn't be used. Sewer too low.

POSTED

75.93

+80		6.0	69.9
5		6.8	69.1
+15		7.9	68.0
+55		8.7	67.2
+85		11.4	64.5
6		11.2	64.7
+45		6.4	69.5
7		2.9	73.0
+21.1 = W.L. 30th		1.4	74.5
+35		0.7	75.2
+37		1.1	74.8
+44		6.5	69.4
+48		6.05	69.9

POSTED

X section, Eagle St. from Washington St. South.

Wash. & Eagle St.					
B.M. N Ecn.	0.67	266.61		265.94	
		S. Line Washington			
E.			2.2	264.4	
ch.			4.0	262.6	
1/4			4.5	262.1	
c			4.2	262.4	
1/4			4.8	261.8	
ch.			4.6	262.0	
W			4.4	262.2	
		25' S. of Washington St.			
W.			4.5	262.1	
ch.			4.9	261.7	
1/4			5.0	261.6	
c			5.2	261.4	
1/4			4.5	262.1	
ch.			4.3	262.3	
E			3.9	262.7	

				0.67	
		50' S.			
E.		266.61	5.1	261.5	
ch.			5.4	261.2	
1/4			5.6	261.0	
c			5.7	260.9	
1/4			5.9	260.7	
ch.			5.6	261.0	
W			5.0	261.6	
		75' S.			
W.			5.4	261.2	
ch.			6.5	260.1	
1/4			6.5	260.1	
c			6.4	260.2	
1/4			6.9	259.7	
ch.			6.8	259.8	
E			5.9	260.7	

POSTED

100' S.

E.	266.61	12.7	253.9
cl.		13.5	253.1
1/4		12.7	253.9
+9'		11.6	255.0
C		8.6	258.0
1/4		6.6	260.0
cl.		7.0	259.6
W.		7.0	259.6

1+25'

W.	266.61	7.3	259.3
cl.		7.3	259.3
1/4		7.6	259.0
+7		8.4	258.2
C		12.7	253.9
1/4	253.97	7.3	246.7
cl.		7.0	247.0
E		7.9	246.1

1+50 S Walsh St.

W.	266.61	7.3	259.3
cl.		7.7	258.9
1/4		8.0	258.6
+10		9.4	257.2
C.		11.8	254.8
1/4	253.97	10.0	244.0
cl.		15.0	239.0
E.		16.9	237.1

1+75 S.

W.	266.61	5.8	260.8
cl.		7.0	259.6
1/4		8.2	258.4
C		10.8	255.8
	253.97		
1/4		3.6	250.4
cl.		7.6	246.4
E.		11.3	241.7

POSTED

2+00 S.

W.		266.61	4.9	261.7
ch.			5.6	261.0
1/4			6.5	260.1
c			8.5	258.1
1/4			12.0	254.6
ch.		253.97	4.0	250.0
E.			7.0	247.0

2+25 S.

W.		266.61	4.1	262.5
ch.			4.1	262.5
1/4			5.1	261.5
c			6.9	259.7
1/4			9.5	257.1
ch.			12.2	254.4
E.			15.4	251.2

2+50 S.

E.		266.61	10.7	255.9
ch.			6.8	259.8
1/4			5.7	260.9
c			5.5	261.1
1/4			5.4	261.2
ch.			5.0	261.6
W.			4.7	261.9

2+75 = N. line Douglas St.

W.		266.61	4.7	261.9
ch.			5.1	261.5
1/4			5.5	261.1
c			5.7	260.9
1/4			6.4	260.2
ch.			6.6	260.0
E.			7.6	259.0
T.P.	0.13	253.97	12.77	253.84

POSTED

N

B.M. = prop. line stake at S.E. cor. Florida & Adams.

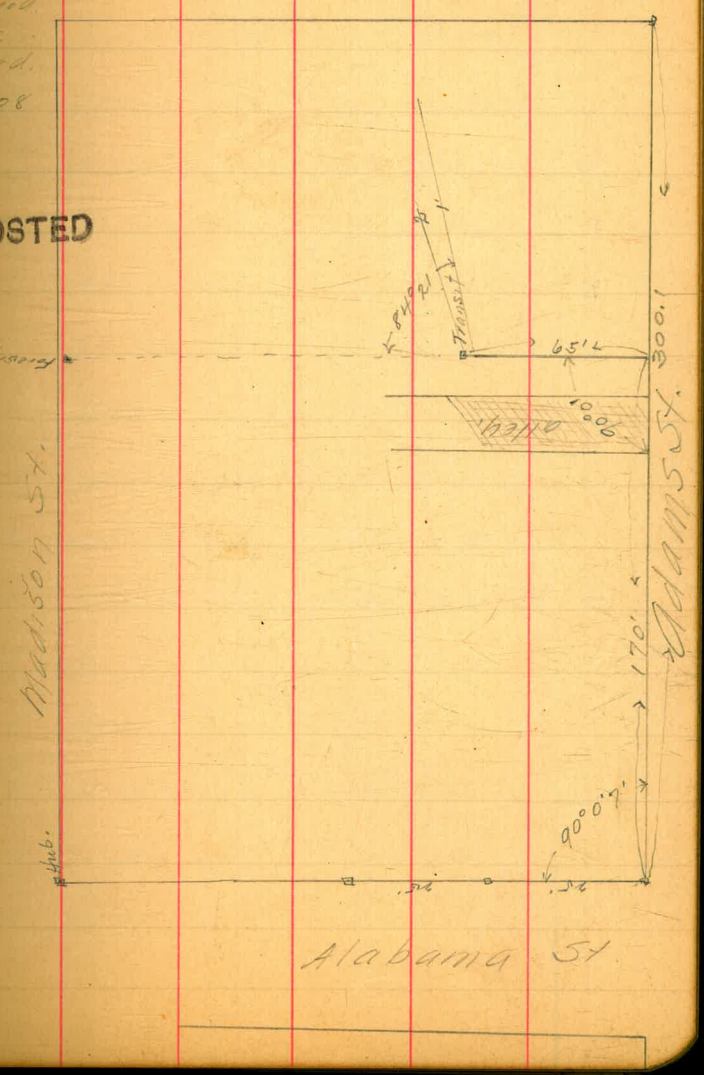
+	-	H.I.	Elev.
2.22			
	8.09		= Height of water
	6.50		= High water line

POSTED

Sketch of pond in Blk 22 Univ. Heights

Davis
Donnan
Colbath
Lockwood
Evans
Foeward
6-18-08

POSTED



Contour of pond Blk 22 Univ. Heights

Angles & Dist. of present waterline

West of alley

Station	Angle	Dist.
1	84°21'R	105.7
2	84°12'R	91.5
3	79°58'R	76.5
4	74°51'R	46.5
5	74°41'R	22.0
6	42°24'L	11.4
7	15°32'L	34.6
8	9°35'L	55.4
9	6°33'L	56.8
10	2°35'L	53.9
11	2°11'R	60.8
12	9°25'R	59.2
13	14°40'R	71.7
14	17°37'R	69.3
15	22°13'R	73.8
16	36°46'R	75.1

sketch page 29

W. side alley

Station	Angle	Dist.
17	44°24'R	83.5
18	46°19'R	81.9
19	48°24'R	85.1
20	50°22'R	84.6
21	54°19'R	88.2
22	58°10'R	94.1
23	64°33'R	95.3
24	80°30'R	106.4

East side alley

Station	Angle	Dist.
1	106°23'L	81.0
2	100°10'L	80.7
3	97°58'L	78.1
4	92°23'L	66.4
5	90°30'L	71.3
6	78°37'L	67.2
7	76°28'L	61.7
8	69°53'L	62.4
9	64°20'L	48.3
10	41°0'L	54.1
11	37°47'L	51.1
12	84°20'L	32.7

Contour of High Water line
Blk 22. University Heights.

Station	Angle	Distance
1	86°31'R.	97.1
2	84°0'R.	119.0
3	66°58'R.	112.3
4	55°41'R.	109.6
5	49°09'R.	110.0
6	36°35'R.	120.5
7	26°0'R.	110.4
8	16°23'R.	101.3
9	4°33'R.	92.6
10	6°01'L	97.5
11	5°20'L	143.4
12	11°37'L	131.4
13	19°50'L	86.2
14	27°53'L	88.0
15	38°22'L	86.2
16	50°48'L	88.7
17	57°28'L	90.4
18	62°59'L	85.7
19	73°15'L	87.8
20	81°52'L	94.5
21	88°33'L	107.0
22	96°03'L	114.0
23	103°50'L	119.8
24	107°33'L	113.5
25	109°09'L	109.2
26	108°57'L	93.6
27	105°53'L	66.9
28	89°58'L	32.2
29	30°24'L	60.6
30	22°19'L	73.0
31	14°22'L	74.7
32	11°12'L	60.8
33	60°07'L	9.8
34	80°47'R	19.8
35	77°41'R.	35.0
36	81°48'R.	66.6

POSTED

Clough Woodie 3-6-09

Crossections of Adams Ave for E Bridge Abutment at Louisiana

				358.27	Mon — SW Adams
	1.62	352.89		357.27	Louisiana
	120'	E of	Louisiana St		
SL			2.8	350.1	
bh		(352.9) CES	2.9	350.0	
Gutter			4.0	348.9	
4			3.2	349.7	
b			3.0	349.9	
4			3.4	349.5	
Gutter			4.4	348.5	
bh			3.3	349.6	
NL			3.3	349.6	
	130'	E of	Louisiana		
NL			5.6	347.3	
bh			4.1	348.8	
4			3.7	349.2	
b			3.0	349.9	
4			3.2	349.7	
bh			3.4	349.5	
SL			4.0	348.9	

		352.89		
	140'	E of	Louisiana	
SL			8.3	344.6
bh		(352.9) CES.	3.5	349.4
4			3.4	349.5
b			3.2	349.7
4			4.1	348.8
bh			5.3	347.6
NL			8.8	344.1
	150'	E of	Louisiana	
NL			14.0	338.9
bh			6.7	346.2
4			4.4	348.5
b			3.3	349.6
4			3.5	349.4
bh			3.7	349.2
SL			9.1	343.8

		352.89			
	160'	E of	Louisiana		(End of Bridge)
SL		(352.9 cls)	10,3	342.6	
bl			6,2	346.7	
y			3,4	349.5	
l			3,5	349.4	
y			4,0	348.9	
bh			10,6	342,3	
NL			17,4	335.5	
	E End	of Bridge	(Top of 3" Planking)		
N line		352.89	3,2	349.57	
bent			3,6	349.33	
SL			3,28	349.61	
	40' E of	End of	Bridge		
S line			2,82	350.07	
bent			3,16	349.73	
N line			2,77	350.12	
TP	0,99	341.78	1,10	340,79	

		341.78			
	170'	E of	Louisiana		
SL		341.78	2,2	339.6	
bl		(341.8 cls)	1,8	340.0	
y			2,0	339.8	
l			3,0	338.8	
y			2,7	339.1	
bh			4,2	337.6	
NL			10,9	330.9	
	180	E of	Louisiana		
NL			15,0	326.8	
bh			11,3	330.5	
y			13,0	328.8	
l			12,3	329.5	
y			9,4	332.4	
bl			6,1	335.7	
SL			3,2	338.6	

		341.78			
	190'	E of	Louisiana		
SL		341.78	3,2	338.6	
bb		(341.8 CES)	7,8	334.0	
S 1/4			13,4	328.4	
	200'	E of	Louisiana		
SL			4,0	337.8	
bb			8,3	333.5	
S 1/4			16,0	325.8	
TP	0,81	330.49	12,10	329.48	
	190'	E of	Louisiana		
berm		(330.5 CES)	5,1	325.4	
N 1/4			5,6	324.9	
bb			5,4	325.1	
N line			8,9	321.6	
	200	E of	Louisiana		
N line			14,6	315.9	
bb			12,3	318.2	
7			12,6	317.9	
6			8,8	321.7	

		330.49			
	215'	E	Top of Sump supported by a bobble stone wall		
N line	(on top of a bobble stone wall)		21.0	309.5	
bb	(4)		21,0	309.5	
	220'	E			
N line	Old Ground Top of bobble wall		30,0	300.5	
bb	(on old Ground)				

Brought Wardie Chamberlain 3.20.09

Crossection of Columbia St (75')

S.L	Chalmers to		N L	Winder	
	13.00	91.09		78.09	BM NW India & Winder
TP	12.87	103.40	0.56	90.53	
TP	12.09	113.99	1.50	101.90	
	N Sin of		Winder St	(114.0) (80)	
WL			14.1	99.9	
bb			12.3	101.7	
4			10.4	103.6	
b			8.6	105.4	
4			6.4	107.3	
bb			4.8	109.2	
EL			2.8	111.2	

POSTED

113.99

Columbia

(114.0)

	N bb of		Winder		
EL			2.2	111.8	
bb			4.0	110.0	
4			5.5	108.5	
b			8.3	105.7	
4			10.1	103.9	
bb			11.3	102.7	
WL			13.3	100.7	
	N 1/4 of		Winder		
WL			13.4	100.6	
bb			11.5	102.5	
4			9.9	104.1	
b			7.8	106.2	
4			6.0	108.0	
bb			4.1	109.9	
EL			2.1	111.9	

POSTED

		113.99	
	Center of	Winder	1140
EL		2,1	111,9
bb		4,5	109.5
4		6,1	107.9
6		7,9	106.1
4		9,4	104.6
bb		11,0	103.0
WL		13,3	100.7
	S ¼ of	Winder	
WL		13,0	101.0
bb		10,7	103.3
4		9,1	104.9
6		7,8	106.2
4		5,9	108.1
bb		4,1	109.9
EL		2,1	111.9

		112.99	
	S bb of	Winder	1140
EL		2,2	111.8
bb		4,3	109.7
4		6,1	107.9
6		8,2	105.8
4		9,9	104.1
bb		11,5	102.5
WL		13,1	100.9
	S ¼ of	Winder	
WL		13,4	100.6
bb		11,1	102.9
4		9,3	104.7
6		7,8	106.2
4		6,0	108.0
bb		4,1	109.9
EL		2,3	111.7

		11399		
	50'	S of	Winder	1140
Ed			2,1	111.9
bl			4,3	109.7
4			6,1	107.9
b			7,7	106.3
bl			10,2	103.8
bl			12,5	101.5
Wl			14,0	100.0
	100'	S of	Winder	
Wl			14,5	99.5
bl			12,7	101.3
7			10,6	103.4
b			8,1	105.9
7			5,6	108.4
bl			2,7	111.3
Ed			0,0	114.0

		11399		
				1140
	150'	S of	Winder	
Wl			15,0	99.0
bl			12,3	101.7
7			9,1	104.9
b			5,6	108.4
4			2,4	111.6
bl			0,0	114.0
	200'	S of	Winder	
Wl			13,5	100.5
bl			10,9	103.1
4			8,2	105.8
b			5,7	108.3
4			3,3	110,7
TP	620	11694	3,25	11074
	150'	S of	Winder	116.9
Ed			0.4	116.5
	200	S of	Winder	
Ed			1.8	115.1
bl			7,2	

		116.94		
	250'	S of	Winder	116.9
EL			6,5	110.4
bb			9,0	107.9
y			10,7	106.2
b			12,5	104.4
	275'	S of	Winder	
EL			11,0	105.9
bb			13,0	103.9
TP	1,47	105.51	12.90	104.04
	250	S of	Winder	105.5
WL			6,6	98.9
bb			4,8	100.7
y			3,0	102.5
	275	S of	Winder st	
WL			9,3	96.2
bb			7,5	98.0
y			6,0	99.5
b			4,5	101.0
y			3,1	

POSTED

		105.51			Columbia
	300'	S = N Sin of Chalmers st (80)			
EL			6,0	99.5	
bb			7,2	98.3	
y			8,3	97.2	
b			9,3	96.2	
y			10,7	94.8	
bb			12,7	92.8	
WL			13,4	92.1	
	N bb of Chalmers				
EL			8,8	96.7	
bb			9,2	96.3	
y			10,3	95.2	
b			12,1	93.4	
TP	2,50	95.65	12,36	93.15	
y			3,1	82.6	
bb			4,9	80.7	
WL			5,4	80.3	

95.65

N 1/4 of Chalmers

Wh			8.7	87.0
Bh			8.7	87.
4			6.0	89.7
b			4.0	91.7
4			2.0	93.7
bh			0.7	95.0
Eh			3.0	92.7

Center of Chalmers

Eh			8.5	87.2
bh			8.2	87.5
4			8.6	87.1
b			8.2	87.5
4			10.0	85.7
bh			10.2	85.5
Wh			11.9	83.8

95.65

S 1/4 of Chalmers.

Wh			13.5	82.2
bh			13.0	82.7
4			12.4	83.3
b			11.6	84.1
4			10.8	84.9
bh			9.8	85.9
Eh			9.2	86.5

Sbh of Chalmers

Eh			7.0	88.7
bh			8.0	87.7
4			9.0	86.7
b			9.6	86.1
4			9.8	85.8
bh			13.4	82.3
Wh			14.3	81.4

95.65

Skin of Chalmers

Wk			13,3	82.4
bb			12,6	83 1
4			5.1	90.6
l			5.9	89.8
4			5.6	90 1
M			4.1	91 6
E1			1,7	93.8
	1,6	84,29	12,52	53,13
	1,62	73,36	12,55	71,74
			5,03	18,33 Bn

POSTED

Clough Churchman Wardwell 3-22-09

Crosssection of Curlew st (80')

S S of Thorn to 68' n of Walnut (PS)

	4.06	254.96		250.90	Bm ice & Walnut
	3.94	249.43	9.47	245.49	
			6.45	242.98	
	S sin of Thorn st				
EL		249.4	4.8	244.6	
bb			5.5		
y			6.6		
b			7.7	241.7	
y			8.6		
bb			9.4		
WL			10.3	239.1	

POSTED

249.43

Curlew

S bb of Thorn st

WL			10.5
bb			9.1
y			8.1
b			7.2
y			6.3
bb			5.3
EL			4.4

S 1/4 of Thorne

EL			4.4
bb			4.9
y			5.5
b			6.4
y			7.5
bb			8.9
WL			10.3

		249.43			
	Center of	Thorne			
WL			10,0		
bl			8,8		
"			7,5		
b			6,4		
"			5,3		
bl			4,5		
EL			4,3		
	N 1/4 of	Thorne st			
EL			4,0		
bl			4,4		
b			5,2		
b			5,9		
b			7,3		
bl			8,8		
WL			9,9		

POSTED

		249.43			Certain
	N bk of	Thorne st			
WL			10,0		
bl			8,5		
"			7,0		
b			5,6		
"			4,9		
bl			4,4		
EL			3,7		
	N Line of	Thorne			
EL		249.4	3,5	245.9	√
bl			4,1		
"			4,5		
b			5,6	243,8	√
"			6,7		
bl			9,0		
WL			10,0	239.4	√

		249.43			
	50'	N of	Thorne		
WL		249.4	10,7	238.7	✓
bl			8,2		
y			3,8		
b			4,5	244.9	✓
y			3,7		
bl			2,9		
EL			2,6	246.8	✓
	100'	W of	Thorne		
EL		249.4	3,2	246.2	✓
bl			3,9		
y			4,1		
b			4,9	244.9	✓
y			6,6 =		
bl			9,3		
WL			11,6	237.8	✓

		249.43			leerlew
	125'	N of	Thorne		
EL		249.4	4,8	244.6	✓
bl			5,3		
y			6,2		
b			7,6	241.8	✓
	150'	N of	Thorne		
EL		249.4	9,3	240.1	✓
bl			9,4		
y			9,3		
b			10,4	239.0	✓
TP	2,82	240.34	11,91	237,52	
	125'	N of	Thorne		
WL			16.1	224.2	✓
bl			11.7		
x 1/4			4.0		
	150'	N of	Thorne		
W 1/4			10.8		

		240.34			
	175'	n f	Thorne		
EL			10.6	229.7	✓
bb			10.0		
y			12.0		
TP	0.74	228.33	12.75	227.59	
b			2.4	225.9	✓
y			9.4		
	150'	n f	Thorn		
WL			15.6	212.7	✓
bb			9.0		
	200'	n f	Thorn		
EL			11.8	216.5	✓
bb			12.0		
y			14.0		
TP	1.72	217.38	12.67	215.66	
	175'	n f	Thorn		
WL			13.3	204.1	✓
bb			7.0		

POSTED

		217.38			Cerlum
	200'	n f	Thorne		
Center			4.5	212.9	✓
W¼			10.7		
	225	n f	Thorne		
EL			13.0	204.4	✓
bb			13.2		
TP	0.59	205.19	12.78	204.60	
y			3.0		
b			4.6	200.6	✓
y			9.8		
bb			13.8		
	200'	n f	Thorne		
WL			10.9	194.3	✓
bb			6.5		
	250'	n f	Thorne		
EL			11.7	193.5	✓
bb			11.5		
y			11.4		
b			12.7	192.5	✓
TP	0.48	193.19	12.48	192.71	

		193.19			
	225'	N of	Thorne		
WL			6,9	186.3	✓
bl			2,4		
y	250'	N of	Thorne		
WL			12,4	180.8	
bl			7,4		
y			2,5		
	275'	N of	Thorne		
EL			11,7	181.5	✓
bl			10,0		
y			9,4		
b			10,1	183.1	✓
y			10,6		
bl			13,0		
TP	153'	182,35	12,37	180,82	
WL			7,3	175.1	

		182.35			Certain
	300'	N = S sin of Upas at (80)			
WL				14,0	168.4 ✓
bl				11,8	
y				10,3	
b				9,3	173.1 ✓
y				10,0	
bl				13,0	
TP	0,55	169.97		129.3	169.42
EL			1,6		168.4 ✓
	S bl	of	Upas		
EL			2,7		
bl			7,0		
y			5,3		
b			4,0		
y			2,5		
bl			4,0		
WL			6,3		

		169.97		
	S 1/4 of Upas			
WL			11,5	
bl			10,4	
y			10,3	
b			10,0	
y			10,3	
bl			8,0	
EL			2,6	
	Center of Upas			
EL			1,8	
bl			7,8	
y			11,4	
b	N 1/4 of Upas			
EL			1,0	
bl			5,2	
y			8,5	
b			12,6	
TP	2.92	161.43	11.46	158.57

		161.43		Carlson
	Center of Upas			
WL			7,9	
bl			7,7	
y			7,4	
b			6,5	
	N 1/4 of Upas			
WL			13,4	
bl			12,4	
1/4			9,1	
	Nbl of Upas			
WL			15,2	
bl			12,4	
y			8,8	
l			4,5	
y			0,0	

		16143			
	N Sin of		N pas st		
WL			14,3		
bb			11,2		
y			7,0		
b			3,3		
	50	n of	N pas		
WL			10,0		
bb			6,5		
y			3,8		
b			+1,2		
	67'	n =	Pueblo Sin		
WL			11,5		
bb			7,5		
y			3,0		
TP	12,88	174,16	0,15	161,28	+
	n bb	of	N pas		
EL			1,7		
bb			7,4		

		174,16			Culvert
	N Sin of		N pas		
EL			1,1		
bb			5,8		
y			10,4		
	50'	n of	N pas		
EL			+0,4	174,6	
bb			2,7		
y			6,4		
b			11,5		
	67'	n of	N pas = Pueblo Sin		
EL			0,7		
bb			3,6		
y			6,0		
b			10,7		

POSTED

Clough
Wardie
Chinchow
3-23-09

Crossection of Eagle St (80)
Horton to Red wood St

					Bm
	0.04	204.06		204.02	
TP	0,30	191,75	12.61	191.45	
TP	0,37	179.13	12,99	178.76	
TP	0,27	167.00	12,40	166.73	
TP	0.48	154.59	12,89	154.11	
TP	0,31	142.54	12,36	142.23	
TP	0,36	129.97	12.93	129.61	
			2.70	127.27	Bm 52.4
	S Line of		Red wood St		
EL			3.5	126.5	
bl			4.8		
4			6,9		
b			8,9	121.1	
4			12,0		
TP	1,67	118,66	12,98	116,99	
bl			2,2		
WL			5.8	112.9	

POSTED

		118.66			Eagle
	50'	S of	Red wood		
WL			11.5	107.2	
bl			9.8		
4			9.3		
b			7.4	111.3	
4			6,2		
bl			6,6		
EL			6.1	112.6	
TP	0,25	105.91	13,00	105.66	
	100'	S of	Red wood		
EL			10.1	95.8	
bl			9.8		
4			9.8		
b			9,6	96.3	
4			10,4		
bl			10,5		
WL			11,6	94.3	

		105.91			
	125	S of	Red	wood	
W2			16.3	89.6	
bl			15.0		
4			13.5		
l			10.0	95.9	
4			7.0		
bl			4.9		
E2			0.5	105.4	
	150	S of	Red	Wood	
W2			11.5	94.4	
bl			7.5		
4			4.9		
b			2.2	103.7	
4			0.0		
TP	12.36	117.91	0.36	105.55	TP
bl			8.0		
E2			3.1	114.8	

		117.91			Eagle
	175	S of	Red	Wood	
E2			0.0	117.9	
bl			3.0		
4			5.8		
b			10.3	107.6	
TP	2.48	108.03	12.36	105.55	+
4			4.2		
bl			8.0	POSTED	
W2			11.8	96.2	
	12.31	117.86		105.55	+
	200	S of	Rodney		
E2			+1.2	119.1	
u			2.0		
4			5.6		
bl			10.0	107.9	
4			13.6		

		117.86		
	250'	S of	Red Wood	
Et			+0,5	118.4
bh			3,8	
4			5,8	
b			10,1	107.8
	300'	S of =	Rosin of Quince (80)	
Et			6,2	111.7
bh			9,2	
4			12,7	
TP	00	104.85	13.01	104.85
	200'	S of	Red Wood	
Wt			10,1	94.8
bh			5,6	
	250'	S of	Red wood	
Wt			15,6	89.3
bh			10,8	
4			4,8	100.1

		104.85			Eagle
	300'	S = N 2	of Quince		
Center			5,3	99.6	
W 1/4			11,4		
TP	.060	.92.67	12.78	92.07	SE Quince
	Rosin	of	Quince		
Wt			11,7	81.0	
bh			7,0		
	S Sin	of	Quincy		
Et			0,6	92.1	
bh			2,6		
7			5,2		
b			8,0	84.7	
4			12,7		
	25'	S of	Quince		
Et			2,6	90.1	
bh			6,6		
7			10,5		
b			13,3	79.4	

		92.67		
	50'	S of	Lunce	
El			4,2	88.5
bl			6,1	
y			8,2	
b			10,6	82.1
TP	0,93	81,15	12,45	80.23
	S Lin	of	Lunce	
wh			9,3	71.9
bl			5,2	
	25'	S of	Lunce	
wh			7,3	73.9
bl			9,5	
y			4,8	
	50'	S of	Lunce	
wh			8,0	73.2
bl			9,0	
y			12,0	

		81.15			
	75'	S of	Lunce		
wh			12,4	68.8	
bl			12,3		
y			4,0		
	100	S of	Lunce		
wh			5,4	75.8	
bl			2,6		
y			1,1		
	29	94.36		92.07	SE Lunce
	75'	S of	Lunce		
El			2,5	91.9	
bl			8,1		
y			10,4		
b			12,6	81.8	
	100	S of	Lunce		
El			3,8	90.6	
bl			7,4		
y			10,7		
b			12,6	81.8	

		94,36		
	150'	S of	Quince	
Et			7,5	86.9
bt			9,9	
y			11,2	
b			12,7	81.7
	200'	S of	Quince	
Et			7,0	87.4
bt			10,3	
y			12,1	
	225	S of	Quince	
Et			10,4	84.0
bt			13,3	
	250'	S of	Quince	
Et			5,4	89.0
bt			10,2	
y			14,0	

		94,36			Eagle
	300'	S = N L	Palm	(80)	
Et			0,8	93.6	
bt			7,5		
y			12,6		
Tp	0,05	81,41	13,00	81,36	
	150'	S of	Quince		
Nt			3,9	77.5	
bt			2,1		
y			1,0		
	200'	S of	Quince		
Nt			8,5	72.9	
bt			5,3		
y			3,2		
b			2,1	79 3	
	225'	S of	Quince		
Nt			11,6	69.8	
bt			10,0		
y			8,1		
b			5,9	75.5	
y			2,7		

		81,41			
	250'	S of	Lunar		
WL			13,3	68.1	
bl			12,6		
y			11,0		
b			7,8	73.6	
	260'	S			
WL			16,4	65.0	
	300' S = WL		Palm		
WL			13,3	68.1	
bl			12,3		
y			17,4		
b			4,6	76.8	
	S Sun of Palm				
EL			4,3	77.1	
bl			7,1		
y			10,0		
b			12,8	68.6	
Mp	727	75,98	12,70	68,71	
bl					
WL					

		75,98			Eagle
	S Sun of Palm				52
W'L			10,0	66.0	
bl			13,4		
WL			9,1	66.9	
	50'	S of	Palm		
WL			8,8	67.2	
bl			10,2		
y			10,6		
b			14,7	61.3	
y			8,4		
bl			4,6		
EL			2,3	73.7	
	78' S = Horizon are on West				
EL			3,1	72.9	
bl			5,8		
y			9,2		
b			14,8	61.2	
y			11,2		
bl			10,6		
WL			7,3	68.7	

		75.98			
	100'	S of	Palm		
EL			4,4	71.6	
bl			6,4		
y			10,6		
f 5'			15,6		
b			12,8	63.2	
y			11,9		
bb = EL Horton			10,8	65.2	
	150'	S of	Palm		
EL			7,2	68.8	
bl			9,3		
y			10,5		
	189	S = EL Horton in E			
EL			8,8	67.2	
BM			8,66	67.32	BM Peg at +189
				62.41	BM Monument bet. Horton & Eagle

	Check			BM Walnut 121
2,30	253.20		250,90	
6,27	150.60	8,87	144,33	
0,53	138.62	12,51	138,09	
0,26	126,13	12,75	125,87	
0,18	213,34	12,97	213,16	
0,10	204,12	9,32	204,02	
4,001	191,30	12,81	191,31	
0,22	179,34	12,18	179,12	
0,69	167,51	12,52	166,82	
0,10	154,70	12,91	154,60	
0,95	143,02	12,63	142,07	
0,03	130,19	12,86	130,16	
1,5		2,90	127,29	BM SE Corner Reservoir
0,34	117,78	12,75	117,44	
1,08	106,11	12,75	105,03	
0,14	93,27	12,98	93,13	
0,83	81,41	12,69	80,58	
1,22	70,50	12,13	69,28	
		3,21	67,29	BM Monument bet. Horton & Eagle
		8,09	62,41	

Clough
Doran
Rodgers
4.10.09

Crossection of Beardsley St (60')
S L Pierce to P L N

	1,57	21,75		20,18	Bm SW Main St + Beardsley
	3,18	17,43	7,50	14,25	
	S L	of	Pierce	(80')	
EL			6,3		
bh			5,1		
+3	2' E Rail		5,3		
Top	Rail		4,8		
1/4+4	2' W Rail		5,3		
b			5,8		
y			6,2		
bh			6,1		
WL			5,6		

POSTED

1743

S bh of Pierce

WL+5'	= 2' E of Rail	5,3
bh		5,4
y		5,7
b		5,3
+4'	= 2' W Rail	5,0
1/4+3'	= 2' E Rail	5,0
bh		5,0
EL		5,4

S 1/4 of Pierce

EL		6,1
bh		5,2
+8'	= 2' E Rail	4,9
1/4+7'	= 2' W Rail	4,7
b		5,0
y		5,3
bh		4,9
+1'	= 2' E Rail	4,9
WL	= 2' W Rail	5,4

17.43

Center of Pierce

WL		4,9
+3'	= 2' W Rail	4,8
bb +2'	= 2' E Rail	4,8
y		4,9
b	= 2' W Rail	4,6
y	= 2' E Rail	4,7
bb		5,5
EL		5,7

N 1/4 of Pierce

EL		5,5
bb		5,4
1/4 y +2'	= 2' E Rail	4,6
b +1'	= 2' W Rail	4,8
1/4 +4'	2' E Rail	4,6
bb +3'	2' W Rail	4,6
WL		5,2

17.43

Boardsley

N bb of Pierce

WL		5,8
+4'		5,7
+6'		4,7
+9'	= 2' W Rail	4,5
bb +8'	= 2' E Rail	4,3
y		4,2
+8'	2' W Rail	4,2
b +7'	= 2' E Rail	4,2
y		4,5
bb		5,1
EL		5,3

N Line of Pierce

EL		5,4	12.0
bb		5,1	12.3
y		4,4	13.0
+4'	= 2' E Rail	4,1	13.1
b +3'	= 2' W of Rail	4,0	13.2
+8'	= 2' E of Rail	4,0	
1/4 +7'	= 2' E of Rail	4,2	13.2
bb		4,1	10.3
WL		4,6	12.8

1743

	25'	n of	Perce	
WL			3,3	14.1
bl			3,4	14.0
+6'	=2' w Rail		3,6	13.8
b+4'	=2' E Rail		3,9	13.5
"			4,4	13.0
bl			4,7	12.7
EL			5,2	12.2
	50'	n of	Perce	
EL			4,8	12.6
bl			4,1	13.3
"			4,0	13.4
+5'	=2' E of Rail		3,5	13.9
//4	=2' w of Rail		3,6	13.8
+7'			3,2	14.2
+9'			4,6	12.8
bl			2,9	14.5
WL			2,5	14.9

POSTED

1743

	75'	n of	Perce	
WL			2,4	15.0
bl			2,5	15.9
+2'			4,0	13.4
+5'			3,0	14.4
//4			2,8	14.6
+3'	=2' w Rail		3,0	14.4
b+4'	=2' E Rail		3,0	14.4
"			3,4	14.0
bl			4,1	13.3
EL			4,3	13.1
	100'	n of	Perce	
EL			3,8	13.6
bl			3,4	14.0
"			2,7	14.7
+6'	=2' E Rail		2,6	14.8
b+6'	=2' w of Rail		2,5	14.9
"			2,4	15.0
+4			2,5	14.9
+6			3,3	14.1
+8			2,5	14.9
bl			2,1	15.3
WL			2,1	15.3

17.43

	125'	n of	Perch	
WL			1,9	15,5
bl			1,9	15.5
+3'			2,0	15.4
+4'			3,0	14.4
+6'			2,2	15.2
y			1,9	15.5
+5'	=2' n Rail		1,9	15.5
b + 4'	=2' E of Rail		2,0	17.4
y			2,2	15.2
bl			3,3	14.1
El			3,2	14.2
	150	n of	Perch	
El			2,7	14.7
bl			2,7	14.7
y			2,1	15.3
+6'	=2' E Rail		1,4	16.0
b + 5'	=2' n Rail		1,4	16.0
y			1,4	16.0
+ 2'			1,6	15.8
+5'			2,5	14.9
+7'			1,8	15.6
bl			1,2	16.2
WL			1,4	16.0
T.P	5,50	2169	1,24	16.19

2169

Beardsley

	175'	n of	Perch	
WL			5,1	16.6
bl			5,2	16.5
+3'			5,4	16.3
+5'			6,3	15.4
+7'			5,5	16.2
y			5,4	16.3
+5	=2' W of Rail		5,2	16.5
b + 4'	=2' E of Rail		5,1	16.6
y			6,1	15.6
bl			6,3	15.4
El			6,5	15.2
	200	n of	Perch	
El			6,0	15.7
bl			5,8	15.9
y			6,1	15,6
+6'	=2' E of Rail		4,7	17.0
b + 5'	=2' n of Rail		4,7	17.0
y			5,0	16,7
bl			5,1	16.6
WL			5,0	16.7

2169

	225'	n f	Pierce	
WL			4,7	17.0
bl			4,7	17.0
y			4,6	17.1
+5 = 2' N Rail			4,1	17.6
b + 4' = 2' E Rail			4,2	17.5
+7'			4,5	17.2
1/4			5,7	16.0
bl			5,3	16.4
EL			5,5	16.2

	250'	n f	Pierce	
EL			4,9	16.8
bl			4,8	16.9
y			4,9	16.8
+3'			3,6	18.1
+6' = 2' E f Rail			3,5	18.2
b + 5' = 2' W f Rail			3,5	18.2
y			4,1	17.6
bl			4,1	17.6
WL			4,3	17.4

2169

Beardsley

	275'	n f	Pierce	
WL			2,5	19.2
bl			4,2	17.5
y			3,1	18.6
+5' = 2' W Rail			3,0	18.7
b + 4' = 2' E Rail			3,0	18.7
+7'			3,0	18.7
1/4			3,8	17.9
bl			4,0	17.7
EL			4,8	16.9

	295'	n f	Pierce	
EL			3,2	18.5
bl			3,3	18.4
y			3,0	18.7
+6' = 2' E f Rail			2,6	19.1
b + 5' = 2' W f Rail			2,3	19.4
y			2,8	18.9
+5			2,4	19.3
+7'			4,0	17.7
bl			4,2	17.5
+3			1,8	19.9
WL			1,6	20.1

2169

(Graded)

800' n = S line of Main St (80)

WL	1.6	20.1	
bl	1.9	19.8	
y	2.6	19.1	
+5' = 2' n of Rail	2.2	19.7	
b + 4' = 2' E of Rail	2.4	17.3	
E Rail			
+14	2.8	18.9	
+5'	3.5	18.2	
+7'	4.4	17.3	
+8'	3.0	18.7	
bl	2.9	18.8	
+5'	1.8	19.9	
EL	1.7	20.0	
TP on Bench	1.57	20.18	Bm

10.38 2056

n line of Main St

WL	9.5	21.1
+8	9.6	21.0
bl	10.9	19.7
+3'	10.0	20.6
y	9.9	20.7
+ 5 = 2' n Rail	9.8	20.8
b + 4' = 2' E Rail	10.0	20.6
	9.7	20.9
E Rail		
y	10.2	20.4
bl	9.8	20.8
EL	9.5	21.1

3456

Beardsley

25' n of Main St

EL	8.8	21.8
bl	9.2	21.4
y	9.7	20.9
+6	9.5	21.1
b + +5	9.5	21.1
y	9.2	21.4
+3	10.4	21.2
+5	9.2	21.4
bl	9.1	21.5
WL	9.2	21.4

50' n of Main St

WL	8.1	22.5
bl	8.2	22.4
+7	9.1	21.5
y	10.0	20.6
+1	9.1	21.5
+5 = 2' n Rail	8.9	21.7
b +4 = 2' E Rail	9.0	21.6
y	9.0	21.6
bl	8.7	21.9
EL	8.2	22.4

POSTED

3056

	75'	n of	Main	s
El			7,2	23.4
bl			7,8	22.8
y			8,2	22.4
+5	at E Rail		8.6	22.0
b +5	= 2 W Rail		8,5	22.1
y			8.8	21.8
bl			7,5	23.1
Wl			7,5	23.1
	100'	n of	Main	s
Wl			6,6	24.0
bl			6.3	24.3
+3			6,7	23.9
+8			8,8	21.8
y			8,0	22.6
+5'	= W Rail		7,8	22.8
b + 4'	= 2' E Rail		7,5	23.1
y			7,5	23.1
bl			7,2	23.4
El			6,4	24,2

3056

Boardally

61

	125'	n of	Main	s
El			5,3	25.3
bl			6,2	24.4
y			7,0	23.6
+4'	= 2' E Rail		7,0	23.6
b + 5	= 2' W Rail		7,2	23.4
y			7,4	23.2
+2			8,6	22.0
+4'			7,4	23.2
bl			5,8	24.8
Wl			5,7	24.9
	150	n of	Main	
Wl	at Man Hole		5,1	25.5
bl			5,3	25.3
+5'			7,2	23.4
y			6,7	23.9
+5'	2' W Rail		6.3	24.3
b + 4'	2' E Rail		6,0	24.6
y			6,1	24.5
bl			5.8	24.8
El			4,6	26,0

	175'	n 7	Main at
E2			3,8 26.8
bl			5,1 25.5
4			5,7 24.9
	+5 = 2' E Rail		5,3 25.3
b +	5' = 2' W Rail		5,7 24.9
4			6,7 23.9
	+9		6,7 23.9
bl			5,0 25.6
W2			5,0 25.6
	200	n 7	Main at
W2			4,3 26.3
bl			4,8 25.8
	+5		4,8 25.8
	+7		6,2 24.4
4			6,7 23.9
	+5 = 2' W Rail		5,0 25.6
b	+4 2' E Rail		5,0 25.6
4			5,0 25.6
bl			4,7 25.9
E2			2,8 27.8

	225'	n 7	Main at
E1			2,2 28.4
	+4		2,3 28.3
	+6		3,4 27.2
bl			4,0 26.6
4			4,7 25.7
	+6' = 2' E Rail		4,4 26.2
b +	5' = 2' W Rail		4,6 26.0
4			5,6 25.0
	+2		6,2 24.4
	+5		4,1 26.5
bl			4,3 26.3
W2			3,9 26.7
	250		
W2			3,3 27.3
bl			3,5 27.1
	+5		4,0 26.6
	+7		6,1 24.5
4			3,2 25.4
	+5 = 2' W Rail		3,8 26.8
b +	4' = 2' E Rail		3,7 26.9
4			4,0 26.6
bl			3,5 27.1
E2			1,7 28.9

		3056		
	275'	N of	Main	st
EL			1,3	29.3
bl			2,8	27.8
y			3,0	27.6
+6	= 2' E Rail		3,0	27.6
b+ 5'	= 2' N Rail		3,0	27.6
y			5,3	25.3
+4'			3,5	27.1
bl			3,3	27.3
WL			2,9	27.7
	300'	N =	S Sin	of Newton st (80')
WL			1,8	28.8
bl			1,3	29.3
+3'			0,9	29.7
+4'			4,5	26.1
y			5,0	25.6
+5			2,3	28.3
	Rail EL	(End)	2,4	28.2
b+4			2,5	28.1
y			3,2	27.4
+8'			2,7	27.9
bl			1,0	29.6
EL			1,2	29.4
TP	695	3691	0,60	29.96

		3691		Beardsley
	S bl	of	Newton	ave
WL			7,3	
bl			7,2	
+3'			7,2	
+4'			10,8	
y			10,3	
b			9,6	
y			9,2	
+4'			8,8	
+5'			8,4	
bl			7,7	
EL			7,5	
	S 1/4	of	Newton	
EL			7,8	
bl			8,2	
y			9,2	
b			9,3	
y			10,3	
+3'			9,9	
~~bl~~ +5'			7,8	
bl			7,5	
WL			6,7	

3691

4½' S of Centre Newton ave = 2' S of RR

WL	9,6
bl	9,4
y	9,5
b	8,5
y	8,4
bl	9,0
EL	8,7
EL E Rail	8,1

4½' N of Center = 2' N of RR

EL	9,1
bl	9,0
y	8,4
b	8,6
y	8,8
bl	9,3
WL	9,5
WL El Rail	8,9

36.91

Beardsley

N 1/4 of Newton ave

WL	7,7
bl	8,2
y	8,5
b	8,7
y	8,2
bl	7,6
EL	6,4

N bl of Newton

EL	6,5
bl	7,4
y	8,1
b	8,3
y	8,1
bl	7,3
WL	7,0

		36.91		
	N Sin	of	Newton	
WL			6.4	30.5
bh			7.0	29.9
y			7.7	29.2
+8'			7.5	29.4
b			8.3	28.6
+3'			9.6	27.3
y +7'			8.0	28.9
			7.7	29.2
bh			6.8	30.1
EL			6.2	30.7
TP	10.95	39.45	8.41	28.50
	25'	n f	Newton	am
WL			8.6	30.9
bh			8.7	30.8
y			9.3	30.2
b			10.6	28.9
4			11.3	28.2
+4'			9.4	30.1
bh			8.0	31.5
+5			7.4	32.1
EL			7.8	31.7

		39.45		
	50'	n f	Newton	
EL			7.6	31.9
bh			7.3	32.2
+6			7.2	32.3
y			10.0	29.5
+4'			11.0	28.5
b			10.3	28.2
y			9.5	30.0
+4'			8.0	31.5
bh			8.2	31.3
WL			8.3	31.2
	75'	n f	Newton	
WL			7.7	31.8
bh			7.8	31.7
+6'			7.6	31.9
y			9.3	30.2
b			9.7	29.8
+7'			10.8	28.7
y			9.8	29.7
+4			7.2	32.3
bh			7.2	32.3
EL			7.4	32.1

		39.45		
	100'	n f	Newton	
EL			7.1	32.4
bl			7.0	32.5
+6'			6.9	32.5
y			10.5	29.0
+6'			8.3	30.2
b			9.3	30.2
y			9.0	30.5
+4'			7.5	32.0
bl			7.5	32.0
WL			7.5	32.0
	125'	n f	Newton	
WL			7.0	32.5
bl			7.3	32.2
+7'			7.3	32.2
y			8.5	31.0
b			8.9	30.6
y			10.0	29.5
+5'			6.0	33.5
bl			5.7	33.8
EL			6.2	33.3

		39.45		
	150'	n f	Newton	am
EL			5.1	34.4
bl			5.2	34.3
y			7.4	32.1
b			8.1	31.4
+6'			8.6	30.9
y			7.5	32.0
+3'			6.9	32.6
bl			6.6	32.9
WL	on Man Hole	lower	6.4	33.1
	175'	n f	Newton	
WL			6.0	33.5
bl			6.3	33.2
+7			6.1	33.4
y			7.2	32.3
+2'			8.2	31.3
b			8.2	31.3
+8'			8.0	31.5
y			7.2	32.3
+4'			5.4	34.1
bl			4.4	35.1
EL			5.0	34.5

		39.45		
	200'	n of	Newton	
EL			4,1	35.4
bl +5'			4,2	35.3
			4,7	34.8
y +3'			7,2	32.3
b			8,0	31.5
+7'			8,0	31.5
			8,0	31.5
y +4'			7,0	32.5
bl			5,8	33.7
			5,9	33.6
WL			5,6	33.9
	225'	n of	Newton	
WL			5,3	34.2
bl +7'			5,5	34.0
			5,4	34.1
y +3'			6,3	33.2
b			7,6	31.9
			7,6	31.9
y +4'			6,5	33.0
			4,3	35.2
bl			4,0	35.5
EL			3,7	35.8

		39.45		
	250'	n of	Newton	
EL			3,5	36.0
bl +5			3,6	35.9
			3,6	35.9
y +4'			6,0	33.5
b			7,3	32.2
+6			7,3	32.2
y			7,2	32.3
+2'			5,3	34.2
bl			4,6	34.9
			4,8	34.7
WL			4,6	34.9
	275'	n of	Newton	
WL			4,0	35.5
bl			4,2	35.3
y +4'			4,6	34.9
			6,7	32.8
b			6,9	32.6
y +5'			6,4	33.1
			2,8	36.7
bl			2,6	36.9
EL			2,8	36.7

		3945			
	300'	n = S L f	National	(Graded) am 80	
EL			3,3	36.2	
bl			4,1	35.4	
+4'			5,0	34.5	
y			4,8	34.7	
b			4,0	35.5	
y			4,0	35.5	
bl			3,7	35.8	
WL			3,3	36.2	
TP	850	4530	2.65	3.80	
	n Lin	f	National	am	
EL			6,7	38.6	
bl			7,1	38.2	
+1'			10,4	34.9	
y			8,6	36.7	
b			9,3	36.0	
y			9,1	36.2	
bl			9,2	36.1	
WL			8,7	36.6	

		45-30			Beardsley
	25'	n f	National	am	
WL			7,7	37.6	
+6'			7,5	37.8	
bl			8,4	36.9	
y			8,6	36.7	
b			8,7	36.6	
y			9,3	36.0	
+6'			9,9	35.4	
+9'			6,5	38.8	
bl			6,7	38.6	
EL			6,6	38.7	
	50'	n f	National	am	
EL			6,3	39.0	
bl			6,1	39.2	
+7'			9,8	35.5	
y			9,2	36.3	
b			8,4	36.9	
y			8,4	36.9	
bl			8,0	37.3	
WL			7,4	37.9	

		45.30		
	75'	n of	National av	
WL			6.7	38.6
+6'			6.3	39.0
+8			7.6	37.7
bl			7.7	37.6
y			8.0	37.3
b			8.0	37.3
y			8.9	36.4
+4			9.3	36.0
+9			6.1	39.2
bl			6.0	39.3
EL			5.6	39.7
	100'	n of	National	
EL			5.4	39.9
bl			5.3	40.0
+6'			9.4	35.9
y			8.7	36.6
b			8.0	37.3
y			7.6	37.7
bl			7.4	37.9
WL			6.6	38.7

		45.30		
	125'	n of	National av	
WL			6.3	39.0
+6'			5.9	39.4
bl			7.2	38.1
y			7.4	37.9
b			8.1	37.2
+8'			8.4	36.9
y			7.3	38.0
+5'			4.8	40.5
bl			4.8	40.5
EL			4.8	40.5
	150'	n of	National	
EL			5.5	39.8
bl			6.0	39.3
y			7.5	37.8
b			7.6	37.7
y			7.1	38.2
bl			6.7	38.6
WL			6.1	39.2

45.30

	175'	N of	National	av
WL			5,0	40.3
bl			6,4	38.9
y			6,6	38.7
b			7,0	38.3
y			7,6	37.7
bl			4,8	40.5
EL			4,5	41.0
	200'	N of	National	
EL			4,2	41.1
+3'			4,2	41.1
bl			7,2	38.1
y			7,3	38.0
b			7,0	38.5
y			6,4	39.1
bl			5,7	39.6
WL			4,4	40.9

45.30

	225'	N of	National	av
WL			4,4	40.9
bl			5,4	39.9
y			6,1	39.2
b			6,6	38.9
y			7,2	38.1
bl			6,7	38.6
EL			4,2	41.1
	250'	N of	National	
EL			3,7	41.6
bl			3,9	41.4
y			6,7	38.6
+8'			7,0	38.3
b			6,0	39.3
y			5,7	39.6
+9'			5,0	40.3
bl			3,8	41.5
WL			4,1	41.2

		4530			
	275'	n of	Natural		
WL			4,3	41.0	
bl			4,8	40.5	
y			5,7	39.6	
b			5,4	39.9	
y			6,3	39.0	
bl			2,9	42.4	
EL			3,7	41.6	
	300'	n =	S L of	Logan (Graded)	on 82
EL			4,5	40.8	
bl			4,8	40.5	
y			4,8	40.5	
b			4,8	40.5	
y			5,0	40.3	
bl			5,0	40.3	
WL			4,8	40.5	
TP	5,83	4728	3,82	41.48 45	✓

1

		4728			Beardsley
	n Line	of	Logan		
WL			5,6	41.7	
bl			5,9	41.4	
y			5,8	41.5	
b			5,8	41.5	
y			5,8	41.5	
bl			5,8	41.5	
EL			5,6	41.7	
	25'	n of	Logan		
EL			5,2	42.1	
bl			5,4	41.9	
y			5,8	41.5	
b			5,9	41.4	
y			6,0	41.3	
bl			5,6	41.7	
WL			5,6	41.7	

		47.28		
	50'	n of	Sogan	am
WL			5,4	41.9
bh			5,5	41.8
"			5,9	41.4
l			5,6	41.7
"			5,5	41.8
bh			5,3	42.0
EL			4,9	42.4
	75'	n of	Sogan	
EL			4,5	42.8
bh			4,8	42.5
"			5,2	42.1
l			5,3	42.0
"			5,5	41.8
bh			5,3	42.0
WL			5,1	42.2

		47.28		
	100'	n of	Sogan	
WL			5,0	42.3
bh			5,0	42.3
"			5,1	42.2
l			5,1	42.2
"			4,9	42.4
bh			4,7	42.6
EL			4,3	43.0
	125	n of	Sogan	
EL			4,3	43.0
bh			4,4	42.9
"			4,8	42.5
bh			4,6	42.7
"			4,9	42.4
bh			4,5	42.8
WL			4,5	42.8

		47.28		
	150'	n f	Logan	
WL			3,4	43.9
bl			3,4	43.9
y			4,3	43.0
b			4,4	42.9
y			4,3	43.0
bl			3,9	43.4
EL			3,9	43.4
	175'	n f	Logan	
EL			2,5	44.8
bl			3,0	44.3
y			3,7	43.6
b			3,9	43.4
y			3,9	43.4
bl			2,6	44.7
WL			2,4	44.9

		47.28		
	200'	n f	Logan	
WL			2,3	45.0
bl			2,6	44.7
+2			3,3	44.0
y			3,6	43.7
b			3,5	43.8
y			3,3	44.0
+5			2,3	45.0
bl			2,5	44.8
EL			2,0	45.3
	225'	n f	Logan	
EL			1,8	45.5
bl			2,2	45.1
y			3,2	44.1
b			3,3	44.0
y			3,3	44.0
+5			3,3	44.0
bl			2,0	45.3
WL			2,3	45.0

		47.28		
	250'	n of	Logan	
WL			1,9	45.4
bl			1,9	45.4
+2			2,4	44.9
y			2,5	44.8
b			2,9	44.4
y			2,8	44.5
bl			2,0	45.3
EL			1,5	45.8
	275'	n of	Logan	
EL			1,2	46.1
bl			1,6	45.7
y			2,5	44.8
b			2,5	44.8
y			2,2	45.1
bl			1,6	45.7
WL			1,6	45.7

		47.28			
	300'	n = S	Line of	Kearney	(80)
EL			1,3	46.0	
bl			1,4	45.9	
y			1,7	45.6	
b			1,7	45.6	
y			2,1	45.2	
bl			1,3	46.0	
EL			1,1	46.2	
TP	3,58	49.86	1,00	46.28	
	n Line of Kearney			ave	
EL			3,5	46.4	
bl			3,8	46.1	
y			4,4	45.5	
b			3,9	46.0	
y			4,1	45.8	
bl			4,1	45.8	
WL			3,5	46.4	

		7986		
	25'	n f	Kearney	
WL			3,5	46.4
bl			3,7	46.2
y			4,5	45.4
b			4,6	45.3
y			4,9	45.0
+6'			4,6	45.3
bl			3,1	46.8
EL			3,0	46.9
	50'	n f	Kearney	
EL			2,6	47.3
bl			3,4	46.5
+5'			5,1	44.8
y			5,2	44.7
b			5,0	44.9
y			4,6	44.3
bl			4,5	44.4
WL			3,5	46.4

		7986		
	75'	n f	Kearney	
WL			3,2	46.7
+2'			4,0	45.9
bl			4,4	45.5
y			4,8	45.1
b			4,5	45.4
y			5,0	44.9
+4'			4,8	45.1
bl			2,4	47.5
EL			1,6	48.3
	100'	n f	Kearney	
EL			1,7	48.2
bl			2,8	47.1
+5'			5,0	44.9
y			5,0	44.9
b			4,9	45.0
y			4,5	45.4
bl			4,6	45.3
+7			3,8	46.1
+8			2,2	47.7
WL			2,2	47.7

		49.86		
	125'	n of	Kearney	
WL			2,6	47.3
+2'			2,6	47.3
+3'			4,0	45.9
bh			4,4	45.5
y			4,8	45.1
b			4,8	45.1
y			5,1	44.8
+3'			5,1	44.8
bh			2,7	47.2
EL			2,1	47.8
	150'	n of	Kearney	
EL			2,3	47.6
bh			3,6	46.3
y			5,1	44.8
b			4,5	45.4
y			4,4	45.5
bh			4,0	45.9
WL			2,5	47.4

		49.86		
	175'	n of	Kearney	
WL			3,0	46.9
bh			3,8	46.1
y			4,4	45.5
b			4,6	45.3
y			5,2	44.7
+4'			4,8	45.1
bh			2,4	47.5
EL			1,5	48.4
	200'	n of	Kearney	
EL			1,5	48.4
bh			1,4	48.5
+6'			4,7	45.2
y			5,2	44.1
b			4,8	45.1
y			4,6	45.3
+8'			4,0	45.9
bh			3,4	46.5
WL			3,0	46.0
TP	300	51.43	1,43	48.43

5143

	225'	n of	Kearney	
WL			4.0	47.4
bl			5.1	46.3
y			6.3	45.1
b			6.2	45.2
y			6.7	44.7
bl			2.6	48.8
EL			2.5	48.9
	250'	n of	Kearney	
EL			2.0	49.4
bl			2.2	49.2
y			7.0	44.4
b			6.5	44.9
y			4.2	47.2
bl			5.2	46.2
WL			4.4	47.0

5143

	275'	n of	Kearney	
WL			3.0	48.4
+5' bl			4.8	46.6
			4.8	46.6
y			6.4	45.0
b			6.7	44.7
y			7.0	44.4
bl			1.6	49.8
EL			2.1	49.3
	290'	n of	Kearney	
EL			2.5	48.9
bl			3.0	48.4
y			7.0	44.4
b			6.7	44.7
y			6.6	44.8
bl			6.3	45.1
WL			4.0	47.4

5143

	300'	n =	S Line of	Julian an (80)	
WL			6,5	44,9	
bL			6,4	45,0	
"			7,0	44,4	
b			6,6	44,8	
"			6,8	44,6	
bL			6,3	45,1	
EL			5,9	45,5	
					End of Return
TP			6,49	44,94	

Continued to Book

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DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

For Single Track Embankment.

Roadway 14 feet wide. Side Slopes 1½ to 1.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	27
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.