359

Return to City Engineers Office
City Hall, San Diego, Cal.

TRANSIT

398

F. B. 359

{W. P. Cook
Home 4050}

TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100.

No. 359

Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100.00	0.44	100.00	0.87	99.99	1.31	89
1	99.98	1.75	99.98	2.18	99.97	2.62	99.95	3.05	88
2	99.94	3.49	99.92	3.93	99.91	4.36	99.88	4.80	87
3	99.86	5.23	99.84	5.67	99.81	6.10	99.79	6.54	86
4	99.76	6.98	99.73	7.41	99.69	7.85	99.66	8.28	85
5	99.62	8.72	99.58	9.15	99.54	9.58	99.50	10.02	84
6	99.45	10.45	99.41	10.89	99.36	11.32	99.31	11.75	83
7	99.25	12.19	99.20	12.62	99.14	13.05	99.09	13.49	82
8	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	15.64	98.70	16.07	98.63	16.50	98.56	16.93	80
10	98.48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98.16	19.08	98.08	19.51	97.99	19.94	97.90	20.36	78
12	97.81	20.79	97.72	21.22	97.63	21.64	97.53	22.07	77
13	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	24.19	96.92	24.62	96.81	25.04	96.70	25.46	75
15	96.59	25.88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.82	73
17	95.63	29.24	95.50	29.65	95.37	30.07	95.24	30.49	72
18	95.11	30.90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35.43	69
21	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38.67	67
23	92.05	39.07	91.88	39.47	91.71	39.87	91.53	40.27	66
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	43.84	89.69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	46.95	88.09	47.33	87.88	47.72	87.67	48.10	61
29	87.46	48.48	87.25	48.86	87.04	49.24	86.82	49.62	60
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	52.99	84.57	53.36	84.34	53.73	84.10	54.10	57
33	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	52
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	45
45	70.71	70.71							
Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees
	DEGREES		¾ DEGREE.		½ DEGREE.		¼ DEGREE.		

390
7325
1.125

MICROFILMED
JUL 1 9 1964

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660.8
Return to City Engineers Office
City Hall, San Diego, Cal.
89-2-1!

Crocker Quality

TRANSIT BOOK

No. 359

MANUFACTURED BY

H. S. CROCKER CO.

SAN FRANCISCO AND SACRAMENTO
CALIFORNIA

FROM
LORING'S BOOK STORE
SAN DIEGO, CAL.

Degrees.	
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Degrees.	

N. E. Cor. Pt. Loma & Catalina Brass plg. 374.78

Near. S. E. Cor. " " & Charles R.R. spk. tree 267.176

N. E. Cor. Landscape " Pt. Loma " " pole 259.76 ✓

Reservoir pump sta. S.W. cor. " " " 252.99 X

Landscape & Pt. Loma inside Homestead. Brass plg. 261.335

—INDEX—

Pages.

Union St. from Palm North, and (39–43, 58–60)

State St. from Redwood North 61—

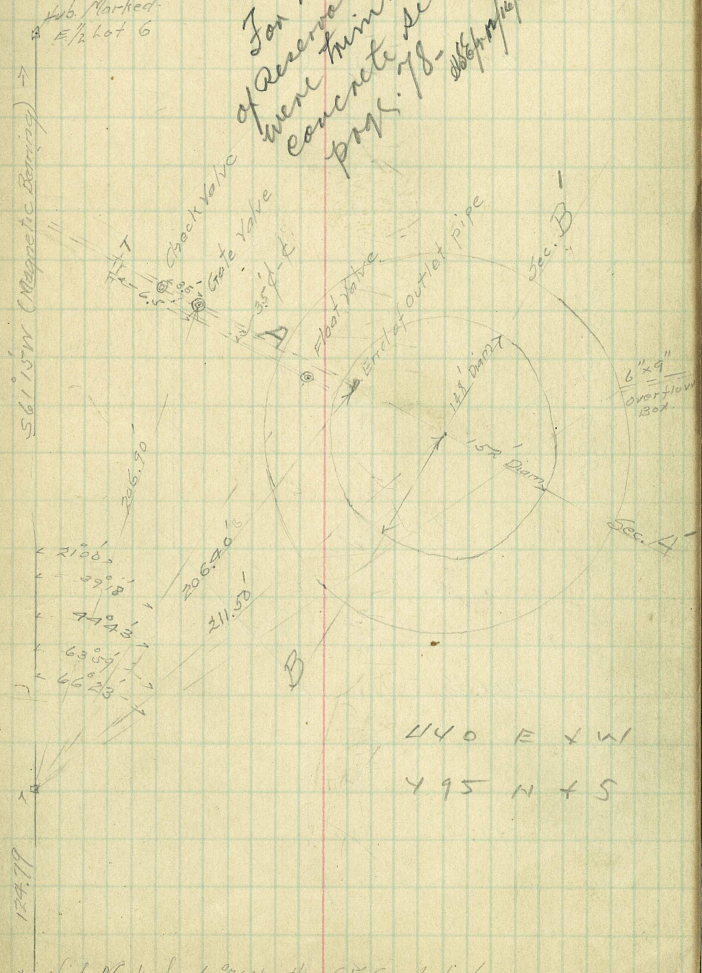
7/23/08 Hath Moore & Churchman

	+	HI	−	Elev.	
BM.	12.87	255.40		242.53	
	12.80	267.86	0.34	255.06	
	12.84	280.41	0.29	267.57	
	13.08	293.02	0.47	279.94	
			8.52	284.50	274.59
	12.45	305.26	0.21	292.81	
			10.91	294.35	274.46
	4.96	309.59	0.63	304.63	
	2.77	320.06	12.30	297.29	
			2.43	297.63	
			2.76	297.30	
Bottom overflow box			4.60	295.46	
			3.10	296.96	
			3.20	296.86	
			4.16	295.90	
			3.36	296.70	
			3.76	296.30	
			3.36	296.70	
TP	6.38	295.86	11.08	288.98	
Water Level			10.0	285.36	
Top of Bell on end of outlet pipe			9.63	285.73	
Inside of Pipe at bottom			10.08	285.28	
Bottom inlet pipe			+2.0	297.36	

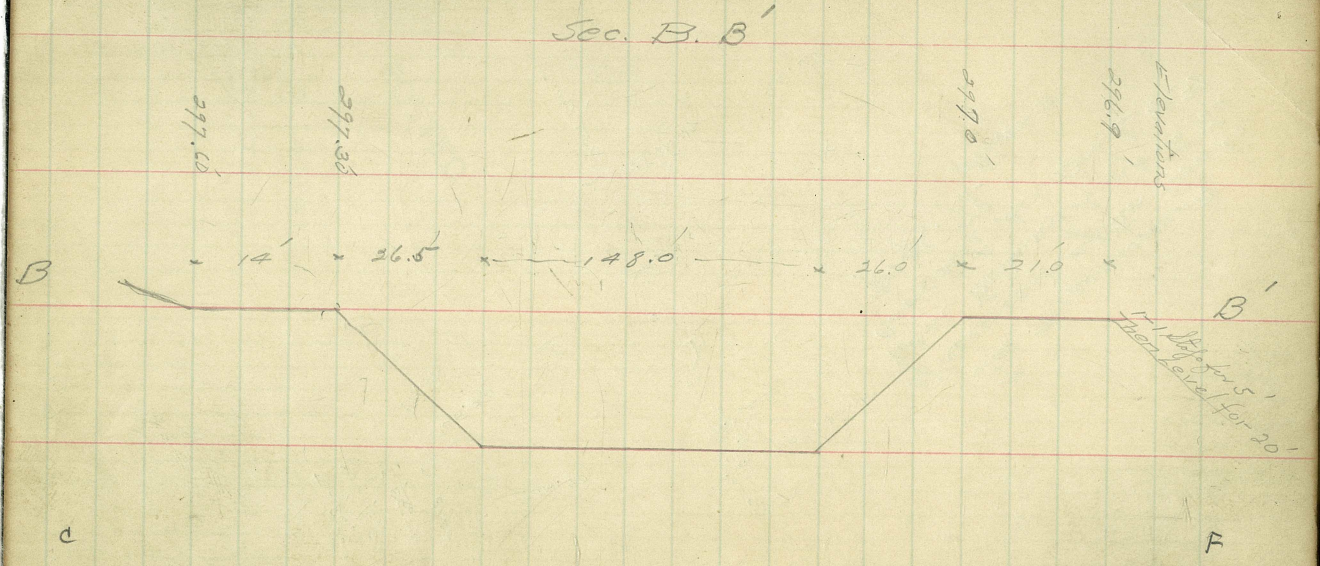
POSTED

Pacific Beach Reservoir

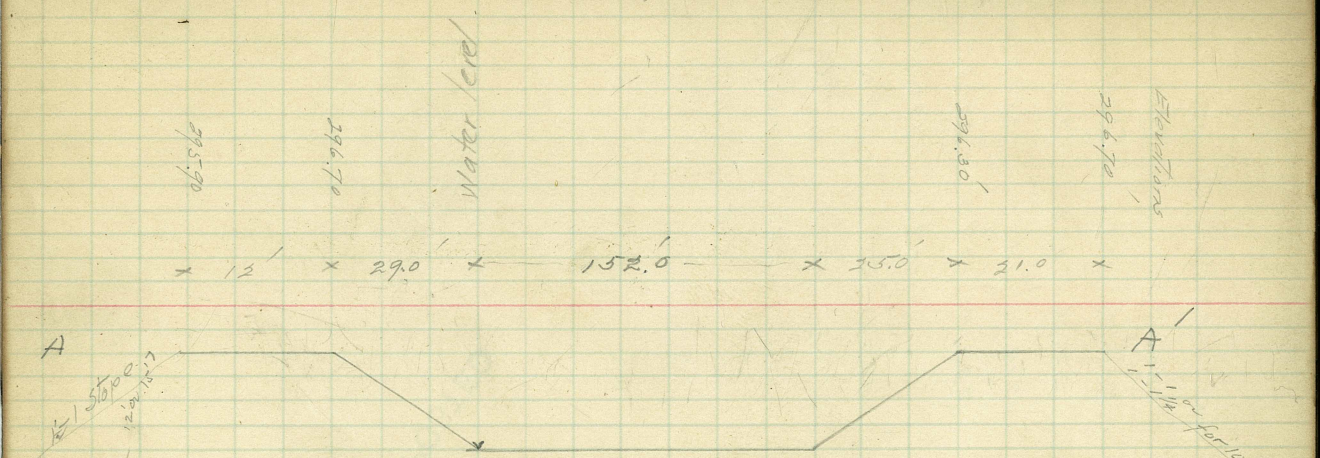
For measurements of Reservoir after Banks were trimmed up to take concrete see Book 431 pgs. 78-



Sec. B. B'



Sec A, A'



Note End of outlet pipe is
1.5' inside water line

Average Bottom 6" below water level.

C F

Check Levels-

5.65	248.18		242.53	
0.76	235.98	12.96	235.22	
3.20	226.26	12.92	223.06	
1.50	214.76	13.00	213.26	
1.07	203.00	12.83	201.93	
		10.96	192.04	192.09
0.02	190.21	12.81	190.19	
0.41	178.27	12.35	177.86	
0.02	165.86	12.43	165.84	
BM		4.65	161.21	161.08

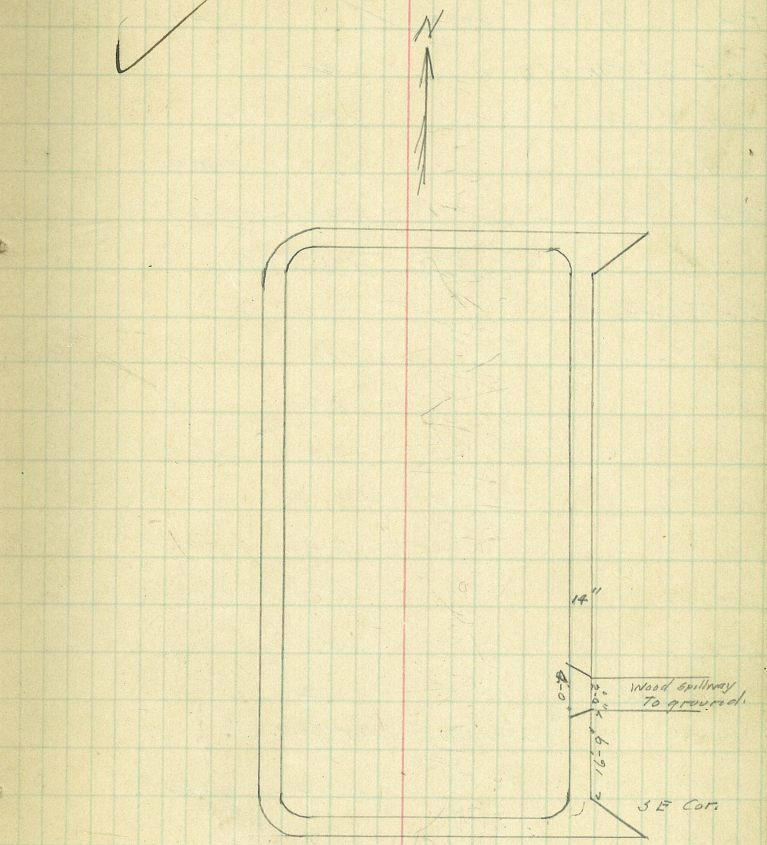
POSTED

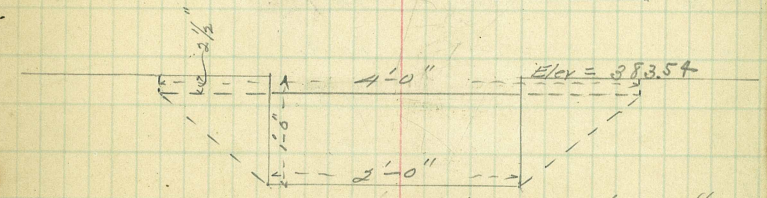
9 Hatch
11 Moore
08 Churchman

Univ Hts Reservoir
Levels

Bm.	2.57	387.18	384.61
NE Cor Top of Wall.		3.67	
NW " " " "		3.73	
SW " " " "		3.65	
SE " " " "		3.68	
Spk in Pole Idaho - El Cajon		10.33	376.85
Top of Wall at overflow		3.64	383.54
T.P.		12.46	374.72

Bolted





Cement Wier Through Wall

9/22/08 Hatch, Moore, Churchman, Profile on Polk from Cr. of Idaho to 10' from E Cb of Oregon (10' from N cb.)
" " Oregon " 10' from N Cb. of Polk. to Cr. El Cajon (10' " E cb.)

Elevations of Corners of Blk 151

T.P.	311	377.83	374.72
NE Cor Blk 151		4.40	
SE " " "		7.60	
SW " " "		9.90	367.93
NW " " "		4.00	

10' from N Cb of Polk.

Cr. Idaho.	7.2
W.L.	7.8
50	8.2
100	8.3
150	8.3
200	8.9
250	9.3
300	10.1
324 = 0+00 of ↗	11.2

10' from E. Cb. Oregon.

T.P.	11.60	366.33
0+24	10.7	
+50	10.9	
1	9.8	
+	9.1	
2	8.2	
+	8.2	
3	7.4	

		377.83		
3+50			6.4	
4			6.1	
+50			5.6	
5			5.1	
+50			4.5	
6			4.1	
+24			4.1	
+50			3.8	
7			3.8	
+50			3.6	
8			3.3	
T.P.	470	379.22	3.31	374.52
+50			4.8	
9.			5.2	
+50			4.6	
10			4.1	
+42	= SL El Cajon		3.6	
+92			4.3	
11+17	cr. "	"	3.9	

Profile on East Gutter Oregon-
Polk to Lincoln

T.P.	0.66	366.89		366.23
6+00				
=SE Gutter Oregon - Polk.			1.4	
50			2.5	
100			3.5	
150			4.1	
200			4.2	
250			5.3	
300			6.4	
350			8.5	
400			9.9	
450			10.3	
500			11.6	
T.P.	0.31	354.74	13.06	353.83
550			0.8	
600			2.2	
619			3.6	
620			3.6	
634			7.6	

Patch

Profile on W. Gutter Oregon.
Polk to Lincoln

T.P	2.21	368.44		366.23
0+00 = SW Cor	Blk 157		0.5	
0+37			2.0	
0+65			2.9	
0+96 = SW Gutter		(Oregon) Polk.	3.8	
1			4.1	
+50			5.4	
2			6.0	
+50			6.4	
3			7.2	
+50	Posted.		8.0	
4			9.7	
+50			11.5	
5			12.5	
T.P.	2.30	358.39	12.35	356.09
+50			3.2	
6			4.8	
+50			6.6	
7			8.2	
+28			10.4	
+40			15.8	

Profile N Gutter Polk
Oregon - West

	211	368.34		366.23
SW Cor	BlK 151		0.4	67.9
0+40			1.5	66.8
+80			2.7	65.6
1			3.8	64.5
+50	Posted		5.4	62.9
2			7.4	60.9
+50			9.4	58.9
3			11.8	56.5
T.P.	1.16	356.53	12.67	355.67
+50			3.9	52.9
4			8.6	48.2
T.P.	0.66	344.71	12.78	344.05
+50			1.9	42.8
5			6.0	38.7
+50			9.6	34.1
6			12.0	32.7
+50			13.4	31.3
7			14.1	30.6
T.P.	1.68	332.48	12.91	331.80
+50			3.9	
8			4.5	
+50			4.9	
9			5.0	

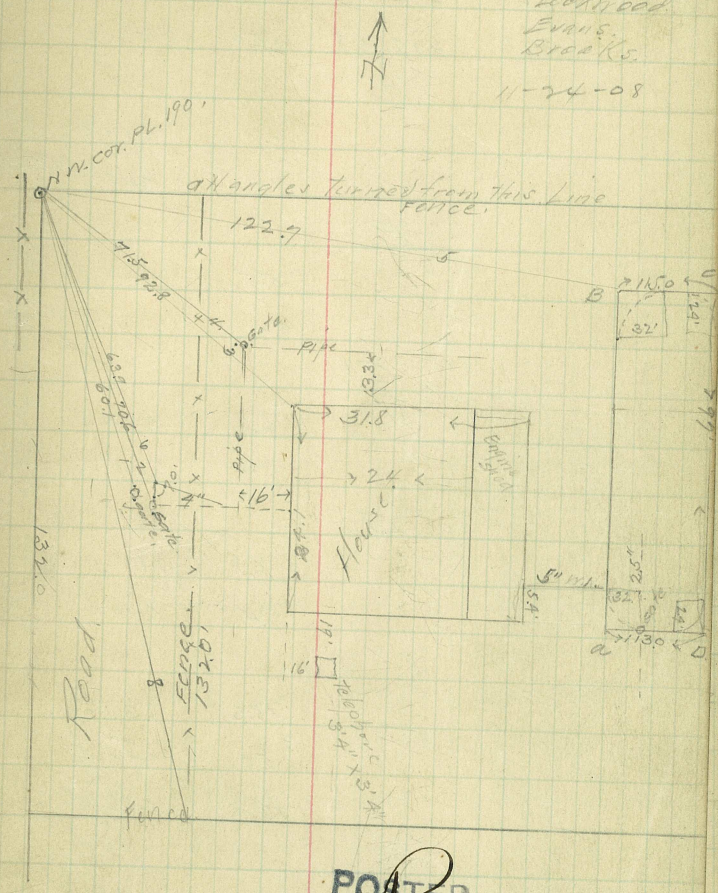
No.		Δ	Dist	
1	✓	76°57'	60.1	
2	✓	73°13'	70.6	
3	✓	36°46'	92.8	N.W. Co. House.
4	✓	35°56'	71.5	
5	✓	5°29'	122.7	
6	✓	71°37'	63.9	
7	✓	16°40'	129.5	

Waste pipe 4" center Res. E. side. gate at toe of slope

8	✓	72°17'		

Sketch Reservoir on P.L. 190.
Lower Reservoir, Pt. Loma.

Lockwood
Ennis
Brooks.
11-24-08



POSTED

Levels on Pt. Loma Reservoir.

B.M.	3.23	256.22		252.99
	3.76	249.48	10.50	245.72
		a.		
			4.7	244.8
			9.4	240.1
		B.		
			5.5	244.0
			9.4	240.1
		C.		
			6.6	242.9
			9.4	240.1
		D.		
			6.1	243.2
			9.4	240.1
			18.3	231.2
			5.0	244.5
			13.0	236.5

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Banks 2½' on top.

Top bank
Water 12.6

Top
Water 10.0

Top
Water 7.5'

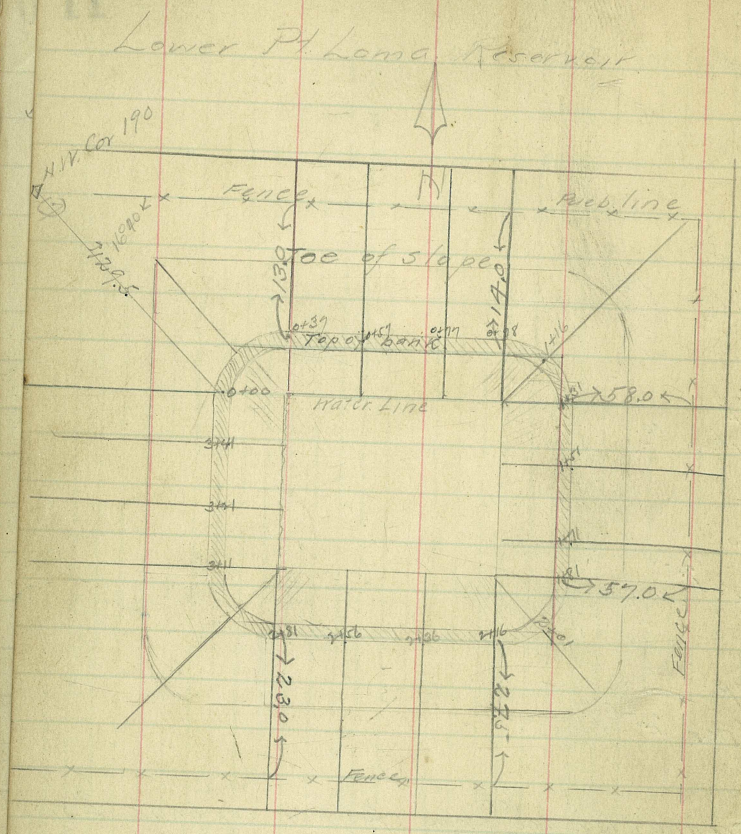
Top
Water 7.5

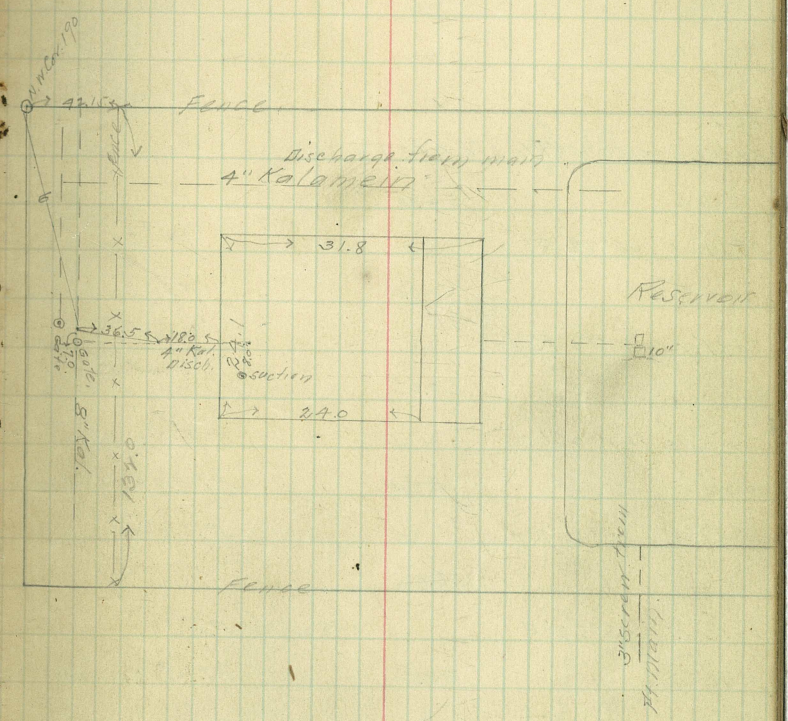
Ground elev. toe of slope 24' from top bank, E. side
" " " " " West side

Bottom reservoir

POSTED

Lower Pt. Loma Reservoir





Lower Pt Loma Reservoir

Sta	Angle	Dist.	
0+00			
3+67.5 =	50°08' Rto sta 0+37		
		56.5	
3+11	46°28 R.		
		30.0	
2+81 Δ	45°0' R.		
		65.0	
2+16 Δ	41°26		P.T.
2+01		35.0	Pt. on curve.
1+81 Δ	47°20' R.		P.C
		50.0	
1+31 Δ	43°23 R.		P.T.
1+16		33.0	Pt. on curve.
0+98 Δ	45°0' R.		P.C.
		61.0	
0+37 Δ	41°14' R.		P.T.
0+18.5		37.0	Pt on curve
0+00	57°10' L		= P.C.

Backsight = H.W. Cor. 190

X Sec. Reservoir (Lower Pt Loma)

3.78	256.27		252.99 BM.	
0.99	244.74	12.52	243.75	
	0+00			
Water 12'		4.2		40.5
Top 4'		0.7		44.0
Toe		1.4		43.3
25' from Toe		0.2		44.5
	0+18.5			
Water 9.0 distance		4.2		40.5
Top 6.0'		0.6		44.1
Toe		2.5		44.2
25'		2.1		44.6
	0+37			
Water 10.0'		4.2		40.5
Top		0.7		44.0
Toe		4.8		39.9
25'		5.2		39.5
	0+57			
Water 8.0		4.2		40.5
Top 10.0		0.8		43.9
Toe		5.5		39.2
25		6.2		38.5
	0+77			
Water 8.0		4.2		40.5
Top 11.0		1.1		43.6
Toe		7.2		37.5
25'		7.8		36.9

average width of top of Bank is 2'

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	0+98		
Water. 7.0	2474	4.2	40.5
Top. 11.0		1.6	43.1
Toe.		7.5	37.2
25'		9.3	32.4
	1+16		
Water. 6.0		4.2	40.5
Top 15.0		1.7	43.0
Toe.		10.0	34.7
25'		12.4	32.3
	1+31		
Water 6.0		4.2	40.5
Top. 25.0'		1.9	44.8
Toe.		13.7	31.0
25'		18.0	26.7
	1+51		
Water. 4.5'		4.2	40.5
Top. 25.0		1.6	43.1
Toe.		13.7	31.0
25'		18.1	26.6
	1+71		
Water 5.5		4.2	40.5
Top. 22.0		1.3	43.4
Toe.		12.1	32.6
25'		16.2	28.5

	1+81		
Water. 7.0		4.2	40.5
Top 21.0		1.3	43.4
Toe.		12.0	32.7
25'		14.7	30.0
	2+01		
Water. 6.0		4.2	40.5
Top 17.0		1.2	43.5
Toe.		9.5	35.2
25'		10.6	34.1
	2+16		
Water. 7.0		4.2	40.5
Top. 15.0		0.8	43.9
Toe.		7.0	37.7
Fence		7.4	37.3
25		6.1	38.6
	2+36		
Water. 8.0		4.2	40.5
Top 13.0		0.5	44.2
Toe.		4.7	40.0
Fence.		5.0	39.7
25		4.5	40.2

POSTED

	2+56			
		244.70		
Water. 9.0			4.2	40.5
Top 8.0			0.7	44.0
Toe.			3.1	41.6
Fence.			3.4	41.3
25			3.1	41.6
	2+81			
Water. 12.0			4.2	240.5
Top 3.0			0.5	44.2
Toe			1.9	42.8
Fence			2.3	42.4
25			1.6	43.1
T.P	3.05	246.80		243.75 B.M.
	2+96			
Water. 11.0			6.3	240.5
Top			2.3	44.5
Toe.			2.8	44.0
25			1.6	45.2
	3+11			
Water. 11.5			6.3	40.5
Top:			2.0	44.8
25'			1.5	45.3
	3+21			
Water. 10.5				40.5
Top 19.0			2.5	44.3
Shed.			1.4	45.4

	3+41		
Water. 10.5		6.3	40.5
Top.		2.6	44.2
25		1.8	45.0
	3+67.5 = 0+00		

POSTED

Levels on Upper Reservoir.

B.M.	12.93	387.71		374.78 BM
T.P.	1.45	385.98	3.18	384.53
T.P.	11.89	397.56	0.31	385.67
T.P.	5.34	401.75	1.15	396.41
		"A" Line		
50' West			12.6	89.1
0			12.4	89.3
+50			12.4	89.3
1+00			11.9	89.8
1+50			11.8	89.9
2			12.2	389.5
50' East			12.8	88.9
		"B"		
50' West			10.3	91.4
0			9.6	92.1
+50			8.9	92.8
1			8.3	93.4
+50			8.2	93.5
2			8.6	93.1
50' East			9.2	92.5
		"C"		
50' West			8.4	93.3
0			7.4	94.3
+50			6.4	95.3

Point Loma.

	H.I. 401.75		
1		6.4	95.3
+50		5.8	95.9
2		6.0	95.7
50' East		6.5	95.2
	"D"		
50' West		6.8	94.9
0		6.1	95.6
+50		5.4	96.3
1		4.7	97.0
+50		4.9	96.8
2+00		5.0	96.7
50' East		5.7	96.0
	"E"		
50' West		6.1	95.6
0		5.9	95.8
+50		5.4	96.3
1		5.2	96.5
+50		5.4	96.3
2		5.6	96.1
35' E.		5.2	96.5
20' N. Bridge		7.5	94.2

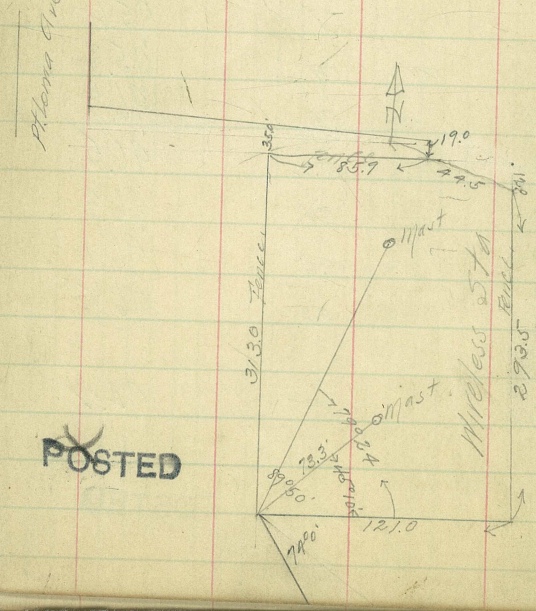
POSTED

Upper Reservoir (New site)

12-14 08
Lockwood
Evans
Brooks

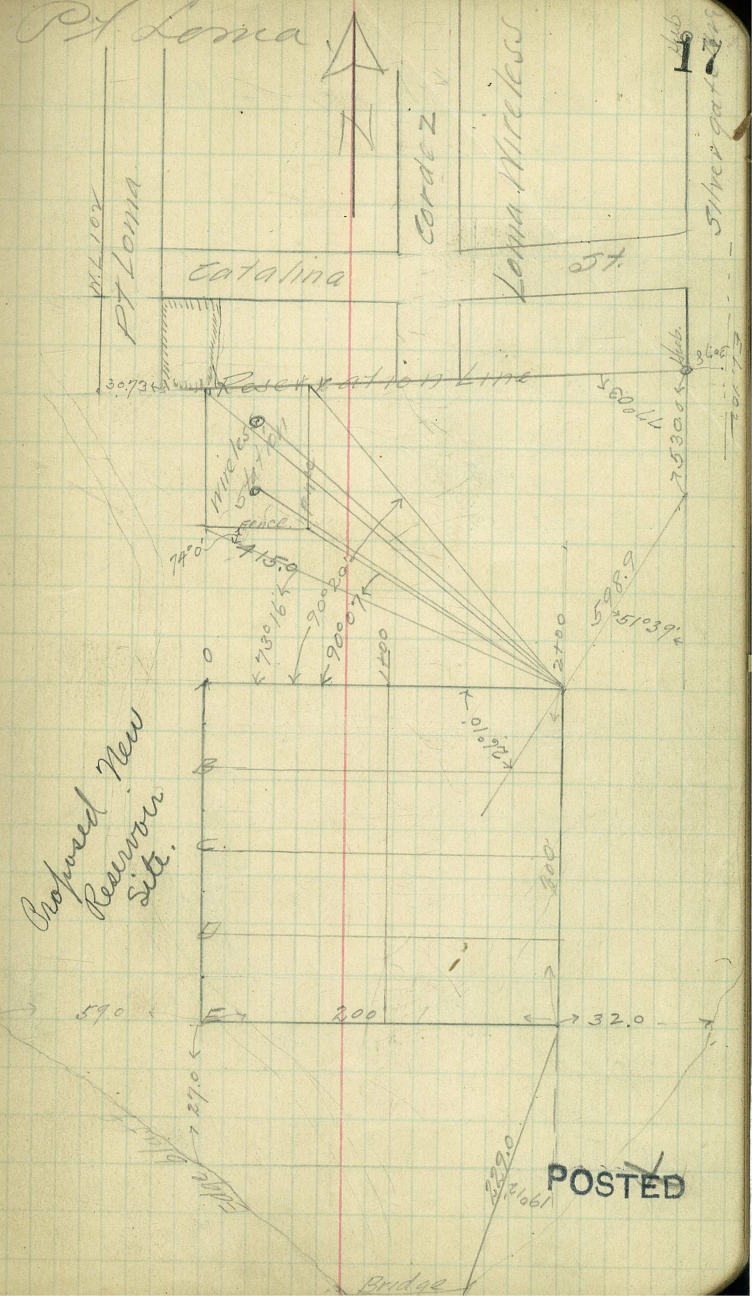
		Distance	
1	73°16	415.0'	S.W. cor. Fence Wireless
2	90°07'	398.8'	S.E " " "
3	90°20'		N.E. " "
4			N.W. " " "
5	81°17'		Mast. South.
6	83°55'		" North.

all above angles turned from sta at N.E. cor. proposed reservoir. foresight on N.W. cor.



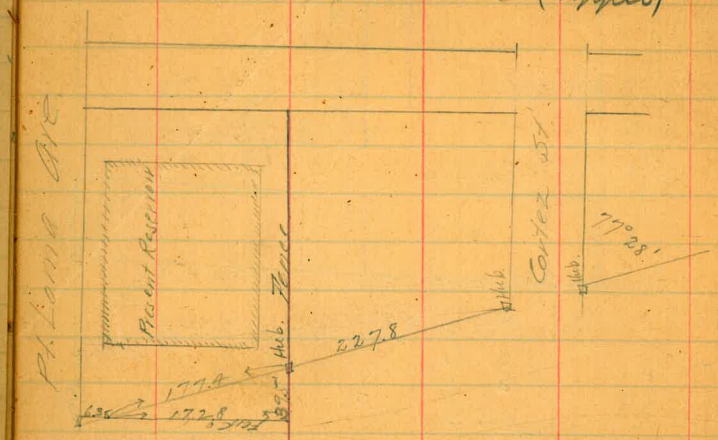
POSTED

Pt Loma



POSTED

Pt Loma Reservoir (Upper)



Levels on ~~Lower~~ upper 227.8 / 177.4 Reservoir Pt Loma.

12.38	387.16		374.78 B.M.
S.W. Cor. Top.		2.0	85.1
Bottom spillway.		3.04	84.12
S.E. Cor. Top.		1.25	85.9
N.E. Cor. Top.		1.2	85.9
N.W. " "		1.6	85.5
Water level		9.65	77.51
Bottom Reservoir 5.5' Water. =			77.0

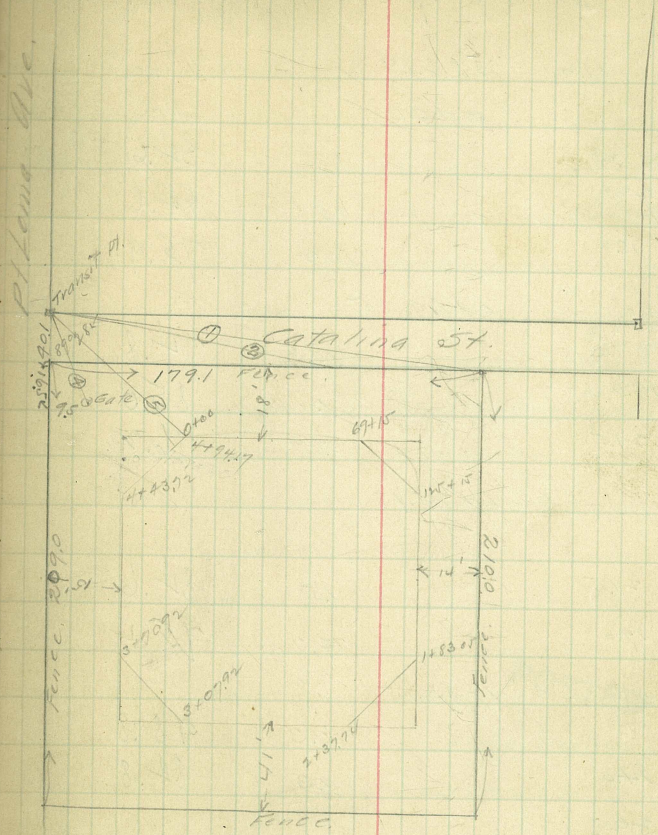
7/31/08

POSTED

Location ~~Lower~~ Upper? Reservoir.

1	11°50' R.	183.3'	N.E. cor Fence
2	13°30' R.	161.0	Gate valve.
3	89°28' R.	40.1	N.W. cor. Fence.
4	82°26' R.	57.2	
5	49°48' R.	78.25	= 0+00 Pt on top of bank
494.17	48°20'		
		50.45	
443.72	38°24'		4+94.17 = 0+00
		72.8	
370.92	52°33'		
		63.0	
307.92	51°57' R.		
		70.18	
237.74	40°29' R.		
		54.69	
183.05	39°50' R.		
		57.9	
125+15	47°07' R.		
		56.0	
69+15	41°19' R.		
		69.15	
0+00	51°20' L.		

B.S. on S.W. Cor. Blk.



POSTED

X

Sections of Present Upper P.L. Reservoir

	11.41	386.19		374.78
		0+00		
Water.			15	84.6
Top bank	22.0		1.5	84.6
Toe	18.0		10.2	75.9
		0+69.15		
Toe.			11.3	74.8
Top.	19.0		1.1	85.0
Water.	21.5		9.9	76.2
		1+25.15		
Water.				
Top	21.5		1.5	84.6
Toe	19.0		10.7	75.4
		1+83.05		
Toe			7.3	78.8
Top	14.0		1.3	84.8
Water.	20.0			
		2+37.74		
Water.				
Top.	20.0	POSTED	1.3	84.8
Toe	14.0		4.8	81.3
		3+07.92		
Toe.			4.3	81.8
Top.	13.0		1.5	84.6
Water.	20.5			

		3+70.92		
Water.				
Top	20.0		1.9	84.2
Toe.	14.0		6.0	80.1
		4+43.72		
Water.				
Top.	21.0		1.7	84.4
Toe.	17.0		8.4	77.7

POSTED

1/29/69 Hatch
Moore
Deziel

Survey of Blk 71 Homestead Union
for F A Binney

95°05'
525.6

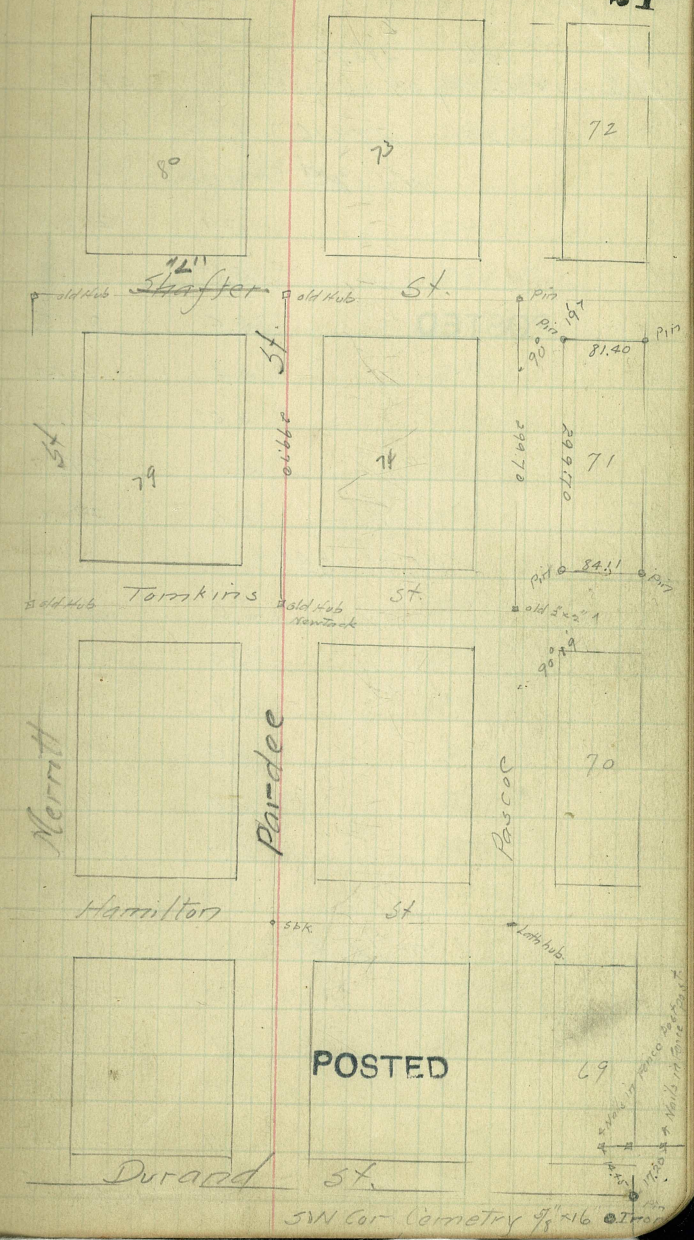
84.11
81.4
2.71 | 300
.009
80
.720

2.700

84.83

POSTED

84.11
72
84.83



3/17/09 (Hatch / Moore / Dezil) Section Broadway from 2st to 4th

	17.6	293.76		
BM Lewis & 3d Plg. SW				292.0
	3.22	294.16	2.82	290.94
		W L 2st Changed to 1st		
S			3.9	290.3
cb			3.5	290.7
1/4	POSTED		3.4	290.8
c			3.4	290.8
1/4			3.5	290.7
cb			3.5	290.7
N			3.1	291.1
		W cb 2st		
N			3.0	291.2
cb			3.0	291.2
1/4			2.9	291.3
c			3.0	291.2
1/4			3.0	291.2
cb			2.7	291.5
S			3.0	291.2
		W 1/4 2st		
S			3.0	291.2
cb			2.7	291.5
1/4			2.7	291.5
c			2.7	291.5
1/4			2.7	291.5

Continued from P 33

			294.16	
cb	x		2.8	291.4
N	x		2.5	291.7
			Cr. 2st	
N	x		2.5	291.7
cb	x		2.7	291.5
1/4	x		2.7	291.5
c	x		2.7	291.5
1/4	x		2.7	291.5
cb	x		2.8	291.4
S	x		3.1	291.1
	x		E 1/4 2st	
S	x		2.8	291.4
cb	x		2.7	291.5
1/4	x		2.5	291.7
c	x		2.4	291.8
1/4	x		2.4	291.8
cb	x		2.3	291.9
N	x		2.1	292.1
			E cb 2st	
N	x		2.3	291.9
cb	x		2.4	291.8
1/4	x		2.6	291.6
c	x		2.5	291.7
1/4	x		2.5	291.7

294.16

cb	2.4	291.6
S	2.7	291.5

EL 2st

S	2.4	291.8
cb	2.1	292.1
1/a	2.2	292.0
c	2.2	292.0
1/a	1.9	292.3
cb	2.1	292.1
N	1.6	292.6

25' E

N	2.8	291.4
cb	3.0	291.2
1/a	2.8	291.4
c	2.2	292.0
1/a	2.3	291.9
cb	2.4	291.8
S	2.5	292.1

50' E

S	2.6	291.6
cb	3.0	291.2
1/4	3.0	291.2
c	3.0	291.2
1/a	3.2	291.0

294.16

cb	3.4	290.8
N	3.1	291.1

75' E

N	4.0	290.2
cb	3.4	290.8
1/a	3.4	290.8
c	3.4	290.8
1/a	3.2	291.0
cb	3.2	291.0
S	3.0	291.2

100 E

S	3.4	290.8
cb	3.9	290.3
1/a	4.0	290.2
c	4.2	290.0
1/a	4.4	289.8
cb	4.7	289.5
N	5.0	289.2

125' E

N	5.3	288.9
cb	5.1	289.1
1/4	4.8	289.4
c	4.5	289.7
1/4	4.4	289.8

294.16

cb	4.2	290.0
B	3.7	290.5

150' E

s	3.7	290.5
cb	4.8	289.4
1/a	5.1	289.1
a	5.2	289.0
1/a	5.2	289.0
cb	5.4	288.8
N	5.0	289.2

175' E

N	5.2	289.0
cb.	5.2	289.0
1/a	5.3	288.9
a	5.3	288.9
1/a	5.2	289.0
cb	5.0	289.2
s	4.2	290.0

200' E F W L Bachman Place

s	4.4	289.8
cb	5.3	288.9
1/a	5.2	289.0
c	4.8	289.4
1/a	4.8	289.4

294.16

cb	4.9	289.3
N	4.4	289.8

W cb. Bachman Place

N	5.2	289.0
cb	5.2	289.0
1/a	5.3	288.9
c	5.6	288.6
1/a	5.8	288.4
cb	5.4	288.8
s	5.0	289.2

W 1/a.

s	5.4	288.8
cb	5.7	288.5
1/a	5.9	288.3
a	6.0	288.2
1/a	5.9	288.3
cb	6.0	288.2
N	5.9	288.3

Cr.

N	6.4	287.8
cb	6.5	287.7
1/a	6.0	288.2
c	5.6	288.6
1/a	5.3	288.9

POSTED

29416		
cb	5.1	289.1
S	5.0	289.2
E 1/4		
S	4.9	289.3
cb	4.9	289.3
1/4	4.9	289.3
c	5.3	288.9
1/4	6.1	288.1
cb	6.2	288.0
N	6.4	287.8
E cb.		
N	6.4	287.8
cb	6.4	287.8
1/4	6.2	288.0
c	5.6	288.6
1/4	5.6	288.6
cb	5.4	288.8
S	5.2	289.0
E L. Bachman Place		
S	5.1	289.1
cb	5.8	288.4
1/4	5.9	288.3
c	6.0	288.2
1/4	6.1	288.1

29416		
cb	6.4	287.8
N	6.4	287.8
25 E		
N	6.7	287.5
cb	6.7	287.5
1/4	6.2	288.0
c	6.4	287.8
1/4	6.2	288.0
cb	5.8	288.4
S	5.4	288.8
50 E		
S	6.0	288.2
cb	6.4	287.8
1/4	7.0	287.2
c	7.0	287.2
1/4	6.7	287.5
cb	6.7	287.5
N	6.8	287.4
75 E		
N	7.3	286.9
cb	7.3	286.9
1/4	7.3	286.9
c	7.0	287.2
1/4	7.0	287.2

		294.16		
cb			6.5	287.7
S			5.4	288.8
T.P.	5.18	292.86	6.48	287.68
		100' E		
S			5.4	287.5
cb			5.7	287.2
1/4			6.1	286.8
C			6.6	286.3
1/4			6.6	286.3
cb			6.4	286.5
N			6.6	286.3
		125' E		
N			7.6	285.3
cb			7.6	285.3
1/4			7.4	285.5
C			7.1	285.8
1/4			6.9	286.0
cb			6.9	286.0
S			6.4	286.5
		150' E		
S			6.8	286.1
cb			6.5	286.4
1/4			6.6	286.3
C			6.7	286.2

	292.86	
1/4	6.8	286.1
cb	7.0	285.9
N.	7.9	285.0
	175' E	
N	7.2	285.7
cb	7.7	285.2
1/4	7.6	285.3
C	7.4	285.5
1/4	7.3	285.6
cb	7.1	285.8
S	6.8	286.1
	200' E	
S	6.6	286.3
cb	6.1	286.8
1/4	6.2	286.7
C	6.1	286.8
1/4	6.6	286.3
cb	6.5	286.4
N	6.6	286.3
	230' E = WL. 3d St	
N	6.6	286.3
cb	6.4	286.5
1/4	6.4	286.5
C	6.4	286.5

292.86		
1/4	6.2	286.7
cb	6.3	286.6
S	6.5	286.4
El. 3d St.		
S	5.1	287.8
cb	5.2	287.7
1/4	5.5	287.4
C	5.3	287.6
1/4	5.1	287.8
cb	5.1	287.8
N	5.2	287.7
25' E		
N	5.1	287.8
cb	4.9	288.0
1/4	4.9	288.0
C	5.3	287.6
1/4	5.4	287.5
cb	5.1	287.8
S	4.9	288.0
50' E		
S	4.9	288.0
cb	5.1	287.8
1/4	5.2	287.7
C	5.3	287.6

292.86		
1/4	5.3	287.6
cb	5.4	287.5
N	5.3	287.6
75' E		
N	5.4	287.5
cb	5.5	287.4
1/4	5.4	287.5
C	5.6	287.3
1/4	5.6	287.3
cb	5.4	287.5
S	5.1	287.8
100' E		
S	5.5	287.4
cb	5.8	287.1
1/4	5.8	287.1
C	5.9	287.0
1/4	5.7	287.2
cb	5.8	287.1
N	6.1	286.8
125' E		
N	6.1	286.8
cb	6.1	286.8
1/4	6.2	286.7
C	6.3	286.6

	292.86		
1/c		6.2	286.7
cb		6.2	286.7
s		6.2	286.7
	150' E		
s		6.7	286.2
cb		6.9	286.0
1/a		6.9	286.0
c		7.0	285.9
1/a		6.8	286.1
cb		6.9	286.0
N.		6.8	286.1
	175' E		
N		5.9	287.0
cb		7.1	285.8
1/a	POSTED	7.6	285.3
c		7.2	285.7
1/a		7.0	285.9
cb		6.9	286.0
s		6.9	286.0
	200' E = N L. 4th		
s		8.1	284.8
cb		8.4	284.5
1/a		8.2	284.7
c		8.2	284.7

292.86		
1/a	8.0	284.9
cb	7.8	285.1
N.	7.6	285.3

POSTED

3/17/09 Hatch Movr Degrel

X sections of Stockton St
1st to Bachman Place

TP	3.84	294.78		290.94
	5.22	295.15	4.85	289.93
	WL 2d (South 1/2)			
s			5.6	289.6
cb	(Seccond St is 80' on S line Stockton w cb)		5.5	289.7
1/a			5.4	289.8
c			5.4	289.8
c			5.0	290.2
1/a			5.2	290.0
cb			5.4	289.8
s			5.6	289.6
	W 1/4			
s			5.7	289.5
cb			5.4	289.8
1/a			5.3	289.9
c			5.2	290.0
	Cr.			
c			5.0	290.2
1/a			5.3	289.9
cb			5.6	289.6
s			5.4	289.8
	E 1/4			
s			5.5	289.7

POSTED

	295.15	
cb	5.4	289.8
1/a	5.3	289.9
c	5.1	290.1
	E cb.	
c	4.8	290.4
1/a	5.1	290.1
cb	5.3	289.9
s	5.6	289.6
	E L.	
s	5.3	289.9
cb	5.2	290.0
1/a	5.1	290.1
c	5.0	290.2
	20' E of 2d on S. side = 50' E N side	
s	5.4	289.8
cb	5.2	290.0
1/a	5.3	289.9
c	5.7	289.5
1/a	5.6	289.6
cb	5.5	289.7
N	5.7	289.5

POSTED

Continued on P 38

29515

W.L. 7st (South 1/2)

N	4.3
cb	5.2
1/a	5.2
c	5.4

25' E

c	5.2
1/a	5.0
cb	4.8
N	4.6

Void

50' E of W.L. 1st (South) = W.L. 1st (North)

N	4.8
cb	4.8
1/a	4.7
c	5.0

W cb 1st (North)

c	4.9
1/a	4.7
cb	4.8
N	5.2

W 1/a 1st

N	5.4
cb	4.9
1/a	4.7
c	4.7

29515

C2 1st

c	4.9
1/a	4.9
cb	5.1
N	5.6

Void

E 1/a 1st

N	5.6
cb	5.3
1/a	5.1
c	4.8

E cb 1st

c	5.3
1/a	5.2
cb	5.4
N	5.6

80' E of 2nd (on N side)

N	5.6	289.6
cb	6.0	289.2
1/a	6.5	288.7
c	6.6	288.6
1/a	6.4	288.8
cb	6.1	289.1
s	6.2	289.0

295.15

105' E

S	6,8	288.4
cb	7,1	288.1
1/a	7,1	288,1
c	7,1	288,1
1/a	7,1	288,1
cb	7,1	288,1
N	7,0	288,2

130' E

N	8,3	286.9
cb	8,2	287.0
1/a	8,4	286.8
c	8.3	286.9
1/a	8,4	286.8
cb	8.0	287.0
S	7.4	287.8

155' E

S	8,4	286.8
cb	8.8	286.4
1/a	9,0	286.2
c	9,0	286.2
1/a	8,6	286.6
cb	8,7	286.5
N	8,5	286.7

295.15

180' E

N	9,1	286.1
cb	9.0	286.2
1/a	9.2	286.0
c	9,2	286.0
1/a	9.3	285.9
cb	9.0	286.2
S	9.2	286.0

205' E

S	11.5	283.7
cb	10.8	284.4
1/a	10.2	285.0
c	10,1	285.1
1/a	10.0	285.2
cb	9.9	285.3
N	10.0	285.2
TP. 063 286.17	9.61	285.54

230' E = W L. Bachman Place

N	9.4	276.8
cb	9.8	276.4
1/a	9.9	276.3
c	9.2	277.0
1/a	8.9	277.3
cb	9.2	277.0
S	10.6	275.6

POSTED

3/19/09 Hatch Moore Deziel X sections Broadway from 2d To 1st

TP.	3.04	293.98		290.94
		25' W of 2d 1st		
S			3.8	290.2
	not?		4.0	290.0
			4.0	290.0
			4.0	290.0
			3.9	290.1
			3.9	290.1
N			3.2	290.8
		50' W		
N			3.8	290.2
			3.9	290.1
			3.9	290.1
			4.1	289.9
			4.2	289.8
			4.4	289.6
			4.4	289.6
		75' W		
S			4.8	289.2
			4.7	289.3
			4.3	289.7
			4.2	289.8
			4.2	289.8
			4.3	289.7
			4.2	289.8

	293.98	
	100' W	
N	4.5	289.5
	4.6	289.4
	4.5	289.5
	4.6	289.4
	4.5	289.5
	4.8	289.2
	4.9	289.1
	125' W	
S	5.7	288.3
	5.7	288.3
	5.5	288.5
	5.0	289.0
	4.7	289.3
	5.0	289.0
	4.6	289.4
	150' W	
N	5.3	288.7
	5.6	288.4
	5.5	288.5
	5.8	288.2
	5.8	288.2
	5.9	288.1
	5.4	288.6

293.98
175' W

S		5.7	288.3
		6.1	287.9
		5.9	288.1
		5.6	288.4
		5.5	288.5
		5.4	288.6
		5.5	288.5
	200' W of 2d = El.		1st
N		5.6	288.4
cb		5.6	288.4
f/a		5.8	288.2
o		5.6	288.4
f/a		5.9	288.1
cb		6.1	287.9
S		6.1	287.9
	Continued on P. 22		
T.P.		2.48	291.50

3/19/09 Hatch Moore Deziel X section of Stockton from W.L. of 60' Road to Hospital to section 30' E. of 2d

T.P.	6.88	298.38		291.50
		W.L. 60' Road.		
S			7.5	290.9
			7.1	291.4
			6.7	291.7
			6.7	291.7
			6.4	292.0
			5.8	292.6
			5.6	292.8
		W. Cb.		
N			5.6	292.8
			5.9	292.5
			6.2	292.2
			6.6	291.8
			6.4	292.0
			6.5	291.9
			6.9	291.5
		W 1/4		
S			6.8	291.6
			6.6	291.8
			6.6	291.8
			6.5	291.9
			6.1	292.3
			5.8	292.6
			5.3	293.1

		298.38	
		Cr	
N		4.9	293.5
		5.8	292.6
		6.2	292.2
		6.6	291.8
		6.3	292.1
		6.2	292.2
		6.7	291.7
		E 1/4	
S		7.2	291.2
		7.2	291.2
		6.8	291.6
		6.3	292.1
		6.0	292.4
		5.5	292.9
		5.3	293.1
		E Cb	
N		4.8	293.6
		4.6	293.8
		4.6	293.8
		4.8	293.6
		5.8	292.6
		7.0	291.4
		7.6	290.8

298.38

EL. 60' Road

S	7.4	291.0
	6.8	291.6
	5.8	292.6
	4.8	293.6
	4.4	294.0
	4.2	294.2
	4.6	293.8

25' E

N	4.3	294.1
	5.6	292.8
	5.5	292.9
	5.7	292.7
	6.0	292.4
	6.4	292.0
	6.9	291.5

50' E

S	6.2	292.2
	6.1	292.3
	5.6	292.8
	5.5	292.9
	5.4	293.0
	4.8	293.6
	3.6	294.8

298.38

75' E

N	4.3	294.1
	3.6	294.8
	3.7	294.7
	3.7	294.7
	4.4	294.0
	5.0	293.4
	5.8	292.6

100' E

S	5.9	292.5
	5.5	292.9
	5.0	293.4
	4.3	294.1
	4.5	293.9
	4.5	293.9
	4.3	294.1

125' E

N	4.3	294.1
	4.5	293.9
	4.5	293.9
	4.1	294.3
	4.1	294.3
	4.5	293.9
	5.3	293.1

298.38

149° E = P.L.

S	3.8	294.6
	4.4	294.0
	4.6	293.9
	3.8	294.6
	3.0	295.4
	2.7	295.7
	3.1	295.3

166' E

N.	4.4	294.0
	3.9	294.5
	4.0	294.4
	4.3	294.1
	4.7	293.7
	4.9	293.5
	4.9	293.5

181' E = E.L. 7th

S	5.3	293.1
	5.0	293.4
	5.1	293.3
	5.2	293.2
	5.0	293.4
	5.0	293.4
	4.9	293.5

298.38

25' E of 1st

		~~293.6~~
N.	4.8	293.6
	4.9	293.5
	5.5	292.9
	5.7	292.7
	5.1	293.3
	4.1	294.3
	4.0	294.4

50' E

S	5.6	292.8
	5.9	292.5
	6.0	292.4
	5.8	292.6
	5.9	292.5
	6.1	292.3
	5.8	292.6

75' E

N	7.1	291.3
	6.5	291.9
	5.9	292.5
	5.7	292.7
	5.7	292.7
	5.9	292.5
	6.0	292.4

298.38

100' E

S	7.4	291.4
	7.3	291.1
	7.5	290.9
	7.7	290.7
	7.6	290.8
	7.7	290.7
	7.8	290.6

125' E

N	7.2	291.2
	7.7	290.7
	7.7	290.7
	7.7	290.7
	7.6	290.8
	7.7	290.7
	8.1	290.3

150' E

S	8.3	290.1
	8.1	290.3
	7.9	290.5
	8.1	290.3
	8.1	290.3
	8.0	290.4
	7.6	290.8

298.38

175' E

N.	8.0	290.4
	8.4	290.0
	8.5	289.9
	8.5	289.9
	8.5	289.9
	8.4	290.0
	7.0	291.4

200' E = N.L. 2d

S	8.9	289.5
	8.7	289.7
	8.7	289.7
	8.6	289.8
	8.4	290.0
	8.4	290.0
	8.2	290.2

T.P. 4.07 294.82 7.63 290.75

W. ch. 2d (North Half)

N	4.3	290.5
d	4.8	290.0
a	4.7	290.1
c	4.7	290.1

{2d St is 50 on North Line Stockton St.}

294.82

W 1/4 2d

C	4.7	290.1
1/4	4.5	290.3
cb	4.7	290.1
N	4.1	290.7

Cr.

N	4.2	290.6
cb	4.5	290.3
1/4	4.6	290.2
C	4.9	289.9

E 1/4

C	4.8	290.0
1/4	4.7	290.1
cb	4.5	290.3
N	4.2	290.6

E cb

N	4.4	290.4
cb	4.4	290.4
1/4	4.5	290.3
C	4.6	290.2

E L. 2d (North half)

C	4.8	290.0
1/4	4.4	290.4
cb	4.4	290.4
N	4.4	290.4

294.82

25' E

N	4.9	289.9
cb	4.6	290.2
1/4	4.5	290.3
C	4.5	290.3

Continued on P. 39.

3/25/09 Hatch Moore Shattuck — Profile levels Union St from Palm North.

	971	203.00		193.29
Nh Palm		1		
50		POS	POSTED	
100				
T.P.	687	202.54	733	195.67
150				
175				
200				
250				
275				
TP	12.45	214.63	0.36	202.18
250				
275				
300 S.L. Quince				
Cr. Quince				
Nh. Quincy				
50				
100				
150				
200				
250				
300 = S.L. Redwood				
T.P.	0.73	206.90	846	206.17
Cr Redwood				

29

W		C		E	
5.2	197.8	4.7	198.3	4.0	199.0
8.3	194.7	6.8	196.7	3.7	199.2
15.4	187.6	8.8	194.2	4.7	198.3
19.3	183.2	11.6	190.9	5.4	197.1
19.5	183.0				
17.1	185.4	11.2	191.3	5.7	196.8
8.4	194.1	4.9	197.6		
5.0	197.5	1.5	201.0		
				12.2	202.4
				10.8	203.8
14.1	200.5	11.1	203.5 ✓	8.5	206.1
10.9	203.7	8.4	206.2	6.8	207.8
9.2	205.4	6.4	208.2	3.6	211.0
8.1	206.5	5.5	209.1	2.2	212.4
7.9	206.7	4.3	210.3	2.1	212.5
6.6	208.0	3.6	211.0	0.9	213.7
6.3	208.3	3.5	211.1	0.9	213.7
6.3	208.3	4.1	210.5	1.0	213.6
8.6	206.0	6.3	208.3	3.1	211.5
3.6	203.3	2.0	204.9 +	0.9	207.8

		206.90		
NL	Redwood			
25				
50				
TP	0.42	192.52	12.80	194.10
50				
75				
100				
TP	0.36	182.28	12.60	181.92
100				
125				
150				
TP	0.59	170.10	12.77	169.51
150				
175				
200				
TP	3.63	161.35	12.38	157.72
200				
225				
250				
275				
300				
Cr. Spring				
NL	"			

W		C		E	
8.1	198.8	6.5	200.4	3.0	203.9
12.4	194.5	11.2	195.7	7.3	199.6
	[illegible]	15.1	191.8	10.8	196.1
5.5	189.0				
11.3	183.2	8.6	185.9	4.3	190.2
		15.0	179.5	9.9	184.6
6.7	175.6				
12.2	170.1	9.6	172.7	3.5	178.8
		15.3	167.0	8.8	173.5
8.2	161.9				
13.7	156.4	7.0	163.1	1.0	169.1
		11.7	158.4	5.4	164.7
11.5	149.9				
17.7	143.7	6.4	155.0	+1.1	162.5
20.8	140.6	9.6	151.8	1.3	160.1
22.2	139.2	11.4	150.0	3.9	157.5
19.8	141.6	11.6	149.8	4.6	156.8
		12.8	148.6	6.4	155.0
				9.6	151.8

		161.35								
TP	0.23	148.98	12.60	148.75						
Cr. Spruce					8.3	140.7				
N.L. "					14.0	135.0	4.4	144.6		
25									7.5	141.5
50									12.1	136.9
75									12.8	136.2
T.P.	0.44	136.75	12.67	136.31						
25					9.4	125.4	1.5	135.3		
50					18.2	118.6	9.4	127.4		
75							10.4	126.4		
100							16.4	120.4	6.9	129.9
TP	0.96	125.13	12.58	124.17						
75					9.8	115.3				
100					10.0	115.1				
125					10.0	115.1	5.6	119.5	+0.2	125.3
150					10.2	114.9	6.4	118.7	2.6	122.5
175					10.7	114.4	8.1	117.0	6.0	119.1
200					10.4	114.7	9.5	115.6	8.8	116.3
225					8.0	117.1	9.4	115.7	8.9	116.2
250					2.2	122.9	7.9	117.2	8.7	116.4
275							1.4	123.7	8.3	116.8
300 = S.L. Sassafras,									4.1	121.0
T.P.	11.86	136.68	0.31	124.82						

			136.68								
275											
300 = S.L. Sassafras.											
Cr. Sassa.											
T.P.	12.15	148.27	0.56	136.12							
300											
Cr. Sassafrass											
T.P.	12.72	160.01	0.98	147.29							
Cr. Sassafrass											
Nh.	"										
25											
T.P.	12.87	172.07	0.81	159.70							
Nt. Sassafrass											
25											
50											
75											
T.P.	12.30	183.66	0.71	171.36							
25											
50											
75											
100											
T.P.	12.22	195.31	0.57	183.09							
75											
100											
T.P.	12.90	204.35	3.86	191.45							

N		C		E	
4.5	137.2				
		2.6	134.1		
				2.5	134.2
5.9	142.4				
		0.1	148.2		
1.5	158.8				
		0.4	159.6	11.5	148.5
				3.0	157.0
1.3	170.8				
		6.1	166.0		
				6.9	165.2
				0.9	171.2
7.7	176.0				
2.1	181.6	9.9	173.8		
		2.8	180.9		
				4.4	179.3
8.0	187.3				
2.8	192.5	8.4	186.9		

5/11/09 Hatch Twins Thomas

125		204.35		
150				
175				
200				
T.P.	11.61	215.34	0.62	208.73
250				
300 = SL Thorn				
Cr.	"			
N.L.	"			
50 N.				
T.P.	7.20	222.13	0.41	214.93
100				
150				
200				
250				
300 = SL Upas				
Cr.	"			
N.L.	"			
50				
100				
150				
200				
250				
300 = SL Vine				
T.P.	0.24	210.83	1.54	210.59

W		C		E	
7.7	196.7	11.7	192.7	18.6	185.8
5.0	199.4	6.8	197.6	12.8	192.1
3.4	201.0	3.6	200.8	9.0	195.4
2.1	202.3	1.6	202.8	6.2	198.2
11.6	203.7	9.5	205.8	10.5	204.8
9.5	205.8	7.6 (Mon.)	207.7	7.2	208.1
8.0	207.3	5.5	209.7	5.4	209.9
5.1	210.2	3.0	212.3	3.8	211.5
2.9	212.4	0.8	214.5	2.0	213.3
7.9	214.2	6.0	216.1	6.7	215.4
7.1	215.0	4.3	217.8	4.3	217.8
9.1	213.0	4.9	217.2	2.9	219.2
12.6	209.5	5.7	216.4	2.6	219.5
15.6	206.5	7.6	214.5	3.6	218.5
		9.5	212.6	3.7	218.4
		11.9	210.2	6.3	215.8
		14.5	207.6	9.6	212.5
				12.2	209.9
				12.5	209.6
				11.1	211.0
				11.0	211.1
				11.2	210.9

Continued on P 58

Pt. Loma. Ave.

Survey of base line for Contour survey on Pt. Loma

3-30-09
Lockwood
Evans
Taylor.

66+03.6 34.1 E of Cor. = N.W. Cor. Res. Lot

53+00 △

33+65.7 Inter. N. Line 1st

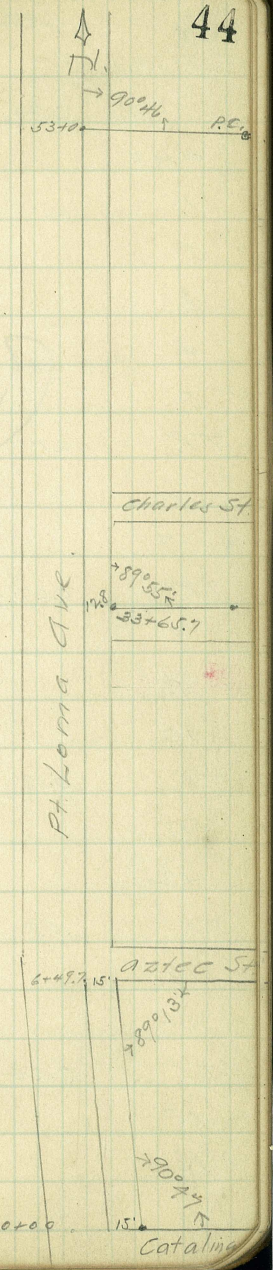
26+00 △

24+00 △

15+00 △

6+49.7 △ 0°47'30" R. S. Line Aztec St.

0+00 △



Levels on base line. Pt. Loma Blvd.
Roadway. 50' wide

Station				Pt Loma & Catalina 374.98 B.M.	West Cut	West Fill	East Cut	East Fill
	2.20	376.98						
0+00			1.9	375.08	1.1		0.5	
1			4.3	372.7	0.8		0.5	
2			6.1	370.9	0.7		0.3	
3			7.6	369.4	1.1		0.8	
4			9.4	367.6	1.8		1.5	
5			11.80	365.2	1.7		1.8	
T.P.	0.17	364.58	12.57	364.41				
6			3.3	361.3	1.1		1.1	
7			8.3	356.3	0.8		0.7	
T.P.	0.07	352.14	12.51	352.07				
8			1.3	350.8	1.0		0.8	
9			7.0	345.1	1.7		1.4	
10			13.0	339.1	1.7		0.8	
T.P.	0.13	339.33	12.94	339.20				
11			6.8	332.5	0.3			0.4
12			12.70	326.6	0.3			2.0
T.P.	0.91	327.41	12.83	326.50				
13			7.0	320.4	0.5			0.5
14			12.0	315.4	0.5			
T.P.	0.04	*315.20	12.25	315.16				
15			4.2	311.0	0.7		0.2	
16			8.0	307.2	0.4			

1260 cu. yd.

Posted

376.98 = bottom of dome of main bldg.
426.0 Top of dome. Theosophists

					West Cut	East Cut
		315.20				
17+00			10.8	304.4	0.6	0.2
18			13.0	302.2	0.5	0.4
T.P.	0.92	303.20	12.92	302.28		
19			2.9	300.3	0.7	
20			4.4	298.8	.5	1.6
21			5.0	298.2		2.0
22			4.9	298.3		1.6
23			5.4	297.8		1.6
24			5.8	297.4		1.9
T.P.	4.10	301.50	5.80	297.40		
25			4.4	297.1		2.3
26			4.7	296.8	0.2	2.3
27			6.2	295.3	0.4	2.7
28			9.3	292.2	0.3	3.0
T.P.	0.29	289.36	12.43	289.07		
B.M.			0.91	opp. Sta. 28. 288.45		
29			1.0	nail in fence 288.4	0.1	2.3
30			5.8	283.6		2.0
31			9.7	279.7		2.5
32			13.3	276.1		3.0
T.P.	0.81	277.35	12.82	276.54		
33			4.8	272.6		2.5
34			7.9	269.5		1.4
35			10.4	267.1		0.9

					West Cut		East Cut		Fill
		277.35							
36			12.4	265.0			1.4		
T.P.	3.05	267.88	12.52	264.83		7252			
37			3.4	264.5			1.2		
38			5.0	262.9	0.1		1.2		
39			6.5	261.4	0.4		1.0		
to Homestead. BM. Post at entrance			7.14	260.74					
40			8.6	259.3	0.0		1.2		
41			11.4	256.5	0.7		1.3		
T.P.	0.81	256.99	11.70	256.18					
42			4.4	252.6	0.8		1.2		
43			8.2	248.8	1.8		0.7		
44			11.2	245.8	0.3		0.0		
45			13.1	243.9					
T.P.	7.45	251.56	12.88	244.11					
45 70			8.3	243.3					
46			8.2	243.4	0.2				Fill
47			6.6	245.0	0.3		1.0		
48			4.4	247.2	0.7		1.8		
49			2.2	249.4	0.3		0.9		
T.P.	11.59	262.91	0.24	251.32					
50			11.3	251.6	0.2		0.8		
51			7.9	255.0	0.7	3370	0.6		
52			4.1	258.8	1.0		1.0		
53			1.9	261.0	Av. 1.0		Av. 1.6		

Alignment of High ground. Theosophists. 356.94 bottom Flagstaff

4-1.09
Lockwood,
Evans
Lambert

POSTED

58+60		100°12' R		= sta 53 on Pt. Loma Ave.
	1030			
48+30 △		26°0' R.		
	740			
40+90 △		3°50' L.	N 14°15' W.	
	285			
38+05.2 △		8°10' L.	N. 10°30' W.	in front of main bldg.
	1650			
21+55 △		20°47' R.	N 2°15' W.	
	1655			
5+00		3°16' R.	N. 23°0' W.	
	500			
0+00		24°0' L.	N 26°15' W.	

0+00 = 15' W. of N. side Catalina
Foresight on line on Pt Loma Ave, 6+49.7

Levels on high ground. Theosophist.

	2.82	377.60		374.78 B.M.
0			2.6	375.0
1			5.0	372.6
2			4.8	372.8
3			5.7	371.9
4			4.9	372.7
5			5.8	371.8
6.			10.2	367.4
T.P.	0.59	365.80	12.39	365.21
7			4.1	361.7
8			9.8	356.0
T.P.	2.99	355.90	12.89	352.91
9			4.4	351.5
10			6.1	349.8
11			4.8	351.1
12			5.2	350.7
13			8.1	347.8
14			12.4	343.5
T.P.	1.03	344.59	12.34	343.56
15			5.2	339.4
16			8.2	336.4
17			6.8	337.8
18			2.7	341.9

POSTED

		344.59		Top
T.P.	10.31	353.72	1.18	343.41
19			7.8	345.9
20			3.8	349.9
21			0.1	353.6
T.P.	4.45	358.08	0.09	353.63
22			3.0	355.1
23			8.9	349.2
T.P.	1.73	347.11	12.70	345.38
24			4.4	342.7
25			7.3	339.8
26			9.4	337.7
27			10.7	336.4
T.P.	0.85	335.06	12.90	334.21
28			4.2	330.9
29			8.0	327.1
30			10.0	325.1
31			10.4	324.7
T.P.	3.75	328.51	10.30	324.76
32			5.2	323.3
33			6.5	322.0
34			8.6	319.9
35			10.1	318.4
36			10.7	317.8
T.P.	11.57	329.50	10.58	317.93
37			7.6	321.9

Ground to west lies from 3 to 1.0' higher.

38	329.50	329.5	4.8	324.7
39			6.6	322.9
bottom step Main Bldg.			0.3	329.2
40			9.7	319.8
T.P.	0.00	317.89	11.61	317.89
41			3.2	314.7
T.P.	0.56	305.65	12.80	305.09
42			2.0	303.7
43			6.4	299.3
44			9.4	296.3
45			11.1	294.6
46			11.3	294.4
47			7.5	298.2
T.P.	8.76	306.91	7.50	298.15
48			4.1	302.8
48+30			3.4	303.5
49			3.7	303.2
50			6.2	300.7
51			9.5	297.4
52			12.3	294.6
T.P.	9.20	304.02	12.09	294.82
53			9.3	294.7
54			5.2	298.8
55			2.1	301.9
56			0.9	303.1

to west 10' higher

15' higher 200' west

200' W. 15' higher

12' "

		304.02		
T.P.	7.23	310.80	0.45	303.57
57			6.5	304.3
58			5.1	305.7
58+60 spk. in pole near Theos. Roseman			4.3	306.5
B.M.			5.44	305.36
T.P.	0.19	298.46	12.53	295.27
T.P.	0.67	286.95	12.18	286.28
T.P.	1.03	275.32	12.66	274.29
T.P.	2.98	265.78	13.52	262.80
			4.62	261.16

Continued from page 47.

.5	1.61	262.91 ~~262.95~~		261.30 ~~261.34~~ B.M.
54			4.7	258.2
55			5.8	257.1
56			6.2	256.7
57			5.6	257.3
T.P.	4.82	262.63 ~~262.67~~	5.10	257.81 ~~257.85~~
58			5.4	257.2
59			4.9	257.7
60			4.7	257.9
61			5.6	257.0
62			6.1	256.5
63			7.8	254.8
T.P.	1.53	256.99 ~~257.03~~	7.17	255.46 ~~255.50~~
64			3.9	253.1
65			5.2	251.8
66+0			8.7	248.3
66+03.6				

Upper Pt. Loma Reservoir

Sta.	11.80	386.58		374.78	B.M.
		5' E of. A. Line			
0+00			13.4	373.2	
0+20			13.1	373.5	
0+40			12.4	374.2	
0+60			11.6	375.0	
0+80			10.6	376.0	
1+00			9.8	376.8	
1+20			8.7	377.9	
1+40			7.6	379.0	
1+60			6.3	380.3	
1+80			4.9	381.7	
2+00			4.0	382.6	
2+10			3.1	383.5	
	Sta "A"				
0+00			13.3	373.3	
0+20			12.7	373.9	
0+40			11.9	374.7	
0+60			10.5	375.9	
0+80			9.1	377.5	
1+00			8.7	377.9	
1+20			7.8	378.8	
1+40			6.9	379.7	
1+60			5.8	380.8	
1+80			4.6	382.0	
2+00			3.6	383.0	
2+10			3.0	383.6	

POSTED

Plat showing plan of x sec. of reserv Lot

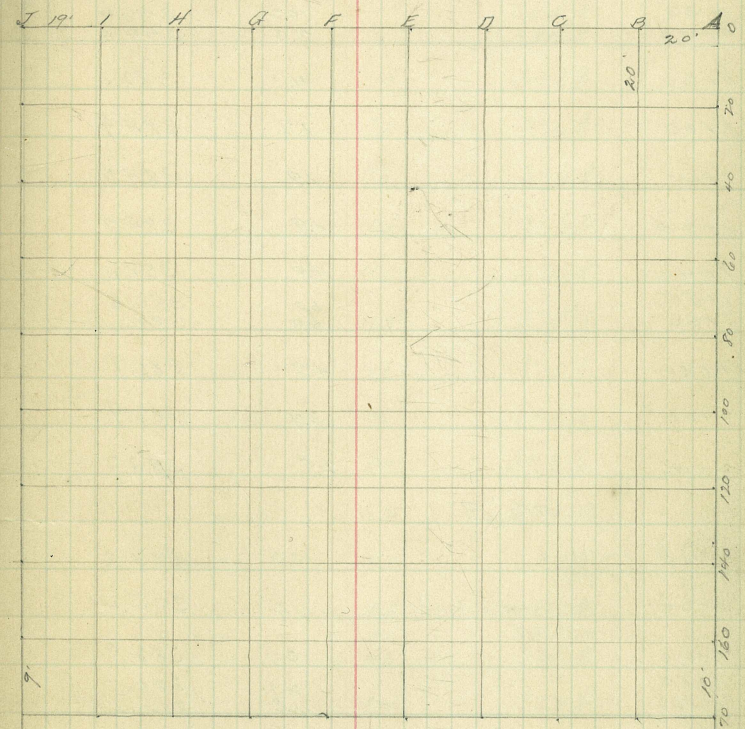
20' between stations.

N.

Lockwood.
Evans
Lambert

4-19-08

Catalina.



Well - at sta "D" - 0+54

6.6 below water level = 370.3

Water level = 376.9

A+14' = Top of E. Bank

0+00		386.6	13.3	373.3
0+20			12.1	374.5
+33			10.2	376.4
0+40			7.3	379.3
0+60			4.3	382.3
0+80			1.7	384.9
1+00			1.9	384.7
1+20			1.9	384.7
1+40			4.0	382.6
1+55			6.0	380.6
1+60			6.0	380.6
1+80			4.9	381.7
2+00			3.7	382.9
2+10			2.9	383.7

Sta "B"

0+00			13.3	373.3
0+20	Toe slope		11.2	375.4
0+40			3.7	382.9
0+50			2.1	384.5
0+60			1.8	384.8
0+80			1.6	385.0
1+00			4.1	382.5
1+20			3.6	383.0
1+40			2.0	384.6
1+60	Toe slope		5.9	380.7
1+80			4.6	382.0
2+00			3.6	383.0
2+10			2.9	383.7

	water line		9.7	376.9

Sta "C"

0+00		386.6	12.5	374.1
0+08	Toe slope		11.0	375.6
0+20			4.3	382.3
0+25			1.8	384.8
0+30			2.5	384.1
0+38			7.8	378.8
0+50			9.8	376.8
0+54			9.8	376.8
0+60			10.6	376.0
0+80			11.1	375.5
1+00			11.5	375.1
1+20			10.8	375.8
1+25	Toe slope		10.6	376.0
1+32			8.0	378.6
1+40			6.2	380.4
1+51	Top bank		2.0	384.6
1+60			3.6	383.0
1+72	Toe slope		5.1	381.5
1+80			4.8	381.8
2+00			3.4	383.2
2+10			2.9	383.7

Sta "D"

0+00	Toe slope		11.6	375.0
0+05			10.2	376.4
0+20			1.5	385.1
0+32			0.7	385.9
0+40			9.8	376.8
0+52			14.0	372.6
0+54			14.8	371.8
0+60			16.2	370.4

Sta "E"

0+00	386.58	11.3	375.3
0+02		10.8	375.8
0+20		1.5	385.1
0+32		7.5	379.1
0+40	water level	9.7	376.9

Sta "F"

0+00		10.9	375.7
0+03		10.3	376.3
0+20		1.4	385.2
0+32		7.0	379.6
0+40	water edge	9.7	376.9

Sta "G"

0+00		10.8	375.8
0+02		10.2	376.4
0+20		1.7	384.9
0+32		7.4	379.2
0+		9.7	376.9

Sta "H"

0+00		11.2	375.4
0+07		9.8	376.8
0+20		3.2	383.4
0+25		1.9	384.7
0+37		7.2	379.4
0+45	water edge	9.7	376.9

Sta "I"

0+00	386.6	11.2	375.4
0+20		8.5	378.1
0+25		8.5	378.1
0+40		3.5	383.1
0+45		2.3	384.3
0+60		2.2	384.4
0+80		3.1	383.5
1+00		4.0	382.6
1+20		4.1	382.5
1+40		3.6	383.0
1+60		1.9	384.7
1+75		5.2	381.4
1+80		5.3	381.3
2+00		4.4	382.2
2+09		3.9	382.7

Line between H & I. dist = 15' E of sta. I at 0+60
" = 10 E " " I at 1+20

0+60	4' E to water edge	8.0	378.6
0+80	3.5' E " "	8.0	378.6
1+00	5.2 " " "	7.8	378.8
1+20	6.0 " " "	7.2	379.4
1+40	6.2 " " "	7.0	379.6

I line 0+60 to 9' W. I line at 2+09 = Top bank

0+60	I line	386.6	2.0	384.6
0+80			2.1	384.5
1+00			2.2	384.4
1+20			2.4	384.2
1+40			2.7	383.9
1+60			4.8	381.8
1+68	Toe slope		5.5	381.1
1+80			5.2	381.4
2+00			4.5	382.1
2+10			4.1	382.5

4' E of J line = Toe slope

0+00	10.6	376.0
0+20	10.4	376.2
0+40	9.2	377.4
0+60	7.7	378.9
0+80	7.2	379.4
1+00	6.9	379.7
1+20	6.3	380.3
1+40	5.7	380.9
1+60	6.0	380.6
1+80	5.4	381.2
2+00	4.6	382.0
2+10	4.3	382.3

J Line

0+00		386.6	10.6	376.0
0+20			10.3	376.3
0+40			9.7	376.9
0+60			8.5	378.1
0+80			7.9	378.7
1+00			7.7	378.9
1+20			7.0	379.6
1+40			6.6	380.0
1+60			6.2	380.4
1+80			5.5	381.1
2+00			4.7	381.9
2+09			4.4	382.2

H

2+10	3.6	383.0
2+00	4.1	382.5
1+80	3.9	382.7
1+72	1.5	385.1
1+60	5.4	381.2
1+50	9.4	377.2

G

2+10	3.4	383.2
2+00	4.0	382.6
1+80	3.5	383.1

1+74	386.6	1.6	385.0
1+60		6.9	379.7
1+54		9.5	377.1
	"F"		
2+10		3.1	383.5
2+00		4.1	382.5
1+80		4.2	382.4
1+70		1.7	384.9
1+60		5.9	380.7
1+54		9.5	377.1
	"E"		
2+10		3.0	383.6
2+00		3.9	382.7
1+80		4.6	382.0
1+62		3.8	382.8
1+65		1.7	384.9
1+60		3.9	382.7
1+52		9.5	377.1
	"D"		
2+10		2.8	383.8
2+00		3.6	383.0
1+80		4.7	381.9
1+70		4.3	382.3
1+62		1.7	384.9
1+60		3.2	383.4

1+56	386.6	9.5	377.1
376.9 = Water Level "D"		Distances below water level.	
1+20	376.9	6.7	370.2
1+24		6.2	370.7
1+30		5.0	371.9
1+00		6.8	370.1
0+80		6.6	370.3
	"E" Line		
0+60		6.8	370.1
0+80		6.8	370.1
1+00		6.8	370.1
1+20		6.8	370.1
1+24		6.7	370.2
1+30		6.4	370.5
	"F"		
1+40		5.4	371.5
1+37		6.0	370.9
1+34		6.4	370.5
1+30		6.8	370.1
1+20		6.8	370.1
1+00		6.8	370.1
0+80		6.8	370.1
0+60		6.8	370.1
0+56	Toe.	6.8	370.1
0+53		5.3	371.6

"G"

0+58	376.9	5.6	371.3
0+60		5.6	371.3
0+80		6.9	370.0
1+00		6.8	370.1
1+20		6.8	370.1
1+35		6.0	370.9
1+39		5.5	371.4

"H"

1+38		2.6	374.3
1+17		4.2	372.7
0+98		4.4	372.5
0+80		2.3	374.6
0+60		1.8	375.1

Continued from P 43

					W		C		E	
		210.83								
Cr. Upas					6.2	204.6				
Nl. "					8.9	201.9				
50					12.4	198.4				
100					15.4	195.4	6.5	204.3		
150					16.8	194.0	9.6	201.2		
200					17.9	193.4	7.4	203.4		
250							7.9	202.9		
300 = Sl. Vine							9.0	201.8		
Cr. "							12.1	198.7	2.0	208.8
Nl. "							15.8	195.0	5.7	205.1
TP	0.10	203.07	7.86	202.97						
250 N of Upas					10.1	193.				
300 = Sl. Vine					9.7	193.4				
Cr. "					12.2	190.9				
Nl. "					16.4	186.7				
25' N.							14.0	189.1	3.1	200.0
50' "									8.2	194.9
TP	0.55	190.91	12.71	190.36						
25' N					7.9	183.0				
50' N					13.1	177.8	8.5	182.1		
75 N							16.0	174.9	2.2	188.7
100									8.8	182.1
125									12.8	178.1
TP	0.21	178.31	12.81	178.10						

					W		C		E	
		178.31								
75 N of Vine					5.8	172.5				
100					11.1	167.2	9.0	169.3		
125							12.4	165.9		
150							16.1	162.2	7.1	171.2
T.P.	0.43	165.80	12.94	165.37						
125					9.5	156.3				
150					17.8	148.0				
175							9.6	156.2	3.4	162.4
200									13.3	152.5
TP	0.40	153.97	12.83	152.97						
175					13.6	139.8				
200							7.1	146.3		
225									2.4	151.0
250									5.0	148.4
275									7.2	146.2
285									7.3	146.1
300 = SL W flow									3.8	149.6
C "									6.5	146.9
C +25									11.6	141.8
NL "									11.6	141.8
T.P.	1.28	142.22	12.43	140.94						
200					9.0	133.2				
225					11.9	130.3	5.8	136.4		
250					12.2	130.0	7.1	135.1		

		142.22			
275					
300 = SL Willow					
Cr	"				
Cr + 10					
N.L	"				
T.P.	12.85	154.64	0.43	141.79	
"	5.07	158.56	1.15	153.49	
Chuck (Magpie)			3.00	155.56	156.44

by Levels on Willow Starting from Wash. and Goldfinch

	0.81	157.67		156.86
	5.03	150.57	12.13	145.54
25' N of Willow				
50				
75				
T.P.	12.07	157.61	5.03	145.54
100				
105.8 = PL. on West				
	0.39	145.93	12.07	145.54
	1.19	134.75	12.37	133.56
	0.30	122.07	12.98	121.77
	0.37	109.75	12.69	109.38
	0.63	97.52	12.86	96.89
	0.85	86.87	11.50	86.02

W		C		E
9.7	132.5	3.6	138.6	
8.5	133.7	1.6	140.6	
9.8	132.4	2.7	139.5	
7.0	135.2			
7.3	134.9	3.9	138.3	

This BM is 155.65 Taken From India and Vine

(East L of Union intersects PL about 13' S. of N.L. Willow)

12.7	137.9	9.4	141.2
11.3	139.3	7.8	142.8
7.0	143.6		
5.7	151.9		
3.4	154.2		

86.87
5.56
81.31
6.65
87.96
5.58
82.38

74.47
5.56
80.03
5.58
85.61
10.38
75.23
157.61
82.38

3.73
6.65
10.38

5/17/09 Hatch Moore Thomas

Profile State St.

Redwood - North

W C E 61

BM	12.98	109.09		96.11	RR Spk. NW. India Bay Redwood.					
	12.795	121.59	0.295	108.795						
	13.09	134.44	0.24	121.35						
	12.68	146.82	0.30	134.14						
	12.80	159.215	0.405	146.415						
	12.895	171.805	0.305	158.91						
	13.04	184.46	0.385	171.42						
	9.28	192.40	1.34	183.12						
N.L. Redwood					12.1	180.3	6.9	185.5	1.4	191.0
25' N.					16.8	175.6	11.7	180.7	5.1	187.3
50									12.0	180.4
TP	0.245	179.575	13.07	179.33						
50					11.4	168.2	5.9	173.7		
75							12.0	167.6	7.4	172.2
TP	0.22	166.965	12.83	166.745						
75					7.4	159.6				
100					6.6	160.4	9.4	157.6	4.5	162.5
125									11.4	155.6
TP	0.21	154.191	12.985	153.98						
125					12.4	141.8	3.9	150.3		
150							11.7	142.5	7.4	146.8
175									13.2	141.0
TP	0.585	141.685	13.09	141.10						
150					5.0	136.7				

POSTED

					W		C		E	
		141.685								
175					15.2	126.5	5.3	136.4		
200									10.0	131.7
TP	0.165	129.065	12.785	128.900						
300					10.2	118.9	2.8	126.3		
225					20.7	108.4	13.2	115.9	5.8	123.3
TP	0.07	116.21	12.925	116.14						
250							9.6	106.6	2.6	113.6
275									11.7	104.5
TP	0.305	103.70	12.815	103.395						
250					4.9	98.8				
275					11.8	91.9	6.4	97.3		
300 = Sh Spruce					14.0	× 89.7	9.1	94.6	3.4	100.3
Cr	"				8.4	95.3	10.1	93.6	6.4	97.3
Nh.	"						4.4	99.3	4.4	99.3
25'									0.5	103.2
TP	12.85	116.39	0.16	103.54						
Nh.					10.0	106.4				
25					0.0	116.4	11.5	104.6		
50							2.1	114.3	8.8	107.6
75									3.3	113.1
TP	12.76	128.865	0.285	116.105						
50					4.9	124.0				
75							5.3	123.6		
100									6.6	122.3

5/15/09				
		128.565		
T.P.	13.01	141.195	0.68	128.185
75				
100				
125				
150				
T.P.	12.985	153.96	0.22	140.975
125				
150				
175				
200				
T.P.	12.515	166.28	0.195	153.765
150				
175				
T.P.	12.44	178.08	0.64	165.64
200				
225				
250				
275				
T.P.	3.85	180.85	1.25	176.83
275				
300 =	Sh. Sassafras			
Cr		"		
Nh		"		
25' N				

checked to here

W		C		E	
9.6	131.6				
3.8	137.4	11.2	130.0		
		5.5	135.7	9.3	131.9
				2.9	138.3
9.1	144.9				
		11.4	142.6		
		2.2	151.8	9.2	144.8
				2.9	151.1
12.0	154.3				
3.2	163.1				
9.8	168.3	11.9	166.2		
6.2	171.9	5.4	172.7	12.1	166.0
3.5	174.6	2.0	176.1	4.7	173.4
2.9	175.2			1.4	176.7
		2.5	178.2		
1.2	173.5	2.6	178.1	1.2	179.5
12.2	168.5	5.3	175.4	0.8	179.9
		10.8	169.9	2.0	178.7
		12.4	168.3	3.5	177.2

	+		−	
		180.68		
50				
75				
100				
125				
150				
175				
200				
225				
250				
T.P.	0.035	167.795	12.92	167.76
N.L. Sassafras				
25				
30				
32				
50				
60				
75				
100				
125				
150				
175				
200				
T.P.	1.16	158.67	10.285	157.51
75				
100				
125				

W		C		E	
				7.0	173.7
				9.4	171.3
				12.6	168.1
				10.5	170.2
				10.5	170.2
				8.7	172.0
				9.2	171.5
				7.0	173.7
				0.9	179.8
7.1	160.7				
9.6	158.2				
9.9	157.9				
13.1	154.7				
12.1	155.7	1.9	165.9		
		5.8	162.0		
		6.8	161.0		
		8.7	159.1		
		10.1	157.7		
		9.6	158.2		
		9.9	157.9		
		7.2	160.6		
7.9	150.8				
9.7	149.0				
12.6	146.1				

		158.67		
150				
175				
TP	13.035	170.545	1.6	157.51
200				
T.P.	12.95	183.52	0.005	170.54
225				
250				
275				
T.P.	12.92	196.39	0.05	183.47
300 = SL	Thorn			
Cr	"			
NL	"			
50				
T.P.	6.225	200.19	2.425	193.965
50				
100				
150				
200				
T.P.	0.47	187.655	13.005	187.185
200				
250				
T.P.	0.165	175.72	12.10	175.555
300 = SL	Upas.			
Cr.				

W		C		E	
14.9	143.8				
7.9	150.8				
8.0	162.5				
12.0	171.5	9.4	174.1		
4.8	178.7	3.9	179.6		
2.8	180.7	1.9	181.6	0.2	183.3
13.7	182.7	12.7	183.7	11.0	185.4
11.2	185.2	9.29	Thorn 187.1	6.0	190.4
8.1	188.3	4.6	191.8	0.7	195.7
5.6	190.8				
		1.6	195.6	1.2	199.0
9.4	190.8	4.7	195.5	1.1	199.1
14.2	186.0	8.4	191.8	4.4	195.8
		13.5	186.7	9.8	190.4
6.3	181.4				
13.4	174.3	8.5	179.2	3.7	184.0
15.2	160.5	9.0	166.7	2.2	173.5
				8.0	167.7

		175.72		
T.P.	0.02	162.95	12.79	162.93
Cr				
Nl. Upas				
25				
50				
75				
100				
125				
150				
T.P.	0.63	150.52	13.06	149.89
Nl. Upas				
10				
25				
50				
75				
100				
110				
115				
125				
150				
175				
200				
204				
T.P.	11.485	160.74	12.65	149.255

W		C		E	
			Mon.		
10.6	157.4	3.8	159.2		
		8.8	154.2	1.3	161.7
		10.2	152.8	2.6	160.4
		13.3	149.7	3.6	159.4
		12.0	151.0	3.1	159.9
		8.8	154.2	2.7	160.3
		10.9	152.1	3.4	159.6
				8.5	154.5
5.4	145.1				
6.2	144.3				
13.0	137.5				
14.9	135.6				
8.4	142.1				
5.2	145.3				
9.0	141.5				
13.0	137.5				
21.2	129.3				
20.6	129.9	8.0	142.5		
16.1	134.4	13.4	137.1	5.2	145.3
4.2	146.3	10.6	139.9	7.8	142.7
				{4.8	{145.7
		7.0	143.5	{1.4	{148.1

			160.74						
225									
235									
250									
275									
300 = Sh. Vine									
T.P.	0.21	147.91	13.04	147.70					
Cr.	"								
T.P.	0.57	136.645	11.835	136.075					
Sh.	Vine								
25 W									
50									
75									
100									
T.P.	0.175	124.050	12.77	123.875					
25									
50									
75									
100									
125									
150									
T.P.	5.88	117.26	12.67	111.38					
90									
125									
150									

W		C		E	
9.8	150.9	10.5	150.2	8.2	152.5
				2.1	158.6
9.0	151.7	4.9	155.8	0.3	160.4
10.1	150.6	6.0	154.7	2.2	158.5
12.9	147.8	10.1	150.6	5.6	155.1
10.9	137.0	8.0	mon. 139.9	7.6	140.3
16.6	120.0	15.2	121.4	3.4	133.2
		14.5	122.1	1.7	134.9
		10.9	125.7	0.2	136.4
		12.4	124.2	2.4	134.2
				9.7	126.9
13.5	110.6				
10.4	113.7				
11.5	112.6				
		7.0	117.1		
				5.2	118.9
				13.3	110.8
9.1	108.2				
16.7	100.6				
16.8	100.5	9.8	107.5		
15.5	101.8	12.7	104.6		

					W		C		E	
		117.26								
175					12.9	104.4	11.6	105.7	12.0	105.3
200					9.0	108.3	8.2	109.1	10.4	106.9
225					3.2	114.1	4.8	112.5	7.4	109.9
250							2.7	114.6		
T.P.	12.76	129.65	0.37	116.89						
250					6.4	123.3			16.0	113.7
275					0.0	129.7	12.1	117.6	11.5	118.2
290							10.7	119.0		
300 = Sh. Willow							4.5	125.2	6.6	123.1
12' N of SL							0.7	129.0		
30' " " "									4.8	124.9
Cr "									0.6	129.1
T.P.	12.725	142.205	0.17	129.48						
300 = Sh. Willow					3.2	139.0				
15							5.3	136.9		
Cr + 08							8.5	133.7		
" +10							2.3	139.9		
T.P.	12.66	154.57	0.295	141.91				Mon.		
Cr.					3.6	151.0	9.17	145.5		
Nh Willow									5.2	149.4
T.P.	9.30	163.51	0.06	154.21						
Check			8.02	155.49						
Nh. Willow										
25					5.2	158.3	9.0	154.5		
					3.4	160.1	5.6	157.9	9.2	154.3

					W		C		E	
5/28 29	Hatch Moore Thomas	163.57								
50					3.8	159.7	5.2	158.3	6.9	156.6
75					6.2	157.3	6.9	156.6	7.1	156.4
100					10.0	153.5	9.7	153.8	9.5	154.0
125					14.2	149.3	13.2	150.3	12.4	151.1
T.P.	0.24	151.02	12.73	150.78						
150					6.5	144.5	5.5	145.5	2.4	148.6
175					12.6	138.4	10.8	140.2	5.6	145.4
200									7.8	143.2
225									9.4	141.6
250									11.4	139.6
T.P.	0.67	139.44	12.25	138.77						
200					9.6	129.8	5.3	134.1		
225					16.5	122.9	8.1	131.3		
250							10.6	128.8		
275							12.9	126.5	3.7	135.7
300 = Sh. Chalmers									9.0	130.4
T.P.	0.22	126.94	12.72	126.72						
250					7.1	119.8				
275					9.5	117.4				
300 Sh.					12.6	114.3	5.4	121.5		
Cr. "									6.2	120.7
20' N of Cr.									6.4	120.5
T.P.	3.45	117.64	12.75	114.19						
Cr.					12.	105.6	7.9	109.7		

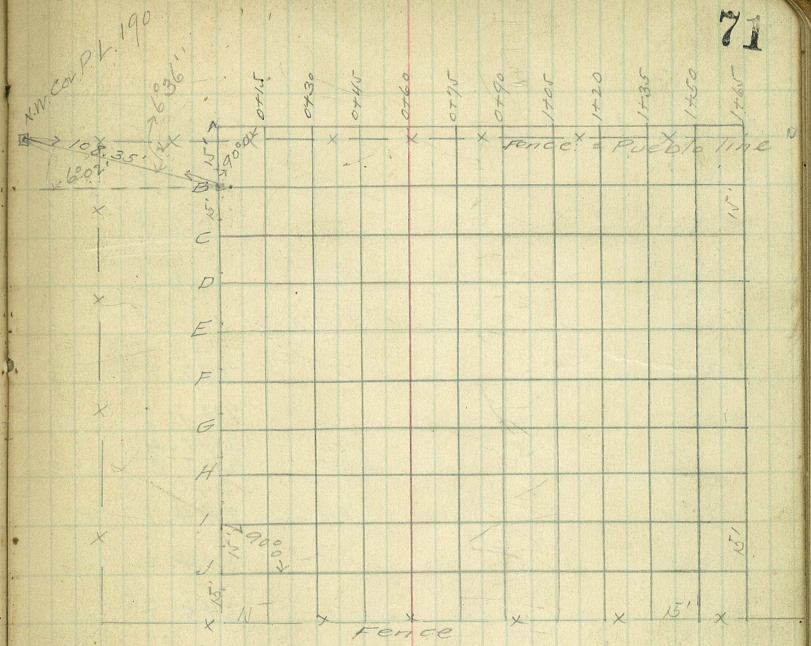
		117.64		
Cr + 20				
" + 30				
Mt. Chalmers				
23° N.				
42.5 = Pl. on East.				
T.P.	12.89	130.23	0.30	117.34
42.5				
75				
T.P.	12.77	142.76	0.24	129.99
100 = Pl. on Cr.				
T.P.	8.88	151.51	0.13	142.63
125				
158 = Pl. on West.				

W		C		E	
13.4	104.2				
17.0	100.6				
12.1	105.5	9.0	106.6	5.1	112.5
3.2	114.4	11.7	105.9	7.2	110.4
		4.3	113.3	4.2	113.4
12.2	118.0				
2.6	127.6	4.7	125.5		
6.1	136.7	6.8	136.0		
8.5	143.0				
23	149.2				

	+	H.I.		B.M.
	2.49	255.48		252.99
	1.61	245.49	11.60	243.88
Sta.		"A"		
A 0+00			3.1	242.4
A 0+15			3.9	241.6
A 0+30			5.0	240.5
A 0+45			5.2	240.3
A 0+60			6.7	238.8
A 0+75			7.5	238.0
A 0+90			8.5	237.0
A 1+05			8.9	236.6
A 1+20			10.1	236.4
A 1+35			11.5	234.0
A 1+50			12.9	232.6
A 1+65			15.2	230.3

"A" + 05' Toe slope N. side

0+00			2.9	242.6
0+15			4.1	241.4
0+30			5.1	240.4
0+45			5.7	239.8
0+60			6.2	239.3
0+75			7.2	238.3
0+90			8.0	237.5
1+05			8.4	237.1



x sec. taken every 15' apart

Posted

245.49 H.I.
10.15
235.34
8.37
H.I. 243.71

See other pages in this book.

245.49

1+20		10.1	235.4
1+35		11.4	234.1
1+50		13.1	232.4
1+65		15.5	230.0

"B" = top of bank N. side.

0+00		2.7	242.8
0+15		3.6	241.9
0+25		4.1	241.4
0+30		3.0	242.5
0+35	Top bank	1.5	244.0
0+45		1.4	244.1
0+60		1.5	244.0
0+75		1.7	243.8
0+90		2.0	243.5
1+05		2.4	243.1
1+10		2.8	242.7
1+20		5.6	239.9
1+35		11.3	234.2
1+50		13.5	232.0
1+65		15.5	230.0

"C"

0+00	245.49	2.4	243.1
0+15		2.4	243.1
0+20	Top of bank.	1.4	244.1
0+30		3.5	242.0
0+45		6.8	238.7
0+60		8.1	237.4

41

245.49

0+75		8.0	237.5
0+90		7.5	238.0
1+05		7.5	238.0
1+20		4.8	240.7
1+25	Top bank	2.5	243.0
1+35		7.1	238.4
1+50		14.1	231.4
1+65		15.5	230.0

"D" Line

0+00	245.49	1.4	244.1
0+15	Top bank	1.4	244.1
1+30		5.8	239.7
1+38		10.7	234.8
1+45		10.4	235.1
1+60		10.3	235.2
1+75		10.2	235.3
1+90		10.5	235.0
1+65		10.6	234.9
1+20		8.2	237.3
1+28	Top bank. 41	0.7	243.0
1+35	243.71	3.0	240.7
1+50		10.7	233.0
1+53	toe slope	12.7	231.0
1+65		15.2	228.5

"E"

0+00	245.49?	0.6	244.9	243.1
0+15	Top bank	1.2	244.3	242.5
0+20		1.7	243.8	242.0
0+30		6.1	239.4	237.6
0+45		9.8	235.7	233.9

0+60		245.49	10.2	235.3	
0+75			10.5	235.0	
0+90			10.3	235.2	
1+05			10.3	235.2	
1+20			7.8	237.7	
+28	Top bank		0.6	243.1	
1+35		243.71	3.3	240.4	
1+50			11.3	232.4	
+53	toe slope		13.5	230.2	
1+65			15.3	228.4	
		"F" Line			
0+00		245.49 ?	0.1	243.6	244.5
0+15	Top bank.		1.0	242.7	244.5
+20			1.7	242.0	243.8
0+30			5.8	237.9	239.7
+45			9.4	234.3	236.1
+60			9.9	233.8	235.6
+75			9.9	233.8	235.6
+90			10.3	233.4	235.2
1+05			10.1	233.6	235.4
+20			7.3	236.4	238.2
+28	Top bank.		0.4	243.3	[illegible]
+35		243.71	2.3	241.4	[illegible]
+50			10.0	233.7	[illegible]
+52	toe slope		11.5	232.2	[illegible]
1+65			14.1	229.6	[illegible]
		"G" Line			
0+00		245.49	0.4	245.1	243.3
0+15			0.7	244.8	243.0
+18			1.0	244.5	242.1
0+30			5.5	240.0	[illegible]

0+45	245.49	9.0	236.5
+60		9.8	235.7
+75		9.6	235.9
+90		9.9	235.6
1+05		9.8	235.7
+20		6.0	239.5
+28 Top bank.		0.2	243.5
+35	243.71	3.4	240.3
+50		11.8	231.9
+65		13.0	230.7
	"H" Line		
0+00	245.49	0.3	245.2
+15		1.2	244.3
+21 Top bank.		0.8	244.7
+30		2.9	242.6
+45		5.0	240.5
+60		5.6	239.9
+75		5.6	239.9
+90		5.8	239.7
1+05 toe slope		5.9	239.6
+18 top bank		1.9	243.6
1+20		2.8	242.7
1+35		9.4	236.1
+45 toe slope		12.8	232.7
1+50		13.5	232.0
1+65		14.6	230.9
	"H" + 0.9 = Top bank S. side		
0+00		0.2	245.3
0+15		1.2	244.3

0+30	245.49	1.4	244.1
0+45		2.4	243.1
0+60		1.6	243.9
0+75		1.3	244.2
0+90		1.4	244.1
1+05		2.4	243.1
+20		6.8	238.7
+30		10.9	234.6
+35		11.9	233.6
+50		13.2	232.3
+65		14.3	231.2

I Line = Toeslope

0+00		0.1	245.4
0+15		1.1	244.4
0+30		1.9	243.6
0+45		2.9	242.6
0+60		3.5	242.0
0+75		4.0	241.5
0+90		5.0	240.5
1+05		6.5	239.0
+20		9.0	236.5
+35		12.0	233.5
+50		12.9	232.6
+65		13.9	231.6

"J" Line

0+00		-0.1	245.6
0+15	245.49	0.6	244.9
+30		2.0	243.5
+45		2.7	242.8
+60		3.8	241.7
+75		5.2	240.3
+90		6.8	238.7
1+05		8.1	237.4
1+20		9.0	236.5
+35		10.6	234.9
+50		12.4	233.1
+65		14.2	231.3

$\frac{1}{2-3}$ 09 { Dams
Churchman
Wallace

252.99 B.M. Spk pole 25' So of S.W. Cor of fence around reservoir
3.14
256.13 H.I.
10.64
245.49 TP X
0.37
245.86 H.I.

344.50 = Top wall

341.00 = Top slope

335.00 = Top floor

334.66 = Sub grade

245.49
4.2
245.91 H.I.

234.66 / 11.20   241.0 / 4.86   244.50 / 1.36

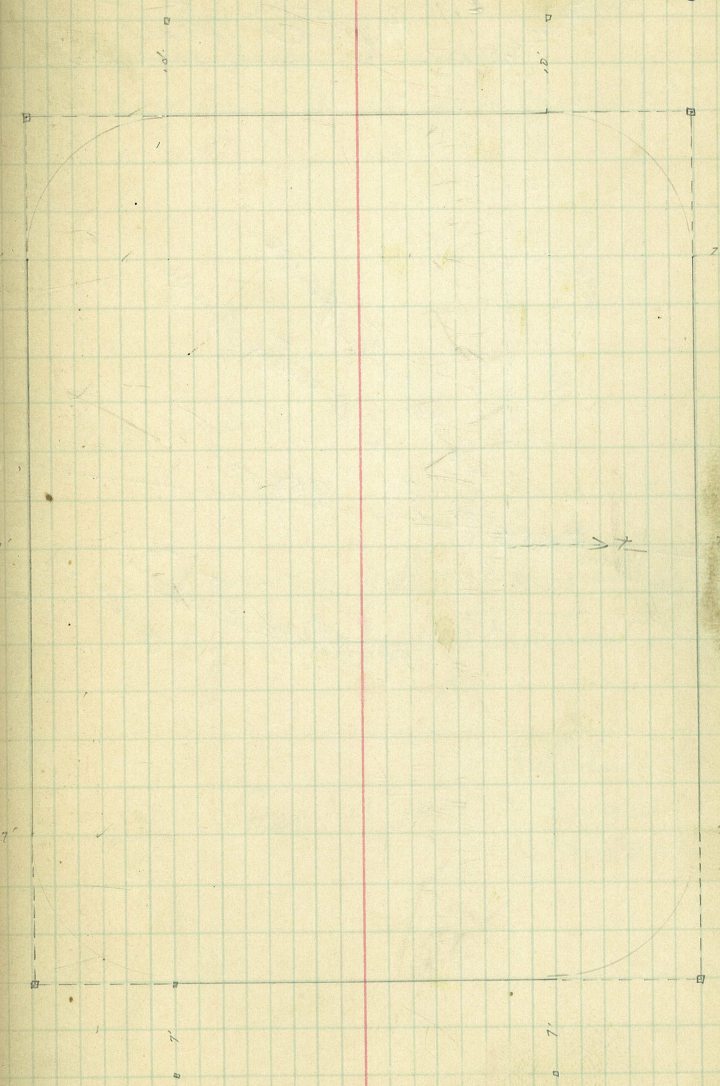
244.50 / 1.41   241.00 / 4.91   234.66 / 11.25   9.11 / 2.14   10.05 / 1.20

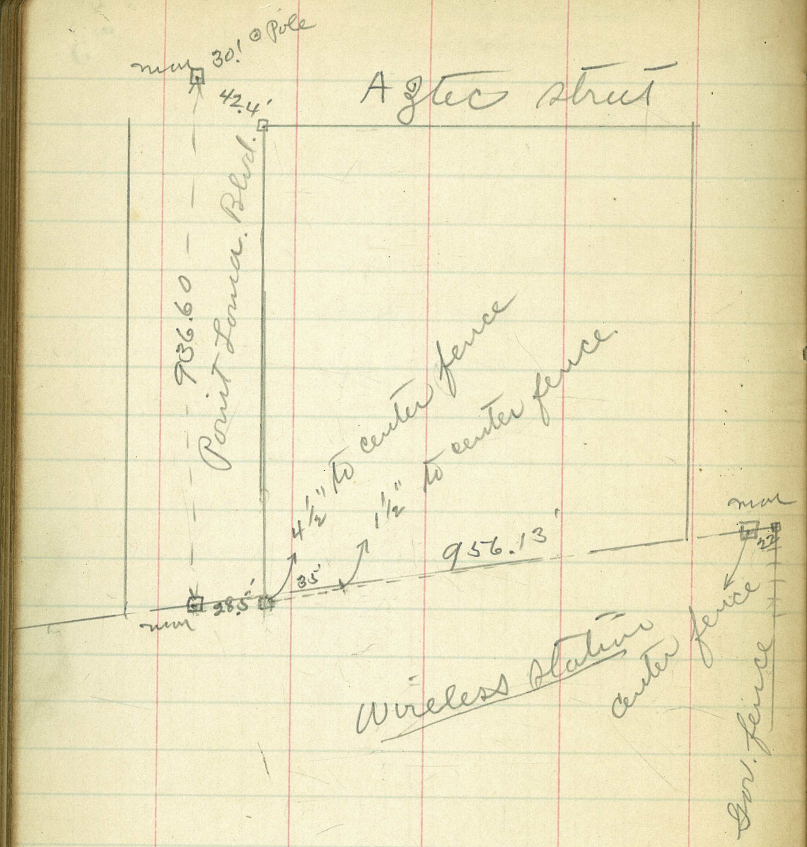
9.62 / 1.63   10.64 / 0.61   10.36 / 0.89   10.20 / 1.05   9.94 / 1.31   10.54 / 0.71   9.89 / 1.36

241.00 / 4.91

245.49 H.I.   334.66 / 10.83   235.00 / 10.49

Point Loma Reservoir Ties



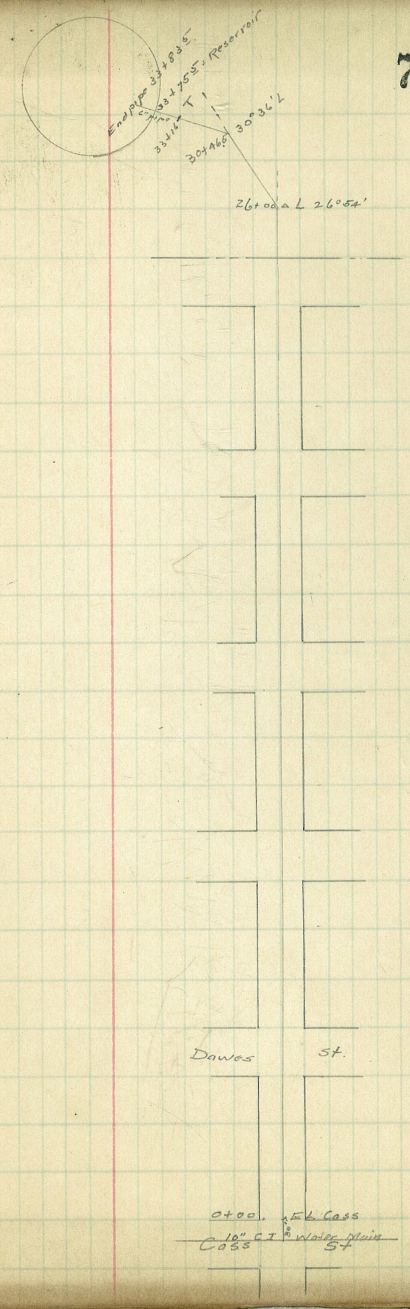


Reservation line

note – Fence posts 6" wide
corner posts 8" wide
overhang is 1.5' from north edge
of post.

Survey of Government fence
by wireless station.

Feb. 15, 1917 { Childs
Evans
Moore


End pipe 33+83.5
33+75.5 = Reservoir
33+16
30+46.5
30°36' L
26+00 ∆ L 26°54'
Dawes St.
0+00 Eb. Cass
10" C.I. Water Main
Cass St

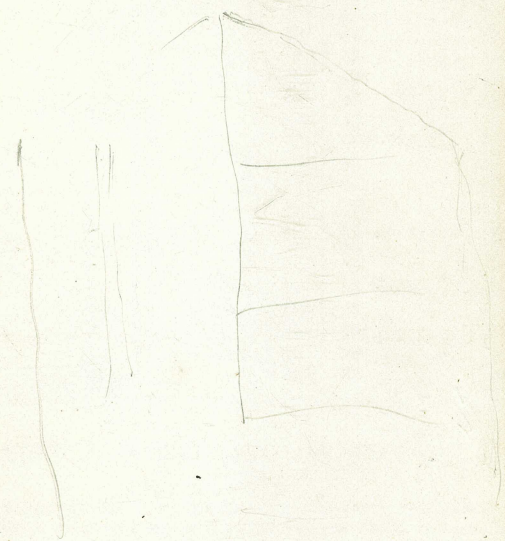


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Table showing the difference of latitude and departure in running 80 chains at any course from 1 to 60 minutes.

MINUTES.	LKS.	MINUTES.	LKS.	MINUTES.	LKS.
1	$2\frac{1}{3}$	21	49	41	$95\frac{2}{3}$
2	$4\frac{2}{3}$	22	$51\frac{1}{3}$	42	98
3	7	23	$53\frac{2}{3}$	43	$100\frac{1}{3}$
4	$9\frac{1}{3}$	24	56	44	$102\frac{2}{3}$
5	$11\frac{2}{3}$	25	$58\frac{1}{3}$	45	105
6	14	26	$60\frac{2}{3}$	46	$107\frac{1}{3}$
7	$16\frac{1}{3}$	27	63	47	$109\frac{2}{3}$
8	$18\frac{2}{3}$	28	$65\frac{1}{3}$	48	112
9	21	29	$67\frac{2}{3}$	49	$114\frac{1}{3}$
10	$23\frac{1}{3}$	30	70	50	$116\frac{2}{3}$
11	$25\frac{2}{3}$	31	$72\frac{1}{3}$	51	119
12	28	32	$74\frac{2}{3}$	52	$121\frac{1}{3}$
13	$30\frac{1}{3}$	33	77	53	$123\frac{2}{3}$
14	$32\frac{2}{3}$	34	$79\frac{1}{3}$	54	126
15	35	35	$81\frac{2}{3}$	55	$128\frac{1}{3}$
16	$37\frac{1}{3}$	36	84	56	$130\frac{1}{3}$
17	$39\frac{2}{3}$	37	$86\frac{1}{3}$	57	133
18	42	38	$88\frac{2}{3}$	58	$135\frac{1}{3}$
19	$44\frac{1}{3}$	39	91	59	$137\frac{2}{3}$
20	$46\frac{2}{3}$	40	$93\frac{1}{3}$	60	140

TABLE FOR RUNNING ON SLOPES.

In the following table the first column shows the angle, the second the number of links to be added to a chain on the slopes, to make one chain, horizontal measurement.

ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS
°		°		°		°	
4	0.24	11	1.88	18	5.14	25	10.54
5	0.38	12	2.24	19	5.76	26	11.26
6	0.55	13	2.63	20	6.42	27	12.24
7	0.76	14	3.06	21	7.11	28	13.37
8	0.98	15	3.53	22	7.85	29	14.34
9	1.24	16	4.02	23	8.64	30	15.47
10	1.55	17	4.56	24	9.47	35	22.07