Preliminary Sewers.

393

Engineer's Office
City Hall, San Diego, Cal.

Chollas Valley.

400

LEVEL

F.B. IND 393

Published by H. S. CROCKER COMPANY, Stationers, Drawing Materials, and Mathematical Instruments, San Francisco.

Table showing the difference of latitude and departure in running 80 chains at any course from 1 to 60 minutes.

MINUTES.	LKS.	MINUTES.	LKS.	MINUTES.	LKS.
1	2⅓	21	49	41	95⅔
2	4⅔	22	51⅓	42	98
3	7	23	53⅔	43	100⅓
4	9⅓	24	56	44	102⅔
5	11⅔	25	58⅓	45	105
6	14	26	60⅔	46	107⅓
7	16⅓	27	63	47	109⅔
8	18⅔	28	65⅓	48	112
9	21	29	67⅔	49	114⅓
10	23⅓	30	70	50	116⅔
11	25⅔	31	72⅓	51	119
12	28	32	74⅔	52	121⅓
13	30⅓	33	77	53	123⅔
14	32⅔	34	79⅓	54	126
15	35	35	81⅔	55	128⅓
16	37⅓	36	84	56	130⅓
17	39⅔	37	86⅓	57	133
18	42	38	88⅔	58	135⅓
19	44⅓	39	91	59	137⅔
20	46⅔	40	93⅓	60	140

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TABLE FOR RUNNING ON SLOPES.

In the following table the first column shows the angle, the second the number of links to be added to a chain on the slopes, to make one chain, horizontal measurement.

ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS
°		°		°		°	
4	0.24	11	1.88	18	5.14	25	10.54
5	0.38	12	2.24	19	5.76	26	11.26
6	0.55	13	2.63	20	6.42	27	12.24
7	0.76	14	3.06	21	7.11	28	13.37
8	0.98	15	3.53	22	7.85	29	14.34
9	1.24	16	4.02	23	8.64	30	15.47
10	1.55	17	4.56	24	9.47	35	22.07

Crocker Quality

LEVEL BOOK

No. 400

MANUFACTURED BY

A. S. Crocker Co.

SAN FRANCISCO
and
SACRAMENTO

1/50 Halsh
10 Thomas

Public Square in Valley Entrance 2

Logan, Ut. Valley.

0+00 = 50' W of 2nd

1

	6.72	78.20		71.48	BM 3rd E. of National
0+02			10.9	67.3	
TP	0.26	65.78	12.65	65.52	
+50'	+ W.L. 3rd E		3.6	62.2	
+80'			4.8	61.0	
1+10 = 0+00 E.L.			8.6	57.2	
+50			11.2	54.6	
1			12.9	52.9	
TP	1.37	53.78	12.37	53.41	
+50			1.7	52.1	
2			3.2	50.6	
+50			4.6	49.2	
+75			5.6	48.2	
3			6.0	47.8	
+25			6.6	47.2	
+50			7.9	45.9	
+75			9.9	43.9	

Profile Started

Note, Line is ℄ of Alley to Sta 5+78 Then Jogs 12.5

		53.78		
4			12.4	41.4
T.P.	0.12	41.32	12.58	41.20
+50			6.6	34.7
+75			8.6	32.7
5			9.2	32.1
			9.0	32.3
+30			7.6	33.7
+50			6.0	35.3
	South		4.1	36.2
+78	North		5.9	35.4
+98			6.7	34.6
6+04			0.6	40.7
T.P.	1.72	42.43	0.62	40.70
+50			2.5	39.9
7			2.5	39.9
+25			4.5	37.9
+50			4.1	38.3
+65			3.3	39.1
+75			4.9	37.5

North and Follows P.L.

		42.43		
5			5.3	37.1
+20			5.3	37.1
+40			11.4	31.0
T.P.	0.25	30.27	12.41	30.02
+65			5.8	24.5
T.P.	0.25	17.44	12.38	17.39
9			1.3	16.1
+10			5.1	12.3
+35			6.0	11.4
+65			5.5	11.9
10			7.0	10.4
+50			7.8	9.6
+75			9.7	7.7
11			12.1	5.3
+50			11.6	5.8
+78			11.5	5.9
			12.7	4.7
12			14.8	2.6
$+28^{5} = 49+50^{5}$ Front Line.			16.3	1.1

on P.T. on last point

1/26/10 Hatch Moore Thomas

Line in Alley bet Ninth & Greeley from 30th to 23rd.

B.M.	8.96	79.87		70.91	NW Brass Logan-30th
T.P. Spk in Pole Home at Greeley	1.91	75.79	5.99	73.88	
0+00 = El 30th			1.8	74.0	
+50			4.3	71.5	
1			6.4	69.4	
+50			9.2	66.6	
2			11.2	64.6	
T.P.	0.15	63.36	12.58	63.21	
+50			0.8	62.6	
3			4.7	58.7	
+50			6.2	57.2	
4			7.2	56.2	
+50			7.8	55.6	
+70			7.6	55.8	
5			10.0	53.4	
T.P.	0.31	50.64	10.03	50.33	
+50			1.4	49.2	
+75			3.4	47.2	
		50.64			
6 = W.L. 31st			7.1	43.5	
+30 = C.L. 31st			10.6	40.0	
+60 = E.L. 31st			12.2	38.4	
7			9.6	41.0	
+50			9.1	41.5	
8			9.1	41.5	
+30			9.2	41.4	
+50			10.3	40.3	
T.P.	2.14	37.90	12.98	37.76	
9			1.0	36.9	
+10			1.7	36.2	
+35			5.3	32.6	
+45			7.5	30.4	
+55			13.9	24.0	
T.P.	1.63	26.58	12.95	24.95	
+625 ℄ R.R. Track			1.5	25.1	
+70			3.2	23.4	

Profile plotted

		26.58		
10			8.1	18.5
+60			10.4	16.2
+55			12.7	13.9
+65			8.6	18.0
+85			5.5	21.1
11			4.6	22.0
+25			3.9	22.7
+50			1.4	25.2
T.P.	10.52	26.84	0.26	26.32
12			6.1	30.7
+15			3.4	33.4
+50			2.3	34.5
+60 = W.L. 32 ft.			2.0	34.8

Watch 27 Moore to Thomas' Line in alley between Walker & Martin from 30 ft to 32 ft

T.P.	0.84	74.72		73.88
T.P.			4.67	70.05
0+10 = El. 30 ft.			7.4	65.3
+50			11.2	63.5
T.P.	5.03	61.67	13.08	61.64
+75			0.3	61.4
1			4.3	57.4
+15			6.4	55.3
+50			9.4	52.3
+75			10.5	51.2
+80			12.1	49.7
2			11.8	49.9
T.P.	0.33	49.53	12.47	49.20
+50			2.3	47.2
3			4.9	44.6
+30			7.2	42.3
+40			10.9	38.6

Argyle Street

		49.53		
+50			8.8	40.7
+55			11.3	38.2
+70			8.6	40.9
4			9.2	40.3
+40			12.1	37.4
+50			14.6	34.9
+60			16.3	33.2
+65			13.8	35.7
5			12.5	37.0
T.P	0.27	37.37	12.21	37.32
+50			2.9	34.7
+75			4.5	33.1
6	= Wk. 31st		7.3	30.3
+10			7.8	29.8
+30	Ch. 31st		7.6	30.0
+55			9.4	28.2
+60	El. 31st		7.1	30.5

		37.69		
+65			3.7	33.9
474	℄ RR		3.0	34.6
+80			4.2	33.4
+85			8.6	29.0
7			10.4	27.2
+25			15.1	22.5
+30			13.1	24.5
+50			12.9	24.7
8			7.2	30.4
T.P	12.72	49.98	0.34	37.25
+60			11.7	38.3
+75			6.7	43.3
9			2.6	47.4
+50			1.4	48.6
+62			0.2	49.8
T.P	9.98	59.64	0.32	49.66
10			6.8	52.8

		59.64		
+30		3.7	56.9	
+50		2.2	57.4	
11		2.1	57.5	
+50		5.1	54.5	
12		8.5	51.1	
+50		12.8	46.8	
+60 = W.h. 32d		13.5	46.1	

1/27 Hatch to Nagle & Thomas

Line in Alley between Washman-Gay

	Valle	from	30 ft. h	32 d.	
BM.	0.80	91.80		91.00	Nor. NW. Washman-30th
0+00 = Et. 30th			7.2	84.6	
+50			9.9	81.9	
+75			11.7	80.1	
T.P.	0.05	79.19	12.66	79.14	
1			1.9	77.3	
+50			9.0	70.2	
2			12.7	66.5	
T.P.	0.16	66.80	12.55	66.64	
+50			4.9	61.9	
3			8.8	58.0	
+50			10.6	56.2	
+75			9.6	57.2	
4			11.5	55.3	
T.P.	0.15	54.29	12.66	54.14	
+75			1.9	52.4	
+50			5.5	48.8	

Profile started

		54.29		
+75			7.0	47.3
5			10.0	44.8
+20			11.3	43.0
TP	215	43.64	1280	41.49
+50			3.6	40.0
6	WL 2nd		7.4	36.2
+20			7.7	35.9
+25			1.4	42.2
+30	OL 2nd		0.6	43.0
+35			1.6	42.0
+50			9.1	34.5
+60	EL 3rd		10.3	33.3
+95			12.9	30.7
7			14.5	29.1
+10			13.4	30.2
+50			10.5	33.1
8			1.3	42.3

		43.64		
T.P	1222	5557	0.29	43.35
+35			7.1	48.5
+50			5.3	50.3
9	1285	6842	0.0	55.57
+50			7.3	61.1
+75			5.2	63.2
10			3.8	64.6
+50			2.1	66.3
11			1.2	67.2
+50			2.4	66.0
12			4.3	64.1
+50			6.0	62.4
+60			6.2	62.2

Line in Alley between Woodman and Franklin from 30th To 33d.

Hdch 2½ Pkard to Thomas

BM	120	86.24		85.14	Set in Tbl SW Franklin-30th
0+00 = E ℄ 30th			2.0	84.2	
+50			4.5	79.7	
1			7.3	78.9	
+50			11.9	74.3	
T.P.	0.21	73.47	12.98	73.26	
2			2.1	71.4	
+25			3.6	69.9	
+50			7.3	66.2	
+75			11.2	62.3	
3			11.4	62.1	
+50			11.3	62.2	
T.P.	0.09	60.81	12.75	60.72	
4			1.8	59.0	
+50			6.1	54.7	
T.P.	3.80	51.17	12.44	47.37	
5			3.3	45.9	

51.17

+40			11.9	39.3
+85			11.8	39.4
+97			13.7	37.5
6			11.5	39.7
+10			9.4	41.8
+25			1.1	50.1
+30			0.6	50.6
+35			1.2	50.0
+45			7.2	44.0
+55			10.7	40.5
+60 = 0+00			6.5	44.7
7+10 0+50			2.0	49.2
T.P.	9.17	60.16	0.18	50.99
1 7+60			5.0	55.2
+50 8+10			1.8	58.4
2 +60			4.9	55.3
+50 9+10			7.8	51.4

Opened and Tied

		60.6		
+75	+35		10.8	49.4
3	+60		10.2	50.0
+25	+85		7.0	53.2
+50	10+10		3.7	56.5
T.P.	1.202	71.79	0.39	59.77
+75	+35		7.9	63.9
4	+60		6.4	65.7
+50	11+10		5.2	66.6
5	+60		4.9	66.9
+50	12+10		3.5	68.3
6 = Wk. 32d.	+60		2.6	69.2
+30	+90		2.3	69.5
+60 = El. = 0+00	13+20		2.2	69.6
0+50	+70		3.5	68.3
+90	14+10		5.2	66.6
1	+20		6.7	65.1
+25	+45		8.5	63.3

		71.79		
+50	+70		8.8	63.0
2	15+30		5.7	66.1
+25	+45		5.8	66.0
+50	+70		10.8	61.0
T.P.	2.74	62.33	1.20	59.59
+75	+45		8.4	53.9
3	16+30		13.4	48.9
+37	+57 Wk. 33d		19.2	43.1
T.P.	12.66	74.52	0.47	61.86
T.P.	8.88	83.25	0.15	74.37

½ Halidi Point 10 ft. Timbers

Line in Alley between Franklin and Clay from 30th to 33rd Sts.

		8325			
0+00 = W½ 33rd			5.0	78.3	
+50			4.3	79.0	
1			2.7	80.6	
+50			3.5	79.8	
2			5.0	78.3	
+50			5.8	77.5	
3			7.1	76.2	
+39 = E½ 32nd			8.7	74.6	
Cr. "			9.8	73.5	
W½ "			11.0	72.3	
=0+00					
T.P	2.96	76.01	10.20	73.05	
0+50 +89			5.0	71.0	
1+14					
+75			7.6	68.4	
1 4+39			8.5	67.5	
+50 +89			8.8	67.2	
5+14					
+75			7.4	68.6	

Profile started

		76.01			
5+39				8.1	67.9
2 +64					
+25 +89				8.8	67.2
+50				8.6	67.4
3 6+39				7.9	68.6
+50 +89				5.0	71.0
4 7+39				5.0	71.0
+50 +89				5.4	70.6
5 8+39				7.2	68.8
+50 +89				9.0	67.0
6 = 9+39 E½ 31st				9.5	67.2
T.P	1.01	67.35	9.67		66.34
+15 9+54				2.0	65.4
+20 +59				8.3	59.1
Cr. +				7.5	59.9
+38 + 77				7.3	60.1
+45 +84				0.8	66.6
W½ 31st +99 = 0+00				1.0	66.4

		67.35		
0	+50 10+49		6.0	61.9
	+75 +74		9.2	58.2
1	10+99		13.5	63.9
	T.P. 3.50	57.93	12.92	54.43
	11+19			
	+20 +39		9.1	48.8
	+40		9.7	48.2
	+58 11+49		9.0	48.9
	+75 +74		4.7	53.2
2	11+99		3.6	54.3
	+50 12+49		4.0	53.9
3	12+99		2.8	55.1
	TBS 13+24		0.5	57.4
	TP 12.15	69.89	0.19	57.74
	+50 13+49		8.0	61.9
4	13+99		4.3	65.6
	+25 14+24		1.5	68.4
	TP 9.75	79.34	0.30	69.59

		79.34		
	+50 14+49		9.1	70.2
	+65 +64		7.0	72.3
5	14+99		5.9	73.4
	+50 15+49		5.3	74.0
	15+99			
	6 = El. 30		3.6	75.7
	BM		5.51	73.83 74.81

Hatch between Webster & Clay

5' Hatch Line between Webster & Clay
10 Thomas. from 30A - 33d.

BM	4.77	77.76		72.99	AA Spk SW Webster - 30m
0+00 = Et. 30A			4.7	73.1	
+50			5.2	72.6	
+75			5.8	72.0	
1			5.2	72.6	
+25			4.3	73.5	
+50			3.5	74.3	
2			4.6	73.2	
+50			5.0	72.8	
+75			3.9	73.9	
3			5.6	72.2	
+25			5.6	72.2	
+50			6.7	71.1	
4			10.0	67.8	
+30			10.9	67.4	
+50			11.8	66.0	
+75			13.2	64.6	
		77.76			
5			11.2	66.6	
+25			7.8	70.0	
+50			6.7	71.1	
6			3.4	74.4	
T.P.	5.71	79.64	3.83	73.93	
+15			4.7	74.9	
+25			10.2	69.4	
+30			10.0	69.6	
+35			10.5	69.1	
+45			3.3	76.3	
+55			0.4	79.2	
+60 = Et. 31st = 0+00			1.7	77.9	
T.P.	6.86	85.10	1.40	78.24	
1+20 +80			5.2	79.9	
+50 7+10			5.2	79.9	
1 7+60			5.0	80.1	
+15 +75			4.6	80.5	

Graphic Sketch of Sheet B-1

	85.70			
+50 8+10		5.7	79.4	
2 8+60		6.8	78.3	
+50 9+10		5.9	79.7	
3 9+60		4.9	80.2	
+50 10+10		4.3	80.8	
TP.	5.86	86.77	4.19	80.91
4 10+60			5.8	81.0
+25 +85			6.1	80.7
+50 11+10			5.2	81.6
+65 +25			4.7	82.1
+75 11+35			6.2	80.6
5 11+60			6.4	80.4
+50 12+10			6.3	80.5
6 12+60			4.5	83.3
+20 +80			3.4	83.4
+20 +90			4.1	82.7
+66 = 0+00 Fl 32°	13+20		4.6	82.2

	86.77			
0+50 +70			5.0	81.8
1 14+20			4.3	82.5
50 +70			4.6	82.2
2 15+30			6.3	80.5
+50 +70			8.2	78.6
+75 +95			9.2	77.6
3 16+20			11.8	75.0
TP.	1.55	76.52	1.80	74.97
+37 = NL. 38°	+57		8.4	68.1
TP on Tenn.			11.34	65.18

5/1/10 Hatch Floor Thomas.

Line between N & N. from 30th & Trunk Line Sewer.

BM.	3.41	78.38		74.97	NW Cor. 30th & N. (Brass)
0+00 = Fl. 30th			4.8	73.6	
+50			4.3	74.1	
1			5.0	73.4	
+50			4.9	73.5	
2			4.9	73.5	
+50			5.2	73.2	
3			5.2	73.2	
+50			5.1	73.3	
4			5.3	73.1	
+50			5.2	73.2	
5			4.9	73.5	
T.P.	6.63	80.11	4.90	73.48	
+50			6.3	73.8	
6			6.5	73.6	
+30			5.8	74.3	
+60			6.2	73.9	

80.11

7			6.2	73.9
+50			5.3	74.8
8			4.9	75.2
+50			4.4	75.7
9			3.1	77.0
+50			3.4	76.7
10			4.9	75.2
+50			5.9	74.2
11			6.0	74.1
+50			5.2	74.9
12			6.7	73.4
+60			7.8	72.3
+90			8.9	71.2
13+20			9.4	70.7
+50			9.9	70.2
+75			10.7	69.4
TP.	2.73	72.20	10.64	69.47

Cylinder Plant Bm

		72.20		
14			2.4	69.8
+30			1.6	70.6
+50			1.8	70.4
+70			3.0	69.2
+80			7.5	64.7
+92 & RR			6.4	65.8
15			7.2	65.0
+05			7.4	64.8
+10			5.1	67.1
+20			7.0	65.2
+50			8.1	64.1
+60			11.1	61.1
TP	1.12	60.30	13.02	59.18
16			1.6	58.7
+20			2.5	57.8
+50			2.7	57.6
17			3.6	56.7

		60.30		
+50			4.6	55.7
+55			5.5	54.8
+66			13.3	47.0
TP	0.70	47.98	13.02	47.28
+77			8.3	39.7
TP	0.47	35.81	12.64	35.34
+90			4.0	31.8
18			9.2	26.6
+10			12.3	23.5
TP	3.50	26.53	13.06	22.75
+50			4.8	22.3
19			4.9	22.2
20			4.6	22.0
+96 = 17+22 of trunk line			4.3	22.8

Hatch Line between Log No. from
Dwd 10. thence 30 12 to Trunk Line -

12 ++	5.23	80,00		74.97
0+00 = N.H. 98 E of Cr. of 30 11.			5.6	74.4
+50			5.8	74.2
1			5.8	74.2
+50			5.0	75.0
2			5.0	75.0
+50			4.3	75.7
3			4.1	75.9
+50			3.4	76.6
4			3.1	76.9
+50			2.8	77.2
5			2.5	77.5
+30 Cr. 21 Rt			2.6	77.4
+60			2.0	78.0
6			2.3	77.7
T.P.	3.21	80.98	2.30	77.70
+50			3.4	77.6

80.98

7	4.6	76.4
+50	4.7	76.3
8	4.7	76.3
+50	5.0	76.0
9	4.8	76.2
+50	4.8	76.2
10	4.0	77.0
+50	4.3	76.7
11	4.5	76.5
+60	6.3	74.7
+85	6.1	74.9
+90 Cr.	5.7	75.3
12	6.2	74.8
+20	6.5	74.5
+50	6.8	74.2
13	4.7	76.3
+50	3.3	77.7

Joseph Stevens

		80.98		
14			3.1	77.9
T.P.	1.25	79.15	3.08	77.90
+50			1.4	77.8
+90			1.4	77.8
+96			3.9	75.3
15			10.9	68.3
T.P.	3.64	68.95	12.84	66.31
+10			9.9	59.1
+15			11.5	57.5
+22.5		℄ RR	10.4	58.6
+35			11.9	57.1
T.P.	0.96	57.23	12.68	56.27
+50			10.5	46.7
T.P.	0.50	44.73	12.90	44.33
+65			6.9	37.9
T.P. (Fence)	1.50	39.21	7.12	37.71
+90			8.8	30.4

		39.21		
16			12.9	26.3
TP	4.77	31.42	12.56	26.65
17			7.7	23.7
18			7.1	24.3

Uniform slope to Trunk Line c 19+96 = 13+42.

2/10 Match Monument Thomas.

Line between K & L from 32d to Trunk Line.

					Mon SE 32d 6.1
P.O.B.	6.94	85.29		78.35	
0+00	E. Line 32d		5.1	80.2	
+50			3.6	81.7	
1			3.6	81.7	
+50			3.9	81.4	
2			6.2	79.1	
+20			7.5	77.8	
+40			10.6	74.7	
T.P.	1.42	73.71	12.60	72.69	
+60			4.0	69.7	
+80			8.1	65.6	
+90			11.9	61.8	
T.P.	0.42	61.76	12.37	61.34	
3			1.6	60.2	
+03			1.7	60.1	
			4.7	57.1	
+10			9.2	52.6	
+13			11.0	50.8	

61.76

+28.5	℄ Cuyamaca		10.1	51.7
+30			11.5	50.3
+45			10.7	51.1
+65			13.8	48.0
T.P.	0.40	49.62	12.54	49.22
+80			5.4	44.2
4			11.2	38.4
T.P.	1.50	38.51	12.61	37.01
+80			8.7	29.8
+88			10.9	27.6
5			11.7	26.8
6			11.8	26.7
7			12.0	26.5
+75	Trunkline		11.8	26.7

Corner Started 10.2

2/11/10 Hatch Moore Thomas

Line between J – K from 30th To 33d.

B.M.	7.70	7806		7036	Level Sta. 45 117 Base Line Drawn
El. 30th = 0+00			4.8	73.3	
+ 02			5.5	72.6	
+ 50			5.4	72.7	
1			5.1	73.0	
+ 50			5.3	72.9	
2			4.9	73.2	
+ 50			4.6	73.5	
3			4.2	73.9	
+ 50			4.2	73.9	
4			4.0	74.1	
+ 50			4.0	74.1	
5			4.3	73.8	
+ 50			3.9	74.2	
6			3.9	74.2	
T.P.	11.20	85.40	3.86	74.20	
+ 50			11.0	74.4	

Graded Started 8-4

85.40

7	10.6	74.8	
+ 50	10.1	75.3	
8 WL 31st	10.0	75.4	
+ 30 "	9.9	75.5	
+ 60 "	9.6	75.8	
9	9.2	76.2	
+ 50	8.7	76.7	
10	8.1	77.3	
+ 50	7.1	78.3	
11	6.7	78.7	
+ 50	5.2	80.2	
12	4.8	80.6	
+ 50	4.5	80.9	
13	4.1	81.3	
+ 50	3.6	81.8	
14	2.2	83.2	
+ 66 WL 32d	2.5	82.9	

		85+70		
+75			1.6	83.8
+80			2.9	81.5
+90			3.5	81.9
15			3.7	81.7
+02			2.6	82.8
+20	F.L. 32d		2.4	83.0
T.P.	4.81	87.71	2.40	83.00
+50			5.2	82.6
16			6.0	81.8
+50			6.8	81.0
17			6.7	81.1
+50			6.4	81.4
18			6.4	81.4
+15			6.4	81.4
+45	W.L. 33d		9.3	78.5
T.P. Rock at Alley Set I-J on 32d			5.52	82.29

Nail SE Cor 32d & Alley

Line between I-J from E.L. Blk. 130

2 Hash
11 Nearc
10 Thomas

To 30th

T.P. (32d I-J)	4.71	87.00		82.29
0+00 = E.L. Blk.			12.4	74.6
+40			4.7	82.3
+50			3.7	83.3
1			2.7	84.3
+50			3.0	84.0
2			2.8	84.2
+50			3.1	83.9
3			4.0	83.0
+33 = F.L. 32d			4.7	82.3
+50			5.7	81.3
+65			5.5	81.5
+80			5.3	81.7
+93 = W.L.			5.7	81.3
4			5.8	81.2
+50			6.5	80.5
5			6.7	80.3

Profile Started 1.5

		87.00		
+50			6.4	80.6
6			6.8	80.2
+50			6.6	80.4
7			6.6	80.4
+50			6.7	80.3
TP	2.30	83.50	6.80	80.20
8			3.7	79.8
+50			3.9	79.6
9			4.7	78.8
+50			4.4	79.1
10			4.6	78.9
+03 El 3.1 ab			4.9	78.6
+33 Cr			4.9	78.6
+63 WL			5.0	78.5
11			5.2	78.3
+50			5.3	78.2
12			5.4	78.1

		83.50		
+50			5.6	77.9
13			6.0	77.5
+50			6.3	77.2
14			6.5	77.0
+50			6.6	76.9
15			6.5	77.0
+50			5.9	77.6
16			5.8	77.7
+50			3.2	80.3
17			2.8	80.7
+50			1.3	82.2
BM SW 3.1 ab T			7.19	76.31	76.304
+75			0.7	82.8
18 about line of Cross sewer-main				

2 Hatch Line between H and I from
11/10 Snow
Thomas 31st to EL. Blk -

					SE 32d - I
BM	766	90.47		82.306	BR Spk
0+00 = EL 31st					
+87 E of 31 = Sewer line			2.4	88.1	
1			2.3	88.2	
+50			2.5	88.0	
2			2.7	87.8	
+50			3.2	87.3	
3			4.1	86.4	
+50			5.0	85.5	
4			5.5	85.0	
+50			6.5	84.0	
5			7.0	83.5	
+50			7.8	82.7	
6 = WL 32d			8.2	82.3	
+30 CL "			8.6	81.9	
+50			9.9	81.1	
+55			8.2	82.3	
+60 EL "			8.4	82.1	

90.47

7			8.7	81.8	
+50			8.3	82.2	
8			8.1	82.4	
+50			8.2	82.3	
9			9.0	81.5	
T.P	2.64	87.35	8.76	81.71	
+10			1.6	81.8	
+25			5.4	77.0	
+35			11.2	71.2	
T.P	0.46	69.93	12.88	69.47	
+50			2.3	67.6	
+75			7.9	62.0	
10			12.5	57.4	
T.P.			6.10	63.83	Top of Board at Fence Cor.

Profile Started 8-14

2/14/10 Hatch Moore Thomas

Line between G and H from 32d to 30th

BM.	8.9'	92.15		83.225	NE Cor. 32d and H. RR Spk.
W.L. 32d.			8.0	84.1	
+50			6.1	86.0	
1			5.8	86.3	
+50			4.8	87.3	
2			3.6	88.5	
+23 Line of Cross Sema-			2.8	89.3	
+50			1.4	90.7	
TP.	13.05	105.14	0.04	92.09	
3			12.0	93.1	
+50			9.6	95.5	
+75			8.1	97.0	
4			6.1	99.0	
+50			1.8	103.3	
TP.	11.0'	115.79	0.36	104.78	
+75			10.0	105.8	
5			8.2	107.6	

Bridge Plates B-5

115.79

+35			6.0	109.8	
+50			6.1	109.7	
6 Eh. 31st			7.5	108.3	
+35 = Cr.			7.3	108.5	
+35			8.2	107.6	
+60 = W.L. 31st			5.2	110.6	
+85			2.9	112.9	
TP.	12.90	128.48	0.21	115.58	
7			13.2	115.3	
+50			4.7	123.8	
+75			1.2	127.3	
TP.	12.76	141.03	0.21	128.27	
8			9.5	131.5	
+35			2.0	139.0	
TP.	12.93	153.74	0.22	140.81	
+50			11.9	141.8	
+75			9.7	144.0	

Note - W.L. 31st. Ground is level 30' North of Sta 10+00, 120' North elevation 15. 128.5

		153.74		
9			8.0	145.7
+50			7.3	146.4
10			5.9	147.8
+50			3.1	150.6
T.P.	9.80	163.51	0.23	153.51
11			8.0	155.3
+50			5.4	157.9
12			4.1	159.2
+50			4.6	158.7
13			5.9	157.4
+15			5.1	158.2
+30			6.5	156.8
+50			7.0	156.3
+80			7.5	155.8
14			9.4	153.9
+30			11.2	152.1
+38 = El	30ft	Sf.	13.2	150.1
+38 = "	"	" (grade)	15.2	148.1

2 1/4 Hatch 10 Nagrr Thomas

Line between CT & PT from - 32d East.

BM	4.32	87.54		83.22
WL 32d			3.4	84.1
+20			3.5	84.0
+22			5.0	82.5
+30			4.8	82.7
+45			(5.2) 3.8	82.3 83.7
+60 = BL 32d			4.3	83.3
+80			4.9	82.6
1			6.8	80.7
+25			8.7	78.8
+50			10.9	76.6
2			12.0	75.5
+50			11.7	75.8
+70			14.0	73.5
+80			11.3	76.2
+85			12.5	75.0
T.P	0.10	64.74	12.90	64.64

Replic Stakes 1 & 6

64.74

+86			3.6	61.1
3			6.0	58.7
+10			11.2	53.5
+25			13.3	51.4
T.P	3.14	52.31	12.57	52.17
+45			2.3	50.1
+50			4.4	47.9
+60			8.4	43.9
+75			9.2	43.1
4			9.4	42.9
+15			10.1	42.2
+20			10.8	41.5
+25			8.7	43.4
+50			8.1	44.2
+60			6.3	46.0
T.P	12.41	64.52	6.20	52.11
+75			11.0	53.5

		64.52		
5			0.3	64.2
TP	4.78	69.09	0.21	64.31
+10			2.4	66.7
+50			2.0	67.1
6			3.4	65.7
+10			5.6	63.5
+25			8.8	60.3
+35			12.2	56.9
TP	0.19	56.52	12.66	56.43
+51 Wl. 33d St.			2.3	54.3
+80			4.6	52.0
+83			6.0	50.6
7			7.7	48.9
+25			11.3	45.3
TP	0.21	45.90	10.93	45.69
+40			1.7	44.2
8			5.6	40.3

		45.90		
+50			7.0	38.9
9			8.2	37.7
+50			9.8	36.1
10			11.1	34.8
TP	1.02	33.92	13.0	32.90
+25			2.2	31.7
+50			3.6	30.3
11			4.7	29.2
12			4.6	29.3
13			4.7	29.2
+525 = Trunkline Sewer			4.3	29.6
TP	6.26	39.80	4.35	29.54
14			4.9	29.9
15			4.4	30.4
16			4.3	30.5
17			3.8	31.0
TP	5.51	36.81	3.50	31.30

	3681		
+15		6.6	31.3
+25		3.6	33.8
+50		4.6	32.2
18		4.7	32.1
+25		6.6	30.2
+50 creekbed.		80	28.8
TP		70.2	29.79 on top of hill.

2 Hatch
10 Stones

Line between H & I in McLaren Addt.

BM	9.65	47.91		38.26	Spike in stump SW 33 ft
TP	10.24	57.89	0.26	47.65	
0+00 = Cr. Alley bet.			9.3	48.6	
+60			10.7	47.2	
+65			13.5	44.4	
+75			11.7	46.2	
1			12.2	45.7	
+25			12.5	45.4	
+50			6.4	51.5	
+70			2.2	55.7	
+80			3.0	54.9	
2			9.7	48.2	
+10			11.7	46.2	
TP	0.68	45.97	12.60	45.29	
+50			2.8	43.2	
3			4.6	41.4	
+25			7.3	38.7	

Profile Started
S-5

45.97

+50			5.8	37.2
4			9.2	36.8
5			9.5	36.5
+10 = WL 38 1/2				
+25			10.4	35.6
+50			9.7	36.3
+65			10.6	35.4
+85			10.9	35.1
6			9.8	36.2
+25			10.2	35.8
+50			11.5	34.5
+75			10.6	35.4
7			11.3	34.7
+50			9.9	36.1
8			9.8	36.2
TP	7.24	43.36	9.85	36.12
+20 edge of creek			7.5	35.9
+25			9.4	34.0

	43.36			
+60		7.8	35.6	
+70		9.2	34.2	
9		11.5	31.9	
+15		11.4	32.0	
+20 edge of creek		9.1	34.3	
+50		6.4	37.0	
10		4.5	38.9	
+35		4.2	39.2	
+40		2.7	40.7	
+50		6.5	36.9	
+7.5	wash	6.3	38.1	
11		5.9	37.5	
+10		6.4	37.0	
+20		5.0	38.4	
+50		4.9	38.5	
12		2.7	40.7	
T.P.		12.6	42.10	

3/10/10 Hatch Moore Thomas. Line between I and J from Alley to 34th St. in Mt Lorens Addn.

T.P.	9.54	73.37		63.83	on top of Board at Fence Cor. West Between H-I - 33 1/2 -
T —	1.26	68.10	6.33	67.04	
R. N & S Alley			0.4	67.7	
+50			6.8	61.3	
+75			10.5	57.6	
			12.4	55.7	
T.P.	0.60	56.83	12.87	55.23	
+25			1.6	54.2	
+50			5.0	50.8	
T.P.	0.95	43.82	12.96	42.87	
+80			3.2	40.6	
2			4.0	39.8	
+50			4.2	39.6	
3			5.2	38.6	
+40			5.8	38.0	
+70			8.0	35.8	
4			8.5	35.3	

Profile Started 10-6

		43.82		
5			9.5	34.3
+15	WL 23d		9.5	34.3
+45			9.2	34.6
+75	EL 23d		9.6	34.2
6			11.1	32.7
+40			11.5	32.3
7			12.4	31.4
TL	7.06	38.55	12.33	31.49
+40			7.3	31.3
+57			9.3	29.3
+65			5.4	33.2
+80			5.0 8.2	33.6 30.4
+85			10.4	28.2
8			10.9	27.7
+20			10.2	28.4
+30			11.5	27.1
+40			9.7 5.8	28.9 32.8

	38.55		
+55		5.0	33.6
9		5.2	33.4
+25		3.8	34.8
+50		3.7	34.9
+75 Force.		3.4	35.2

3/10/11 Hatch Trivett Thomas

Line between N & Parsons

			J – K Addt.	
TP	7.98	75.02		67.04
Cr. of alley at W end of Tract			3.8	71.2
+38			11.0	64.0
TP	6.80	63.26	12.56	62.46
+50			5.8	57.5
TP	0.53	51.35	12.46	50.82
+65			1.9	49.5
+80			8.3	43.1
+95			13.0	38.4
TP	0.0	38.91	12.44	38.91
1			1.2	37.7
+30			3.3	35.6
2			4.4	34.5
3			4.2	34.7
4			5.6	33.3
5			7.0	31.9
+15 W.L	33.d		7.4	31.5

Graphic Hatter
B-6

38.9'

+45			6.9	32.0
+75	El. 33.d		7.7	31.2
6			8.1	30.8
+30			9.4	29.5
7			9.1	29.8
TP	5.76	35.04	9.53	29.38
+80			5.6	29.4
+89			4.1	30.9
+93			8.5	26.5
8			10.6	24.4
+15			10.5	24.5
+30			7.0 5.2	28.0 29.8
+35			4.1	30.9
+65			4.8	30.2
9			4.2	30.8
+30			3.8	31.2
+75			3.4	31.6

3/14/10 Match Mound Thomas — Line between F and G Grants 32d to 30th

BM	7.04	58.28		81.24	Mile in Cor of Fence Grants 32
W2 - 32d			4.4	83.9	
+25			3.0	85.3	
+50			1.1	87.2	
TP	12.80	100.93	0.15	88.13	
+75			12.9	88.9	
1			10.2	90.7	
+25			8.6	92.3	
+50			4.9	96.0	
+75			3.2	97.7	
TP	11.84	112.46	0.31	100.62	
2			11.2	101.3	
+25			9.5	103.0	
+50			7.5	105.0	
+75			5.4	107.1	
3			3.5	109.0	
+25			1.3	111.2	

Corner Started 8.7

			112.46		
TP	12.93	125.29	0.10	112.36	
+50			11.8	113.5	
+75			9.1	116.2	
4			4.9	120.4	
+25			0.4	124.9	
TP	12.81	137.98	0.12	125.17	
5 +50			7.0	131.0	
+75			2.7	135.3	
TP	12.60	150.37	0.21	137.77	
5			10.6	139.8	
+25			7.8	143.6	
+50			6.0	146.4	
+75			4.9	145.6	
6 El 31d			3.6	146.8	
+30 Cr 31d			2.1	148.3	
TP	12.41	162.23	0.55	149.82	
+60	W 31d		11.4	150.8	

		162.23		
+85			10.4	151.8
7			7.2	156.0
+25			4.4	157.8
+50			5.7	156.5
+75			8.2	154.0
8			8.4	153.8
+25			6.8	155.4
+50			3.9	158.3
+75			1.9	160.3
9			0.1	162.1
+70	163	163.43	0.43	161.80
+25			0.2	163.2
+50			2.5	160.9
+75			5.0	158.4
10			1.8	161.6
+25			2.1	161.3
+50			2.3	161.1

		163.43		
+75			1.9	161.5
11			2.5	160.9
+25			4.1	159.3
+50			5.6	157.8
+75			8.6	154.8
12			15.9	147.5
+10			15.9	147.5
+25			9.9	153.5
+50			7.7	155.7
+62 = El. 30 ft			3.1	160.3

3/14/25 Katch. Snow Thomas

Line between F and G from 32d to 35th.

BM	3.90	85.14		81.24	32d G see P 32
W/L 32d			1.3	83.8	
+ 20	Cr.		1.9	83.2	
+ 50			2.7	82.4	
+ 55			5.1	80.0	
+60 - 0+00 B/L			5.5	79.6	
+25			6.9	78.2	
+30			6.7	78.4	
+75			4.7	80.4	
			5.1	80.0	
+25			7.3	77.8	
+40			9.3	75.8	
+50			13.0	72.1	
+60			13.6	71.5	
+65			11.5	73.6	
+75			12.0	73.1	
T.P.	1.63	73.76	13.01	72.13	

Cycle Started 8-7

				73.76	
2			6.5	66.3	
+25			8.3	65.5	
+30			10.8	63.0	
+25			9.4	64.4	
+50			9.1	64.7	
+75			9.7	64.1	
+81 = 12+72 off line in Canon West of 32d Street			9.9	63.9	
3			7.6	66.2	
T.P.	11.22	84.52	11.46	73.30	
+25			6.9	77.6	
+50			4.6	79.9	
+75			5.3	79.2	
4			4.5	80.0	
+25			5.5	79.0	
+50			6.2	78.3	
+75			5.9	78.6	
5			6.6	77.9	

		84.52		
+25			6.4	78.1
+50			6.7	77.8
+75			7.2	77.3
6	Rt 32°		6.9	77.6
+20			6.5	78.0
+30			7.8	76.7
+60	Rt 133°		8.0	76.5
7			8.2	76.3
TP	2.09	77.46	9.15	75.37
			0.2	77.3
+17			9.3	68.2
	Reservoir		9.9	67.6
+45			0.4	77.1
+65			1.2	76.3
+70			6.4	71.1
8			7.6	69.9
+50			9.2	68.3
9			10.6	66.9
+50			13.2	64.3

		77.46		
TP	0.36	64.81	13.01	64.45
10			2.7	62.1
+59			3.9	60.9
+65			6.1	58.7
+80			10.9	53.9
TP	0.84	52.19	13.01	51.35
+90			5.6	46.6
11			7.7	49.5
+10			8.8	43.4
TP	2.81	47.49	7.51	44.68
+50			5.7	41.8
12			5.4	42.1
TP	5.94	48.03	5.40	42.09
13			5.8	42.2
14			5.7	42.3
15			4.3	43.7
16			4.1	43.9

	4803			
17		3.2	44.8	
18		3.3	44.7	
19		3.4	44.6	
+21	Fence near creek	2.7	45.3	

3 Sets Monuments to Thurmer — Line E. of 32d from I to Brooklin Hts following Canon

BM	278	41.09		38.26	Spike in Fence Cor SW N-32d
Cr. 33d I = 0+00			5.2	35.8	
+30 = W.L. 33			4.8	36.2	
1			3.7	37.3	
2			2.5	38.5	
3			0.4	40.6	
TR	1303	53.60	0.47	40.57	
+30			12.0	41.6	
+40			13.1	40.5	
			11.9	41.7	
+58	∠ 63°00' R		11.1	42.5	
+90			10.6	43.0	
+95			12.3	41.3	
4			12.3	41.3	
+50			11.2	42.4	
+80			11.0	42.6	
5			9.1	44.5	
+10			8.1	45.5	

Angle Station

8
1
8

		53.60		
+50			7.6	46.0
+90			6.6	47.0
6			7.9	45.7
+10			7.9	45.7
+20			6.0	47.6
+50			5.8	47.8
+95			4.9	49.2
7			2.0	51.6
T.P.	5.97	59.37	0.20	53.40
+10			2.1	57.3
+20			1.7	57.7
+29	∠ 19°20'	R.	5.9	53.5
+35			5.8	50.6
+60			9.9	49.5
+80			8.7	50.7
8			8.0	51.4
+25			7.5	51.9

		59.37		
+50			8.5	50.9
+60			7.3	52.1
+90 =	Sta 4 Line bet. G-H		6.5	52.9
9			6.2	53.2
+50			4.7	54.7
10			3.1	56.2
+15			3.4	56.0
+25			5.1	54.3
+35			2.7	56.7
+50			1.4	58.0
T.P.	13.00	7.37	1.00	58.37
11			1.4	60.0
+50			1.0.2	61.2
12			8.6	62.8
+50			7.8	63.6
+72 =	2+81.4 Line bet F-G		7.5	63.9
13			6.5	64.9

		71.37		
+50			4.5	66.9
14			3.4	68.0
+40			2.6	68.8
TP	9.59	80.81	0.15	71.22
+53			5.3	75.5
+67 ∠	24°30R		4.4	76.9
+80			5.5	75.3
+90			12.6	68.2
15			11.5	69.3
+50			9.9	70.9
16			8.8	72.0
+50			8.9	71.9
+75			6.2	74.6
17			5.7	75.1
+50			4.7	76.1
18			3.9	76.9
+40			4.3	76.5

		80.81		
+50			1.7	79.1
TP	12.90	92.65	1.06	79.75
+70			11.3	81.4
+80			15.0	77.7
19			12.8	79.9
+50			10.9	81.8
+75			9.2	83.5
+55			6.5	86.2
20			5.4	87.3
+50			6.4	86.3
21			6.4	86.3
+50			5.2	87.5
22			3.6	89.1
+25			1.0	91.7
+50			1.3	91.4
+56 ∠	20°30L		3.6	90.1
TP	12.87	104.20	1.32	91.33

		104.20		
+65			13.8	90.4
23			12.7	91.5
+35			11.9	92.3
+40			12.8	91.4
+50			11.2	93.0
24			9.6	94.6
+50			7.3	96.9
25			6.5	97.7
+25			5.0	96.2
+35			5.9	98.3
+50			7.3	96.9
+60			5.3	98.9
26			4.0	100.2
+20			5.5	98.7
+36	∠ 19°30'		3.6	100.6
+50			2.9	101.3
27			1.5	102.7

		104.20		
TP	12.95	115.69	1.46	102.74
+40			13.5	102.2
+15			12.7	103.0
+50			11.3	104.4
28			9.8	105.9
+50			9.2	106.5
+75			9.6	106.1
29			8.0	107.7
+50			6.5	109.2
30			4.8	110.9
+54			5.0	110.7
+65			5.9	109.8
+75			4.0	111.7
31			2.9	112.8
+15			3.1	112.6
+20			3.8	111.9
+50			3.0	112.7

		115.69		
+70			1.7	114.0
TP	12.93	128.09	0.53	115.16
32			12.5	115.6
+50			11.2	116.9
+75			9.7	118.4
+92 ∠	20°30'R		9.6	118.5
33			10.9	117.1
+30			8.6	119.5
+50			7.4	120.7
34			5.8	122.3
+20			6.4	121.7
+50			8.4	119.7
+60			6.2	121.9
+80			4.9	123.2
35			3.4	124.7
TP	11.98	139.73	1.34	127.75
+50			12.2	127.5

		139.73		
+83 ∠	21°00'L		11.2	128.5
36			12.1	127.6
+35			10.9	128.8
+50			12.5	127.2
+65			9.0	130.7
37			7.9	131.8
+25			6.6	133.1
+50			6.1	133.6
38			5.3	134.4
+50			3.6	136.1
+75			3.6	136.1
39			4.3	135.4
+35			1.9	137.8
+50			1.2	138.5
TP	1.29	152.35	0.30	139.43
40			12.1	140.3
+50			10.1	142.3

		152.35		
41			8.8	143.6
+50			6.9	145.5
+85			6.9	146.0
42			5.7	146.7
+50			3.2	149.2
+69	< 19°30'		2.4	150.0
43			1.5	150.8
+50			1.3	151.0
TP	11.77	163.78	0.34	152.01
44			10.9	152.9
+50			9.7	154.1
+75			11.2	152.6
45			9.1	154.7
+50			5.7	158.1
+75			4.7	159.1
46			5.9	157.9
+05			6.9	156.9

Profile Started B-8

		163.78		
+20			4.8	159.0
+50			3.5	160.3
47			1.6	162.2
+50			0.7	163.1
+65			2.0	161.8
+75			0.3	162.5
TP			0.36	163.42

3/10 Hatch
3/10 Moore
3/10 Thomas

Line between E & F from 32d to sewer bet. 29½-30½.

T.P.	12.55	84.07		71.52
=	12.30	96.28	0.09	83.98
Cr. 32d St. Sp. Cast Sewer pipe			3.40	92.9
Ground			6.0	90.3
West line = 0+00			7.9	88.4
+25			4.7	91.6
+50			0.8	95.5
T.P.	12.74	108.83	0.19	96.09
+75			4.3	104.5
1			1.2	107.6
T.P.	13.04	121.25	0.62	108.21
+25			12.1	109.1
+50			10.6	110.6
+75			9.1	112.1
2			6.9	114.3
+25			9.9	116.8
T.P.	12.76	133.85	0.16	121.09

		133.85		
+50			12.8	121.0
+75			9.0	124.8
3			4.6	129.2
TP	12.89	146.19	0.55	133.30
+25			10.9	135.8
+50			3.0	143.2
TP	12.66	146.27	0.24	133.61
+75			9.0	137.3
4			1.6	144.7
TP	13.00	159.17	0.10	146.17
+25			9.6	149.6
+50			4.3	154.9
+75			0.7	158.5
TP	7.10	166.14	0.13	159.04
5			5.7	160.4
+25			4.6	161.51
+50			4.6	161.5

		166.14		
+75			5.2	160.9
6 = EL 31.0			6.0	160.1
+30	Cr.		7.4	158.7
+60	WL		8.4	157.7
7			10.0	156.1
+50			6.3	159.8
8			1.2	164.9
TP	7.38	173.10	0.42	165.72
+50			6.1	167.0
+75			4.7	168.4
9			5.7	167.4
+50			5.4	167.7
10			5.5	167.6
+50			5.5	167.6
11			6.0	167.1
+50			6.6	166.5
12			7.2	165.9

		173.10		
+50			9.8	163.3
+60 Ek 30 14			8.8	164.3
+90 Cr			8.7	164.4
13			8.8	164.3
+20 WL			8.2	164.9
+25			7.0	166.1
+50			6.9	166.2
14			7.2	165.9
+50			8.2	164.9
15			9.6	163.5
TP	1.11	164.31	9.90	163.20
+50			4.2	160.1
+75			9.7	154.6
TP	0.24	152.75	12.30	152.01
16			2.0	150.2
+25			5.3	146.9
+50			10.0	142.2

		152.25		
TP.	0.47	140.66	12.0C	140.19
+75			5.6	135.0
17			12.2	128.5
TP	0.96	128.94	12.68	127.98
+25			5.5	123.4
+50			11.0	117.9
+75			12.8	116.1
+90			14.3	114.6
18			12.7	116.2
+12 Man Hole			12.3	116.6

3/17/10 Hatch Murry Thomas — Line between 32d & 33d — E by F from

TP	2.89	98.48		96.09
Wh. 32d = 0+00			10.1	88.4
0+50			3.9	94.6
+60 = EL 32d			4.0	94.5
+75			2.5	96.0
1			2.5	96.0
+50			4.3	94.2
2			5.7	92.8
+50			9.3	89.2
+75			9.8	88.7
3			12.6	85.9
TP	0.85	86.45	12.88	85.60
+25			5.8	80.6
+50			13.2	73.2
+65 = 16+63 on line Ea of 32d in Cañon			14.0	72.4
+75			13.3	73.1
4			12.5	73.9

86.45

+25			7.7	78.7
+50			4.2	82.2
+75			1.3	85.1
TP	7.15	93.38	0.22	86.23
5			6.2	87.2
+50			5.8	87.6
6			5.5	87.9
+50			4.5	88.9
+60 = Wh. 33d			3.5	89.9
TP	1.58	94.09	0.87	92.51

3/17 Hatch Line on ℄ of Lemon Grove Blvd
3/10 thence from 23° E

		94.09		
0+00 = El. 33.8			1.5	92.6
+50			0.9	93.2
1			0.7	93.4
+50			1.1	93.0
+75			1.5	92.6
2			2.8	91.3
+50			6.0	88.1
3			9.1	85.0
+50			12.5	81.6
T.P.	0.24	81.63	12.70	81.39
4			3.6	78.0
+50			7.1	74.5
5			10.0	71.6
+50			12.7	68.9
T.P.	0.64	69.47	12.80	68.83
6	Wk. 34.4		3.4	66.1
+30	Cr.		4.5	65.0

		69.47		
+60	El. 34.4		5.5	64.0
7			7.0	62.5
+50			9.1	60.4
8			10.6	58.9
+50			11.7	57.8
9			12.2	57.3
T.P.	0.93	58.13	12.27	57.20
+50			2.3	55.8
10			4.1	54.0
+50			5.0	53.1
11			5.8	52.3
+50			5.9	52.2
12			5.6	52.5
+60	Wk. 35.1		5.1	53.0
+90	Cr.		4.8	53.3
13			4.6	53.5
+20	El.		4.5	53.6

		5813		
+70			4.3	53.8
10			4.1	54.0
+20 Bridge -			4.0	54.1

3/17 Kalch
Survey Line bet. Benesch & Thomas from 33rd East

TP	11.40	103.91		92.51
0+00 = East line 33rd			8.6	95.3
+50			7.7	96.2
1			6.1	97.8
+50			4.4	99.5
2			2.7	101.2
+50			3.5	100.4
3			4.8	99.1
+50			7.3	96.6
4			10.8	93.1
TP	0.28	91.45	12.74	91.17
+50			5.2	86.2
5			8.0	83.4
+50			11.2	80.2
6	WL 34th		12.5	78.9
TP	0.25	79.40	12.30	79.15
+30 ℄			1.9	78.0

		79.40		
+60 WL 34			3.0	76.4
7			5.1	74.3
+50			7.0	72.4
8			8.8	70.6
+50			10.1	69.2
9			11.2	68.2
+50			12.0	67.4
10			13.0	66.4
TP	1.25	67.80	12.85	66.55
+50			2.8	65.0
11			4.3	63.5
+50			5.7	62.1
12			7.9	59.9
TP	2.07	57.10	12.77	55.03
+40			3.3	53.8
+60 WL 35			4.0	53.1
+90 C			4.6	52.5

		57.10		
13			4.8	52.3
+20 EL			4.9	52.2
+50			5.6	51.5
14			6.0	51.1
+25			5.1	52.0
+50			7.7	49.4
+75			6.8	50.3
15			5.9	51.2
+05 Creek bed			12.1	35.0

3/17/10 Hatch Thomas — Line between D-E 32d West

T.P.	6.04	98.55		92.51
0+00 = WL 33d			0.2	97.4
+50			1.5	97.1
1			2.7	95.9
+25			4.5	94.1
+50			8.0	90.6
+89 = 20+50 Sorg Line East of 32d in Cañon			12.1	86.5
2			12.4	86.2
+25			14.1	84.5
+50			14.0	84.6
+75			12.1	86.5
3			3.8	94.67
+10			0.2	98.4
T.P.	12.99	110.84	0.70	97.85
+25			10.8	100.0
+50			9.6	101.2
+75			9.7	101.1

3/18/10

		110.84		
4			8.7	102.6
+25			6.2	104.6
+50			4.5	106.3
+75			3.0	107.8
5			1.1	109.7
T.P.	12.70	123.46	0.08	110.76
+25			10.9	112.6
+50			6.0	117.5
+80			1.5	122.0
T.P.	12.70	135.96	0.20	123.26
6 = EL 32d			10.3	125.7
+30 Cr.			4.0	132.0
T.P.	12.59	148.31	0.24	135.72
+60 WL			10.4	137.9
+80			4.9	143.4
T.P.	12.71	160.37	0.65	147.66
7			11.2	149.2

		160.37		
+25			6.2	154.2
+50			2.9	157.5
T.P	12.64	172.47	0.54	159.83
+75			11.9	160.6
8			7.7	164.8
+25			13.1	169.4
+50			2.4	170.1
+75			4.0	168.5
TP.	0.76	164.13	9.10	162.37
9			1.3	162.8
+25			6.7	157.4
+50			11.6	152.5
TP	0.28	151.39	13.02	151.11
+ 75			4.5	146.9
10			10.1	141.3
+25			13.1	138.3
TP.	0.77	139.06	13.10	138.29

		139.06		
10+50			9.1	130.0
TP.	0.23	126.29	13.00	126.06
+75			3.9	122.4
+90			10.1	116.2
11			7.5	118.8
+25			8.1	118.2
+45			11.4	114.9
+50			9.5	116.8
+75			2.5	123.8
TP	12.49	138.52	024	126.85
12			7.6	130.9
TP	12.18	150.40	032	138.32
+30			12.9	137.5
+60 EL 31st			6.6	143.8
TP	13.02	163.20	022	150.18
+90			9.5	153.7
13			7.6	155.6

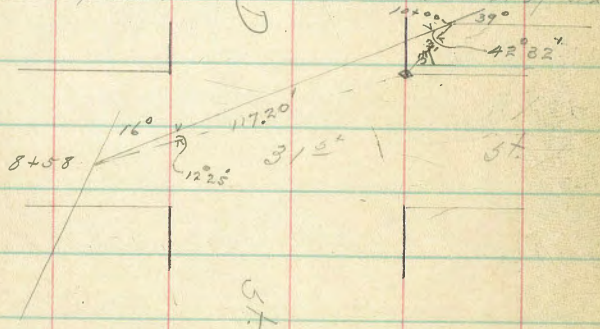
		163.20			
+20	WL		4.0	159.2	
TP	12.82	175.75	0.27	162.93	
+50			8.0	167.7	
+75			0.5	175.2	
TP	12.63	188.02	0.36	175.39	
10			8.9	179.1	
+25			6.6	181.6	
+50			4.0	184.0	
15			0.6	187.4	
TP	8.87	196.63	0.26	187.76	
+25			5.6	182.6	
+50			3.2	184.8	
+78	Manhole		2.2	185.8	

3/26/10 Water Main Line between C-D from 32nd East

TP	13.01	123.77		110.76	
=	13.07	136.59	0.25	123.52	
	12.99	149.42	0.16	136.43	
	12.32	161.33	0.41	149.01	
TP at 32nd and Alley	11.73	171.19	1.87	159.46	
WL 32nd 50+00			6.6	164.6	
+25			9.9	161.2	
+50			14.6	156.6	
+75			15.7	155.5	
1			14.4	156.8	
+25			13.0	158.2	
+50			11.8	159.4	
+75			12.7	158.5	
TP	0.11	158.51	12.79	158.40	
2			2.2	156.3	
+25			5.0	153.5	
+50			8.1	150.4	
TP	0.07	145.77	12.81	145.70	Continued on P.59

Alignment for Levels on P.S.S

0+00 = Pt on ℄ 32d on Alley between D-E		
0+73	33°10 R.	N72°15W
3+50	22°30 R	N49°45W
5+77	27°50 L	N77°30W
7+50	19°20 R	N58°00W
8+58	16°00 R	N42°00W
10+00	39°00 R	N3°00W
13+35 ℄ C St.	12°30 L	N15°30W
15+25 ℄ Alley	34°30 L	N50°00W
17+58 ℄ B.	19°40 R	N30°20W = 101.1 N of NW 31st



3 Hatch
31 Moore
10 Thomas

Line in Court from 32d between E-F
To 4 St between 30-31

Sidewalk State 200'W of SW Cor 31st B -	2.78	208.28		205.50
20+50			9.0	199.3
20+25			13.2	195.1
T.P.	0.39	195.45	13.22	195.06
20			1.8	193.6
19+75			4.3	191.1
19+50			6.0	189.4
19+25			6.5	188.9
19			6.4	189.0
18+75			8.3	187.1
18+50			10.2	185.2
18+38			10.4	185.0
18+25			7.0	188.4
TP	12.71	208.02	0.14	195.31
18			3.4	204.6
17+75			4.1	203.9
17+58 < 19°40 R			4.3	203.7

		20802		
17+25			4.9	203.1
17+13			4.6	203.4
17			11.8	196.2
T.P.	0.0	19542	12.60	195.42
16+75			13.6	182.4
T.P.	0.11	183.05	12.48	182.94
16+50			9.4	173.6
16+25			11.1	171.9
T.P.	1.20	171.19	13.06	169.99
16			3.2	168.0
15+75			5.6	165.6
15+50			7.2	164.0
15+25 ∠	34°30' L		8.3	162.9
15+10			9.9	161.3
15			9.1	162.1
T.P.	3.84	16530	9.73	161.46
14+75			2.9	162.4

		16530		
14+50			6.3	159.0
14+25			9.6	155.7
14			10.6	154.7
13+95			10.3	155.0
T.P.	6.32	170.92	0.70	164.60
13+75			1.5	169.4
13+50			1.9	169.0
13+35 ∠	12°30' L		1.7	169.2
13			2.4	168.5
12+95			3.5	167.4
T.P.	0.0	157.95	12.97	157.95
12+75			2.2	155.7
12+50			11.2	146.7
12+25			12.6	145.3
T.P.	3.55	148.65	12.85	145.10
12+00			4.5	144.1
11+75			2.6	146.0
11+50			5.5	143.1

		148.65		
11+25			8.6	140.0
11			9.1	139.5
10+75			10.7	137.9
10+50			10.2	138.4
10+25			12.9	135.7
10+00 ∠ 39°00' R.			13.2	135.4
T.P.	0.410	135.85	13.20	135.45
9+75			0.6	135.2
9+50			0.0	135.8
9+25			2.9	132.9
9			5.1	130.7
8+75			4.9	130.9
8+58 ∠ 16°00' R.			6.3	129.5
8+50			10.1	125.7
T.P.	2.30	128.21	9.94	125.91
8+25			2.1	126.1
8			1.8	126.4

		138.21		
7+75			7.2	131.0
7+50 ∠ 19°20' R			9.9	118.3
7+25			9.0	119.2
7			11.8	116.4
6+75			13.2	115.0
T.P.	2.38	117.72	12.87	115.34
6+72 = 11+46 Alley Line			2.7	115.0
6+50			3.4	114.3
6+25			1.6	116.1
6			2.2	115.5
5+77 ∠ 27°50' L			3.7	114.0
5+50			4.1	113.6
5+25			6.4	111.3
5			8.6	109.1
4+82			9.4	108.3
4+75			7.2	110.5
4+65			5.4	112.3

		117.72		
4+50			9.2	108.5
4+25			11.6	106.1
4			12.7	105.0
TP	4.09	109.15	12.66	105.06
3+75			6.7	102.4
3+50 ∠	22°30' R		4.9	104.2
3+25			9.0	100.1
3			8.9	100.2
2+75			11.1	98.0
2+50			11.8	98.3
2+25			11.0	98.1
2			13.2	95.9
1+75			11.7	97.4
1+50			9.1	100.0
1+25			6.0	103.1
1+20			4.9	104.2
1			10.1	99.0

		109.15			
TP	0.94		13.05	96.10	96.09
0+73 ∠	33°0' R		3.0	106.1	

3/5/1 Hahl 10 Thomas

Continued from P 54

		145.77		
+75			1.3	144.5
3			10.2	135.6
T.P	0.25	133.17	12.85	120.32
+25			9.4	123.8
T.P	0.03	120.28	12.92	120.25
+50			6.8	113.5
+75			12.6	107.7
TP	2.04	109.89	12.83	107.45
4			7.5	102.4
+25			10.4	99.5
+50	=24+47	Cañonbine	13.2	96.7
+75			13.8	96.1
5			14.2	95.7
+25			12.9	97.5
+30			1.3	108.6
TP	10.85	120.35	0.39	109.56
+75			9.4	110.9

		120.35		
6			9.5	110.8
+30	@ 38d		10.3	110.0
+60			10.5	109.8
7			10.6	109.7
+50			10.2	110.1
8			8.8	111.8
+25			5.9	114.4
+50			5.2	115.1
+75			7.5	112.8
9			7.7	112.6
+50			5.6	114.7
10			6.7	113.6
+50			6.8	113.5
11			8.1	112.2
+50			7.4	112.9
12			8.1	112.2
			9.4	110.9
TP	0.15	111.04	9.46	110.89

		111.04		
+90			2.3	108.7
13			2.8	108.2
+20			3.0	108.0
+50			2.5	108.5
14			3.8	107.2
+50			9.0	102.0
15			10.2	100.8
+50			13.0	98.0
TP	1.58	99.92	12.70	98.34
16			6.2	93.7
+50			9.9	90.0
17			12.0	87.9
TP	0.09	86.94	13.07	86.85
+25			0.6	86.3
+30			1.6	85.3
+35			5.7	81.2
+40			6.8	80.1

		86.94		
+50			12.8	74.1
TP	0.36	74.50	12.80	74.14
+75			7.3	67.2
+90			13.0	61.5
TP	1.69	63.27	12.92	61.58
18			2.8	60.5
+50			3.8	59.5
19			4.6	58.7
+50	King of Lincoln 35th St.		6.0	57.3
TP	1.65	57.66	7.26	56.01

5/31/10 Hatch Notes Thomas	Line East.	between	& C	from	32d
T.P	12.46	172.92		159.46	
0+00 = El. 32d			6.9	162.0	
T.P.	026	161.84	11.34	161.58	
+25			3.7	158.1	
+50			10.4	151.4	
T.P.	4.18	150.31	12.71	149.13	
+75			5.1	145.2	
1			10.6	139.7	
T.P	2.38	139.72	12.97	137.34	
+25			4.0	135.7	
+50			8.2	131.5	
+75			11.9	127.8	
T.P.	1.12	128.40	12.44	127.28	
2			2.1	126.3	
+25			3.1	125.3	
+50			4.1	124.3	
+75			7.6	120.8	

		128.40		
TP	2.90	118.57	12.73	115.67
3			4.5	114.1
+25			10.8	107.8
+49 = 28+47 Gfrom line.			11.2	107.4
+75			10.5	108.1
4			5.5	113.1
+25			3.7	114.9
+50			4.2	114.4
+75			7.8	110.8
+85			9.1	109.5
5			4 3	114.3
TP	12.44	130.45	0.56	118.01
+25			11.6	118.8
+50			4 5	125.9
T.P.	10.98	141.19	024	130.21
+75			9 8	131.4
6			5.4	135.8

		141.19			
+30			3.4	137.8	
+60			1.7	139.5	
TP	11.20	151.78	0.61	140.58	
7			8.9	142.9	
+50			5.0	136.8	
8			0.0	151.8	
TP	13.90	164.44	0.34	151.44	
+50			5.3	159.1	
9			0.5	163.9	
TP	8.83	173.06	0.21	164.23	
+50			5.7	167.4	
10			3.5	169.6	
+50			4.2	168.9	
11			7.1	166.0	
+50			12.5	160.6	
TP			11.86	161.20	Fence Cor.

Nat. & 16th NW cor. Hd. Spk post, brs. 4.106

N & 16th NE cor. brass plg. 12.52

	+	H.I.	−	
	3.86	7.97		4.11
Nat + "N"			3.87	4.1
+50			4.55	3.4
1			4.72	3.2
+50			4.54	3.4
2			4.42	3.5
+50			4.40	3.5
3+00			4.50	3.4
+50			4.30	3.6
4+00			4.25	3.7
+50			4.20	3.7
5+00			4.10	3.8
+50			4.05	3.9
Inter. 16th			3.70	4.2
+50			5.65	2.3
1+00			6.70	1.2

Commence at Nat. + N. thence E. on alley to 16th thence S. on 16th to alley

1+50		7.30	0.6
2+00		8.10	−0.2
+50		7.50	0.4
3+00		6.05	1.9

0.6 × 24 = 3.0

6 / 7.2 / 18

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TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100.00	0.44	100.00	0.87	99.99	1.31	89
1	99.98	1.75	99.98	2.18	99.97	2.62	99.95	3.05	88
2	99.94	3.49	99.92	3.93	99.91	4.36	99.88	4.80	87
3	99.86	5.23	99.84	5.67	99.81	6.10	99.79	6.54	86
4	99.76	6.98	99.73	7.41	99.69	7.85	99.66	8.28	85
5	99.62	8.72	99.58	9.15	99.54	9.58	99.50	10.02	84
6	99.45	10.45	99.41	10.89	99.36	11.32	99.31	11.75	83
7	99.25	12.19	99.20	12.62	99.14	13.05	99.09	13.49	82
8	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	15.64	98.70	16.07	98.63	16.50	98.56	16.93	80
10	98.48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98.16	19.08	98.08	19.51	97.99	19.94	97.90	20.36	78
12	97.81	20.79	97.72	21.22	97.63	21.64	97.53	22.07	77
13	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	24.19	96.92	24.62	96.81	25.04	96.70	25.46	75
15	96.59	25.88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.82	73
17	95.63	29.24	95.50	29.65	95.37	30.07	95.24	30.49	72
18	95.11	30.90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35.43	69
21	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38.67	67
23	92.05	39.07	91.88	39.47	91.71	39.87	91.53	40.27	66
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	43.84	89.69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	46.95	88.09	47.33	87.88	47.72	87.67	48.10	61
29	87.46	48.48	87.25	48.86	87.04	49.24	86.82	49.62	60
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	52.99	84.57	53.36	84.34	53.73	84.10	54.10	57
33	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	52
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	45
45	70.71	70.71							
Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees
	DEGREES		¾ DEGREE.		½ DEGREE.		¼ DEGREE.		