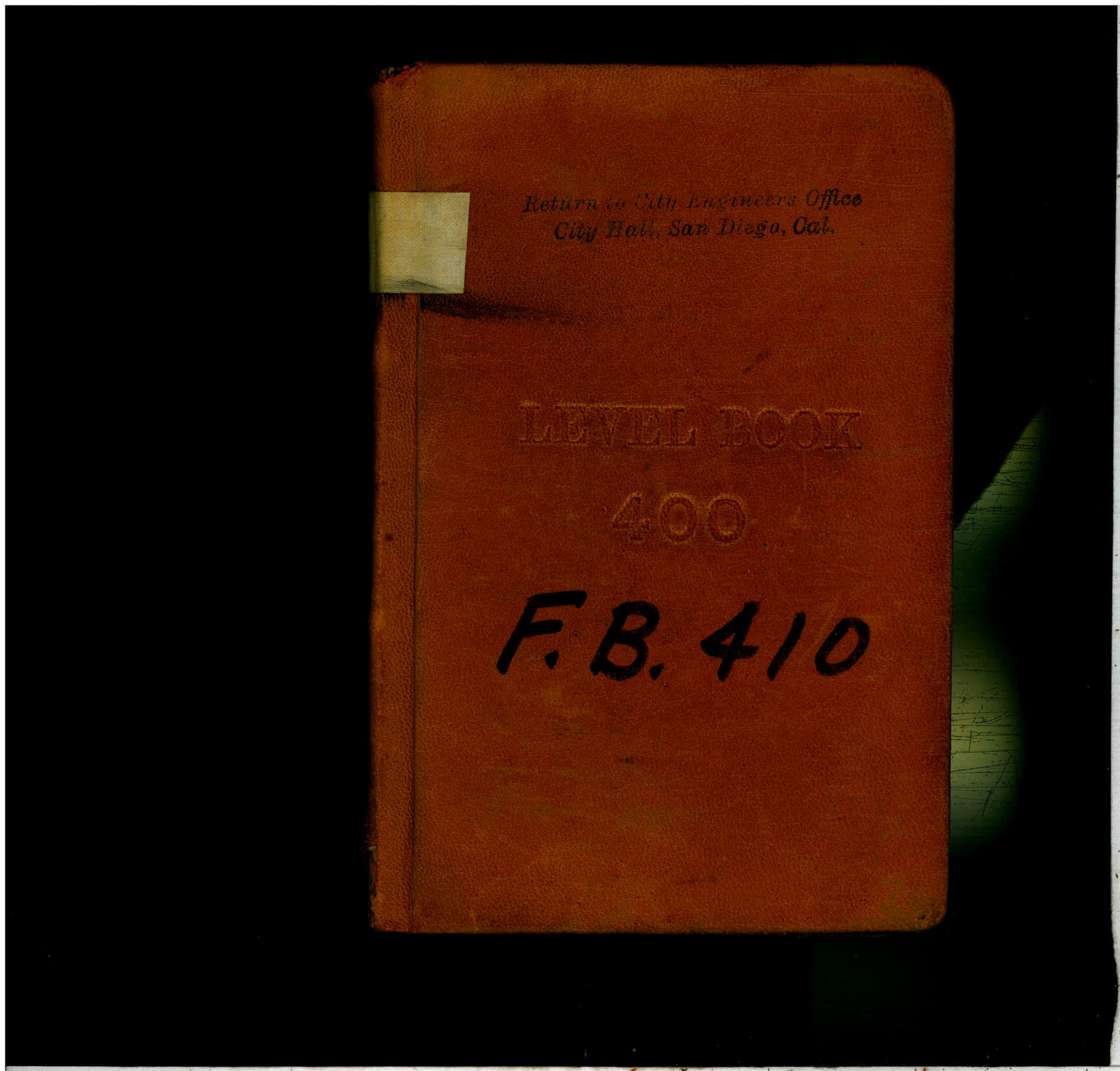
Return to City Engineers Office
City Hall, San Diego, Cal.
LEVEL BOOK
400
F.B. 410

H. S. CROCKER COMPANY
DRAWING MATERIALS AND
SURVEYING INSTRUMENTS
SAN FRANCISCO

410

TABLES FOR EXCAVATIONS AND EMBANKMENTS

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING

Roadway 18 Feet Wide. Slopes 1½ to 1.
For Single Track Excavation.

"Copyright, 1895, by Kueffel & Esser Co."

MICROFILMED
DEC 10 1964

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19 5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

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FROM
Loring's Book Store
SAN DIEGO, CAL.

Xsection of Law St.

Continued from Book 407

100' W of Jewel.

S.P.L.		141.98	18.30	123.7
C			16.50	125.5
¼			15.60	126.4
℄			14.40	127.6
¼			12.70	129.3
C			11.40	130.6
N.P.L.			9.50	132.5

150' W of Jewel

N.P.L.			10.20	131.8
C			11.70	130.3
¼			12.70	129.3
℄			13.60	128.2
¼			14.80	127.2
C			16.40	125.6
S.P.L.			16.20	123.8
T.T.			11.98	130.00

200' W. of Jewel 130.00

S.P.L.	0.72	130.72	8.50	122.2
C			6.80	123.9
¼			6.00	124.7
℄			4.80	125.9
¼			4.10	126.6
C			2.70	128.0
N.P.L.			0.80	129.9

200' S. of Jewel

N.P.L.			1.60	129.7
C			2.70	128.0
¼			4.00	126.7
℄			4.60	126.1
¼			5.40	125.3
C			7.30	123.4
S.P.L.			9.30	121.4
T.T.			4.16	126.56
	3.66	130.22		

300' W of Jewel

S.P.L.	130.22	10.10	120.1
C		8.10	122.1
¼		7.00	123.2
℄		5.90	124.3
¼		4.40	125.8
C		3.40	126.8
N.P.L.		1.20	129.0

350' W. of Jewel

N.P.L.		3.40	126.8
C		6.00	124.2
¼		7.50	122.7
℄		8.80	121.4
¼		10.00	120.2
C		10.40	119.4
S.P.L.		12.30	117.9

400' W of Jewel

S.P.L.	130.22	14.10	116.1
C		11.90	118.3
¼		11.20	119.0
℄		10.20	120.0
¼		9.30	120.9
C		6.10	122.1
N.P.L.		6.30	123.9

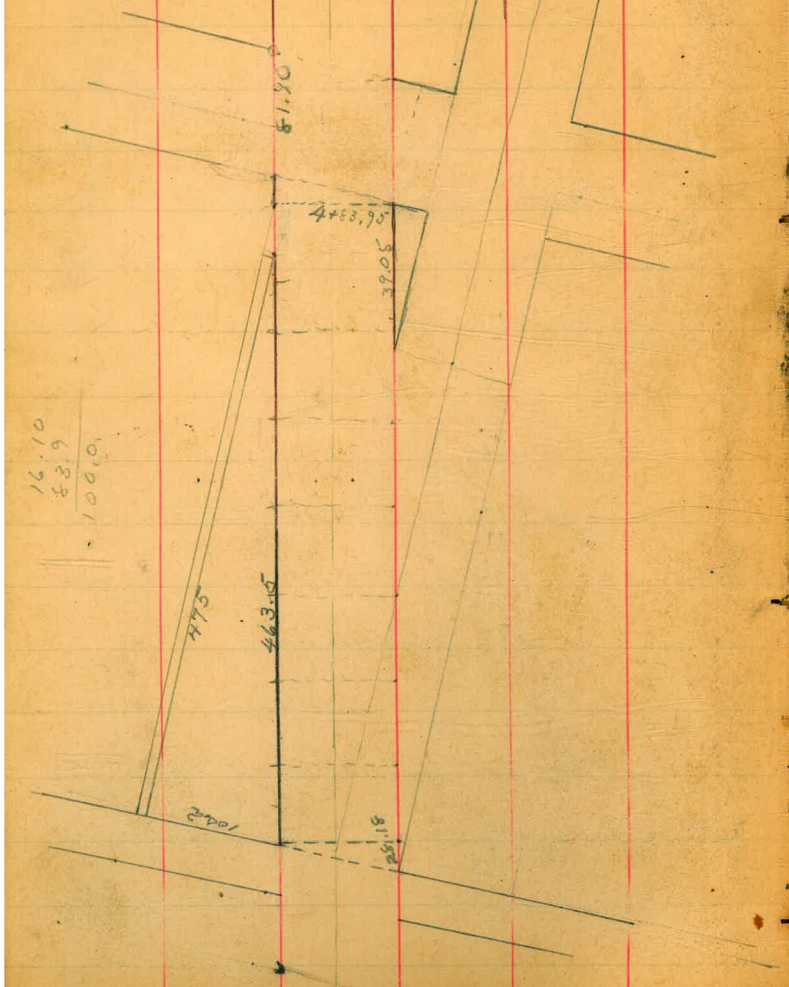
450' W. of Jewel

N.P.L.		9.90	120.3
C		10.90	119.3
¼		11.70	118.5
℄		12.10	118.1
¼		12.90	117.3
C		13.40	116.8
S.P.L.		14.50	115.7

500' W of Jewel

S.P.L.		130.22	16.20	114.0
C			15.20	115.0
¼			14.60	115.6
℄			14.30	115.9
¼			13.70	116.5
C			13.40	116.8
N.P.L.			12.50	117.7

Xsections Grand Ave
Lamont to Pendleton



B.M. Brass Plug N.W. Cor Lamont Grand 50.37

E. Line of Lamont

N.P.L.	1.55	51.92	0.90	51.1 POSTED
C			2.70	49.3
1/4			3.10	48.9
			2.60	49.4
℄ N.P. Track			2.40	49.6
1/4			3.20	48.8
+6			4.10	48.9
+8 N.P. Track			3.30	48.7
+14			4.10	47.9 POSTED
C			4.40	47.6
S.P.L.			4.90	47.1

From N.E. Cor to 28.18' E. of S.E. Cor see Sketch

S.P.L.			4.60	47.4
C			4.60	47.4
4			4.30	47.7
+10 N.P.			3.52	48.5
+2			4.26	47.7
+20			3.90	48.1

℄ 1/4	51.92	3.30	48.6	
+15		2.70	49.2	
N. ℄ Rail		2.42	49.5	
+2		2.50	49.4	
℄		3.10	48.8	
+18		2.90	49.0	
C		1.70	50.2	
N.P.L		0.90	51.0	
	50' E. of Lamont			
N.P.L.		1.70	50.2	
C		3.50	48.4	
℄		3.80	48.1	
+19		3.70	48.2	
N.R. ℄		2.96	48.9	
+6		3.70	48.2	
1/4		4.20	47.7	
C		4.80	47.1	
℄ Rail		4.09	47.8	

+8	51.92	4.90	47.0	
S.P.L.		4.90	47.0	
	100' E. of Lamont			
S.P.L. 2'Sa/Rail		5.60	46.3	
+8, Rail		4.61	47.3	
+10		5.00	46.9	
+15		4.60	47.3	
C		5.20	46.7	
℄		4.30	47.6	
+7		5.20	46.7	
+15		4.30	47.6	
℄ Rail		3.50	48.4	
+2		4.30	47.6	POSTED
℄		4.70	47.2	
C		4.30	47.6	
N.T.L		3.00	48.9	

	150' E of Lamont			
N.P.L	51.92	4.50	47.4	
C		5.00	46.9	
1/4		5.10	46.8	
+14		4.40	47.5	
+17		5.00	46.9	
℄ N. Rail		3.93	48.0	
+8		4.50	47.4	
1/4		4.80	47.1	
C		5.40	46.5	
+15		4.70	47.2	
S.P.L.		6.30	45.6	
	200' E of Lamont			
S.P.L		5.60	46.3	
C		5.90	46.0	
1/4		5.70	46.2	
+14		5.10	46.8	
℄ N. Rail		4.38	47.5	
+2	51.92	4.80	47.1	
1/4		5.40	46.5	
C		5.30	46.6	
N.P.L		4.60	47.3	
	250' E of Lamont			
N.P.L.		4.80	47.1	
C		5.40	46.5	
1/4		5.60	46.3	
+19		5.60	46.3	
℄ N. Rail		4.75	47.1	
+8		5.50	46.4	
1/4		6.60	45.3	
C		6.60	45.3	POSTED
S.P.L		6.46	45.5	

300' E of Lamont

S.P.L.	51.92	6.>8	45.2
C		>.10	44.8
1/4		6.60	45.3
+14		5.90	460
℄ N. Rail		5.16	46.7
+2		6.10	45.8
1/4		5.60	46.3
C		5.60	46.3
N.P.L.		4.>0	46.2

350' E of Lamont

N.P.L.		4.20	47.7
C		5.40	46.5
1/4		6.30	45.6
+19		6.30	45.6
℄ N. Rail	POS---)	5.50	46.4
+8		6.40	45.5
1/4		6.8o	45.1
C		7.5o	44.4
S.P.L.		>.5o	44.4

400' E of Lamont

S.P.L	51.92	8.10	43.8
C		>.>o	44.2
1/4		>.20	447
+14		6.60	45.3
℄ N. Rail		5.>5	46.1
+2		6.50	45.4
1/4		6.40	45.5
C		6.10	45.8
N.P.L.		4.60	47.3

4+44.9 E of Lamont

N.P.L.		4.20	47.7
+4		5.>o	46.2 POS---)
C		6.20	45.7
1/4		6.60	45.3
+19		6.>8	45.2
℄ N. Rail		5.9>	45.9
+8		6.>o	45.2

1/4		51.92	7.40	44.5
C			8.00	43.9
S.P.L			8.60	43.3
T.P.			8.47	43.45
	4+83.95 E. of Lamont			See Sketch Rt. Ls
S.P.L.	5.74	49.19	5.70	43.5
C			5.60	43.6
1/4			5.00	44.2
+14			4.30	44.9
℄ N. Rail			3.45	45.7
+2			4.10	45.1
1/4			4.10	45.1
C			3.80	45.4
+17			3.30	45.9
N.P.L.			1.30	47.9

W. P.L. of Morell

N.P.L.	49.19	2.40	46.8
+4		3.30	45.9
C		4.00	45.2
1/4		4.20	45.0
+19		4.00	45.2
℄ N. Rail		3.50	45.7
+8		4.30	44.9
1/4		5.00	44.2
C		5.50	43.7
S.P.L.		5.70	43.5

W. Curb Line Morell

S.P.L.		5.90	43.3
C		5.50	43.7
1/4		5.20	44.0
+14		4.50	44.7
℄ N.R.		3.64	45.6
+2		4.10	45.1

POSTED

1/4		49.19	4.20	45.0
C			4.00	45.2
+18			3.40	45.8
N.P.L.			2.20	47.0
	N. 1/4 of Morell			
N.P.L.			2.60	46.6
C			3.60	45.4
1/4			3.60	45.4
+19			3.80	45.4
℄ N.Rail			3.77	45.4
+8			4.00	45.2
1/4			4.90	44.3
C			5.60	43.6
S.P.L.			5.80	43.9
	℄ of Morell			
S.P.L.			5.90	43.8
℄			5.70	43.5

1/4			4.80	44.4
+14			3.70	45.5
℄ N.Rail			3.68	45.5
+2			3.70	45.5
1/4			3.90	45.3
C			3.90	45.3
N.P.L.			2.60	46.6
	E. 1/4 of Morell			
N.P.L.			2.60	46.6
C			3.60	45.9
1/4			4.00	45.2
+19			3.80	45.9
℄ Rail			3.71	45.5
+8			3.90	45.3
1/4			4.70	44.5
C			5.70	43.5
S.P.L.			5.90	43.3

E Curb Line of Morell

S.P.L.	49.19	6.00	43.2
C		5.70	43.5
1/4		5.20	44.0
+14		4.00	45.2
℄ N. Rail		3.72	45.5
+8		4.00	45.2
1/4		4.30	44.9
C		3.80	45.4
N.P.L.		2.70	46.5

E.P.L. of Morell

N.P.L.		1.90	47.3
+8		3.70	45.5
C		4.00	45.2
1/4		4.30	44.9
+19		4.60	44.6
℄ N. Rail		3.80	45.4
+8		4.60	44.6
1/4		5.30	43.9
C		5.70	43.5
S.P.L.		5.60	43.6

on Line from N.E. Cor. to +28.18 on S

S.P.L.		5.60	43.6
C		5.80	43.4
1/4		5.60	43.6
+14		4.50	44.7
℄ N. Rail		3.84	45.4
+2.		4.60	44.6
1/4		4.40	44.8
C		4.00	45.2
+16		3.60	45.6
N.P.L.		1.90	47.3

50' E of Morell POST

N.P.L.		2.70	46.5
C		4.30	44.9
+10		8.50	40.7
1/4		4.80	44.9

+19		49.19	4.60	44.6
℄ N. Rail			3.94	45.3
+8			4.70	44.5
¼			5.20	44.0
C			5.80	43.4
S.P.L.			5.70	43.5
	100' E of	Morell		
S.P.L.			5.70	43.5
C			5.80	43.4
¼			5.50	43.7
+14			4.70	44.5
℄ N. Rail			4.04	45.2
+2			4.60	44.6
¼			4.70	44.5
C			4.70	44.5
+19			4.00	45.2
N.P.L.			3.80	46.2
+1				

	150' E of	Morell		
N.P.L.			4.30	44.9
C			4.70	44.5
¼			4.80	44.4
+19			4.70	44.5
℄ N. Rail			4.09	45.1
+7			4.90	44.3
¼			5.60	43.6
C			5.90	43.3
S.P.L.			6.40	42.8
	200' E of	Morell		
S.P.L.			7.10	42.1
C			6.00	43.2
¼			5.80	43.4
+14			5.00	44.2
℄ N. Rail			4.06	45.1
+2			4.80	44.4
¼			4.80	44.4

POSTED

C	49.19	4.80	44.4
N.P.L.		3.90	45.3
	250' E of Morell		
N.P.L.		4.70	44.5
C		4.70	44.5
1/4		4.70	44.5
+10		5.70	43.5
+19		4.80	44.4
℄ N. Rail		4.06	45.1
+7		4.90	44.3
1/4		5.50	43.7
C		5.80	43.4
S.P.L.		7.20	42.0
	300' E of Morell		
S.P.L.		8.70	42.2
+5		6.90	42.3
C		5.90	43.3
1/4		5.60	43.6
+14		5.00	44.2
N ℄ Rail		4.11	45.1
+2		4.90	44.3
+7		5.80	43.4
1/4		5.90	43.3
C		4.80	44.4
N.P.L.		5.20	44.0
	350' E. of Morell		
N.P.L.		4.80	44.4
C		4.90	44.3
1/4		4.70	44.5
+14		5.30	43.9
+19		4.80	44.4
℄ N. Rail		4.08	45.1
+7		5.00	44.2
1/4		5.80	43.4

POSTED

C.		49.19	6.80	43.1
+13			6.40	92.8
S.P.L.			8.30	90.9
	400' E of Morell			
S.P.L.			6.50	92.7
C			5.90	93.3
1/4			6.30	93.9
+14			4.80	99.4
& N. Rail			4.02	95.2
+2			4.80	99.4
1/4			4.90	99.3
C			4.70	99.5
N.P.L.			4.70	99.5
T.P.			4.24	44.95
	450' E. of Morell			
N.P.L.	6.76	51.71	6.30	
C			6.70	45.0

1/4		51.71	6.90	44.8
+19			7.30	99.4
& N. Rail			6.53	95.2
+7			7.30	99.4
1/4			7.40	99.3
C			7.80	93.9
S.P.L.			7.90	93.8
	483.9' E. of Morell			
S.P.L.			6.50	95.2
+3			7.70	99.0
C			7.30	99.4
1/4			6.70	95.0
+14			7.40	99.3
& N. Rail			6.60	95.1
+2			6.30	95.4
+10			6.20	95.5
1/4			6.00	95.7
C			6.10	95.6
+15			5.70	96.0
N.P.L.			4.90	96.8

POSTED

E. P. L. of Noyes

N. P. L.	51.71	4.40	97.3
C		5.60	96.1
1/4		5.50	96.2
+10		5.40	96.3
+19		7.30	99.9
℄ N. Rail		6.62	95.1
+7		7.40	99.3
+18		6.30	95.9
1/4		6.40	95.8
C		7.20	94.5
+~~15~~		7.70	99.0
S. P. L.		~~6.60~~	95.1

E. C. L. of Noyes

S. P. L.		6.70	95.0
C		6.70	95.0
1/4		6.00	95.7
+9		6.00	95.7
+14		7.40	99.3

℄ N. Rail		6.62	95.1
+8		7.40	99.3
+7		4.70	97.0
1/4		5.00	96.7
C		4.80	96.9
+18		4.20	97.5
N. P. L.		2.70	99.0

E 1/4 of Noyes

N. P. L.		1.20	50.5
+3		3.40	48.3
C		4.50	47.4
1/4		4.70	97.0
+12		3.90	97.8
+19		7.30	99.4
℄ N. Rail		6.63	95.1
+7		7.40	99.3
+13		5.70	96.10
1/4		6.10	95.6

C	52.71	6.70	45.0
S.P.L.		6.80	44.9
	℄ of Noyes		
S.P.L.		7.30	44.4
C		6.60	45.1
1/4		5.70	46.0
+6		5.60	46.1
+14		7.30	44.4
℄ N. Rail		6.64	45.1
+2		7.20	44.5
+10		3.70	48.0
1/4		4.30	47.4
C		4.00	47.2
+18		3.20	48.5
N.P.L.		2.10	49.6

E. 1/4 of Noyes

N.P.L.		1.50	50.2
+4		3.40	48.3
C		4.30	47.4
1/4		4.30	47.4
+14		4.70	47.0
+19		7.00	44.7
℄ N. Rail		6.70	45.0
+7		7.30	44.4
+12		5.40	46.3
1/4		5.80	45.9
C		6.50	45.2
S.P.L.		7.00	44.7
	E.C.L. of Noyes		
S.P.L.		7.10	44.6
C		6.40	45.3
1/4		5.50	46.2
+9		5.30	46.4

POSTED

+14	51.71	7.40	44.3
℄ N. Rail		6.69	45.0
+2		7.20	44.5
+10		3.60	48.1
¼		4.10	47.6
C		4.30	47.4
+18		2.70	49.0
N.P.L.		1.20	50.5
E.P.L. of Noyes			
N.P.L.		1.30	50.4
+3		2.60	49.1
C		4.00	47.7
¼		4.00	47.7
+9		3.80	47.9
+19		7.30	44.4
℄ N. Rail		6.70	45.0
+7		7.30	44.4

+16	5.40	46.3
¼	5.40	46.3
C	6.50	45.2
S.P.L.	7.10	44.6
on Line from N.E. Cor to 0+28.18 on S		
S.P.L.	7.00	44.7
C	6.80	44.9
¼	5.80	45.9
+8	5.70	46.0
+14	7.60	44.1
℄ N. Rail	6.73	45.0
+2	7.40	44.3
+10	4.40	47.3
¼	4.10	47.6
C	4.00	47.7
+18 N.P.L.	2.70	49.0
N.P.L.	1.30	50.4

POSTED

50' E. of Noyes

N.P.L.	51.71	1.90	49.8
+3		3.20	48.5
C		4.10	47.6
1/4		4.60	47.1
+10		4.10	47.6
+19		7.60	44.1
& N. Rail		6.91	44.8
+7		7.60	44.1
+14		5.60	46.1
3/4		5.80	45.9
C		6.50	45.2
S.P.L.		6.90	44.8

100' E of Noyes

S.P.L.		6.30	45.4
C		6.00	45.7
1/4		5.90	45.8
+12		5.90	45.8
+14		7.90	43.8
& N. Rail		7.21	44.5
+2		7.90	43.8
+10		4.60	47.6
1/4		4.50	47.2
C		4.60	47.1
N.P.L.		3.70	48.0

150' E of Noyes ~~3.70~~

N.P.L.		3.80	47.9
C		5.20	46.5
1/4		5.10	46.6
+9		4.70	47.0
+19		8.20	43.5
& N. Rail		7.58	44.1
+7		8.20	43.5
+11		5.90	45.8
1/4		5.60	46.1

POSTED

C		51.71	6.40	45.3
+18			6.70	45.0
S.P.L.			5.50	46.2
	200' E. of Noyes			
S.P.L.			7.60	44.1
C			7.20	44.5
1/4			6.40	45.3
+6			6.50	45.2
+14			8.80	42.9
℄ N. Rail			8.00	43.6
+2			8.60	43.1
+10			5.60	46.1
1/4			6.20	45.5
C			6.20	45.5
N.P.L.			5.10	46.6
	250' E of Noyes			
N.P.L.			5.70	46.0
+4			6.80	44.9

C			7.20	44.5
1/4			7.20	44.5
+9			6.80	44.9
+19			9.30	42.4
℄ N. Rail			8.74	43.0
+7			9.30	42.4
+11			7.80	44.4
1/4			7.60	44.1
C			8.40	43.3
S.P.L.			8.70	43.0
	300' E of Noyes			
S.P.L			9.70	42.0
C			9.30	42.4
1/4			8.60	43.1
+4			8.80	42.9
+6			11.00	40.7
+14			10.30	41.4

℄ N. Rail		51.71	9.50	42.2
+ 2			10.20	41.5
+ 10			9.80	41.9
+ 12			9.50	42.2
¼			9.60	42.1
C			9.80	41.9
N. P.L.			6.30	45.4
	300' E of Noyes			
T.P.			10.46	41.25
N.P.L.	3.15	44.40	0.20	44.2
+ 4			1.30	43.1
C			1.70	42.7
¼			1.50	42.9
+ 6			1.30	43.1
+ 15			3.50	40.9
+ 19			3.60	40.8
℄ N. Rail			2.90	41.5

+ 7		44.40	3.60	40.8
+ 13			3.70	40.7
+ 17			1.90	42.5
¼			2.60	41.8
C			2.80	41.6
S.P.L.			3.20	41.2
	400' E of Noyes			
S.P.L			4.20	40.2
C			4.20	40.2
¼			3.60	40.8
+ 9			3.00	41.4
+ 11			4.60	39.8
+ 14			4.40	40.0
℄ N. Rail			3.68	40.7
+ 2			4.40	40.0
+ 7			4.50	39.9
+ 10			2.80	41.6

POSTED

¼	44.40	2.80	41.6
C		3.10	41.3
N.P.L.		1.80	42.6
450' E. of Noyes			
N.P.L.		1.80	42.6
+3		3.20	41.2
C		4.20	40.2
¼		3.90	40.5
+11		3.90	40.5
+15		5.30	39.1
+19		5.10	39.3
℄ N.Rail		4.44	40.0
+7		5.10	39.3
+15		5.50	38.9
+16		4.50	39.9
¼		4.70	39.7
C		5.40	39.0
+19		6.00	38.4
S.P.L.		5.30	39.1

4783.9 E. of Noyes

S.P.L.	5.70	38.7
+3	6.70	37.7
C	6.20	38.2
¼	5.80	38.6
+14	5.60	38.8
℄ N.Rail	4.90	39.4
+2	5.50	38.9
+6	5.70	38.7
+10	4.70	39.7
¼	4.80	39.6
C	4.90	39.5
+17	3.90	40.5
N.P.L.	2.70	41.7

POSTED

N.P.L. of Olney

N.P.L.	4.40	40.0
C	5.20	39.2
¼	5.20	39.2

+10	44.40	5.10	39.3
+12		5.90	38.6
+19		5.70	38.7
℄ N. Rail		5.11	39.3
+7		5.80	38.6
¼		5.50	38.9
C		6.20	38.2
S.P.L.		5.70	38.7
	W. C.L. of Olney		
S.P.L.		6.30	37.9
C		6.70	37.7
¼		6.30	38.1
+14		6.10	38.3
℄ N. Rail		5.45	39.0
+2		6.10	38.3
¼		5.70	38.7
C		5.60	38.8
N.P.L.		5.30	39.1

W. ¼ of Olney

N.P.L.		5.10	39.3
C		5.70	38.7
¼		5.80	38.6
+19		6.20	38.2
℄ N. Rail		5.61	38.8
+7		6.30	38.1
¼		6.50	37.9
C		6.80	37.6
S.P.L.		6.60	37.8
	℄ of Olney		
S.P.L.		7.10	37.3
C		7.00	37.4
¼		7.20	37.2
+14		6.40	38.0
℄ N. Rail		5.75	38.6
+2		6.00	38.4
¼		5.80	38.6

POSTED

C	44.40	5.90	38.5
N.P.L.		5.70	38.7

E ¼ of Olney

N.P.L.		6.00	38.4
C		6.00	38.4
¼		5.90	38.5
+19		6.10	38.3
℄ N. Rail		5.87	38.5
+7		6.20	38.2
¼		7.20	37.2
C		7.20	37.2
S.P.L.		7.70	36.7

E.C.L. of Olney

S.P.L.		7.60	36.8
C		7.50	36.9
¼		7.20	37.2
+14		6.30	38.1
℄ on Rail		6.00	38.4
+2		6.30	38.1
¼		6.20	38.2
C		6.30	38.1
N.P.L.		6.20	38.2

E.P.L. of Olney

N.P.L.		6.60	37.8
C		6.60	37.8
¼		6.70	37.7
+19		6.90	37.5
℄ on Rail		6.31	38.1
+7		6.90	37.5
¼		7.60	36.6
C		7.90	36.5
S.P.L.		8.00	36.4

POST

on Line from 0+28.1 ons to N. E Cor

S.P.L.		44.40	6.50	35.9
C			6.40	36.0
¼			7.90	36.5
+14			7.20	37.2
℄ on Rail.			6.45	37.9
+2			7.10	37.3
¼			6.90	37.5
C			6.70	37.7
N.P.L.			6.60	37.8
	50' E of Olney			
N.P.L.			7.10	37.3
C			7.40	37.0
¼			7.60	36.8
+19			7.90	36.5
℄ N. Rail			7.15	37.2
+7			7.90	36.5
¼			6.60	35.9

C		44.40	9.20	35.2
S.P.L.			9.70	34.7
T.P.			7.35	37.02
	100' E of Olney			
S.P.L.	2.26	39.26	6.40	33.9
C			4.60	34.6
¼			4.10	35.2
+14			3.40	35.9
℄ N. Rail			2.65	36.6
+2			3.40	35.9
¼			2.90	36.4
C			2.80	36.5
N.P.L.			2.60	36.7
	150' E of Olney			
N.P.L.			3.30	36.0
C			3.70	35.6
¼			3.70	35.6

POSTED

+19		39.28	4.10	35.2
℄ N. Rail			3.84	36.0
+7			4.10	35.2
¼			4.90	35.4
C			5.40	33.9
S. P. L.			5.80	33.5
	200' E of Olney			
S. P. L.			6.90	32.4
C			6.20	33.1
¼			5.40	33.9
+14			4.90	34.4
℄ N. Rail			4.12	35.2
+2			4.80	34.5
¼			4.60	34.7
C			4.70	34.6
N. P. L.			4.20	35.1

	200' E of Olney			
N. P. L.			4.10	35.2
+3			5.20	34.1
C			5.70	33.6
¼			5.40	33.9
+19			5.70	33.6
℄ N. Rail			4.85	34.4
+7			5.60	33.7
¼			6.30	33.0
C			7.10	32.2
S. P. L.			7.70	31.6
	300' E of Olney			
S. P. L.			8.50	30.8
C			7.80	31.5
¼			7.30	32.0
+14			6.80	32.8
℄ N. Rail			5.62	33.7
+2			6.40	32.9

POSTED

1/4		39.28	6.30	33.0
C			6.50	32.8
+17			6.90	33.4
N.P.L.			4.80	34.5
	350' E of Olney			
N.P.L.			6.90	33.4
+4			7.00	32.8
C			7.20	32.1
1/4			7.20	32.1
+19			7.10	32.2
& N. Rail			6.39	32.9
+7			7.30	32.0
1/4			7.90	31.4
C			8.50	30.8
S.P.L.			9.60	29.7
	400' E of Olney			
S.P.L.			10.50	28.8

+6			9.60	29.7
C			9.20	30.1
1/4			9.20	30.1
+14			7.90	31.4
& N. Rail			7.23	32.1
+2			8.10	31.2
1/4			7.60	31.5
C			8.30	31.0
N.P.L.			6.90	32.4
	450' E of Olney			
N.P.L.			8.70	30.6
C			9.20	30.1
1/4			9.20	30.1
+18			8.90	30.4
N. Rail +20			7.99	31.3
+6			8.70	30.6
+11 X			10.00	29.3

& 145' of N. Rail.

POSTED

1/4		39.28	10.00	29.3	
C			10.60	28.7	
S.P.L.			12.10	27.2	
	439.9 E of Olney				
S.P.L.			13.20	26.1	
C			11.20	28.1	
1/4			10.70	28.6	
+10			10.60	28.7	℄ 2±'S of N. Rail
+16			9.10	30.2	
℄ +2			8.44	30.9	
+4			9.00	30.3	
+8			10.20	29.1	
+18			~~9.50~~ 10.90	28.4	
1/4			~~10.9~~ 9.50	29.8	
C.			9.20	30.1	
N.P.L.			9.50	29.8	

W.P.L. of Pendleton

N.P.L.		39.28	9.60	29.7	
C			9.70	29.6	
1/4			10.40	28.9 POSTED	
+5			10.60	28.7	
+16			5.50	33.8	
N Rail			8.66	30.6	℄ = 3±'S of N. Rail
℄ +5			9.30	30.0	
+10			10.70	28.6	
C			11.00	28.3	
1/4			11.60	27.7	
S.P.L.			13.20	26.1	
B.M			8.93	30.35	30.5/3

X sec. of Lamont St. Grande Ave to Pacific Ave

S. P. L. of Grand Ave [50.3] By

E.P.L.	0.93	51.30	3.70	47.6
C			4.00	47.3
¼			4.00	47.3
℄			4.00	47.3
¼			4.50	46.8
C			3.30	48.0
W.P.L.			2.20	49.1

~~30~~ 20' S. of Grande

W.P.L.			2.80	48.5
C			4.10	47.2
¼			5.20	46.1
℄			5.40	45.9
¼			5.10	46.2
C			4.90	46.4
E.P.L.			4.70	46.6

POSTED

~~100~~ 70' S. of Grande

E.P.L.	51.30	6.30	45.0
C		6.00	45.3
¼		6.40	44.9
℄		6.00	45.3
¼		6.30	45.0
C		6.20	45.1
W.P.L.		5.00	46.3

~~150~~ 120' S. of Grande

W.P.L.		5.30	46.0
C		6.40	44.9
¼		6.70	44.6
℄		6.70	44.6
¼		6.90	44.4
C		7.30	44.0
W.P.L.		7.20	44.1

POST

~~120~~ 200' S. of Grand

E.P.L.	57.30	8.50	42.8
C		8.30	43.0
¼		7.70	43.6
¢		7.40	43.9
¼		7.50	43.8
C		7.00	44.3
W.P.L		5.90	45.4

280' S. of Grand

W.P.L.		6.50	44.8
C		7.70	43.6
¼		8.20	43.1
¢		8.00	43.3
¼		8.70	42.6
C		9.90	41.4
E.P.L		9.50	41.8

270' S. of Grande = N.P.L. of Thomas

E.P.L	57.30	10.20	41.1
C		9.80	41.5
¼		9.00	42.3
¢		8.40	42.9
¼		8.50	42.8
C		7.40	43.9
W.P.L		7.30	44.0

N.C.L. ~~N. ¼~~ of Thomas

W.P.L.		7.40	43.9
C		8.20	43.1
¼		8.80	42.5
¢		8.70	42.6
¼		9.30	42.0
C		10.40	39.9
E.P.L.		11.00	40.3

N. ¼ of Thomas

E.P.L.	51.30	10.80	39.5
C		10.50	39.8
¼		9.40	41.9
¢		8.70	42.6
¼		8.90	42.4
C		8.90	42.4
W.P.L.		7.80	43.5

¢ of Thomas

W.P.L.		8.00	43.3
C		9.00	43.3
¼		9.00	43.3
¢		8.80	42.5
¼		9.50	41.8
C		10.10	41.2
E.T.L.		10.50	39.8

S. ¼ of Thomas

E.T.L.	51.30	10.80	39.5
C		10.20	41.1
¼		9.50	41.8
¢		8.90	42.4
¼		9.10	42.2
C		9.20	42.1
W.T.L.		8.00	43.3

SC.L. of Thomas

W.T.L.		8.50	42.8
C		9.10	42.2
¼		9.10	42.2
¢		9.00	42.3
¼		9.50	41.5
C		10.70	39.6
E.T.L.		11.10	40.2

S.P.L. of Thomas				
E.P.L.		51.30	11.00	46.3
C			10.70	39.6
¼			10.00	41.3
℄			9.30	42.0
¼			9.50	41.8
C			9.80	41.5
W.P.L.			8.10	43.2
T.P.			6.82	42.48
20' S. of Thomas				
W.P.L.	3.75	46.23	3.10	43.1 (40.66)
C	5.89	46.55	4.70	41.9
¼			5.00	41.6
℄			4.80	41.8
¼			5.50	41.1
C			6.20	40.4
E.P.L.			6.60	40.0
T.P.		46.23	5.57	40.66

70' S. of Thomas				
E.P.L.		46.55	7.80	39.8
C			6.90	39.7
¼			6.20	40.4
℄			5.40	41.2
¼			5.80	40.8
C			5.40	41.2
W.P.L.		46.23	3.90	43.3
120' S. of Thomas				
W.P.L.			4.20	42.4
C		46.55	5.30	41.3
¼			5.90	40.7
℄			5.80	40.8
¼			6.50	40.1
C			7.10	39.5
E.P.L.			8.00	38.6

	170' S. of Thomas			
E.P.L.		46.65	7.90	38.7
C			7.30	39.3
¼			6.50	40.1
¢			5.70	40.9
¼			5.80	40.8
C			5.70	40.9
W.P.L.		46.23	4.00	42.6
	220' S. of Thomas			
W.P.L.			4.20	
C		46.65	5.50	41.1
¼			5.80	40.8
¢			5.60	41.0
¼			6.30	40.3
C			7.20	39.4
E.P.L.			7.80	38.8

	270' S. of Thomas = N.P.L. of Reed			
E.P.L.		46.65	7.50	39.1
C			6.90	39.7
¼			6.20	40.4
¢			5.70	40.9
¼			5.90	40.7
C			5.60	41.0
W.P.L.		46.23	4.60	42.0
	N.C.L. of Reed			
W.P.L.		46.65	5.10	41.5
C			6.00	40.6
¼			5.90	40.7
¢			5.50	41.1
¼			6.10	40.5
C			7.20	39.4
E.P.L.			7.90	38.7

POOR COPY

N. ¼ of Reed

E.P.L.	46.55	7.50	39.1
C		7.00	39.6
¼		5.90	40.7
¢		5.50	41.1
¼		5.90	40.7
C		5.70	40.9
W.P.L.		4.80	41.8

¢ of Reed

W.P.L.		5.20	41.4
C		5.40	41.2
¼		5.70	40.9
¢		5.40	41.2
¼		5.70	40.9
C		6.50	40.1
E.P.L.		6.80	39.8
T.P.		5.11	41.44
	4.54	45.98	

S. ¼ of Reed

E.P.L.	45.98	6.80	39.8
C		5.70	40.3
¼		5.10	40.9
¢		4.80	41.2
¼		5.10	40.9
C		5.40	40.6
W.P.L.		4.50	41.5

S.C.L. of Reed

W.P.L.		4.50	41.5
C		4.90	41.1
¼		5.10	40.9
¢		4.80	41.2
¼		5.00	41.0
C		6.00	40.0
E.P.L.		6.10	39.9

S. P. L. of Reed

E. P. L.	45.98	5.90	40.1
C		5.70	40.3
¼		4.90	41.1
℄		4.90	41.1
¼		5.20	40.8
C		5.20	40.8
W. P. L.		4.60	41.4

20' S. of Reed

W. P. L.		4.60	41.4
C		5.20	40.8
¼		5.00	41.0
℄		4.70	41.3
¼		4.80	41.2
C		5.60	40.4
E. P. L.		6.00	40.0

40' S. of Reed

E. P. L.		5.70	40.3
C		5.50	40.5
¼		4.70	41.3
℄		4.70	41.3
¼		5.20	40.8
C		5.40	40.6
W. P. L.		5.00	41.0

120' S. of Reed

W. P. L.		4.90	41.1
C		5.30	40.7
¼		5.20	40.8
℄		4.80	41.2
¼		4.90	41.1
C		5.30	40.7
E. P. L.		5.00	41.0

	170' S. of Reed		
E.P.L.	45.98	5.50	40.5
C		5.60	40.4
1/4		5.10	40.9
¢		4.90	41.1
1/4		5.30	40.7
C		5.60	40.4
W.P.L		5.00	41.0
	220' S. of Reed		
W.P.L.		5.10	40.9
C		5.60	40.4
1/4		5.40	40.6
¢		4.90	41.1
1/4		5.30	40.7
C		5.60	40.2
E.P.L.		5.50	40.5

270' S. of Reed = N.P.L. of Oliver			
E.P.L.		5.80	40.2
C		6.00	40.0
1/4		5.50	40.5
¢		5.20	40.8
1/4		5.50	40.5
C		5.90	40.1
N.P.L.		5.30	40.7
	N.		
	N.C.L. of Oliver		
W.P.L.		5.50	40.5
C		5.60	40.2
1/4		5.60	40.4
¢		5.20	40.8
1/4		5.50	40.5
C		6.20	39.8
E.P.L.		6.10	39.9

N. ¼ of Oliver

E.P.L.	45.98	6.10	39.9
C		6.40	39.6
¼		5.60	40.4
℄		5.20	40.8
¼		5.60	40.4
C		5.90	40.1
W.P.L.		5.50	40.5

℄ of Oliver

W.P.L.		5.60	40.4
C		5.90	40.1
¼		5.70	40.3
℄		5.30	40.7
¼		5.70	40.3
C		6.00	40.0
E.P.L.		6.00	40.0

S. ¼ of Oliver

E.P.L		6.40	39.6
C		6.20	39.8
¼		5.60	40.4
℄		5.40	40.6
¼		5.80	40.2
C		6.00	40.0
W.P.L.		5.70	40.3

SCL of Oliver

W.P.L		5.80	40.2
C		6.10	39.9
¼		5.80	40.2
℄		5.50	40.5
¼		5.80	40.2
C		6.40	39.6
E.P.L.		6.40	39.6

S.P.L. of Oliver

E.P.L.		45.98	6.20	39.8
C			6.50	39.5
¼			5.90	40.1
℄			5.80	40.2
¼			6.20	39.8
C			6.30	39.7
W.P.L.			6.00	40.0
	50'	S. of Oliver		
W.P.L			6.50	39.5
C			6.10	39.3
¼			6.10	39.3
℄			6.40	39.6
¼			6.60	39.4
C			7.30	38.7
E.P.L			7.10	38.9

100' S of Oliver

E.T.P.		46.98	7.90	38.1
C			7.80	38.1
¼			7.60	38.8
℄			7.40	38.6
¼			7.70	38.3
C			7.80	38.2
W.T.P.L.			7.60	38.4
T.P.			8.50	37.48
	150'	S. of Oliver		
W.P.L.	3.71	41.19	3.82	37.4
C			4.40	36.8
¼			4.00	37.2
℄			3.70	37.5
¼			3.90	37.3
C			4.40	36.8
E.T.L			4.20	37.0

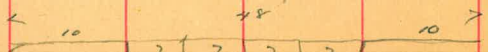
200' S. of Oliver

E.P.L.	41.19	5.30	35.9
C		5.60	35.6
1/4		5.10	36.1
℄		5.00	36.2
1/4		5.20	36.0
C		5.40	35.8
W.P.L.		4.90	36.3

262± S. of Oliver = N.P.L. of Pacific

Pacific = 48' Wide 10' Walks

W.P.L.	6.80	34.4
C	6.80	34.4
1/4	7.00	34.2
℄	6.60	34.6
1/4	6.90	34.3
C	7.30	33.9
E.P.L.	7.10	34.1



N. C.L. of Pacific

E.P.L.	7.90	33.3
C	8.00	33.2
1/4	7.30	33.9
℄	6.80	34.4
1/4	7.10	34.1
C	7.30	33.9
W.P.L.	7.00	34.2

N. 1/4 of Pacific

W.P.L.	7.20	34.0
C	7.40	33.8
1/4	7.30	33.9
℄	6.90	34.3
1/4	7.40	33.8
C	8.00	33.2
E.P.L.	7.70	33.5

POSTED

℄ of Pacific

E.P.L.	41.19	7.90	33.3
C		8.00	33.2
1/4		7.40	33.8
℄		7.10	34.1
1/4		7.60	33.6
C		7.50	33.7
W.P.L.		7.30	33.9

S 1/4 of Pacific

W.P.L.		7.50	33.7
C		7.70	33.5
1/4		7.70	33.5
℄		7.30	33.9
1/4		7.60	33.6
C		8.30	32.9
E.P.L.		8.40	32.8

S.C.L. of Pacific

E.P.L.		8.10	33.1
C		8.20	33.0
1/4		7.70	33.5
℄		7.50	33.7
1/4		8.00	33.2
C		7.80	33.4
W.P.L.		7.80	33.4

S.P.L. of Pacific

W.P.L.		7.80	33.4
C		8.30	32.9
1/4		8.30	32.9
℄		7.70	33.5
1/4		8.10	33.1
C		8.40	32.8
E.P.L.		8.30	32.9

POSTED

X sections Wilbur Cre Lamont to Morrell

E.P.L. Lamont [189.50]

N.P.L.	548	195.03	1.30	193.7
C			3.50	191.5
¼			4.70	190.3
℄			6.50	188.5
¼			6.80	188.2
C			7.50	187.5
S.P.L.			8.40	186.6

25' E. of Lamont

S.P.L			7.10	187.9
C			6.30	188.7
¼			7.30	187.7
℄			8.20	186.8
¼			7.30	187.7
C			6.00	189.0
N.P.L.			3.50	191.5

50' E. of Lamont

N.P.L.			4.60	190.4
C			7.60	187.4
¼			8.80	186.2
℄			8.70	186.3
¼			7.90	187.1
C			7.40	187.6
S.P.L.			7.50	187.5

100' E. of Lamont

S.P.L.			9.90	185.1
C			8.80	186.2
¼			8.70	186.3
℄			9.00	186.0
¼			9.40	185.6
C			8.30	186.7
N.P.L.			6.00	189.0

POSTED

150' E. of Lamont

N.P.L.	19503	5.50	189.5
C		7.40	187.6
¼		8.80	186.7
℄		9.70	185.3
¼		11.10	183.9
C		12.60	182.4
S.P.L.		12.80	182.2

200' E. of Lamont

S.P.L.		14.80	180.2
C		13.00	182.0
¼		11.90	183.1
℄		11.30	183.7
¼		10.10	184.9
C		9.70	185.3
N.P.L.		7.50	187.5
T.P.		7.80	187.16

250' E of Lamont

N.P.L.	2.68	189.86	1.40	188.5
C			3.70	186.2
¼			4.70	185.2
℄			5.70	184.2
¼			6.70	183.2
C			7.80	182.1
S.P.L.			9.50	180.4

300' E. of Lamont

S.P.L.		10.00	179.9
C		8.40	181.5
¼		7.30	182.6
℄		6.50	183.4
¼		5.50	184.4
C		4.50	185.4
N.P.L.		2.20	187.7

350' E of Lamont

N.P.L.	189.86	2.00	187.9
C		4.00	185.9
1/4		5.00	184.9
℄		5.90	184.0
1/4		6.70	183.2
C		7.50	182.4
S.P.L.		9.20	180.7

400' E of Lamont

S.P.L.		9.30	180.6
C		7.60	182.3
1/4		6.40	183.5
℄		5.40	184.5
1/4		4.30	185.6
C		3.00	186.9
N.P.L		0.70	189.2

450' E of Lamont

N.P.L		3.60	186.3
C		5.50	184.4
1/4		6.50	183.4
℄		7.60	182.3
1/4		8.40	181.5
C		9.40	180.5
S.P.L.		10.70	179.2

500' E. of Lamont = N.P.L. of Morell

S.P.L.		12.30	177.6
C		10.10	179.8
1/4		9.50	180.4
℄		8.70	181.2
1/4		8.00	181.9
C		7.20	182.7
N.P.L.		6.20	183.7

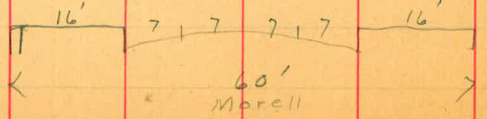
POSTED

Xsection of Morell St from Pacific Ave South

T.P.	Morell = 60' wide			37.48	
	1.93	39.41	6.73	32.68	S.W. Hub Pacific and Morell
B.M.	1.80	33.88	9.03	24.35	
	3.36	27.71			

S.T.L. of Pacific Ave

E.T.L.	27.71	5.20	22.5	
C		5.00	22.7	
¼		4.70	23.0	
℄		4.70	23.0	
¼		4.50	23.2	
C		4.20	23.5	
W.T.L.		3.40	24.3	



50' S. of Pacific

W.T.L.	2.80	25.4
C	3.40	24.3
¼	3.30	24.4
℄	3.30	24.4
¼	3.10	24.0
C	4.00	23.7
E.T.L.	4.70	23.0

100 S. of Pacific

E.T.L.	4.50	23.2
C	3.10	24.0
¼	3.50	24.2
℄	3.20	24.5
¼	3.30	24.4
C	3.20	24.5
W.T.L.	2.80	24.9

POSTED

150' S. of Pacific

W.T.L.	27.71	3.70	24.0
C		4.10	23.6
¼		4.20	23.5
℄		4.10	23.6
¼		4.00	23.2
C		4.10	23.0
E.T.L.		4.80	22.9

200' S. of Pacific

E.T.L.		5.50	22.2
C		5.30	22.4
¼		5.20	22.5
℄		4.80	22.9
¼		4.90	22.8
C		4.70	23.0
W.T.L.		4.00	23.7

250' S. of Pacific

W.T.L.		5.40	22.3
C		6.00	21.7
¼		6.30	21.4
℄		6.20	21.5
¼		6.50	21.2
C		6.70	21.0
E.T.L.		6.90	20.8

300' S. of Pacific

E.T.L.		8.10	19.6
C		7.80	19.9
¼		7.90	19.8
℄		7.80	19.9
¼		7.70	20.0
C		7.20	20.5
W.T.L.		6.80	20.9

350' S. of Pacific

W.T.L		27.71	8.00	19.7
C			9.00	18.7
¼			9.30	18.4
℄			9.10	18.6
¼			9.40	18.3
C			9.50	18.2
E.T.L.			10.20	17.5

400' S. of Pacific

E.T.L.			12.60	15.1
C			11.50	16.2
¼			11.00	16.7
℄			10.80	16.9
¼			10.90	16.8
C			10.60	17.1
W.T.L.			9.90	17.8

450' S. of Pacific

W.T.L.			11.60	16.1
C			12.50	15.2
¼			12.20	15.5
℄			12.00	15.7
¼			12.60	15.1
C			13.60	14.1
E.T.L.			13.80	13.9
T.P.			12.63	15.06

500' S. of Pacific

E.T.L.	6.93	22.01	8.60	13.4
C			8.50	13.5
¼			7.50	14.5
℄			6.70	15.3
¼			7.00	15.0
C			7.40	14.6
W.T.L.			7.00	15.0

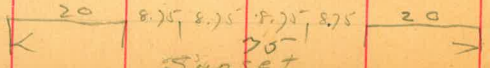
POSTED

550' S. of Pacific

W.T.L.	22.01	6.70	15.3
C		7.40	14.6
1/4		7.00	15.0
℄		6.80	15.2
1/4		7.00	15.0
C		7.90	14.1
E.T.L.		8.20	13.8

Sunset = 75 wide 612.8' S. of Pacific = N.L. of Sunset

E.T.L.		6.50	15.5
C		6.90	15.1
1/4		6.40	15.6
℄		6.30	15.7
1/4		6.30	15.7
C		5.80	16.2
W.T.L.		5.40	16.6



N.C.L. of Sunset

W.T.L.		5.30	16.7
C		5.70	16.3
1/4		5.80	16.2
℄		5.80	16.2
1/4		6.10	15.9
C		6.10	15.9
E.T.L.		6.10	15.9

N. ¼ of Sunset

E.T.L.		6.60	15.4
C		6.10	15.9
1/4		6.00	16.0
℄		5.60	16.4
1/4		5.50	16.5
C		5.60	16.4
W.T.L.		5.50	16.5

POSTED

℄ of Sunset

W.P.L.	22.01	5.20	16.8
C		5.40	16.6
¼		5.40	16.6
℄		5.60	16.4
¼		5.80	16.2
C		6.00	16.0
E.P.L.		6.40	15.6
		~~6.20~~	

S. ½ of Sunset

E.P.L.		6.20	15.8
C		5.80	16.2
¼		5.70	16.3
℄		5.50	16.5
¼		5.40	16.6
C		5.30	16.7
W.P.L.		5.30	16.7

S.C.L. of Sunset

W.P.L.		4.50	17.5
C		4.60	17.4
¼		5.30	16.7
℄		5.30	16.7
¼		5.30	16.7
C		5.10	16.9
E.P.L.		5.10	16.9

S.P.L. of Sunset

E.P.L.		5.00	17.0
C		5.10	16.9
¼		5.10	16.9
℄		4.70	17.3
¼		4.90	17.1
C		4.90	17.1
W.P.L.		4.70	17.3

60' S. of Sunset

W.P.L.	22.01	4.00	18.0
C		4.10	17.9
¼		4.10	17.9
℄		3.70	18.3
¼		3.90	18.1
C		3.60	18.2
E.P.L.		3.30	18.7

109.5' S of Sunset

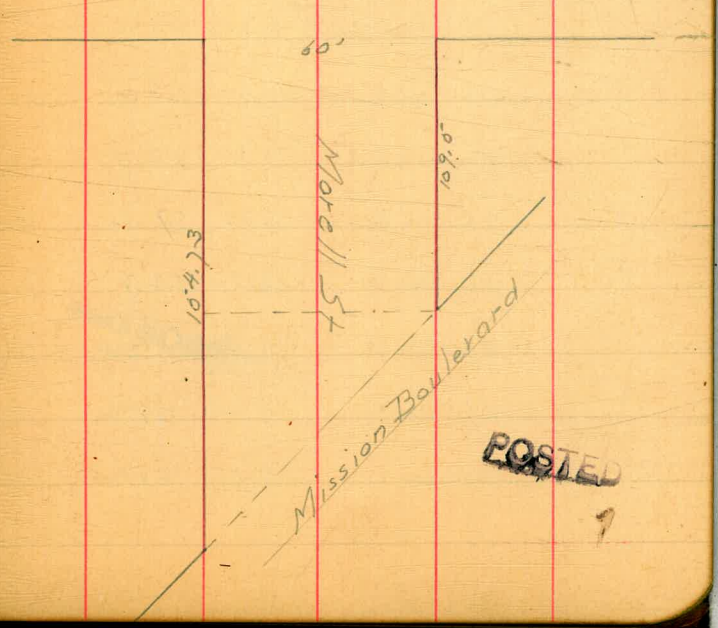
E.P.L.		2.90	19.1
C		2.80	19.2
¼		3.00	19.0
℄		2.80	19.2
¼		2.80	19.2
C		3.20	18.8
W.P.L.		3.10	18.9
		3.04	.10

Hub N.W. cor Mission Boul & Morrill

on Line from 109.5 on E. to 1+54.73 on N.

= N.P.L. of Mission Boulevard

W.P.L.		3.00	19.0
C		3.20	18.8
¼		3.20	18.8
℄		3.00	19.0
¼		3.30	18.7
C		3.10	18.9
E.P.L.		2.90	19.1



POSTED

Xsection of Kendall

Beryl to Chalcedony

B.M				143.13
T.P.	1.27	144.40	12.82	131.58
T.P.	4.33	135.91	5.11	130.80
T.P.	6.18	138.98		

N.P.L. of Chalcedony

E.P.L.		138.98	10.80	128.2
C			11.30	127.7
¼			11.80	127.2
¢			12.30	126.7
¼			12.40	126.6 POSTED
C			12.80	126.2
W.P.L.			13.40	125.6

20' N. of Chalcedony

W.P.L.			13.00	126.6
C			12.20	126.8
¼			11.80	127.2
¢			11.70	127.3
¼			11.10	127.9
C			10.70	128.3
E.P.L.			10.40	128.6

70' N. of Chalcedony

E.P.L.			8.80	130.2
C			9.20	129.8
¼			9.50	129.5
¢			9.80	129.2
¼			10.20	128.8 POSTED
C			10.50	128.5
W.P.L.			11.30	127.7

140 3

120' N. of Chalcedony

W.P.L.	138.98	9.60	129.4
C		8.90	130.1
¼		8.50	130.5
℄		8.20	130.8
¼		7.80	131.2
C		7.30	131.7
E.P.L.		7.10	131.9

170' N. of Chalcedony

E.P.L.		5.70	133.3
C		5.70	133.3
¼		6.20	132.8
℄		6.60	132.4
¼		7.00	132.0
C POST		7.50	131.5
W.P.L.		8.50	130.5

220' N. of Chalcedony

W.P.L.	138.98	7.70	131.3
C		7.20	131.8
¼		6.40	132.6
℄		6.00	133.0
¼		5.60	133.4
C		5.10	133.9
E.P.L.		4.20	134.8
T.P.		0.31	138.67

270' N. of Chalcedony = S.P.L. of Law

E.P.L.		3.20	135.8
C		4.40	134.6
¼		4.70	134.3
℄		4.80	134.2
¼		4.90	134.1
C	11.69	150.36 16.50	133.8
W.P.L.		17.10	133.3

POSTED

for intersection see X section of Law.

N.P.L. of Law

W.P.L.	150.36	13.70	136.7
C		12.70	137.7
¼		12.40	138.0
℄		11.80	138.6
¼		11.60	138.8
C		11.30	139.1
E.P.L.		10.90	139.5

20' N. of Law

E.P.L.		9.10	141.3
C		9.30	141.1
¼		9.50	140.9
℄		9.80	140.6
¼		10.40	140.0
C		10.60	139.6
W.P.L.		12.00	138.0

70' N. of Law

W.P.L.		6.80	143.6
C		6.10	144.3
¼		5.90	144.5
℄		5.40	145.0
¼		5.10	145.3
C		4.80	145.6
E.P.L.		4.50	145.9
T.P.		1.63	148.73

120' N. of Law

E.P.L.	12.79	161.52	10.60 150.9
C			10.60 150.9
¼			11.00 150.5
℄			11.30 150.2
¼			11.60 149.9
C			12.00 149.5
W.P.L.			12.60 148.9

POSTED

	170' N. of Law			
W.P.L.		161.52	7.00	154.5
C			6.10	155.4
¼			5.70	155.8
℄			5.50	156.0
¼			5.30	156.2
C			4.80	156.7
E.P.L.			4.80	156.7
T.P.			2.51	159.01
	220' N. of Law			
E.P.L.	12.47	171.48	9.80	161.7
C			9.50	162.0
¼			9.70	161.8
℄			9.90	161.6
¼			10.10	161.4
C			10.20	161.3
W.P.L.			10.80	160.7

POSTED

270' N. of Law = S.P.L. Beryl.					
W.P.L.		171.48	3.80	167.7	
C			3.80	167.7	
¼			3.60	167.9	
℄			4.00	167.5	
¼			3.80	167.7	
C			4.50	167.0	
E.P.L.			4.50	167.0	
T.P.			8.03	163.49	
T.P.	1.39	164.84	10.63	154.21	
	0.33	154.54	11.41	143.13	143.13
B.M. Spike in tel pole NE Grand & Pendleton				30.35	
T.P.	11.84	42.19	0.38	41.81	
T.P.	12.42	54.23	0.40	53.78	
B.M.	12.33	66.11	8.69	57.42	Hub N.E. Cor Feldspar & Pendleton
T.P.			0.11	66.00	
	4.08 36.09 9.52 27.07	70.08	9.52	57.42 27.07 30.35	

PC

Xsection Emerald Ave.

Pendleton St East

E.P.L. Pendleton St

N.P.L.	70.08	1.9	68.2
C		2.2	67.9
¼		1.8	68.3
℄		2.0	68.1
¼		1.9	68.2
C		2.3	67.8
S.P.L.		2.3	67.8

50' E. of Pendleton

S.P.L.		3.7	66.4
C		3.8	66.3
¼		4.1	66.0
℄		4.3	65.8
¼		4.4	65.7
¼		5.5	64.6
C		4.3	67.8
N.P.L.		5.7	64.4
		5.1	65.0

100' E. of Pendleton

N.P.L.		7.5	62.6
C		10.6	59.5
¼		10.5	59.6
℄		11.4	58.7
¼		10.1	60.0
C		9.4	60.7
S.P.L.		8.7	61.4

140' E. of Pendleton

S.P.L.		14.2	55.9
C		15.6	54.5
¼		14.4	55.4
℄		13.6	56.5
¼		12.7	57.4
C		11.5	58.6
N.P.L.		8.5	61.6

POSTED

150' E of Pendleton

N.P.L.		70.08	8.5	61.6
C			11.4	58.7
¼			13.6	56.5
¢			14.6	55.5
¼			15.3	54.8
C			16.6	53.5
S.P.L.			17.0	53.1

200' E of Pendleton

S.P.L.		57.93	8.5	49.4
C			6.4	51.5
¼			4.8	53.1
¢		70.08	17.0	53.1
¼			14.6	55.5
C			12.8	57.3
N.P.L.			10.2	59.9
T.P.	0.80	57.93	12.95	57.13

250' E of Pendleton

N.P.L.	57.93	5.0	52.9
C		4.2	53.7
¼		4.1	53.8
¢		4.5	53.4
¼		5.4	52.5
C		6.7	51.2
S.P.L.		9.6	48.3

300' E of Pendleton

S.P.L.		15.4	42.5
C		13.6	44.3
¼		12.8	45.1
¢		12.4	45.5
¼		12.5	45.4
C		12.8	45.1
N.P.L.		12.5	45.4

325' E of Pendleton

N.P.L.	57.93	14.4	43.5
C		15.3	42.6
¼		16.0	41.9
¢		16.7	41.2
¼		17.0	40.9
C		17.9	40.0
S.P.L.		18.6	39.3

350' E of Pendleton

S.P.L.		18.7	39.2
C		18.4	39.5
¼		17.7	40.2
¢		17.3	40.6
¼		17.2	40.7
C		16.0	41.9
N.P.L.		15.2	42.7

400' E of Pendleton

N.P.L.	57.93	12.0	45.9
C		13.2	44.7
¼		13.8	44.1
¢		14.5	43.4
¼		15.0	42.9
C		15.7	42.2
S.P.L.		16.7	41.2

450' E of Pendleton

S.P.L.		16.5	41.4
C		15.5	42.4
¼		15.0	42.9
¢		14.2	43.7
¼		14.0	43.9
C		13.3	44.6
N.P.L.		12.1	45.8

500 E of Pendleton = W.L. of Quincy

N.P.L.	57.93	8.7	49.2
C		9.8	48.1
¼		10.4	47.5
¢		11.0	46.9
¼		11.5	46.4
C		12.2	45.7
S.P.L.		12.2	44.7

W. C. of Quincy

S.P.L.		10.5	47.4
C		9.8	48.1
¼		9.4	48.5
¢		8.7	49.2
¼		8.1	49.8
C		7.3	50.6
N.P.L.		6.9	51.5

W ¼ of Quincy

N.P.L.	57.93	4.9	53.0
C		5.8	52.1
¼		6.5	51.4
¢		7.1	50.8
¼		8.1	49.8
C		8.9	49.0
S.P.L.		9.4	48.5

¢ of Quincy

S.P.L.		8.3	49.6
C		6.9	51.0
¼		6.5	51.4
¢		6.0	51.9
¼		5.3	52.6
C		4.6	53.3
N.P.L.		3.6	54.3

E. ¼ of Quincy

N.P.L.		57.93	2.1	55.8
C			3.3	54.6
¼			4.2	53.7
¢			5.0	52.9
¼			5.7	52.2
C			6.1	51.8
S.P.L.			7.5	50.4

E.C.L. of Quincy

S.P.L.			7.3	50.6
C			5.6	52.3
¼			4.9	53.0
¢			4.1	53.8
¼			3.2	54.7
C			2.3	55.6
N.P.L			0.4	57.5
T.R	1.52	59.17	0.28	57.65

E.P.L. of Quincy

59.2

N.P.L.		59.14	1.4	57.8
C			3.3	
¼			4.3	
¢			5.4	
¼			6.3	
C			7.8	
S.P.L.			9.0	50.2

50' E. of Quincy

S.P.L.			8.7	50.5
C			7.3	
¼			6.6	
¢			6.0	
¼			5.0	
C			4.1	
N.P.L.			1.7	57.5

100' E of Quincy

N.P.L.	59.17	1.6	57.6
C		3.6	
¼		4.2	
℄		4.6	
¼		5.2	
C		5.8	
S.P.L.		7.2	52.0

150' E of Quincy

S.P.L.		6.9	52.3
C		5.8	
¼		5.2	
℄		4.6	
¼		4.0	
C		3.4	
N.P.L.		2.0	57.2

200' E of Quincy

N.P.L.	59.17	3.3	55.9
C		4.8	
¼		5.4	
℄		5.8	
¼		6.2	
C		6.6	
S.P.L.		7.8	51.4

250' of Quincy

S.P.L.		9.7	49.5
C		8.6	
¼		8.3	
℄		8.0	
¼		7.4	
C		6.9	
N.P.L.		5.8	53.4

300' E of Quincy

N.P.L.		59.17	11.0	48.2
C			11.6	
1/4			11.7	
℄			11.8	
1/4			11.7	
C			11.6	
S.P.L.			12.2	47.0
	0.85	47.05	12.97	46.20

350' E of Quincy

S.P.L.			4.1	42.9
C			4.2	
1/4			4.8	
℄			5.3	
1/4			5.5	
C			5.5	
N.P.L.			5.5	41.5

400' E of Quincy

N.P.L.	47.05	9.2	37.8
C		10.3	
1/4		10.3	
℄		10.6	
1/4		10.2	
C		10.6	
S.P.L.		8.1	38.9

450' E of Quincy

S.P.L.		15.9	31.1
C		13.8	
1/4		13.0	
℄		12.4	
1/4		11.9	
C		11.1	
N.P.L.		8.9	38.1

500' E of Quincy = W.L. of Randall

N.P.L.		47.05	10.2	36.8
C			11.6	
1/4			12.2	
℄			13.0	
1/4			13.4	
C			13.7	
S.P.L.			15.0	32.0

W.C.L. of Randall

S.P.L.			15.9	
C			15.1	
1/4			15.0	
℄			14.4	
1/4			13.7	
C			13.0	
N.P.L.			11.7	
F.P	1.39	36.73	12.21	34.84

W 1/4 of Randall

N.P.L.	36.23	1.5	
C		2.8	
1/4		3.5	
℄		4.0	
1/4		4.6	
C		5.0	
S.P.L.		5.4	

℄ of Randall

S.P.L.		6.9	
C		5.6	
1/4		5.7	
℄		4.6	
1/4		4.0	
C		3.3	
N.P.L.		1.9	

E ¼ of Randall

N.P.L.	36.23	2.3	
C		3.9	
¼		4.9	
℄		5.5	
¼		6.2	
C		6.4	
S.P.L.		7.8	

E.C.L. of Randall.

S.P.L.		8.6	
C		7.4	
¼		6.9	
℄		6.1	
¼		5.2	
C		4.2	
N.P.L.		2.4	

E.L. of Randall

N.P.L.	36.23	2.4	33.8
C		4.9	
¼		5.8	
℄		6.7	
¼		7.3	
C		8.4	
S.P.L.		9.8	26.4

50' E of Randall

S.P.L.		12.7	23.5
C		11.7	
¼		10.7	
℄		9.7	
¼		8.6	
C		7.8	
N.P.L.		5.8	30.4

100' E of Randall

N.P.L.		36.23	11.7	24.5
C			12.7	
¼			13.5	
℄			14.4	
¼			14.9	
C			15.6	
S.P.L.			16.6	19.6
T.P	1.16	25.04	12.35	23.88

150' E of Randall

S.P.L		25.04	8.7	16.3
C			7.5	
¼			7.0	
℄			6.5	
¼			6.1	
C			5.5	
N.P.L.			4.4	20.6

210' E of Randall

N.L.		25.04	7.4	17.6
C			8.2	
¼			8.6	
℄			9.0	
¼			9.5	
C			9.8	
S.L			10.5	
			10.26	14.78
	6.61	21.39	1.56	19.83
	10.8.8	30.71	.042	30 29 30.35

POSTED

Xsection Feldspar Pendleton E-

TP			57.42	
		E. P.L of Pendleton		
N.P.L.	2.83	60.25	2.80	57.4
C			4.20	
1/4			4.80	
℄			5.70	
1/4			6.30	
C			7.10	
S.P.L.			8.50	51.7
		50' E of Pendleton		
S.P.L.			6.60	53.6
C			5.30	
1/4			4.90	
℄			4.40	
1/4			3.90	
C			3.10	
N.P.L.			2.00	58.1

100' E of Pendleton

N.P.L.	1.70	58.5
C	2.60	
1/4	3.00	
℄	3.30	
1/4	3.70	
C	4.10	
S.P.L.	5.20	55.0
	150' E of Pendleton	
S.P.L	4.40	55.8
C	3.70	
1/4	3.20	
℄	2.70	
1/4	2.60	
C	2.20	
N.P.L.	1.70	58.5

60.2
200' E of Pendleton.

N.P.L.	2.50	57.7	
C	2.40		
1/4	2.60		
¢	2.90		
1/4	3.20		
C	3.60		
S.P.L.	4.20	56.0	

250 E. of Pendleton

S.P.L.	4.40	55.4	
C	3.90		
1/4	3.70		
¢	3.60		
1/4	3.70		
C	3.90		
N.P.L.	5.00	55.7	

60.2
297' E of Pendleton

N.P.L	12.40	47.8	
C	11.30		
1/4	11.30		
¢	9.40		
1/4	9.20		
C	8.80		
S.P.L.	8.70	51.5	

75°

Xsection Hornblend

Pendleton St Enst 30.33

E.P.L. of Pendleton

T.P.	0.26	30.61	6.92	23.69
S.P.L.	1.27	24.96	3.00	22.0
C			2.30	
1/4			2.20	
℄			2.00	
1/4			2.00	
C			1.80	
N.P.L.			1.90	23.1

50' E of Pendleton

N.P.L.			3.30	21.7
C			3.00	
1/4			3.00	
℄			3.10	
1/4			3.10	
C			3.20	
S.P.L			3.50	21.6

75°

100' E of Pendleton

S.P.L.			4.50	20.5
C			4.20	
1/4			4.30	
℄			4.20	
1/4			4.30	
C			4.30	
N.P.L.			4.20	20.8

150' E. of Pendleton

N.P.L.			5.30	19.7
C			5.70	
1/4			5.70	
℄			5.60	
1/4			5.70	
C			5.60	
S.P.L.			5.70	19.3

25-0

200' E of Pendleton

S.P.L.		24.96	7.60	17.4
C			7.10	
¼			7.10	
℄			7.00	
¼			6.90	
C			7.00	
N.P.L.			7.00	18.0

250' E. of Pendleton

N.P.L.			7.90	17.1
C			8.20	
¼			8.00	
℄			8.30	
¼			8.30	
C			8.50	
S.P.L.			8.90	16.1

25-0

297' E. of Pendleton

S.P.L.		24.96	9.10	15.3
C			9.50	
¼			9.50	
℄			9.40	
¼			9.40	
C			8.80	
N.P.L.			9.10	15.9
T.P.			7.81	17.15
	2.01	19.16	12.25	6.91
	1.23	8.14		

8.1

Xsection Thomas Ave Pendleton St E.

N.P.L.	E. P.L. of Pendleton		
N.P.L.	8.14	0.40	7.7
C		1.20	
¼		1.40	
¢		1.20	
¼		2.00	
C		2.50	
S.P.L.		2.70	5.4
	50' E. of Pendleton		
S.P.L.		3.80	4.3
C		3.30	
¼		2.80	
¢		2.10	
¼		2.10	
C		2.00	
N.P.L.		1.00	7.1

8.1

	100' E. of Pendleton		
N.P.L		2.00	6.1
C		2.70	
¼		3.00	
¢		2.80	
¼		3.60	
C		4.10	
S.P.L.		4.70	3.4
	150' E of Pendleton		
S.P.L.		5.60	2.5
C		4.70	
¼		4.40	
¢		3.50	
¼		3.10	
C		3.80	
N.P.L.		3.00	5.1

8.1

200' E of Pendleton

N.P.L.	8.14	4.40	3.7
C		5.20	
¼		5.30	
¢		5.10	
¼		5.70	
C		6.00	
S.P.L.		6.20	1.9

250' E of Pendleton

S.P.L.		7.00	0.6
C		6.90	
¼		6.60	
¢		6.60	
¼		6.50	
C		6.50	
N.P.L.		5.60	2.5

8.1

297' E. of Pendleton

N.P.L.		6.30	1.8
C		6.60	
¼		6.50	
¢		6.50	
¼		6.60	
C		7.20	
S.P.L.		7.00	1.1

/

Xsection of Reed Ave

Pendleton St East

E.P.L. of Pendleton

N.P.L.	8.14	7.80	0.3
C		8.00	
1/4		8.00	
℄		8.00	
1/4		8.20	
C		8.20	
S.P.L.		8.00	-0.4

50' E of Pendleton

S.P.L.		8.50	-0.4
C		8.70	
1/4		8.40	
℄		8.30	
1/4		8.40	
C		8.20	
N.P.L.		8.10	0.0

8.1

100' E of Pendleton

N.P.L		8.00	0.1
C		8.30	
1/4		8.60	
℄		8.80	
1/4		8.30	
C		8.30	
S.P.L.		7.90	0.7

150' E. of Pendleton

S.P.L.		8.00	0.1
C		7.90	
1/4		8.00	
℄		8.10	
1/4		8.20	
C		7.70	
N.P.L.		7.60	0.5

200' E of Pendleton

N.P.L.	8.14	7.70	0.4
C		7.90	
¼		7.80	
℄		8.20	
¼		7.90	
C		8.10	
S.P.L.		8.10	0.0

250' E of Pendleton

S.P.L.		7.70	0.4
C		8.10	
¼		7.70	
℄		7.90	
¼		7.80	
C		7.80	
N.P.L.		7.90	0.2

297' E of Pendleton = EEnd

N.P.L		8.20	0.9
C		7.40	
¼		7.40	
℄		7.20	
¼		7.40	
C		7.30	
S.P.L.		7.30	0.8

Bench-Marks - Pacific Beach

N.E. Cor. Bayard + Missouri. Spike in pole	48.244
Grand + Bdy	55.847
" + Morell	46.413
Spike in fence post E. side of Bdy - 35'± N of Chalcedony	107.90
on Hub - N.W. Cor. Beryl + Bdy	131.05
" " " " " " + Morell	155.20
" " S.W. " " " " Noyes	133.95
" Stake 3 nails :- S.T.L. of Beryl 20'± E. of Olney	172.94
Grand + Fanuel - N. side spike root central cedar tree - group of 3	37.107
" + Bdy - N.E. Cor Brassplug	55.847
" + Jewel N.W. " " "	57.844
" " Kendall N.W. " " "	51.506
" " Lamont N.W. " " "	50.373
Lamont + Garnet Brs plg S.W. Cor.	65.89
" " Hornblend " " " " "	59.84
Kendall + Garnet " " " " "	64.825
Spike into pole N.E. Cor Grand + Pendleton	30.35

J 1½1
S 1½11
R 111111

W. R. Bates – Sunset 1425

Colbath – Sunset 1553

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

For Single Track Embankment.

Roadway 14 feet wide. Side Slopes 1½ to 1.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	27
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.