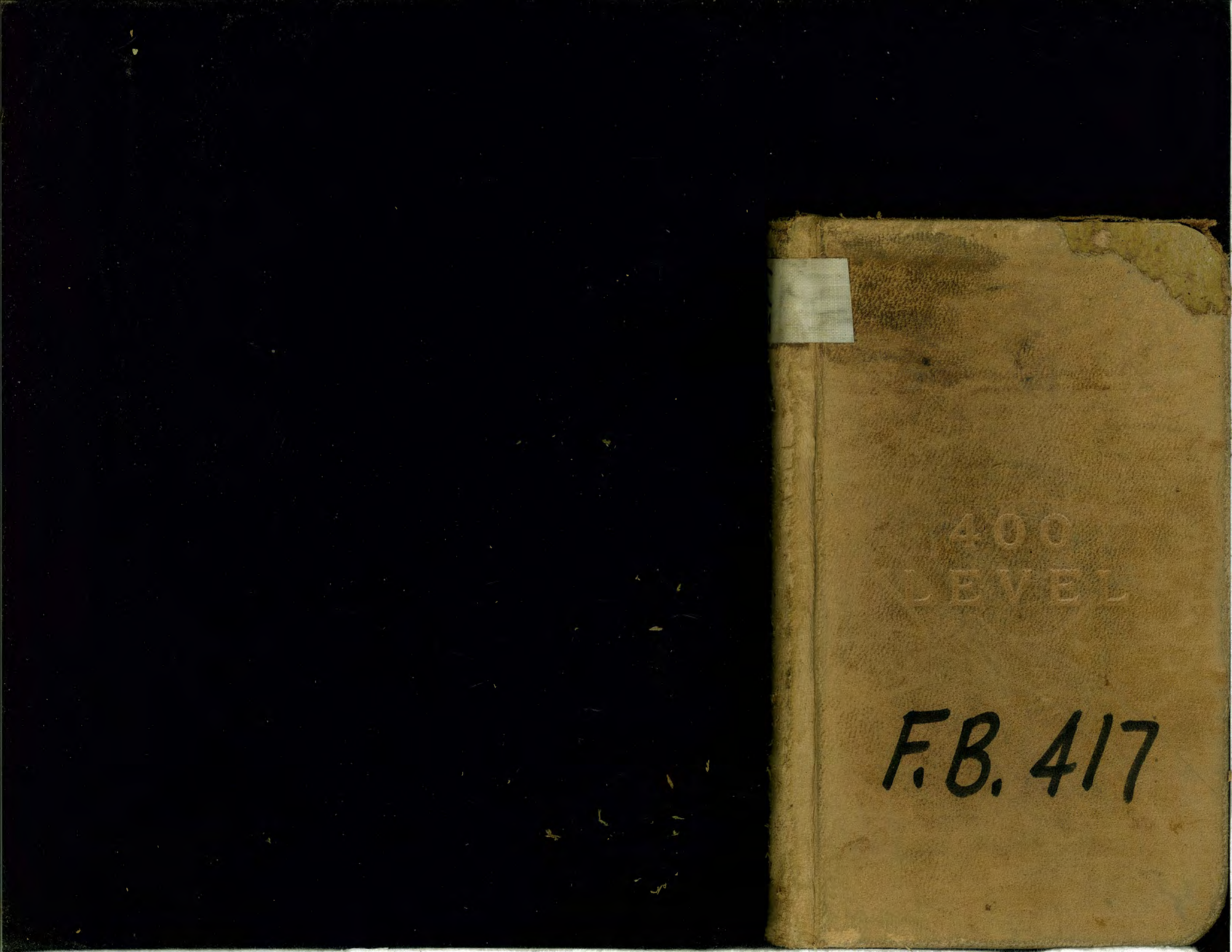
400
LEVEL
F.B. 417

Published by H. S. CROCKER COMPANY, Stationers, Drawing Materials, and Mathematical Instruments, San Francisco.

Table showing the difference of latitude and departure in running 80 chains at any course from 1 to 60 minutes.

417

MINUTES.	LKS.	MINUTES.	LKS.	MINUTES.	LKS.
1	2⅓	21	49	41	95⅔
2	4⅔	22	51⅓	42	98
3	7	23	53⅔	43	100⅓
4	9⅓	24	56	44	102⅔
5	11⅔	25	58⅓	45	105
6	14	26	60⅔	46	107⅓
7	16⅓	27	63	47	109⅔
8	18⅔	28	65⅓	48	112
9	21	29	67⅔	49	114⅓
10	23⅓	30	70	50	116⅔
11	25⅔	31	72⅓	51	119
12	28	32	74⅔	52	121⅓
13	30⅓	33	77	53	123⅔
14	32⅔	34	79⅓	54	126
15	35	35	81⅔	55	128⅓
16	37⅓	36	84	56	130⅓
17	39⅔	37	86⅓	57	133
18	42	38	88⅔	58	135⅓
19	44⅓	39	91	59	137⅔
20	46⅔	40	93⅓	60	140

MICROFILMED
DEC 03 1964

TABLE FOR RUNNING ON SLOPES.

In the following table the first column shows the angle, the second the number of links to be added to a chain on the slopes, to make one chain, horizontal measurement.

ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS
°		°		°		°	
4	0.24	11	1.88	18	5.14	25	10.54
5	0.38	12	2.24	19	5.76	26	11.26
6	0.55	13	2.63	20	6.42	27	12.24
7	0.76	14	3.06	21	7.11	28	13.37
8	0.98	15	3.53	22	7.85	29	14.34
9	1.24	16	4.02	23	8.64	30	15.47
10	1.55	17	4.56	24	9.47	35	22.07

B.M. 4" cor. 2nd & Lemon Grove 5.78

B.M. opp. Dr. Baker's House N.E. side Hd. R.R. spk. Pole. grd: 53.08

N.E. cor. Rt. Loma & Catalina Brass plug in Concrete Mt. 374.78

N.E. Co. Talbot & Rosecrans. Hd. R.R. spk. pole. grd. 21.72

Hd spk Eucalyptus Tree 269.72

Dr. Mercer place Hd sp on fence post 264.38

Near old Palms Hd sp white pole at ground 7.80

Geo. S. Place. Hd spk on fence post 2' above ground. 215.19

LORING'S BOOK STORE 182 5TH ST. SAN DIEGO

Pub
Ma

Tabl
ri

MINU

1..
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In the

ANGL

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9
10

$1°46 = 12+25$

$3°35$

$5°21$	$+50$
$8°56$	$+75$
$12°31$	1300
$16°06$	$+25$
$19°41$	$+50$
$23°16$	$+75$
$1°24$	$+84.77$
$24°40$	

LEVELS on Ocean Beach Blvd.

		H.I.		Elev.
B.M. 2" Brass	2.23	9.33		7.10
T.P.	4.47	8.34	5.46	3.87
T.P. Nail 2nd ~~L. Brass~~	~~2.54~~	8.32	2.54	5.78
T.P.	7.63	12.59	3.36	Lath Hub 4.96
T.P.			1.0	Nail Fence 11.59
	3.12	8.08		Lath Hub 4.96
T.P.	7.70	10.31	5.97	2.61
Sta				
0+00			10.3	0.0
+50			10.4	-0.1
1+00			11.1	-0.8
+50			11.0	-0.7
2+00			12.0	-1.7
+50			13.2	-2.9
3+00			13.0	-2.9
3+50			12.4	-2.1

POST

Sta	H.I.		
1+00	10.31	10.4	-0.1
+50		10.7	-0.4
5		10.8	-0.5
+50		10.8	-0.5
6+00		10.5	-0.2
+50		8.6	1.7
+50		7.1	3.2
7		9.7	0.6
+50		9.3	1.0
T.P.	9.57	10.85	9.03	1.28
8+00			9.3	1.5
+50			9.3	1.5
9			9.8	1.0
+50			9.7	1.1
10+0			9.8	1.0
10+35			9.8	1.0

POSTED

Sta		H.I.		
10+50		10.85	9.6	1.2
11+00			8.5	2.3
+50			8.3	2.5
12+00			8.1	2.7
+50			9.3	1.5
13			9.3	1.5
13+40			9.4	1.4
+50			9.3	1.5
14+0			9.9	0.9
T.P	10.63	12.01	9.47	1.38
14+50			11.8	0.2
15+0			11.6	0.4
+25			12.0	0.0
+50			11.5	0.5
16+0			10.2	1.8
+50			9.1	2.9
17+0			8.1	3.9

Sta		H.I.		
17+50		12.01	7.0	5.0
18			6.5	5.5
+50			6.4	5.6
+50			7.3	4.7
19			7.0	5.0
+50			6.8	5.2
20			6.5	5.5
T.P.	8.80	14.86	5.95	6.06
20+38.5			8.8	6.1
+50			8.4	6.5
21			7.9	7.0
21+38.4	B.C		6.9	8.0
+50			6.8	8.1
22			5.3	9.6
B.M.			3.2	Nail trvse 11.79 11.62
T.P	6.50	18.09		11.59
T.P	7.19	24.49	0.79	17.30
T.P.	3.53	26.74	1.28	23.21 T.P.

POSTED

		H.I		
T.P	3.53	26.74	1.28	23.21
T.P	8.70	32.25	3.19	23.55
T.P.			3.40	28.95=ST 38
	HH1	16.00	~~HH~~	16.59
22+50			4.2	11.8
23+00			4.1	11.9
23+50			2.5	13.5
24+00			1.4	12.6
T.P.	6.78	22.12	0.66	15.34
24+50			6.6	15.6
25+00			5.9	16.2
25+50			5.3	16.8
26+00			4.7	17.4
26+42.88=B.C			4.1	18.0
26+50			4.2	17.9
27+00			3.7	18.4
27+50			3.1	19.0
27+86.9=B.C			2.4	19.7

		H.I		
		22.12		
T.P.	7.04	26.78	1.38	19.74
28+00			6.8	20.0
28+50			6.2	20.6
29+00			5.6	21.2
29+50			5.2	21.6
30+00			4.5	21.3
30+50			4.4	22.4
30+98.96=P.R.C.			4.1	22.7
31+50			3.4	23.4
T.P.	5.43	29.25	2.96	23.82
32+00			5.7	23.5
32+50			5.3	23.9
33+00			5.2	24.0
33+43.42			4.8	24.4
33+50			4.6	24.6
34+00			4.6	24.6
34+50			4.1	25.1

		H.I 29.25		
35+00			3.3	25.9
35+33.42			2.8	26.4
T.P	6.22	32.64	2.83	26.42
35+50			5.9	26.7
36+00			5.1	27.5
36+50			4.9	27.7
37+00			5.0	27.6
37+50			4.1	28.5
38+00			3.7	28.9
B.M	6.23 ~~28.85~~	35.08		B.M 28.85
T.P	3.27	33.65	4.70	30.38
T.P	7.62	36.99	4.28	29.37
B.M. Hub 47+00			6.28	30.71
B.M. Hub 38+00	5.80	34.65	~~5.80~~	28.85
38+50 ~~B.M~~			5.5	29.1
39+00			4.7	29.9
39+50			4.3	30.3

		H.I 34.65		
40+00			4.7	29.9
40+50			4.5	30.1
41+00			5.0	29.6
41+50			5.0	29.6
42+60.57			5.2	29.4
T.P.	3.17	32.65	T.P. 29.48	5.17
42+00			3.8	28.8
42+50			4.5	28.1
43+00			4.6	28.0
43+50			4.7	27.9
44+00			4.3	28.3
T.P.	5.51	34.70	POKE ~~29.19~~	29.19 ~~3.46~~
B.M	~~30.71~~	34.70	3.99	30.71 ~~3.99~~
T.P.	5.37	3608	~~4.72~~	H 30.71
1-Bench witness Stake			1.72	34.36

		H.I.		
B.M.	6.35	37.06		30.71
SL 44+50			6.8	30.2 ✓
C			8.2	28.8
N.L.			9.4	27.6
45				
N.L			9.8	27.2
C			8.6	28.4
S.L			6.9	30.1
45+50				
S.L			7.3	29.7
C			8.9	28.1
N.L			11.0	26.0
46				
N.L.			10.5	26.5
C			8.1	28.9
S.L			6.5	30.5

		I.T.		
P.C. 46+50.67		37.06		
S.L.			6.1	30.9
C			7.4	29.6
N.L			9.5	27.5
47				
N.L.			8.5	28.5
C			6.9	30.1
S.L.			5.5	31.5 ✓
47+50				
S.L.			5.3	31.7 ✓
C			6.6	30.4
N.L			7.5	29.5
47+60.57				
N.L			7.4	29.6
C			6.1	30.9
S.L			4.8	32.2

		H.I					H.I		ELE	
48+00		37.06				50+00		37.06		
S.L			4.9	32.1		S.L			6.6	30.4
C			6.2	30.8		C			7.5	29.5
N.L			7.1	29.9		N.L			8.5	28.5
P.C. 48+60.1						T.P	1.78	30.43	8.41	28.65
N.L			7.1	29.9		50+65				
C			5.8	31.2		N.L			5.8	24.6
S.L			4.5	32.9		C			5.9	24.5
49+00						S.L			5.0	25.4
S.L			4.4	32.6		50+85				
C			5.9	31.1		S.L			9.1	21.3
N.L			7.2	29.8		C			8.3	22.1
49+50						N.L			8.8	21.6
N.L			7.6	29.4		51+00 Edge of 12L 88				
C			6.1	30.9		N.L			12.7	17.7
S.L			5.0	32.0		C			12.8	17.6
						S.L			14.0	16.4

		H.I.		
			EL.	
		30.43		
T.P.	0.52	18.74	12.21	18.22
T.P.	2.22	8.42	12.54	6.20
Bottom of BL ~ft 52+25			13.00	- 4.6
Edge of Slough			13.0	- 4.6
Bottom SL ough			15.0	- 6.6
Intersection Public Level Water's edge		Aerons	10.1 12.8	- 4.4
T.P.	12.38	20.47	0.33	8.09
80+56.5				
S.L			0+00	20.5
C			1.7	18.8
N.L.			0.3	20.2
T.P.	12.13	31.69	0.91	19.56
T.P.	6.41	37.14	0.96	30.73
B.M. Natural Stake	2.76	37.12		34.36
81				
N.L		~~6.3~~	9.2	27.9
C		~~6.3~~	6.3	30.8
S.L			3.3	33.8

	H.I.		
81+50	37.12		
S.L		4.0	33.1
C		6.3	30.8
N.L		8.0	29.1
82+00			
N.L		9.0	28.1
C		7.1	30.0
S.L		5.1	32.0
82+50			
S.L		6.0	31.1
C		8.3	28.8
N.L.		10.8	26.3
83+00			
N.L		13.3	23.8
C		9.8	26.3
S.L		6.8	30.3

POSTED

		H.I		
83+50		37.12		
S.L			8.1	29.0
C.			11.0	26.1
N.L			14.4	22.7
T.P	7.88	29.57	10.43	26.69
84+00				
N.L			7.5	22.1
C			3.6	26.0
S.L			00	29.6
84+50				
S.L			00	29.6
C			3.8	25.8
N.L			8.6	21.0
85+00				
N.L			9.9	19.7
C			5.4	24.2
S.L			1.0	28.6

		H.I		
85+50		29.57		
S.L			2.0	27.6
C			7.2	22.4
N.L			12.7	16.9
86+00				
N.L			13.8	15.8
C			8.8	20.8
S.L			4.4	25.2
86+50				
S.L			6.4	23.2
C			10.3	19.3
N.L			15.5	14.1
T.P	7.34	26.53	10.28	19.19
87+00				
N.L			14.1	12.4
C			8.5	18.0
S.L			3.0	23.5

POST

		H.I 26.53		
87+35.8 = E.C				
S.L			3.7	22.8
C			8.6	17.9
N.L			14.4	12.1
87+50				
N.L.			14.3	12.2
C			8.7	17.8
S.L.			3.7	22.8
88+00				
S.L			1.9	24.6
C			7.7	18.8
N.L			13.4	13.1
88+50				
N.L			13.4	13.1
C			6.2	20.3
S.L			1.0	26.5

		H.I 26.53		
89+00				
S.L			00	26.5
C			5.0	21.5
N.L			11.1	15.4
89+50				
N.L			10.6	15.9
C			3.7	22.8
~~S.L~~				
T.P	7.61	31.08	3.06	23.47
S.L			1.8	29.3
90+00				
S.L			1.5	29.6
C			8.1	23.0
N.L			15.0	16.1
90+50				
N.L			14.8	16.3
C			8.5	22.6
S.L			3.6	27.5

POOLED

		H.I 31.08		
91+00				
S.L			3.4	27.7
C			10.0	21.1
N.L			16.0	15.1
B.M	Temecula St & West Pt Loma		1.65	29.43
91+50				
N.L			17.1	13.1
C			12.0	19.1
S.L			7.6	23.5
92+00				
S.L			9.4	21.7
T.P.	1.33	30.31	12.10	18.98
92+00				
C			4.7	15.6
N.L			10.2	10.1

		H.I. 20.31		
92+50				
N.L			12.1	8.2
C			6.6	13.7
S.L			2.4	17.9
93+00				
S.L			4.4	15.9
C			9.4	10.9
N.L			13.7	6.6
93+50				
N.L			15.4	4.9
C			11.2	9.1
S.L			6.6	13.7
94+00				
S.L			8.3	12.0
C			13.0	7.3
N.L			16.6	3.7
T.P.	3.69	14.00	10.00	10.31

B.M = N. Pt Loma Triangle

POSTED

	HI 14.00		
94+50			
N.L		11.5	2.5
C		7.3	6.7
S.L		2.4	11.6
95+00			
S.L		4.2	9.8
C		8.5	5.5
N.L		12.0	2.0
95+50			
N.L		12.4	1.6
C		9.4	4.6
S.L		5.3	8.7
96+00			
S.L		5.7	8.3
C		10.0	4.0
N.L		12.6	1.4

	HI 14.00		
96+50			
N.L		12.7	1.3
C		10.4	3.6
S.L		6.5	7.5
97+00			
S.L		7.4	6.6
C		10.3	3.7
N.L		12.8	1.2
97+50			
N.L		13.3	0.7
C		10.7	3.3
S.L		7.6	6.4
98+00			
S.L		8.3	5.7
C		10.9	3.1
N.L		13.0	1.0

98+50		HI 14.00		
N.L			13.1	0.9
C			11.1	3.9
S.L			8.6	5.4
T.P	0.73	7.07	7.66	6.34
98+90 = break				
S.L			3.2	3.9
C			5.9	1.2
N.L			9.5	-2.4
99+00				
N.L			11.4	-4.3
C			8.3	-1.2
S.L.			8.7	-1.6
B.M 98+99 = 13.C			8.34	-1.27
Ctr 99+12			11.5	-4.4
T.P	3.52	HI 2.25		B.M -1.27
99+89.6 = edge of slough, bank			6.7	-4.5
99+92 = bottom " "			8.6	-6.4

POSTED

Evans Brooks 9-18-09

		H.I 2.25		
100+00			8.6	-6.4
100+50 = bottom of slough E. side			9.3	-7.1
100+57 = bank " " "			7.1	-4.9
100+60			5.8	-3.6
101+00			5.1	-2.9
102+00			5.1	-2.9
103+00			5.0	-2.8
104+00			4.6	-2.4
105+00			4.6	-2.4
T.P	12.67	10.66	4.26	-2.01
106+00			12.7	-2.0
107+00			12.7	-2.0
108+00			13.9	-3.2
108+20 ctr			13.8	-2.1
N.L			12.8	-2.1
S.L			12.8	-2.1
108+50 S.L			12.9	-2.2

		HI 10.66		
108+50				
Ctr.			6.3	4.4
N.L			00	10.7
109+00				
S.L			4.4	6.3
T.P.	10.56	18.21	3.01	7.65
109+00				
ctr.			6.3	11.9
N.L			1.9	16.3
109+50				
N.L			1.9	16.3
Ctr.			2.4	15.8
S.L.			5.5	12.7
110+00				
S.L			3.8	14.4
Ctr.			3.4	14.8
N.L			3.1	15.1

		HI 18.21		
110+50				
N.L			3.8	14.4
Ctr.			5.0	13.2
S.L			5.8	12.4
110+65				
S.L			6.7	11.5
ctr.			6.5	11.7
N.L			5.1	13.1
T.P	0.39	6.16	12.44	5.77
111+00				
SL.			4.6	4.2
Ctr			6.8	-0.4
N.L.			8.0	-1.8
111+15				
N.L			9.7	-3.5
Ctr			9.7	-3.5
S.L			9.7	-3.5

111+60		+I 6.16				H.I 5.62				
Ctr.			8.4	-2.2	123+91.4 △			4.5	1.1	
112+00			8.0	-1.8	124+00			5.1	0.5	
113+00			8.6	-2.4	125+00			5.3	0.3	
113+29.5 △			8.4	-2.2	T.P.	3.13	4.19	4.56	1.06	
T.P.	6.83	4.66	8.33	-2.17	126+00			1.3	2.9	
114+00			5.7	-1.0	126+50			1.8	2.4	
115+00			4.7	00	T.P. 127+00	12.10	14.02	2.27	T.P. 1.92	
116+00			4.4	0.3	T.P			1.30	2.89	– Rock
116+9.5 = 2nd of P.L.			4.4	0.3	127+65					
117+00			4.7	0.0	N.L			12.8	1.7	
118+00			4.7	0.0	Ctr			5.6	8.4	
119+00			4.6	0.1	T.P.	11.29	25.31	0.0	14.02	
T.P.	5.08	5.62	4.12	0.54	T.P.	13.02	37.60	0.73	24.58	
120+00			5.6	0.0	127+89.8					
121+00			5.2	0.4	Ctr.			3.4	34.2	
122+00			5.0	0.6	N.L.			8.0	29.6	
123+00			4.6	1.0						

		HI		
		37.66		
T.P.	11.97	46.21	3.36	34.24
12765				
S.L.			4.7	41.5
12789.8				
S.L			3.7	42.5
12800				
S.L			3.7	42.5
C.L.			8.3	37.9
N.L			13.3	32.9
12818.6 = Inv. P/L.				
N.L			12.0	34.2
Ctr.			4.2	42.0
S.L			0.0	46.2
T.P.	12.16	54.16	4.21	42.00
12870				
S.L. LINE			3.0	51.2
Cen.			7.9	46.3

		HJ		
		54.16		
12900				
S.L INE			1.7	52.5
12930				
S.LINE			6.3	47.9
T.P.	0.61	42.39	12.38	41.78
T.P.	2.38	32.60	12.17	30.22
(12900	Center)		10.0	22.6
12930				
S.LINE				47.9
Center			13.0	19.6
12950				
Center			14.6	18.0
T.P.	1.97	22.98	11.64	20.96
T.P.	4.92	15.21	12.64	10.29
12930				
N.LINE			11.5	3.7
12870				
N.LINE			11.0	4.2

		H J					H J			
129+50		15.21					9.40			
IV. LINE			14.2	1.0		133+0			9.1	0.3
130+0						DYKE			5.5	3.9
S LINE		(Estimated ELE		26.0	)	133+282			9.5	-0.1
Cen			7.1	8.1		DYKE			4.9	4.5
IV. LINE 129+00			11.8	3.4		134			9.9	-0.5
IV LINE			13.2	2.0		DYKE			5.3	4.1
B.M. Rock			12.31	2.9	2.89 2.90	135			9.7	-0.3
130+50			9.5	5.7		DYKE			4.9	4.5
130+80						136			9.8	-0.4
S. LINE			9.0	6.2		DYKE			4.9	4.5
Center			9.9	5.3		T.P.	9.18	9.62	8.96	0.74
IV. LINE			11.0	4.2		137			9.6	0.0
						D			4.9	4.7
131.			13.4	1.8		138			9.4	0.2
B.M.	6.5X	9.40			2.89	D			4.7	4.9
132			7.4	2.0		138+77.3			9.2	0.4
DYKE			5.4	4.0		D			5.0	4.6

		H.I		
139		9.67	9.5	0.1
D			4.6	5.0
140			9.5	0.1
D			4.2	5.4
141			9.3	0.3
D			4.2	5.4
142			9.1	0.5
D			4.1	5.5
T.P	450	10.08	4.04	5.58
143			9.5	0.6
D			4.6	5.5
143+99.2 △			9.1	1.0
D			4.5	5.6
144+0			9.1	1.0
D			4.5	5.6
145			9.7	0.4
D			4.7	5.4

		H.I		
146		10.08	9.7	0.4
D			4.1	6.0
147			9.4	0.7
D			4.0	6.1
148			9.2	0.9
D			3.6	6.5
149			9.3	0.8
D			3.6	6.5
T.P	9.42	11.05	8.45	1.63
150			10.1	0.9
D			4.6	6.4
150+28.8			9.9	1.1
D			5.1	5.9
151			10.4	0.6
D			5.0	6.0
152			10.3	0.8
D			4.7	6.4

		H.I		
153		11.05	10.3	0.7
D			4.9	6.1
154			9.8	1.3
D			5.1	5.9
154+63.5			10.3	0.8
D			5.2	5.8
T.P.	5.82	11.66	5.21	5.84
155			11.0	0.7
DUKE			5.4	6.3
156			11.1	0.6
D			4.9	6.8
157			10.7	1.0
D			4.7	7.0
158			10.1	1.6
D			4.6	7.1
159			9.9	1.8
D			4.6	7.1

		H.I			
159+32.2		11.66	9.4	2.3	
D			4.8	6.5	
160			10.5	1.2	
D			4.8	6.9	
B.M.			7.91	3.75	Nail in fence NEAR Sta 160

Continued in Book 345 P. 45

POSTED

Levels on Point Loma Blvd
From Landscape & Hemelita St to

B.M.	9.80	31.52		21.72
T.P.	11.85	42.58	0.79	30.73
		0+00		
E.			3.3	39.3
C.			2.4	40.2
W.			2.1	40.5
TP	5.75	46.72	1.61	40.97
		1+00		
E			6.4	40.3
C.			5.6	41.1
W.			4.8	41.9
		1+50		
W			5.9	41.7
C.	X		5.7	41.0
E			6.5	40.2
		2+00		
E.			7.3	39.4
C.			6.4	40.3
W.			5.6	41.1

Readings on ℄ & 15' each side

Wireless Station

24

		2+50		
W		46.72	2.4	44.3
C			4.3	42.4
E			7.6	39.1
T.P.	11.69	58.29	0.12	46.60
		3+00		
E			14.5	43.8
C			10.5	47.8
W			5.6	52.7
		3+60.5		
W			-0.3	58.6
C.		X	1.6	56.7
E			4.7	54.1
T.P.	11.96	69.96	0.29	58.00
		4+00		
E			17.4	52.6
C			10.7	59.3
W			8.5	61.5

		4+50		
W.		69.96	6.1	63.9
C			8.6	60.4
E			11.0	59.0
		5+00		
E			7.8	67.2
C.			5.0	65.0
W.			2.3	67.7
T.P	12.78	82.19	0.55	69.41
		5+50		
W.			9.6	72.7
C			12.9	69.3
E.			16.7	66.0
	6+06			
E.			11.3	70.9
C.			6.8	66.4
W.			2.6	79.6

		6+50		
W.		87.19	1.6	80.6
C.			4.7	77.5
E.			8.7	73.5
		7+00		
E			12.6	69.6
C			10.5	71.7
W			6.6	75.6
T.P.	12.87	94.99	0.01	87.18
		7+50		
E.			8.7	86.3
C.			4.5	90.5
W.			0.6	94.4
T.P.	12.91	107.62	0.28	94.71
		8+00		
E			13.7	94.4
C			9.6	98.0
W.			5.8	101.8

T.P		HI 107.62			
	9.35	116.95	0.02	107.60	
		8+50			
E			15.2	101.7	
C			11.6	105.3	
IV			7.4	109.5	
		9+00			
IV			3.6	114.3	
C			6.0	110.9	
E			9.9	107.0	
		9+23.5			
E			8.8	108.1	
C			4.7	112.2	
IV			0.9	116.0	
		9+50			
IV			3.4	113.5	
C			7.4	109.5	
E			11.9	105.0	

		10+00		
E		116.9	17.0	99.9
C			15.7	101.2
IV			12.6	104.3
		10+45		
IV		116.95	1.1	115.8
C			3.2	113.7
E			5.0	111.9
T.P	12.89	129.38	0.46	116.49
		10+89.9		
E			13.3	116.1
C			9.7	119.7
IV			4.8	124.6
		11+00		
IV			3.0	126.4
C			7.8	121.6
E			12.3	117.1

		11+11.7		
E		129.38	7.6	121.8
C.			3.2	126.2
W.			-2.5	131.9
Sp. in pole. opp. Sta 11+11.7				
B.M.			9.59	119.79
		11+50		
W.			0.5	128.9
C.			2.4	127.0
E			6.0	123.4
		12+05		
E.		129.38	18.6	110.8
C.			16.0	113.4
W.			11.3	118.1
T.P	13.06	142.10	0.34	129.04
		12+50		
E			13.5	128.6
C.			9.3	132.8
W.			5.3	136.8

		13+00		
W.		142.10	-0.5	142.6
C.			4.1	138.0
E			8.4	133.7
T.		13+50		
E			8.0	134.1
C.			4.5	137.6
W.			0.8	141.3
		14+00		
W.		142.10	2.3	139.8
C.			4.5	137.6
E.			7.5	134.6
T.P	12.99	154.83	0.26	141.84
		+50		
W			8.1	146.7
C			11.2	143.6
E			14.4	140.4

		15+00		
F		154.83	1.25	142.3
C			8.6	146.2
W			5.6	149.2
		1+50		
W			5.9	148.9
C			8.8	146.0
E			11.2	143.6
		1+65		
W			-0.3	155.1
C			4.3	150.5
E			7.6	147.2
		16+00		
E			10.3	
C			6.0	148.8
W			0.8	
T.P	11.81	166.38	0.26	154.57

		16+50		
W		166.38	9.1	
C			13.4	153.0
E			16.3	
		17+00		
E			13.2	
C			9.2	157.2
W			5.8	
		17+50		
W		166.38	2.1	
C			4.6	161.8
E			8.2	
T.P	12.26	178.08	0.56	165.82
		18+00		
W			8.4	
C			10.8	167.3
E			14.5	

		18+50			
E		178.08	12.6		
C.			10.7	167.9	
W.			7.1		
		19+00			
W.			2.7		
C.			6.6	171.5	
E.			11.0		
		19+50			
E		178.08	4.5		
C.			2.0	176.08	
W.			-1.3	179.4	
T.P.	10.58	188.60	0.06	178.02	
		20+00			
E			14.7		
C.			12.7	175.9	
W.			10.3		

		20+50			
W		188.6	9.9		
C.			11.7	176.9	
E.			13.0		
		21+00			
E.			8.5		
C.		188.60	6.4	182.2	
W.			4.5	184.1	
T.P	12.98	201.05	0.53	188.07	BM on Hub: Sta 21+39.
		21+50			
W.			9.0		
C.			10.4	190.6	
E			11.9		
		21+75			
E			6.2		
C			4.2	196.8	
W			4.3		

T.		22+00		
W		201.0	7.8	
C			10.2	190.8
E			11.6	
		22+25		
E			5.3	
C			3.4	197.6
W			3.2	
		22+50		
W		204.05	1.4	
C			2.5	198.5
E			4.1	
T.P.	12.50	213.06	0.49	200.56
		23+00		
E			12.3	200.8
C			11.1	202.0
W			10.0	

		23+50		
W		213.06	1.2	
C			3.1	210.0
E			3.7	
T.P.	12.91	225.49	0.48	212.58
		23+75		
E			7.7	
C			7.5	218.0
W			4.6	
		24+00		
W		225.49	1.4	
C			4.2	221.3
E			6.3	
T.P.	12.57	238.00	0.06	225.43
		24+50		
W			9.5	
C			12.9	225.1
E			16.7	

		25+00			
E		238.00	10.8		
C.			5.4	232.6	
W.			1.4		
		25+50			
W.			4.5		
C.			8.9	229.1	
E			13.7		
		26+00			
E			21.00		
C.			16.8	221.2	
W.			12.8		
		26+50			
W			5.2		
C			6.3	231.7	
E			13.3		

		26+70			
E		238.0	20.5		
C.			16.5	221.5	
W			9.2		
		27+00			
W.		23800	2.4		
C.			7.4	231.6	
E			13.8		
T.P	1237	250.30	0.07	237.93	
		27+50			
E			11.3		
C			8.8	241.5	
W.			5.2		
		27+75			
W.			1.7		
C.			3.9	246.4	
E			1.0		
T.P	5.70	255.61	0.39	249.91	

	255.61		
B.M.		5.77	249.84 mail in post at Sta 28+00
	27+85		
E		5.5	250.1
C.		4.1	251.5
W.		3.2	
	28+00		
E		5.2	
C.		3.2	252.4
W.		1.3	
	29+00		
W.		5.1	
C.		6.4	249.2
E		8.0	
	30+00		
E		11.1	
C.		9.8	245.8
W.		8.3	

	31+00		
W	255.6	9.2	
C.		10.5	245.1
E		12.1	
	31+40		
W.		10.7	
C.		13.5	242.4
E		14.3	
	31+60		
E		11.7	
C.		9.2	246.4
W.		7.4	
	32+00		
W		6.0	
C		8.0	247.6
E		10.1	

		32+50			
E			9.2		
C			7.1	248.5	
W			4.8		
		33+00			
W		255.61	0.4		
C			1.9	253.7	
E			3.6		
T.P	12.5	267.80	0.36	255.75	
		33+50			
W			8.3		
C			9.9	257.9	
E			11.7		
		34+00			
E			8.5		
C			6.0	261.8	
W			4.8		

		34+50			
W		267.80	3.6		
C			5.6	262.3	
E			8.7		
		35+00			
E			4.3		
C			2.7	265.1	
W			1.5		
					cont 6.5 to 35+36
T.P	12.46	279.8.5	0.41	267.39	BM
		+50			
W			10.3		
C			11.4	268.4	
E			12.3		
		36+00			
E			9.6		
C			8.6	271.2	
W			7.1		

		36+50		
		279.85		
W.			3.5	
C.			5.0	274.8
E			6.6	
		37+00		
E			3.5	
C.			1.1	278.7
W.			-0.3	280.1
T.P.	12.61	292.37	0.09	279.76
		37+50		
W			8.3	
C			10.1	282.3
E			11.6	
		38+00		
E			10.7	
C			8.4	284.0
W.			7.3	

		38+50		
W		294.4	4.4	
C			6.1	286.3
E			8.6	
		39+00		
E			7.7	
C.			4.6	288.4
W.			2.4	
		39+50		
W		292.37	1.3	
C.			2.5	289.9
E			4.8	
T.P.	12.31	303.64	10.4	291.33
		40+00		
W			12.4	
C.			14.0	289.6
E			15.0	

	40+50			
	303.64			
E		13.8		
C		12.5	291.1	
W		11.1		
	41+00			
W		10.1		
C		10.6	293.0	
E		11.7		
	41+50			
E		9.8		
C		8.1	295.5	
W		6.5		
	42+00			
W		4.5		
C		7.0	296.6	
E		8.0		

	42+50			
E	303.6	6.8		
C		4.6	299.0	
W		2.8		
	43+00			
W		1.4		
C		3.5	300.1	
E		6.0		
	43+50			
E	303.64	5.8		
C		3.6	300.0	
W		1.2		
T.P	1285	316.19	030	303.34
	44+00			
W		7.7		
C		8.9	307.2	
E		10.1		

		44+50		
E.		316.19	4.6	
C			4.0	312.2
W			3.1	
T.P	10.21	325.03	1.39	314.82
		45+00		
W			8.8	316.2
C			9.6	315.4
E			10.4	
		45+50		
E			8.6	
C.			7.3	318.7
W.			6.5	
		46+00		
W.			4.0	
C.			4.8	320.2
E.			5.9	

		46+50		
E		325.03	3.1	
C.			2.4	322.6
W.			1.3	
T.P	12.10	336.79	0.34	324.69
		47+00		
W.			10.6	
C.			11.4	325.4
E.			12.2	
		47+50		
E			9.9	
C.			9.2	327.6
W.			8.4	
		48+00		
W			5.7	
C.			6.6	330.2
E			7.2	

		48+50		
E		336.99	5.7	
C			4.6	334.7
W.			3.4	
T.P.	12.69	348.60	0.88	335.91
		49+00		
W			12.8	335.8
C			14.0	334.6
E			15.0	
		49+50		
E			12.7	
C			11.8	336.8
W.			11.0	
		49+81		
W			11.6	337.0
C			11.1	337.5
S			10.8	337.8

		50+00		
E		348.6	9.4	339.2
C			9.8	338.8
W			9.7	338.9
		50+50		
W			7.5	341.1
C			7.3	341.3
S			6.7	341.9
		51+00		
S			4.6	344.0
C			5.1	343.5
W			5.1	343.5
		51+50		
W			3.4	345.2
C			3.1	345.5
S			2.7	345.9

		52+00		
S		348.6	1.9	346.7
C			2.3	346.3
N			2.4	346.2
		52+50		
N			2.6	346.0
C			2.5	346.1
S			2.2	346.4
		53+00		
S		348.60	3.4	345.2
C			3.7	344.9
N			3.7	344.9
T.P	2.13	346.33	4.40	344.20
		53+50		
N			2.9	343.4
C			2.9	343.5
S			2.6	343.7

		53+98.9 =		
N		346.33	4.9	341.4
C			4.7	341.6
S			4.4	341.9
T.P	4.42	349.13	1.62	344.71
			5.80	343.33

Readings on ℄ & 15' each side

Levels on Fort Stockton Blvd.

B.M.	Cor Mendes Fence 0.48	264.86		264.38
T.P.	0.20	259.14	11.92	252.94
T.P.	1.01	241.30	12.85	240.29
Sta 0+00				
S			4.3	236.0
C			5.1	236.2
N.			5.9	235.4
0+50				
N			12.4	228.9
C			11.4	229.9
S			10.1	231.2
T.P.	1.84	230.62	12.62	228.78
1+00				
S			4.8	225.8
C			6.0	224.6
N			7.1	223.5

150+00		230.62		
N			12.4	218.2
C			11.8	218.8
S			11.1	219.5
T.P.	0.39	218.61	12.40	218.22
2+00			3.4	215.2
S			3.4	215.2
C			3.4	215.2
N			3.2	215.4
2+50				
N			6	212.3
C			6.7	211.9
S			6.9	211.7

POSTED

POSTED

		H	
		218.61	
3+00			
S		8.9	209.7
C		8.7	209.9
N		8.1	210.5
3+50			
N		9.0	209.6
C		10.5	208.1
S		11.2	207.4
4+00			
S		12.3	206.3
C		12.0	206.6
N		10.9	207.7
B.M. Croft Place		3.34	215.19 215.27

		H.J.		218.61 3.34 215.27	
		218.53			
T.P.	0.68	208.10	11.11	207.42	
4+50					
N			3.2	204.9	
C			5.0	203.1	
S			5.8	202.3	
5+00					
S			7.4	200.7	
C			6.6	201.5	
N			5.9	202.2	
5+57.5 = 5+45					
N			4.6	203.5	
C			6.2	201.9	
S			8.6	199.5	

POSTED

		H		
		208.10		
6+00				
S			10.0	198.1
C			8.9	199.2
N			6.5	201.6
6+50				
N			10.4	197.7
C			12.3	195.8
S			16.0	192.1
T.P.	2.34	198.43	12.01	196.09
7+00				
S			14.0	184.4
C			9.0	189.4
N			5.0	193.4

		H. 198.43		
7+50				
N			7.3	191.1
C			9.7	188.7
S			13.3	185.1
T.P.	1.32	187.91	11.84	186.59
8+00				
S			8.2	199.7
C			2.7	185.2
N			0.0	187.9
8+50				
N			3.9	184.0
C			6.8	181.1
S			11.2	176.7
8+88 S			15.4	172.5
C			10.4	177.5
N			7.3	180.6

POSTED

		H.I		
		187.91		
9+00				
N			7.3	180.6
C			11.1	176.8
S			17.4	170.5
9+50				
S			15.3	172.6
C			9.8	178.1
N			7.4	180.5
10+00				
N			9.8	178.1
C			12.1	175.8
S			14.4	173.5
T.P.	2.31	178.52	11.70	176.21

		H.I		
		178.52		
10+50				
S			9.7	168.8
C			6.7	171.8
N			4.1	174.4
11+00				
N			9.5	169.0
C			10.7	167.8
S			13.0	165.5
T.P.	3.31	170.09	11.74	166.78
11+50				
S			7.0	163.1
~~N~~ C			4.0	166.1
C N			2.3	167.7

POSTED

		H		
11+93.1		170.09		
N			1.9	168.2
C			3.3	166.8
S			5.1	165.0
12+00				
S			5.3	164.8
C			3.3	166.8
N			2.0	168.1
12+50				
N			2.0	168.1
C			3.5	166.6
S			5.7	164.4

		H		
13+00		170.09		
S			10.3	159.8
C			8.8	161.3
N			7.0	163.1
13+50				
N			12.1	158.0
C			14.0	156.1
S			15.6	154.5
T. P.	3.42	161.05	12+6	157.63
14+00				
S			8.1	152.9
C			7.7	153.3
N			6.3	154.7

	H.I		
14+25	161.05		
N		5.0	156.0
C		6.5	154.5
S		8.1	153.6
14+50			
S		10.6	151.4
C		8.0	153.0
N		6.2	154.8
15+00			
N		8.9	152.1
C		10.4	150.6
S		12.1	148.9

	H.I			
15+50	161.05			
S			16.0	145.0
C			11.6	149.4
N			8.8	152.2
16+00				
N			10.4	150.6
C			15.2	145.8
S			18.2	142.8
T.P.	0.93	149.13	12.85	148.20
16+50				
S			11.7	137.4
C			7.7	141.4
N			3.6	145.5

POSTED

		H.I 149.13		
17+00				
N			5.6	143.5
C			9.4	139.7
S			14.9	134.2
17+50				
S			19.0	130.1
C			12.8	136.3
N			7.2	141.9
T.P.	1.58	138.32	12.39	136.74
18+00				
N			−2	138.5
C			4.2	134.1
S			10.7	127.6

		H.I 138.32		
18+50 △				
S			16.0	122.3
C			8.7	129.6
N			2.8	135.5
19+00				
N			4.0	134.3
C			10.2	128.1
S			16.5	121.8
19+50				
S			16.7	121.6
C			10.6	127.7
N			4.8	133.5
20+00				
T.P.	1.81	128.53	11.58	126.74

POSTED

		HI		
20+00		128.55		
N			00	178.6
C			5.2	123.3
S.			10.2	118.4
20+50				
S			15.8	112.8
C			10.7	117.8
N.			5.9	122.7
21+00				
N.			6.2	121.4
C			10.4	118.1
S.			15.5	113.1
T.P.	1.30	117.71	12.14	116.41
21+65				
N			1.8	115.9

		HI		
21+65		117.71		
C			6.5	111.2
S			12.1	105.6
22+00				
S			13.6	104.1
C			9.1	108.6
N			5.4	112.3
22+50				
N.			8.3	109.4
C			12.7	105.0
S			17.6	100.1
T.P.	00	105.13	12.58	105.13
23+00				
S.			8.7	96.4
C			4.8	100.3
N.			1.0	104.1

POSTED

		HI 105.13		
23+75				
N			2.8	102.3
C			6.7	98.4
S			10.9	94.2
24+00				
S			13.0	92.1
C			9.5	95.7
N			6.0	99.1
24+50				
N			9.9	95.2
C			13.3	91.8
S			16.0	89.1
T.P	2.59	94.96	12.76	92.37

		HI 94.96		
25+00				
S			6.7	88.2
C			3.0	91.9
N			0.0	95.0
25+50				
N			3.3	91.6
C			5.7	89.2
S			8.9	86.0
26+05.8				
S			11.4	83.5
C			8.0	86.9
N			5.6	89.3
26+50				
N			6.1	88.8
C			9.7	85.2
S			13.1	81.8

POSTED

		HI		
26+70		94.96		
S			13.8	81.1
C			11.3	83.6
N			7.0	87.9
T.P.	00	84.33	10.63	84.33
27+00				
N			3.2	81.1
C			6.8	77.5
S			9.8	74.5
27+50				
S			14.1	70.2
C			12.4	71.9
N			9.9	74.4
28+00				
N			6.3	78.0
C			9.3	75.0
S			11.8	72.5

		HI.		
28+00 = A		84.33		
S			11.9	72.4
C			8.2	76.1
N			5.6	78.7
28+50				
N.			6.3	78 0
C			9.7	74.6
S			13.6	70.7
29+00 = A				
S			16.1	68.2
C			14.0	70.3
N			12.1	72.2
T.P.	0.38	71.95	12.76	71.57
29+50				
S			6.4	65.5
C			6.4	65.5
N			5.5	66.4

		HI.		
30+00		71.95		
N			11.6	60.3
C			11.8	60.1
S			11.0	60.9
T.P.	3.70	63.52	12.13	59.82
30+50 = Δ				
W.			7.5	56.0
C			5.9	57.6
E			5.0	58.5
31+00				
E			8.0	55.5
C			9.3	54.2
W			9.9	53.6
31+80				
W			10.0	53.5
C			9.0	54.5
E			7.6	55.9

		HI.		
32+00		63.52		
E			10.4	53.1
C			12.4	51.1
W			13.7	49.8
T.P.	2.92	53.92	12.52	51.00
32+50				
W			17.9	36.0
C			13.3	40.6
E			9.2	44.7
33+00				
W			15.3	38.6
C			11.2	42.7
E			8.6	45.3
T.P.	0.43	42.10	12.25	41.67
33+40.3 = Δ				
W.			4.0	38.1
C			1.0	41.1
E			-2.0	43.1

POST-

		HI		
34+00		42.10		
E			8.4	33.7
C			12.0	30.1
W			16.0	26.1
34+25				
W			11.7	30.4
C			8.4	33.7
E			4.3	37.8
T.P.	0.03	30.67	11.46	30.64
35+00				
E			4.0	26.7
C			7.9	22.8
W			13.3	17.4
T.P.	0.27	19.13	11.81	18.86

		HI		
35+35		19.13		
E			0.5	18.6
C			3.3	15.8
W			6.2	12.9
T.P.	1.85	12.14	8.84	10.29
				7.80 = 13.11
T.P.			4.43	7.71

POSTED

Levels on Escondido Blvd

City datum 5.82 Lomita Grt. B.M.

	+	H.I.	−	
B.M.	4.34	32.34		28.00
				inside pool farm fence
R.P. of Flume			3.14	29.20
T.P.	11.23	43.35	0.22	32.12
	12.12	54.76	0.71	42.64
	8.51	60.30	2.97	51.79

P.C. Curve on Hospital Grade.

P.C. Curve			1.8	58.5
+25			2.2	58.1
+50			6.4	53.9
1			9.5	50.8
+40 Bottom Ditch			12.4	47.9
+50			11.8	48.5
+55			10.4	49.9
2			11.2	49.1
+50			12.8	47.5
3			14.7	45.6
+50			14.7	45.6
+40.3 P.T. = 2+00 Old line			11.8	48.5

POSTED

Commence at pool farm Grade

		60.30		
T.P	12.20	72.48	0.02	60.28
	8.65	80.50	0.63	71.85
2+70.6			1.2	79.3
3+00			1.7	78.8
3+30			2.6	77.9
+50			10.2	70.3 on P.C. 3+50
T.P. on P.C.	0.90	70.14	1.26	67.24
3+80			10.0	60.1
T.P	0.54	58.81	11.87	58.27
+95			7.2	51.6
4+00			12.4	46.4
T.P	1.63	47.75	12.69	46.12
4+25			10.1	37.6
+50			13.8	34.7
5+00			13.8	33.9
T.P.	0.04	35.03	12.76	34.99
+50			3.8	31.2
6+00			4.9	30.1
7+00			7.2	27.8

POSTED

		35.03		
8+00			7.9	27.1
				29.20
B.M. Filmore			5.83	29.20
T.P.	1.82	31.43	5.42	29.61
9+00			4.7	26.7
10+00			4.8	26.6
11+00			4.8	26.6
12+00			5.4	26.0
13			4.6	26.8
13+58.7			4.9	26.5
T.P.	2.53	30.80	3.16	28.27
14			4.2	26.6
15			4.6	26.2
16			4.6	26.2
17			4.3	26.5
18			4.5	26.3
19			5.2	25.6
20			4.9	25.9

POSTED

		30.80		
T.P.	5.21	31.21	4.80	26.0
21+0			5.7	25.5
22+0			5.4	25.8
23+0			4.6	26.6
24+0			3.6	27.6
25+0			3.6	27.6
26+0			3.6	27.6
T.P.	1.99	30.25	2.95	28.26
27+0			2.6	27.6
River Bed +75			3.3	26.9
28			6.7	23.5
29			7.0	23.2
+15			7.2	23.0
+25			5.7	24.5
30			5.3	24.9
31			4.8	25.4
32			5.3	24.9

POS.

		30.25			
T.P.	3.90	31.11 ~~30.11~~	3.04	27.21 ~~26.21~~	
33+0			5.7	25.4	
34			5.3	25.8	
35			4.7	26.4	
B.C. 35+79.1			4.6	26.5	
36+0			5.1	26.0	
36+50			4.5	26.6	
37			4.4	26.7	
37+35			4.2	26.9	
37+50			2.2	28.9	
T.P.	7.25	36.55 ~~36.55~~	1.81	29.30 ~~28.30~~	
B.M. on N.W. cor Rear fence			7.79	22.75 / 28.76	correction +.94
38			8.7	27.8	
38+50			9.6	26.9	
39			9.7	26.8	
39+40			7.2	29.3	
+50			4.4	32.1	

		36.55		
T.P.	11.56	48.07	0.04	36.51
39+75			9.6	38.5
40+0			2.9	45.2
+10			1.4	46.7
40+50			0.0	48.1
T.P.	6.94	54.84	0.17	47.90
40+60			1.8	53.0
B.C. 40+83.95			2.6	52.2
41+0			3.9	50.9
Intersection Pueblo 41+65			9.0	45.8
42+0			9.7	45.1
43+0			6.9	47.9
T.P.	8.20	~~56.15~~	6.89	47.95
44+00			7.3	48.8
44+50			7.6	48.5
45+00			8.7	47.4
45+50			7.5	48.6
46+00			9.3	46.8

		56.15		
T.P.	5.23	51.18	10.20	45.95
46+50			5.4	45.8
47+00			6.5	44.7
Inter of P.L. 47+30.3			5.0	46.2
47+50			3.2	48.0
48+00			4.4	46.8
48+50			3.5	47.7
49+00			3.2	48.0
49+25			3.1	48.1
49+75			4.6	46.6
50+00			3.1	48.1
T.P.	9.70	54.10	6.78	44.40
51+00			4.6	49.5
51+15			4.4	49.7
51+35			4.0	50.1
52+00			5.3	48.8
52+40			5.1	49.0
52+50			5.0	49.1

		H.I		
		54.10		
53+00			4.4	49.7
53+50			5.7	48.4
54+00			7.3	46.8
T.P.	7.64	53.92	7.82	46.28
54+50			5.4	49.5
55+00			3.6	50.3
55+40			3.0	50.9
56+00			5.8	48.1
56+75			7.6	46.3
57+00			7.0	46.9
58+00			4.3	49.6
59+00			3.2	50.7
T.P.	6.74	56.89	3.77	50.15
59+50			5.0	51.9
60+00			3.9	53.0
60+50			4.2	52.7
61+00			3.8	53.1

		H.I 56.89		
62+00			2.7	54.2
62+25			7.0	49.9
62+75			9.5	47.4
63+00			8.9	48.0
T.P.	9.53	57.03	9.39	47.50
64+00			8.1	48.9
65+00			5.4	51.6
66+00			5.0	52.0
T.P.	9.42	64.91	1.54	55.49
67+00			10.2	54.7
68+00			8.8	56.1
69+00			5.6	59.3
70+00			3.5	61.4
T.P.	10.25	73.21	1.95	62.96
71+00			9.5	63.7
72+00			6.9	66.3
72+30			6.3	66.9

		H.I. 73.21		
72+45			6.4	66.8
72+50			9.0	63.9
72+95			7.8	65.4
73+00			4.1	69.1
T.P.	10.60	80.03	3.78	69.43
74+00			5.6	74.4
74+20			4.5	75.5
75+00			2.5	73.5
75+50			5.3	74.7
75+60			6.5	73.5
76+00			5.3	74.7
T.P.	10.19	86.54	3.68	76.35
77+00			10.2	76.3
77+50			8.4	78.1
78+00			7.9	78.6
79+00			5.7	80.8
79+45			4.00	82.5

		H.I 86.54		
opp. 79+45				
B.M.-3 nails in Phone Pole			3.76	82.78
80+00			3.3	83.2
T.P.	12.60	96.47	2.67	83.87
80+50 ℄ to left			12.1	84.4
81+00			9.5	87.0
81+50			7.3	89.2
82+00			6.5	90.0
82+00 B.M.			6.47	90.00

POSTED

1

Levels on Escondido Blvd bet 1105 & 1106

	+	H.I.	−	Elev.
BM	2.19	24.37		22.18
0+00			5.5	18.9
1+00			3.3	21.1
T.P	3.60	25.71	2.26	22.11
2+00			5.2	20.5
3+00			5.1	20.6
4+00			4.7	21.0
+85			4.2	21.5
5+00			4.9	20.8
+60			7.1	18.6
5+75			8.8	16.9
6+00			7.7	18.0
+30			4.7	21.0
7+00			5.3	20.4
T.P	5.59	27.06	4.24	21.47
8+00			5.8	21.3
9			5.0	22.1
+30			5.6	21.5
+50			8.7	18.4
10			7.9	19.2
10+20	27.06		6.7	20.4
11+00			6.5	20.6
T.P	4.53	25.06	6.53	20.53
11+15			5.9	19.2
+17			10.1	15.0
12+00			9.1	16.0
+40			9.0	16.1
+50			7.8	17.3
+60			5.2	19.9
+70			6.3	18.8
+80			4.7	20.4
13+00			4.8	20.3
14+0			5.6	19.5
15+00			5.2	19.9
1640			4.5	20.6
T.P	4.01	25.05	4.02	21.04
17+0			6.5	18.5
18+0			5.9	19.1

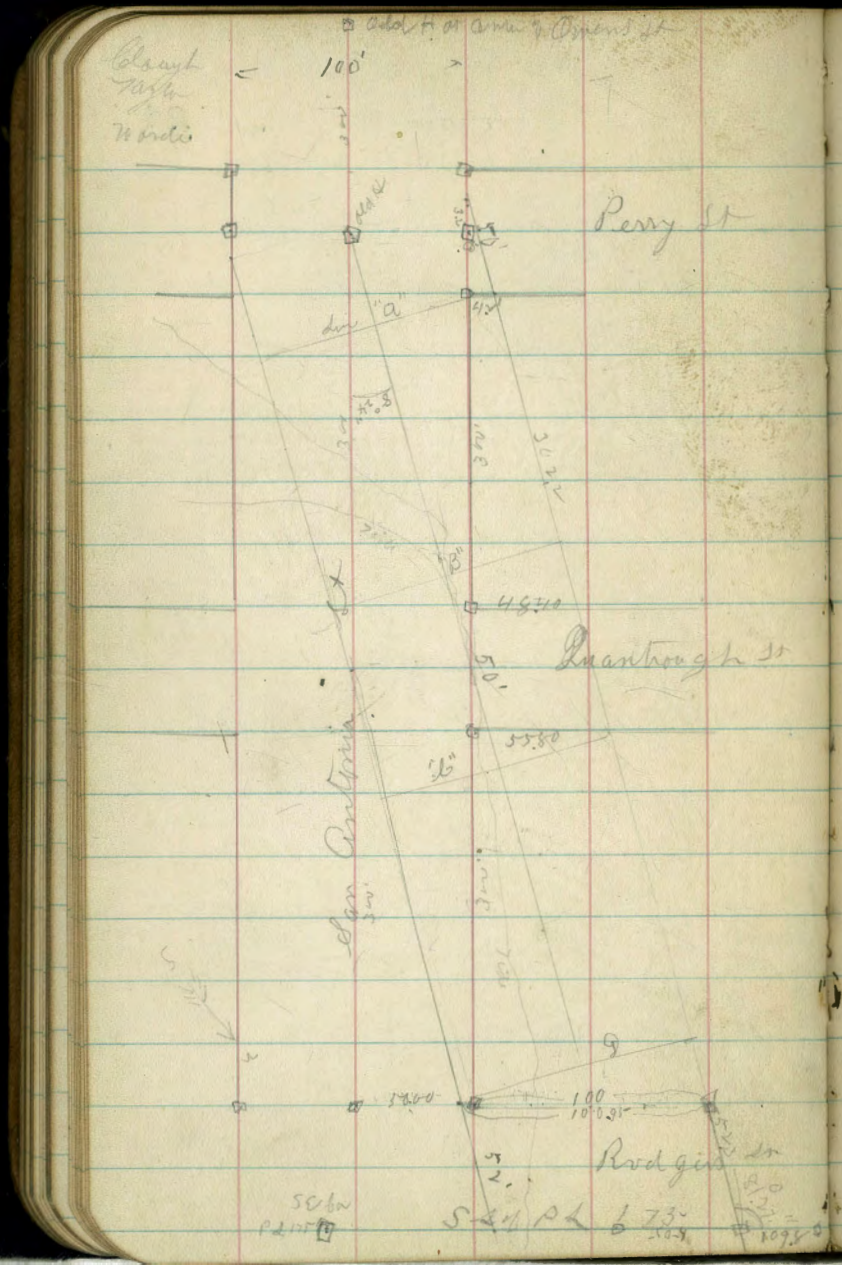
Posted

P

19+0		25.05	7.7	17.3
19+35			7.3	17.7
+45			4.5	20.5
20+0			4.5	20.5
21+00			4.6	20.4
22+0			4.9	20.1
T.P	2.65	23.84	3.86	21.19
23+0			4.6	19.2
24			4.1	19.7
25			4.7	19.1
B.C. 25+43.08			7.0	16.8
25+50			7.9	15.9
25+65			6.5	17.3
+75			4.5	19.3
26+0			4.5	19.3
26+25			5.2	18.6
+50			4.9	18.9
+75			2.2	21.6

		P1		
27+0		23.84	0.2	23.6
E.C. 27+16.53			0.2	23.6
T.P	5.22	28.56	0.50	28.34
28+00			5.9	22.7
29+00			5.8	22.8
T.P	10.64	34.28	4.92	23.64
30+00			9.8	24.5
30+50			3.5	30.8
T.P	11.90	44.31	1.87	32.41
31+00			7.1	37.2
31+25			6.1	38.2
31+45			6.3	38.0
31+55=Δ			7.2	37.1
31+75			7.3	37.0
32+00			8.6	35.7
32+50			8.6	35.7
33+00			8.0	36.3
33+25			7.7	36.6

		H.I 44.31		
33+50			6.2	38.1
3 T.P	8.54	44.82	8.05	36.28
34+00			4.2	40.6
34+15			7.0	37.8
34+50			4.9	39.9
Intersection ▷			3.6	41.2
				T.P
T.P.	1.485	37.765		36.28
T.P.	2.645	29.18	16.23	26.535
				B.M 22.94
			6.31	22.87



Change in Location of North End of San Antonio St

Jo P. Cayo

0.14	46.09		45.95	BM ++ Cut Sd Pd 175-
0.41	144.0	12.10	33.99	
3.19	245.8	13.01	21.39	++ on Pd
2.68	179.3	9.33	15.25-	
2.73	125.6	8.10	9.83	BM ++ NW Cor Perry & San Antonio

Center Line of Perry St (59)

WL	2.3
11	4.6
7	6.5-
6	8.2
7	9.8
11	11.1
EL	12.5-

1256

N'ly of Perry st

El	12.9
bk	11.4
4	10.3
6	8.5
4	6.6
bk	4.6
WL	2.1

N'ly of Perry st

WL	2.2
bk	5.0
4	6.9
6	9.0
4	10.6
bk	11.5
El	13.1

1256 San Antonio

N'ly of Perry st

El	13.4
bk	12.3
4	10.8
6	9.5
4	7.3
bk	4.9
WL	1.9

N'ly in Perry } line "C"
14' N'ly Perry }

WL	1.9
bk	4.8
4	7.5
6	9.4
4	10.9
bk	12.5
El	13.5

12.56

	50'	n of	Perry St	
EL			15,8	
bk			13,6	
y			12,5	
b			9,5	
y			7,7	
bk			4,3	
WL			1,6	
	100'	n of	Perry St	
WL			0,0	
bk			2,5	
y			5,0	
b			7,4	
y			10,5	
bk			14,0	
EL			16,0	

12.56 San Antonio

64

	150'	n		
EL			16,0	
bk			14,0	
y			11,7	
b			7,0	
y			4,2	
bk			1,7	
TD	9,66	20,36	1,86	10,70
WL			6,4	
	175'	n of	Perry	
WL			6,7	
bk			8,9	
y			11,4	
b			14,2	
	200'	n of	Perry St	
WL			3,0	
bk			7,8	
y			11,5	
TD			13,0	

POSTED

2036

	225'	n of	Perry	
wk			4.7	
bk			7.4	
4			10.4	
+5			12.0	
n	250	n of	Perry	
wk			0.4	
bk			5.3	
4			9.5	
+7			11.5	
TP	5.40	2073	5.03	15.33
	275'	n of	Perry	
wk			1.0	
bk			5.2	
+10			8	

2073

Line, "B" (14' Sof Quantrough
288 n = (S 2 " " E

wk	0.5
bk	4.8
+10	7.0
	S Div of Quantrough at 50'
wk	1.2
bk	3-4
4	9.0
	S bk of Quantrough at
wk	0.2
bk	7.4
4	9.5
	S 1/4 of Quantrough at
wk	1.2
bk	1.2
4	10.7

San Antonio 1918

2073

Center of Quantrough St

WL		1.6
bl		8.2
4		11.4

N bl of Quantrough

WL		1.6
bl		8.2
4		10.4

N bl of Quantrough

WL		6.5
bl		7.5
4		9.5

N Line of Quantrough

WL		6.2
bl		6.9
4		9.0

2073

San Antonio St

Line "B" = {N bl Quantrough on W / 10' N " " E}

WL			0.2	
bl			6.7	
4			9.0	
TP	6.41	2.66	5.48	15.25

25' N of Quantrough

WL		6.0
bl		6.4
4		8.2

50' N of Quantrough

WL		7.0
bl		5.8
4		9.5

75' N of Quantrough

WL		6.3
bl		7.2
4		12.5
TT		13.5

	100'	n of	Quantrough
WL			1,4
bk			7,0
4			10,4
	125'	n of	Quantrough
WL			1,7
bk			8,2
4			11,2
	150'	n of	Quantrough
WL			1,0
bk			10,0
4			13,0
	175'	n of	Quantrough
WL			1,6
bk			5,5
4			11,0

	200'	n of	Quantrough
WL			1,6
bk			5,3
4			11,0
	225	n	
WL			1,6
bk			6,0
4			10,8
b			15,0
	250'	n of	Quantrough
WL			3,1
bk			6,6
4			10,6
b			14,0
	288	n =	Line "D"
WL			3,9
bk			4,6
4			7,8
b			9,7

POSTED

2166

S Line Rodgers St 52

WL	3,7
bb	4,6
4	7,0
6	13,2

Sbb of Rodgers St

WL	3,0
bb	4,6
4	6,5
6	9,6

S 1/4 of Rodgers

WL	2,8
bb	4,8
4	5,7
6	8,1
4	10,0
bb	11,7

Strays to down

2166 San Antonio

Center of Rodgers St

WL	2,5
bb	4,8
4	5,4
6	7,2
4	9,0
bb	11,0

N 1/4 of Rodgers

WL	1,9
bb	4,8
4	7,8
6	6,8
4	8,7
bb	10,2

21.66

n bk of Rodgers

Wk	1,0
bk	4,0
y	4,5
b	6,2
y	8,6
bk	10,3

n d = SA P-2 175-

W2	0,2
bk	4,4
y	4,4
b	7,0
y	8,1
bk	10,5

Straight down

San Antonio

175' n of Perry

	9,83
E2	14,0
bl	13,2
y	12,0

BM of Perry

200 n b Perry

E2	13,0
bk	14,0
y	12,0
b	6,8

225 n b Perry

E2	13,6
bl	15,0
y	15,2
b	9,6

10.33

250' N of Perry

EL			13,5-
bl			13,4
4			14,5-
6			11,0
TP	4,28	1.66	12,95-

288' N of Sec 13 Quarter on E 14's cor on

E2			7,0
bl			6,5-
4			6,4
6			6,0
4			8,0

S2 of Dunthorpe

E2			6,9
bl			6,4
4			6,2
6			5-6
+10			1.0

1.66

Sec Section

S bl of Dunthorpe

E2			6,9
bl			6,9
4			6,4
6			6,2
+12			3,4

S 1/4 of

E2			6,9
bl			6,9
4			6,5-
6			6,2
+10			5,0

Center of Dunthorpe

E2			6,9
bl			6,9
4			6,5-
6			6,2
+10			5,2

16 L

N ¼ of Quantonyx

Et	69
bl	69
4	64
l	62
+00	30

N bl of Quantonyx

Et	69
bl	68
4	66
l	62
+81	2.6

N Dia of Quantonyx

Et	69
bl	6,8
4	6,2
l	4,6
+8	2,7

16 O

San Antonio

14' N on E = Sine "6"

E	69
bl	68
4	5-2
b	4,3
+b	2,0

50' N of Quantonyx

Et	7,3
bl	7,1
4	6,0
l	3,1-

100 N of Quantonyx

Et	7,0
bl	6,9
4	7,2
b	2,0

150' n of Quantrough

El	7,8
bk	7,9
4	7,4
6	4,0

200 n of Quantrough

El	8,0
bk	7,4
4	5,5
6	2,0

250 n of Quantrough

El	7,6
bk	6,3
4	4,3

288 n = Sta "D" Sdiv of Rodgers E

El	7,3
bk	5,8
4	2,4

Sdiv of Rodgers

El	7,2
bk	5,8
4	2,0

S bk of Rodgers

El	7,2
bk	5,5
4	0,0

S 1/4 of Rodgers

El	7,2
bk	5,0

Center of Rodgers

El	7,0
bk	5,0

N bk of Rodgers

El	6,8
bk	4,8

1.66

2 Lbs of Rivets

62 66

66 48

2 Lbs of Rivets = 52 pcs 175-

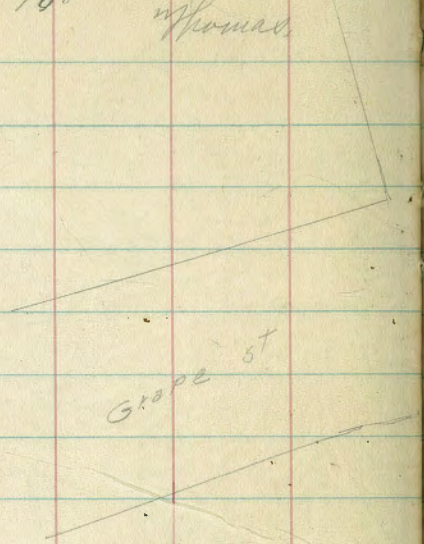
62 64

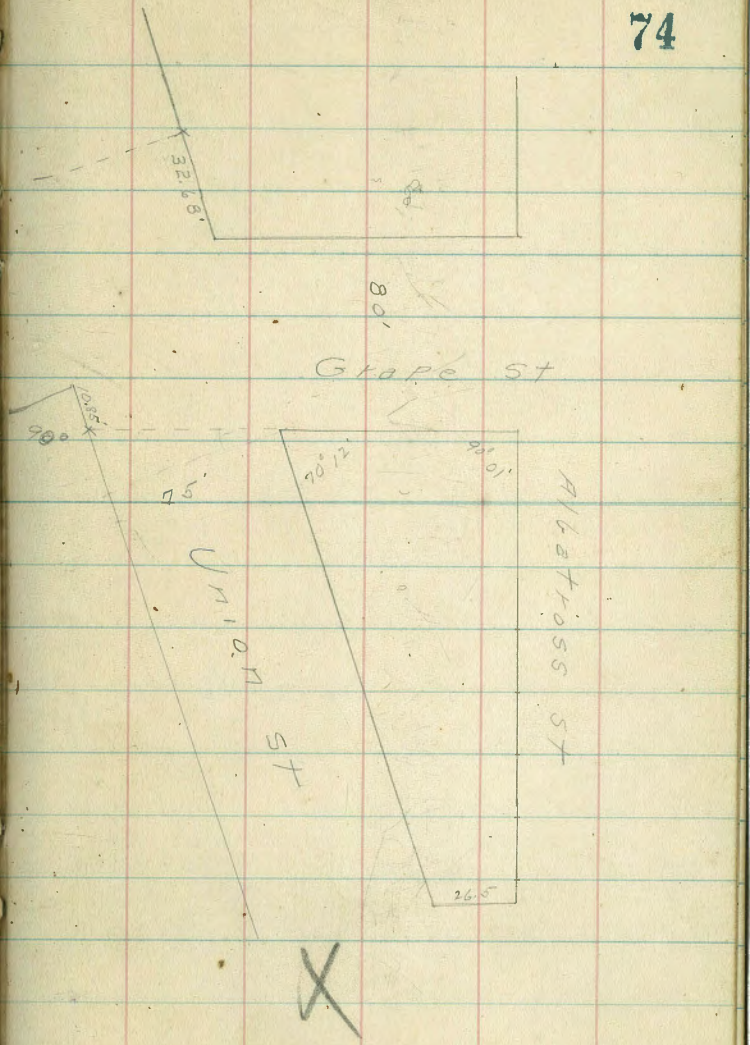
66 48

Straight-Wk

POSTED

12/29/08 Dunfee Sham Thomas





Levels for storm sewer on Grapest
E.L. California to Bay
Levels taken on lines 14' & 24' N of center 17/29 Dunkle 1908 Ham Thomas.

B.M. brass plg S.W. Cor Indiana Grape				44.02
B.M.	1.06	45.08		44.02
T.P.	0.54	33.16	12.46	32.62
T.P.	0.90	21.15	12.91	20.25

0+0 = E.L. Calif

14' N of ctr	3.3	17.9
24' " " "	2.1	

0+14 = E. Eond. bar culvert

24' N of c=center bottom culvert	4.0	
+14 " " "	1.9	19.3

0+25 X

14' N of C	2.4	18.8
24' " "	2.4	

0+27.6 = N. rail of 1st switch

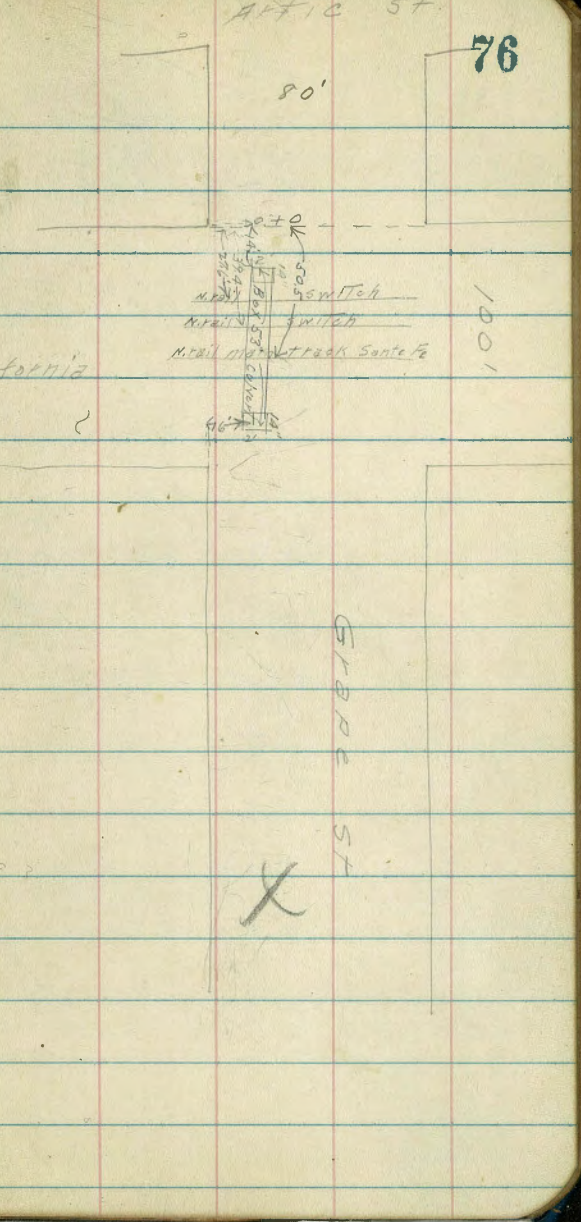
24' N. of c	2.2	

0+39.4 = N rail 2nd switch

24' N. of Ctr.	2.5	

0+49.55 = S. rail main track

24' N of ctr	2.7	



21.15

0+50 = center Calif

14' N of ctr Calif	2.8	18.6
24' " " "	2.7	
0+67 = W. end box culvert		
24' N of ctr bottom Culvert	8.3	
14' " " "	5.2	16.0
0+75		
14' N of C	6.8	14
24' " " "	7.8	
1+0 = W. L. Calif		
14' N of ctr	6.0	15.2
24' " " "	7.5	
1+25		
14' N of ctr	4.8	16.4
24' " " "	6.3	
1+40		
14'	5.1	16.1
24'	6.2	
1+44		
14'	9.4	11.8
24'	9.9	
1+50		
14'	11.2	10.0
24'	11.5	
1+62		
14'	9.8	11.4
24'	10.5	
1+65		
14'	7.0	14.2
24'	7.2	
1+75		
14	7.5	13.7
24	7.9	

		21.15				9.07	
		2+0				3+04	
14' N of ℄			9.1	12.1	14' N of ℄	5.9	3.2
24' " " "			9.7		24' " " "	5.9	
		2+25				3+08	
14'			10.9	10.3	14'	11.8	-2.7
24'			11.1		24'	11.4	
		2+50				3+25	
14'			12.7	8.5	14'	13.7	-4.6
24'			12.7		24'	13.8	
T. P.	0.87	9.07	12.95	8.20			
		2+75					
14'			2.4	6.7			
24'			2.1				
		3+0					
14'			4.7	4.4			
24'			4.5				

Levels on "A" Line Pt Loma Blvd from Kemper to Sta 54 to Sherman Gate Inv

	5+42	255.26	2+984	BM	
255.26					
12.29		12+12.6	44.8		
242.97					
0.76					
243.73	S.	234.87	14.8	220.1	
12.92					
230.81					
4.04	C		13.1	221.8	
234.87					
	N		10.8	222.1	
		12+50			
N		234.87	5.8	229.1	
C			9.6	226.3	
S.			12.8	222.1	
		13+00			
N		243.75	3.3	240.5	
C.			7.9	235.9	
S.			12.0	231.8	
		13+25			
S		255.26	17.2	238.1	
C			11.2	244.1	
N			3.8	251.5	

	13+50			
N		255.26	-0.5	255.8
C			5.0	250.3
S			15.0	240.3
	13+75			
S.			14.9	240.4
C			10.4	244.9
N.			5.8	249.5
	13+84.8 = P.T.			
N			20.7	234.6
C			12.5	242.8
S			14.8	240.5
	14+00			
S			15.4	239.9
C			14.8	240.5
N			10.9	244.4

			14+50 Hil.							17+00		
N			25576		5.9	244.4	E			25807	16.8	241.3
C.					8.3	247.0	C				13.3	244.8
S.					11.2	244.1	N			17+25	9.4	246.7
			14+75				N				5.6	255.5
S.					2.2	253.1	C				8.1	250.0
C					7.0	248.3	E				28.7	247.4
N					8.8	246.5				17+50		
T.P	7.09	258.07	4.28	250.98			E				10.9	247.2
			14998				C				9.1	247.0
E.					2.5	250.6	N			25807	7.7	250.4
C.					1.5	256.6				18+00		
N.					7.0	265.1	N			25807	7.3	246.8
			15+50				C				13.9	244.2
N					6.0	257.1	E				15.3	244.8
C					10.1	249.0	T.P	1.18	246.87		12.38	245.69
E					16.3	241.8				18+50		
			16+00				N				4.2	247.9
E					13.5	244.6	C				5.8	241.1
C.					8.6	249.5	E				12.4	243.5
N.					4.4	253.7				19+00		
			16+50				E				10.9	236.0
N					4.2	253.9	C				8.6	238.3
C					10.4	247.7	N.				7.1	239.8
E					16.5	241.6						

19+48.5 Prob Cr.

W.	24687	8.6	236.3	
C		10.0	236.9	
E		12.5	234.4	
	20+00			
E		11.9	235.0	
C		10.1	236.8	
W.		9.4	239.5	
	20+50			
W		7.8	239.1	
C		9.9	237.0	
E		11.9	235.0	
	20+60 = break			
E	24687	11.6	235.3	
C		9.9	237.0	
W.		9.9	239.0	
T.P.	5.77	243.59	9.05	237.82
	20+65			
E		13.3	230.3	
C		10.4	233.2	
W		11.1	232.5	
	21+00			
E		14.4	229.2	
C		14.3	229.3	
W.		11.8	231.8	

243.59

21+25

W			7.2	236.6
C			10.6	239.0
E			12.1	231.5
	21+35			
E			9.2	234.4
C			2.8	240.8
W			9.8	237.8
	21+50			
W			0.2	243.4
C			2.6	241.0
E			8.5	235.1
	22+00			
E		24359	6.3	237.3
C				
T.P.	1.53	255.11	0.01	243.58
E			11.7	243.4
W			9.1	246.0
	22+50			
W			2.9	252.2
C			4.0	251.1
E			7.8	247.3

		755.11									
T.P.	8.90	762.90	W	754.00				24+72.9			
		23+00				W		762.90	4.9	758.0	
						C			12.1	750.8	
E				8.1	754.8	E			18.2	744.7	
C				6.7	756.2						
W				5.0	757.9			25+00			
		23+50				E			17.5	745.4	
									10.5	752.4	
W				3.3	759.6	W			3.5	759.4	
C				9.6	753.3						
E				13.4	749.5			24+50			
		23+65				W			7.8	760.1	
						E			8.2	753.7	
E				10.9	756.0	E			14.1	749.8	
C				5.7	751.2						
W				3.5	759.4			26+00			
		24+00				E		762.90	10.2	752.7	
									2.5	760.4	
W				5.0	757.9	C	T.P.	12:35	2.08	760.82	
C				7.3	755.6	W			7.2	756.0	
E				9.6	753.3			26+50			
		24+50				W			5.0	764.2	
E				16.5	746.4	C			7.5	765.6	
C				11.2	751.7	E			14.8	758.3	
W				5.9	757.0						
								27+00			
						E			7.0	764.2	
						C			5.9	765.3	
						W			4.2	769.0	

		27+50						30+50			
W		273.17		4.4	268.6	W			8.2	277.3	
C				7.0	266.9	C			9.9	277.6	
E				9.8	263.4	E			11.8	270.1	
		28+00						30+60			
E				9.7	263.5	E			12.4	271.4	
C				7.0	266.2	C			9.7	277.9	
W				4.5	268.7	W			8.3	277.7	
		28+50						31+00			
W				3.7	268.5	W			5.8	276.7	
C				5.7	267.6	C			6.5	276.0	
E				9.6	263.6	E			7.6	277.9	
		29+00						31+50			
E		273.17		7.6	265.6	S		282.45	4.5	278.0	
C				4.5	268.7	E			2.5	280.0	
T.P.	1306	282.45		5.78	269.39	T.P	1280	293.37	1.88	280.57	
W				11.1	271.4	W			12.1	269.3	
		29+50						32+00			
W				14.5	271.0	W			6.8	286.6	
C				13.5	269.0	E			7.5	285.9	
E				16.3	266.4	S			7.7	285.7	
		30+00						32+50			
E				14.3	268.4	S			2.4	291.0	
C				11.9	270.6	E			1.7	291.7	
W				10.5	271.0	W			0.4	293.0	

		293.37		
T.P.	9.82	302.17	10.2	292.35
		33400		
N			5.9	987.5
E			6.5	986.9
S.			7.9	985.5
		33450		
S.			4.6	988.8
E			3.7	989.7
N			2.2	991.2
			12.6	289.55

26.74 23.55
3.19 87.0 23.21
23.55 3225 3.33
20.70

26.69
2.58
29.57

37.12
10.43
26.69

37.14 38.79
34.36
2.78

50.18
11.39

18.98
1.33
20.31

Published by H. S. Crocker Company, Stationers, Drawing Materials. Mathematical Instruments, etc., San Francisco.

TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100.00	0.44	100.00	0.87	99.99	1.31	89
1	99.98	1.75	99.98	2.18	99.97	2.62	99.95	3.05	88
2	99.94	3.49	99.92	3.93	99.91	4.36	99.88	4.80	87
3	99.86	5.23	99.84	5.67	99.81	6.10	99.79	6.54	86
4	99.76	6.98	99.73	7.41	99.69	7.85	99.66	8.28	85
5	99.62	8.72	99.58	9.15	99.54	9.58	99.50	10.02	84
6	99.45	10.45	99.41	10.89	99.36	11.32	99.31	11.75	83
7	99.25	12.19	99.20	12.62	99.14	13.05	99.09	13.49	82
8	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	15.64	98.70	16.07	98.63	16.50	98.56	16.93	80
10	98.48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98.16	19.08	98.08	19.51	97.99	19.94	97.90	20.36	78
12	97.81	20.79	97.72	21.22	97.63	21.64	97.53	22.07	77
13	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	24.19	96.92	24.62	96.81	25.04	96.70	25.46	75
15	96.59	25.88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.82	73
17	95.63	29.24	95.50	29.65	95.37	30.07	95.24	30.49	72
18	95.11	30.90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35.43	69
21	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38.67	67
23	92.05	39.07	91.88	39.47	91.71	39.87	91.53	40.27	66
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	43.84	89.69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	46.95	88.09	47.33	87.88	47.72	87.67	48.10	61
29	87.46	48.48	87.25	48.86	87.04	49.24	86.82	49.62	60
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	52.99	84.57	53.36	84.34	53.73	84.10	54.10	57
33	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	52
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	45
45	70.71	70.71							

Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees
	DEGREES		¾ DEGREE.		½ DEGREE.		¼ DEGREE.		