400

LEVEL

F.B. 425

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Table showing the difference of latitude and departure in running 80 chains at any course from 1 to 60 minutes.

425

MINUTES.	LKS.	MINUTES.	LKS.	MINUTES.	LKS.
1	2⅓	21	49	41	95⅔
2	4⅔	22	51⅓	42	98
3	7	23	53⅔	43	100⅓
4	9⅓	24	56	44	102⅔
5	11⅔	25	58⅓	45	105
6	14	26	60⅔	46	107⅓
7	16⅓	27	63	47	109⅔
8	18⅔	28	65⅓	48	112
9	21	29	67⅔	49	114⅓
10	23⅓	30	70	50	116⅔
11	25⅔	31	72⅓	51	119
12	28	32	74⅔	52	121⅓
13	30⅓	33	77	53	123⅔
14	32⅔	34	79⅓	54	126
15	35	35	81⅔	55	128⅓
16	37⅓	36	84	56	130⅓
17	39⅔	37	86⅓	57	133
18	42	38	88⅔	58	135⅓
19	44⅓	39	91	59	137⅔
20	46⅔	40	93⅓	60	140

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TABLE FOR RUNNING ON SLOPES.

In the following table the first column shows the angle, the second the number of links to be added to a chain on the slopes, to make one chain, horizontal measurement.

ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS
°		°		°		°	
4	0.24	11	1.88	18	5.14	25	10.54
5	0.38	12	2.24	19	5.76	26	11.26
6	0.55	13	2.63	20	6.42	27	12.24
7	0.76	14	3.06	21	7.11	28	13.37
8	0.98	15	3.53	22	7.85	29	14.34
9	1.24	16	4.02	23	8.64	30	15.47
10	1.55	17	4.56	24	9.47	35	22.07

Clough Bothell Wendt

Crossection of Macauley St (60')

Continued from Book #24

16305-

50' W of Angle

SL			11.3	151.8
BL			11.5	151.6
"			11.8	151.3
C			12.0	151.1
"			12.3	150.8
BL			12.9	150.2
NL			13.3	149.8
TP	2.29	15340	11.94	151.11
	100'	W		
NL			7.7	145.7
BL			7.3	146.1
"			6.9	146.5
C			6.4	147.0
"			6.0	147.4
BL			5.7	147.7
SL			5.8	147.6

POST

15340

127' W

SL	7,9	145,5
bk	9,0	144,4
y	8,6	144,8
b	8,8	144,6
y	9,3	144,1
bl	10,0	1434
wh	10,0	1434

127' W of S Jct Edwy RR Roy Way
165' W of S Jct Edwy RR Roy Way

wh	10,0	1434
bl	10,2	143,2
y	10,1	143,3
b	10,0	143,4
y	10,0	1434
br	9,0	144,4
SL	7,4	145,0

15340 Macauley Dr

2

+ 14' W of E-W RR Roy Way (Top of Bank)

SL	1,3	152,1
bl	1,6	151,8
y	1,8	151,6
b	1,9	151,5
y	2,1	151,3
bl	2,0	151,4
wh	2,4	151,0

30' W = W RR Bank

wh	2,4	151,0
bl	2,1	151,3
y	2,2	151,2
b	2,2	151,2
y	1,8	151,6
bl	1,5	151,9
SL	1,3	152,1

POST

15-340

43'w = w line of Rt of way

SL			9,1	144,3
6			9,5	143,9
5			11,0	142,4
4			12,0	141,4
3			12,0	141,4
2			13,0	140,4
1			13,0	140,4
IP	1,04	141,96	12,48	140,92

31'w of Rt of way on n line = 127'Eg between ons

n1			5,0	137,0
2			4,5	137,5
3			4,3	137,7
4			3,9	138,1
5			2,9	139,1
6			0,6	141,4
SL				144,3

141,96 Macaulay

100' E of between ons

SL	5,8	136,2
1	6,6	135,4
2	6,7	135,3
3	7,0	135,0
4	6,7	135,3
5	6,6	135,4
n1	6,5	135,5

(450) 50' E of between ons
40' E of between ons

n1	8,6	133,4
2	8,5	133,5
3	8,5	133,5
4	8,4	133,6
5	8,2	133,8
6	8,0	134,0
SL	7,7	134,3

14196

E Side of Catalina Blvd

S 2	7.7	134.3
"	8.1	133.9
"	8.4	133.6
"	8.7	133.3
"	8.8	133.2
"	9.0	133.0
N 2	9.3	132.83

Cross section of Alley from West line of Pueblo Ave E line of Iowa Ave to Alley East of Anaheim St (60')

	293	211.75	208.82
	W line of Anaheim St (60')		
S2		8.4	203.4
1		8.8	203.0
4		9.3	202.5
6		9.8	202.0
4		10.3	201.5
6		11.0	200.8
N2		11.7	200.1
	W 1/4 of Anaheim St		
N2		12.2	199.6
1		11.6	200.2
4		10.8	201.0
6		10.0	201.8
4		9.6	202.2
6		9.0	202.8
S2		8.4	203.4

	211.75		Alley East
	W 1/4 of	Anaheim St	
S2		8.6	203.2
1		9.0	202.8
4		10.0	201.8
1		10.5	201.3
4		11.0	200.8
1		11.7	200.1
N2		12.6	199.2
	Center of Anaheim		
N2		13.0	198.8
1		12.0	199.8
4		11.2	200.5
1		10.2	201.5
4		9.7	202.1
1		9.1	202.7
S2		8.4	203.4

POSTED

211.75

E ½ of Anakota

SL			8,8	203,0
bL			9,5	202,3
7			10,1	201,7
6			10,7	201,1
7			11,3	200,5
bL			12,1	199,7
mL			13,3	198,5

E bL of Anakota

mL			13,5	198,3
bL			14,7	199,1
4			14,0	198,8
6			11,1	200,7
7			10,4	201,4
bL			9,5	202,3
SL			8,9	202,9
TP	1,50	204,06	9,19	202,60 SBM 202,86 Anakota

204,06 Alyphant

E line of Anakota "

SL	1,50	202,6
L	2,0	202,1
7	2,6	201,5
6	3,3	200,8
4	4,20	199,9
bL	5,4	198,7
mL	6,2	197,9

50° E of Anakota

mL	9,5	194,6
bL	8,4	195,7
4	7,3	196,8
6	6,6	197,5
4	5,7	198,4
bL	4,8	199,3
SL	4,0	200,1

2040.06

	100	E	Analemma	
SL			7,1	197,0
bL			8,2	195,9
4			9,2	194,9
L			10,4	193,7
4			11,6	192,5
bL			12,6	191,5
nL			13,7	190,4
TP	250	19361	12,95	191,11

	150	E	Analemma	
nL			8,2	185,4
M			6,1	187,5
4			4,7	188,9
b			3,4	190,2
4			2,6	191,0
tL			1,4	192,2
SL			0,4	193,2

19361

Alcyphant

7

	200	E	Analemma	
SL			4,4	189,2
bL			5,5	188,1
4			6,9	186,7
b			8,2	185,4
4			9,0	184,6
M			10,2	183,3
nL			11,9	181,7

	250	E	Analemma	
nL			15,2	178,0
bL			14,1	179,5
4			13,5	180,1
L			12,4	181,2
4			10,9	182,3
M			10,1	183,5
SL			9,0	184,6
TP	050	18128	12,83	180,78

POSTED

18128

	275°	E of Anakapa		
S2			0.80	180.5
bl			2.0	179.3
4			2.7	178.6
6			3.9	177.4
4			5.5	175.8
bl			6.8	174.5
N2			8.7	172.6
	300°	E of Anakapa		
N2			13.9	167.4
bl			12.5	168.8
4			11.4	169.9
6			10.3	171.0
4			8.9	172.4
bl			8.1	173.2
S2			6.7	174.6
TP	0.45	16901	12.72	168.52

16901 Ellyfhant 11

360°	360°	E = W dir of	Warmington (60')	
S2			5.4	163.6
bl			6.7	162.3
4			7.7	161.3
6			8.7	160.3
4			9.7	159.3
bl			10.8	158.2
N2			11.4	157.6
	W-bl of	Warmington		
N2			12.4	156.6
bl			11.3	157.7
4			10.6	158.4
6			9.9	159.1
4			8.7	160.3
bl			8.0	161.0
S2			6.7	162.3

16901

W ¼ of Warrington

SL		8.7	160.3
¼		9.7	159.3
1		10.2	158.7
¼		11.3	157.7
½		12.1	156.9
¾		13.3	155.7
NL		13.9	155.1

Cents of Warrington

NL		14.6	154.4
¾		13.8	155.2
½		12.5	156.5
¼		11.8	157.2
1		10.9	158.1
¾		10.1	158.9
SL		9.5	159.5
TP	3.40	160.98	11.43	157.58	Bm SL Warrington

16098

Oglethorpe

E ¼ of Warrington

SL		2.4	158.6
¾		3.6	157.4
½		3.7	157.3
¼		4.6	156.4
1		5.5	155.5
¾		6.8	154.2
NL		7.5	154.5

E ¾ of Warrington

NL		8.6	153.4
¾		7.5	153.5
1		6.6	154.4
¼		5.7	155.3
½		4.9	156.1
¾		4.0	157.0
SL		2.1	157.9

160.98

E Line of Warrington

S2		161.0	2,40	157.6
bl			4,9	156.1
4			5,5	155.5
b			6,0	155.0
4			7.1	153.9
bl			7,8	153.2
N2			9.1	151.9

50 E of Warrington

N2			12,7	148.3
bl			11,7	149.3
4			10,5	150.5
b			9,8	151.2
4			9,0	152.0
bl			8,1	152.9
S2			7,3	153.7
TP	0,45	148.82	12.81	148.17

148.82 Alyphant 10

100' E of Warrington

S2		148.8	2.1	146.7
bl			3,1	145.7
4			3,6	145.2
b			4,5	144.3
4			4,6	144.2
bl			5,6	143.2
N2			6,4	142.4

125'

N2			9,8	139.0
bl			9,7	139.1
bl			8,4	140.4
b			8,0	140.8
4			7,4	141.4
bl			6.6	142.2
S2			6,0	142.8

POSTED

1488

	150' E of		Warrington
SL	148.8	8,2	140.6
bl		8,8	140.0
y		9,2	139.6
l		10,3	138.5
y		11,8	137.0
bl		12,7	136.1
nL		13,2	135.6
TP	0,47	13632	12,97	135,85

	200' E of	Warrington
SL		1,3	135.0
bl		2,0	134.3
y		2,8	133.5
b		3,6	132.7
y		4,3	132.0
bl		6,1	130.2
nL		5,8	130.5

13632

Alyshurst 2

	250' E of	Warrington
nL		12,0	124.3
bl		11,5	124.8
y		10,8	125.5
b		9,5	126.8
y		8,9	127.4
bl		8,0	128.3
SL		7,9	128.4
TP	0,12	12390	12,54	12378

	300' E of	Warrington
SL		0,4	123.5
bl		1,3	122.6
y		1,1	122.8
b		1,6	122.3
y		2,5	121.4
bl		2,5	120.4
nL		5,0	118.9

POSTED

123.90

350 E of Warrington

BR		123.9	9,8	114.1
bl			9,3	114.6
y			8,8	115.1
l			7,8	116.1
y			7,1	116.8
bl			6,1	117.8
SL			5,9	118.0

400 E of Warrington

SL			10,5	113.4
bl			11,0	112.9
y			10,6	113.3
l			11,3	112.6
y			11,7	112.2
bl			12,5	111.4
BR			12,8	111.1
TP	090	112.51	12,9	181.61 TP

112.51 Clyphant

450 E of Warrington

BR		112.5	3,7	108.8
bl			3,4	109.1
y			3,5	109.0
l			3,4	109.1
y			3,3	109.2
bl			2,9	109.6
SL			2,4	110.1

500 E of Warrington

SL			5,7	106.6
bl			6,2	106.3
y			6,4	106.1
l			6,7	105.8
y			6,8	105.7
bl			7,1	105.4
BR			7,2	105.3

POSTED

1125-1

	550'	E of Warning		
SL		112.5	10.1	102.4
L			9.6	102.9
L			9.4	103.1
L			9.6	102.9
L			9.4	103.1
L			9.8	102.7
SL			8.9	103.6
	600'	E of Warning		
SL			11.4	101.1
			11.8	100.7
			12.7	99.8
			13.2	99.3
			14.2	98.3
			14.0	98.5
			14.5	98.0
TP	6.10	106.73	11.86	100.63 ✓ Brass in bolthead

106.73 Elephant V

	647'	E = Wing of bolthead		(70')
SL		106.7	6.10	100.6
L			6.8	99.9
L			7.3	99.4
L			8.0	98.7
L			8.6	98.1
L			8.9	97.8
NL			9.5	97.2
	Side of bolthead			
NL			9.0	97.7
L			8.6	98.1
L			8.0	98.7
L			7.5	99.2
L			7.6	99.1
L			6.3	100.4
SL			5.2	101.1

10673

W ¼ of blk 100

S2	106.7	5.0	101.7
11		5.8	100.9
10		6.4	100.3
9		7.2	99.5
8		7.5	99.2
7		8.3	98.4
N2		8.8	97.9

Center of blk 100

N2		8.7	98.0
7		8.2	98.5
8		7.7	99.0
9		7.0	99.7
10		6.1	100.6
11		5.6	101.1
S2		4.5	102.2

10673 Oythaut

E ¼ of blk 100

S2	106.7	4.8	101.9
11		5.4	101.3
10		6.2	100.5
9		7.0	99.7
8		7.8	98.9
7		8.5	98.2
N2		8.9	97.6

E 6th of blk 100

N2		8.4	98.3
7		8.0	98.7
8		7.3	99.4
9		6.6	100.1
10		5.7	101.0
11		5.0	101.7
S2		4.7	102.5

10.6.73

	Ε Lin	ϕ	blutwert
S2	106.7	4,9	101.8
bl		5,0	101.7
4		6,5	100.2
b		7,2	99.5
4		7,9	98.6
bl		8,5	98.2
n2		9,2	97.5

	5-0	Ε ϕ	blutwert
n2			6,9 99.8
bl			6,6 100.1
4			6,4 100.3
b			6,0 100.7
4			5,7 101.0
bl			5,1 101.6
S2			4,5 102.2

10.6.73 Olympia

	160	Ε ϕ	blut wert
S2	106.7	6,4	100.3
bl		7,4	99.3
4		8,5	98.2
bl		9,2	97.5
4		8,8	96.9
bl		10,3	96.4
n2		10,4	96.3

	12,5	Ε ϕ	blut wert
n2			12,2 94.5
bl			11,0 95.7
4			10,5 96.2
bl			9,1 97.6
4			8,5 98.2
b			7,6 99.1
S2			6,9 99.8

10.6.73

150 E of Chatsworth			
SL	12,0	94.7	
M	12,4	94.3	
Y	13,0	93.7	
L	13,6	93.1	
Y	13,9	92.8	
M	14,3	92.4	
ML	14,5	92.2	
175 E of Chatsworth			
ML	13,4	93.3	
M	11,9	94.8	
Y	10,4	96.3	
L	9,0	97.7	
Y	8,4	98.0	
M	7,7	99.0	
SL	6,8	99.9	

10.6.73 Clyphant II

200 E of Chatsworth			
SL	7,8	98.9	
M	8,5	98.2	
Y	9,0	97.7	
L	12,8	93.9	
Y	11,5	95.2	
M	10,9	95.8	
ML	11,5	95.2	
230 E of ML of Brandola Rd (60°)			
ML	9,6	97.1	
M	9,1	97.6	
Y	8,1	98.6	
L	7,9	98.8	
Y	7,3	99.4	
M	6,6	100.1	
SL	6,2	100.5	
TP 1051	111,06	6.18	100,55

POSTED

111.06

W bb of Mendota 10

SL	9,8	101.2
bL	10,4	100.6
4	11,0	100.0
b	11,5	99.5
4	11,8	99.2
bL	12,7	98.3
nL	13,4	97.6

N b/4 of Mendota

nL	12,9	98.1
bL	12,3	98.7
4	11,5	99.5
b	11,0	100.0
4	10,5	100.5
bL	9,9	101.1
SL	9,4	101.6

111.06 Clyphant

Centr of Mendota

SL	8,7	102.3
bL	9,3	101.7
4	9,8	101.2
b	9,9	101.1
4	10,3	100.7
bL	11,0	99.7
nL	12,2	98.6

E b/4 of Mendota

nL	11,0	100.0
bL	10,7	100.3
4	9,6	101.4
b	9,0	102,0
4	9,2	101.8
bL	8,8	102.2
SL	8,4	102.6

11106

E bk of of Mendota

S L	8,0	103.0
bk	8,2	102.8
4	8,7	102.3
L	8,7	102.3
4	8,8	102.2
bk	9,6	101.4
N L	10,4	100.6

E L of Mendota

N L	7,8	101.2
bk	9,2	101.8
4	8,8	102.2
L	8,7	102.3
4	8,6	102.4
bk	8,1	102.9
SL	8,0	103.0

11106 Clay Farm

50' E of Mendota

SL	7,4	103.6
bk	7,9	103.1
4	8,4	102.6
L	8,6	102.4
4	9,0	102.0
bk	9,2	101.8
SL	9,4	101.6

100' E of Mendota

N L	7,2	103.8
bk	6,9	104.1
4	6,9	104.1
L	6,7	104.3
4	6,4	104.6
bk	6,1	104.9
SL	5,8	105.2

111.06

	150'	E of	Mean data	
S2			3,4	107.6
1			3,5	107.5
4			3,6	107.4
3			3,6	107.4
4			3,5	107.5
1			3,6	107.4
N2			4,0	107.0
TP	12,63	12369	0,0	111,06
	200	E of	Mean data	
N2		123.7	11,6	111.4
1			11,5	112.2
4			11.4	112,3
3			11,5	112.2
4			11,9	111.8
1			12,0	111.7
S2			11,8	111,9

12369 Alyphant ss

	225'	E =	N Side of Cofferdam (60)	
S2		123.7	9,4	114.3
1			9,4	114.3
4			9,6	114.1
3			9,3	114.4
4			9,3	114.4
1			9,2	114.5
N2			8,7	115.0
		N 1/2 of	Cofferdam	
N2			7,4	116.3
1			7,8	115.9
4			8,2	115.5
3			7,7	116.0
4			8,3	115.4
1			8,4	115.3
S2			8,5	115.2

12369

W ¼ of Capistrano

SL	123.7	7,2	116.5
M		7,3	116.4
4		7,5	116.2
6		7,2	116.5
4		7,3	116.4
M		6,8	116.9
NL		6,3	117.4

Center of Capistrano

NL		5,5	118.2
M		5,8	117.9
4		6,2	117.5
6		6,0	117.7
4		6,2	117.4
M		6,0	117.7
SL		6,0	117.7

12369

City Plans

E ¼ of Capistrano

SL	123.7	4,5	119.2
M		4,4	119.3
4		4,5	119.2
6		4,9	118.8
4		5,4	118.3
M		5,2	118.5
NL		4,8	118.9

E M of Capistrano

NL		4,2	119.5
M		4,5	119.2
4		4,6	119.1
6		4,2	119.5
4		4,0	119.7
M		3,7	120.5
SL		4,0	120.7
TP	484	12647	2,10	12159

Brn SE of Capistrano

POSTED

12647

E line of Capistrano

				Bm
S2		126.5	4.90	121.59
1			5.2	121.3
4			5.7	120.4
1			6.0	120.5
4			6.6	119.9
1			6.4	120.1
N2			6.4	120.1

50' E of Capistrano

N2			3.7	122.6
1			3.5	123.0
4			3.2	123.3
1			3.0	123.5
4			2.9	123.6
1			2.7	123.8
S2			1.9	124.6

12647 Alythan et

100 E of Capistrano

S2		126.5	1.1	125.4
1			1.8	124.7
4			2.3	124.2
1			2.6	123.9
4			2.8	123.7
1			3.0	123.5
N2			3.6	122.9

130 E of Capistrano

N2			7.7	114.8
1			7.1	119.4
4			6.4	120.1
1			5.0	121.5
4			3.5	123.0
1			2.3	124.2
S2			1.8	124.7

12647

150' E of Copestone

SL		126.5	4,0	122.5
BL			4,6	121.9
4			5,6	120.9
L			6,8	119.7
4			7,1	119.4
BL			7,2	119.3
NL			7,5	119.0

175' E of Copestone

NL			8,3	118.2
BL			8,2	118.3
4			8,8	117.7
L			8,8	117.7
4			7,7	118.8
BL			6,6	119.9
SL			6,2	120.3

12647 Clyphant sa

200 E of Copestone

SL		126.5	9,8	116.7
BL			10,3	116.2
4			10,9	115.6
L			11,5	115.0
4			12,0	114.5
BL			12,6	113.9
NL			13,3	113.2
TP	0,12	114.61	11,28	114,49

255' E of = Junction of (60)

NL			9,4	105.2
BL			8,7	105.9
4			8,0	106.6
L			7,7	106.9
4			7,3	107.3
BL			7,0	107.6
SL			6,7	107.9

POSTED

11461

W bk of Trustin st

SL		114.6	8,3	106.3
bk			8.8	105.8
y			9,0	105.6
b			9,4	105.2
y			9,9	104.7
bk			10,5	104.1
NL			11,0	103.6

W y of Trustin st

NL			12,5	102.1
bk			11,9	102.7
y			10.6	103.0
b			11,0	103.6
y			10,6	104.0
bk			10,1	104.5
SL			9,9	104.7

11461

Elephant st

Center of Trustin st

SL			11,4	103.2
bk			11,9	102.7
y			12,6	102.0
b			12,5	102.1
y			12,8	101.8
bk			13,5	101.1
NL			13,6	101.0
TP	0,00	101.93	12,68	101.93

E y of Trustin st

SL		101.9	0,0	101.9
bk			0,4	101.5
y			0,7	101.2
b			1,0	100.9
y			1,4	100.5
bk			1,8	100.1
NL			2,0	99.9

101,93

E Ext of Trustin st

N2	101.9	2,8	99.1
M		2,7	99.2
4		2,4	99.5
L		2,1	99.8
4		1,9	100.0
M		1,6	100.3
S2		1,1	100.8

E Lin of Trustin

S2		2,01	99,92
M		2,5	99.4
4		2,8	99.1
L		3,0	98.9
4		3,2	98.7
M		3,4	98.5
N2		3,5	98.4

BM 53 Trustin

101,93 Elephant st

30' E of Trustin st

N2	101.9	6,0	95.9
M		6,0	95.9
4		5,7	96.2
L		5,6	96.3
4		5,4	96.5
L		4,7	97.2
S2		4,1	97.8

30' E of Trustin

S2		5,6	96.3
M		6,4	95.5
4		7,3	94.6
L		8,0	93.9
4		8,2	93.7
M		8,8	93.1
N2		9,6	92.3

101,93

	16v	E of	Justin	
N2		101.9	16,8	85.1
bl			15,4	86.5
y			13,4	88.5
l			12,3	89.6
y			11,0	90.9
bl			9,9	92.0
S2			9,0	92.9
TP	0,33	93.06	9,20	92,73
	15-4	E = intersection of	Elsmere	on Nauls
S2		93.0	0,1	92.9
bl			2,0	91.0
y			4,0	89.0
l			5,7	87.3
y			7,4	85,6
bl			9,2	83.8
N2			11,3	81,7

9306 Elysburg et

	17-4	E = nbl of	Elsmere	
N2		93.0	9,5	83.5
bl			8,0	85.0
y			7,2	85.8
l			6,1	86.9
y			4,5	88.5
bl			3,1	89.4
S1			1,2	91.8
	19.4'	E =	2c 4-8	Elsmere
S2			0,2	92.8
u			1,3	91.7
y			3,0	90.0
l			4,3	88.7
y			6,0	87,0
bl			7,5	85.5
N2			8,9	84.1

9306

2½4' E = Center of Elsinore

N2	93.0	9.6	83.4
W		6.1	86.9
Y		5.3	87.7
L		4.5	88.5
Y		2.9	90.1
W		1.6	91.4
S2		0.4	92.6

2½4' E = E ½ of Elsinore

S2		1.1	91.9
W		1.9	91.1
Y		3.1	89.9
L		4.9	88.1
Y		6.1	86.9
W		7.4	85.6
N2		9.2	83.8

9306

2½5' E = {West side of Elsinore / E ½ of Elsinore

N2	93.0	11.2	81.8
W		9.8	83.2
Y		8.5	84.5
L		6.7	86.3
Y		5.5	87.5
W		3.9	89.1
S2		2.9	90.1

W ½ of Elsinore

S2		2.5	90.5
W		4.0	89.0
Y		5.6	87.4
W		7.2	85.8
Y		8.7	84.3
W		10.7	82.3
N2		12.1	81.9

POSTED

9306

275° ε = Intensität der Linie des Elsinan

NR	93.0	12,4	80.6
M		10,9	82.1
4		9,0	84.0
1		7,0	86.0
4		5,4	87.6
M		3,5	89.5
SR		2,4	90.6

Centrum des Blume 25

SR		2,6	90.4
M		3,7	89.3
4		5,0	88.0
1		6,3	86.7
4		8,5	84.5
M		10,9	82.1
NR		13,3	79.7

9306 Elysium

ε 1/4 des Blume 25

NR	93.0	14,0	79.0
M		12,0	81.0
4		9,8	83.2
1		7,1	85.9
4		5,6	87.4
M		4,0	89.0
SR		2,7	90.3

ε M des Blume 25

SR		3,0	90.0
M		4,3	88.7
4		5,2	87.4
1		7,8	85.2
4		10,1	82.9
M		12,3	80.7
NR		14,6	78.4

9366

		E line	℄	blow	el
			93.0	16,3	77.7
				13,5	79.5
				11,0	82.0
				8,1	84.9
				6,1	86.9
				4,6	88.4
				3,6	89.4
TP	0,05	8949		3,62	8944
	50'	E ℄		blow	
			89.5	7,1	82.4
				9,6	79.9
				12,4	77,1
TP	0,09	7746		12,12	77,37
			77.5	4,0	73.5
				4,8	72.7
				7,7	69.8
				10,0	67.5

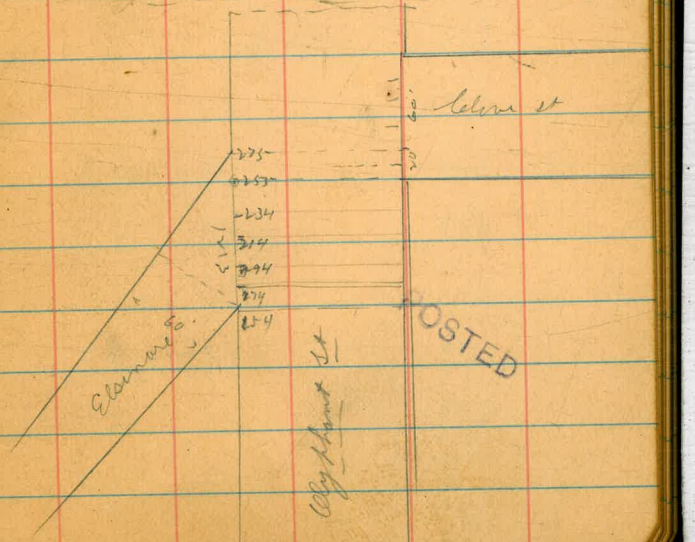
Bm SE blow

7746 Alley Plant St

755' E ℄ blow = Pueblo line

	77.5	15,5	62.0
		12,9	64.6
		10,2	67.3
		6946	Bm
		.775	6971
		5,3	72.2
		2,5	752
		0,8	79.4

Alley Plant St is 70' wid E ℄ this



Crossection of Elsinore St (60')
From E line of Catalina to end at Skyblest

E line of Catalina = 192' W of Rt of way on N. Bm SE Catalina

	12,56	14,80		129.24
SR			12,6	129.2
bl			12,5	129.3
y			12,5	129.3
b			13,0	128.8
y			13,4	128.4
bl			13,3	128.5
NR			13,4	128.6

47' E on N } = 150' W of RR on N
20 E on S }

NR			9,1	132.7
bl			9,3	132.5
y			9,8	132.0
b			10,0	131.8
y			9,9	131.9
bl			10,0	131.8
SR			10,0	131.8

14,80 Elsinore St

100' W of Rt of way on N

SR		141.8	6,6	135.2
bl			6,4	135.4
y			6,0	135.8
b			5,1	136.8
y			4,4	137.4
bl			4,0	137.8
NR			3,7	138.1

75' W of Rt of way

NR			0,2	141.6
bl			1,1	140.7
y			1,4	140.4
b			2,3	139.5
y			3,2	138.6
bl			4,0	137.8
SR			4,8	137.0

		141.80			
	50'	W of	Rt of	way	n
SL		141.8	3.7	138.1	
"			2.9	138.9	
"			2.0	139.8	
"			1.2	140.6	
"			0.4	1414	
TP	9.00	150.57	0.29	141.51	
"			8.0	142.5	
n2			7.3	143.2	
	15'	W of	Rt of	way	n
n2			6.0	144.5	
"			6.5	144.0	
"			7.2	143.3	
"			8.3	142.2	
"			9.2	141.3	
"			9.6	140.9	
SL			9.6	140.9	

150.57 Elsmere

+29.5 E of S } = w line of RR Rt of way (36)
+15.5 E of n }

SL	150.5	7.0	143.5	
"		7.0	143.5	
"		6.6	143.9	
"		4.0	146.5	
"		1.0	149.5	
"		1.0	149.5	
n2		4.0	146.5	
10'E = W line RR Bank				
n2		0.4	150.1	
"		0.7	149.8	
"		0.8	149.7	
"		0.8	149.7	
"		1.0	149.5	
"		0.8	149.7	
SL		0.6	149.9	

15057

Top of Bank

+162 = 10' W of ℄ line of RR R/W

S2	150.5	0.4	150.1
11		0.4	150.1
4		0.5-	150.0
6		0.5-	150.0
7		0.5-	150.0
11		0.5-	150.0
N2		0.4	150.1

+75' = 5' W of ℄ line of RR R/W

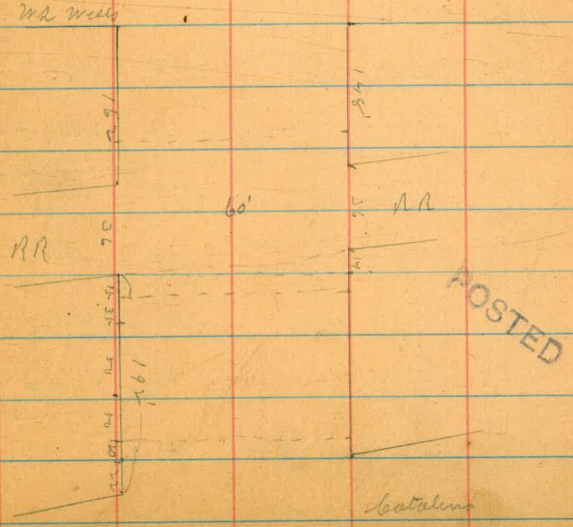
N2	1.6	148.9
11	2.6	147.9
4	3.4	147.1
1	3.9	146.6
4	4.1	146.4
11	4.1	146.4
S2	3.8	146.7

15057

Elevations

E line of RR R/W of way = {162' N of Wells on N / 148 N of Wells on S

S2	150.5	3.4	147.1
11		3.6	146.9
4		3.5-	147.0
1		3.1	147.4
4		2.8	147.7
11		1.8	148.7
N2		1.1	149.4
TP	12.12	162.48	0.13- 150.36



162.48

62' E of RR on N } 100' W of Wells
48' E of Bldg S }

N2	162.5	8,2	154.3
M		8,7	153.8
4		9,2	153.3
3		9,3	153.2
2		9,9	152.6
M		10,1	152.4
S2		10,3	152.2

50' W of Wells

S2		5-3	157.2
M		4,7	157.8
3		4,6	157.9
2		3,6	158.9
1		2,8	159.7
M		2,6	159.9
N2		2,3	160.2
T.P	1210 17436	0,2 W	16226

17436 Elevations

W Side of Wells at (60')

N2	174.4	8,2	166.2
M		8,9	165.5
4		9,7	164.7
3		8,8	165.6
2		9,5-	164.9
M		9,0	165.4
S2		8,1	166.3

W side of Wells at

S2		6,2	168.2
M		6,5	167.9
4		7,0	167.4
3		6,8	167.6
2		6,6	167.8
M		7,5-	166.9
N2		7,0	167.4

17436

W ¼ of Wells at

N2		174.4	5.6	168.8
"			6.6	167.8
"			5.2	168.8
"			5.8	168.6
"			5.8	168.6
"			4.8	169.6
S2			4.4	170.0

Center of Wells at

S2			2.7	171.7
"			2.1	171.3
"			2.4	171.0
"			3.5	170.9
"			2.5	171.9
"			2.4	171.0
N2			3.0	171.4

17436 Elsinore St

E ¼ of Wells at

N2		174.4	0.8	173.6
"			0.4	174.0
"			1.2	173.2
"			1.6	172.8
"			1.2	173.2
"			0.8	173.6
S2			0.3	174.1
TP	9.04	183.22	0.18	174.18

Elev of wells at

S2		183.2	5.8	177.4
"			6.2	177.0
"			6.6	176.6
"			6.8	1764
"			6.3	176.9
"			6.4	1768
N2			5.7	177.5

POSTED

1832

E line of Wells at

NL	183.2	3,54	179.68	3m NE Wells
M		2,4	180.8	
L		2,0	181.2	
K		2,0	181.2	
J		1,5	181.7	
H		1,2	182.0	
SL		0,4	182.8	

50' E of Wells at

SL		1,6	181.6
M		2,4	180.8
L		3,2	180.0
K		4,3	178.9
J		5,0	178.2
H		5,9	177.3
NL		6,5	176.7

1832

Elsinore

100 E of Wells at

NL	183.2	11,4	171.8
M		10,2	173.0
L		9,1	174.1
K		7,3	175.9
J		5,8	177.4
H		4,5	178.7
SL		4,0	179.2
TP	0,0	175.97	7,25 175.97

150 E of Wells at

SL		+0,4	176.3
M	176	1,1	174.9
L		3,0	173.0
K		4,3	172.7
J		5,9	170.1
H		7,1	168.9
NL		7,9	168.1

1759-97

	270°	E of	Wells	st
N 2		176.0	10,9	165.1
1			10,6	165.4
4			9,5	166.5
6			8,0	168.0
4			7,0	169.0
1			6,0	170.0
S 2			4,7	171.6
	270°	E = W line of	Anaconda (60')	
S 2			5,6	170.4
1			6,7	169.3
4			7,8	168.2
6			8,7	167.3
4			10,0	166.0
1			11,0	165.0
N 2			12,6	163.4

1759-97 Elsmere st

	W line of	Anaconda	st
N 2	176.0	13,0	163.0
1		11,8	164.2
4		11,0	165.0
6		9,7	166.3
4		8,5	167.5
1		7,2	168.8
S 2		6,2	169.8
	W line of	Anaconda	st
S 2		7,2	168.8
1		8,4	167.6
4		8,6	166.4
6		10,8	165.2
4		12,0	164.0
1		13,1	162.9
N 2		14,0	162.0

POSTED

175.97

Center of Anacapa st

h2		176.0	14.7	161.3
bl			13.4	162.6
4			12.4	163.6
6			11.0	165.0
4			10.4	166.0
bl			9.0	167.0
S2			7.6	168.4

E 1/4 of Anacapa

S2			8.2	167.7
bl			9.7	166.3
4			10.8	165.2
6			12.1	164.0
TP	0.59	167.01	9.55	166.42
4			4.5	162.5
bl			5.5	161.5
h2			7.0	160.0

167.01

Elsinore st

E bl of Anacapa

h2		167.0	7.9	159.1
bl			6.3	160.7
4			5.4	161.6
6			4.0	163.0
4			2.8	164.2
bl			1.4	165.6
S2			0.0	167.0

Elsin of Anacapa st

BM S2 Anacapa

S2			0.59	166.42
bl			2.2	164.8
4			3.3	163.7
6			4.7	162.3
4			6.5	160.5
bl			7.0	159.7
h2			8.8	158.2

POSTED

167.01

	50	E-f	Anacapa ↓	
M2		167.0	14,7	152.3
bb			12,7	154.3
y			11,4	155.6
l			9,3	157.7
y			7,6	159.4
M			6,8	160.2
S2			5,0	162.0
TP	0,40	155,23	14,8	154.83
	100	E-f	Anacapa ↓	
S2			10,4	154.8
bb			1,8	153.4
y			3,2	152.0
l			5,8	149.4
y			6,5	148.7
bb			7,9	147.3
M2			9,0	146.2

155.23

Elsinore ↓

	150	E-f	Anacapa	
M2		155.2	15,9	139.3
bb			13,6	141.6
y			12,8	142.4
l			11,8	143.4
y			9,8	145.4
M			8,7	146.5
S2			7,2	148.0
TP	0,16	142,78	12,61	142,62
	200	E-f	Anacapa ↓	
S2		142.8	3,2	139.6
M			4,1	138.7
y			5,6	137.2
l			7,0	135.8
y			7,6	135.2
M			8,8	134.0
M2			9,0	133.8

14278

	250'	E of	Anaeapa st	
M2		142.8	12,1	130.7
M			11,6	131.2
"			10,7	132.1
L			10,1	132.8
"			9,0	133.8
LL			9,2	133.6
S2			7,2	135.6
	300'	E of	Anaeapa st	
S2			9,4	133.4
LL			9,8	133.0
"			10,5	132.3
L			11,6	131.2
"			12,2	130.6
M			13,2	129.6
M2			14,0	128.8

14278 Elsinore st

	360'	E= W line of	Warrington st	60
N2		142.8	17,0	125.8
LL			16,3	126.5
"			15,4	127.4
L			14,4	128.4
"			13,8	129,0
LL			13,0	129,8
S2			12,50	130,5
TP	151	131,92	12,30	13048 Brn Sw Warrington
	NLL of		Warrington	
S2		132.0	1,8	130.2
LL			2,6	129.4
"			3,2	128.8
L			3,7	128.3
"			4,3	127.7
LL			5,7	126.3
M2			6,3	125.7
			6,5	

13199

	N 1/4 of	Warrington	
N2	132.0	6,8	125.2
6		6,2	125.8
4		5,4	126.6
6		4,6	127.4
4		4,2	127.8
6		3,0	129.0
S2		2,1	129.9
	Center of	Warrington	
S2		2,4	129.6
6		3,4	128.6
4		4,2	127.8
6		5,1	126.9
4		5,7	126.3
6		6,5	125.5
N2		7,0	125.0

13199

Elevations

	E 1/4 of	Warrington	
N2	132.0	7,2	124.8
6		6,5	125.5
4		5,8	126.2
6		4,8	127.2
4		4,1	127.9
6		3,2	128.8
S2		2,6	129.4
	E 6t of	Warrington	
S2		0,1	129.9
6		3,5	128.5
4		4,4	127.6
6		5,0	127.0
4		6,2	125.8
6		7,0	125.0
N2		8,0	124.0

		13.99		
	Elm of Warrington			
NL			8.0	124.0
bl			7.2	124.8
y			6.2	125.8
l			5.2	126.8
y			4.5	127.5
bl			4.0	128.0
SL			3.6	128.4
	50'	E of	Warrington	
SL			8.5	123.5
bl			8.5	123.5
y			9.0	123.0
l			9.3	122.7
y			9.9	122.1
bl			10.6	121.4
NL			10.9	121.1
TP	1.57	120.62	12.94	119.04

		120.62		Elsinore St
	100'	E of	Warrington	
NL			3.8	116.8
bl			3.8	116.8
y			3.5	117.1
l			3.4	117.2
y			3.3	117.3
bl			2.9	117.7
SL			3.0	117.6
	150	E of	Warrington	
SL			7.5	113.1
bl			7.7	
y			8.0	
l			8.1	112.5
y			8.5	
bl			8.9	
NL			8.7	111.9

		1067		
	200'	E of	Warrington	
M2			14,3	106.3
M			13,0	
4			13.8	
6			13,3	107.3
7			12.8	
8			12,3	
S2			11,8	108.8
TP	1,48	109,55	12,52	108.10
	250'	E of	Warrington	
S2			4,4	105.2
8			4,6	
7			4,6	
6			4,8	104.8
5			5,2	
4			5,7	
M2			6,2	103.4

		1095		Elsinore 11
	300'	E of	Warrington	
M2			7,7	101.9
4			7,6	
5			7,4	
6			7,5	101.1
7			7,4	
8			7,3	
S2			6.8	104.8
	350'	E of	Warrington	
S2			8,1	101.5
8			8,5	
7			8,7	
6			9,0	100.6
5			9,4	
4			9,6	
M2			9,7	99.9

10955

	400	E of	Warrington	
M2			10,9	98.7
11			10,7	
7			10,4	
6			10,2	99.4
4			10,0	
11			9,8	
S2			9,5	100.1
	450	E of	Warrington	
S2			10,2	99.4
11			10,5	
7			10,7	
6			10,7	98.9
4			10,8	
11			11,1	
M2			11,4	98.8
TP	0,99	98,47	12,07	97,48

98.47

Elsinore 1st

	500	E of	Warrington	
M2			3.1	95.4
11			2,3	
4			2,3	
6			2,2	96.3
7			1,8	
11			1,8	
S2			1,4	97.1
	550	E of	Warrington	
S2			3,7	94.8
11			4,5	
4			5,1	
6			5,8	97.7
4			5,3	
11			6,1	
M2			6,5	97.0

POSTED

98.47

	Coal	E of	Warrington	
Nl			9.5	89.0
bl			9.0	
7			8.2	
6			7.3	91.2
5			6.2	
4			5.4	
Sl			4.7	93.8
TP	0.25	91.33	7.41	91.06

68 ft Brn Sh
Ground

Coal E = Nl in of Blackrock Mill (70)

Sl			0.2	91.1
bl			0.7	90.6
7			1.3	90.0
6			2.6	88.7
5			3.8	87.5
4			4.5	86.8
Nl			4.9	86.4

91.33 Elevation at

Nbl of Blackrock Mill

Nl	5.3	86.0
bl	5.1	86.2
7	4.7	86.6
6	4.1	87.2
5	3.9	88.4
4	3.1	89.2
Sl	1.5	89.8

Nl of Blackrock Mill at

Sl	3.1	88.2
bl	3.7	87.6
7	4.6	86.7
6	5.5	85.8
5	6.0	85.3
4	6.2	85.1
Nl	6.1	85.2

9133

Center of Chelsea at

N2	6.4	84.9
11	6.3	85.0
7	6.0	85.3
6	5-8	85.5
4	5-4	85.9
11	4-5-	86.8
S2	3.8	87.5

E ½ of Chelsea

S2	4.6	86.7
11	5-4	85.9
7	6.0	85.3
6	6.6	84.7
4	6.8	84.5
11	7.2	84.1
N2	7.3	84.0

9133 Elsinore st

Ebb of Chelsea

N2	8.5	87.8
11	7.8	83.5
7	7.5-	83.8
6	7.3	84.0
4	6.7	84.6
11	6.0	85.3
S2	5-4	85.9

Elsinore of Chelsea

S2	5-4	85.7
11	6.6	84.7
7	7.6	83.7
6	8.2	83.1
4	8.2	83.1
11	8.5-	82.8
N2	9.2	82.1

9133

	50°	E of	blots	want
N2			11,4	79.9
4			11,0	80.3
3			10,5	80.8
2			10,1	81.2
1			9,8	81.5
1			9,2	82.1
S2			8,8	82.5
	100°	E of	blots	want
S2			9,4	81.9
4			9,7	81.6
3			10,1	81.2
2			10,4	80.9
1			10,8	80.5
4			11,4	80.8
N2			11,9	79.2
TP	890	9028	9935	8738

9028

Elsmare w

	140°	E of	blots	want
N2			13,4	76.9
4			12,4	77.9
3			11,9	78.4
2			11,3	79.0
1			10,7	79.6
4			10,2	80.1
S2			9,7	80.6
	150°	E of	blots	want
S2			12,8	77.5
4			12,7	77.6
3			12,6	77.7
2			12,7	77.6
1			12,9	77.4
4			12,8	77.5
N2			13,0	77.3

90.28

	155'	E of	Abutment	Invert
N2			12.0	78.3
6			11.6	78.7
4			11.2	79.1
6			10.9	79.4
7			10.7	79.9
6L			10.0	80.7
S2			9.8	80.5
	200'	E of	Abutment	
S2			5.0	85.3
6L			4.2	86.1
4			4.0	86.7
6			3.8	86.5
6			3.1	87.7
6L			2.8	87.5
N2			3.1	87.7
TP	1220	101.67	0.81	89.47

101.67

Elevation of

	250'	E of	Abutment	Invert
N2			5.8	95.9
6L			5.8	95.9
7			5.7	96.0
6			5.7	96.0
7			5.7	96.8
6L			6.0	95.7
S2			6.3	95.4
TP	566	105.91	1.42	100.25
	200'	E of	Abutment	Invert
S2			3.3	102.6
6L			3.5	102.4
7			3.7	102.2
6			4.1	101.8
7			4.8	101.1
6L			5.5	100.4
N2			6.5	99.4

POSTED

10-5-91

	350'	E 6	blobs	mm
N2			7,9	98.0
bl			>,3	98.6
4			6,1	99.8
b			4,9	101.0
4			3,7	102.2
bl			3,0	102.9
S2			2,5-	103.4

	400'	E 6	blobs	mm
S2			6,7	99.2
bl			7,5-	98.6
3			8,3	97.6
1			9,3	96.6
2			10,2	95.7
b			11,2	94.7
N2			14,4	93.5

10-5-91

Elsinore 10

	450'	E 6	blobs	mm
N2			15,7	90.2
bb			13,3	92.6
4			12,4	93.5
b			11,9	94.0
4			11,9	94.0
bl			10,9	95.0
S2			10,1	95.8
TP	04,5-	95-36	11,00	94,91

371 E 1= N2 Capistrano (60')

S2			1,7	97.7
bl			3,10	97.3
4			4,7	90.7
b			6,3	89.1
2			8,2	87.2
b			9,5-	85.9
N2			12,1	83.3

POSTED

95-36

NBL Corpus Luteum

N2	12.1	83.3
1	10.6	84.8
2	8.8	86.6
3	7.0	88.4
4	5.0	90.4
5	3.1	92.3
S2	2.0	93.4

W½ of Corpus Luteum

S2	2.6	97.8
1	3.4	92.0
2	4.6	90.8
3	6.0	89.4
4	7.4	88.0
5	9.8	85.6
N2	12.0	83.4

95-36 Elsmon #1

Center of Corpus Luteum

N2	11.9	83.6
1	10.7	84.7
2	9.1	86.3
3	7.3	88.1
4	5.8	89.6
5	4.2	91.2
S2	2.9	92.5

E½ of Corpus Luteum

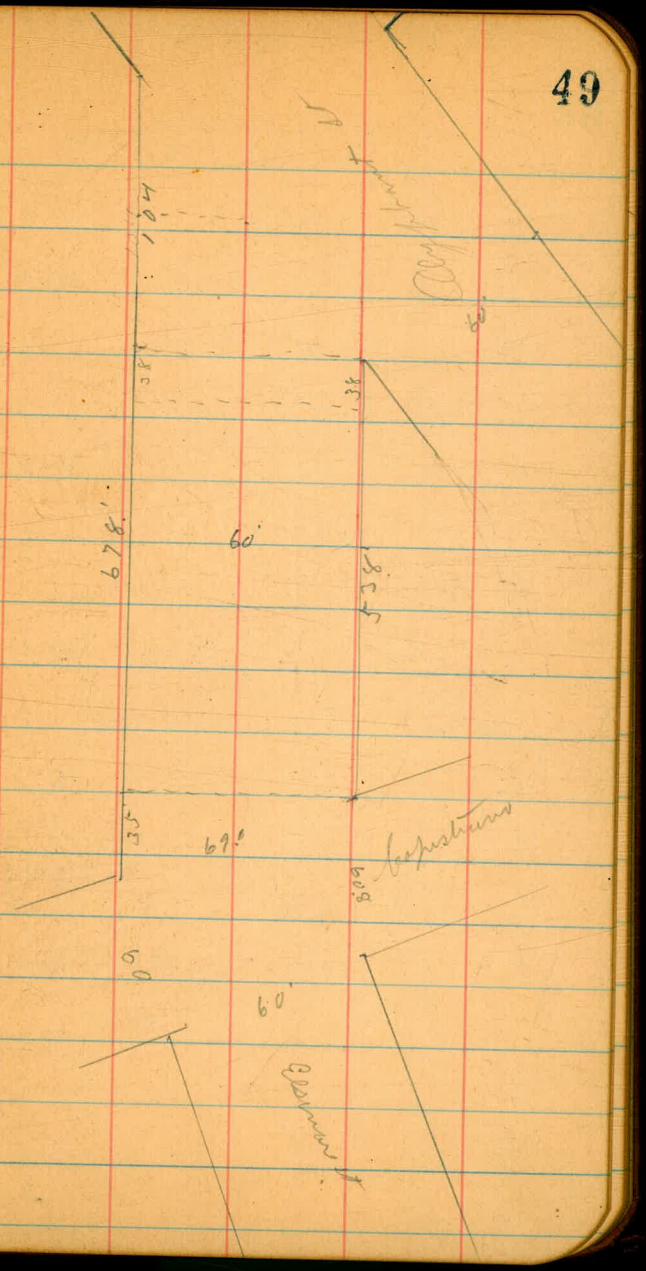
S2	2.8	92.6
1	3.7	91.7 POSTED
2	4.8	90.6
3	6.9	88.5
4	8.7	86.7
5	10.7	84.7
N2	11.7	83.7

95-96.

Elbow of Corporation

M2		11.3	84.1
"		9.9	85.5
"		9.0	86.4
"		7.6	87.8
"		5.5	89.9
"		2.1	93.3
S2		1.7	93.7 (69')
	E line of Corporation		
S2		1.5	93.9
"		2.3	93.1
"		4.6	90.8
"		6.8	88.6
"		7.4	88.0
"		8.4	87.0
M2		10.4	85.0
TP		11.5	94.21

Bm SE Corporation



35' E of Capistrano on N
SE Cor on S = 00

	8:08	10:29			BM SE Capistrano
SL			8,1	94.2	
bl			9,0		
y			11,3		
b			12,0	90.3	
y			12,0		
bl			12,0		
rd			12,3	90.0	

50' E of Capistrano

rd			11,2	91.1
bl			10,0	
y			9,3	
b			7,9	94.4
y			5,8	
bl			4,0	
SL			3,0	99.3

10:29 Elsinore

100 E of Capistrano

SL			0,0	109.3
bl			2,1	
y			3,4	
b			4,9	97.4
y			6,4	
bl			8,0	
rd			9,4	97.9

150 E of Capistrano

rd			10.6	91.1
bl			7,8	
y			6,2	
b			4,6	99.4
TP	7,72	10:57	4,44	97.85
y			3,4	
bl			2,8	
SL			0,2	107.1

POSTED

10557

185° E ч Барышник

S2	4,2	101.4	
1	6,3		
4	8,0		
2	9,6	96.0	
4	11,0		
1	13,2		
N2	15,8	89.8	

200° E ч барышник

N2	15,9	89.1	
1	12,6		
4	10,0		
6	9,3	96.3	
4	8,5		
1	7,1		
S2	4,7	100.9	

10557 Елизаветинская

230° E ч барышник

S2	5,0	100.6	
1	7,5		
4	9,6		
2	11,4	94.2	
4	13,0		
1	13,0		
N2	17,9	87.1	

250° E ч барышник

N2	18,5	87.1	
1	15,4		
4	13,6		
6	12,0	93.6	
4	9,4		
1	7,1		
S2	5,4	100.2	

105-7

	300	E y	bapsiteno	
SR			8,4	97.2
bl			10,6	
y			14,5	
TP	35-1	96,10	12,98	92,9
b			5,0	91.1
y			6,2	
bl			8,0	
nR			10,1	86.0

	325	E y	bapsiteno	
nR			8,5	87.6
bl			7,0	
y			6,0	
b			5,2	90.9
y			4,3	
bl			2,4	
SR			0,1	96.0

96.10

Esemare 10

	350	E y	bapsiteno	
SR			1,8	94.3
bl			3,7	
y			4,8	
b			5,7	90.4
y			7,0	
bl			8,6	
nR			10,2	85.9

	400	E y	bapsiteno	
nR			12,5	83.6
bl			11,6	
y			10,2	
b			9,3	86.8
y			7,6	
bl			6,3	
SR			5,0	91.1

Q6.10

	450'	E of	Capistrano	
S2			E,7	86.4
bl			10,6	
y			12,0	
b			13,2	87.9
TR	312	8641	1281	83.29
y			4,4	
bl			5,7	
M2			7,0	79.4
	500'	E of	Capistrano	
M2			14,5	71.9
bl			13,3	
y			10,4	
b			9,4	77.0
y			8,1	
fl			6,2	
S1			4,8	81.6

8641 Elsinore Dr

	5-10'	E y	Capistrano	
S2			7,5-	78.9
			8,8	
y			10,7	
b			12,8	73.6
y			14,0	
bl			15,8	
M2			17,9	68.5-
	5-38	E of =	Intersection of Alley plant ons	
M2			11,8	74.6
bl			10,5-	
y			9,2	
b			7,8	78.6
y			6,5-	
bl			5,7	
S2			4,7	81.7

8641

	5-58' E =	30' to Ctr of intersection	
nL		84	77.5
bl		80	
y		63	
d		45	81.9
y		35	
bb = nDir of Elyphat		24	840
	5-90' E =	30' to Cent of intersection	
nL		60	80 4
bl		50	
y		34	
b = nDir of Elyphat		18	84.6
	64' E =	intersection in nDir	
nL		59	80.5

Cross section of Poe st (60')
From E line of Catalina to the Bay
E line of Catalina

	124.3	139.80	127.37	Bm NE Catalina
N2		12,4	127.4	
4		12,2		
4		12,2		
1		11,8	128.0	
4		11,8		
4		11,9		
S2		11,7	128.1	
	00 on S2 } = 00			
S2		11,7	128.1	
4		11,6		
4		11,4		
6		11,0	128.8	
4		11,0		
4		11,1		
		11,4	128.4	

139,80 Poe st

50' E of Catalina ⌐ S

N2	8,2	131.5
4	8,0	
4	7,8	
1	7,8	132.0 x
4	8,0	131.8
4	8,4	
S2	8,1	130.7

90' E of Catalina

S2	5,4	134.4
4	5,9	
4	6,0	
1	5,6	134.2
4	5,7	
4	5,2	
N2	5,0	134.8

13980

	100	E f	Catalina	
N2			45-	13√.3
bl			4,4	
y			4,1	
l			4,6	13√,2
y			4,7	
bl			4,6	
S2			35-	136,3
T.P	12,64	15197	0,47	129,33

	130	E f	Catalina	
S2			6,6	14√.4
bl			7,3	
y			8,6	
l			11,0	141,0
y			12,1	
bl			12,2	
N2			12,8	139,2

15197

Pac st

	170	E f	Catalina	
N2			10,3	141.7
bl			9,1	
y			8,7	
l			8,4	143.6
y			9,0	
bl			7,0	
S2			5-2	146.8

	200	E f	Catalina	
S2			7,5-	144.√
bl			6,2	P
y			5-8	
l			5,7	146.3
y			5-9	
bl			5-9	
N2			6,2	14√.8

15-1.97

240' E = RR Rt of way cen n

NR	2,6	149.4	
1	3,0		
2	2,9		
3	3,2	148.8	
4	3,5		
5	3,7		
SR	4,0	148.0	

00 cen n
+11' E cen S sin } = w sin of Rt RR (36') of way (35)

SR	3,3	148.7	
1	3,2		
2	3,0		
3	2,8	149.2	
4	2,7		
5	2,7		
NR	2,6	149.4	

15-1.97 Page 57

25' E of w sin of Rt of way

NR	2,8	149.7	
1	2,7		
2	2,5		
3	2,4	1496	
4	2,3		
5	2,3		
SR	2,0	1V.0.0	

27' E of w sin of RR POC

SR	1,0	1V1.0	
1	0,9		
2	0,8		
3	0,9	1V1.1	
4	0,5		
5	0,8		
NR	0,2	1V1.8	
TP	808	160.05	00 15-1.97

1605-

E line of R R R/W way 227' N of mills S.
244 N of mills N

N2		8,1	1	2.0
M		7,8		
4		8,0		
6		8,4	1	1.7
4		8,4		
M		8,4		
S2		8,3	1	1.8
	20.5' N of Wells St =	22' E of R R R/W S		
S2		6,3	1	3.8
M		6,0		
4		6,2		
6		6,1	1	4.0
4		5,3		
M		4,6		
N2		4,1	1	6.0

1605-

Page 2

	200'	W of	Wells St	
S2			5,3	1 4.6
M			5,2	
4			5,0	
6			4,3	1 5.8
4			3,6	
	190	W of	Wells St	
S2			4,2	1 5.8
M			4,1	
4			3,9	
+8'			2,8	
	160'	W of	Wells St	
S2			1,0	1 9.1
TP	11.72	170.57	1,10	1595-
	200'	W of	Wells St	
N2			4,2	166.5
M			4,3	

POSTED

17067

	190'	wf	Wells	ot
m2			5.2	165.5
bl			4.0	
y			3.0	
b			3.0	167.7
	160'	wf.	Wells	
m2			8.0	162.7
bl			7.2	
y			5.9	
b			4.8	165.9
bl			3.4	
y			1.4	
75'			3.0	167.7

17067 Par et

	150'	wf	Wells	ot
SL			1.0	169.7
bl			2.8	
y			4.0	
b			5.3	165.4
y			6.6	
bl			7.8	
m2	140'	wf	8.8	161.9
	100'	wf	Wells	ot
m2			11.7	159.0
bl			10.6	
y			9.5	
b			8.6	162.1
y			8.0	
bl			7.0	
SL			6.2	164.5

17067

50' W of Wells at

SL			8,6	162.1	
bl			9,7		
y			10,5		
b			11,5	1V9.2	
y			12,3		
bl			13,2		
NL			13,9	1V6.8	
TP	1,02	16033	11,37	15-9,50	13m SW Wells

W Line of Wells at (60')

SL			1,0	1V9.3	
bl			1,7		
y			2,5-		
bl			3,2	1V7.1	
y			4,0		
b			4,8		
NL			5,8	1V4.V	

16033 Pac st

Nbl of Wells at

NL			6,2	1V-4.1	
b			5,2		
y			4,5-		
b			3,9	1V6,4	
y			3,0		
bl			2,0		
SL			1.1	1V9.2	

W'ly of Wells at

SL			1,5-	1V8.8	
bl			2,2		
y			3,1		
b			4,0	1V6.3	
y			4,8		
bl			5-6		
NL			66	1V3.7	

POSTED

160.33

	center of	wells at	
N2		7,0	1 V 3.3
4		6,3	
4		5,2	
6		4,3	1 V 6.0
4		3,6	
4		2,7	
S2		2,1	1 V 8.2
	E 1/4 of	wells at	
S2		2,5	1 V 7.8
4		3,2	
4		4,0	
6		4,8	1 V 5.5
4		5,7	
4		6,6	
N2		7,4	1 V 2.9

160.33

Par 2

	E 4 of	wells at	
N2		8,1	1 V 2.2
4		7,2	
4		6,1	
6		5,0	1 V 1.0
4		4,6	
4		3,7	
S2		3,0	1 V 7.3
	E 1/4 of	wells at	
S2		3,5	1 V 6.8
4		4,2	
4		5,1	
6		5,9	1 V 4.4
4		6,8	
4		8,0	
N2		8,9	1 V 1.4

POSTED

16033

	50'	E of	Wells	N
NL			13,0	147.3
bl			12,2	
y			11,3	
b			10,5	149.8
y			9,4	
bl			8,6	
SR			7,7	152.6
TP	0,96	15769	10,60	14973
	100'	E of	Wells	N
SR			1,0	1497
bl			1,5	
y			2,6	
b			3,4	147,3
y			4,0	
bl			4,9	
NL			5,7	145.0

15069

Pat

	150'	E of	Wells	N
NL			8,7	142.0
bl			7,6	
y			6,8	
b			6,0	1447
y			4,8	
bl			4,0	
SR			3,2	147.5
	200'	E of	Wells	N
SR			8,3	142.4
bl			9,6	
y			10,2	
b			11,5	139.2
y			13,0	
TP	0,60	13879	12,52	13817
bl			2,7	
NL			4,5	134.3

13879

	250'	E of	wells st	
N2			12,6	126.2
bl			12,0	
y			10,8	
b			9,7	129.1
y			8,8	
bl			7,6	
S2			6,5	132.3
7P	0.15'	12676	12,8	12661
	300'	E of	wells st	
S2			0,5	126.3
bl			1,2	
y			1,9	
b			2,7	124.1
y			3,4	
bl			4,2	
N2			4,6	122.2

12676 Par st

	350'	E of	wells st	
N2			8,3	178.5
bl			8,0	
y			7,4	
b			6,8	120.0
y			6,4	
bl			6,3	
S2			5,9	120.9
	400'	E of	wells st	
S2			8,1	118.7
bl			8,5	
y			9,1	
b			9,6	117.2
y			10,0	
bl			10,2	
N2			10,6	116.2

POSTED

12676

	450' E of	wells	
N2		11.6	115.2
ll		11.3	
y		10.6	
b		10.2	116.6
y		9.7	
ll		9.0	
S2		8.7	118.1
TP	0.41	11447	11.70 114.06

	500' E of	wells	
S2		+1.0	115.5
ll		0.0	
y		0.6	
b		0.8	113.7
y		1.7	
ll		2.2	
N2		2.5	112.0

11447

Pad 22

63

	550' E of	wells	
N2		5.7	108.8
ll		5.3	
y		5.1	
b		4.6	109.9
y		4.0	
ll		3.8	
S2		3.2	111.3

	600' E of	wells	
S2		4.4	110.1
ll		5.1	
y		5.4	
b		6.1	108.4
y		6.8	
ll		7.4	
N2		7.5	107.0

11447

640' E. = N Line Warrington (60')

N2		9.0	104.5
"		8.5	
"		7.9	
"		7.2	107.3
"		6.6	
"		6.1	
S2		5.3	109.0

W line of Warrington

S2		5.8	108.7
"		6.2	
"		6.4	
"		7.4	107.1
"		8.3	
"		9.0	
N2		9.4	104.5

11447

Par of

64

W 1/4 of Warrington

N2		9.6	104.9
"		9.0	
"		8.7	
"		8.3	106.2
"		7.3	
"		7.0	
S2		6.4	108.1

Center of Warrington St

S2		6.9	107.6
"		7.7	
"		8.2	
"		8.5	106.0
"		9.0	
"		9.4	
N2		10.0	104.5

POSTED

1947

	E ½ of	Warrington		
N2			10.2	104.3
11			9.4	
7			9.2	
6			8.9	10√.6
4			8.2	
11			7.7	
S2			7.0	107.√
	E 11	of	Warrington	
S2			7.9	106.6
11			8.3	
7			8.5	
6			9.2	10√.3
4			9.7	
11			10.0	
N2			10.6	103.9

1947 Page 25

	E Line	of	Warrington	
N2			10.7	103.6
11			10.0	
4			9.7	
6			9.2	10√.3
4			8.6	
11			8.3	
S2			7.6	10687
	3-4	E	of Warrington	
S2			9.0	10√.√
11			9.4	
7			9.7	
6			10.3	104.2
4			10.5	
11			10.8	
N2			11.4	103.1
TP	1.15	10328	1.34	10√.13

Bgn 14 SE Warrington

10328

	100'	E of	Warrington	
N2			3,4	99.9
1			3,0	
1			2,8	
6			2,2	101,1
4			1,9	
4			1,7	
S2			1,2	102,1
	150'	E of	Warrington	
S2			4,8	98.5
4			5-2	
4			5-5	
4			5,7	97.6
4			6.0	
4			6,1	
N2			6,5	96.8

10328

Par 0+

	200'	E of	Warrington	
N2			8,0	95.3
4			7,8	
4			7,7	
4			7,6	95.7
4			7,4	
4			7,3	
S2			7,1	96.2
	250'	E of	Warrington	
S2			8,0	95.3
4			7,9	
4			8,3	
4			8,5	94.1
4			8,6	
4			8,8	
N2			9,0	94.3

POSTED

10328

	300'	E of	warmglow	
32			10,0	93.3
11			9,8	
4			9,4	
6			9,2	94.1
4			8,8	
11			8,7	
52			8,6	94.7
	350'	E of	warmglow	
52			9,8	93.5
11			10,1	
4			10,1	
6			10,6	92.7
4			10,8	
11			11,3	
n2			12,1	91.2
TP	2,66	9513	10,75	92,52

9513

	400'	E of	warmglow	Pat
n2			6,2	88.9
11			5,2	
7			4,8	
6			4,6	90.5
7			4,2	
11			3,8	
52			3,3	91.8
	450'	E of	warmglow	
52			5,9	89.2
11			6,7	
7			7,8	
6			9,2	85.9
7			9,7	
11			10,3	
n2			12,0	84.1

POST-C

95-13

	550	ε	Warmyle	
22			10,3	84.8
11			9,9	
4			9,4	
88			8,8	86.3
7			8,4	
11			7,7	
52			7,1	88.0

	550	ε	Warmyle	
52			8,3	86.8
11			8,7	
4			9,3	
6			9,7	85.4
7			10,2	
11			11,2	
22			11,6	83.5

95-13

Pas 2

68

	601	ε	Warmyle	
22			12,8	82.3
11			12,4	
7			11,7	
6			11,4	83.7
4			11,4	
11			11,1	
52			11,3	83.8

77	274	85,32	1249	18,64	18,58 Bm Sm
	640	84 =	22 4		blanc
52			2,7	82.6	
11			2,3	82.0	
4			3,7	81.6	
1			4,0	81.3	POST
4			4,4	809	
11			4,9	806	
22			5,4	799	

8532

W'ly of Westmount

NE	6,2	79.1
E	5,5	79.8
S	4,9	80.2
SE	4,5	80.8
S	4,2	81.1
SE	3,8	81.5
SE	3,4	81.9

W'ly of Westmount

SE	4,8	80.5
E	5,1	80.2
S	5,2	80.1
SE	5,9	79.4
S	6,5	78.8
SE	7,2	78.1
NE	7,9	77.4

8532 Part

Centre of Westmount

NE	8,3	77.0
E	7,7	77.6
S	7,1	78.2
SE	6,4	78.9
S	6,2	79.1
SE	6,1	79.2
SE	5,6	79.7

E'ly of Westmount

SE	5,9	79.4
E	6,4	78.9
S	7,0	78.3
SE	7,5	77.8
S	8,2	77.1
SE	9,2	76.1
NE	9,2	76.1

POSTED

8532

	8 bl	blat worth	st		
nL			9,5	75.8	
h			9,4	75.9	
4			9,1	76.2	
L			8,9	76.4	x
4			8,4	76.9	
h			8,0	77.3	
SL			7,4	77.9	
	2 Sm	of blatworth	st		
SL			8,0	77.3	
h			8,5	76.8	
4			8,9	76.4	
L			9,3	76.0	
4			9,5	75.8	
h			9,8	75.5	
nL	110	7457	9,9	75.40	Bm NE H blat

7650

Pal 24

	50'	E of	blatworth	st	
nL			3,9	72.6	
h			3,6	72.9	
4			3,5	73.0	
L			3,3	73.2	
4			2,8	73.7	
h			2,8	73.7	
SL			2,4	74.1	
	100	E of	blatworth	st	
SL			5,5	71.0	
h			5,8	70.7	
4			6,0	70.5	
L			6,2	70.3	
4			6,5	70.0	
h			6,5	70.0	
nL			6,5	70.0	

7650

	150' E of	blabs		
N2			8.4	68.1
4			8.4	68.1
2			8.4	68.1
6			8.4	68.1
4			8.2	68.3
4			7.6	68.9
S2			7.2	69.3
	200' E of	blabs		
S2			8.3	68.2
4			8.7	67.8
2			9.0	67.5
6			9.5	67.0
2			9.0	67.5
4			8.8	67.7
NR	= Top of Bank RR		6.3	70.2
	198' E of	Blabs		
N2	= Top of Bank RR		8.5	68.0

7650

Page 2

	245' E of	blabs		
N2			7.2	69.3
	250 E of	blabs		
N2			4.7	71.8
76			7.2	69.3
4			7.4	69.1
4			7.0	69.5
6			7.4	69.1
75	Top of Bank	Brook	7.4	69.1
2			14.0	66.5
4			10.7	65.8
S2			10.1	66.4
	270' E of	blabs		
S2			11.5	65.0
4			10.7	65.8
2	Bank	RR Brook	7.7	68.8
6			7.5	69.0
2			7.2	69.3
6	RR	Brook	8.0	68.5
74			7.5	69.0
76			7.6	68.9
N2			29	72.6

POSTED

765.0

	280' E of Abutment			
SL			11.1	67.4
+1			7.8	68.7
bk			7.7	68.8
	290' E of Abutment			
SL	Top of RR Grade		8.0	68.5
	300' E of Abutment			
SL			8.0	68.5
bk			7.8	68.7
4			7.9	68.6
6			8.3	68.2
4			4.4	67.1
bk			3.0	73.5
TL			2.2	74.3
TP	7.03	825.4	0.99	755.1

825.4

	325' E of Abutment			
SL			13.7	68.6
bk			15.8	66.7
4	340' E of Abutment			
SL			14.5	66.0
	350' E of Abutment			
SL			16.7	67.8
bk			15.4	66.7
4			11.9	70.6
bk			10.4	72.1
4			8.4	74.1
bk			6.5	76.0
TL			3.0	77.5
	360 E of Abutment			
SL			17.0	67.5
bk			14.7	
TP			17.1	
	390' E of Abutment			
SL			13.7	69.3

POSTED

8254

	406'	E of	Chalsmarct	
S2			12,7	69.8
b			10,9	
y			8,8	
d			7,0	75,5
y			5,0	
bl			2,8	
N2			1,0	81.5
	450	E of	Blatsmarct	
N2			0,0	85.5
bl			0,8	
y			1,8	
d			3,4	
y			5,5	77.0
bl			7,6	
S2			9,8	90.7

8254 Pge 47

	506'	E = W Sin of Copistrano (60')	
S2		8,5	70.0
bl		7,2	
y		6,3	
d		5,4	77.1
y		4,4	
bl		3,2	
N2		2,5	90.0
	NBL of Copistrano		
N2		3,2	
bl		3,9	
y		4,8	
d		5,8	
y		6,5	
bl		7,6	
S2		8,8	

8254

W ¼ of Capistrano

S2	9.7	
1	8.5	
4	7.6	
3	6.8	
2	5.6	
1	4.5	
N2	3.9	

Center of Capistrano

N2	4.5	78.0
1	5.0	
4	5.8	
3	7.0	75.5
2	8.5	
1	9.2	
S2	10.4	71.1

8254 Plat 2

E ¼ of Capistrano

S2	11.2	71.3
1	10.4	
4	9.8	
3	8.0	73.5
2	7.2	
1	6.0	
N2	5.2	77.3

E ½ of Capistrano

N2	6.0	76.5
1	6.8	
4	7.8	
3	9.4	73.1
2	10.7	
1	11.2	
S2	11.8	70.7

POSTED

E Line of Coquitlam (68')

			12.48	70.06
			11.7	
			11.2	
			10.6	71.9
			9.2	
			8.1	
			7.0	75.5
TP	726	7722	12.48	70.06
	35.1			
	44			
			6.1	71.1
			6.0	
			6.5	
			6.6	70.6
			6.7	
			6.9	
			7.2	70.0

BM 5824 Coquitlam

50' E of Coquitlam

	12.3	64.9
	12.2	
	12.0	
	11.2	65.0
	12.3	
	12.2	
	12.0	65.2

75' E of Coquitlam

	14.3	62.9
	14.6	
	15.1	
	15.2	62.0
	15.4	
	16.2	
	16.6	60.6

7722

	100'	E.T	Capacitance	
SL			14.2	63.0
M			13.2	
7			11.2	
1			10.0	67.2
7			8.7	
M			8.2	
SL			7.9	69.3

	125'	E.T	Capacitance	
SL			2.2	7.50
M			3.4	
7			4.6	
1			5.0	72.2
7			6.8	
M			8.7	
SL			10.2	67.2

7722 Rev 2

	150'	E.T	Capacitance	
SL			9.8	67.4
M			7.4	
7			4.4	
1			2.1	75.1
7			1.0	
M			0.2	
SL			0.0	77.2

	185'	E.T.	Capacitance	
SL			+0.2	77.4
M			0.1	
7			1.4	
1			2.5	74.1
7			4.0	
M			6.3	
SL			9.3	67.9

POSTED

7.22

	250'	E of	baptisms	
SL			10.0	67.2
bl			7.8	
½			6.0	
L			4.6	72.6
½			3.4	
bl			2.4	
NL			2.2	75.0

	250'	E of	baptisms	
NL			8.2	69.0
bl			9.0	
½			9.4	
L			10.3	66.9
½			11.0	
bl			11.7	
SL			12.3	64.9

7.22 Pa 11

57

250' E of N } = ditch
280' E of S

SL			16.2	61.0
bl			15.1	
½			14.5	
L			13.6	63.6
½			13.1	
bl			11.1	
NL			10.9	66.6

	300'	E of	baptisms	
NL			6.0	71.2
bl			7.6	
½			9.5	
L			10.8	66.4
½			11.9	
bl			12.9	
SL			13.9	63.3

77.22

	350	ε γ	bapiskano	
S2			13,5	63.7
M			12,6	
4			11,9	
1			11.0	66.2
4			9,7	
M			8,2	
N2			7,0	70.7
	450	ε γ	bapiskano	
N2			4,5	72.7
M			5,4	
4			6,5	
1			7,8	69.4
4			8,3	
M			9,7	
S2			11,4	65.8
TP	6,50	72,88	10,84	66.38

72.88

Pa M

	450	ε γ	bapiskano	
S2			7,7	65.2
M			6,3	
4			4,7	
1			3,7	69.2
4			2,8	
M			1,6	
N2			0,7	72.2
	500	ε γ	bapiskano	
N2			5,2	67.7
M			6,0	
4			6,7	
1			7,6	65.3
4			8,5	
M			9,2	
S2			9,3	63.6

7288

	550	E y	Copestham	
SL		15,2	57.7	
bL		14,0		
½		13,3		
L		12,3	60.6	
½		11,2		
M		10,3		
NL		9,5	63.4	
	575	E y	Copestham	
NL		7,9	65.0	
bL		8,7		
½		9,6		
L		10,7	62.2	
½		11,3		
M		12,3		
SL		13,8	59.1	

7288 Pw 1

	600	E y	Copestham	
SL		13,9	59.0	
bL		12,6		
½		11,2		
L		9,7	63.2	
½		8,5		
M		7,9		
NL		7,6	65.3	
	650	E y	Copestham	
NL		4,7	68.2	
bL		6,8		
½		7,8		
L		8,6	64.3	
½		9,5		
M		10,8		
SL		13,0	59.9	

POSTED

7.58

	700	E y	bofastam	
SL			11,6	61.3
H			8,5	
?			5,2	
b			3,4	69.5
4			1,5	
M			0,4	
NL			0,0	7v9
TP	1,80	7168	3,00	6988
	750	E y	bofastam	
NL			2,7	70.7
M			4,5	
?			6,3	
b			8,0	649
?			9,3	
H			10,9	
SL			12,4	60.5

Continuum in Buch 426

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TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100.00	0.44	100.00	0.87	99.99	1.31	89
1	99.98	1.75	99.98	2.18	99.97	2.62	99.95	3.05	88
2	99.94	3.49	99.92	3.93	99.91	4.36	99.88	4.80	87
3	99.86	5.23	99.84	5.67	99.81	6.10	99.79	6.54	86
4	99.76	6.98	99.73	7.41	99.69	7.85	99.66	8.28	85
5	99.62	8.72	99.58	9.15	99.54	9.58	99.50	10.02	84
6	99.45	10.45	99.41	10.89	99.36	11.32	99.31	11.75	83
7	99.25	12.19	99.20	12.62	99.14	13.05	99.09	13.49	82
8	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	15.64	98.70	16.07	98.63	16.50	98.56	16.93	80
10	98.48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98.16	19.08	98.08	19.51	97.99	19.94	97.90	20.36	78
12	97.81	20.79	97.72	21.22	97.63	21.64	97.53	22.07	77
13	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	24.19	96.92	24.62	96.81	25.04	96.70	25.46	75
15	96.59	25.88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.82	73
17	95.63	29.24	95.50	29.65	95.37	30.07	95.24	30.49	72
18	95.11	30.90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35.43	69
21	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38.67	67
23	92.05	39.07	91.88	39.47	91.71	39.87	91.53	40.27	66
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	43.84	89.69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	46.95	88.09	47.33	87.88	47.72	87.67	48.10	61
29	87.46	48.48	87.25	48.86	87.04	49.24	86.82	49.62	60
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	52.99	84.57	53.36	84.34	53.73	84.10	54.10	57
33	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	52
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	45
45	70.71	70.71							

Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees
	DEGREES		¾ DEGREE.		½ DEGREE.		¼ DEGREE.		