

441

Return to City Engineers Office
City Hall, San Diego, Cal.

TRANSIT

398

F.B. 441

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City Hall, San Diego, Cal.

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Table showing the difference of latitude and departure in running 80 chains at any course from 1 to 60 minutes.

MICROFILMED

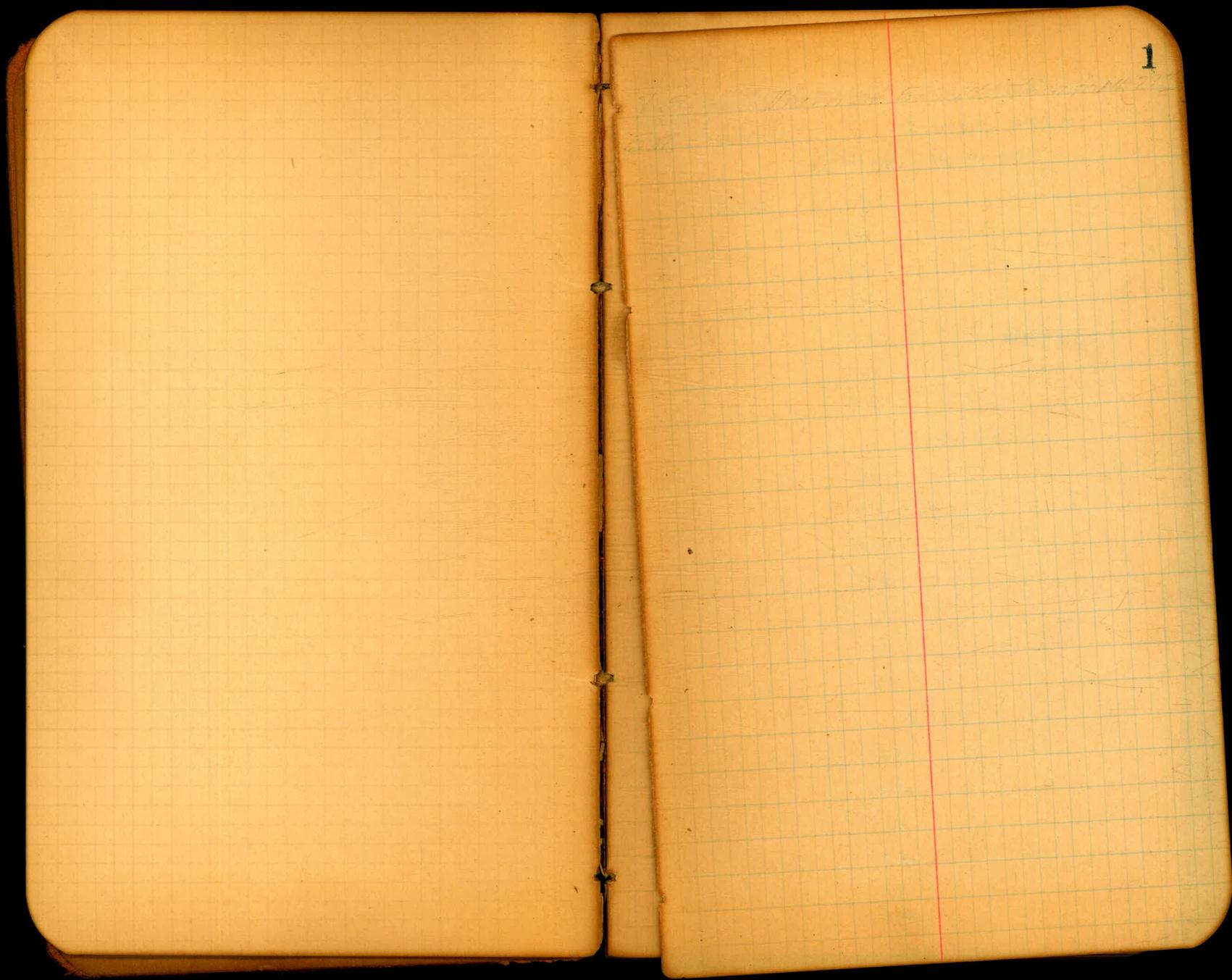
DEC 10 1964

MINUTES.	LKS.	MINUTES.	LKS.	MINUTES.	LKS.
1.....	2 $\frac{1}{8}$	21.....	49	41.....	95 $\frac{3}{8}$
2.....	4 $\frac{1}{4}$	22.....	51 $\frac{1}{2}$	42.....	98
3.....	7	23.....	53 $\frac{3}{8}$	43.....	100 $\frac{1}{2}$
4.....	9 $\frac{1}{2}$	24.....	56	44.....	102 $\frac{3}{8}$
5.....	11 $\frac{3}{8}$	25.....	58 $\frac{1}{2}$	45.....	105
6.....	14	26.....	60 $\frac{3}{8}$	46.....	107 $\frac{1}{2}$
7.....	16 $\frac{1}{2}$	27.....	63	47.....	109 $\frac{3}{8}$
8.....	18 $\frac{3}{8}$	28.....	65 $\frac{1}{2}$	48.....	112
9.....	21	29.....	67 $\frac{3}{8}$	49.....	114 $\frac{1}{2}$
10.....	23 $\frac{1}{2}$	30.....	70	50.....	116 $\frac{3}{8}$
11.....	25 $\frac{3}{8}$	31.....	72 $\frac{1}{2}$	51.....	119
12.....	28	32.....	74 $\frac{3}{8}$	52.....	121 $\frac{1}{2}$
13.....	30 $\frac{1}{2}$	33.....	77	53.....	123 $\frac{3}{8}$
14.....	32 $\frac{3}{8}$	34.....	79 $\frac{1}{2}$	54.....	126
15.....	35	35.....	81 $\frac{3}{8}$	55.....	128 $\frac{1}{2}$
16.....	37 $\frac{1}{2}$	36.....	84	56.....	130 $\frac{3}{8}$
17.....	39 $\frac{3}{8}$	37.....	86 $\frac{1}{2}$	57.....	133
18.....	42	38.....	88 $\frac{3}{8}$	58.....	135 $\frac{1}{2}$
19.....	44 $\frac{1}{2}$	39.....	91	59.....	137 $\frac{3}{8}$
20.....	46 $\frac{3}{8}$	40.....	93 $\frac{1}{2}$	60.....	140

TABLE FOR RUNNING ON SLOPES.

In the following table the first column shows the angle, the second the number of links to be added to a chain on the slopes, to make one chain, horizontal measurement.

ANGLE	COR. IN LINKS						
°		°		°		°	
4	0.24	11	1.88	18	5.14	25	10.54
5	0.38	12	2.24	19	5.76	26	11.26
6	0.55	13	2.63	20	6.42	27	12.24
7	0.76	14	3.06	21	7.11	28	13.37
8	0.98	15	3.53	22	7.85	29	14.34
9	1.24	16	4.02	23	8.64	30	15.47
10	1.55	17	4.56	24	9.47	35	22.07



X Section Thorn St. From W.L. 30th to W.L. 29th =
 B.M. 4.240 329.675 320.435
 60' wide
 Non. SE
 Cor. 30th
 x Thorn.

0+00 = W.L. 30th St.

N.L.	4.1	320.6
✓	4.2	
14	4.4	
✓	4.5	320.2
14	4.4	
✓	4.5	
5 L	4.6	320.1

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0+50

5 L	4.6	320.1
✓	4.7	
14	4.9	
✓	4.9	319.8
14	4.8	
✓	4.9	
N.L.	5.0	319.7

POSTED

POSTED

1+00

N.L.	4.6	320.1
✓	4.5	
14	4.4	
✓	4.2	320.5
14	3.9	
✓	4.0	
5 L	4.1	320.6

X Section Thorn St. (Cont)

	17.50		
	324.675		
5L		4.8	319.9
U		4.5	
14		4.5	
L		4.4	320.3
14		4.4	
U		4.2	
NL		3.8	320.9
	2700		
NL		3.8	320.9
U		4.0	
14		4.3	
L		4.7	320.0
14		5.0	
U		5.2	
5L		5.4	319.3
	2750		
5L		5.9	318.8
U		5.6	
14		5.5	
L		5.3	319.4
14		5.0	
U		4.6	
NL		4.4	320.3

N. Section Thorn St (Cont)

^{324.17}
 2+70 = E.L. Dale St. 60' wide

N.L.	4.1	320.1
U	4.4	
14	4.7	
E	4.9	319.3
14	5.3	
U	5.5	
5.L.	5.8	318.4

E.C.L. Dale St.

5.L.	5.9	318.3
U	5.6	
14	5.3	
E	5.1	319.1
14	4.6	
U	4.5	
N.L.	4.2	320.0

E 1/4 Dale St.

N.L.	4.5	319.7
U	4.6	
14	4.9	
E	5.0	319.2
14	5.4	
U	5.7	
5.L.	5.8	318.4

of Daley Thorn.
 Note Intersection taken from continuation of Dale St H&E=324.17

7 Section Thorn St. (Cont.)

↳ Dale St
324.17

S.L.	59	318.3
U	57	
14	53	
↳	51	319.1
14	50	
U	48	
N.L.	45	319.7

N 14 Dale St.

N.L.	47	319.5
U	50	
14	53	
↳	54	318.8
14	58	
U	59	
S.L.	62	318.0

M.C.L. Dale St.

S.L.	65	317.7
U	61	
14	59	
↳	57	318.5
14	54	
U	52	
N.L.	49	319.3

X Section Thorn St (Cont.)

3+30 = N.L. Dale St
324.17

N.L.	51	319.1
0	52	
14	56	
2	59	318.3
14	62	
0	64	
5L	65	317.7

3+40
324.675

5L	74	317.3
0	72	
14	69	
2	67	318.0
14	63	
0	61	

3+50

N.L.	59	318.8
N.L.	62	318.5
0	64	
14	66	
2	69	317.8
14	70	
0	77	
5L	83	316.4

Section Thorn St (Cont)

		3175		
		324.675		
SL			13.3	311.4
U			9.9	
14			8.6	
Q			7.8	316.9
14			7.3	
U			7.0	
NL			6.8	317.9
		3190		
NL			7.8	316.9
U			8.5	
14			9.4	
Q			10.4	314.3
14			12.6	
U			14.5	
SL			17.3	307.4
TP	2.65	316.95	10.38	314.30
		A+00		
SL			10.9	306.0
U			9.7	
14			7.7	
Q			6.4	310.5
14			5.2	
U			4.2	
NL			2.8	314.1

X Section Thorn St. (Cont)

		4+2.5		
		316.95		
NL			8.3	308.6
c			8.3	
14			7.6	
2			7.2	309.7
14			6.6	
c			5.1	
SL			3.8	313.1
T.P.	12.18	326.43	2.65	314.30
		4+5.0		
SL			6.1	320.4
c			6.0	
14			6.3	
2			6.6	319.9
14			7.0	
c			7.2	
NL			7.5	319.0
		4+7.5		
NL			5.5	321.0
c			5.1	
14			4.6	
2			4.6	321.9
14			4.5	
c			4.7	
SL			4.7	321.8

Section Thorn St (Cont)

5100
326.78

5L	5.2	321.3
c	4.9	
14	4.7	
L	4.4	322.1
14	4.4	
c	4.6	
NL	4.9	321.6

5150

NL	4.4	322.1
c	4.4	
14	4.2	
L	4.2	322.3
14	4.2	
c	4.2	
5L	4.2	322.3

519811 = E.L. 29th St. 60' wide

5L	2.7	323.8
c	2.8	
14	2.9	
L	3.0	323.5
14	3.2	
c	3.5	
NL	3.8	322.7

N Section Thorn St (Cont)

ECL 29th St

326.78

N.L.	3.2	323.8
0	3.3	
14	3.1	
2	2.8	323.7
14	2.6	
0	2.5	
S.L.	2.5	324.0

E 1/4 29th St

S.L.	2.4	324.1
0	2.2	
14	2.4	
2	2.3	324.2
14	2.3	
0	2.6	
N.L.	2.8	323.7

2 29th St

N.L.	2.5	324.0
0	2.2	
14	1.7	
2	1.5	325.0
14	2.1	
0	2.3	
S.L.	2.2	324.3
T.P.	6.06	328.78
		376
		322.72

Section Thorn St (cont)

W 1/2 29th St.

328.78

S.L.	4.4	324.4
o	4.4	
14	3.8	
2	3.5	325.3
14	3.9	
o	4.3	
N.L.	4.4	324.4

W.C.L 29th St.

N.L.	4.0	324.8
o	3.9	
14	3.4	
2	3.2	325.6
14	3.5	
o	3.8	
S.L.	4.1	324.9

W.L 29th St

S.L.	3.6	326.2
o	3.6	
14	3.5	
2	3.1	325.7
14	3.4	
o	3.8	
N.L.	3.9	324.9

60' wide.
 Section 29th St From N^L Thorn to S^L Upas St.

BNT	42.40	324.675		320.435
	2.65	316.95	10.38	314.30
	12.18	326.48	2.65	314.30
	6.06	328.78	3.76	322.72

0+00 = N^L Thorn St.

E.L.			6.1	322.7
c			5.5	
1/4			5.1	
1/2			4.8	324.0
3/4			4.4	
c			4.0	
N ^L			3.9	324.9

0+50

N ^L			4.0	324.8
c			4.2	
1/4			4.6	
1/2			5.1	323.7
3/4			5.5	
c			5.8	
E.L.			6.0	322.8

Section of 29th St (Cont)

	1400 328.78		
EL		64	322.4
o		58	
1/4		53	
EL		49	323.9
1/4		47	
o		46	
N.L.		42	324.6
	1750		
N.L.		39	324.9
o		46	
1/4		52	
EL		60	322.8
1/4		64	
o		67	
EL		71	321.7
	2100		
EL		75	321.3
o		73	
1/4		69	
EL		65	322.3
1/4		62	
o		58	
N.L.		55	323.3

X Section 29th St (Cont.)

		2+50 328.78		
W.L.			57	323.1
U			62	
1/4			66	
2			69	321.9
1/4			72	
U			75	
E.L.			79	320.9
T.P.	10.52	332.32	6.98	321.80
		3+00		
E.L.			98	322.5
U			98	
1/4			94	
2			88	323.5
1/4			82	
U			79	
W.L.			77	324.6
		3+50		
W.L.			64	325.9
U			68	
1/4			73	
2			76	324.7
1/4			79	
U			88	
E.L.			92	323.1

Section 29th St. (Cont)

	4+00 332.32		
EL.		8.0	324.3
o		7.9	
14		7.3	
2		6.8	325.5
14		5.9	
o		5.4	
N.L.		5.0	327.3

	4+50		
N.L.		3.6	328.7
o		4.5	
14		5.3	
2		6.0	326.3
14		6.5	
o		6.7	
EL.		6.8	325.5

	5+00		
EL.		6.0	326.3
o		6.0	
14		5.7	
2		5.4	326.9
14		5.0	
o		4.4	
N.L.		4.2	328.1

X Section 29th St (Cont)

5+50
332.32

W.L.	29	329.4
0	3.7	
1/4	4.4	
1/2	4.7	327.6
3/4	4.8	
0	4.7	
EL	5.3	327.0

5+99.41 = SL Upas St.

EL	4.2	328.1
0	4.6	
1/4	4.6	
1/2	4.1	328.2
3/4	3.8	
0	3.7	
W.L.	3.5	328.8

60' wide
 V. Section Dale St. From N.L. Thorn to S.L. Ubas
 B.M. 372 324.155 320.435
 Man. SE
 Cor. 20th
 & Thorn

17

0+00 = N.L. Thorn St.

E.L.		4.1	320.1
U		4.2	
1/4		4.5	
2		4.5	319.7
1/4		4.7	
U		4.9	
N.L.		5.1	319.1
	0+50		
N.L.		4.2	320.0
U		4.0	
1/4		3.9	
2		3.7	320.5
1/4		3.7	
U		3.6	
E.L.		3.6	320.6
	1+00		
E.L.		3.2	321.0
U		3.1	
1/4		3.2	
2		3.2	321.0
1/4		3.2	
U		3.4	
N.L.		3.4	320.8

POSTED

V. Section Date St (Cont)

		1+50		
		327.155		
NL			2.7	321.5
U			2.6	
14			2.6	
Q			2.5	321.7
14			2.3	
U			2.2	
EL			2.2	321.0
T.P.	7.20	329.515	1.84	322.315
		2700		
EL			7.5	322.0
U			7.4	
14			7.6	
Q			7.6	321.9
14			7.5	
U			7.5	
NL			7.4	322.1
		2750		
NL			6.9	322.6
U			7.3	
14			7.1	
Q			7.2	322.3
14			7.1	
U			7.1	
EL			6.9	322.6

X Section Dale St. (Cont)

	3400		
	329.515		
EL		6.8	322.7
o		6.7	
14		6.7	
2		6.6	322.9
14		6.6	
o		6.8	
N.L.		6.8	322.7
	3450		
N.L.		6.3	323.2
o		6.5	
14		6.3	
2		6.3	323.2
14		6.3	
o		6.3	
EL		6.4	323.1
	4100		
EL		5.8	323.4
o		6.2	
14		6.2	
2		6.3	323.2
14		6.3	
o		6.5	
N.L.		6.9	322.6

Section Date 54 (Cont.)

20

4+50
329.515

M.L.	60	323.5
0	58	
1/4	60	
1/2	57	323.8
1/4	58	
0	59	
E.L.	57	323.8

5+00

E.L.	52	324.3
0	54	
1/4	54	
1/2	53	324.2
1/4	53	
0	52	
M.L.	54	324.1

5+50

M.L.	50	324.5
0	4.8	
1/4	4.8	
1/2	5.1	324.4
1/4	4.9	
0	5.1	
E.L.	5.1	324.4

Section Dale St (Cont)

$\frac{5498.20}{329.515} = 54. \text{ Upas St.}$

E.L.	A.1	225.4
0	4.6	
14	4.6	
2	4.6	324.9
14	4.6	
0	4.6	
11	4.7	324.8

0081-3

4 Hatch
 25 Moore
 19 Thomas
 Xsec, at Upper Pt Loma Res. for
 fill for Water-Tower.

B.M. Mar. 11.75 386.53 374.78

Sec. A

0 = North Liza Reservation	4.4	382.1
10' N.	4.7	381.8
20	5.1	381.4
30	5.4	381.1
40	5.7	380.8
50	6.2	380.3
60	6.4	380.1
70	6.9	380.1
80	6.7	379.8
90	6.9	379.6
100	7.4	379.1

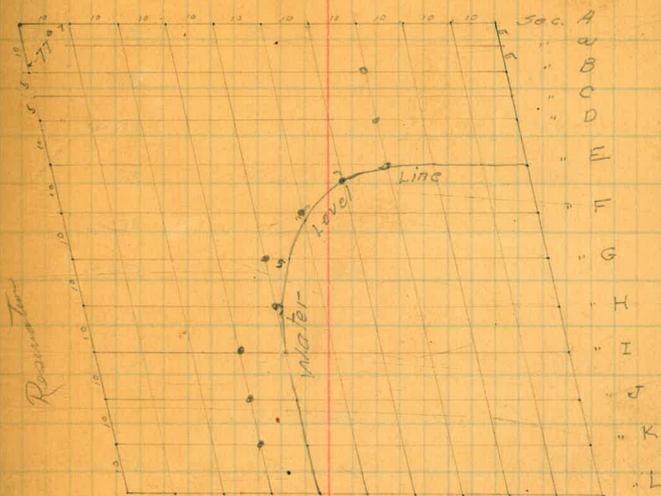
Sec. a

100 N	6.4	380.1
90	6.0	380.5
80	5.7	380.8
70	5.5	381.0
60	5.7	380.8
50	5.8	380.7
40	5.7	380.8

Sec. B.

0	4.1	382.4
10 N.	4.6	381.9

NE. Cor Pt Loma Ave and Catalina



POSTED

	386.53		
20		2.9	381.6
30		5.9	381.1
40		8.6	380.9
50		5.1	381.4
60		5.9	381.1
70		4.1	382.4
80		3.9	382.6
90		4.0	382.5
100		4.2	382.3

Sec C Top of Bank

100 N.		2.2	384.3
90		2.3	384.2
80		2.4	384.1
70		2.2	384.3
60		2.4	384.1
50		3.5	383.0
40		3.2	381.3
30		5.4	381.1
20		5.0	381.5
10		4.6	381.9
0		4.1	382.4

Sec D

0		3.9	382.6
10		4.6	381.9

	386.53		
20		4.0	371.5
30		3.0	381.5
40		3.7	382.8
50		2.0	384.5
60		2.7	383.8
70		3.9	382.6
80		4.0	384.5
90		4.3	384.4
100		4.3	384.4

Sec E

100 N. Water Level		5.4	378.1
90		8.4	378.1
80		8.4	378.1
70		8.4	378.1
60		6.4	380.1
50		4.2	382.3
40		1.8	384.7
27	Top of Bank	1.7	384.8
30		3.7	384.8
20		4.7	381.8
10		4.5	382.0
0		4.0	384.5

386.53			
Sec F			
0			
10	4.0	389.5	
20	4.6	381.9	
25	4.2	389.3	
28	3.3	383.2	
30	Top of Bank	1.5	385.0
40	3.9	382.6	
50	7.2	379.3	
53	Water Level	8.9	378.1
Sec G			
45	Water level	8.9	378.1
40	6.1	380.4	
30	2.0	384.5	
27	Top of Bank	1.5	385.0
20	3.5	383.0	
10	4.5	382.0	
0	4.1	382.4	
Sec H			
0	4.1	382.4	
10	4.5	382.0	
20	3.2	383.3	
25	Top of Bank	1.5	385.0
30	3.5	383.0	
40	7.5	379.0	
41	Water Level	8.9	378.1

386.53			
Sec I			
40	Water Level	8.9	378.1
30	3.4	383.1	
24	Top of Bank	1.9	384.6
20	3.0	383.5	
10	4.6	381.9	
0	4.1	382.4	
Sec J			
0	4.2	382.3	
10	4.6	381.9	
20	2.9	383.6	
24	Top of Bank	1.7	384.8
30	3.8	382.7	
40	Water Level	8.9	378.1
Sec K			
40	Water Level	8.9	378.1
30	3.6	382.9	
23	1.6	384.9	
20	2.6	383.9	
10	4.6	381.9	
0	4.3	382.2	
Sec L			
0	4.3	382.2	
10	4.6	381.9	

386.53

20		2.1	383.4
24	Top of Bank	1.7	384.8
30		4.0	382.8
40	Water Level	8.9	378.1

± Hatch
25 Moore
10 Thomas

Xsections Catalina St.

40' St.
10' Curbs

25

R21. 196 376.74 374.73

El. Pt. Room.

N. 1.7 374.8

cl 1.7

1/2 1.5

0 1.3 375.4

1/6 1.3

cl 1.2

50 0.9 375.8

50 E

5 1.4 375.3

cl 2.3

1/6 2.5

0 2.5 374.2

1/6 2.5

cl 2.7

N 2.9 373.8

100 E

N 4.1 372.6

cl 3.8

1/6 3.7

0 3.5 373.2

1/6 3.5

cl 2.9

3 2.0 374.7

376.77

150'E

s	3.3	373.4
cb	3.7	
1/6	4.0	
c	4.2	372.5
1/4	4.3	
cb	4.5	
H	4.5	372.2

200'E

N	5.1	371.6
cb	4.7	
1/6	4.7	
c	4.6	372.1
1/4	4.5	
cb	4.3	
s	3.9	372.5

250'E

s	4.5	372.2
cb	4.8	
1/6	4.9	
c	5.1	371.6
1/4	5.1	
cb	5.2	
N	5.4	371.3

26

376.74

300'E

N	6.0	370.7
cb	5.8	
1/6	5.7	
c	5.5	371.2
1/4	5.4	
cb	5.2	
s	4.9	371.8

350'E

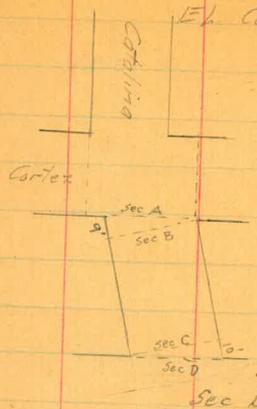
s	5.8	370.9
cb	6.0	
1/6	6.0	
c	6.5	370.2
1/4	6.6	
cb	7.0	
N	7.2	369.5

200'E = Mt. Cortez

N	9.0	367.7
cb	8.6	
1/6	8.2	
c	8.1	368.6
1/4	7.9	
cb	7.8	
s	7.5	369.2

376.74

	EL. Cortex	sec A	
N		12.1	364.6
cb		11.6	
1/2		11.3	
c		11.1	365.6
1/2		10.9	
cb		10.6	
S		10.1	366.6
	Sec B		
		10.7	366.0
cb		10.4	
1/2		10.9	
c		11.1	365.6
1/2		11.4	
cb		11.7	
N	0.58	365.15	12.1 7
			364.60 Hub
			50' E of sec B.
N		2.9	361.3
cb		2.6	
1/2		2.0	
c		2.8	362.4
1/2		2.8	
cb		2.3	
S		2.3	362.9



365.18

	100' E	
S		5.3
cb		6.3
1/2		5.9
c		6.0
1/2		6.5
cb		6.8
N		7.0
	150' E	
N		9.9
cb		9.5
1/2		9.0
c		8.5
1/2		8.8
cb		9.0
S		8.1
	200'	
S		10.2
cb		11.0
1/2		10.8
c		10.8
1/2		11.3
cb		11.6
N		11.9

359.9
359.2
358.2
355.3
356.7
357.1
355.0
354.4
353.3

		365.18		
TP	4.50	357.43	13.25	357.93
		200 E		
N			4.8	352.6
cb			4.9	
1/2			3.8	
c			3.5	353.9
1/4			3.7	
cb			3.5	
s			3.1	354.3
		300 E		
s			4.0	353.4
cb			4.2	
1/4			4.7	
c			4.6	352.8
1/4			4.8	
cb			5.7	
N			6.8	351.6
		350 E		
N			6.0	351.4
cb			6.0	
1/4			5.3	
c			5.0	352.4
1/4			6.0	
cb			4.8	
s			4.3	353.1

		357.43		
		400 E		
s			3.7	353.7
cb			4.0	
1/2			4.3	
c			4.2	353.2
1/4			4.5	
cb			5.3	
N			5.2	352.4
		425 E = Sec C		
N			4.3	353.1
cb			4.7	
1/4			3.8	
c			3.8	353.6
1/4			3.8	
cb			3.4	
s			3.2	354.2
		Sec D		
s			3.2	354.2
cb			3.3	
1/4			3.6	
c			3.5	353.9
1/4			3.9	
cb			4.3	
N			4.1	353.3

4 Hatch
25 Wood
10 Thomas

Rev. Cortez St 50' Street
10' Curbo.

TP.	1247	377.07	364.60
		Sec A	POSTED
W		2.3	374.8
cb		2.8	
1/2		2.9	
c		3.2	373.9
1/2		3.4	
cb		4.1	
E		4.3	372.8
		12.7 Sec B = 104.5 S. of Catalina	
E		4.3	372.8
cb		4.1	
1/2		3.6	
c		3.7	373.4
1/2		3.5	
cb		3.2	
W.		2.8	374.3
		50's of Catalina	
W		5.4	371.7
cb		5.8	
1/2		6.1	
c		6.4	370.9
1/2		6.5	
cb		7.0	
E		7.2	369.9



377.07
S. L. Catalina sec C

E	9.9	367.2
cb	9.6	
1/2	9.0	
c	8.9	368.2
1/2	8.4	
cb	8.1	
W	7.8	369.3
	Sec D	
W	7.8	369.3
cb	8.3	
1/2	8.7	
c	9.2	367.9
1/2	9.6	
cb	10.0	
E	10.4	366.7
	5 cb.	
E	10.9	366.2
cb	10.3	
1/2	9.8	
c	9.5	367.6
1/2	9.0	
cb	8.6	
W	8.2	368.9

377.07
5/4

W	8.3	368.8
cb	8.8	
1/2	9.3	
c	10.0	367.1
1/2	10.1	
cb	10.5	
E	11.2	365.9

Cl.

E	11.4	365.7
cb	10.7	
1/2	10.3	
c	9.9	367.2
1/2	9.4	
cb	8.9	
W	8.4	368.7

N 1/4

W	8.5	368.6
cb	9.2	
1/2	9.7	
c	10.3	367.8
1/2	10.6	
cb	11.0	
E	11.7	365.4

377.07

N cb.

E	11.9	365.2
cb	11.3	
1/2	10.9	
c	11.5	366.6
1/2	10.0	
cb	9.5	
W	8.9	368.2

N.L. sec E

W	9.3	367.8
cb	10.0	
1/2	10.4	
c	10.9	366.2
1/2	11.4	
cb	11.8	
E	12.5	364.6

sec F

E	12.5	364.6
cb	11.8	
1/2	11.5	
c	11.2	365.9
1/2	10.9	
cb	10.5	
W	10.0	367.1

HS

377.07
50' N of Catalina

W			12.0	3651
cb	0.60	365.07	12.60	364.97
1/4			1.0	
c			1.5	3636
1/4			1.8	
cb			2.5	
E			3.0	3641

100' N

E			5.5	3596
cb			4.9	
1/4			4.4	
c			4.1	3610
1/4			3.6	
cb			3.2	
W			2.5	3626

150' N

w			4.9	3602
cb			5.5	
1/4			6.1	
c			6.6	3585
1/4			7.1	
cb			7.5	
E			7.9	3572

365.07
500' N

E			10.1	3553
cb			9.7	
1/4			9.1	
c			9.0	3561
1/4			8.4	
cb			7.9	
W			7.2	3579

750' N

W			9.6	3565
cb			10.2	
1/4			10.6	
c			11.1	3540
1/4			11.5	
cb			12.0	
E			12.5	3546
TR	312	356.37	11.0	353.27

277.5 - 3L Montezuma

E			5.2	3512
cb			4.7	
1/4			4.0	
c			3.9	3525
1/4			3.4	
cb			2.9	
W			2.3	3541

356.39

5 cb.

w	2.6	353.8
cb	3.2	
1/4	3.7	
c	4.1	352.3
1/2	4.2	
cb	4.9	
E	5.4	361.6

5 1/4

E	5.5	350.9
cb	5.0	
1/2	4.2	
c	4.3	352.1
1/4	3.8	
cb	3.5	
w	2.6	363.8

cr.

w	2.7	363.7
cb	3.2	
1/4	4.0	
c	4.5	351.9
1/2	4.6	
cb	5.3	
E	5.7	350.7

31

356.39

1 1/4

E	5.8	350.6
cb	5.3	
1/4	4.8	
c	4.5	351.9
1/2	4.1	
cb	3.5	
w	2.8	353.6

nd

w	2.9	353.5
cb	3.6	
1/2	4.1	
c	4.8	351.6
1/4	4.9	
cb	5.5	
E	6.2	350.2

Nk. Montezuma

E	6.5	349.9
cb	5.8	
1/2	5.2	
c	4.8	351.6
1/4	4.2	
cb	3.7	
w	3.1	353.3

356.39

50' N

W	4.4	3520
cb	5.1	
1/2	5.7	
c	6.3	3501
1/4	6.6	
cb	7.3	
E	7.8	348.6

100' N

E	9.2	347.2
cb	8.3	
1/4	7.9	
c	7.4	349.0
1/2	6.9	
cb	6.2	
W	5.4	351.0

150' N

W	6.9	349.5
cb	7.7	
1/4	8.2	
c	8.9	347.5
1/2	9.4	
cb	9.9	
E	10.3	346.1

356.39

200' N

E	11.9	344.5
cb	11.4	
1/2	10.7	
c	10.2	346.2
1/4	9.6	
cb	9.1	
W	8.4	348.0

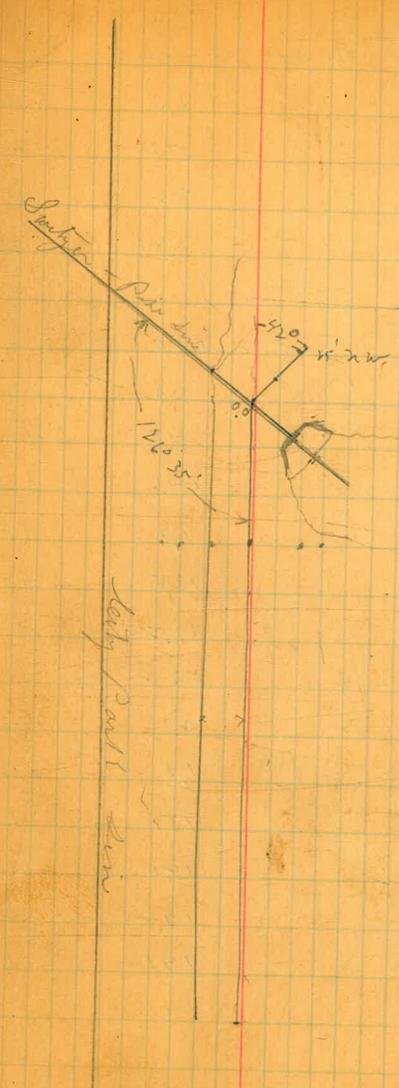
250' N

W	10.1	346.3
cb	10.8	
1/4	11.4	
c	12.0	344.4
1/2	12.2	
cb	12.5	
E	13.0	349.4

300' N = 56.4 sec

E	14.7	341.7
cb	14.3	
1/4	13.6	
c	13.3	343.1
1/2	12.7	
cb	12.3	
W	11.8	344.6

	170	9634		94.84	8m SW D.R. 20
	0.0	8457	1253	84.01	
	0.47	7225	1273	71.78	
	5.45	6944	828	63.97	
	7.22	7583	081	88.61	
	15.34		34.35 15.34 19.01		
0.0			1.70	74.83	3m Habot 0.0
5' S on Pike line			1.8	74.0	
35' S " " "			11.0	64.8	7th-6 Pike
3' m " " "			1.8	74.0	
23' N " " " Top of Wing Wall			9.4	66.4	
23' N " " " Bottom of Pike			15.7	60.1	
33' N " " " " South			15.1	60.7	
10' N W of			0.0	75.8	
6			1.65	74.0	
8' S of 6			1.9	73.9	
23' S " "			7.1	68.7	
50' S " "			14.7	61.1	
2' m " "			1.7	74.1	
30' m " " End of Wing Wall			14.2	61.6	
40' m " "			14.5	71.3	



75.83

	25'	n w	f	i	
6				1.3	74.5
17'		n of 6		5.1	70.7
45'		" " "		8.2	67.6
19'		S " "		0.0	75.8

	25'	E. of	Sta. 0	
6			2.0	73.8
20' w = 7ae			14.5	61.3
30' w in bank			14.6	61.2
10' S			1.9	73.9
30' S = 7ae			13.5	62.3
40' S			11.2	64.6

	50'	E of	Sta. 10	
6			2.0	73.8
10' S			1.9	73.9
30' S = 7ae			13.9	61.9
40' S			15.0	60.8
23' w = 7ae			13.2	62.6
33' w in bank			14.1	61.7

34

	75'	E of	Sta 00	
6			1.8	74.0
10' S			1.9	73.9
31' S = 700			13.7	62.1
41' S			12.2	63.6
13' N			8.5	67.3
21' N = 700			11.1	64.7
31' N			11.9	63.9
	390	7803	170	74.3

	100'	E of	Sta 00	
6			4.0	74.0
20' N = 700			13.5	64.5
30' N			14.5	63.5
10' S			3.8	74.2
27' S = 700			12.8	65.2
37' S			12.8	65.2

	125'	E of	Sta 00	
6			3.9	74.1
10' S			3.8	74.2
27' S = 700			12.5	65.5
37' S			13.00	65.0
17' N = 700			13.1	64.9
27' N			13.0	65.0

87.03
78.03

	150'	E of	Sta 0.0		
6			3.9	74.1	
10' S			4.0	83.0	74.0
26' S = 7m			12.0	75.0	66.0
36' S			12.3	74.7	65.7
15' N = 7m			11.6	75.4	66.4
25' N			11.8	75.2	66.2
	175'	E of	Sta 0.0		
6			3.9	83.1	74.1
12' N = 7m			10.3	76.7	67.7
22' N			10.6	76.4	67.4
11' S			3.9	83.1	74.1
20' S = 7m			11.4	75.0	66.6
33' S			11.8	75.2	66.2
	200'	E of	Sta 0.0		
6			3.7	83.3	74.3
11' S			4.0	83.0	74.0
23' S = 7m			11.1	75.9	66.9
33' S			11.3	75.7	66.7
14' N = 7m			11.0	76.0	67.0
24' N			11.3	75.7	66.7

36

8703
78.03

225'		Σ f	Sta 00		
6			3,9	83.1	74.1
14' n = 700			10,6	76.4	67.4
24' n			11,0	76.0	67.0
10' S			3,8	83.0	74.2
22' S = 700			10,8	76.2	67.2
30' S			10,5	76.5	67.5
250'		Σ f	Sta 00		
1			3,8	83.2	74.2
10' S			4,0	83.0	74.0
21' S = 700			10,6	76.4	67.4
31' S			10,2	76.8	67.8
13' n = 700			10,3	76.7	67.7
23' n			10,4	76.6	67.6
275'		Σ f	Sta 00		
6			3,8.1	83.2	74.2
14' n = 700			10,1	76.9	67.9
24' n			10,1	76.9	67.9
10' S			3,7	83.1	74.1
22' S = 700			9,9	77.1	67.1
22' S			10,2	76.8	67.8
TP	4,95	79,38	360	7443	

79.38

300	E of Sta 60		
6		5.3	74.1
11' n = toe		11.0	68.4
21' n		11.0	68.2
10' S		5.4	74.0
20' S = toe		10.3	69.1
30' S		10.5	68.9

325'	E of Sta 60		
6		5.1	74.3
9' S		5.2	74.2
20' S = toe		10.1	69.3
30' S		10.5	68.9
11' n = toe		10.5	68.9
21' n		10.6	68.8

350'	E of Sta 60		
6		5.4	74.0
10' n = toe		9.8	69.6
20' n		9.9	69.5
10' S = toe		5.2	74.2
20' S = toe		10.3	69.1
30' S		10.1	69.3

38

79.38

86

	375'	E 7	St 0.0	
b			5.4	74.0
10' S			5.2	74.2
18' S = 70a			9.3	70.1
28' S			9.4	70.0
8' n = 70a			9.9	69.5
18' n			9.8	69.6
	400	E 7	St 0.0	
b			5.1	74.3
6' n = 70a			8.7	70.7
16' n			9.1	70.3
10' S			5.3	74.1
17' S = 70a			8.3	71.1
27' S			8.0	71.4
	425	E 7	St 0.0	
b			5.4	74.0
10' S			5.3	74.1
13' S = 70a			6.3	73.1
23' S			6.5	72.9
2' n = 70a			6.0	73.4
12' n			6.3	73.1

39

4.36' E

6

5.0

Hubs

74.4

10' S

5.1

74.3

12' S

5.7

73.7

22' S

5.8

73.6

2' N

5.4

74.0

7P

5.1

74.3

4.97

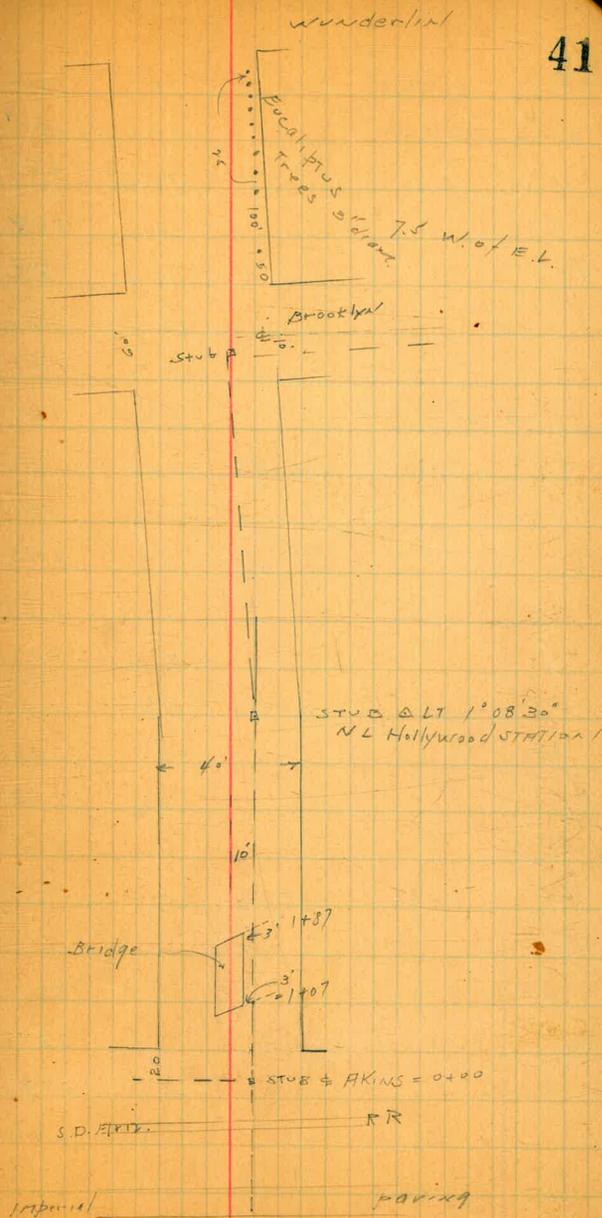
74.1

on Hubs

Cross Section of Water Line
 on 60th St Imperial to Brooklyn
 10' EAST of E 60th = 40' wide

Storo
 Walter
 16
 Preston
 26
 5900

11/11/1913	1.00	180.74	179.74
00-167		3.7	177.0
-159		7.6	173.1
-152.5	Sedge paving	7.90	172.84
-137.3	N. "	7.66	173.88
-100		8.4	172.3
-85		8.4	172.3
-80		9.7	171.0
-71	E S.D. RR	8.9	171.8
-50		10.1	170.6
0+00	T.P. stub 9.69	11.13	169.61
+50		10.3	169.0
+69		10.0	169.3
+90		10.6	168.7
	Floor bridge sand	7.9	171.4
+07	SL Bridge	12.6	166.7
+08		15.6	163.7
+19		16.5	162.8
+28		13.6	165.7
+57	NL Bridge	12.0	167.3
	Floor elev. bridge N. end	4.96	174.34
+91		7.5	177.8
+75		7.2	172.1
+57		0.5	178.8
T.P.	129.2	192.3	0.00
			179.30



		19v. v3		
2	+87		10.3	181.9
	3+10		9.5	182.7
	+30		10.0	182.2
	+70		3.7	188.5
4			3.0	189.2
	+50		2.1	190.1
5			1.4	191.0
5	+39	¹⁰⁰⁸³⁰¹⁷ A STUB	0.39	191.84
	T.P.	131.4	40496	0.39
	+60		17.6	192.4
6			9.9	195.1
	+50		5.4	199.6
7			0.6	204.4
	T.P.	13.11	418.03	0.04
	+50		9.5	208.5
8			5.8	212.2
	+50		2.5	215.5
	T.P.	14.93	430.86	0.10
9			12.2	218.6
	+50		9.2	221.7
10			6.9	224.0
	+50		3.6	227.4
11			1.9	229.0
	T.P.	12.83	443.56	0.13
	+50		12.6	231.0

		243.56		
12	+00		10.9	232.7
	+51.8 = 10.5 at 4 Brooklyn		8.30	235.26 on stub
	Set 81 spike Sulfide ^{Brooklyn} 6070		7.25	236.31

42

Cross Section of 60th
Brooklyn to underlin

40' wide
5' sidewalks
7 1/4' 1/4"

Moore
4/16/wb > 43.56

See page 41 for trees

243.56

NL Brooklyn 100

w/	4.9	238.7
cb	5.4	238.2
1/4	5.7	237.9
c	5.6	238.0
1/4	5.8	237.8
cb	7.5	236.1
E	8.0	235.6
+5	8.1	235.5
75' N		
-5	6.6	237.0
E	6.1	237.5
cb	5.3	238.3
1/4	3.9	239.7
c	3.6	240.0
1/4	5.8	239.8
+5	4.5	239.1
cb	3.5	240.1
w/	2.8	240.8
50' N		
w/	0.4	243.2
cb	1.4	242.2
+5	2.5	241.1
1/4	1.6	242.0

c	1.6	242.0
1/4	2.1	241.5
cb	3.7	239.9
E	4.2	239.4
+5	4.6	239.0
T.P.	12.69	256.06
75' N		
-5	16.0	240.1
E	15.1	241.0
cb	14.5	241.6
1/4	12.4	243.7
c	11.8	244.3
1/4	12.0	244.1
cb	11.8	244.3
w/	10.8	245.3
100' N		
w/	7.4	248.7
cb	8.2	247.8
+3	9.3	246.8
1/4	9.3	246.8
c	9.0	247.1
1/4	9.2	246.9
cb	11.9	244.2
E	12.8	243.3
+5	13.5	242.6

256.06 π

195' N		
-5	10.6	245.5
E	9.9	246.2
cb	9.0	247.1
+w	8.7	247.4
1/4	6.7	249.4
e	6.6	249.5
1/4	7.1	249.0
+v	7.1	249.0
cb	7.8	251.3
w	4.1	252.0

150' N

w	1.0	255.1
cb	1.6	254.5
+5	4.4	251.7
1/4	4.6	251.5
c	4.6	251.5
1/4	4.3	251.8
cb	5.9	250.2
E	6.7	249.4
+5	7.8	248.3

175' N

-5	4.4	251.9
cb	3.4	252.7
cb	2.6	253.5

256.06 π

60 + 7

44

1/4	2.0	254.1	
e	2.4	253.7	
1/4	2.5	253.6	
TP 12.78	~68.68	0.16	255.90
+5	12.6	256.1	
cb	12.5	256.2	
w	12.0	256.7	
200' N			
w	9.9	258.8	
cb	10.4	258.3	
+3	11.1	257.6	
1/4	12.8	255.9	
c	12.7	256.0	
1/4	12.6	256.1	
cb	12.9	255.8	
E	13.9	254.8	
+5	14.5	254.2	
225' N			
-5	12.0	256.7	
E	11.4	257.3	
cb	10.7	258.0	
1/4	10.8	257.9	
c	10.7	258.0	
1/4	11.2	257.5	
+5	8.7	260.0	

268.68

cb	8.7	260.0
w/	8.0	260.7
250'N		
w/	5.9	262.8
cb	6.5	262.2
+v	6.6	262.1
1/4	8.6	269.1
e	8.8	259.9
1/4	8.7	260.0
cb	8.9	259.8
E	9.4	259.3
+5	9.9	258.8
275'N		
-5	7.9	260.8
E	7.4	261.3
cb	7.1	261.6
1/4	6.9	261.8
c	6.7	262.0
1/4	6.9	261.8
+v	6.6	262.1
cb	5.1	263.6
w/	4.4	264.3
300'N		
w/	3.4	265.5
cb	3.9	264.8

268.68

6076

45

1/4	5.4	263.5
c	4.9	263.8
1/4	5.4	263.3
cb	6.0	262.7
E	6.6	262.2
+5	7.0	261.7
325'N		
-5	4.7	264.0
E	4.4	264.3
cb	4.1	264.0
1/4	3.6	265.1
c	3.4	265.3
1/4	3.6	265.1
cb	2.8	265.9
w/	2.1	266.6
350'N		
w/	0.0	268.7
cb	0.6	268.1
1/4	1.6	267.1
c	1.5	267.2
1/4	1.7	267.0
cb	2.2	266.5
E	2.3	266.4
+5	2.6	266.1
T.P	12.98	281.57
	0.09	268.59

281.57

375¹/₂

-5	13.7	267.9
E	13.5	268.1
cb	13.0	268.6
1/4	13.0	268.6
e	12.7	268.9
1/4	12.7	268.9
cb	12.0	269.7
v	11.4	270.2

400¹/₂

v	9.5	272.1
cb	10.0	271.6
1/4	10.4	271.2
e	10.7	270.9
1/4	11.2	270.4
cb	11.3	270.3
E	11.6	270.0
±5	11.6	270.0

435.5 = St Wunderlin

E	9.2	272.4
cb	9.0	272.6
1/4	8.6	273.0
c	8.0	273.6
1/4	7.7	273.9
cb	7.5	274.4

381.57

60¹/₂

v	6.9	274.7	46
scr spine vnd pale 60 ¹ / ₂	1.8	279.76	
TP 1195	29.18	270	280.87
check to 2 marks SE Cor Body + 60 ¹ / ₂	6.70	286.14	284.24

Water line on Brooklyn 60' wide
10' S of E

Jul Brooklyn - 60' wide	21.7	238.48		236.31
0+00 = 10' E of E of 60' b			3.0 ✓	235.26
+50			5.5	233.0
+75			6.5	232.0
1			8.7	229.8
+50			10.8	227.7
2			11.3	227.2
+50			10.7	227.8
3			7.5	231.0
+50			4.9	233.6
+97.8 = 10' E of E of 61' +			2.6	235.9
T.P.	12.3 ✓	250.68	0.1 ✓	238.3 ✓
+50			12.0 ✓	238.5
5			9.4	241.3
+50			10.0 ✓	240.5
6			11.5	239.2
+50			10.4	240.3
7			9.0 ✓	241.5
+50			6.3	244.4
check to spike sw Fergus & Brooklyn			6.36	244.3 ✓
7+73.6 = 10' E of E of Fergus			5.3	245.4
8+00			3.7	247.0
+50			2.7	248.0
9+00			1.6	249.1
9+50			0.6	250.1

250.32

47

7.0	6.95	257.50	0.13	250.55
10+00			6.1	251.4
+50			6.1	251.4
11			6.9	250.6
+50			8.7	248.8
+70			9.3	248.2
12			12.4	245.1
+30			16.3	241.4 ✓
+35 = 10' E of E			16.8	240.7
+40 = 62' here somewhere			17.3	240.2
+50			12.1	245.4
13			6.5	251.0
+50			2.6	254.9
14			0.0 ✓	257.48
T.P.	12.83	270.31	11.4	258.9
+50			6.7	263.6
15			2.3	268.0
+50			0.1 ✓	270.19
T.P.	9.33	279.5 ✓	8.0	271.5
+50			6.4	273.1
16			5.0	274.3
+30 = w/L 63'			6.4	273.1
+45			6.4	273.1
+67 = New water main			6.4	273.1
T.P. 30' N of sw Brooklyn			7.70	271.8 ✓
bad 106	272.88		1.0 ✓	271.78
17				271.7

272.88

+50			2.8	270.1
18			4.2	268.7
+50			5.6	267.3
19			6.2	266.7
+50			6.1	266.8
20			5.3	267.6
+50			5.2	267.7
+97 = 10' E of E. of STARK			5.1	267.5
21 +50			6.1	266.8
22			7.2	265.7
+50			9.4	263.5
T.P.	0.69	261.11	12.46	260.42
23			1.7	259.4
+50			7.1	254.0
+80			10.8	250.3
24			12.3	248.8
T.P.	0.22	248.62	12.72	248.39
+50			3.0	245.6
+80			4.6	244.0
25			6.9	241.7
+33 = E of 64th 30' wide			11.6	237.0
+50			14.5	234.1
T.P.	9.14	244.83	12.93	235.69
+75			17.1	227.7
+85			17.8	227.0

244.83 Brooklyn WATER

48

26			12.0	232.8
+25			1.7	243.1
T.P.	12.21	256.69	0.35	244.48
+50			4.9	251.8
T.P.	11.79	268.18	0.30	256.39
+75			10.2	257.9
27			5.2	263.0
+25			2.0	266.2
+38			1.0	267.2
T.P.	7.19	275.37	0.00	268.18
+53 = Cypress Lane approx.			5.3	270.1
+65			5.2	270.2
+82 = Top wooden water main			8.2	267.2
check to 3rd Sulpice ^{Brooklyn} 65th			6.46	268.91
				268.88

WATER LINE 10' off of 62 ^m d ST 60' wide			
Imperial to Brooklyn			
	12.69	✓ 100.25	
17.0 soft & AKINS 0400	0.0	200.3	187.56
+4	4.9		195.4
+8 = SL paving	4.3		196.0
+26.4 - NL ✓	4.24		196.01
+70	6.1		194.2
+95 & SDD ARR RR	7.4		192.9
+25	10.6		189.7
+50	13.0		187.3
+70 = & AKINS	13.6		186.7
T.P. 440	12.69	191.96	187.56
✓	5.2		186.8
+50	4.5		187.5
+75	5.5		186.5
→ Sedge creek	8.2		183.8
+41.1	8.7		183.3
+43	6.6		185.4
+50	6.6		185.4
4	4.8		187.2
+50	3.3		188.7
T.P. 11.47	0.03	✓ 103.40	191.93
5	9.8		193.6
+50	3.5		199.9
T.P. 12.27	0.34	✓ 15.33	✓ 103.06
6	11.1		204.2

215.33			
6+50	7.2		208.1
7	3.7		211.6
T.P. 11.96	✓ 26.90	0.37	✓ 14.94
+50	11.4		215.5
8	7.2		219.7
+50	2.8		224.1
T.P. 13.02	✓ 39.83	0.09	✓ 26.81
9	10.6		229.2
+50	6.8		233.0
10	5.4		234.4
+50	6.0		233.8
11	7.3		232.5
+50	6.1		233.7
12	2.0		237.8
T.P. 8.94	✓ 48.35	0.42	✓ 39.41
+38 = 10' soft & if Brooklyn	7.3		241.0
& Hub gate?	Approx.		
on ground at Sta. 12+30 Brooklyn	6.94	✓ 11.4	✓ 241.2
LINE			See page 47

WATER LINE 10' E of C of FERGUS ST
IMPERIAL TO BROOKLYN
60' wide

Nursery Atkins Fergus 639	186.13		179.74
160 S. of Atkins = 0400 = SL paving	3.87		182.26
+18.5 = NL v	3.77		182.36
+25	4.2		181.9
+30	6.9		179.2
+45	9.2		176.9
+65	9.3		176.8
+70	5.3		180.8
+84.25 = SDAH 12 RR	3.3		182.8
+93	3.2		182.9
+108 = Sedge creek	11.8		174.3
+34	10.5		175.6
+32 = 1/2 bank creek	6.5		179.7
+160 = Atkins	6.8		179.3
v	6.0		180.1
+50	2.6		183.5
T.P. 14.25	198.16	0.22	185.91
D	10.5		187.6
+50	5.7		192.4
v	2.2		195.9
+50	0.5		197.6
T.P. 10.38	208.08	0.46	197.70
v	8.2		199.8
+50	6.9		201.2
6	5.4		202.7

Moore
6/13/76

208.08

50

+50	2.1		206.05 w 1' Lower
T.P. 12.85	206.6	0.51	207.57
7	11.8		208.65 w 1' Lower
+50	7.7		212.7 v r 1 ✓
8	5.0		215.45 w 1.5 ✓
+50	0.8		219.6 (1.0 ✓
T.P. 12.86	233.14	0.14	230.78
9	9.9		223.2
+50	6.1		227.0
10	4.0		229.1
+50	1.8		231.3
T.P. 11.50	244.17	0.37	234.77
11	10.0		234.2
+50	6.9		237.35 w 1.50 Lower
12	4.0		240.2 v 1.0 ✓
T.P. 4.76	248.56	0.37	243.80
+50	4.2		244.4 (1.3 ✓
+96 = 10 S. of 1/4 Brooklyn	3.3		245.3
check BM ^{Brooklyn} Fergus	4.7		244.49 + 4.70
T.P. 10.8	238.37	11.27	237.14

14000 WATER LINE 10' E of E of 61st ST
 Brooklyn to Imperial
 6/10/66

		238.37	from last page (50)	
10' S of E of Brooklyn = 0700			2.3	236.1
+50			6.0	232.4
1			9.5	228.9
+50			13.2	225.2
T.P.	0.80	226.47	12.90	223.47
~			3.8	222.5
+50			6.0	220.3
3			8.4	217.9
+50			11.3	215.0
+75			12.5	213.8
T.P.	0.97	214.71	12.53	213.74
4			2.8	211.9
+45			5.8	208.9
+70			10.2	204.5
+95			10.9	203.8
5 + 30			9.3	205.4
+50			10.0	204.7
6			11.8	202.9
T.P.	1.34	203.75	12.80	201.91
+50			2.4	200.9
7			5.4	197.9
+183			5.9	197.4
+50			6.2	197.1
8			8.1	195.2

~ NL Hollywood Station

203.25

51

8 + 50			9.6	193.7
9			10.6	192.7
+40			12.0	191.3
T.P.	0.97	191.58	12.59	190.66
+75			6.4	185.2
10			11.5	180.1
T.P.	1.65	180.39	12.84	178.74
+50			5.5	174.9
11			6.5	173.9
+50			6.7	173.7
+60			6.6	173.8
+65			11.0	169.4
+92.2			10.73	169.66 on stub
12 + 20			10.1	170.3
+25			6.8	173.6
+50			4.4	176.0
T.P.	7.35	183.51	4.23	176.16
+65.94			6.2	177.3
+75			7.1	176.4
+80			5.2	178.2
13			4.7	178.8
+33			5.03	178.48
13 + 51.505			5.08	178.43
on to BM			3.81	179.70
ALC. 115				179.77
Perquis				

Cross Section of ^{50' wide} _{10' cbs}
BRANT ST
Douglas to Univ. Ave

2.57 270.57 Douglas
268.00 BRANT

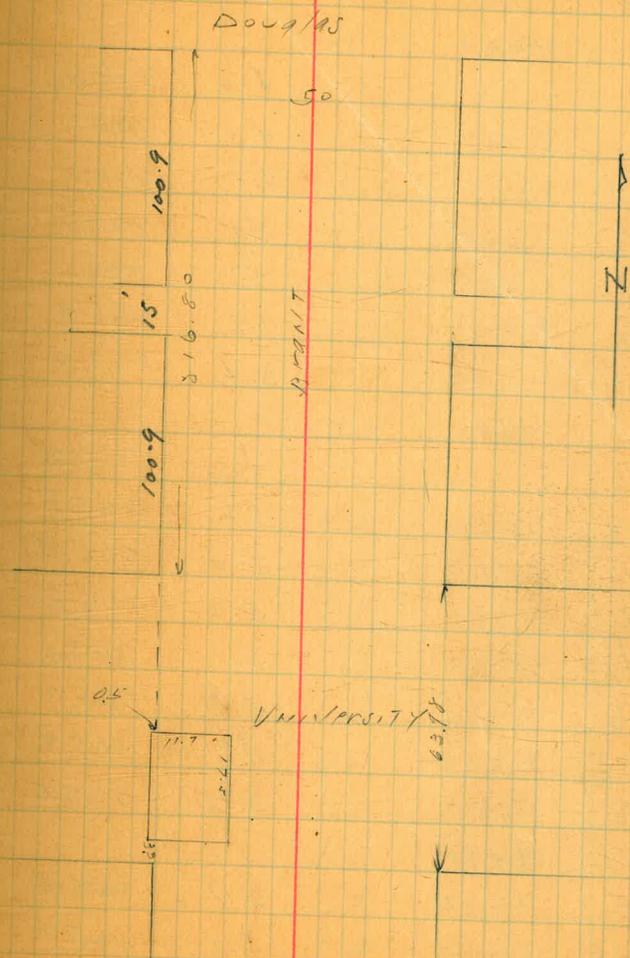
St Douglas = 00

w/		3.1	267.5
cb	Top cb	3.49	267.08
gut		4.0	266.6
1/4		3.9	266.7
c		3.8	266.8
1/4		4.0	266.6
gut		4.0	266.6
cb	top cb	3.48	267.09
E		2.9	267.7
	0 + 07		
E		2.5	268.1
cb		2.5	268.1
1/4		3.5	267.1
c		3.5	267.1
1/4		2.3	267.3
cb		3.0	267.6
w/		2.6	268.0
	0 + 50		
w/	outlain	2.7	267.9
cb		2.9	267.7
1/4		3.0	267.6
e		3.1	267.5

Plotted
6/2/71
J.P.

cb + pl

52



270.57

1/4		3.2	267.4
cb		3.3	267.3
E		3.0	267.6
	1+00		
E		4.0	266.6
cb		4.3	266.3
1/4		4.1	266.5
e		4.1	266.5
1/4		4.1	266.5
cb		3.9	266.7
w		3.4	267.2
	1+50		
w		4.6	266.0
cb		5.1	265.5
1/4		5.0	265.6
e		5.0	265.6
1/4		5.1	265.5
cb		4.9	265.7
+5		4.7	265.9
E		3.6	267.0
	1+95		
E		3.5	267.2
cb		5.2	265.4
1/4		5.6	265.0
c		5.5	265.1

270.57

Brant

58

1/4		5.5	265.1
cb		5.7	264.9
+5		5.4	265.2
w		4.7	265.9
	2+00		
w		5.0	265.6
cb		5.7	264.9
1/4		5.5	265.1
e		5.5	265.1
1/4		5.7	264.9
cb		5.2	265.4
E		4.5	266.2
	3+05		
-5		9.5	261.1
E		7.9	262.7
+w		7.9	262.7
+6		8.1	262.5
cb		6.4	264.2
+5		5.3	265.3
1/4		5.5	265.1
c		5.8	264.8
1/4		5.7	264.9
cb		5.9	264.7
w		5.4	265.2

270.57

	3 + 16.80	= 21 L	UNIV	17.0	= 62.9 ^{wick}
W				5.7	264.9
cb				6.1	264.5
1/4				5.8	264.8
C				5.9	264.7
+5				5.6	265.0
1/4				6.3	264.3
cb				8.5	262.1
+3				10.4	260.2
EL				13.7	256.9
+10				15.3	254.3
TP	3.13	265.92	7.78	267.79	
	N cb	2+76.8			
-15				17.5	248.4
-7				17.2	248.7
E				12.1	251.8
+7				11.4	252.5
cb				10.0	255.9
1/4				6.2	259.7
C				1.3	264.6
1/4				1.5	264.4
cb				1.6	264.3
W				1.4	264.5
	N 1/4	2+38.05			
W				1.3	264.6

265.92

BRANT

54

cb	1.3	264.6
1/4	1.8	264.1
0	2.5	263.4
+5	2.6	263.3
1/4	4.0	261.9
cb	9.0	256.9
+6	11.6	254.3
+7	13.2	252.7
E	14.7	251.2
+10	20.1	245.8
+20	25.2	240.7
	E Univ.	2+49.3
-20	26.0	239.9
-16	24.5	241.4
-15	23.2	242.7
E	11.8	254.1
cb	7.3	258.6
+5	4.1	261.8
1/4	4.1	261.8
+3	4.6	261.3
C	2.1	263.8
1/4	1.5	264.4
cb	0.9	265.0
W	1.1	264.8

	26.59 ^W	
S 1/4	2+60.55	
W	1.1	264.8
cb	1.0	264.9
1/4	2.3	263.6
C	3.0	262.9
+2	6.3	259.6
1/4	5.8	260.1
+5	4.5	261.4
cb	6.8	259.1
E	12.5	253.4
+20	24.0	241.9
+30	30.0	235.9

	S cb	2+71.8
-30	31.3	234.6
-20	24.1	241.8
E	14.6	251.3
cb	9.7	256.2
+5	7.0	258.9
1/4	7.3	258.6
C	8.7	257.2
+2	8.7	257.2
+4	4.5	261.4
cb	3.4	262.5
W	1.5	264.4

	265.9 ^W	Branch	55
S L Univ. F10	2+81.8		
W	2.4	263.5	
cb	5.5	260.4	
1/4	9.6	256.3	
+5	10.5	255.4	
C	9.9	256.0	
1/4	9.3	256.6	
cb	12.5	253.4	
E	18.1	247.8	
+30	32.0	233.9	
8.5 ^{2+89.8} / S L _n = N L of residence			
-30	31.0	234.9	
E	23.2	242.7	
+2	18.0	247.9	
cb	14.4	251.5	
1/4	14.5	251.4	
C	11.5	254.4	
1/4	13.1	252.8	
+5	12.5	253.4	
cb	10.1	255.8	
W	3.9	262.0	
20.5 ^{2+81.8} / S L _n = Univ. F10 = 3+81.8			
W	5.5	260.4	
+8	11.4	254.5	
cb	15.7	250.2	

265.94

BRANT

7/4		15.2	250.7	
+4		14.9	251.0	
C		16.8	249.1	
+3		20.0	245.9	
1/4		20.3	245.6	
66		21.5	244.1	
E		23.4	242.5	
+3.5	= residence Floor elev.	23.6	242.3	
TP	6.9	270.71	1.40	264.52
check to B.M.		2.71	265.00	265.00

Plotted
6/2/71
Burgster

56

Cross Section of Fall on West Side
of 29th St South of Juniper 10' curb

NE Tabled 0.03 270.16 270.13
T.P. 1.40 265.81 575 264.41

150' S of 1st Juniper = Sewer curb + sidewalk

Web top cement 1.48 264.33
W/L 1.3 264.5

175' S

Web 1.7 264.1
W/L 2.0 263.8
+11 9.0 256.8

191' S

Web 2.3 263.5
W/L 1.7 261.1
+30 22.3 243.5

200' S = North end of curb

Web top cement 1.84 263.99
W/L 5.2 260.6
+32 27.4 238.6

220' S

Web top cement 1.95 263.86
W/L 4.8 261.0
+20 21.5 244.3
+40 30.2 235.6

235' S

Web top cement 4.15 263.66
W/L 5.8 260.0

4/11/21

265.81

Moore

W/L + 20 23.0 242.8
" + 35 27.7 238.1

240' S

Web top cement 2.11 263.70
W/L 5.8 260.0
+15 14.7 251.1
+35 27.6 238.2

245' S

Web top cement 2.07 263.74
W/L 4.0 261.8
+15 14.3 251.5

250' S

Web top cement 2.07 263.74
W/L 3.5 262.3
+10 11.1 254.7

268' S = North end of sidewalk (cement)

Web top cement 2.12 263.69
W/L 3.1 262.7

52

Moore Curb Levels on
 5/1/27 Torrence betw Pringle + Mission Hills Blvd
 Torrence = { 50' wide 12' curbs
 26' Roadway

Torrence is graded and accepted. Private Contract.

obsol. 740' north of Pringle

Top Hght 11.5' 248.78' 237.27 Pringle Torrence

NL Pringle = 00

Wcb Top cement Return 14.8' 235.94

Ecb " " " 10.8" 237.96

20' n

Ecb top dirt curb 9.1 239.7

Wcb " " " 10.0 238.8

40' n

Wcb 7.8 241.0

Ecb 7.0 241.8

60' n

Ecb 5.5 243.0

Wcb 6.4 242.6

80' n

Wcb 5.6 243.2

Ecb 5.0 243.8

100' n

Ecb 4.8 244.0

Wcb 5.3 243.5

120' n

Wcb 5.7 243.1

Ecb 5.1 242.7

PLOTTED
 57' n
 APR

248.78

58

140' n

Ecb 6.0 242.8

Wcb 6.7 242.1

160' n

Wcb 8.3 240.5

Ecb 7.7 241.1

200' n

Ecb 11.7 237.1

Wcb 12.5 236.3

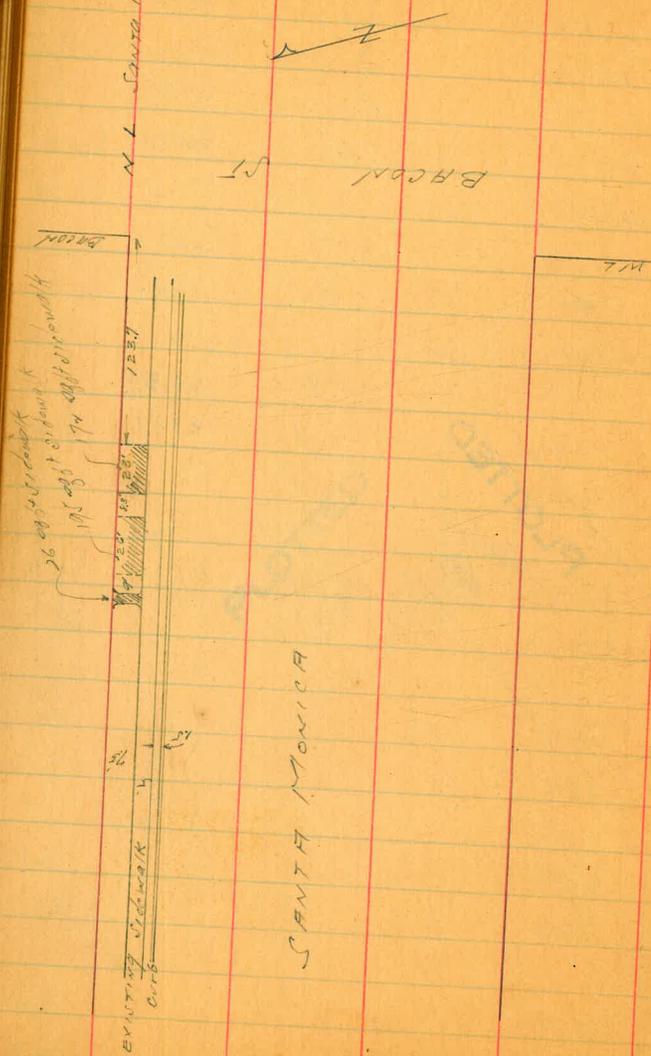
240' n this section is 4194

Wcb 12.9 238.9

Ecb 12.9 233.9

PLOTTED
 57' n
 APR

5/4/67 Moore
 Sidewalk to be excerpted on
 Santa Monica west of Bacon St
 Show cross hatched



SANTA MONICA

26
 76
 130
 184
 175

45
 75
 115
 161
 170.5

Bliss Levels on Improvements on
1071-7 Brant St. Douglass to Univ.

1	2.28	270.28		268.00
0+24			2.10	<u>270.3</u> 268.2
0+65			2.59	267.7
0+66			2.79	267.5
0+85			2.88	267.4
0+86			2.56	267.7
0+9			3.29	267.0
0+91			2.27	268.0
T.P.	5.39	270.32	5.35	264.93
0+00	Levels on Univ. West Prop Univ & Brant			<u>270.3</u>
0+43			9.09	266.2
0+64			9.91	265.9
0+98			5.25	265.0
1+51			6.33	264.0
Side Walk West End of Univ			11.12	259.2
Porch of House West End of Univ			10.16	260.2
B.M.			4.33	267.99

Side walk on West side Brant
" " " " " "

Side walk East Side

Auto Drive way West side

Step of Residence East side

" " " West side

Porch of residence

Side walk N. Side Univ

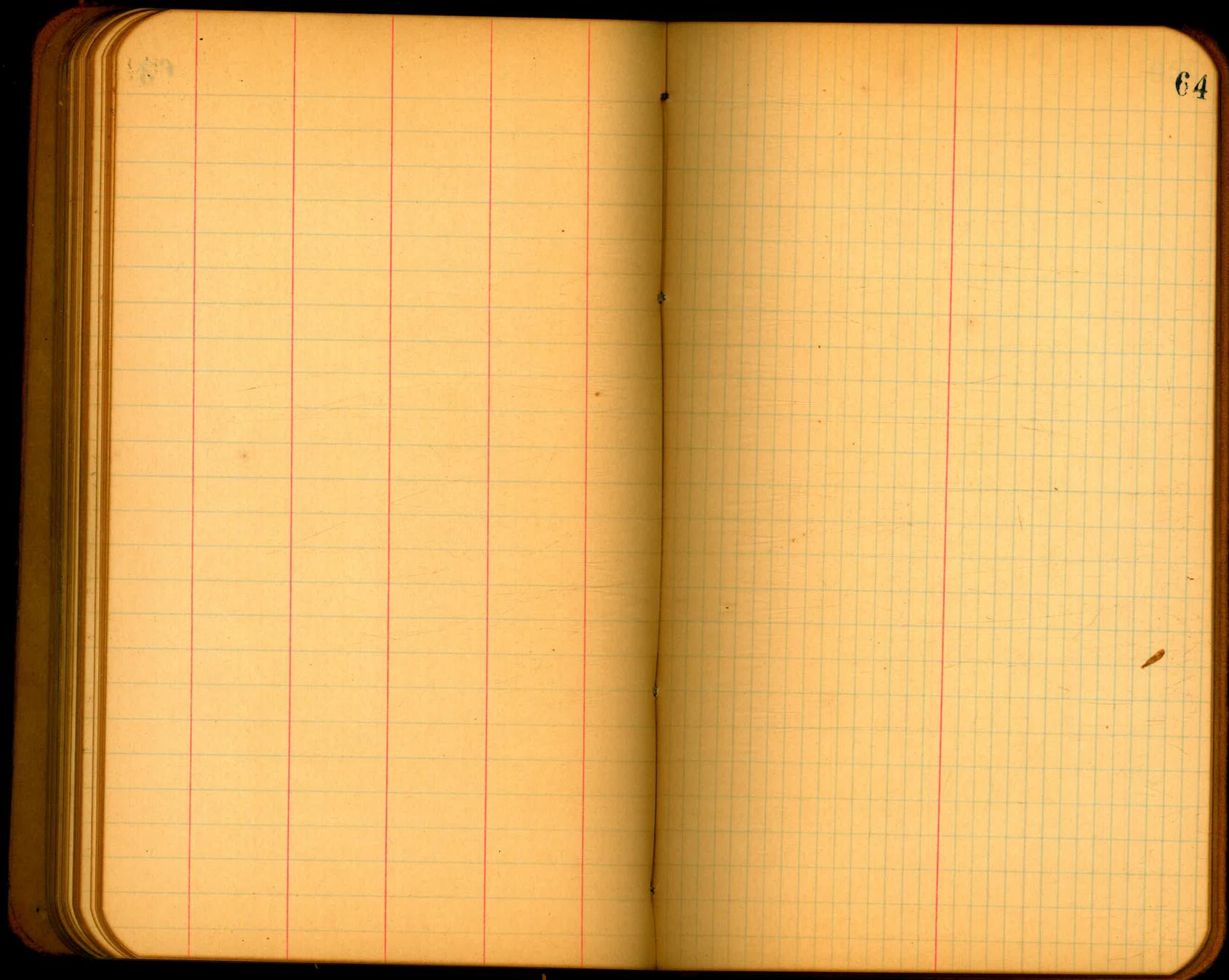
Auto Drive way North Side Univ

Side walk N. Side

" " " "

60

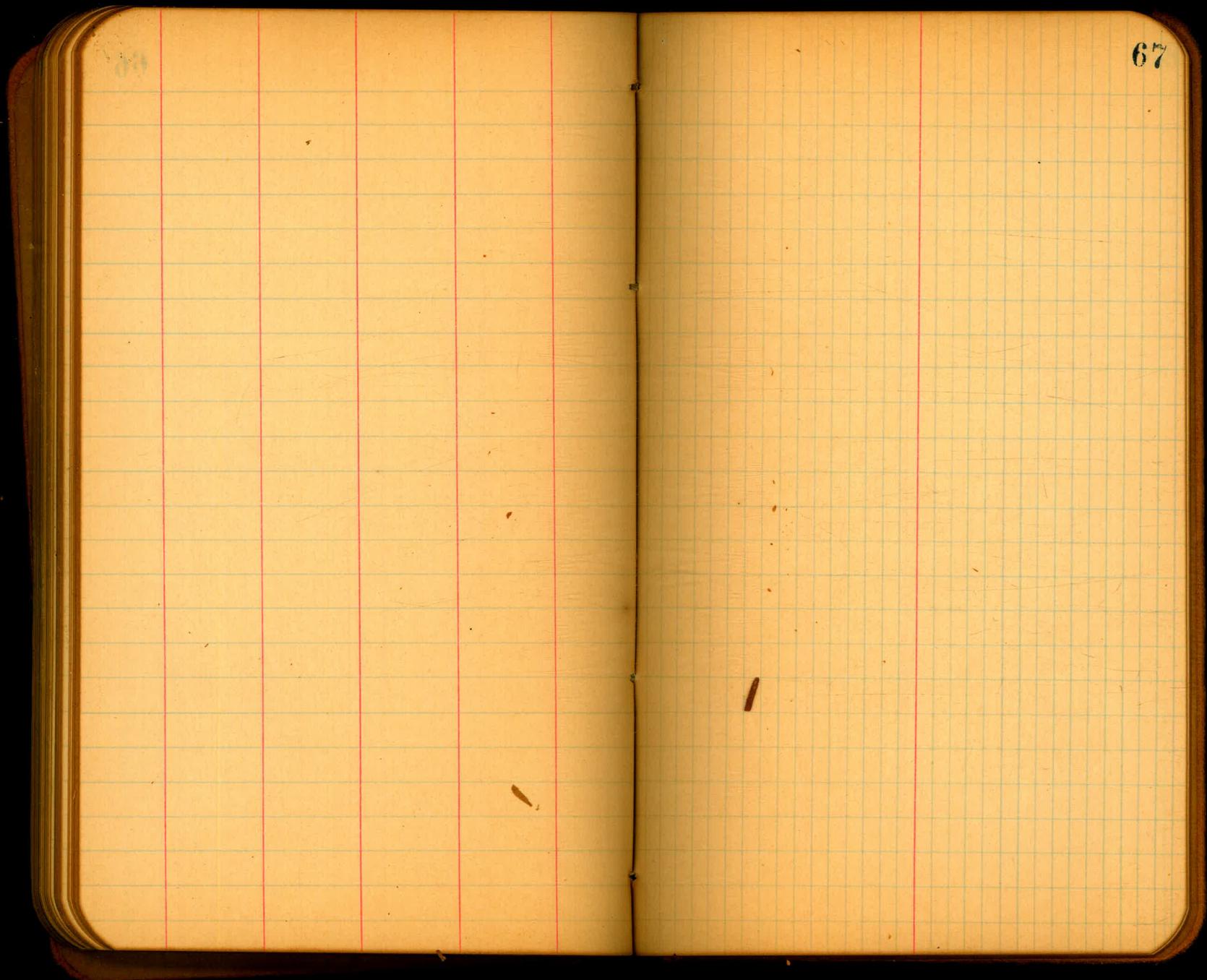
63

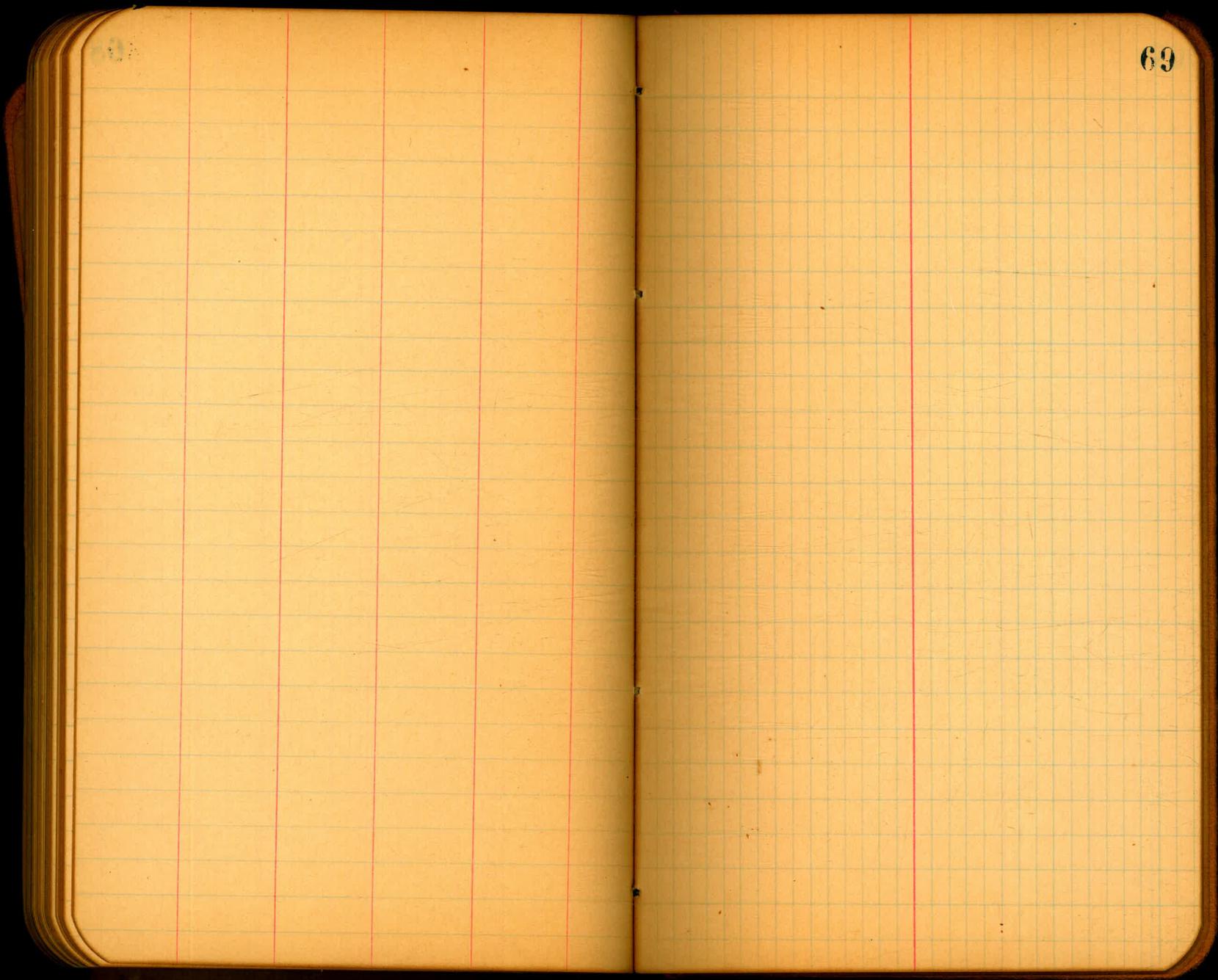


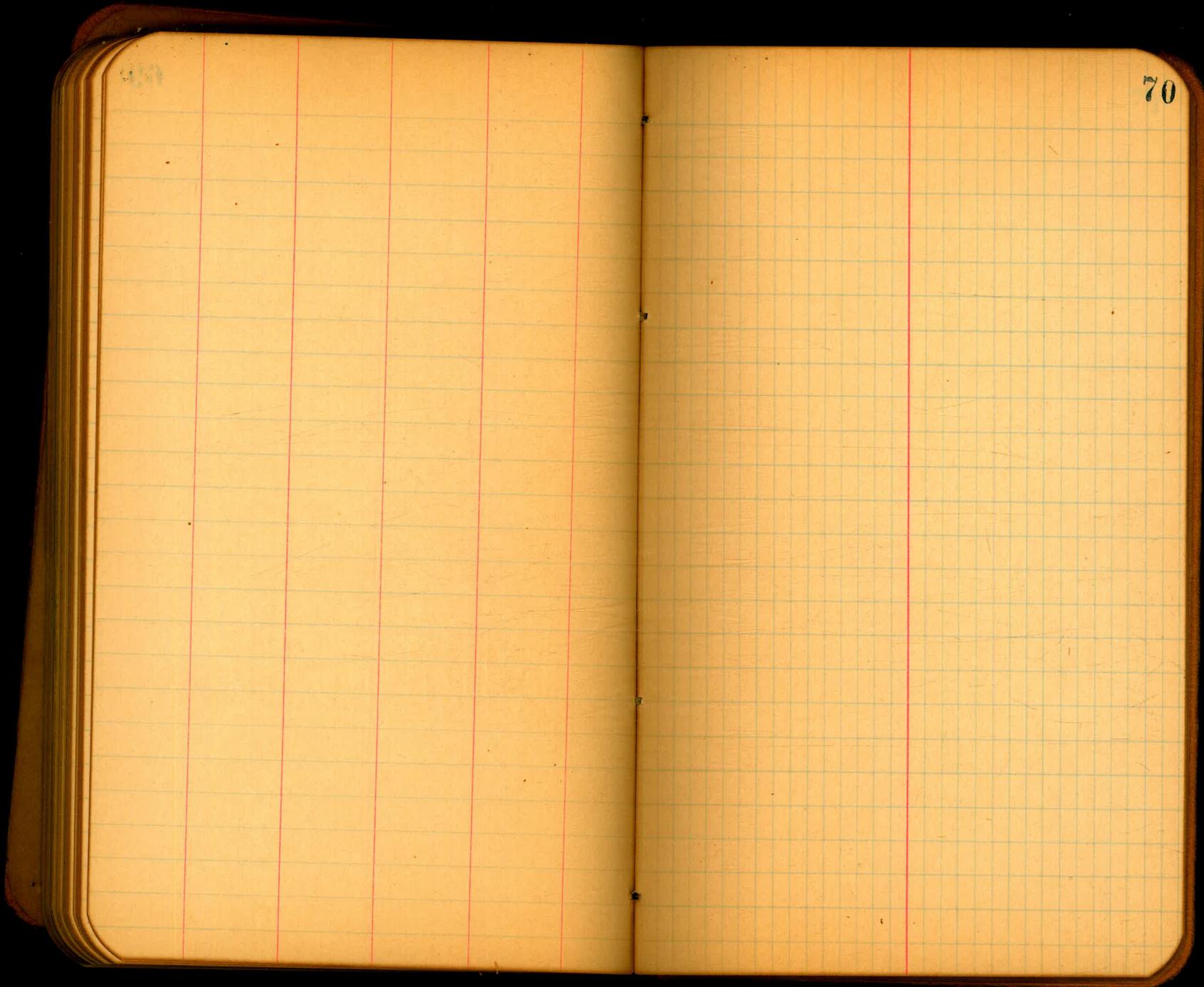
64

65

66

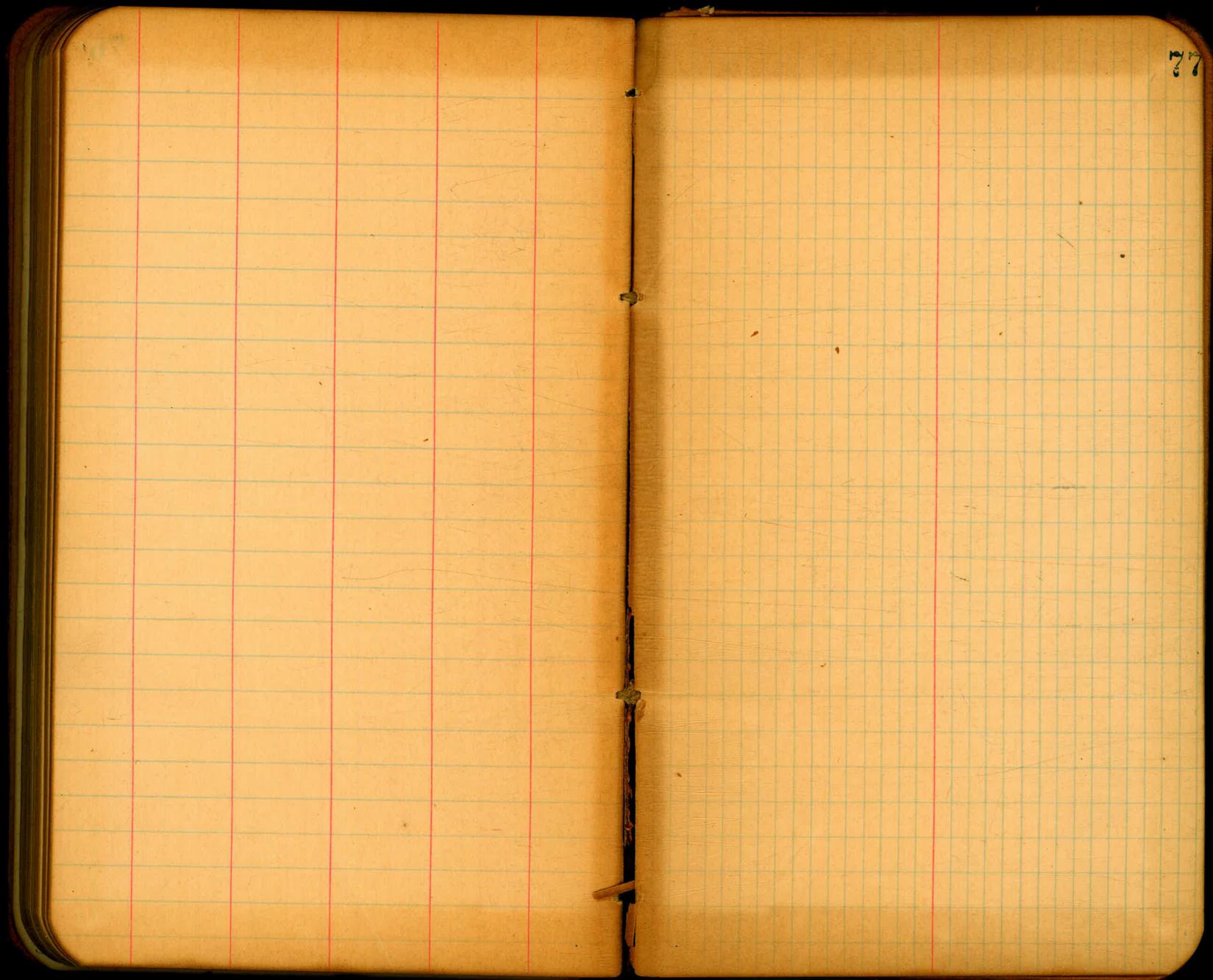




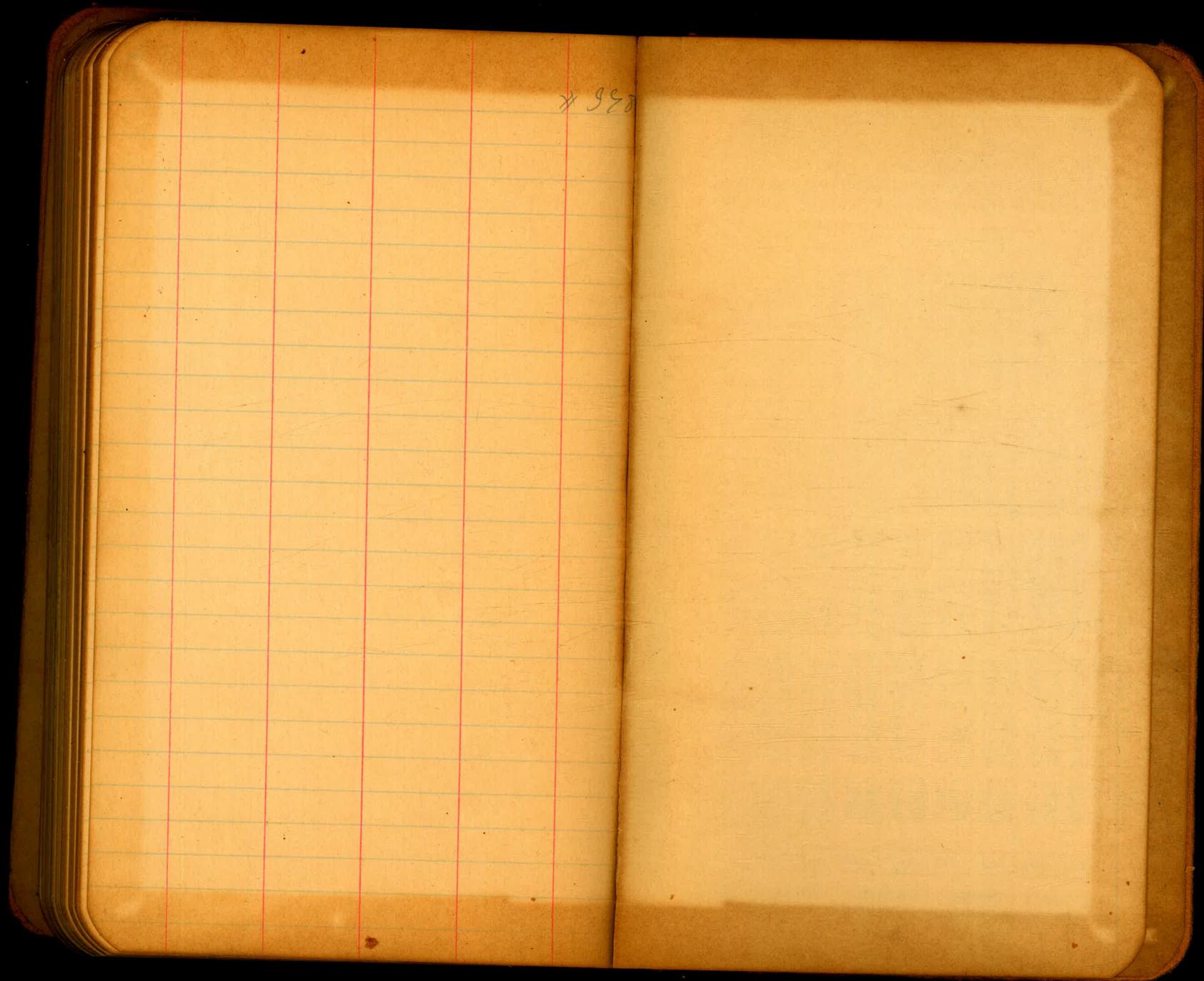


[Faint pencil scribbles]

74



77



* 998

12635
 160
 75.95
 84.25
 1192.2
 75.75
 1268.95

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TRAVERSE TABLE FOR TRANSIT BOOK.
 From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100.00	0.44	100.00	0.87	99.99	1.31	89
1	99.98	1.75	99.98	2.18	99.97	2.62	99.95	3.05	88
2	99.94	3.49	99.92	3.93	99.91	4.36	99.88	4.80	87
3	99.86	5.23	99.84	5.67	99.81	6.10	99.79	6.54	86
4	99.76	6.98	99.73	7.41	99.69	7.85	99.66	8.28	85
5	99.62	8.72	99.58	9.15	99.54	9.58	99.50	10.02	84
6	99.45	10.45	99.41	10.89	99.36	11.32	99.31	11.75	83
7	99.25	12.19	99.20	12.62	99.14	13.05	99.09	13.49	82
8	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	15.64	98.70	16.07	98.63	16.50	98.56	16.93	80
10	98.48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98.16	19.08	98.08	19.51	97.99	19.94	97.90	20.36	78
12	97.81	20.79	97.72	21.22	97.63	21.64	97.53	22.07	77
13	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	24.19	96.92	24.62	96.81	25.04	96.70	25.46	75
15	96.59	25.88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.82	73
17	95.63	29.24	95.50	29.65	95.37	30.07	95.24	30.49	72
18	95.11	30.90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35.43	69
21	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38.67	67
23	92.05	39.07	91.88	39.47	91.71	39.87	91.53	40.27	66
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	43.84	89.69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	46.95	88.09	47.33	87.88	47.72	87.67	48.10	61
29	87.46	48.48	87.25	48.86	87.04	49.24	86.82	49.62	60
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	52.99	84.57	53.36	84.34	53.73	84.10	54.10	57
33	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	52
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	45
45	70.71	70.71							
Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees.
	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		