Return to City Engineers Office
City Hall, San Diego, Cal.

400 LEVEL

F.B. 457

Return to City Engineers Office
City Hall, San Diego, Cal.

Cocker Duchy

Published by H. S. CROCKER COMPANY, Stationers, Drawing Materials, and Mathematical Instruments, San Francisco.

Table showing the difference of latitude and departure in running 80 chains at any course from 1 to 60 minutes.

457

MINUTES.	LKS.	MINUTES.	LKS.	MINUTES.	LKS.
1	2⅓	21	49	41	95⅔
2	4⅔	22	51⅓	42	98
3	7	23	53⅔	43	100⅓
4	9⅓	24	56	44	102⅔
5	11⅔	25	58⅓	45	105
6	14	26	60⅔	46	107⅓
7	16⅓	27	63	47	109⅔
8	18⅔	28	65⅓	48	112
9	21	29	67⅔	49	114⅓
10	23⅓	30	70	50	116⅔
11	25⅔	31	72⅓	51	119
12	28	32	74⅔	52	121⅓
13	30⅓	33	77	53	123⅔
14	32⅔	34	79⅓	54	126
15	35	35	81⅔	55	128⅓
16	37⅓	36	84	56	130⅓
17	39⅔	37	86⅓	57	133
18	42	38	88⅔	58	135⅓
19	44⅓	39	91	59	137⅔
20	46⅔	40	93⅓	60	140

MICROFILMED
DEC 10 1964

TABLE FOR RUNNING ON SLOPES.

In the following table the first column shows the angle, the second the number of links to be added to a chain on the slopes, to make one chain, horizontal measurement.

ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS
°		°		°		°	
4	0.24	11	1.88	18	5.14	25	10.54
5	0.38	12	2.24	19	5.76	26	11.26
6	0.55	13	2.63	20	6.42	27	12.24
7	0.76	14	3.06	21	7.11	28	13.37
8	0.98	15	3.53	22	7.85	29	14.34
9	1.24	16	4.02	23	8.64	30	15.47
10	1.55	17	4.56	24	9.47	35	22.07

Crocker Quality

LEVEL BOOK

No. 400

COMMUNI CONSENSU PRIMO TRADE MARK

FROM Loring's Book Store

MANUFACTURED BY
A. S. Crocker Co.
SAN FRANCISCO
and
SACRAMENTO

Levelright
Tollbridge
Woods
1/26/09

Cross section of James st (70)
continued from Book 447

5-611

Wm J. Rosecrans et (100' Broadway)

SL		4.7	51.6
½		5.0	51.1
"	Plotted	5.0	51.1
½		5.5	50.6
"		5.6	50.3
½		6.1	50.0
NL		6.5	49.6

5 Wm J Rosecrans

NL		5.1	51.0
½		4.0	52.1
"		4.9	53.2
½		5.1	53.9
"		5.5	54.6
½		0.9	55.2
SL		0.5	55.6
TP	1.65	6.54	0.11	55.8

POSTED

685-4

	50'	w/f	Rusticans	
S2		9.8	9.8	58.7
bk		10.1	10.1	58.4
y			10.6	57.9
b			11.2	57.3
y			12.2	56.3
bk			12.9	55.6
N2			13.7	54.8
	75'	w/f	Rusticans	
N2			12.7	55.8
bk			11.8	56.7
y			11.1	57.4
b			10.1	58.4
y			8.8	59.7
bk			7.7	60.8
S2			7.1	61.4

685-4

	100'	w/f	Rusticans	
S2			6.1	62.4
bk			6.6	61.9
y			8.1	60.4
b			9.4	59.1
y			9.8	58.7
bk			9.9	58.6
N2			9.6	58.9
	125'	w/f	Rusticans	
N2			8.1	60.4
bk			7.9	60.6
y			8.2	60.3
b			7.9	60.6
y			7.6	60.9
bk			7.1	61.5
S2			6.8	61.7

685-4

	150	W of	Ruscarons	
SL			5-1	63.4
"			5-6	62.9
"			5-7	62.8
"			6.6	61.9
"			7.5-	61.0
"			7.9	60.6
ms			8.1	60.4
	200'	W of	Ruscarons	
ms			4.9	63.6
"			4.4	64.1
"			4.1	64.4
"			3.9	64.6
"			3.8	64.7
"			3.5-	65.0
SL			2.9	65.6

685-4

James

	250	W of	Ruscarons	2?
SL			1.2-	67.3
"			1.5-	67.0
"			1.6-	66.9
"			1.9	66.6
"			2.0	66.5-
"			2.4	66.1
ms			2.2	66.3
TP	5.28	73.1.0	0.72	67.82
	300'	W =	E line of Locust st (70)	
ms			5-3	67.8
"			4.2	68.5-
"			4.6	68.5-
"			3.5-	69.6
"			3.8	69.3
"			4.1	69.0
SL			3.6	69.5-

7310

W Line of Locust st

S2		33	69.6
4		34	69.7
4		39	69.2
6		43	68.8
4		47	68.4
4		50	68.1
N2		53	67.8

50' W of Locust st

N2		65	66.6
4		58	67.3
4		54	67.7
6		57	67.9
4		59	68.1
4		49	68.2
S2		49	68.2

7310

James

100 W of Locust st

S2		69	66.2
4		76	65.5
4		77	65.4
6		72	65.9
4		74	65.7
4		82	64.9
N2		90	64.1

150 W of Locust

N2		112	61.9
4		140	62.1
4		107	62.4
4		101	63.0
4		93	63.8
4		86	64.3
S2		84	64.7

7310

	200'	W of	Locust	
S2			10.5	62.6
bl			10.6	62.5
4			11.3	61.8
6			11.7	61.4
7			12.4	60.7
bl			12.7	60.4
N2			12.9	60.2
	250'	W of	Locust	
N2			12.2	60.5
bl			12.8	60.3
4			12.7	60.4
6			12.4	60.7
4			12.2	60.9
bl			11.7	61.4
S2			11.2	61.9

7310

James

	300'	W of	Elm St	Elm St Gr
S2			8.4	64.1
bl			9.2	63.9
4			9.2	63.8
6			10.1	63.0
7			10.6	62.5
bl			10.4	62.7
N2			10.4	62.7
		W of	Elm St	
N2			7.5	65.6
bl			7.5	65.6
4			7.3	65.8
6			6.8	66.3
7			6.1	67.0
bl			4.9	68.2
S2			3.8	69.3
TP	1011	7936	38.5	69.25

7936

	50'	w q	Elm	st
S2			8.3	71.1
ll			9.2	70.2
4			9.9	69.5
b			10.4	69.0
4			10.7	68.7
ll			10.8	68.6
N2			11.3	68.1
	10'	w q	Elm	st
N2			9.3	70.1
ll			9.2	70.2
4			8.7	70.7
b			8.1	71.3
4			7.2	72.2
ll			7.0	72.4
S2			6.9	72.5

7936

James 6

	150'	w q	Elm	st
S2			5.4	74.0
ll			5.3	74.1
4			5.2	74.2
b			6.1	73.3
4			6.7	72.7
ll			6.9	72.5
N2			6.9	72.5
	200'	w q	Elm	st
N2			4.4	75.0
ll			4.5	74.9
4			4.4	75.0
b			4.3	75.1
4			3.8	75.6
ll			3.5	75.9
S2			3.9	75.5

7936

	>62'	W =	Pueblo Sur or Platte
SL		3.0	76.4
bh		3.2	76.2
y		3.7	75.7
b		3.7	75.7
y		4.0	75.4
bh		4.1	75.3
nL		4.2	75.2

POSTED

Clough Colbert Wardi

Cross section of Kingsley st (70') 77 ft

1/28 09

E Lin Tide St — Pueblo W Lin — BM SE Stoffle

380 — 694 — 314

E Lin of Tide St

N 2	8.4	-1.5
b	8.5	-1.6
4	8.2	-1.7
b	8.4	-1.8
7	8.6	-1.7
b	8.6	-1.7
S 2	8.5	-1.6

Plotted

35' W of Tide St

S 2	8.1	-1.2
b	8.2	-1.3
4	8.1	-1.2
b	8.1	-1.2
4	8.1	-1.2
b	8.1	-1.2
N 2	8.1	-1.2

POSTED

694

Kingsley 8

105' W of Tide St

N 2	7.7	-0.8
b	7.7	-0.8
7	7.7	-0.8
b	7.6	-0.7
4	7.2	-0.3
b	7.3	-0.4
S 2	7.4	-0.5

135' W of Tide St

S 2	7.1	-0.2
b	7.0	-0.1
4	7.0	-0.1
b	7.2	-0.3
4	7.2	-0.3
b	7.0	-0.1
N 2	6.9	00

6.84

	200' W of	Tide at	
N2		6.2	0.7
4h		6.1	0.8
4		6.1	0.8
6		6.3	0.5
4		5.7	1.2
4h		5.7	1.2
S2		6.0	0.9
	250' W of	Tide at	
S2		5.2	1.7
4h		5.2	1.7
4		5.2	1.7
6		5.4	1.5
4		5.5	1.4
4h		5.6	1.3
N2		5.4	1.5

6.94 Kingsley

9

	300' W =	℄ Line of Shafter St (70')	
N2		4.1	2.8
4h		4.0	2.9
4		3.6	3.3
6		3.8	3.1
4		3.8	3.1
4h		3.8	3.1
S2		3.8	3.1
	W Line of	Shafter St.	
S2		1.2	5.7
4h		1.6	5.3
4		1.5	5.4
6		1.6	5.3
4		1.5	5.4
4h		1.7	5.2
N2		1.9	5.0
TP	11.84	18.60	0.2	5.7

1860

50' W of Shaft 2

N 2	11.7	6.9
4	11.5	7.1
7	11.7	6.9
6	11.2	7.4
7	11.0	7.6
4	11.2	7.4
S 2	10.8	7.8

100' W of Shaft

S 2	8.1	10.5
4	8.9	9.7
7	9.2	9.4
6	9.4	9.2
7	9.5	9.1
4	10.0	8.6
N 2	10.2	8.4

1860 Kingsley

10

150' W of Shaft

N 2	8.7	9.9
4	8.7	9.9
7	8.3	10.3
6	7.3	11.3
4	6.7	11.9
4	6.2	12.4
S 2	5.9	12.7

200' W of Shaft

S 2	4.2	14.4
4	4.9	13.7
7	5.4	13.2
6	6.0	12.6
7	6.6	12.0
4	6.8	11.9
N 2	6.8	11.8

1860

	250'	W of	Shaft	
N2			5,2	13.4
4			5,1	13.5
4			5,2	13.4
4			4,3	14.3
4			3,1	15.5
4			2,2	16.4
S2			1,6	17.0
	300'	W of E Line of	Scott 2nd	P.C.
S2			3,2	15.4
4			3,4	15.2
4			3,6	15.0
4			3,7	14.9
4			3,9	14.7
4			4,0	14.6
N2			4,2	14.4

1860

		W Line of	Scott	
N2			0.5	18.1
4			0.7	17.9
4			1,0	17.6
4			1,2	17.4
4			1,5	17.1
4			1,6	17.0
S2			1,6	17.0
TP	1215	3073	00	18.58
	50' W Scott St			
S2		3073	9.8	20.9
2			9.6	21.1
4			9.2	21.5
4			9.0	21.7
4			9.2	21.5
2			9.3	21.4
N2			9.6	21.1

30.73

100 W. Scott St.

N.		7.5	23.2
C		6.8	23.9
¼		6.5	24.2
½		6.2	24.5
¾		5.7	25.0
S.		5.3	25.4
		5.0	25.7

150 W. Scott St.

S.		0.2	30.5
C		0.7	30.0
¼		1.3	29.4
½		2.0	28.7
¾		2.4	28.3
N.		2.9	27.8
		3.5	27.2
T.P.	12.22	42.93	0.02 30.71

42.93

200 W. Scott St.

N.		8.7	34.2
C		8.3	34.6
¼		7.7	35.2
½		7.4	35.8
¾		6.7	36.2
S.		6.4	36.5
		6.2	36.7

250 W. Scott St.

S.		0.2	41.7
C		1.0	41.9
¼		0.6	42.3
½		0.6	42.3
¾		0.8	42.1
N.		1.0	41.9
		1.3	41.6
T.P.	7.92	50.32	0.53 42.40

50.32

(400')
Graded

300' W. Scott = E. Pasecrans

N.		
c	4.4	45.9
4	4.5	46.8
2	4.9	45.4
4	6.2	44.1
c	6.5	43.8
St	6.3	44.0
	6.4	43.9

W. Kina Pasecrans St

St	4.0	46.3
c	4.2	46.1
4	4.5	45.8
2	4.6	45.7
4	4.8	45.5
c	3.0	47.3
N.	1.4	48.9

50.32

Kingsley

50' W. Pasecrans St

N.	2.77	47.55
c	4.6	45.7
4	6.7	43.6
2	9.8	40.5
4	12.6	37.7
c	14.2	36.1
St	15.3	35.0

100' W. Pasecrans St

St	15.0	35.3
c	15.6	34.7
4	13.4	36.9
2	10.4	39.9
4	7.5	42.8
c	5.6	44.7
N.	4.3	46.0

50.32

150' W. Pasadena

NL	7.0	43.3
C	9.0	41.3
4	11.4	38.9
4	13.4	36.9
4	11.8	38.5
C	10.8	39.5
SL	9.1	40.9

200 W. Pasadena St

SL	3.0	47.3
C	4.2	46.1
4	6.2	44.1
4	9.2	41.1
4	11.1	39.2
C	10.0	40.3
NL	7.8	42.5

50.32

Kingsley

250' W. Pasadena St

NL	7.0	43.3
C	9.0	41.3
4	8.2	42.1
4	5.3	45.0
4	3.7	46.6
C	2.5	47.8
SL	1.7	48.6

300' W. Pasadena-E/ locust.

SL	1.6	~~38.7~~ 48.7
C	2.6	47.7
4	4.2	46.1
4	6.3	44.0
4	7.1	43.2
C	7.0	43.3
NL	5.5	44.8
+R	12.90	61.59 1.63 48.69

6/1.59

W line Locust St

NL	12.9	48.7
C	11.9	49.7
¼	10.9	49.7
℄	10.4	51.2
¼	11.0	50.6
C	12.0	49.6
SL	12.6	49.0

50' W Locust St

SL	9.7	51.9
C	8.6	53.0
¼	7.6	53.8
℄	7.8	53.8
¼	8.5	53.1
C	9.0	52.6
NL	9.6	52.0

6/1.59

100 W Locust St

NL	57	55.9
C	5.5	56.1
¼	5.8	55.8
℄	6.2	55.4
¼	6.7	54.9
C	7.1	54.5
SL	7.6	54.0

150' W Locust St

SL	50	56.6
C	4.8	56.8
¼	4.5	57.1
℄	4.8	56.8
¼	4.8	56.8
C	5.0	56.6
NL	5.8	55.8

61.59

200' W Locust St

N		1.3	57.3
C		3.9	57.7
¼		3.8	57.8
½		3.6	58.0
¼		3.5	58.1
C		3.4	58.2
S		3.3	58.3

250' W Locust St

S		1.8	59.8
C		1.9	59.7
¼		1.9	59.7
½		2.0	59.6
¼		2.1	59.2
C		2.5	59.1
N		2.9	58.7
T.R	13.04	73.48	1.15	60.44

73.48

Kingsley

300' W Locust & E. Elm St

N	1.30	60.15
C	1.26	60.9
¼	1.27	60.8
½	1.23	61.2
¼	1.22	61.3
C	1.29	60.8
S	1.20	61.6

W. Line Elm St

S	9.10	64.38
C	9.1	64.1
¼	9.3	64.2
½	9.0	64.5
¼	8.6	64.9
C	8.6	64.9
N	8.6	64.9

7348

50' W. Elm St

N	7.3	66.2
c	6.7	66.8
¼	6.4	67.1
d	6.4	67.1
¼	6.3	67.2
c	6.3	67.2
S	6.1	67.1

100' W. Elm St

S	3.9	69.6
c	3.6	69.9
¼	3.4	70.1
d	3.5	70.0
¼	4.5	69.0
c	5.2	68.3
N	5.8	67.7

7348 Kingsley

150' W Elm St

N	4.0	69.5
c	3.4	70.1
¼	3.4	70.1
d	3.1	70.4
¼	3.1	70.4
c	2.6	70.9
S	2.3	71.2

200' W Elm St

S	2.1	71.4
c	2.3	71.2
¼	2.1	71.4
d	2.0	71.5
¼	2.3	71.2
c	2.8	70.7
N	3.0	70.5

7378

Pavilion

263 W. Elm = W.L. Roseville

W.L.		1.8	71.7
C		1.5	72.0
¼		1.5	72.0
½		1.4	72.1
¾		1.4	72.1
C		1.4	72.1
S.L.		1.02	73.7

Pavilion as platted.

POSTED

Eb.

Bb.

X Section of Meredith from W.L. Shafter St to E. Line of Elm St

B.M.	0.84	14.96		14.12 W.M. 406 Meredith & Scott

W. Line Shafter St

S.L.	14.96	18.0	-3.0
C		18.0	-3.0
¼		18.2	-3.2
½		18.3	-3.3
¾		18.3	-3.3
C		18.5	-3.5
W.L.		18.6	-3.6

Plotted

POSTED

50' W. Shafter St

W.L.	18.0	-3.0
C	18.0	-3.0
¼	17.9	-2.9
½	17.8	-2.8
¾	17.7	-2.7
C	17.7	-2.7
S.L.	17.6	-2.6
	17.6	-2.6

14.96

100' W. Shafter St

S/	15.5	-0.8
C	15.8	-0.8
¼	16.0	-1.0
¢	16.3	-1.3
¾	16.7	-1.7
C	16.2	-1.2
N/	17.0	-2.0

150' W. Shafter St

N/	8.1	6.9
C	7.7	7.3
¼	7.9	7.1
¢	7.9	7.1
¾	7.0	8.0
C	6.5	8.5
S/	6.6	8.4

14.96 Meredith

200' W. Shafter St

S/	24	12.6
C	24	12.6
¼	2.6	12.4
¢	24	12.6
¾	24	12.6
C	24	12.6
N/	23	12.7

250' W. Shafter St

N/	1.0	14.0
C	0.8	14.2
¼	0.8	14.2
¢	1.0	14.0
¾	0.9	14.1
C	0.8	14.2
S/	0.9	14.1

1.4.96

300' W. Shaffer - E. Scott St.

S.		0.9	14.1
C		0.9	14.1
¼		0.9	14.1
¢		0.9	14.1
¼		0.8	14.2
C		0.8	14.2
N.		0.8	14.2
T.P.	10.04 24.15	0.85	14.11

Wilma Scott St.

N.	24.15	9.4	14.7
C		9.6	14.5
¼		9.5	14.6
¢		9.4	14.7
¼		9.4	14.7
C		9.7	14.4
S.		9.4	14.7

24.15

Meredith

50' N. Scott St.

S.		8.9	15.8
C		8.6	15.5
¼		8.6	15.5
¢		8.7	15.4
¼		8.9	15.2
C		8.9	15.2
N.		8.8	15.3

100' N. Scott St.

N.		7.8	16.3
C		7.8	16.3
¼		7.7	16.4
¢		7.5	16.6
¼		7.4	16.7
C		7.3	16.8
S.		7.4	16.7

Meredith

24.15

150' W. Scott St

S.		5.0	19.1
C		4.9	19.2
¼		5.0	19.1
¢		5.3	18.8
¼		5.3	18.8
¢		5.5	18.6
N.		5.6	18.5

200' W. Scott St

N.		2.0	22.1
C		3.2	20.9
¼		3.0	21.1
¢		2.2	21.9
¼		1.5	22.6
C		2.2	21.9
S.		2.2	21.9
T.R	12.84	36.74	0.25 23.90

36.74

220' W. Scott St

S.	13.5	23.2
C	10.0	26.7
¼	9.2	27.5
¢	9.2	27.5
¼	9.5	27.2
C	13.4	23.0
N.	13.6	23.1

250' W. Scott St

N.	10.5	26.2
C	7.7	29.0
¼	5.9	30.8
¢	5.3	31.4
¼	5.1	31.6
C	6.6	30.7
S.	10.8	25.9

36.74 Graded (100')

300' W. Scott - E. Rosecrans St

N.	3.4	33.3
c	3.6	33.1
¼	3.8	32.9
c	4.0	32.7
¼	4.3	32.4
c	4.4	32.3
S.	4.3	32.4

W. Line Rosecrans St

S.	2.6	34.1
c	2.5	34.2
¼	2.2	34.5
c	2.2	34.5
¼	2.0	34.7
c	1.5	35.2
S.	1.7	
I.P. 12.57	49.31	6.0 36.74

49.31 Meredith

5' W. Rosecrans St

S.	7.1	42.2
c	7.4	41.9
¼	7.6	41.7
c	7.6	41.7
¼	7.6	41.7
c	8.3	41.0
N.	8.7	40.6

50' W. Rosecrans St

N.	3.1	46.2
c	2.9	46.4
¼	2.5	46.8
c	1.9	47.4
¼	1.5	47.8
c	1.5	47.8
S.	1.4	
12.84	60.72	1.43 47.88

60.72

100' W. Rosecrans St

S.		9.1	51.6
C		9.1	51.6
¼		9.0	51.7
½		9.0	51.7
¾		9.1	51.6
C		9.5	51.2
N.		9.6	51.1

150' W. Rosecrans St

N.		5.8	54.9
C		5.7	55.0
¼		5.6	55.1
½		6.0	54.7
¾		5.7	55.0
C		5.1	55.6
S.		5.0	55.7

60.72

Meredith

200' W. Rosecrans St

S.		2.9	57.8
C		2.6	58.1
¼		2.2	58.5
½		2.0	58.7
¾		2.0	58.7
C		2.4	58.3
N.		2.4	58.3
T.P.	9.10	69.46 0.36	60.36

250' W. Rosecrans St

N.	6946	7.8	61.7
C		7.9	61.6
¼		7.7	61.8
½		8.0	61.5
¾		7.9	61.2
C		8.1	61.1
S.		8.6	60.9

6946

300' W. Pescrams-E. Locust

S.	6.6	62.9
C	6.2	63.3
¼	5.6	63.9
C	5.3	64.2
¼	5.4	64.1
C	5.5	64.0
N.	5.0	64.5

W. Line Locust St

N.	2.9	66.6
C	3.1	66.4
¼	3.4	66.1
C	3.7	65.8
¼	4.0	65.5
C	4.7	64.8
S.	4.8	64.7

6946 Meredith

50' W. Locust St

S.	4.4	65.1
C	4.2	65.3
¼	3.9	65.6
C	3.5	66.0
¼	3.2	66.3
C	3.0	66.5
N.	2.8	66.7

100' W. Locust St

N.	2.3	67.2
C	2.4	67.1
¼	3.2	66.3
C	3.7	65.8
¼	3.8	65.7
C	3.8	65.7
S.	3.7	65.8

6.9.16

150' W. Locust St

S.		4.1	65.4
C		4.0	65.5
¼		3.2	66.3
℄		2.8	66.7
¼		3.8	65.7
C		3.6	65.9
N.		3.4	66.1

200' W. Locust St

N.		4.7	64.8
C		4.5	65.0
¼		4.6	64.9
℄		4.9	64.6
¼		5.9	63.6
C		5.1	64.4
S.		4.0	65.5
T.R.	1.13	5.29 5.30	64.16

6.5.29

250' W. Locust St

S.		1.2	64.1
C		5.2	60.1
¼		6.0	59.3
℄		6.0	59.3
¼		4.8	60.5
C		3.1	62.2
N.		4.5	60.8

210 W. Locust St

N.		20.0	45.3

220' W. Locust St

N.		29.0	42.3
C		11.4	53.9
¼ + 6'		11.5 22.0	53.8 53.3
℄		4.9	60.4
¼		3.5	61.8
C		2.5	62.8
S.		1.6	63.7

Meredith.

65.29

290' W. Locust St.

S.	2.1	63.2
C	2.8	62.5
¼	3.9	61.4
C	5.8	59.5
¼	21.8	42.5
C	22.5	42.8
N.	29.0	42.3

300' W. Locust = E. Elm St.

N.	2.0	63.3
C	14.6	50.7
¼	7.6	57.7
C	5.0	60.3
¼	3.7	61.6
C	2.4	62.9
S.	2.0	63.3

POSTED

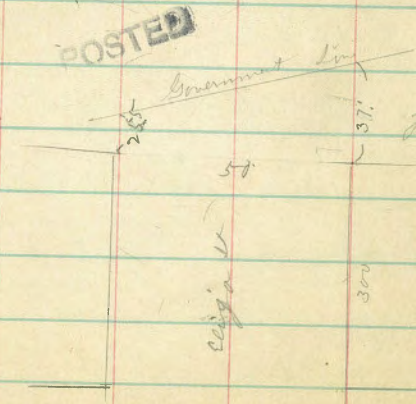
Cross section of San Elijo St (50')

Government Line to P.L. 17.6

12.38	47.40		35.10	BM Kellogg & San Dimas
11.81	59.02	0.19	47.71	
11.12	69.63	0.51	58.51	BM N Ely Kellogg & Elijo
12.49	82.12	0.0	69.63	
12.03	94.15	0.0	82.12	
		1.074	83.41	BM pnt SW for Kellogg & 70 Strands
11.75	105.80	0.10	94.05	
11.70	117.71	0.49	105.31	
		2.40	114.31	BM SE & Kellogg & Quail

Boreholes

POSTED



Oldsight Work Mar 3 09

San Elijo St

Government Line

7.67 16.18 58.51 BM Kellogg & Elijo

E 2	9.2	57.0
4	8.7	57.5
3	8.0	58.2
6	7.8	58.4
4	7.4	58.8
4	6.6	59.6
W 2	6.0	60.2

N line of Jenkins St 50'

W 2	5.7	60.5
4	6.3	59.9
4	6.8	59.4
4	7.4	58.8
3	8.0	58.2
4	8.6	57.6
E 2	9.2	57.0

POSTED

66.18

	35'	n of	Jenkins st	
EL			8.6	57.6
bh			8.4	57.8
y			7.9	58.3
b			7.4	58.8
y			6.8	59.4
bh			6.2	60.0
WL			5.7	60.5
	51	n of	Jenkins st	
WL			6.2	60.0
bh			6.7	59.5
y			7.2	59.0
b			8.0	58.2
y			8.4	57.8
bh			8.5	57.7
EL			14.0	52.2

66.18

Elwyn

	75'	n of	Jenkins st	
EL			17.4	48.8
bh			12.1	54.1
y			8.3	57.9
b			7.8	58.6
y			7.0	59.2
bh			6.4	59.6
WL			6.0	60.2
	90'	n of	Jenkins st	
WL			13.6	52.6
bh			14.2	52.0
y			14.7	51.5
b			11.7	54.5
y			13.2	53.0
bh			15.2	51.0
EL			16.8	49.4

6.6.18

100' n of Jenkins at

El	8.8	57.4
bl	14.0	52.2
y	14.7	51.5
b	14.8	51.4
y	15.0	51.2
bl	13.2	53.0
wh	11.7	54.5

125' n of Jenkins at

wh	6.6	59.6
bl	6.7	59.5
y	6.8	59.4
b	7.7	58.5
y	8.8	57.4
bl	9.0	57.2
El	9.7	56.5

6.6.18

150' n of Jenkins at

El	8.0	57.2
bl	8.2	58.0
y	7.7	58.5
b	7.3	58.9
y	6.8	59.4
bl	6.4	60.0
wh	5.7	60.5

xxx n of Jenkins at

wh	4.9	61.3
bl	5.2	61.0
y	5.8	60.4
b	6.1	60.1
y	6.6	59.6
bl	7.1	59.1
El	7.6	58.6

POSTED

6618

	250	ny	y st
E2		8,0	58.2
4		7,6	58.6
4		7,0	59.2
6		6,6	59.6
7		6,2	60.0
4		5,5	60.7
W2		5,3	60.9
	300	n = 3 d y Kellogg st (50)	
W2		4,5	61.7
4		5,3	60.9
7		5,7	60.5
1		6,5	59.7
7		7,0	59.2
4		7,8	58.4
E2		8,0	58.2

6618

Slb of Kellogg

E2	8,5	57.7
4	7,7	58.5
4	7,0	59.2
6	6,5	59.7
7	5,8	60.4
4	5,2	61.0
W2	4,5	61.7
	5'/4 of Kellogg	
W2	4,7	61,5
4	5,2	61.0
7	6,1	60.1
6	6,7	59.5
7	7,3	58.9
4	7,9	58.3
E2	8,7	57.9

66.18

Center of Kellogg

E2			8.5	57.7
bb			7.8	58.4
y			7.4	58.8
b			7.0	59.2
y			6.4	59.8
bb			5.9	60.3
W2			5.2	61.0

N 1/4 of Kellogg

W2			4.8	61.4
bb			5.4	60.8
y			6.1	60.1
b			6.4	59.8
y			7.0	59.2
bb			7.5	58.7
E2			8.4	57.8

1118

N bdr of Kellogg

E2			8.4	57.8
bb			7.6	58.6
y			7.2	59.0
b			6.6	59.6
y			6.2	60.0
bb			5.5	60.7
W2			5.0	61.2

N line of Kellogg

W2			5.2	61.0
bb			5.4	60.8
y			6.0	60.2
b			6.6	59.6
y			7.0	59.2
bb			7.6	58.6
E2			8.3	57.9
TP	6.55	6506	7.67	58.37

Eliza

6506

	50	n f	Kellogg	
E2			6,8	58.3
M			6,4	58.7
4			5,7	59.4
L			5,3	59.8
M			4,7	60.4
M			4,4	60.7
M2			3,8	61.3
	100	n f	Kellogg	
M2			4,2	60.9
M			4,8	60.3
4			5,3	59.8
L			6,3	58.8
4			6,6	58.5
M			7,0	58.1
E2			7,1	58.0

6506

Eliza

	150	n f	Kellogg	
E2			8,2	56.9
M			8,1	57.0
4			7,5	57.6
L			7,0	58.1
4			6,1	59.0
M			5,6	59.5
M2			5,3	59.8
	200	n f	Kellogg	
M2			4,4	60.7
M			5,0	60.1
4			5,7	59.4
L			6,3	58.8
4			7,2	57.9
M			7,7	57.4
E2			7,8	57.8

65-06

	250'	n of	Kelley ave	
E2			6.0	59.1
4			5.9	59.2
7			5.5	59.6
10			5.0	60.1
7			4.2	60.9
4			3.8	61.3
W2			3.4	61.7
	300'	n = SE/4 of	Lawrence st (50)	
W2			1.7	63.4
4			2.7	62.4
7			3.3	61.8
10			3.5	61.6
7			4.1	61.0
4			4.1	61.0
E2			4.6	60.5

65-06

Elwyn

32

	SEC	of	Lawrence st	
E2			4.9	60.7
4			4.2	60.9
7			3.8	61.3
10			3.2	61.9
7			2.7	62.4
4			2.2	62.9
W2			1.5	63.6
	S 1/4	of	Lawrence st	
W2			1.5	63.6
4			2.0	63.1
7			2.7	62.4
10			3.0	62.1
7			3.7	61.4
4			4.5	60.6
E2			5.0	60.1

POSTED

1506

Center of Laurence st

E1		5.4	59.7
tk		4.6	60.5
7		4.1	61.0
1		3.3	61.8
9		2.5	62.6
tk		2.3	62.8
W1		1.8	63.3

N ¼ of Laurence st

W1		1.8	63.3
tk		2.3	62.8
7		2.8	62.3
1		3.5	61.6
7		4.0	61.1
tk		4.5	60.6
E2		5.7	59.4

1505

2 tk of Laurence st

E1		3.8	59.3
tk		3.0	60.1
7		4.5	60.6
1		3.8	61.3
9		3.2	61.9
tk		2.4	62.7
W1		1.9	63.2

2 Line of Laurence st

W1		2.2	62.9
tk		2.9	62.2
7		3.2	61.9
1		4.0	61.1
7		4.5	60.6
tk		5.4	59.7
E1		5.8	59.3
TP	5.46 -	6.837	2.15	62.91

BM 2 W of Laurence

6837

	50'	n of	Lawrence st	
E2			9.1	59.3
bh			8.9	59.5
4			8.2	60.2
6			8.1	60.3
4			7.1	61.3
4			6.3	62.1
W2			5.0	63.4

	100'	n of	Lawrence st	
W2			5.0	63.4
bh			5.4	62.8
4			6.3	62.1
6			7.0	61.4
4			7.2	61.2
bh			7.9	60.5
E2			8.4	59.8

6837

	150'	n of	Lawrence st	
E2			8.0	60.4
bh			7.4	60.8
7			7.0	61.4
6			6.4	61.8
4			5.4	62.8
bh			4.8	63.6
W2			4.0	64.4

	200'	n of	Lawrence st	
W2			3.5	64.9
bh			4.5	63.9
7			5.0	63.4
6			6.0	62.4
7			6.6	61.8
bh			6.9	61.5
E2			7.5	60.9

POSTED

6837

	r 50'	n of	Lawrence St	
E2			6,0	62.4
bk			5,6	62.8
y			4,8	63.6
b			4,4	64.0
y			3,3	65.1
bk			2,3	66.1
W2			1,3	67.1
	300'	n = S Line of the ball (50')		
W2			0,6	67.8
bk			1,3	67.1
y			2,2	66.2
b			3,2	65.2
y			3,8	64.6
bk			4,5	63.9
E2			5,4	63.0
TP	11,10	7437	5,10	63,27

Bm SE mc

7437

Elijo

	S bk of the ball		
E2		11,2	63.2
bk		10,0	64.4
y		9,4	65.0
b		9,1	65.3
y		8,3	66.1
bk		7,5	66.9
W2		6,5	67.9
	S ¼ of the ball		
W2		6,1	68.3
bk		7,2	67.2
y		7,8	66.6
b		8,6	65.8
y		9,4	65.0
bk		10,4	64.0
E2		11,2	63.2

7437

Center of Mc ball

EL	11,3	63.1
bk	10,0	64.4
y	9,2	65.2
b	8,4	66.0
y	8,0	66.4
bk	7,1	67.3
WL	5,8	68.6

N 1/4 of Mc ball st

WL	5,7	68.7
bk	6,7	67.7
y	7,6	66.8
b	8,1	66.3
y	9,3	65.1
bk	10,2	63.8
EL	10,9	63.5

7437

Elijo

N bk of Mc ball

EL	10,4	64.0
bk	9,4	65.0
y	9,8	64.6
b	8,0	66.4
y	7,1	67.3
bk	6,6	67.8
WL	5,5	68.9

N. Sec of Mc ball st

WL	5,3	69.1
bk	7,4	67.0
y	8,8	65.6
b	8,0	66.4
y	8,6	65.8
bk	9,3	64.9
EL	10,3	63.9

7437

50' n of mc ball 2

E2		9.7	64.7
bk		9.1	65.3
4		8.3	66.1
2		7.3	67.1
4		6.3	68.1
bk		5.7	68.7
W2		4.6	69.8

100' n of mc ball

W2		4.5	69.9
bk		3.2	69.2
7		6.2	68.2
2		7.0	67.4
7		7.5	66.9
bk		8.7	65.7
E2		9.4	65.0

7437

150 n of mc ball

E2		9.2	65.2
bk		8.6	65.8
4		7.6	66.8
2		7.1	67.3
4		6.0	68.4
bk		5.0	69.4
W2		4.0	70.4

200' n of mc ball

W2		3.7	70.7
bk		4.4	70.0
4		4.7	69.7
2		5.3	69.1
4		5.7	68.7
bk		6.9	67.5
E2		7.8	66.6

Eliza

7437

250 N of Inc hall

E2			3,9	70.5
bk			3,5	70.9
4			2,6	71.8
6			1,5	72.9
7			0,4	74.0
TP	12,40	86.76	0,1	74.56
bk			11,8	75.0
W2			10,8	76.0

300 N = S dim of Nichols st (50) Bm Sur to Nichols

W2			9,4	77.4
bk			10,3	76.5
2			10,6	76.2
4			11,2	75.6
4			11,9	74.9
bk			13,2	73.6
E2			13,8	73.0

8676

Elev 0

S bk of Nichols st

E2			13,3	73.5
bk			12,8	74.0
4			11,9	74.9
6			11,0	75.8
7			10,4	76.4
bk			9,9	76.9
W2			8,8	78.0

S ¼ of Nichols

W2			8,5	78.3
bk			9,3	77.5
2			10,0	76.8
6			10,2	76.2
4			11,5	75.3
bk			12,2	74.6
E2			12,9	73.9

8676

Center of Nichols

E2		12.6	74.2
bb		12.0	74.8
y		11.3	75.5
b		10.4	76.4
y		8.6	77.2
bl		8.8	78.0
W2		8.0	78.8

N ¼ of Nichols st

W2		7.7	79.1
bl		8.8	78.0
y		9.3	77.5
b		10.1	76.7
y		10.8	76.0
bl		11.7	75.1
E2		12.2	74.6

8676

N bb of Nichols st

E2		12.0	74.8
bl		11.3	75.5
y		10.6	76.2
b		9.9	76.9
y		9.1	77.7
bl		8.0	78.8
W2		7.2	79.5

N line of Nichols st

W2		6.8	80.0
bl		7.8	79.0
y		8.3	78.5
b		8.9	77.9
y		9.6	77.2
bl		10.4	76.4
E2		11.4	75.4

Elev 0

POSTED

86.76

	50'	n of	Nichols	
E2			8.8	78.0
bk			8.3	78.5
4			7.6	79.2
L			6.9	79.9
4			6.0	80.8
bk			4.9	81.9
W2			4.3	82.5
	100'	n of	Nichols	
W2			1.3-	85.3
bk			2.5-	84.3
4			3.5-	83.3
L			4.4	82.4
4			5.1	81.7
bk			6.2	80.6
E2			6.9	79.9

86.76

	150'	n of	Nichols	
E2			4.7	82.4
bk			4.0	82.8
4			3.2	83.6
TP	12.06	98.04	0.78	85.98
L			12.5	85.5
4			11.7	86.3
bk			11.0	87.0
W2			9.9	88.1
	200'	n of	Nichols	
W2			8.1	89.9
bk			9.4	88.6
4			9.9	88.1
L			10.5-	87.5
4			11.0	87.0
bk			11.9	86.1
E2			12.5	85.5

98.04

	2 50'	2 ½	Metals	at
E2			3.6	94.4
bb			3.0	95.0
y			2.6	95.4
b			2.2	95.8
y			2.4	95.6
bb			2.2	95.8
W2			2.5	95.5
TP	85-5	106.39	0.20	97.84

300 N = 5 Stns y Owens at 5-0 Bm SW to Owens

W2			2.79	103.60
bb			3.0	103.4
y			3.1	103.3
b			3.6	102.8
y			4.2	102.2
bb			5.2	101.2
E2			6.2	100.2

106.39

S bb y Owens

E2	6.3	100.1
bb	5.0	101.4
y	3.8	102.6
b	3.0	103.4
y	2.3	104.1
bb	1.7	104.7
W2	1.4	105.0

S ¼ y Owens

W2	0.2	106.2
bb	1.0	105.4
y	1.4	104.6
b	2.8	103.6
y	3.7	102.7
bb	5.4	101.0
E2	6.8	99.5

POSTED

10639

Center of Avenue

E2		84	98.0
bl		5-6	100.8
y		3.8	102.6
l		2.8	103.4
y		2.0	104.0
bl		1.0	105.4
W2		0.0	106.4

N ¼ of Avenue

W2		0.0	106.4
bl		1.1	105.3
y		2.1	104.3
l		3.1	103.3
y		4.7	101.7
bl		7.0	99.4
E2		9.7	96.5

10639

N bl of Avenue

E2		12.5	93.9
bl		2.0	97.4
y		6.6	99.8
l		5.4	101.0
y		4.3	102.1
bl		2.6	103.8
W2		+2.0	108.4

N Line of Avenue

W2		0.9	105.5
bl		4.0	102.4
y		7.4	99.2
l		9.4	96.6
y		11.8	94.6
TP	0.53	94.85	12.07 94.32
bl			3.8 91.1
E2			7.0 87.9

94.85

	25'	n of	Arrows	
E2			14.0	80.9
bl			12.3	82.6
y			10.3	84.6
l			6.8	88.1
y			3.0	91.9
bl			0.0	94.9
W2			+4.0	98.9
	50	n of	Arrows	
W2			3.8	91.1
bl			7.3	87.6
y			9.4	85.5
l			12.4	82.5
TP	4.74	87.30	12.29	82.56
y			7.3	80.0
bl			9.8	77.5
E2			11.0	76.3

87.30

Edge

	85'	n of	Arrows	
E2			13.8	73.5
	100'	n of	Arrows	
E2			9.0	78.3
bl			12.0	75.3
y			11.0	76.3
l			8.0	79.3
y			6.8	80.5
bl			6.0	81.3
W2			5.2	82.1
	125'	n of	Arrows	
W2			8.6	79.7
bl			8.8	78.5
y			8.4	78.9
l			8.1	79.2
y			6.8	80.5
bl			6.3	81.0
E2			6.2	81.1

87.30

	150'	n of	Owens at	
E2			+0.0	87.5
bk			1.8	85.5
4			2.7	84.6
b			3.0	84.3
4			2.9	84.4
bk			3.1	84.2
W2			3.2	84.1
TP	11.83	99.13	0.0	87.30
	200'	n of	Owens	
W2			7.7	91.4
bk			4.7	94.4
4			1.7	97.4
b			0.0	99.1
TP	11.68	110.66	0.15	98.98
4			9.8	100.9
bk			7.0	103.7
E2			7.4	103.3

110.66

	225'	n of	Owens at	
W2			13.0	97.7
bk			9.4	101.3
4			6.0	104.7
b			3.0	107.7
4			0.0	110.7
	250'	n of	Owens at	
W2			5.0	105.7
bk			0.5	110.2
TP	12.32	122.71	0.7	110.39
	225'	n of	Owens at	
E2			7.5	115.2
bk			6.3	116.4 ✓
	250'	n of	Owens	
W 4			10.0	112.7
b			1.4	121.3
	275'	n of	Owens	
W-Sne			14.0	108.7 ✓
bk			10.0	112.7 ✓
4			6.0	116.7 ✓
b			0.0	122.7 ✓

Elev

POSTED

122.71

	300'	n = S line of Perry (50)			✓
W 2			6,6	116.1	✓
b			3,7	119.0	✓
TP	1286	1357	0,36	122,35	
	250	n of	Owens		
E 2			10.1	125.1	✓
b			10,5	124.7	✓
4			11,0	124.2	✓
	275'	n of	Owens		
E 2			5.0	130.2	✓
b			5,3	129.9	✓
4			8.5	126.7	✓
	300' n = S line of Perry				
W 1/4			9,0	126.2	✓
b			4,5	130.7	✓
E 1/4			1,0	134.2	✓

1352'

Elijo

	S bk of Perry			
W 2			15.0	120.2
b			13,7	121.5
4			9,4	125.8
b			5,0	130.2
4			1,7	133.5
	S 1/4 of	Perry		
W 2			12,0	128.2
b			13,0	122.2
4			9,0	126.2
b			4,3	130.9
4			0,3	134.9
	Center of	Perry		
W 2			9,3	125.9
b			11,5	124.0
4			9,0	126.2
b			4,8	130.4
4			1,0	134.2

135-21

	N ¼ of		Perry		
WL			6,9	128.3	
bb			7,6	127.6	
4			7,0	128.2	
6			4,0	131.2	
7			0,8	134.4	
	N bb of		Perry		
WL			4,2	131.0	
bb			4,2	131.0	
4			3,0	130.2	
6			2,8	132.4	
7			+0,4	135.6	
	N Sec of		Perry		
WL			+0,4	135.6	
bb			0,6	134.6	
4			3,2	132.0	
6			1,2	134.0	
TP	12,31	147,29	0,23	134,98	
			11,2	136,07	BM SE Zinc Perry

147,29

Elijo

	300 N ± Sd	Perry		
E2		11,2	136.1	✓
bb		11,8	135.5	✓
	S bb of	Perry		
E2		9,8	137.5	
bb		10,0	137.3	
	S ¼ of	Perry		
E2		9,0	138.3	
11		9,8	137.5	
	Center of	Perry		
E2		8,4	138.9	✓
bb		9,5	137.8	✓
	N ¼ of	Perry		
E2		7,9	139.4	
bb		8,0	138.3	
	N bb			POSTED
E2		7,2	140.1	
bb		9,0	138.3	
		11,8	135.5	

14729

	n Line of	Perry		
E2		6.7	140.6	
b		7.6	139.5	
4		10.8	136.5	
	50' n of	Perry		
E2		2.5	144.8	
b		3.4	143.7	
4		3.5	143.8	
b		2.8	144.5	
4		2.5	144.8	
b		1.8	145.5	
W2		1.2	146.1	
TP	12274	15896	1.17	14622

W 50

15896

Elizo

	100'	n of	Perry	
W2			8.4	150.6
b			9.2	149.8
4			9.5	149.5
b			9.9	149.1
4			10.3	148.7
b			10.3	148.7
E2			9.9	149.1
	150	n of	Perry	
E2			3.6	155.4
b			3.0	154.0
4			4.6	154.4
b			3.0	154.0
4			3.9	153.1
b			3.9	153.1
W2			3.7	153.8

15896

	200'	n-f	Perry	
WL			27	156.8
bl			32	155.8
y			39	155.1
b			44	154.6
y			57	153.3
bl			50	154.0
EL			63	152.7
	250'	n-f	Perry	
EL			41	154.9
bl			34	155.6
y			28	156.2
b			21	156.9
y			20	157.0
bl			14	157.6
TP	12,50	17037	11,2	157.84
WL			11,7	158.6

17034

Elvyn

	300'	n = 5d f. Quantrough (50)	
WL		92	161.1
bl		99	160.4
y		101	160.2
b		100	160.3
y		104	159.9
bl		110	159.3
EL		122	158.1
	5 bl f. Quantrough		
EL		11,6	158.7
bl		103	160.0
y		95	160.8
b		90	161.3
y		95	160.8
bl		95	160.8
WL		84	161.9

17034

S ¼ of Quantrough

WL	7,7	162.6
BL	9,0	161.3
4	9,1	161.2
L	8,7	161.6
4	9,5	160.8
M	10,1	169.2
EL	11,4	158.9

Center of Quantrough

EL	11,1	159.2
BL	10,0	160.3
4	9,3	161.0
L	8,5	161.8
4	8,6	161.7
BL	9,0	161.3
WL	7,8	162.5

17034 Elyza

N ¼ of Q

WL	6,7	163.6
BL	8,0	162.3
4	8,7	161.6
L	8,0	162.3
4	8,5	161.8
M	9,4	160.9
EL	11,0	159.3

N Bk of Quantrough

EL	10,7	159.6
BL	9,4	160.9
4	8,5	161.8
L	7,7	162.6
4	8,4	161.9
M	7,2	163.1
WL	6,1	164.2

17634

N Line of Quantonquit

BM near Quantonquit

WL	5,26	163.08	
bk	6,4	163.9	
"	7,8	162.5	
l	7,3	163.0	
"	7,4	162.9	
bk	8,5	161.8	
SL	10,1	160.2	

50' N of Quantonquit

SL	7,7	162.6
bk	6,5	163.8
"	5,7	164.6
l	3,0	165.3
"	4,4	165.9
bk	3,4	166.9
	1,8	168.5

17634

100' N of Quantonquit

WL	0,7	169.6
bk	3,0	168.3
"	4,0	166.3
b	5,1	165.2
"	6,0	164.3
bk	7,0	163.3
SL	8,0	162.3
TP	7,26	16258

150' N of 2

SL	9,0	160.9
bk	7,4	162.5
"	6,4	163.5
l	5,2	164.7
"	3,9	166.0
bk	2,4	167.5
WL	0,8	169.1

16989

	20'	n	Quantity	
W2			3,3	166.6
bb			4,5	165.4
y			5,6	164.3
b			6,8	163.1
y			8,2	161.7
bb			9,7	160.2
E2			11,8	158.1
	250	n	Quantity	
E2			13,7	156.2
bb			12,4	157.5
y			11,7	158.2
b			10,4	159.5
y			9,3	160.6
bb			8,2	161.7
W2			7,0	162.9
TR	161	160.18	11,2	158.57

160.18

Elijo

	30'	n = 5	Sin of	Rubberset
W2			5,0	155.2
bb			5,6	154.6
y			6,0	154.2
b			6,4	153.8
y			7,4	152.8
bb			8,0	152.2
E2			9,0	151.2
	17.66	177.4		165,08
	17.94	180.38	0,30	177.44
	11.91	201.71	0,58	189.80
	6,45	208.07	0,09	201,62

POSTED

Brought inside

Transection of San Fernando st (57)

3/3-07 S 24 Rodgers to Government Line

S Line of Rodgers st

20807 Page 57

E2		0.3	207.8
bk		0.0	208.1
y		+0.2	208.3
b		+0.4	208.5
y		+0.6	208.7
bk		+0.3	208.4
W2		+0.4	208.5

50' S of Rodgers

W2		5.6	202.5
bk		6.2	201.9
y		6.5	201.6
b		6.6	201.5
y		6.5	201.6
bk		6.2	201.9
E2		5.9	202.2

POSTED

20807

San Fernando

100' S of Rodgers

E2		10.8	197.3
bk		10.9	197.2
y		11.0	197.1
b		11.0	197.1
y		11.2	196.9
bk		12.0	196.1
W2		12.5	195.6

150' S of Rodgers

W2		14.7	193.4
bk		10.3	194.8
y		13.0	195.1
b		12.7	195.4
y		12.4	195.7
bk		12.2	195.9
E2		11.6	196.5

POSTED

208.07

175' S of Rodgers

E2	7.4	200.7
tk	8.2	199.9
y	9.4	198.7
b	9.8	198.3
y	10.3	197.8
tk	11.3	196.6
WL	13.3	194.8

200 S of Rodgers

WL	12.2	195.9
tk	10.1	198.0
y	8.6	199.5
b	7.2	200.9
y	6.0	202.1
tk	4.3	203.8
E2	3.3	204.8

208.07

250' S of Rodgers

E2	3.3	204.8
tk	4.6	203.5
y	6.0	202.1
b	7.2	200.9
y	8.6	199.5
tk	10.5	197.6
WL	12.7	194.4

300' S = n line of Quantrough

BM n w M

TrWL	7.87	206.62	8.32	198.75 Quantrough
tk			5.8	200.7
y			4.2	202.4
b			3.4	203.2
y			2.0	204.6
tk			1.6	205.0
E2			1.0	205.6

20662

North of Quantrill

E2	1,2	205.4
bk	1,3	205.3
4	1,8	204.8
6	2,9	203.7
4	3,8	202.8
bk	4,8	201.8
W2	7,9	98.7

N 1/4 of Quantrill

W2	7,3	199.3
bk	5,1	201.5
4	4,0	202.6
6	3,0	203.6
4	2,1	204.5
bk	1,6	205.0
E2	1,5	205.1

20662

South of Quantrill

E2	2,3	204.3
bk	2,1	204.5
4	2,3	204.3
6	2,8	203.8
4	3,5	203.1
bk	4,2	202.4
W2	6,4	200.2

S 1/4 of 2

W2	7,0	199.6
bk	5,3	201.3
4	4,4	202.2
6	3,8	202.8
4	2,4	203.2
bk	2,0	203.6
E2	2,2	203.4

20662

	S bb y	Quantrayt	
E2		4,2	202.4
bb		4,0	202.6
y		4,1	202.5
b		4,2	202.4
y		3,0	201.6
M		6.0	200.6
W2		8,0	198.6
	S Lin 11	2	
W2		9,6	197.0
bb		7,8	198.8
y		6,9	199.7
b		6,1	200.5
y		5,7	200.9
M		5,6	201.0
E2		5,8	200.8

206.62

	30°	S y	Quantrayt	
E2			12,0	194.6
bb			12,3	194.3
y			12,4	194.0
b			12,7	193.9
TP	0,38	1944	12,54	194.08
y			0,4	193.9
bb			2,0	192.5
W2			5,8	188.7
	75°	S y	Quantrayt	
W2			8,5	186.0
M			6,4	188.1
y			6,4	188.1
b			7,0	187.5
y			6,4	188.1
M			5,6	188.9
E2			4,8	189.7

Zeinander

19446

	161'	Sof	Quantity	
E2			11,4	183.1
bh			12,7	181.8
TP	0,39	181,96	12,89	181,57
4			2,0	180.0
b			2,5	179.5
4			5,4	176.6
bh			6,0	176.0
W2			8,5	173.5
	125'	Sof	Quantity	
E2			9,3	172.7
bh			12,0	170.0
TP	0.68	170.09	12,53	69.47
4			5,0	165.1
b			8,5	161.6
4			10,9	159.2
bh			12,7	157.4
TP	1,30	15-983	11,76	158,20
W2			12,4	144.4

15-983

	150'	Sof	Quantity	
W2			2,4	157.4
bh			7,0	150.8
4			13,2	146.6
b			21,4	138.4
4			11,0	148.8
bh			8,4	151.4
E2			2,6	157.2
	190'	Sof	Quantity	
E2			28,0	131.8
bh			22,5	137.3
4			17,0	142.8
b			9,2	150.6
4			1,0	159.8
	200'	Sof	Quantity	
E2			21,0	138.8
bh			17,0	142.8
4			10,5	149.3
			3,5	156.5

15983

	225'	S of	Quantrough	
E2			11,4	148.4'
bk			5,1	154.7
TP	12,29	170.62	1,50	158.33
	190'	S of	Quantrough	
W bk			4,2	166.4
	200'	S of	Quantrough	
W 1/4			5,0	165.6
	225'	S of	Quantrough	
E 1/4			10,7	159.9
b			7,0	163.6
W 1/4			2,0	169.6
	250'	S of	Quantrough	
E2			7,9	162.7'
bk			2,0	168.6
TP	12,95	18357	0,0	170.62
	190'	S of	Quantrough	
W2			5,0	178.6'

18357

Forward

57

	200'	S of	Quantrough	
W2			5,0	178.6'
bk			9,5	174.1
	225'	S of	Quantrough	
W2			7,2	176.4'
bk			11,2	172.4
	250'	S of	Quantrough	
E 1/4			11,0	172.6
b			6,5	177.1
W 1/4			2,4	181.2
	275'	S of	Quantrough	
E2			12,2	171.4'
bk			8,4	175.2
7			4,3	179.3
b			1,6	182.0
TP	3,84	187,21	0,20	183,37

POSTED

1874

250' S of Quantrop

WL		0.3	186.9
bl		3.8	183.4

275 S of Quantrop

WL		0.9	186.3
bl		1.4	185.8
4		3.0	184.2

300' S = WL of Perry st (SE)

BM NW Perry

WL		2.45	184.76
bl		3.1	184.1
4		3.8	183.4
b		4.6	182.6
4		5.8	181.4
M		7.8	179.4
EL		9.8	177.3

1874

N bl of Perry st

EL		10.2	177.0
bl		8.7	178.5
4		7.3	179.9
b		6.2	181.0
4		4.6	182.6
bl		4.4	182.8
WL		3.6	183.6

N 4 of Perry

WL		5.0	182.2
bl		5.3	181.9
4		5.8	181.4
1		6.8	180.4
4		7.8	179.4
bl		9.0	178.2
EL		10.4	176.8

Leonard

1872

Center of Pump

E2		11.1	176.1
bl		9.3	177.9
y		8.1	179.1
l		7.4	179.8
y		6.7	180.5
bl		6.4	180.8
W2		6.1	181.1

S 1/4 of Pump st

W2		7.6	179.6
bl		8.0	179.2
y		8.0	179.2
l		8.6	178.6
y		9.6	177.6
bl		10.7	176.5
E2		12.1	175.1

1872

S bl of Pump st

E2		13.0	174.2
bl		11.9	175.3
y		11.3	175.9
l		10.1	177.1
y		9.6	177.6
bl		10.0	177.2
W2		9.6	177.6
TP	0.79	175.48	12.52	174.69

S Sim of Pump st

W2		22	173.3
bl		22	173.3
y		1.7	173.8
l		1.7	173.8
y		1.7	173.8
bl		2.3	173.2
E2		4.1	171.4
TP	0.09	162.96	12.61	162.87

162.96

50' S of Perry st

WL			13.6	149.4 ✓
bh			13.7	149.3
4			13.0	150.0
b			13.0	150.0
4			13.0	150.0
bh			12.4	150.6
E2			12.6	150.4 ✓
TP	4.10	154.74	12.32	150.64

65' S of Perry st

E2			13.8	140.9 ✓
bh			13.5	141.2
4			14.7	140.0
b			15.3	139.4
4			14.8	139.9
bh			14.0	140.7
WL			17.3	132.4 ✓

154.74

85' S of Perry st

E2			26.4	128.3 ✓
bh			24.2	130.5

100' S of Perry st

E2			22.8	131.9 ✓
bh			16.8	137.9
bh			11.6	143.1
b			6.7	147.8
4			3.5	151.2
bh			0.0	154.7
WL			1.9	152.8 ✓
TP	5.54	158.78	0.50	154.24

125' S of Perry st

WL			4.0	160.8 ✓
bh			0.8	~~160.6~~ 159.0
4			2.0	~~160.8~~ 157.8
b			3.2	~~163.0~~ 155.6
4			4.6	~~164.4~~ 155.2
bh			7.4	~~167.2~~ ~~165~~ 152.4
E2			18.7	~~170.5~~ 149.1 ✓

15.9.78

	150'	S of	Perry st	
EL			6,2	153.6 ✓
bk			4,8	155.0
y			4,0	155.8
b			3,0	156.8
y			2,3	157.5
bk			1,8	158.0
WL			0,7	159.1 ✓

	175'	S of	Perry st	
WL			3,8	156.0 ✓
bk			4,8	155.0
y			5,5	154.3
b			6,3	153.5
y			6,6	153.2
bk			6,9	152.9
EL			9,0	150.8 ✓

15.9.78

	200'	S of	Perry st	
EL			12,0	147.8 ✓
bk			10,5	149.3
y			9,7	150.1
b			9,2	150.6
y			7,8	152.0
bk			7,2	152.6
WL			5,2	154.2 ✓

	225'	S of	Perry st	
WL			8,2	151.5 ✓
bk			11,7	148.1
TP	0,19	147,58	12,39	147.39
y			14	146.2
b			35	144.1
y			37	143.9
bk			31	144.5
EL			31	144.5 ✓

14758

250' S of Perry

EL	12,6	135.0	✓
bb	12,0	135.6	
4	11,0	136.6	
b	7,3	140.3	
4	4,0	143.6	
bb	0,0	147.6	
WL	+3,0	150.6	✓

275' S of Perry

WL	+1,0	148.6	✓
bb	1,8	145.8	
4	4,0	143.6	
b	6,8	140.8	
4	10,3	137.3	
bb	Bm's = n L of Owens (SP)		Bm nw 4 Owens
WL	0,90	146.68	✓
bb	6,5	141.1	
4	10,0	137.6	
b	12,0	135.6	

14758

1/4 bb of Owens

WL	1,3	146.3	✓
bb	6,5	141.1	
4	8,5	138.1	
b	12,0	135.6	

1/4 of Owens

WL	2,2	145.4	✓
bb	7,3	140.3	
4	10,7	136.9	
b	13,2	134.4	

Center of Owens

WL	3,7	143.9	✓
bb	6,4	141.2	
4	8,9	138.7	
b	13,0	134.6	

S 1/4 of Owens

WL	5,4	142.2	
bb	8,5	139.1	
4	11,2	136.4	
b	13,8	133.8	

14758

Sth of Owens

WR		6,6	141.0 ✓
bk		9,0	138.6
4		11,4	136.2
6		14,0	133.6

S ¼ of Owens

WR		9,1	138.5 ✓
bk		11,6	136.0
4		13,2	134.6
TP	333 13821	12,70	134.88

275' S of Perry

ER		8,7	129.5 ✓
bk		5,5	132.7

800' S of N ¼ of Owens

ER		11,2	128.0 ✓
bk		8,1	130.1
4		5,3	132.9

13821

Nbk of Owens

ER		10,8	127.4
bk		8,8	129.4
4		6,2	132.0

N ¼ of Owens

ER		11,2	127.0
bk		9,2	129.0
4		6,6	131.6

Center of Owens

ER		11,7	126.5
bk		9,8	128.4
4		7,7	130.5

S ¼ of Owens

ER		12,6	125.6
bk		10,2	127.9
4		8,2	130.0

13821

Sdw of Owens

EL		12.9	125.3
bk		10.7	127.5
y		8.6	129.6

Sdw of Owens N.

EL		13.3	124.9
bk		10.8	127.4
y		8.4	129.8
b		5.4	132.8

50' S of Owens N

EL		13.5	124.7
bk		12.7	125.5
y		11.6	126.6
b		11.4	127.0
y		10.1	128.1
bk		11.4	127.0
WL		11.0	127.2

13841

Forward

85' S of Owens

WL		+0.6	138.8
bk		1.0	137.2
y		2.8	135.4
b		4.3	133.9
y		6.0	132.2
bk		8.0	130.2
EL		10.2	128.0

-100' S of Owens

EL		10.5	127.7
bk		8.8	129.4
y		7.6	130.6
b		6.3	131.9
y		5.4	132.8
TP	2.75	135.63	5.33	130.84
bk			0.9	134.7
WL			+0.4	136.0

135.63

	125'	S of	Owens	
W2			3,5	132.1
bl			4,8	130.8
4			5,2	130.4
b			5,3	130.3
4			5,4	130.0
bl			6,6	129.0
E2			8,4	127.2
	150	S of	Owens	
E2			11,0	124.6
bl			9,1	126.5
4			8,7	126.9
b			9,2	126.4
4			10,2	125.4
bl			10,5	125.1
W2			9,6	126.0
Tot	174	125.97	11,40	124,23

125.97

Fremont

65

	175'	S of	Owens	
W2			4,0	122.0
bl			5,5	120.5
4			6,3	119.7
b			7,1	118.9
4			8,0	118.0
bl			8,7	117.3
E2			9,2	116.8
	200	S of	Owens	
E2			13,0	111.0
bl			13,9	111.1
4			12,2	113.4
b			11,4	114.6
4			9,9	116.1
bl			7,8	118.2
W2			5,7	120.3

12597

	225'	S of	Owens	
WL			1.1	124.9
bb			3,1	122.9
y			5,0	121.0
b			7,0	119.0
y			9,3	116.7
bb			11,4	114.6
EL			13,5	112.5
TP	10,72	13146	5,23	120,74

	240	S of	Owens	
EL			11,9	119.6
bb			9,2	122.3
y			7,4	124.1
b			5,3	126.2
y			4,1	127.4
bb			3,3	128.2
WL			2,5	129.0

13146

Fernando

	250'	S of	Owens	
WL			2,2	129.3
bb			2,8	128.7
y			2,6	128.9
b			2,7	128.8
y			3,7	127.8
bb			5,7	125.8
EL			10.3	121.2

	275'	S of	Owens	
EL			4,9	126.6
bb			2,4	129.1
y			1,2	130.3
b			1,3	130.2
y			2,3	129.2
bb			2,4	129.1
WL			2,3	129.2

13146

here

300' S = N2 of Nicholson (50)

BM NW of Nichols

W2		4,31	127.15 ✓
b2		3,9	127.6
4		3,3	128.2
6		2,8	128.7
4		2,8	128.7
b2		2,7	128.8
E2		3,5	128.0 ✓

N b of Nichols

E2		4,3	127.2 ✓
b2		4,2	127.3
4		3,2	128.3
6		3,0	128.5 ✓
4		3,3	128.2
b2		4,1	127.4
W2		4,5	127.0 ✓

13146

N 4 of Nichols

W1		4,7	126.8 ✓
b1		4,1	127.4
4		3,8	127.7
6		3,4	128.1
4		3,4	128.1
b1		5,0	126.5
E1		5,6	125.9 ✓

Center of Nichols

E2		6,6	124.9 ✓
b2		5,5	126.0
4		4,2	127.3
6		4,1	127.4
4		4,0	127.5
b1		4,2	127.3
W2		4,7	126.8 ✓

13146

S 1/4 of Nichols

W2		4,6	126.7
6		4,4	127.1
4		4,3	127.2
6		4,5	127.0
4		4,7	126.8
6		5,9	125.6
E2		7,9	123.6

S 6 of Nichols

E2		8,8	122.7
6		6,8	125.7
4		5,6	125.9
6		5,0	126.5
4		4,9	126.6
6		4,5	127.0
W2		4,6	126.9

13146

S 1/2 of Nichols

W2		4,7	126.8
6		5,2	126.3
4		5,4	126.1
6		5,7	125.8
4		6,5	125.0
6		7,7	123.8
E2		9,1	122.4

25' S of Nichols

E2		12,0	119.5
6		10,5	120.9
4		9,3	122.2
6		8,1	123.4
4		7,1	124.4
6		6,6	124.9
W2		6,1	125.4

Fernando

13146

	50'	S.f.	Inches	
W2			12,2	119.3 ✓
bl			11,8	119.7
4			12,1	119.4
6			12,2	119.3
4			12,3	118.8
bl			13,7	117.8
E2			14,7	116.8 ✓
TP	0,45	119.36	12.55	118.91

	100'	S.f.	Inches	
E2			7,5	111.9 ✓
bl			7,1	112.8
4			7,0	112.4
6			7,4	112.0
4			7,2	112.3
bl			7,0	112.4
W2			6,8	112.6 ✓

119.36

	125'	S.f.	Inches	
W2			11,1	108.3 ✓
bl			10,4	109.0
4			11,0	108.4
6			10,8	108.6
4			11,0	108.4
bl			11,4	108.0
E2			12,2	107.2 ✓

	135'	S.f.	Inches	
E2			15,3	104.1 ✓
bl			14,3	105.1
4			13,0	106.4
6			11,4	108.0
4			10,1	109.3
bl			9,1	110.3
W2			7,8	111.6 ✓

119.36

200' S of Nichols

W2			8.5	110.9
bb			9.6	109.8
4			10.5	108.9
b			11.4	108.0
4			12.5	106.9
TP	2.61	10.961	12.16	107.20
bb			4.0	105.8
E2			4.8	105.0

250' S of Nichols

E2			6.8	103.0
bb			5.9	103.9
4			5.0	104.8
b			4.0	105.8
4			3.3	106.5
bb			2.2	107.6
W2			1.0	108.8

10981

Leonard

300' S=N2 Inc Coll (30)

W2			4.4	105.4
bb			5.2	104.6
4			5.7	104.1
b			6.4	103.4
4			7.7	102.1
bb			7.8	102.0
E2			9.2	100.6

N bb of Inc Coll.

E2			9.5	100.8
bb			8.8	101.0
4			8.5	101.3
b			8.1	101.7
4			6.8	103.0
bb			5.3	104.3
W2			4.7	105.1

10981

N 1/4 of Mc Coll

W2		30	106.8
bk		41	105.7
4		52	104.6
6		66	103.2
4		80	101.8
bk		94	100.4
E2		104	99.4

Center of Mc Coll

E2		109	98.9 ✓
bk		100	99.8
4		89	100.9
6		69	102.9
4		53	104.5
bk		34	106.4
W2		18	108.0 ✓

10981

Fernando

S 1/4 of Mc Coll

W2		19	107.9 ✓
bk		33	106.5
4		42	105.6
6		58	104.0
4		75	102.3
bk		94	100.4
E2		114	98.4 ✓

S bk of Mc Coll

E2		115	98.3 ✓
bk		97	100.1
4		83	101.5
6		69	102.9
4		56	104.2
bk		47	105.6
W2		25	105.3 ✓
		315	106.66

POSTED

BMSW Same Mc Coll

10961

	S Line of Mc Call st			
W2		3.3		106.5 ✓
bb		4.7		105.1
y		5.7		104.1
b			7.0	102.8
g			8.1	101.7
bl			9.4	100.4
E2			11.2	98.6 ✓
	50'	S of	Mc Call	
E2			13.6	96.2 ✓
bb			11.8	98.0
y			10.4	99.4
b			9.4	100.4
y			8.4	101.4
bb			6.9	102.9
W2			5.8	104.0 ✓

10961

Fernando

	100'	S of	Mc Call st	
W2			9.8	100.0 ✓
bb			11.0	98.8
y			12.0	97.8
b			12.7	97.1
TP	0.7 ~	98.10	12.43	97.38
y			2.0	96.1
bb			2.7	95.4
E2			4.4	93.7 ✓
	150'	S of	Mc Call	
E2			4.8	93.3 ✓
bb			4.0	94.1
y			3.1	95.0
b			2.5	95.6
y			2.0	96.0
bb			1.8	96.23
W2			0.5 ~	97.6 ✓

9/10

	200' S of Mc Call			
W2			2.2	95.9
b1			2.9	95.2
4			3.5	94.6
1			4.2	93.9
4			4.8	93.3
W2			5.0	93.1
E2			5.8	92.3
	250' S of Mc Call			
E2			8.4	89.7
b1			7.5	90.6
4			7.0	91.1
1			6.6	91.5
4			6.1	92.0
b1			5.3	92.8
W2			4.5	93.6

9/10

Leonard

	300' S = N bank of Lawrence			at Bm N W of Lawrence
W2			7.0	90.8
b1			8.0	90.1
4			8.4	89.7
1			8.5	89.6
4			9.0	89.1
b1			9.7	88.4
E2			10.6	87.5
	N bk of Lawrence			
E2			11.0	87.1
b1			10.2	87.9
4			9.3	88.8
1			9.0	89.1
4			8.8	89.3
b1			8.2	89.9
W2			7.4	90.7

9810

N ¼ of Lawrence

W	7.2	90.9 ✓
¼	8.0	90.1
4	8.5	89.6
1	9.0	89.1
7	9.6	88.5
¼	10.2	87.9
E	11.0	87.1 ✓

Center of Lawrence

E	11.0	87.1 ✓
¼	10.0	88.1
7	9.6	88.5
1	8.9	89.2
7	8.2	89.9
¼	7.7	90.4
W	7.1	91.0 ✓

9810

S ¼ of Lawrence

W	6.8	91.3 ✓
¼	7.6	90.5
7	7.9	90.2
1	8.5	89.6
7	9.0	89.1
¼	9.9	88.2
E	10.6	87.5 ✓

S ¼ of Lawrence

E	10.2	87.9 ✓
¼	8.6	89.5
7	9.1	89.0
1	8.5	89.6
7	8.1	90.0
¼	7.6	90.5
W	6.6	91.5 ✓

98.10

	S sur of Lowmere			
W2			6.0	92.1 ✓
bb			7.1	91.0
y			7.7	90.4
b			8.3	89.8
y			8.9	89.2
bb			9.6	88.5
E2			10.2	87.9 ✓
	50'	S of	Lowmere	
E2			11.1	87.0 ✓
bb			9.3	88.8
y			8.7	89.4
b			8.0	90.1
y			7.2	90.9
bb			6.6	91.5
W2			5.7	92.0 ✓
TP	1.06	93.40	5.76	92.34

93.40

	100'	S of	Lowmere	
W2			1.5	91.9 ✓
bb			2.4	91.0
y			3.3	90.1
b			4.0	89.4
y			4.6	88.8
bb			5.5	87.9
E2			6.0	87.4 ✓
	150'	S of	Lowmere	
E2			7.1	86.3 ✓
bb			6.6	86.8
y			6.0	87.4
b			3.4	88.0
y			4.7	88.7
bb			4.0	89.4
W2			2.9	90.5 ✓

Terrace

9340

2 vi S of Lawrence

W2		4,2	89.2 ✓
bk		5,6	87.8
4		6,2	87.2
6		6,8	86.6
4		7,4	86.0
bk		8,0	85.4
E2		8,7	84.7 ✓

2 vi S of Lawrence

E2		10,2	83.2 ✓
bk		9,8	83.6
4		9,2	84.2
6		8,8	84.6
4		7,9	85.5
bk		7,3	86.1
W2		6,5	86.9 ✓

9340

3 vi S of Kellogg (cr)

W2		8,6	84.8 ✓
bk		9,9	83.5
4		10,5	82.9
6		11,2	82.2
4		11,5	81.9
bk		12,1	81.4
E2		12,6	80.8 ✓

W bk of Kellogg

E2		12,7	80.7 ✓
bk		12,2	81.2
4		11,8	81.6
6		11,3	82.1
4		10,5	82.9
bk		10,0	83.4
W2		9,3	84.1 ✓

Terrace

...STED

9340

N ¼ of Kellogg

WL		9.5	83.9 ✓
bb		10.4	83.0
y		11.2	82.2
b		11.7	81.7
y		12.0	81.4
bb		12.7	80.7
EL		13.2	80.2 ✓

Center of Kellogg

EL		13.4	80.0 ✓
bb		12.7	80.7
y		12.3	81.1
b		11.7	81.7
y		11.2	82.2
bb		10.8	82.6
WL		9.6	83.8 ✓

9340

S ¼ of Kellogg

WL		9.6	83.8 ✓
bb		10.6	82.8
y		11.2	82.2
b		12.0	81.4
y		12.4	81.0
bb		13.0	80.4
EL		13.2	80.1 ✓

SBB of Kellogg

EL		13.0	80.4 ✓
bb		12.6	80.8
y		12.0	81.4
b		11.6	81.8
y		11.0	82.4
bb		10.7	82.7
WL		9.7	83.7 ✓
		994	8346

0,7 8414 83.47 BM.

S 2 ℄ Kellogg rd

WL	0,7	83.5	✓
bk	1.6	82.6	
4	1,7	82.5	
6	2.0	82.2	
7	2,7	81.5	
bk	3,1	81.1	
E2	3,9	80.3	✓

50' S ℄ Kellogg

E2	4,6	79.6	✓
bk	4,7	80.0	
7	3,7	80.8	
6	2,8	81.4	
4	2,1	82.1	
bk	1,6	82.6	
WL	0,8	83.4	✓

84.18

75' S ℄ Kellogg

WL	1,5	82.7	✓
bk	4,4	79.8	
4	2,2	82.0	
6	2,8	81.4	
7	3,5	80.7	
bk	4,0	80.2	
E2	4,7	79.5	✓

90' S ℄ Kellogg

E2	4,7	79.5	✓
bk	4,6	79.6	
7	6,6	77.6	
6	8,0	76.2	
4	9,8	74.4	
bk	9,7	74.9	
WL	7,8	76.6	✓

8418

	100'	S of	Kellogg	
WL			{1.7 / 7.3}	82.5 ✓ / 76.9 ✓
bk			{2.0 / 8.5}	82.2 / 75.7
y			8.8	75.4
b			10.0	74.2
y			10.5	73.7
bk			10.8	73.4
EL			10.9	73.3 ✓
	115'	S of	Kellogg	
EL			4.4	79.8 ✓
bk			4.0	80.2
y			3.5	80.7
b			3.0	81.2
y			2.5	81.7
bk			1.7	82.5
WL			0.5	83.7 ✓

8418

	130'	S of	Kellogg	
WL			0.8	83.4 ✓
bk			2.1	82.1
y			2.4	81.8
b			2.9	81.3
y			3.5	80.7
bk			4.1	80.1
EL			4.7	79.5 ✓
	215'	S of	Kellogg	
EL			4.8	79.4 ✓
bk			4.3	79.7
y			4.1	80.1
b			3.7	80.5
y			3.3	80.9
bk			2.7	81.5
WL			1.2	83.0 ✓
TP	4.52	87.23	1.29	82.91

87.23

	250'	S of	Kellogg	#400
WL			2.6	84.6 ✓
bl			3.8	83.4
y			4.2	83.0
l			4.8	82.4
y			5.3	81.9
bl			5.4	81.8
EL			6.5	80.7 ✓
	300'	S = NL	Jenkins	(50')
EL			5.0	82.2 ✓
bl			4.0	83.2
y			3.4	83.8
l			3.0	84.2
y			2.4	84.8
bl			1.9	85.3
WL			0.45	86.78 ✓

Continued in Book 4 54

Bm 83.23 Jenkins

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TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100.00	0.44	100.00	0.87	99.99	1.31	89
1	99.98	1.75	99.98	2.18	99.97	2.62	99.95	3.05	88
2	99.94	3.49	99.92	3.93	99.91	4.36	99.88	4.80	87
3	99.86	5.23	99.84	5.67	99.81	6.10	99.79	6.54	86
4	99.76	6.98	99.73	7.41	99.69	7.85	99.66	8.28	85
5	99.62	8.72	99.58	9.15	99.54	9.58	99.50	10.02	84
6	99.45	10.45	99.41	10.89	99.36	11.32	99.31	11.75	83
7	99.25	12.19	99.20	12.62	99.14	13.05	99.09	13.49	82
8	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	15.64	98.70	16.07	98.63	16.50	98.56	16.93	80
10	98.48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98.16	19.08	98.08	19.51	97.99	19.94	97.90	20.36	78
12	97.81	20.79	97.72	21.22	97.63	21.64	97.53	22.07	77
13	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	24.19	96.92	24.62	96.81	25.04	96.70	25.46	75
15	96.59	25.88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.82	73
17	95.63	29.24	95.50	29.65	95.37	30.07	95.24	30.49	72
18	95.11	30.90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35.43	69
21	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38.67	67
23	92.05	39.07	91.88	39.47	91.71	39.87	91.53	40.27	66
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	43.84	89.69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	46.95	88.09	47.33	87.88	47.72	87.67	48.10	61
29	87.46	48.48	87.25	48.86	87.04	49.24	86.82	49.62	60
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	52.99	84.57	53.36	84.34	53.73	84.10	54.10	57
33	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	52
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	45
45	70.71	70.71							
Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees
	DEGREES		¾ DEGREE.		½ DEGREE.		¼ DEGREE.		