Return to City Engineers Office
City Hall, San Diego, Cal.

400

LEVEL

F.B. 463

Return to City Engineers Office
City Hall, San Diego, Cal.

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Table showing the difference of latitude and departure in running 80 chains at any course from 1 to 60 minutes.

MINUTES.	LKS.	MINUTES.	LKS.	MINUTES.	LKS.
1	2 1/3	21	49	41	95 2/3
2	4 2/3	22	51 1/3	42	98
3	7	23	53 2/3	43	100 1/3
4	9 1/3	24	56	44	102 2/3
5	11 2/3	25	58 1/3	45	105
6	14	26	60 2/3	46	107 1/3
7	16 1/3	27	63	47	109 2/3
8	18 2/3	28	65 1/3	48	112
9	21	29	67 2/3	49	114 1/3
10	23 1/3	30	70	50	116 2/3
11	25 2/3	31	72 1/3	51	119
12	28	32	74 2/3	52	121 1/3
13	30 1/3	33	77	53	123 2/3
14	32 2/3	34	79 1/3	54	126
15	35	35	81 2/3	55	128 1/3
16	37 1/3	36	84	56	130 1/3
17	39 2/3	37	86 1/3	57	133
18	42	38	88 2/3	58	135 1/3
19	44 1/3	39	91	59	137 2/3
20	46 2/3	40	93 1/3	60	140

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TABLE FOR RUNNING ON SLOPES.

In the following table the first column shows the angle, the second the number of links to be added to a chain on the slopes, to make one chain, horizontal measurement.

ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS	ANGLE	COR. IN LINKS
°		°		°		°	
4	0.24	11	1.88	18	5.14	25	10.54
5	0.38	12	2.24	19	5.76	26	11.26
6	0.55	13	2.63	20	6.42	27	12.24
7	0.76	14	3.06	21	7.11	28	13.37
8	0.98	15	3.53	22	7.85	29	14.34
9	1.24	16	4.02	23	8.64	30	15.47
10	1.55	17	4.56	24	9.47	35	22.07

Crocker Quality

LEVEL BOOK

No. 400

COMMUNI COMSENSU PRIMO TRADE MARK

MANUFACTURED BY

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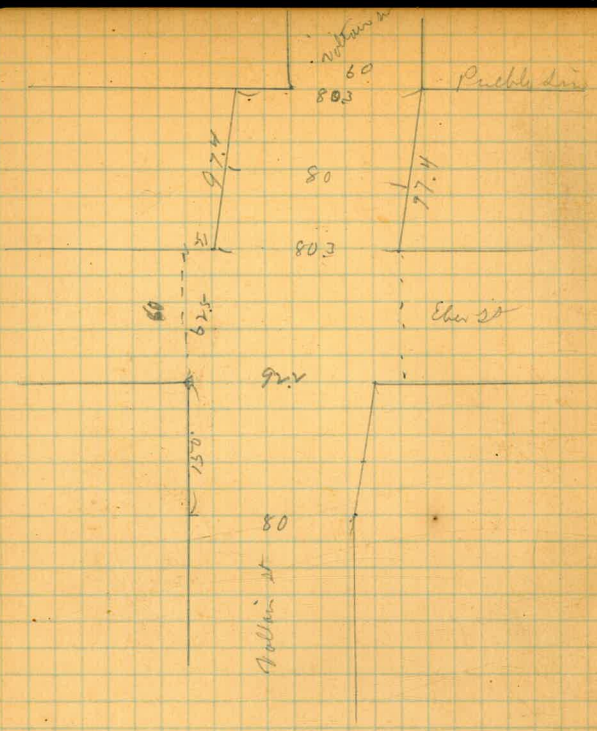


Borough Bronx Podzus

Cross section of Voltaire St (80')
From E & Pd 208.5 to End

1 2

5.13.09					Bm monument Voltaire & Prichard
	6.94	85.84		79.00	
	4.02	89.86	0.46	85.46	
	.10	76.58	13.00	76.48	
	0.42	64.11	12.89	63.69	
	0.07	51.52	12.62	51.49	
	E & P 208 = 97.4 St. Founded at (80.3)				
N2			5.8	45.8	
61			5.5	46.1	
4			5.1	46.5	
+11 = 2'n Rail			5.1	46.5	
6+7'	2'n Rail		5.0	46.6	
4			5.3	46.3	
61			5.3	46.3	
S2			5.3	46.3	
	Elev Rail			466	

	47.4	W = 50	E of Fraude St	
SL			5.4	46.2
bh			5.6	
y			5.4	
++	= 2 S R		5.2	
b+i	= 2 in R		5.3	
y			5.6	
bl			5.9	
n2			5.8	45.8
(80.3)	E elev of Fraude St (60')			
n2			6.1	45.5
bl			6.2	45.4
y			5.9	45.7
+,2	= 2 in R		5.8	45.8
b+8	= 2 S R		5.9	45.7
y			5.8	45.8
bh			6.2	45.4
S2			5.6	46.0
	Elev of Riv			45.64

	E blw of Fraude St		
S2		5.7	45.9
bl		6.2	45.4
y		5.9	45.7
+3	= 2 S of R	6.0	45.6
b	= 2 in of R	6.1	45.5
y		6.3	45.3
bh		6.3	
n2		65	45.1
	E hyd Fraude St		
n2		6.4	45.2
bh		6.3	
y		6.2	
b		6.1	
+1	= 2 in of R	6.3	
+10		6.2	
y		5.8	
bl		5.8	
s2		5.8	45.8

5.56

Centre of Fraude st

SQ	5,6	46.0
bl	5,8	
y	6,0	
+2' = 2' SR	6,3	
+11' = 2' n Rui	6,4	
b	6,3	
y	6,3	
bl	6,4	
NL	6,4	45.2

W 1/4 of Fraude st

NL	6,9	44,7
bl	6,7	
y	6,7	
1	6,3	
+3' = 2' n f R	6,4	
+12 = 2 S + R	6,3	
y	6,2	
bl	6,1	
SL	6,0	45.6

5.56

W bl of Fraude st

SL	6,5	45,1
bl	6,7	
y	6,4	
+1'	6,6	
+10	6,5	
b	6,7	44,9
y	6,9	
bl	7,2	
NL	7,6	44,0

(9,2') W line of Fraude st

NL	7,3	44,3.
bl	7,1	44,5
y	7,0	44,6
b	6,8	44,8
+4 = 2' n R	6,5	45,1
+13 = 2 S R	6,7	44,9
Elev 1 Rui 44,90		
y	6,5	45,1
Cb.	6,4	45,2
S.L.	6,2	45,4
TP 0,78 4,616	6,8	45,38

(88)	50	W of	Transit	
S2			21	44.1
M			2,1	
4			2,3	
+1' = 1's Rail			2,6	
+10' = 2's Rail			2,6	
6			2,5	43.7
4			2,9	
Sch			3,0	
N2			3,1	43.1
84	100'	W of	Transit at	
N2			45	41.7
Sch			4,6	41.6
4			4,4	41.8
6			4,1	42.1
+3' = 3's Rail			4,2	42.0
+4 = 4's Rail			4,0	42.2
4			3,7	42.5
M			3,6	42.6
S2			3,7	42.5

(80)	150'	W of	Transit	
S2			5,5	40.7
M			5,9	
4			5,6	
+1' = 2's R			5,7	
+10 = 2's R			5,7	
6			5,6	40.6
4			5,8	
Sch			6,5	
N2			6,2	40.0
	200	W of	Transit at	
N2			7,7	38.5
M			8,0	38.2
4			7,6	38.6
6			7,4	38.8
+2' = 2's R			7,4	38.8
+11' = 2's R			7,4	38.8
4			7,3	38.9
M			7,9	38.3
S2			7,4	38.8

	250'	W y	Fronde	
SL			8.9	37.9
bl			9.1	
y			9.2	
	+3' = 2'3 of R		9.0	
	+1' = 2' ng R		9.0	
b			9.0	37.2
bl			9.1	
y/R			9.7	
nL			9.0	37.2

	300'	W y	Fronde	
nL			10.6	35.6
bl			11.0	35.2
y			10.5	35.7
b			10.5	35.7
				35.7
	+1' = 2' n R		10.5	35.7
	+1.1 = 2' s R		10.4	35.8
y			10.5	35.7
bl			11.2	35.0
SL			10.5	35.7
TP	130	36.4	10.72	35.44

	350	W y	Fronde	
nL			2.3	34.4
bl			2.5	
y			2.1	
	+3' = 2'5 R		2.4	
	+1' = 2' n R		2.4	
b			2.4	34.3
bl			2.2	
bl			2.8	
nL			2.3	34.4

	400	W y	Fronde	
nL			3.2	33.5
bl			3.4	33.3
y			3.2	33.5
b			3.5	33.2
			3.4	33.1
			3.6	33.1
y			3.3	33.6
bl			3.7	33.0
SL			3.4	33.3

	450'	W of	Trough at	
SL			4.2	32.2
bk			4.3	
y			4.2	
+3' = 2'S R			4.5	
+12' = 2' N R			4.5	
b			4.5	32.2
y			4.0	
bk			4.8	
NL			4.2	32.2
	500'	W of	Trough	
NL			4.9	31.8
bk			5.7	31.0
y			5.0	31.7
b			5.2	31.2
+1' = 2' N R			5.3	31.4
+10' = 2' S R			5.0	31.7
y			4.9	31.8
bk			5.4	31.3
SL			5.0	31.7

3674

	550'	W of	Trough at	
SL			5.7	31.1
bk			5.6	
y			5.5	
+3' = 2'S R			5.5	
+12' = 2' N R			5.8	
b			5.8	30.9
y			5.4	
bk			5.8	
NL			5.5	31.2
	600'	W = Σ Lin ft Ether at (60)-		
NL			5.8	30.9
bk			6.2	30.5
y			5.9	30.8
b			5.8	30.9
+1'			6.0	30.7
10'			6.0	30.7
y			6.0	30.7
bk			6.0	30.7
SL			5.9	30.8
	Elev of	Rail		30.63

3674

E bdr of Eben St

SL		6.4	30.3
bk		6.1	
4		5.8	
+3' = 2' 8 1/2 R		6.1	
+12' = 2' 11 1/2 R		6.1	
b		6.1	30.6
4		6.0	
bk		6.4	
nL		6.4	30.3

E 1/4 of Eben St

nL		5.8	30.9
bk		5.9	
4		5.8	
b		6.0	30.7
+1' = 2' nR		6.0	
+10' = 2' 5 R		6.1	
4		5.8	
bk		6.0	
SL		5.9	30.8

3674

Center of Eben St

SL		5.7	31.0
bk		6.0	
4		5.9	
+3 = 2' 8R		6.2	
+12 = 2' 3R		6.2	
b		6.2	30.5
4		6.0	
bk		5.9	
nL		5.9	30.8

W 1/4 of Eben St

nL		6.1	30.6
bk		6.1	
4		5.9	
b		6.4	30.3
+1' = 2' nR		6.4	
+10 = 2' 5R		6.2	
4		6.0	
bk		6.1	
SL		6.1	30.6

W Elton

7

3274

	W bk of Eber St			
S2			6,6	30,1
1L			6,6	
4			6,2	
+3'	=2' SR		6,5-	
+12'	=2' NR		6,5-	
6			6,5-	30,2
4			6,1	
6L			6,5	
N2			6,6	30,1
	W line of	Eber St		
N2			6,0	30,7
1L			6,6	30,1
4			6,2	30,5
+7'	=2' NR		6,4	30.3
+10'	=2' SR		6,5-	30.2
6	Elev of Bar	30x4	6,2	30,5
4			6,4	30.3
1L			6,7	30.0
S2			6,1	30.6
TP	2,91	3373	5-9	30,5

3373

	50'	W of	Eber St	
S2			3,5-	30.2
1L			4,1	
4			3,5-	
+3	=2' SR		3,8	
+12	=2' NR		4,0	
6			4,0	29.7
4			3,4	
6L			3,8	
N2			3,5-	30,2
	100'	W of	Eber St	
N2			4,0	29.7
1L			4,4	29.3
4			3,6	30,1
6			4,1	29.6
+1	=2' NR		4,1	29.6
+10	=2' SR		4,2	29.5
4			3,9	29,8
1L			4,5-	29,2
S2			3,9	29,8

Valtaire

3373

	150	W of	Elev	at
S2			4.4	29.3
bl			4.7	29.0
y			4.5	29.2
+3' = 2' S R			4.6	29.1
+12 = 2' N R			4.4	2
b			4.5	29.2
y			4.5	
bl			5.0	
N2			4.3	29.4

	200	W of	Elev	
N2			4.9	28.8
bl			5.4	28.3
y			5.0	28.7
b			5.0	28.7
+1			5.0	28.7
+10			5.0	28.7
y			4.9	28.8
bl			5.3	28.4
S2			5.0	28.7

3373 Valtura 9

	250	W of	Elev	
S2			5.6	28.1
bl			5.6	
y			5.4	
+3 = 2' S R			5.5	
+12 = 2' N R			5.5	
b			5.5	28.2
y			5.5	
bl			5.7	
N2			5.1	28.6

	300	W of	Elev	at
N2			5.4	28.3
bl			5.9	27.8
y			5.8	27.9
b			5.8	27.9
+1			5.8	27.9
+10			5.8	27.9
y			5.7	28.0
bl			6.3	27.4
S2			6.0	27.7

3373

	35-0'	N of	Eber	st
S2			6.0	27.7
bl			6.7	
y			6.0	
43' = 2' SR			6.2	
412' = 2' NR			6.0	
b			6.0	27.7
y			6.2	
bl			6.5	
N2			6.0	27.7
TP	31.2	3731	5.54	28.19
	400'	N of	Eber	st
N2			4.0	27.3
bl			4.4	26.9
y			4.2	27.1
b			4.1	27.2
41' = 2' NR			4.1	27.2
410 = 2' SR			4.0	27.3
y			4.0	27.3
bl			4.6	26.7
S2			4.0	27.3

3431

	450'	N of	Eber	st
S2			4.1	27.2
bl			4.8	
y			4.1	
43 = 2' SR			4.3	
412 = 2' NR			4.2	
b			4.2	27.1
y			4.5	
bl			4.5	
N2			4.2	27.1
	500'	N of	Eber	st
N2			4.7	26.6
bl			4.5	26.8
y			4.8	26.5
b			4.7	26.6
41 = 2' NR			4.7	26.6
410 = 2' SR			4.7	26.6
y			5.0	26.3
bl			5.0	26.3
S2			4.7	26.6

3+31

	550' W of	Elev at	
SL		4.7	26.6
M		4.7	26.6
4		5.0	26.3
+3' = 2' SR		4.9	26.4
+12' = 2' WR		5.0	26.3
b		5.0	26.3
4		4.9	26.4
bL		5.0	26.3
WL		5.1	26.2
	600' W = E line De Zoe 1460')		
WL		5.2	26.1
bL		5.5	25.8
4		5.4	25.9
L		5.3	26.0
+1' = 2' WR		5.3	26.0
+10' = 2' SR		5.3	26.0
4		5.2	26.1
bL		5.3	26.0
SL		5.0	26.3
Elev of Point			26.14

3+31

Valtaw

	Ebb of	De Zoe pt	
SL		5.7	2√.6
M		5.6	
4		5.2	
+3 = 2' SR		5.4	
+12 = 2' WR		5.4	
b		5.3	26.0
4		5.5	
M		5.6	
WL		5.9	2√.4
	E 1/4 of	De Zoe pt	
WL		5.3	26.0
M		5.2	
4		5.3	
b		5.3	26.0
+1 = 2' WR		5.3	
+10 = 2' SR		5.3	
4		5.2	
bL		5.2	
SL		5.2	26.1

31.31

Center of De Forest

SL		5.4	26.3
bl		5.0	
y		5.2	
+3 = 2' S R		5.5	
+12 = 2' n R		5.2	
b		5.2	26.1
y		5.2	
bl		5.1	
nL		5.0	26.3

W 1/4 of De Forest

nL		5.2	26.1
bl		5.2	
y		5.0	
b		5.2	26.1
+1 = 2' n R		5.2	
+10 = 2' S R		5.5	
y		5.0	
bl		5.1	
SL		5.1	26.2

31.31

W bl of De Forest

SL		5.9	25.4
bl		5.7	
y		5.5	
+3 = 2' SR		5.5	
+12 = 2' n R		5.4	
b		5.4	25.9
y		5.2	
bl		5.7	
nL		5.9	25.4

W line of De Forest

nL		5.0	26.0
bl		5.7	25.6
y		5.2	26.1
b		5.4	25.9
+1 = 2' n R		5.4	25.9
+10 = 2' S R		5.5	25.8

Elev of Pair 26.00

y		5.3	25.8
bl		5.6	25.7
SL		5.0	26.0
2.94	29.01	5.4	26.07

Bm SW # De Forest

2901

	50'	W y	Qz Zn	
SL			3,3	25.7
bl			3,3	
y			3,2	
+3'	=2'SR		3,5	
+4'	=2'nR		2,3	
b			3,3	25.7
y			3,4	
bl			3,3	
nL			3,4	25.6

	100	W y	Qz Zn	
nL			3,7	25.3
bl			3,8	25,2
y			3,7	25,3
b			3,8	25.2
+1	=2'nR		3,8	25,2
+10	=2'SR		4,0	25.0
y			3,4	25.6
bl			3,7	25.3
SL			3,6	25.4

2901

	150	W y	Qz Zn		Tourtelin 3
SL			4,3	24.7	
bl			4,3		
y			4,2		
+3			4,4		
+4			4,5		
b			4,5	24.5	
y			4,4		
bl			4,0		
nL			4,2	24.8	

	200	W y	Qz Zn	
nL			4,7	24.3
bl			5,1	24.9
y			5,0	24.0
b			5,2	23.8
+1			5,2	23.8
+10			5,1	23.9
y			5,0	24.0
bl			5,0	24.0
SL			5,2	23.8

29.01

	250'	W of	Dr Zone	
S2			5.8	23.2
b			5.8	
4			5.8	
+3			5.7	
+12			5.6	
b			5.8	23.2
4			5.8	
M			5.8	
N2			5.8	23.2

	300'	W of	Dr Zone	
N2			6.2	22.8
M			6.3	22.7
4			6.3	22.7
b			6.4	22.6
+1			6.4	22.6
+10			6.4	22.6
4			6.4	22.6
M			6.3	22.7
S2			6.5	22.8

29.01

Vastan

	350'	W of	Dr Zone	
S2			7.2	21.8
M			7.0	
4			7.3	
+3			7.0	
+12			7.0	
b			7.4	21.6
4			7.3	
M			7.4	
N2			7.1	21.9

a bit stark

	1.53	23.95	6.59	23.42

	400'	W of	Dr Zone	
N2			2.8	21.2
M			2.9	21.1
4			2.7	21.3
b			2.8	21.2
+1			2.8	21.2
+10			2.9	21.1
4			3.0	21.0
M			2.7	21.3
S3			2.7	21.3

2395

	450'	W of	De Zaan	
SL			3.3	20.7
bl			3.5	
4			3.3	
+3' = V SK			3.4	
+1V = 2' SW			3.4	
b			3.4	20.6
4			3.4	
bl			3.3	
NL			3.3	20.7

	500'	W of	De Zaan	
NL			4.0	20.0
bl			4.2	19.8
4			4.2	19.8
b			4.2	19.8
+1			4.2	19.8
+10			4.4	19.6
4			4.2	19.8
bl			4.6	19.4
SL			4.6	19.4

2395

	550	W of	De Zaan		Voltan
SL			3-0	19.0	
bl			3-0		
4			3-0		
+3			3-0		
+1V			3-2		
b			3-2	18.8	
4			3-0		
bl			4.6		
NL			3-0	19.0	

600 · W = E bar of bobl 14 (60)

NL			3-7	18.3	
bl			3-6	18.4	
4			3-9	18.1	
+1			3-9	18.1	
+10			3-8	18.2	
4b			3-9	18.1	
4			3-9	18.1	
bl			3-7	18.3	
SL			3.88	18.07	B m SEA bobl pt
Elev of Rail				18.20	

23.95

E bk of bakb st

SL		6.5	17.5
bk		6.5	
4		6.0	
+1' = 2' SR		6.1	
+10 = 2' NR		6.0	
b		6.0	18.0
4		6.1	
bk		6.2	
RL		6.5	17.5

E ¼ of bakb st

NL		6.0	18.0
bk		6.0	
4		6.2	
b		6.2	17.8
+1 = 2' NR		6.2	
+10 = 2' SR		6.1	
4		6.0	
bk		6.1	
SL		6.1	17.9

23.95

Center of bakb st

Galtaw

SL		6.2	17.8
bk		6.2	
4		6.0	
+3 = 2' SR		6.3	
+12 = 2' NR		6.3	
b		6.3	17.7
4		6.3	
bk		6.2	
NL		5.7	18.3

W ¼ of bakb st

NL		6.0	18.0
bk		6.2	
4		6.3	
b		6.4	17.6
+1 = 2' NR		6.4	
+10 = 2' SR		6.3	
4		6.3	
bk		6.5	
SL		6.4	17.6

2395

Width of Cable 2

S2	7.0	17.0	
M	6.9		
4	6.3		
3' = 2' SR	6.5		
1½' = 2' NR	6.6		
	6.4		
6	6.6	17.4	
4	6.4		
M	6.7		
N2	6.5	17.5	

Width of Cable 2

N2	6.2	17.8	
M	6.3	17.7	
4	6.4	17.6	
6	6.4	17.6	
1' = 2' NR	6.7	17.3	
1½ = 2' SR	6.7	17.3	
4	6.4	17.6	
M	7.2	16.8	
S2	7.0	17.0	

Elev of Rail 17.2

2395

Valtari

50' N of Cable 2

S2	7.6	16.4	
M	7.8		
4	7.2		
3' = 2' SR	7.4		
1½ = 2' NR	7.4		
6	7.4	16.6	
4	7.3		
M	7.0		
N2	7.1	16.9	
TP 1.00	16.30	6.65	17.30

100' N of Cable

N2	2.3	16.0	
M	2.6	15.7	
4	2.1	16.2	
6	2.4	15.9	
1' = 2' NR	2.4	15.9	
1½ = 2' SR	2.5	15.8	
	2.3	16.0	
4		15.7	
M	2.6		
S2	2.4	15.9	

18.30

	150'	w.y	babb	v
SL			3.4	14.9
bb			3.4	"
y			3.2	
+3	=2'3R		3.2	
+12	=2'nR		3.2	
b			3.2	15.1
y			3.0	
bb			3.0	
nL			3.0	15.3

	200'	w.y	babb	
nL			3.9	14.4
bb			4.1	14.2
y			3.8	14.5
b			3.9	14.4
+1	=2'nR		3.9	14.4
+10	=2'3R		4.0	14.3
y			4.1	14.2
bb			4.1	14.2
SL			4.0	14.3

18.30

Vallair

18

	250'	w.y	babb	v
SL			5.0	13.3
bb			4.8	
y			5.0	
+3'	=2'3R		4.6	
+12	=2'nR		4.8	
b			4.8	13.5
y			4.8	
bb			5.4	
nL			4.8	13.5

	300'	w.y	babb	v
nL			5.4	12.9
bb			5.3	13.0
y			5.4	12.9
b			5.4	12.9
+1'	=2'nR		5.4	12.9
+10	=2'3R		5.6	12.7
y			5.9	12.4
bb			5.5	12.8
SL			5.5	12.8

1830

	330'	N of	Cable	
SL			6.1	12.2
bl			6.1	
y			6.1	
+0 = 2' SR			5.9	
+12 = 2' NR			5.0	
b			5.9	12.4
y			6.0	
bl			6.6	
NL			6.0	12.3
	400'	N of	Cable	
NL			6.6	11.7
bl			6.5	11.8
y			6.5	11.8
b			6.3	12.0
+1 = 2' NR			6.3	12.0
+10 = 2' SR			6.5	11.8
bl			6.6	11.7
bl			6.6	11.7
SL			6.5	11.8

1830

Valley

	450'	N of	Cable	
SL			7.7	10.6
bl			7.5	
y			7.6	
+0 = 2' SR			7.2	
+12 = 2' NR			7.1	
b			7.1	11.2
y			7.4	
bl			7.3	
NL			7.2	11.1
	501'	W = Buckley Line (N.L. p.L 201)		
NL			7.9	10.4
bl			8.0	10.3
y			8.1	10.2
b			8.0	10.3
+1 = 2' NR			8.0	10.3
+10 = 2' SR		Edge of Rail 1066	8.0	10.3
y			8.3	10.0
bl			8.0	10.3
SL			8.0	10.3
Br			8.03	10.27

Br SE H

Cross section of Latus St (50)
Schuyl Conn Railways
5-14-19 — W Line of Fronde St —

		41.1	47.99	45.38	
S 2			5,20	42,79	Bm S on Latus & Fronde
b 1			5,3		
7			5,3		
b			5,2	42.8	
7			5,7		
b 1			5,8		
N 2			5,9	42,1	
	50'	W of	Fronde St		
N 2			7,7	40.3	
b 1			7,2		
7			7,4		
b			7,0	41,0	
7			7,2		
b 1			7,0		
S 2			7,0	41,0	

Latus
20

		41.99		
	100	W of	Fronde St	
S 2			8,4	39.6
b 1			8,6	
7			8,8	
b			8,6	39.4
7			9,1	
b 1			9,1	
N 2			9,0	39.0
	150	W of	Fronde St	
N 2			10,2	37.8
b 1			10,1	
7			10,1	
b			9,6	38,4
7			9,9	
b 1			9,8	
S 2			9,7	38.3

47.99

	200	w f	Froude n	
S2			10,5	37.5
bl			10,8	
4			10,8	
b			10,6	37,4
4			11,0	
bl			10,9	
n2			11,0	37.0
	250	w f	Froude n	
n3			11,6	36,4
bl			11,5	
4			11,9	
b			11,4	36.6
4			11,7	
bl			11,6	
S2			11,5	36,5
7p	175	38,15	11,09	3690

38.15

Lotus

	300	w f	Froude n	
S2			2,6	35.6
bl			2,7	
4			2,8	
b			2,4	35.8
4			2,8	
bl			2,5	
n2			2,5	35.7
	350	w f	Froude n	
n2			3,2	35.0
bl			3,7	
4			3,9	
b			3,5	34.7
4			3,7	
bl			3,7	
S2			3,6	34.6

38.15-

	400'	W of	Found 21-	
SL			4,7	33.5
bl			4,6	
4			4,5-	
b			4,5-	33.7
4			4,6	
bl			4,5-	
SL			4,2	34.0

	415-0	W of	Found	
SL			5-2	33,0
bl			5-3	
4			5-4	
b			5-0	33.2
4			5-2	
bl			5-3	
SL			5-4	32.8

38.15-

	500'	W of	Found		Totals
SL			6,2	32.0	
bl			6,0		
4			6,0		
b			5-5	32.7	
4			5-8		
bl			5-8		
SL			5-8	32.4	

	5-5-0	W of	Found	
SL			6,4	31.8
bl			6,2	
4			6,3	
b			6,3	31.9
4			6,4	
bl			6,3	
SL			6,1	32.1

Lotus

38.15

	60'	W = E Line of	Eber St (60)	
S2		6,7	31.5	
6		6,6		
7		6,8		
8		6,6	31.6	
7		6,7		
6		6,7		
N2		6,7	31.5	
	E 6 of	Eber St		
N2		7,6	30.6	
6		7,5		
7		6,9		
6		7,1	31.1	
4		7,0		
6		7,3		
S2		7,5		
TP	35.1	34.92	6.74	31.46

SC H
Eber

34.92

	E ¼ of	Eber St	
S2		3,7	31.2
6		3,8	
7		3,6	
6		3,5	31.4
7		3,5	
6		3,5	
N2		3,6	31.3
	Center of	Eber St	
N2		3,4	31.5
6		3,4	
7		3,3	
6		3,31	31.6
7		3,4	
6		3,4	
S2		3,6	31.3

34.92

	W ¼ of	Eben	St
S 2		3,8	31.1
bk		3,8	
4		3,6	
6		3,4	31,3
4		3,5	
bk		3,5	
N 2		3,4	31,3

	W bk of	Eben	St
N 2		4,2	30.7
bk		3,7	
4		3,9	
6		3,6	31,3
4		3,9	
bk		4,3	
S 2		4,2	30,6

34.92

Lotus

	W line of	Eben	St
S 2		3,8	31.1
bk		3,9	
4		3,8	
6		3,4	31.1
4		3,7	
bk		3,7	
N 2		3,7	31.2

	50 W of	Eben	St
N 2		3,9	31,0
bk		4,0	
4		4,0	
6		3,8	31.1
4		3,9	
bk		3,9	
S 2		4,1	30.8

3492

	Level	W of	Elev	
SL			4.3	30.6
bk			4.3	
℄			4.3	
L			4.0	30.9
℄			4.0	
bk			4.1	
NL			4.1	30.8
	150	W of	Elev	
NL			4.8	30.1
bk			4.4	
℄			4.7	
L			4.4	30.5
℄			4.9	
bk			4.6	
SL			4.5	30.4

3492

Setters

	Level	W of	Elev	
SL			5.3	29.6
bk			5.0	
℄			5.4	
L			4.8	30.1
℄			5.2	
bk			5.3	
NL			5.0	29.9
	250	W of	Elev	
NL			5.5	29.4
bk			5.3	
℄			5.7	
L			5.6	29.3
℄			5.8	
bk			5.5	
SL			5.7	29.2

3492

	300'	N of	Elev	P
S2			62	28.7
BL			62	
4			62	
6			61	28.8
4			63	
BL			64	
N2			63	28.6
TP	262	3159	5-95	2897

	350'	N of	Elev	P
N2			35	28.1
BL			33	
4			33	
6			33	28.3
4			36	
BL			33	
S2			36	28.0

3159

	400'	N of	Elev	P
S2			38	27.8
BL			38	
4			39	
6			38	27.8
4			39	
BL			39	
N2			40	27.6

	450'	W of	Elev	P
N2			46	27.0
BL			45	
4			46	
6			45	27.1
4			45	
BL			43	
S2			47	27.8

31.59

	5-00	w of	Eben	st
S2			5-1	26.5
bb			5-0	
4			5-2	
b			5-0	26.6
4			5-1	
bb			5-1	
N2			5-0	26.6

	5-50	W of	Eben	st
N2			5-8	2 5.8
bb			5-7	
4			5-4	
b			5-2	26.4
4			5-7	
bb			5-5	
S2			5-6	26.0

31.59

Satus

	6-00	w =	E Lin	of De Tar	st (60)
S2			5-8	2 5.8	
bb			5-6		
4			6.0		
b			5-8	2 5.8	
4			6.0		
bb			6.1		
N2			5-9	2 5.7	

	E bb	of	De Tar	st
N2			6.7	24.9
bb			6.6	
4			6.1	
b			6.0	2 5.6
4			6.2	
bb			6.5	
S2			6.7	24.9

3159

E 1/4 of De Zavala

S2			6.0	2 V. 6
bb			6.0	
y			5.9	
b			6.0	2 V. 6
y			6.0	
bb			6.1	
N2			6.0	2 V. 6

center of De Zavala st

N2			5.9	2 V. 7
bb			6.0	
y			6.0	
b			6.0	2 V. 6
y			5.8	
bb			5.9	
S2			5.9	2 V. 7

3159

W 1/4 of De Zavala st

S2			6.2	2 V. 4
bb			6.3	
y			6.2	
b			6.1	2 V. V.
y			6.1	
bb			6.1	
N2			6.2	2 V. 4

W bb of De Zavala st

N2			6.9	2 4.7
bb			6.8	
y			6.6	
b			6.3	2 V. 3
y			6.2	
bb			6.7	
S2			6.6	2 V. 0
TP	3.73	29.08	6.24	25.35

Lots

S W bb De Zav

2908

	Wdin.	W	De Zar.	st
St			3,7	2V.4
bl			3,7	
y			3,9	
l			3,7	2V.4
y			3,9	
bl			3,7	
rz			3,8	2V.3
	30	W	De Zar	
rz			4,V	24.9
bl			4,2	
y			4,3	
l			3,9	2V.2
y			4,0	
bl			4,1	
St			4,0	2V.1

2908

	160	W	De Zar	st
St			4,1	2V.0
bl			4,2	
y			4,2	
l			4,0	2V.1
y			4,2	
bl			4,3	
rz			4,5	24.6
	130	W	De Zar	st
rz			4,8	24.3
bl			4,7	
y			4,7	
l			4,4	24.7
y			4,7	
bl			4,5	
St			4,6	24.V

2905

	200	W.S.	Q Tot	H
S2			4,9	24.2
b2			5,0	
4			5,0	
2			4,8	24.3
1			4,9	
b1			5,0	
n2			5,1	24.0

	250	W.S.	Q Tot	H
n2			5,5	23.6
3			5,4	
4			5,5	
1			5,3	23.8
4			5,3	
b1			5,3	
S1			5,5	23.6

2908

	300	W.S.	Q Tot	H
S2			5,9	23.2
b2			6,0	
4			5,9	
2			5,5	23.6
4			6,0	
b1			5,8	
n2			6,0	23.1

	350	W.S.	Q Tot	H
n2			6,7	22.4
b2			6,7	
4			6,6	
2			6,5	22.6
4			6,4	
b1			6,5	
S1			6,6	22.5
TP	2,00	24,93	6,15	22,93

Soltis
20

24.93

	4 ovi	w f	D Zw	st
S2			3,4	21.5
bl			3,3	
y			3,3	
l			3,2	21.7
y			3,2	
bl			3,3	
n2			3,3	21.6
	4/50	w f	D Zw	st
n2			4,0	20.9
bl			4,0	
y			4,0	
l			3,8	21.1
y			4,0	
bl			4,0	
S2			4,1	20.8

24.93

Satiro

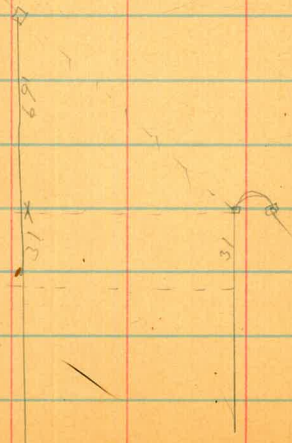
	5 ovi	w f	D Zw	
S2			4,8	20.1
bl			4,7	
y			4,9	
l			4,5	20.4
y			4,6	
bl			4,7	
n2			4,8	20.1
	5-31	w = Boulevard		on n. 2
S2			5-2	19.7
bl			5,0	
y			5-3	
l			5-0	19.9
y			5-2	
bl			5-2	
n2			5-3	19.6

24.03

5-31 m n = Bruksvann
600 m s = E. babb

N2	5-3	19.6
fb	5-2	
y	5-5	
d	5-5	19.4
y	5-8	
d	6,1	
Se	6,0	18.9
Bm	6,15	18,78

SE H
Babb



Intersection of Main St (5-0) C2, P2 205 & next Sta.

5-5½ 5-0.92 45.38

E 2 P 2 205 = 97.E of Fronde st

n2		1,1	48.8
bl		1,5	49.4
4		1,2	49.7
b		0,7	50.2
4		0,7	50.2
bl		0,4	50.5
S2		0,3	50.6

5-0' E of Fronde st

S2		1,0	49.9
bl		1,3	49.6
4		1,4	49.5
b		1,7	49.2
4		2,2	48.7
bl		2,3	48.6
n2		2,4	48.5

X Sections plotted for grading & paving Oct 9-11-54

5-0.92

E Line of Fronde st (60) Main

n2		2,9	48.0
bl		2,9	48.0
4		3,0	47.9
b		2,9	48.0
4		2,9	48.0
bl		3,2	47.6
S2		3,2	47.7

Ebl of Fronde

S2		3,4	47.5
bl		3,5	47.4
4		3,3	47.6
b		3,0	47.9
4		3,0	47.9
bl		3,2	47.7
n2		3,2	47.7

50.92

E 1/4 of Section 21

N2	31	47.8
bl	31	47.8
4	31	47.8
6	31	47.8
5	33	47.6
bl	33	47.6
S2	34	47.5

Center of Section 21

S2	34	47.5
bl	34	47.5
4	34	47.5
6	31	47.7
4	33	47.6
bl	31	47.7
N2	33	47.6

50.92

W 1/2 of Section 21

N2	39	47.0
bl	39	47.0
4	38	47.1
6	36	47.3
4	38	47.1
bl	38	47.1
S2	39	47.0

W bk of Section 21

S2	44	46.5
bl	45	46.4
4	39	47.0
6	40	46.9
4	43	46.6
bl	43	46.6
S2	45	46.4

50.92

	Width of	Trench	
N2		4,3	46.6
bl		4,2	46.7
4		4,3	46.6
b		3,9	47.0
4		4,4	46.5
bl		4,9	46.0
S2		4,60	46,2 Bm Sw Trench

	Sw	W 4	Trench	
S2			6,6	44.3
bl			6,0	44.9
4			6,0	44.9
b			5,6	45.3
4			5,8	45.1
bl			5,7	45.2
N2			5,6	45.3
TP	1,03	44,72	7,23	43,69

44.72

	W 4	Trench	
N2		1,4	43.3
bl		1,4	43.3
4		1,4	43.3
b		1,0	43.7
4		1,3	43.4
bl		1,5	43,2
S2		1,4	43.3

	1,28	W	of	Trench
S2			2,0	42.7
bl			2,2	42.5
4			2,2	42.5
b			2,0	42.7
4			2,4	42.3
bl			2,4	42.3
N2			2,0	42.7

4432

	150'	W J	Zone	
N2			31	41.6
M			3,2	41.5
4			2,9	41.8
6			2,8	41.9
4			3,4	41.6
bh			3,1	41.6
S2			3,0	41.7
	200'	W J	Zone	
S2			4,1	40.6
bh			4,6	40.1
4			4,3	40.4
6			4,3	40.4
4			4,5	40.2
bh			4,6	40.1
N2			4,7	40.0

4432

	250'	W J	Zone	V
N2			6,0	38.7
bh			6,0	38.7
4			6,1	38.6
6			5,5	39.2
4			5,7	39.0
bh			5,3	39.4
S2			5,3	39.4
	300'	W J	Zone	V
S2			7,1	37.6
bh			7,3	37.4
4			7,3	37.4
6			7,2	37.5
4			7,6	37.1
bh			7,5	37.2
N2			7,7	37.0

	350	w/	44.72 Found	
N2			9.0	35.4
bk			9.1	35.6
y			9.0	35.7
b			8.7	36.0
y			9.0	35.7
bk			8.9	35.8
S2			8.8	35.9
	400'	w/	Found	st
S2			9.8	34.9
bk			10.0	34.7
y			10.1	34.5
b			9.9	34.8
y			10.4	34.3
bk			10.4	34.3
N2			10.5	34.2
TP	1.72	36.41	10.03	34.69

	450'	w/	36.41 Found	st
N2			3.0	33.4
bk			3.1	33.3
y			3.0	33.4
b			2.5	33.9
y			2.7	33.7
bk			2.5	33.9
S2			2.5	33.9
	500'	w/	Found	st
S2			2.5	33.9
bk			3.0	33.4
y			3.1	33.3
b			3.1	33.3
y			3.7	32.7
bk			3.6	32.8
N2			3.8	32.6

3641

	550	W of	Franck	11-
NL			4,2	32.2
bk			4,3	32.1
4			4,3	32.1
6			3,9	32.5
4			3,8	32.6
bk			3,6	32.8
SL			3,4	33.0
	6 00	W of	Eckerin	Eben 20 (60)
SL			4,5	31.9
bk			4,5	31.9
4			4,8	31.6
6			4,7	31.7
4			4,9	31.5
bk			5,0	31.4
NL			4,9	31.5

3641

	Ebk	of	Eben	11
NL			5,0	31.4
bk			5,0	31.4
4			5,2	31.2
6			4,9	31.5
4			5,2	31.2
bk			4,8	31.6
SL			4,5	31.9
	E 1/4	of	Eben	
SL			5-0	31.4
bk			5,0	31.4
4			5,0	31.4
6			5-0	31.4
4			5-0	31.4
bk			5-1	31.3
NL			5,2	31.2

3641

Center of Eben

N2	4,9	31.5
bk	4,8	31.6
4	5,0	31.4
6	4,9	31.5
4	5,0	31.4
bk	4,8	31.6
S2	4,8	31.6

W¼ of Eben

S2	5,2	31.2
bk	5,1	31.3
4	5,1	31.3
6	5,0	31.4
4	5,2	31.2
bk	5,0	31.4
N2	5,1	31.3

3641 Muir

Wbk of Eben

N2	5,5	30.9
bk	5,7	30.7
4	5,9	30.5
6	5,2	31.1
4	5,6	30.8
bk	5,2	31.2
S2	5,2	31.2

N2 of Eben

S2	5,25	31.16 BM SW Eben
bk	5,2	31.1
4	5,5	30.9
6	5,2	31.2 x
4	5,5	30.9
bk	5,2	31.1
N2	5,5	30.9

36411

	50'	W	of Elev	
N2			6,0	30.4
bk			5,9	30.5
4			5,8	30.6
6			5,6	30.8
4			6,0	30.4
bk			5,8	30.6
S2			5,7	30.7

	100'	W of	Elev	
S2			6,1	30.3
bk			5,9	30.5
4			6,1	30.3
6			5,9	30.5
4			6,4	30.0
bk			6,3	30.1
N2			6.1	30.3
TP	2,07	32,80	5,68	30,73

32810

	150'	W of	Elev	
N2			2,9	29.9
bk			3,3	29.5
4			3,3	29.5
6			3,0	29.8
4			3,1	29.7
bk			3,3	29.5
S2			3,1	29.7

	200'	W of	Elev	
S2			3,6	29.2
bk			3,6	29.2
4			3,8	29.0
6			3,6	29.2
4			3,7	29.1
bk			3,8	29.0
N2			3,7	29.1

3280

	250'	W J	Eben	2t
N2			4,2	28.6
bb'			4,3	28.5
y			4,4	28.4
b			4,1	28.7
y			4,5	28.3
bb			4,3	28.5
S2			4,1	28.7

	300'	W J	Eben	2t.
S2			4,7	28.1
bb			4,7	28.1
y			4,7	28.1
b			4,6	28.2
y			4,7	28.1
bb			4,6	28.2
N2			4,8	28.0

3280

	350	W J	Eben	2t
N2			5,1	27.7
bb			5,2	27.6
y			5,0	27.8
b			4,9	27.9
y			5,1	27.7
bb			4,9	27.9
S2			5.0	27.8

	400'	W J	Eben	2t
S2			5,5	27.3
bb			5,1	27.7
y			5,4	27.4
b			5,2	27.6
y			5,5	27.3
bb			5,2	27.6
N2			5,5	27,3

3280

	450	W f	Eben	st
N2			5,7	27.1
bh			5,5	27.3
4			5,8	27.0
b			5,4	27.4
4			5,7	27.1
bh			5,7	27.1
S2			5,7	27.1
	500'	W f	Eben	st
S2			5,7	27.1
bh			5,7	27.1
4			6,2	26.6
b			5,8	27.0
4			6,1	26.7
h			6,0	26.8
N2			6,2	26.6
TP	3,14	3014	5,80	27,00

3014

	550	W f	Eben	st
N2			3,7	26.4
bh			3,6	26.5
4			3,6	26.5
b			3,2	26.9
4			3,5	26.6
h			3,5	26.6
S2			3,4	26.7
4	600'	W =	Eben	st 2. Tür
S2			4,0	26.1
bh			3,9	26.2
4			3,9	26.2
b			3,7	26.4
4			3,9	26.2
bh			4,0	26.1
N2			4,0	26.1

3014

E bb of Q Sec

N2		4.0	26.1
bb		3.9	26.2
"		4.0	26.1
bb		3.8	26.3
"		4.2	25.8
bb		3.8	26.3
S2		4.0	26.1

E 1/4 of Q Sec

S2		4.0	26.1
bb		4.0	26.1
"		4.0	26.1
"		4.0	26.1
"		4.0	26.1
bb		4.0	26.1
N2		4.0	26.1

3014

Center of Q Sec

N2		4.1	26.0
bb		4.1	26.0
"		4.1	26.0
bb		4.0	26.1
"		4.0	26.1
bb		3.9	26.2
S2		3.8	26.3

W 1/4 of Q Sec

S2		4.2	25.9
bb		4.4	25.7
"		4.3	25.8
bb		4.3	25.8
"		4.4	25.7
bb		4.4	25.7
N2		4.4	25.7

30.14

	Wlch f	Qu Zoe	
n2		4,3	25.8
bl		4,4	25.7
y		4,8	25.3
b		4,5	25.6
y		4,6	25.5
bl		4,4	25,7
s2		4,4	25,7

	Wlin f	Qu Zoe w	
s2		4,35	25.79 x
bl		4,4	25.7
y		4,3	25.8
l		4,7	25.9 x
y		4,5	25.6
bl		4,4	25.7
n2		4,3	25.8

30.14

	50'	W b	Qu Zoe st	
n2			4,8	25.3
bl			4,9	25.2
y			4,9	25.2
bl			4,7	25.4
y			4,9	25.2
bl			4,6	25.5
s2			4,8	25.3

	100	w b	Qu Zoe st	
s2			5,5	24.6
bl			5,4	24.7
y			5,4	24.7
l			5,2	24.9
y			5,5	24.6
bl			5,3	24.8
n2			5,4	24.7

3014

	130'	N T	De Zn	ST
N2			5.9	24.2
bl			5.9	24.2
4			6.0	24.1
6			5.7	24.4
4			6.2	23.9
bl			5.9	24.2
S2			5.9	24.2
	200'	N T	De Zn	ST
S2			6.5	23.6
bl			6.8	23.3
4			6.7	23.4
6			6.5	23.6
4			6.6	23.5
bl			6.7	23.4
N2			6.5	23.6
TP	209	26.08	6.15	23.99

2608

	250'	N T	De Zn	ST
N2			3.3	22.8
bl			3.1	23.0
4			3.3	22.8
6			3.0	23.1
4			3.3	22.8
bl			3.1	23.0
S2			3.0	23.1
	300'	N T	De Zn	
S2			3.9	22.2
bl			4.0	22.1
4			4.2	21.9
6			3.8	22.3
4			4.1	22.0
bl			3.9	22.2
N2			3.8	22.3

2608

	350	wf	De Tau	
N2			4,6	21.5
bl			4,8	21.3
y			4,8	21.3
l			4,4	21.7
y			4,6	21.5
bl			4,6	21.5
S2			4,8	21.3
	400	wf	De Tau	
S2			5,3	20.6
bl			5,5	20.6
y			5,5	20.6
l			5,3	20.8
y			5,7	20.4
bl			5,5	20.6
N2			5,3	20.8

2608

	450	wf	De Tau	
N2			6,3	19.8
bl			6,3	19.8
y			6,5	19.6
l			6,2	19.9
y			6,4	19.7
bl			6,6	19.5
S2			6,5	19.6
	500	wf	De Tau	
S2			7,3	18.8
bl			7,0	19.1
y			7,3	18.8
l			7,1	19.0
y			7,4	18.7
bl			7,3	18.8
N2			7,2	18.9
TP	1,85	2108	6,85	19,23

21.08

	550	n f	De Zon	so
N2			29	18.2
bl			3,1	18.0
y			3,2	17.9
b			3,0	18.1
y			3,3	17.8
bl			3,3	17.8
S2			3,3	17.8

6vó n = Ezin f bobb ss (60)

S2			4,3	16.8
bl			4,1	17.0
y			4,3	16.8
b			3,9	17.2
y			4,0	17.1
bl			4,0	17.1
N2			4,0	17.1

21.08

Mint

Ebl f bobb

N2			4,1	17.0
bl			4,3	16.8
y			4,3	16.8
b			4,1	17.0
y			4,5	16.4
bl			4,4	16.7
S2			4,1	17.0

E ½ f bobb it

S2			4,5	16.6
bl			4,5	16.6
y			4,3	16.8
b			4,2	16.9
y			4,3	16.8
bl			4,2	16.9
N2			4,2	16.9

21.08

	Center of	Cable at	
N2		4,3	16.8
bb		4,2	16.9
y		4,3	16.8
b		4,4	16.7
y		4,5	16.6
bb		4,4	16.7
S2		4,5	16.6
	W. ¼ of	Cable at	
S2		4,6	16.5
bb		4,7	16.4
y		4,8	16.3
b		4,7	16.4
y		4,7	16.4
bb		4,6	16.5
N2		4,7	16.4

21.08

	W bb of	Cable at		
N2		4,6	16.5	
bb		4,8	16.3	
y		5,2	15.9	
b		4,9	16.2	
y		4,9	16.2	
bb		4,6	16.5	
S2		4,9	16.2	
	W line of	Cable at		
S2		4,87	16.21	BM SW cable
bb		4,9	16.2	
y		5,2	15.9	
b		4,9	16.2	
y		5,0	16.1	
bb		4,8	16.3	
N2		4,8	16.3	

2108

	50'	w b	babb	
N2			5.3	15.6
bk			5.4	15.7
y			5.5	15.6
b			5.4	15.7
y			5.7	15.4
bk			5.4	15.7
S2			5.7	15.4

	100'	w b	babb	
S2			6.3	14.8
bk			6.3	14.8
y			6.4	14.7
b			6.1	15.0
y			6.2	14.9
bk			6.2	14.8
N2			6.0	15.1

2108

	150'	w y	babb	at
N2			6.7	14.4
bk			7.0	14.1
y			7.0	14.1
b			6.7	14.4
y			7.2	13.9
bk			7.2	13.9
S2			6.8	14.3

	200'	W of	babb	at
S2			7.8	13.3
bk			7.8	13.3
y			7.5	13.6
b			7.4	13.7
y			7.7	13.4
bk			7.5	13.6
N2			7.5	13.6
TP	2.53	16.57	7.04	14.04

1657

	250'	w	bobb	st
N2			3,7	12.9
bb			3,7	12.9
4			4,0	12.6
b			3,8	12.8
4			3,8	12.8
bb			4,0	12.6
S2			4,2	12.4
	300'	w f	bobb	st
S2			4,4	12.2
bb			4,5	12.1
4			4,5	12.1
b			4,3	12.3
4			4,5	12.1
bb			4,4	12.2
N2			4,4	12.2

1657

	350'	w f	bobb	st
N2			4,9	11.7
bb			4,9	11.7
4			4,8	11.8
b			4,5	12.1
4			5,0	11.6
bb			5,1	11.5
S2			5,0	11.6
	400'	w f	bobb	st
S2			5,5	11.1
bb			5,7	10.9
4			5,5	11.1
b			5,4	11.2
4			5,4	11.2
bb			5,4	11.2
N2			5,3	11.3

1657

	4150	n of	Cable at
M2		6,1	10.5
bl		6,1	10.5
4		6,2	10.4
b		6,0	10.6
4		6,2	10.4
bl		6,2	10.4
S2		6,1	10.5
	3-01'	n = N P Lin of P2 205	Bm
S2		7,12	9.45
bl		7,0	9.6
4		6,7	9.9
b		6,6	10.0
4		6,8	9.8
bl		7,0	9.6
M2		6,8	9.8

Construction of Mound (50')

Blough Donor Pedigo

E Lin of P2 205 to W2 Guyot

	9,04	5-5.16	46.2

Br SW 4 Tranda

E Lin of P2 205 = 97' E of Tranda at

S2	4,6	√0.6
bl	4,7	50.5
4	4,9	50.3
b	5,0	√0.2
4	5,6	49.6
bl	6,0	49.2
M2	6,4	48.8

53' E of P Lin

M2	5,6	49.6
bl	5,2	50.0
4	4,7	50.5
b	4,2	√1.0
4	4,6	50.6
bl	4,3	50.9
S2	4,2	√1.0

Pipe 4" 2 Ins. 9-18-57 Path 10

	103	Ef	P lin		✓
S2			3,3	√1.9	
bh			3,6	51.6	
y			3,8	51.4	
b			3,6	√1.6	
y			4,3	50.9	
bl			4,4	50.8	
n2			4,8	√0.4	

	153	Ef	P2		✓
n2			3,0	√2.2	
bh			2,6	52.6	
y			2,7	52.5	
b			2,1	√3.1	
y			2,3	52.9	
bl			2,0	53.√	
S2			2,0	√3.2	
I.P	1209	6686	0,39	54,77	

6686

	203	Ef	P2		✓
S2			11,7	√√.2	
bl			12,0	54.9	
y			12,2	54.7	
b			12,0	√4.9	
y			12,6	54.3	
bh			12,9	54.0	
n2			13,1	√3.8	

	253	Ef	P2		✓
n2			11,6	√√.3	
bh			11,0	55.9	
y			10,5	56.4	
b			10,1	√6.8	
y			10,0	56.9	
bl			9,8	57.1	
S2			9,5	√7.4	

6686

	303'	E 6	P2		
S2			6,6	60.3	✓
bb			7,0	59.9	
y			7,1	59.8	
b			7,2	59.7	
y			7,4	59.3	
bb			7,5	59.4	
N2			8,1	✓8.8	

✓ 4+30

	353'	E 7	P2		
N2			4,5	62.4	
bb			4,3	62.6	
y			4,1	62.8	
b			3,5	63.4	
y			3,7	63.2	
bb			3,4	63.5	
S2			3,1	63.8	
TP	12,72	7933	0,25	66,1	

7933

	403'	E 6	P2		
S2			11,0	68.3	
bb			11,3	68.0	
y			11,9	67.4	
b			12,0	67.3	
y			12,4	66,9	
bb			12,5	66,8	
N2			12,6	66.7	

5+00

	453'	E 7	P2		
N2			8,1	71.2	
bb			7,7	71.6	
y			7,7	71.6	
b			7,2	72.1	
y			7,1	72.2	
bb			7,0	72.3	
S2			6,3	73.0	

5+50

79.33

503' E = W Line of Guyot at 6+00

SL		1,4	77.9
bk		1,5	77.8
y		1,9	77.4
b		2,1	77.2
y		2,7	76.6
bk		2,9	76.4
NL		3,1	76.2
TP	1293	9166	0,60	7873

Cross section of Long Branch St (58) 58
NL of Guyot to WL of PL 205

91.66

WL of ~~Guyot~~ Guyot

SL		0,2	91.5
bk		0,0	91.7
y		0,1	91.0
b		0,9	90.8
y		1,4	90.3
bk		1,2	90.6
NL		2,0	89.7

50 W of Guyot

NL		5,4	86.3
bk		5,0	86.7
y		5,5	86.2
b		5,2	86.5
y		4,6	87.1
bk		4,6	87.1
SL		4,6	87.1

9.66

	100'	WT	Guiyot	
SL			9,2	82.5
bh			9,6	82.1
4			10,5	81.2
6			10,2	81.5
4			10,6	81.1
bh			10,7	81.0
NL			10,7	81.0
TP	0,81	82,39	10,08	81,58

	150'	WT	Guiyot	
NL			7,1	76.3
bh			6,1	76.3
4			5,9	76.5
6			5,6	76.8
4			5,6	76.8
bh			4,3	78.1
SL			3,8	78.6

82.39

Long Branch

	200'	WT	Guiyot	
SL			8,2	74.2
bh			8,5	73.9
4			9,2	73.2
6			9,1	73.3
4			9,8	72.6
bh			9,4	73.0
NL			9,4	73,0
TP	0,92	73,05	10,26	72,13

	250'	WT	Guiyot	
NL			5,1	68.0
bh			4,7	68.4
4			4,6	68.5
6			3,9	69.2
4			4,1	69.0
bh			3,8	69.3
SL			3,3	69.8

7305

	300	w f	Gunyat	
S2			7,4	65.7
bh			7,7	65.4
y			8,2	64.9
b			7,9	65.2
y			8,7	64.4
bh			8,6	64.5
m2			8,9	64.2
	350	w f	Gunyat	
m2			12,3	60.8
bh			12,0	61.1
y			11,7	61.4
b			11,1	62.0
y			11,3	61.8
bh			11,2	61.9
S2			11,0	62.1
TP	022	6148	11,79	61,26

6148

	400	w f	Gunyat	
S2			1,9	59.6
bh			1,9	59.6
y			2,2	59.3
b			2,0	59.5
y			2,7	58.8
bh			2,9	58.6
m2			3,2	58.3
	450	w f	Gunyat	
m2			4,9	56.6
bh			4,8	56.7
y			4,7	56.8
b			4,1	57.4
y			4,1	57.4
bh			4,0	57.5
S2			37	57.8

6148

503 w = E L-f Pd 205

S2		5-4	√6.1
th		5,6	√5.9
y		5-7	√5.8
l		5-9	√√.6
y		6,4	√5.1
th		6,3	√5.√
n2		6,6	√4.9

5-50 w f Guigat

n2		8,6	√2.9
th		8,3	√3.√
y		8,3	√3.√
l		8,0	√3.√
y		7,8	√3.7
th		7,6	√3.9
S2		7,4	√4.1

6148

Long Branch

600 w = E Lin f Froude et (60)

S2		9,0	√2.√
th		9,3	√√.5
y		9,6	√1.9
l		9,8	√1.7
y		10,0	√1.5
th		10,0	√1.5
n2		10,2	√1.3

E th f Froude et

n2		10,4	√1.1
th		10,6	√1.5
y		10,4	√1.1
l		10,1	√1.4
y		9,6	√1.9
th		9,5	√√.0
S2		9,2	√2.3

61.48

E ½ of Found

BL	9,6	↓1.9
bl	9,8	↑1.7
y	9,9	↑1.6
b	10,0	↓1.7
y	10,5	↑1.0
bl	10,8	↑0.7
RL	11,2	↓0.3

Center of Found

RL	11,4	↓0.1
bl	11,5	↑0.3
y	11,1	↑0.7
b	10,8	↓0.7
y	10,4	↑1.1
bl	10,1	↑1.4
SL	9,7	↓1.8

61.48

Long Branch

W ½ of Found

SL	10,3	↓1.2
bl	10,5	↑1.0
y	10,6	↑0.9
b	10,8	↓0.7
y	11,2	↑0.3
bl	11,6	↓0.9
RL	11,7	49.8

W bl of Found

RL	12,0	49.↓
bl	11,8	↓0.1
y	11,6	↓0.9
b	11,2	↓0.3
y	10,9	↑0.6
bl	10,8	↑0.7
SL	10,4	↓1.1

10,60

Long Branch

L1.48

	W Line of	Trough		Bm sm Trough
SR		10.0	50.8	
bk		10.8	50.7	
y		11.4	50.1	
b		11.4	↓0.1	
y		11.8	↓9.7	
bk		12.0	↓9.5	
NR		12.2	49.3	
TP	2.70	5358	11.60	50.8 ↓

5358

	50' W of	Trough st	
NR		3.2	48.4
bk		3.1	↓8.5
y		4.7	↓8.9
b		4.4	49.2
y		4.2	↓9.2
bk		3.8	↓9.8
SR		3.6	↑0.0

5358

	100 W of	Trough st	
SR		4.0	49.6
bk		4.5	↓9.1
y		5.0	↓8.6
b		5.0	48.6
y		5.3	↓8.7
bk		5.2	↓8.7
NR		5.4	48.2

	150 W of	Trough st	
NR		6.6	47.0
bk		6.3	↓7.3
y		6.6	↓7.0
b		6.0	47.6
y		5.8	↓7.8
bk		5.5	↓8.1
SR		5.2	48.4

5358

	200'	W of	Loads at	
S2			6.6	47.0
bk			7.0	46.6
"			7.5	46.1
l			7.5	46.1
"			8.0	45.6
bk			8.0	45.6
N2			8.1	45.5

	250'	W of	Loads at	
N2			9.8	43.8
bk			9.2	44.4
"			9.2	44.4
l			8.6	45.0
"			8.5	45.1
bk			8.2	45.4
S2			7.8	45.8

5358

	300'	W of	Loads at	
S2			9.0	44.6
bk			9.2	44.4
"			9.6	44.0
l			9.7	43.9
"			10.3	43.3
bk			10.3	43.3
N2			10.8	42.8
TP	180	45.07	10.31	43.27

	350'	W of	Loads at	
N2			3.1	42.0
bk			3.1	42.0
"			2.8	42.3
l			2.5	42.6
"			2.4	42.7
bk			2.3	42.8
S2			2.2	42.9

45.07

	460	w/	Froude #	
SL			4.1	41.0
BL			4.1	41.0
Y			4.2	40.9
L			4.0	41.1
Y			4.5	40.6
BL			4.4	40.7
SL			4.1	40.7

	450	w/	Froude	
SL			6.0	39.1
BL			6.5	38.6
Y			6.5	38.6
L			6.2	38.9
Y			6.2	38.9
BL			5.8	39.3
SL			6.2	38.9

45.04

	550	w/	Froude	
SL			8.2	36.9
BL			8.5	36.6
Y			8.4	36.7
L			8.0	37.1
Y			8.4	36.7
BL			8.2	36.9
SL			8.2	36.9

	550	w/	Froude #	
SL			10.2	34.9
BL			10.4	34.7
Y			10.4	34.7
L			10.1	35.0
Y			10.4	34.7
BL			10.2	34.9
SL			10.3	34.8
TP	164	3689	9.8	35.25

3689

600 W = E Line of Eben St (60)

S2	3,7	33.7
4	3,5	33.4
4	3,9	33.0
4	3,6	33.3
4	3,9	33.0
4	3,7	33.2
N2	3,8	33.1

E 4 of Eben St

N2	4,0	32.9
4	3,9	33.0
4	4,2	32.7
4	3,9	33.0
4	4,0	32.9
4	3,8	33.1
S2	3,4	33.5

3689

E 1/4 of Eben St

S2	4,0	32.9
4	4,0	32.9
4	4,0	32.9
4	4,1	32.8
4	4,1	32.8
4	4,2	32.7
N2	4,2	32.7

Center of Eben St

N2	4,2	32.7
4	4,1	32.8
4	4,1	32.8
4	4,1	32.8
4	4,0	32.9
4	3,9	33.0
S2	3,7	33.2

Army Branch

3689

	W'ly of	Elev	St
SL		4,1	32.8
bk		4,2	34.7
"		4,3	34.6
L		4,3	32.6
"		4,5	34.1
bk		4,6	34.3
NL		4,6	32.3
	W bk of	Elev	St
NL		4,4	32.2
bk		4,8	34.1
"		5,0	31.9
L		4,6	32.3
"		4,4	34.5
bk		4,2	34.7
SL		4,1	32.8

3689

	N bk of	Elev	St	Long Branch S W ± Elev St
SL		4,30	32.9	
bk		4,4	34.5	
"		4,7	34.7	
L		4,5	32.4	
"		4,8	34.1	
bk		4,8	34.1	
NL		4,8	32.1	
	50' W of	Elev	St	
NL		5,3	31.6	
bk		5,2	31.7	
"		5,2	31.7	
L		4,9	32,0	
"		5,0	31.9	
bk		4,8	34.1	
SL		4,7	32.2	

3689

	100'	W of	Elev	ft
SL			5.5	31.4
bk			5.6	31.3
y			6.0	30.9
l			5.6	31.3
y			5.9	31.0
bk			5.9	31.0
NL			5.8	31.1

	150'	W of	Elev	ft
NL			6.7	30.2
bk			6.7	30.7
y			6.8	30.1
l			6.6	30.3
y			6.7	30.7
bk			6.6	30.3
SL			6.7	30.2

3689

	200'	W of	Elev	ft
SL			7.0	29.9
bk			7.4	29.5
y			7.4	29.5
l			7.4	29.5
y			7.6	29.3
bk			7.6	29.3
NL			7.3	29.6

Set mag. S Side

TP	336	332	6.28	29.91

	250'	W of	Elev	ft
NL			4.1	29.2
bk			4.2	29.1
y			4.2	29.1
l			4.1	29.2
y			4.1	29.2
bk			4.1	29.2
SL			4.1	29.2

3327

	300'	W of S	Elev	ft
S2			45	28.8
"			45	W8.8
"			45	W8.8
"			44	28.9
"			44	W8.9
"			41	W9.V
N2			43	29.0

	350'	W of S	Elev	ft
N2			46	28.7
"			46	W8.7
"			48	W8.5
"			45	28.8
"			47	W8.6
"			45	W8.8
S2			46	28.7

3327

	400'	W of S	Elev	ft
S2			46	28.7
"			46	W8.7
"			47	W8.6
"			44	28.9
"			48	W8.5
"			48	W8.5
N2			47	28.6

	450'	W of S	Elev	ft
N2			48	28.V
"			48	W8.5
"			50	W8.3
"			49	28.4
"			49	W8.V
"			50	W8.3
S2			50	28.3

3377

500' N of Elm St

SR			5.0	28.3
"			5.0	28.3
"			4.8	28.5
"			4.7	28.6
"			5.0	28.3
"			5.2	28.1
NR			5.2	28.1

550 N of Elm St

NR			5.5	27.8
"			5.5	27.8
"			5.3	28.0
"			5.1	28.2
"			5.4	27.9
"			5.5	27.8
SR			5.5	27.8
TP	193	2905	615	27.2

BM SE Elm St

2905

600' N of SR & Dr Fm St

SR	2.0	27.1
"	2.0	27.1
"	1.8	27.3
"	1.9	27.2
"	1.9	27.2
"	2.0	27.1
NR	2.0	27.1

Ebb & Dr Fm St

NR	2.0	27.1
"	1.9	27.2
"	2.1	27.0
"	2.1	27.0
"	2.3	26.8
"	2.0	27.1
SR	2.2	26.9

Long Branch

2905

E ½ of De Zon 21

SE	21	27.0
ll	22	26.9
y	21	27.0
l	21	27.0
y	20	27.1
ll	21	27.0
NE	21	27.0

Center of De Zon 21

NE	19	27.2
ll	20	27.1
y	23	26.8
l	22	26.9
y	21	27.0
ll	22	26.9
SE	23	26.8

2905

Long Branch

E ½ of De Zon

SE	25	26.6
ll	25	26.6
y	25	26.6
l	25	26.6
y	25	26.6
ll	25	26.6
NE	25	26.6

E ll of De Zon

NE	27	26.4
ll	27	26.4
y	30	26.1
l	27	26.4
y	28	26.3
ll	26	26.5
SE	26	26.5

2905

	W Line	Qu Tur	Yt
S2		2.8	26.3
11		2.5	26.6
4		2.9	26.7
1		2.8	26.3
4		3.1	26.0
11		2.8	26.3
N2		3.0	26.1
	50 W	Qu Tur	Yt
N2		36	25.5
11		35	25.6
4		38	25.3
1		34	25.7
4		3.8	26.3
11		3.6	25.5
S2		3.6	25.5

2905

	100	W	Qu Tur	Yt
S2			4.2	24.9
11			4.3	26.8
4			4.5	26.6
1			4.3	24.8
4			4.4	26.7
11			4.1	25.0
N2			4.5	24.6
	150	W	Qu Tur	Yt
N2			4.8	24.3
11			5.1	26.0
4			5.0	26.1
1			4.7	24.4
4			5.0	26.1
11			5.0	26.1
S2			5.1	24.0

Tony Bunch

2905

	300	2.5	Dens	st
S2			7.0	22.1
bl			6.7	22.2
y			6.7	22.2
g			6.7	22.4
y			6.7	22.2
bl			6.8	22.2
R2			6.4	22.7
	330	2.5	Dens	st
R2			7.5	21.6
bl			7.5	21.6
y			7.5	21.6
g			7.6	21.5
y			7.7	21.6
bl			7.6	21.6
S2			7.7	21.4
TP	0.75	2137	8.43	2062

2905

	200	2.5	Dens	st
S2			5.7	23.4
bl			5.6	23.4
y			5.5	23.6
g			5.6	23.5
y			5.6	23.6
bl			5.4	23.6
R2			5.6	23.5
	250	2.5	Dens	st
R2			6.1	23.0
bl			6.1	23.0
y			6.1	23.0
g			6.0	23.1
y			6.1	23.0
bl			6.1	23.0
S2			3.8	23.3

2137

	400'	W of	De Zu	21
SR			1.1	20.3
h			1.1	20.3
4			1,0	20.4
6			1,0	20,4
4			1,0	20.4
66			0,9	20.5
72			1,0	20,4

	450	W of	De Zu	21
72			1,7	19.7
66			1,8	19.6
4			1,9	19.5
6			1,8	19.6
4			2,0	19.4
66			2,2	19.2
52			2,2	19.2

2137

	500	W of	De Zu	21
SR			3.0	18.4
h			3.0	18.4
4			2,9	18.5
6			3.0	18.4
4			2,8	18.6
66			2,9	18.5
72			2,9	18.5

	350	W of	De Zu	21
72			4,0	17.4
66			3,9	17.5
4			4.0	17.4
6			3,8	17.6
4			4.0	17.4
66			4,2	17.2
52			4,1	17.3

2137

	600'	N =	E Sin of Cable at (60)	
S2			5-4	16.0
bk			5-3	16.1
4			5-3	16.1
L			5-0	16.4
4			5-2	16.2
bk			5-0	16.4
N2			4-9	16.5
	E bk of		Cable at	
N2			5-1	16.3
bk			5-1	16.3
4			5-3	16.1
L			5-4	16.0
4			5-2	15.8
bk			5-4	16.0
S2			5-5	15.9

2137

	E ¼	of	Cable at	
S2			5-4	15.7
bk			5-6	15.8
4			5-7	15.7
L			5-5	15.9
4			5-4	16.0
bk			5-4	16.0
N2			5-4	16.0
	Center of		Cable at	
N2			5-4	16.0
bk			5-5	15.9
4			5-2	15.8
L			5-2	15.8
4			5-6	15.8
bk			5-6	15.8
S2			5-6	15.8

2137

W¼ of bobb

S2	6.1	15.3
bb	5.9	15.5
4	5.8	15.6
5	5.9	15.5
4	5.8	15.6
bb	5.9	15.5
N2	5.8	15.6

W bb of bobb

N2	6.0	15.4
bb	6.0	15.4
7	6.4	15.0
6	6.2	15.2
4	6.2	15.2
bb	6.0	15.4
S2	6.2	15.2

2137

Long Branch

71

W Sec 4 bobb at

BM SW bobb

S2	6.37	15.00
bb	6.3	15.1
4	6.6	14.8
5	6.2	15.2
4	6.4	15.0
bb	6.2	15.2
N2	6.2	15.2

50' W of bobb at

N2	6.8	14.6
bb	6.8	14.6
7	6.8	14.6
6	6.7	14.7
4	6.8	14.6
bb	6.9	14.5
S2	6.8	14.6

2134

	100'	wf	bobl	
SR			7,6	13.8
bl			7,4	14.0
y			7,5	13.9
b			7,3	14.1
y			7,4	14.0
bl			7,4	14.0
RR			7,4	14.0
	150'	wf	bobl	
RR			8,2	13.2
bl			8,2	13.4
y			81	13.3
b			81	13.3
y			8,3	13.1
bl			8,4	13.0
SR			8,2	13.2
TD	2,45	1497	885	12,52

1497

	200	wf	bobl	
SR			2,8	12.2
bl			2,8	14.2
y			2,7	14.3
b			2,5	12.5
y			2,7	14.3
bl			2,5	14.4
RR			2,5	12.5
	250	wf	bobl	
RR			3,2	11.8
bl			3,3	11.7
y			3,5	11.5
b			3,3	11.7
y			3,4	11.6
bl			3,3	11.7
SR			3,5	11.5

14.97

	300'	wf	bobb	st
S2			4,2	10.8
bl			4,4	10.6
4			4,3	10.7
b			3,9	11.1
4			4,2	10.8
bl			4,1	10.9
N2			4,0	11.0

	350'	wf	bobb	st
N2			4,4	10.6
bl			4,6	10.4
4			4,7	10.3
b			4,5	10.5
4			4,6	10.4
bl			4,6	10.4
S2			4,7	10.3

14.97

	400'	wf	bobb	st
S2			5-2	9.8
bl			5-0	10.0
4			5-1	9.9
b			5-0	10.0
4			5-0	10.0
bl			5-1	9.9
N2			4,7	10.1

	450'	wf	bobb	st
N2			5-4	9.6
bl			5-7	9.3
4			5-7	9.3
b			5-7	9.3
4			5-7	9.3
bl			5-5	9.7
S2			5-8	9.2

1497

5-01' W = W2 P2 2.05

S2		6.5	8.5
1		6.4	8.6
2		6.4	8.6
3		6.4	8.6
4		6.1	8.9
5		6.3	8.7
N2		6.2	8.8
BM		5.5	9.45

P2 is min

Intersection of Franklin st (60') & E L of Brighton

	10.98	6.86	5.88

BM S W door Burnett

Westerly of Brighton st

N2	2.2	9.7
C	1.8	
1/4	2.0	
C	1.5	60.4
1/4	1.7	
C	1.3	
E L	0.9	61.0

50' W Brighton

E L	3.3	8.6
C	3.4	
1/4	4.0	
C	3.7	8.2
1/4	4.1	
C	4.3	
N P	4.3	7.6

E.917

61.86

100' n of Brighton Rt

W R	6.4	√√√
C	6.2	
¼	6.1	
C	5.7	√6.2
¼	5.9	
C	5.5	
E.L.	5.4	√6√

150' n Brighton Rt

E.L.	7.2	√4.7
C	7.4	
¼	7.7	
C	7.8	√4.1
¼	8.1	
C	8.3	
W.L.	8.5	√3.4

61.86

200' n. Brighton Rt.

W.L.	10.5	√1.4
C	10.3	
¼	9.9	
C	9.5	√2.4
¼	9.4	
C	9.9	
E.L.	9.8	√3.1

215 n = N.L. Long Branch (50')

E.L.	9.4	√2.√
C	9.6	
¼	9.9	
C	10.2	√1.7
¼	10.6	
C	10.9	
W.L.	11.0	√0.9
T.P.	3.61	54.49	10.98	50.88

463

N.L. Long Branch St.

W.L.	5.3	49.2	
C	5.0		
¼	4.7		
C	4.6	49.9	
¼	4.2		
C	3.7		
E.L.	3.4	51.1	

50' N. Long Branch.

E.L.	4.6	49.9	
C	4.8		
¼	5.3		
C	5.6	48.9	
¼	5.9		
C	6.2		
W.L	6.5	48.0	

100' N. Long Branch.

W.L.	7.6	46.9	
C	7.3		
¼	6.7		
C	6.2	48.3	
¼	6.1		
C	5.7		
E.L	5.6	48.9	

150' N. Long Branch.

E.L.	6.1	48.4	
C	6.3		
¼	6.7		
C	6.9	47.6	
¼	7.7		
C	7.8		
W.L.	7.9	46.6	

54.49

200' n long Branch

W. L.			8.2	46.3
C			7.6	
¼			7.3	
C			7.0	47.5
¼			7.0	
C			6.8	
E. L.			6.4	48.1

215' n = ℄ Linc Main St. (5-0')

E L			6.7	47.8
C			6.7	
¼			7.0	
C			7.0	47.5
¼			7.6	
C			7.6	46.9
W. L.	5.86	51.94	8.43	46.12 / 46.06

51.98

n. L. main St.

W. L.	5.4	46.6
C	5.2	
¼	5.0	
C	4.2	47.8
¼	4.2	
C	3.8	
E. L.	3.8	48.2

5-0' n. main St.

E. L.	4.5	47.5
C	4.5	
¼	4.6	
C	4.6	47.4
¼	5.3	
C	5.3	
W. L.	5.4	46.6

51.98

100' N. mini Alt

W. L.		5.2	46.8
C		5.4	
1/4		5.4	
C		5.0	47.0
1/4		5.0	
C		5.0	
E. L.		5.0	47.0

150' N. mini Alt.

E. L.		5.3	46.7
C		5.4	
1/4		5.7	
C		5.5	46.5
1/4		5.8	
C		5.9	
W. L.		6.2	45.8

51.98

197.75' N = S.L. Voltaire on East line

W. L.			6.6	45.4
C			6.4	
1/4			6.4	
C			6.0	46.0
1/4			6.3	
C			6.0	
E. L.			6.0	46.0

197.75 on E } = S.L. Voltaire (80 / 92)
202.75 on W }

E. L.			6.0	46.0
C			6.1	
1/4			6.4	
C			6.1	45.9
1/4			6.4	
C			6.7	
W. L.			6.6	45.4
T. P.	4.63	50.01	6.60	45.38

(62.5') North line Voltaire (See Page 1)

E. L.	4.6	4√.4
C	4.5	
¼	5.0	
C	4.9	4√.1
¼	5.4	
C	5.5	
W. L.	5.4	44.2

(60') North line Voltaire W. 15'. N on the E. = 0.0

W L.	5.4	44.2
C	5.6	
¼	5.5	
C	5.0	4√.0
¼	5.0	
C	4.5	
E. L.	4.6	4√.4

50' North Voltaire St

E. L.	4.9	4√.1
C	5.1	
¼	5.4	
C	5.4	44.6
¼	6.0	
C	6.1	
W. L.	6.0	44.0

100' N Voltaire St.

W. L.	6.5	43√
C	6.3	
¼	6.2	
C	5.6	44.4
¼	5.3	
C	5.1	
E. L.	5.1	44.9

50.01

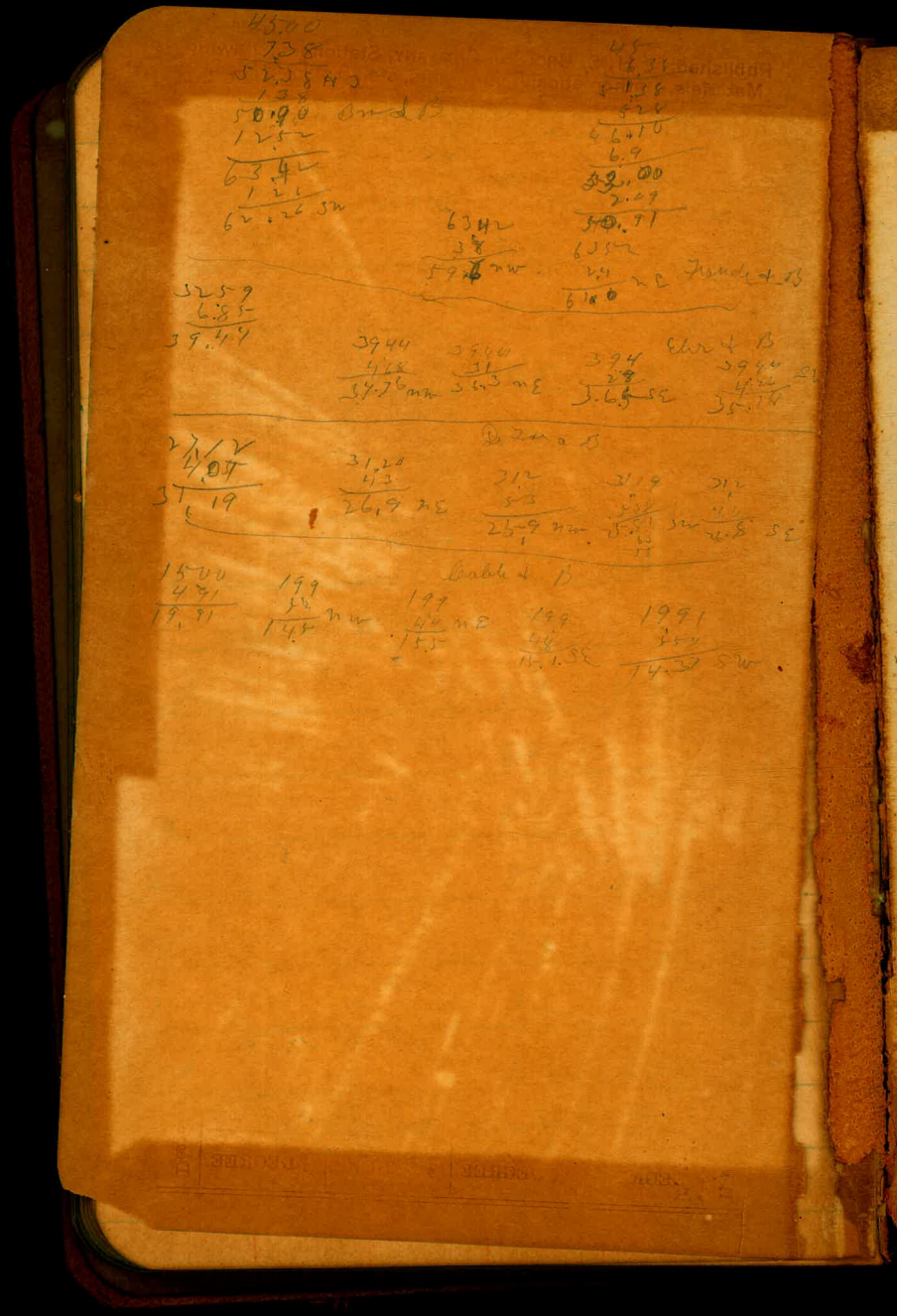
150' n. Voltaire St. #400

E.L.	5.2	44.8
C	5.2	
¼	5.7	
C	5.5	44.5
¼	6.2	
C	6.5	
W.L.	6.7	43.3

200' n. Voltaire St.

W.L.	6.9	43.1
C	6.9	
¼	6.3	
C	5.8	44.2
¼	5.6	
C	5.3	
E.L.	5.1	44.9

Continued Book 464.



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TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100.00	0.44	100.00	0.87	99.99	1.31	89
1	99.98	1.75	99.98	2.18	99.97	2.62	99.95	3.05	88
2	99.94	3.49	99.92	3.93	99.91	4.36	99.88	4.80	87
3	99.86	5.23	99.84	5.67	99.81	6.10	99.79	6.54	86
4	99.76	6.98	99.73	7.41	99.69	7.85	99.66	8.28	85
5	99.62	8.72	99.58	9.15	99.54	9.58	99.50	10.02	84
6	99.45	10.45	99.41	10.89	99.36	11.32	99.31	11.75	83
7	99.25	12.19	99.20	12.62	99.14	13.05	99.09	13.49	82
8	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	15.64	98.70	16.07	98.63	16.50	98.56	16.93	80
10	98.48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98.16	19.08	98.08	19.51	97.99	19.94	97.90	20.36	78
12	97.81	20.79	97.72	21.22	97.63	21.64	97.53	22.07	77
13	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	24.19	96.92	24.62	96.81	25.04	96.70	25.46	75
15	96.59	25.88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.82	73
17	95.63	29.24	95.50	29.65	95.37	30.07	95.24	30.49	72
18	95.11	30.90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35.43	69
21	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38.67	67
23	92.05	39.07	91.88	39.47	91.71	39.87	91.53	40.27	66
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	43.84	89.69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	46.95	88.09	47.33	87.88	47.72	87.67	48.10	61
29	87.46	48.48	87.25	48.86	87.04	49.24	86.82	49.62	60
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	52.99	84.57	53.36	84.34	53.73	84.10	54.10	57
33	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	52
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	45
45	70.71	70.71							

Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees
	DEGREES		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		