563

MINING
TRANSIT BOOK
363

F.B.563

KEUFFEL & ESSER CO.

DRAWING MATERIALS
AND
SURVEYING INSTRUMENTS.

NEW YORK.

CHICAGO. SAN FRANCISCO. ST. LOUIS.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EXCAVATION.

"Copyright, 1895, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MICROFILMED DEC 11 1964

14.1
1.5
1.8.6

Alignment Sisson East to Fairmount

F. B. 563

ENGINEERING DEPARTMENT,
CITY OF EAST SAN DIEGO,
CALIFORNIA.

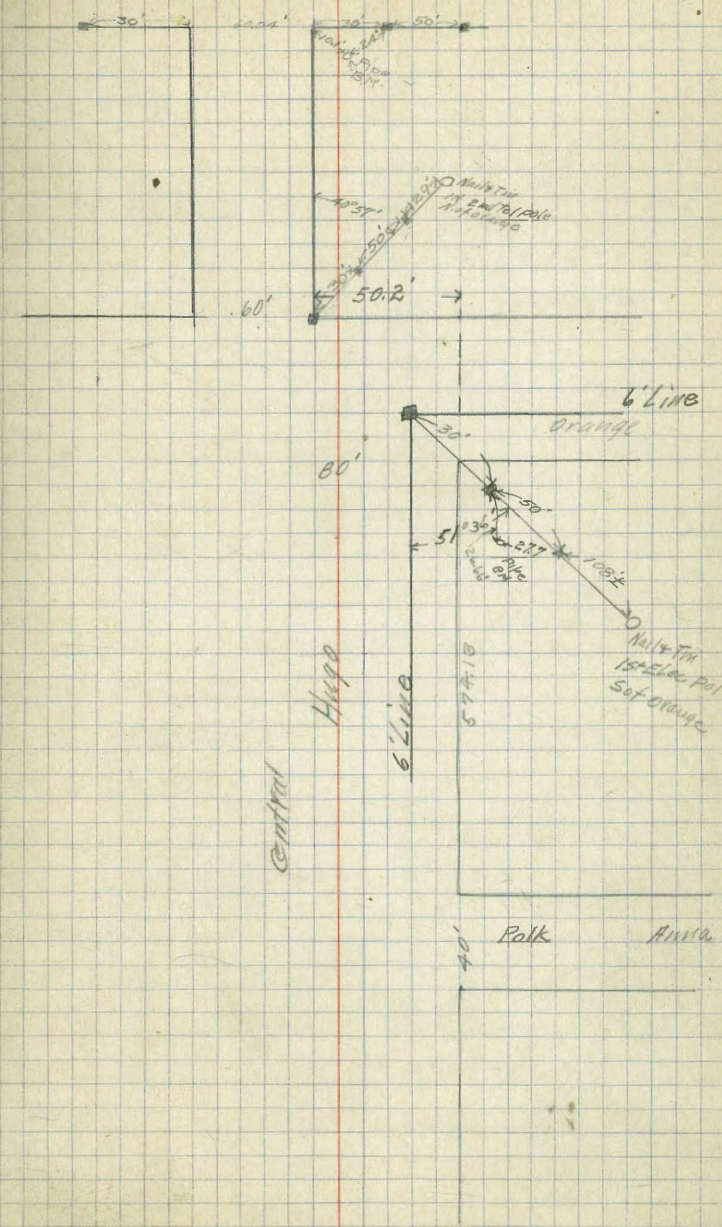
Card Indexed Mar. 21, 1918

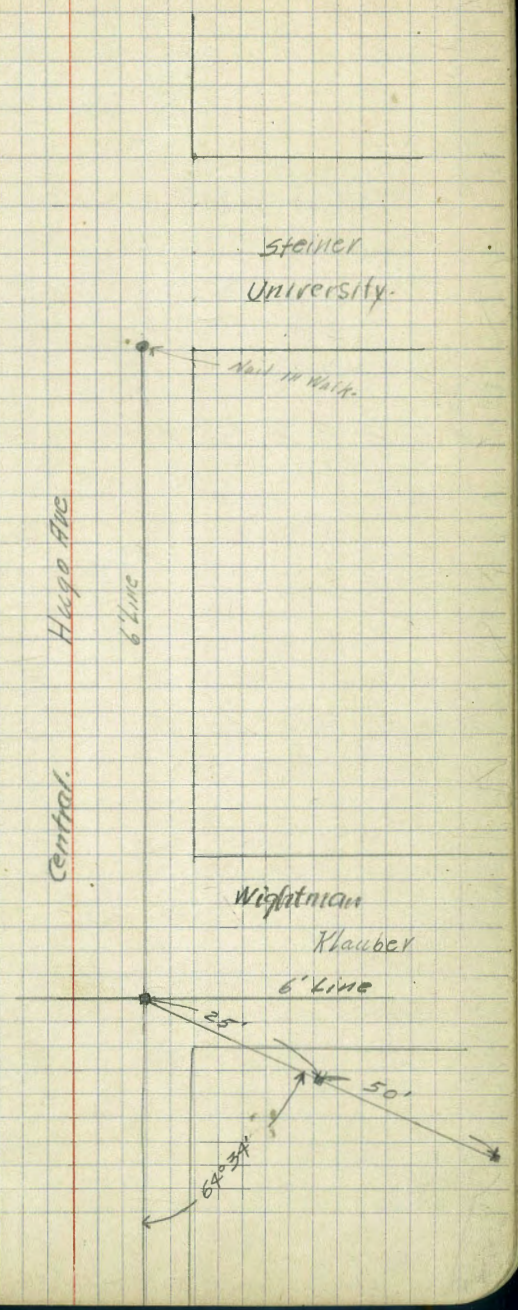
Notes [illegible]
to page 5.

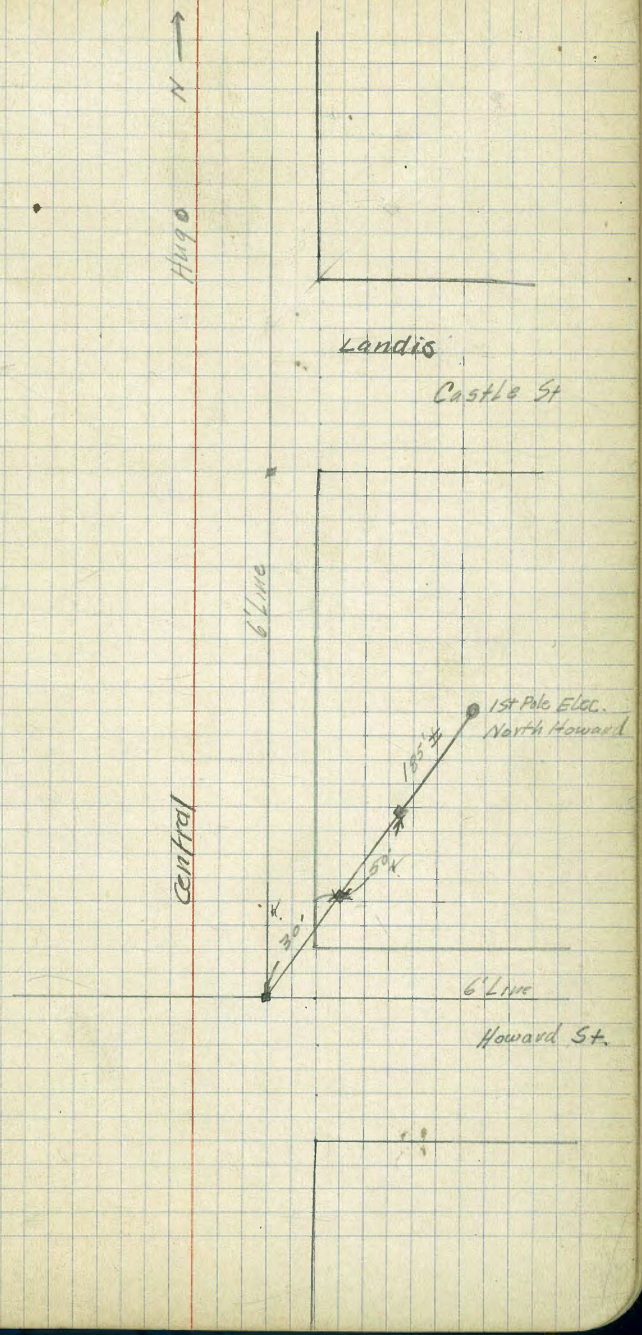
Index.

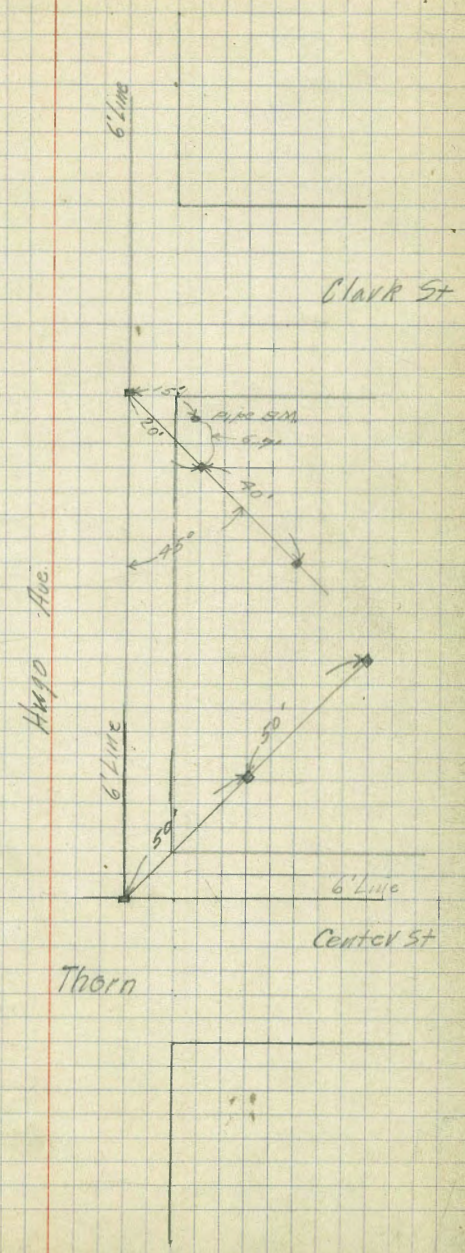
Page
Alignment Central Hugo Av. 1

Ford Hyatt Graf
Dec 18-1915




Steiner
University.
Nail in Walk.
Hugo Ave
6' Line
Central.
Wightman
Klauber
6' Line
25'
50'
64° 34'


N
Hugo
Landis
Castle St
6' Line
Central
1st Pole Elec.
North Howard
6' Line
Howard St.


6' Line
Clark St
15°
Pipe S.M.
20'
40'
45°
Hugo Ave.
6' Line
50'
50'
6' Line
Center St
Thorn

6" Line
Hugo AVE
Redwood
Chatham St
B.M.
Pipe
90°
92.7'
10'
40'
Central

Bench Marks at Carmel Hgths.

Tom J Allen — April 9, 1926.

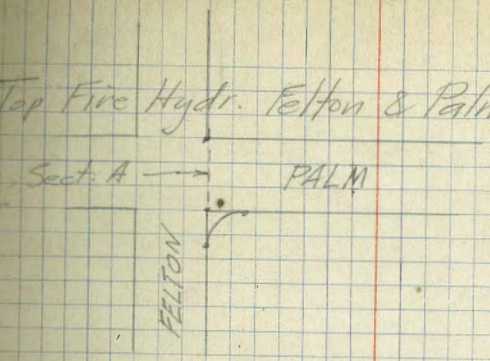
Pacific Building Co

B.M.	313.01	Redwood & Felton - Br Plug N.W. Cor.
B.M.	305.86	Pipe N.W. Lot 4 - BLK A
B.M.	295.45	Pipe N.E Lot 1 BLK C
B.M.	296.65	Pipe N.E Lot 1 BLK D
B.M.	300.66	Lot Stake Lot 1 BLK E
B.M.	299.26	Pipe NE Lot 1 BLK F
B.M.	292.96	Pipe S.W. Lot 12 BLK E
B.M.	289.49	Pipe S.E. Lot 39 BLK F
B.M.	300.71	Pipe S.W Lot 30 BLK F
B.M.	298.36	Top of Fire Hydrant N.E Palm and Felton
B.M.	312.94	Redwood and Felton Br Plug N.W. Cor.

Palm St.

	+		−		
BM.	0.37	308.73		308.36	
	Sect. A N.W. Cor. Lot 26, Bk. F. (PI)				
S ℞			308.7 ~~3.15~~	305.5	✓
Curb			3.60	3051	✓
1/4			3.95	304.7	✓
℄			3.80	3049	✓
1/4			3.70	3050	✓
Curb			3.60	3051	✓
N ℞			3.75	3049	✓
	50' east.				
S ℞			4.70	3040	✓
Curb			6.70	3040	✓
1/4			5.55	3031	✓
℄			5.15	3035	✓
1/4			5.05	3036	✓
Curb			5.40	3033	✓
N ℞			4.50	3044	✓
	50' east N.E. cor. Lot 26, Bk. F				
S ℞			6.80	3019	✓
Curb			9.30	2994	✓
1/4			8.25	3004	✓
℄			8.20	3005	✓
1/4			8.15	3005	✓
Curb			9.10	2996	✓
℞			6.70	3040	✓

Top Fire Hydr. Felton & Palm.



	308.73			
		308.7		
	25' east (middle of Lot 25)			
S ℄		8.40	3063	✓
Curb		11.10	2976	✓
1/4		10.40	2983	✓
℄		10.50	2982	✓
1/4		10.60	2981	✓
Curb		11.50	2972	✓
N ℄		8.25	3004	✓
	25' east NE cor. Lot 25, Bk F			
S ℄		13.00	2957	✓
Curb		14.30	2944	✓
1/4		13.40	2953	✓
℄		13.50	2952	✓
1/4		13.90	2948	✓
Curb		14.50	2942	✓
N ℄		14.60	2941	✓
	40' east. bottom of creek			
S ℄		25.4	2833	✓
Curb		21.5	2872	✓
1/4		18.0	2907	✓
℄		16.0	2927	✓
1/4		16.5	2922	✓
Curb		21.0	2877	✓
℄		25.0	2837	✓

		308.73			
	60' east NE. Lot 33, Bk. F				
			308.17		
S ℄			14.3	2944	✓
Curb			13.7	2950	✓
1/4			13.5	2952	✓
℄			12.8	2959	✓
1/4			12.9	2958	✓
Curb			11.1	2976	✓
N ℄			10.3	2984	✓
TP	7.20	305.22	10.71	298.02	
	50' east N.E. Cn. Lot 22, Bk. F				
			305.22		
S ℄			7.60	2976	✓
Curb			7.15	2980	✓
1/4			7.20	2980	✓
℄			6.60	2986	✓
1/4			6.70	2985	✓
Curb			5.80	2994	✓
N ℄			5.20	3000	✓
	N.W. Cor. Lot 12, Bk D (PI)				
S ℄			5.30	2999	✓
Curb			5.10	3001	✓
1/4			4.85	3003	✓
℄			4.80	3004	✓
1/4			4.70	3005	✓
Curb			4.15	3010	✓
N ℄			3.90	3013	✓

305.2

NW. Cor. Lot 11, Bk. D

S ℄	4.25	3010	✓
Curb	4.10	301.1	✓
1/4	4.20	3010	✓
℄	3.90	3013	✓
1/4	4.10	3011	✓
Curb	3.65	3015	✓
N ℄	3.30	3019	✓

N. W. Cor. Lot 10, Bk D.

S ℄	4.75	3004	✓
Curb	4.60	3006	✓
1/4	4.60	3006	✓
℄	4.45	3007	✓
1/4	4.55	3006	✓
Curb	4.40	3008	✓
N ℄	4.15	3010	✓

N. W. Cor. Lot 9, Bk D

S ℄	5.10	3001	✓
Curb	5.10	3001	✓
1/4	5.20	3000	✓
℄	4.90	3003	✓
1/4	5.05	3001	✓
Curb	4.65	3005	✓
N ℄	4.80	3004	✓

305.2

N.W. Cor. Lot 8, Bk. D

S ℄	5.30	2999	✓
Curb	5.30	2999	✓
1/4	5.25	2999	✓
℄	4.80	3004	✓
1/4	5.05	3001	✓
Curb	5.00	3002	✓
N ℄	4.95	3001	✓

N.W. Cor. Lot 7, Bk. D

S ℄	5.50	2997	✓
Curb	5.45	2997	✓
1/4	5.40	2998	✓
℄	5.25	2999	✓
1/4	5.15	3000	✓
Curb	5.25	2999	✓
N ℄	5.50	2997	✓

N.W. Cor. Lot 6, Bk. D

S ℄	5.40	2998	✓
Curb	5.30	2999	✓
1/4	5.30	2999	✓
℄	5.00	3002	✓
1/4	5.20	3000	✓
Curb	5.15	3000	✓
N ℄	4.70	3005	✓

305' ✓

N.W. Cor. Lot 5, Bk D

S ℄	5.00	3064	✓
Curb	4.90	3003	✓
1/4	5.10	3001	✓
℄	4.70	3005	✓
1/4	4.90	3003	✓
Curb	4.70	3005	✓
N ℄	4.60	3006	✓

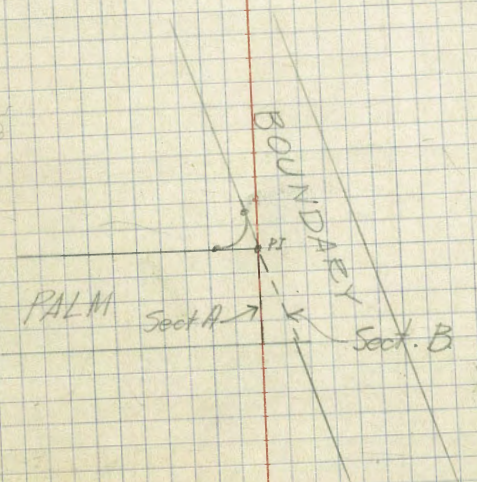
N.W. Cor. Lot 4, Bk D

S ℄	5.30	√999	✓
Curb	5.20	3000	✓
1/4	5.40	√998	✓
℄	5.00	3002	✓
1/4	5.45	√997	✓
Curb	5.30	√999	✓
N ℄	4.60	3006	✓

N.W. Cor. Lot 3, Bk D

S ℄	5.80	√994	✓
C.	5.85	√993	✓
1/4	6.10	√991	✓
℄	5.55	√996	✓
1/4	5.90	√993	✓
C	5.50	√997	✓
N ℄	5.30	√999	✓

			305 ≈		
	N.W. Cor. Lot 2, Bk D				
S. Pt.			5.50	997	✓
C			5.50	997	✓
1/4			6.45	987	✓
℄			5.55	996	✓
1/4			6.40	988	✓
C			5.25	999	✓
N. Pt.			4.95	300 ≈	✓
	N.W. Cor. Lot 1, Bk D				
S. Pt.			6.00	999	✓
C			6.00	999	✓
1/4			7.50	977	✓
℄			6.45	987	✓
1/4			7.05	981	✓
C			6.15	990	✓
N. Pt.			6.20	990	✓
	48' east	Sect. A			
N. Pt.			8.60	966	✓
C			8.70	965	✓
1/4			8.90	963	✓
℄			8.30	969	✓
1/4			8.90	963	✓
C			7.75	974	✓
S. Pt.			7.65	975	✓



305.22

Sect. B - Palm & Boundary.

N	PL.	305.2 ~~9.00~~	296.2	✓
	C.	10.00	295.2	✓
	1/4	9.55	295.6	✓
	℄	9.60	295.6	✓
	1/4	10.10	295.1	✓
	C	8.90	296.3	✓
S	PL.	8.65	296.5	✓

End of Palm.

McKinley St.

305.22

Starting at Palm, working north.

S.W. Cor. Lot 7 - Blk C (PI)

E	PL	305.2 ~~5.25~~	3006	✓
	Curb	5.35	2998	✓
	1/4	5.15	3000	✓
	℄	5.00	3002	✓
	1/4	5.00	3002	✓
	Curb	5.40	2998	✓
W	PL	4.90	3003	✓
	50' north.			
E	PL	5.75	2994	✓
	C	5.65	2995	✓
	1/4	5.70	2995	✓
	℄	5.45	2997	✓
	1/4	6.10	2991	✓
	C	5.20	3000	✓
W	PL	5.15	3006	✓
	50' north			
E	PL	7.00	2982	✓
	C	7.00	2982	✓
	1/4	7.25	2980	✓
	℄	6.75	2984	✓
	1/4	6.95	2982	✓
	C	6.50	2987	✓
W	PL	6.30	2989	✓

305.22

N.W. Cor. Lot 6 - Bk. C (PI)

E	PL		305.2 ~~10.40~~	2948	✓
	C		10.40	2948	✓
	1/4		9.80	2954	✓
	℄		9.50	2957	✓
	1/4		9.40	2958	✓
	C		8.75	2964	✓
W	PL		8.25	2969	✓
TP		3.68	299.53 9.37	295.85	

S.W. Cor. Lot 6, Bk. B (PI)

E	PL		299.5 ~~9.15~~	2903	✓
	C		6.60	2929	✓
	1/4		6.20	2933	✓
	℄		5.65	2938	✓
	1/4		5.60	2939	✓
	C		4.00	2955	✓
W	PL		2.70	2968	✓

50' north

E	PL		9.20	2903	✓
	C		7.75	2917	✓
	1/4		7.50	2920	✓
	℄		7.15	2923	✓
	1/4		7.30	2922	✓
	C		4.60	2949	✓
W	PL		3.00	2965	✓

~~799.5~~

S.W. Cor. Lot 5, Bk. B.

E	Pt.	11.90	876 ✓
	C	10.10	894 ✓
	1/4	10.40	891 ✓
	℄	9.40	901 ✓
	1/4	9.50	900 ✓
	C	7.00	945 ✓
W	Pt.	5.60	939 ✓

44' north Creek bottom on East

E	Pt.	24.0	755 ✓
	C	23.0	765 ✓
	1/4	13.3	862 ✓
	℄	11.55	879 ✓
	1/4	11.60	879 ✓
	C	13.00	865 ✓
W.	Pt	13.00	865 ✓

20' South of N.W. Cor. Lot 5, Bk. B (Pt) Creek West

E	Pt.	11.30	882 ✓
	C	10.80	887 ✓
	1/4	10.30	892 ✓
	℄	9.95	895 ✓
	1/4	10.0	892 ✓
	C	13.30	864 ✓
W	Pt.	15.70	838 ✓

		299.53			
			299.5		
	N.W. Cor. Lot. 5, Bk. B (PI)				
E	PL		7.20	293	✓
	C		7.60	919	✓
	1/4		8.15	913	✓
	℄		7.95	915	✓
	1/4		8.50	910	✓
	C		9.30	902	✓
W	PL		8.80	907	✓
	S.W. Cor. Lot. 5 Bk. A. (PI)				
E	PL		2.30	297	✓
	C		4.30	295	✓
	1/4		4.15	293	✓
	℄		3.80	297	✓
	1/4		4.05	294	✓
	C		0.0	299.5	✓
W	PL		-1.0	300	
	PP	12.00 309.19	2.36	297.17	
	50' north				
			309.2		
E	PL		7.35	301.8	✓
	C		7.10	302.1	✓
	1/4		8.70	300.5	✓
	℄		7.75	301.4	✓
	1/4		8.15	301.0	✓
	C		6.00	303.2	✓
W	PL		5.75	303.4	✓

30919

309

S.W. Cor. Lot 4, Bk A.

E ℞.	5.90	3033	✓
C	5.55	3036	✓
1/4	6.10	3031	✓
℄	5.30	3039	✓
1/4	5.65	3035	✓
C	4.50	3047	✓
W ℞	4.60	3046	✓

N.W. Cor. Lot 4, Bk A. (PI)

E ℞.	3.15	306.04	✓
C	2.80	3064	✓
1/4	2.65	3065	✓
℄	2.20	3070	✓
1/4	2.50	3067	✓
C	2.05	3071	✓
W ℞.	1.90	3073	✓

End McKinley at Redwood.

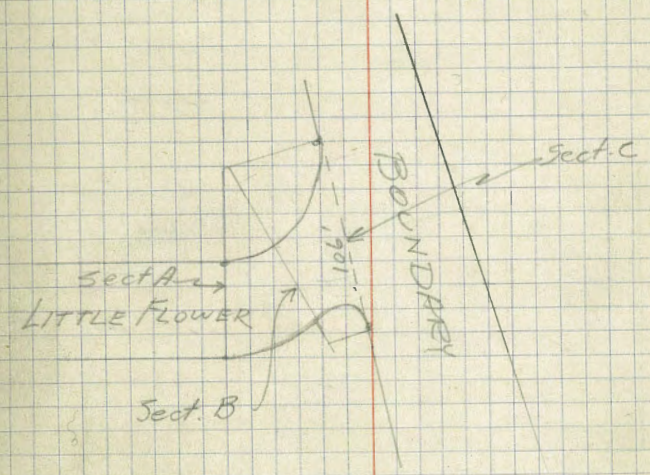
Little Flower

Start at McKinley & Work East.

TP		0.89	298.06		297.17
	S.W. Cor. Lot 5, Bk A. (PT.)				
N	PL			298.1 0.70	2974 ✓
	C			3.45	2946 ✓
	1/4			3.45	2946 ✓
	℄			3.60	2945 ✓
	1/4			3.85	2942 ✓
	C			4.35	2937 ✓
S	PL			5.30	2928 ✓
	S.E. Cor. Lot 5, Bk A.				
N	PL			3.45	2946 ✓
	C			5.90	2922 ✓
	1/4			5.10	2930 ✓
	℄			5.15	2929 ✓
	1/4			5.40	2927 ✓
	C			5.90	2922 ✓
S	PL			6.70	2914 ✓
	S.E. Cor. Lot 6, Bk A				
N	PL			6.00	2921 ✓
	C			9.20	2889 ✓
	1/4			8.50	2896 ✓
	℄			8.20	2899 ✓
	1/4			8.05	2900 ✓
	C			8.30	2898 ✓
S	PL			9.90	2882 ✓

Sect A. 5 E. Con Lot 7 Bk A

N PL	~~298.1~~ 9.10	890	✓
C	11.80	863	✓
1/4	11.30	868	✓
E	11.15	869	✓
1/4	11.10	870	✓
C	12.80	853	✓
S PL	16.00	841	✓
Sect B.			
N PL	10.4	879	
C	12.8	853	✓
1/4	13.0	851	✓
E	13.4	847	✓
1/4	15.0	831	✓
C	16.4	817	✓
S PL	18.8	793	✓
Sect. C			
N PL	8.0	901	✓
20 C	9.0	891	✓
37.50 1/4	12.0	861	✓
50 E	12.1	860	✓
68 1/4	15.6	825	✓
86 C	21.0	771	✓
106 S PL	28.8	693	✓



QUINCE ST.

Start at McKinley, work east to Boundary

TP	6.60	302.45 ~~301.45~~		295.85	
	N.W. Cor. Lot 6 - Bk. C (PI)				
S PL			302.5 ~~7.60~~	2949	✓
Curb			8.70	2938	✓
1/4			8.90	2936	✓
℄			9.00	2935	✓
1/4			9.00	2935	✓
C			9.00	2935	✓
N PL			12.10	290.4 ~~2894~~	✓
	N.W. Cor. Lot 5, Bk. C				
S PL			5.70	2968	✓
C			6.30	2962	✓
1/4			6.90	2956	✓
℄			6.80	2957	✓
1/4			7.15	2953	✓
C			7.30	2952	✓
N PL			9.50	2930	✓
	N.W. Cor. Lot 4, Bk. C				
S PL			3.90	2986	✓
C			5.50	2970	✓
1/4			5.00	2975	✓
℄			4.90	2976	✓
1/4			5.20	2973	✓
C			5.50	2970	✓
N PL			7.00	2945	✓

N.W. Cor. Lot 3 Bk C

S	PL	301.5 3.30	982	✓
	C	4.40	981	✓
	1/4	4.15	983	✓
	℄	3.95	985	✓
	1/4	3.95	985	✓
	C	4.15	983	✓
N	PL	5.10	974	✓

N.W Cor Lot 2, Bk C

S	PL	3.00	985	✓
	C	4.35	981	✓
	1/4	3.90	986	✓
	℄	3.85	986	✓
	1/4	4.10	984	✓
	C	4.30	982	✓
N	PL	5.30	972	✓

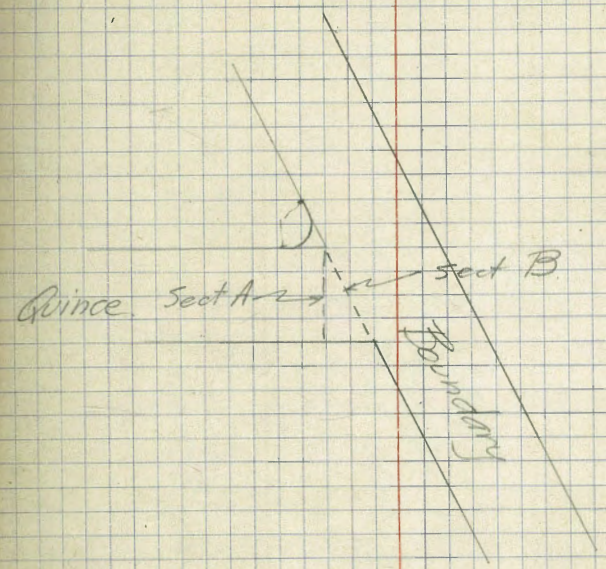
N.W. Cor. Lot 1 - Bk C.

S	PL	4.95	975	✓
	C	6.10	964	✓
	1/4	5.65	968	✓
	℄	5.80	967	✓
	1/4	6.00	965	✓
	C	6.30	962	✓
N	PL	6.80	957	✓

301.45

Sect. A	301.5		
S PL	6.25	963	✓
Curb	7.40	951	✓
1/4	7.20	953	✓
℄	7.35	951	✓
1/4	7.80	947	✓
C	8.00	945	✓
N PL	8.65	938	✓
Sect. B			
S PL	7.00	955	✓
C	8.20	943	✓
1/4	7.85	946	✓
℄	8.00	945	✓
1/4	8.30	942	✓
C	8.60	939	✓
N PL	8.65	292.80	✓

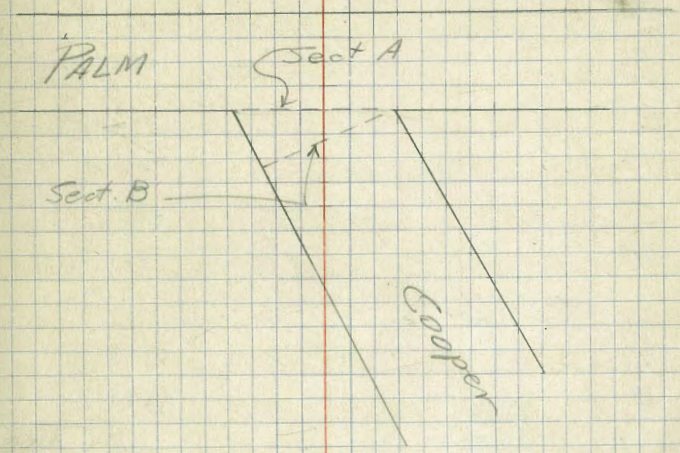
End of Quince at Boundary



Cooper St.

Start at Palm, work South & east to Boundary

T.P	3.33	301.35		298.02
	Sect A - Cooper at Palm			
E PL			301.4 / 1.50	299 ✓
Curb			2.10	993 ✓
1/4			2.50	989 ✓
℄			2.65	987 ✓
1/4			3.25	981 ✓
C			3.25	981 ✓
W PL			3.80	976 ✓
	Sect B			
E PL			1.50	999 ✓
C			2.00	994 ✓
1/4			2.40	990 ✓
℄			2.65	987 ✓
1/4			3.30	981 ✓
C			3.60	978 ✓
W PL			4.10	973 ✓
	N.E. Cor Lot 21 - Bk.			
E PL			3.20	982 ✓
C			3.35	980 ✓
1/4			3.90	975 ✓
℄			4.00	974 ✓
1/4			4.50	969 ✓
C			4.80	966 ✓
W PL			5.25	961 ✓



301 d

N.E. Cor. Lot 20, Bk F

E. Pl.	3.75	976 ✓
C	4.20	971 ✓
1/4	4.85	965 ✓
℄	4.60	968 ✓
1/4	5.40	960 ✓
C	5.50	959 ✓
W Pl.	5.90	955 ✓

N.E. Cor. Lot 19. Bk. F.

E Pl.	4.35	970 ✓
C	4.80	966 ✓
1/4	5.55	958 ✓
℄	5.35	960 ✓
1/4	5.90	955 ✓
C	5.90	955 ✓
W. Pl.	6.40	950 ✓

N.E. Cor. Lot 18, Bk. F

E Pl.	6.10	953 ✓
C	5.70	957 ✓
1/4	6.40	950 ✓
℄	6.30	951 ✓
1/4	6.80	946 ✓
C	7.00	944 ✓
W Pl.	7.40	940 ✓

301 ¼

N.E. Cor. Lot 17, Bk. F

E.	Pt.	6.25	951 ✓
	C	6.50	949 ✓
	¼	7.25	941 ✓
	℄	6.95	944 ✓
	¼	7.55	938 ✓
	C	7.50	939 ✓
W	Pt.	8.50	929 ✓

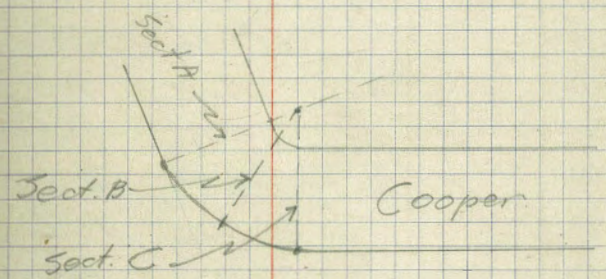
N.E. Cor. Lot 16, Bk. F

E	Pt.	6.85	945 ✓
	C	7.00	944 ✓
	¼	7.50	939 ✓
	℄	7.25	941 ✓
	¼	7.90	935 ✓
	C	8.15	932 ✓
W.	Pt.	8.40	930 ✓

N.E. Cor. Lot 15, Bk. F

E	Pt.	6.90	945 ✓
	C	7.50	939 ✓
	¼	7.90	935 ✓
	℄	7.65	937 ✓
	¼	8.40	930 ✓
	C	8.70	927 ✓
W	Pt.	9.25	921 ✓

		301.35	301 1/4	
	N.E. Cor. Lot 14, Bk. F			
E Pl.			7.55	293.5 ✓
C			8.00	293.1 ✓
1/4			8.55	292.8 ✓
E			8.60	292.8 ✓
1/4			9.20	292.2 ✓
C			9.50	291.9 ✓
W Pl.			10.20	291.2 ✓
BM	5.55	298.50	8.40	292.95
	Sect. A		298.5	
E Pl.			5.70	292.8 ✓
C			6.05	292.4 ✓
1/4			6.60	291.9 ✓
E			6.55	291.9 ✓
1/4			7.00	291.5 ✓
C			7.40	291.1 ✓
W. Pl			8.15	290.3 ✓
	Sect. B.			
E Pl.			5.70	292.8 ✓
C			5.75	292.7 ✓
1/4			6.00	292.5 ✓
E			6.50	292.0 ✓
1/4			6.65	291.8 ✓
C			7.10	291.4 ✓
W Pl.			7.30	291.2 ✓



985

Sect. C

N Pt.	5.70	948	✓
C	5.90	946	✓
1/4	6.45	940	✓
℄	6.25	944	✓
1/4	6.80	917	✓
C	6.70	918	✓
S Pt.	6.90	916	✓

N.W. Lot 10, Bk F.

N Pt.	5.10	934	✓
C	5.40	931	✓
1/4	5.95	925	✓
℄	5.70	928	✓
1/4	6.25	944	✓
C	6.00	945	✓
S Pt.	6.30	944	✓

N.W. Lot 9, Bk. F

N Pt.	4.60	939	✓
C	5.05	934	✓
1/4	5.55	929	✓
℄	5.15	933	✓
1/4	5.45	930	✓
C	6.10	924	✓
S Pt.	6.60	919	✓

298 5

N.W. Cor. Lot 8, Bk F.

N Pl.	4.30	944	✓
C	4.60	939	✓
1/4	5.30	993	✓
℄	5.10	934	✓
1/4	5.60	929	✓
C	5.45	930	✓
S Pl.	5.70	926	✓

N.W. Cor. Lot 7, Bk. F.

N Pl.	4.65	938	✓
C	5.20	933	✓
1/4	6.20	923	✓
℄	5.80	927	✓
1/4	6.30	922	✓
C	6.10	924	✓
S Pl	6.40	921	✓

N.W. Cor. Lot 6, Bk. F

N Pl.	6.00	925	✓
C	6.50	920	✓
1/4	6.65	918	✓
℄	6.30	922	✓
1/4	6.80	917	✓
C	8.90	896	✓
S Pl.	9.90	886	✓

		298.50			
			298.5		
	N.W. Lot 5, Bk. F				
N Pt.			5.55	919	✓
C			5.70	918	✓
1/4			7.20	913	✓
E			6.95	915	✓
1/4			7.40	911	✓
C			6.50	920	✓
S Pt.			6.50	920	✓
TP.	5.55	294.70	9.35	289.15	
	N.W. Lot 4, Bk. E				
			294.7		
N Pt.			6.0	887	✓
C			6.20	885	✓
1/4			7.00	877	✓
E			6.75	879	✓
1/4			6.40	883	✓
C			6.30	884	✓
S Pt.			6.25	885	✓
	30' east in Creek.				
N Pt.			9.30	854	✓
C			8.30	863	✓
1/4			9.30	854	✓
E			12.00	847	✓
1/4			13.75	809	✓
C			14.60	801	✓
S Pt.			16.20	785	✓

		2947	(3) 2947		
	N.W. Lot 2, Bk F				
N Pt.			3.80	2909	✓
C			4.50	2902	✓
1/4			6.60	2881	✓
℄			6.50	2881	✓
1/4			7.40	2873	✓
C			8.80	2859	✓
S Pt.			10.00	2847	✓
	N.W. Lot 2, Bk F				
N Pt.			0.80	2939	✓
C			1.25	2934	✓
1/4			2.15	2925	✓
℄			1.95	2927	✓
1/4			2.25	2924	✓
C			2.80	2919	✓
S Pt.			3.50	2912	✓
T.P	7.90	302.60	0.0	2947.0	
	N.W. Lot 1, Bk F		302.6		
N Pt.			4.70	2979	✓
1/4			5.10	2975	✓
C			5.50	2971	✓
℄			5.50	2971	✓
C			6.20	2964	✓
1/4			5.95	2966	✓
S Pt.			6.30	2963	✓

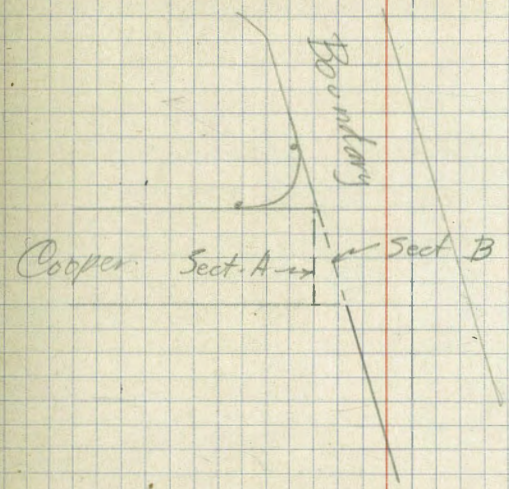
302.6

Sect. A. 30v 6

N Pt.	2.90	✓997	✓
C	3.00	✓996	✓
1/4	3.35	✓994	✓
℄	3.30	✓993	✓
1/4	3.65	✓989	✓
C	3.70	✓989	✓
S Pt.	3.90	✓987	✓

Sect. B.

N Pt.	2.90	✓997	✓
C	2.95	✓996	✓
1/4	3.10	✓995	✓
℄	3.00	✓996	✓
1/4	3.30	✓993	✓
C	3.15	✓994	✓
Pt.	3.32	✓99.28	✓

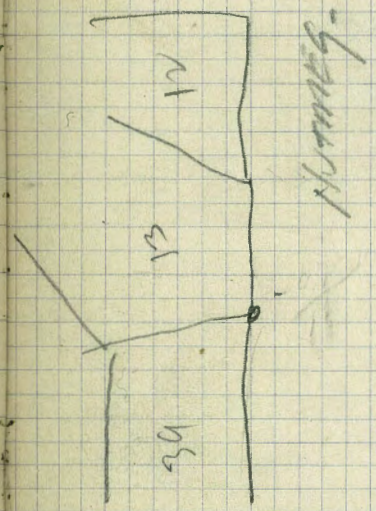


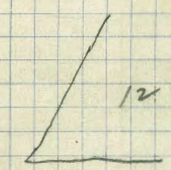
(MH12) 13

SW Cor ~~12~~ Blk F along S.L. Blk F. $-\frac{5}{10}$ $-\frac{6.5}{14}$ $-\frac{6^{\circ}}{30}$ $-\frac{1^{\circ}}{46}$ $+\frac{4^{\circ}}{(5)}$

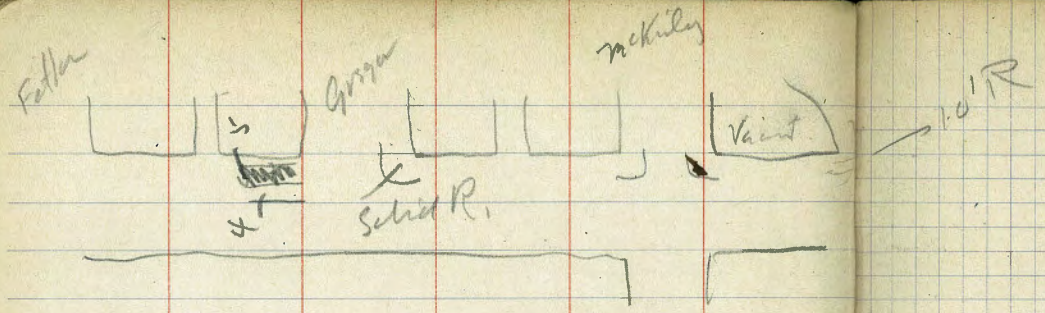
SW 12 West (MH11) $-\frac{5}{19}$ $-\frac{14}{39}$ $-\frac{15}{54}$ $-\frac{20}{66}$ $-\frac{23^{5}}{73}$

$-\frac{0.7}{18}$





$-\frac{0.7}{10}$


Fetter
Gosgen
McKinley
Vacant
Solid R.
10' R

Profiles ℄ Linda Rosa.

BM.		3.97	171.88		167.91
℄ Colima	13+29			4.4	167.48
13				4.3	167.58
12+94				3.6	168.28
+84				8.4	163.48
+62				9.7	162.18
+46				9.2	162.68
+30				2.8	169.08
12+00				3.7	168.18
+50				5.8	166.08
11				8.2	163.68
+50				10.8	161.08
10		4.87	163.83	12.92	158.96
+50				7.1	156.73
9				8.3	155.53
+50				9.9	153.93
8				10.3	153.53
+50				10.0	153.83
7				8.7	155.13
℄ Midway	6+710			7.5	156.33
+50				7.2	156.63
6				5.3	158.53
+50				4.9	158.93
5				5.9	157.93

			163.83		
4+50				6.0	157.83
4				7.4	156.43
+50				6.4	157.43
3				1.9	161.93
+50		11.79	174.26	1.36	162.47
+20				13.3	160.96
2				12.5	161.76
+50				8.4	165.86
1				6.0	168.26
+50				3.6	170.66
0+00	℄ Forward			4.3	169.96
TP		0.73	162.48	12.51	161.75

Profile ℄ Taft.

		162.48			
0+00 = ℄ Forward	2.17	151.63	13.02	149.46	
+50			1.6	150.03	
1			2.8	148.83	
+50			3.5	148.13	
2			4.4	147.23	
+50			6.0	145.63	
3			7.7	143.93	
+50			10.2	141.43	
4	1.29	140.34	12.58	139.05	
+50			3.20	137.14	
5			5.30	135.04	
+50			5.80	135.54	
6			7.0	133.34	
+50			7.4	132.94	
℄ Midway			6.8	133.54	
7			5.1	135.24	
+50			4.7	135.64	
8			4.4	135.94	
+50			4.1	136.24	
9			5.0	135.34	
+50			5.2	135.14	
10	13.45	149.09	4.70	135.64	
+50			12.2	136.8	

		149.09		
11			9.8	139.29
+50			6.2	142.89
12			3.7	145.39
+50			2.9	146.19
13			1.9	147.19
℄ Colima			1.3	147.79
TP			4.46	144.63

Profile ℄ Bellevue

TP	4.05	123.45		119.40
℄ Colima			1.1	122.35
13			2.0	121.45
+50			2.8	120.65
12			3.8	119.65
+50			5.1	118.35
11			5.2	118.25
+50			5.1	118.35
10			5.0	118.45
+50			5.1	118.35
9			5.7	117.75
+50			5.9	117.55
8			4.9	118.55
+50			3.6	119.85
7			2.0	121.45
℄ Midway	12.81	134.94	1.32	122.13
+50			12.5	122.44
6			11.0	123.94
+50			9.9	125.04
5			8.8	126.14
+50			8.0	126.94
4			7.1	127.84
+50			6.0	128.94

			134.94		
3				4.90	130.04
+50				4.50	130.44
2				4.0	130.94
+50				3.4	131.54
1				2.3	132.64
+50				1.0	133.94
0+00 ℄ Forward				+0.9	134.04
TP		1.68	135.47	1.15	133.79

℄ Waverly

		135.47		
℄ Forward = 0+00			12.2	
TP	0.61	124.23	11.85	123.62
0+50			2.2	122.13
1			3.0	121.33
+50			4.4	119.9
2			5.2	119.1
+50			6.0	118.3
3			6.9	117.4
+50			7.9	116.4
4			8.9	115.4
+50			10.2	114.1
5	1.70	114.73	11.20	113.03
+50			2.5	112.23
6			3.5	111.23
+50			4.9	109.83
℄ Midway			4.4	110.33
7			5.1	109.63
+50			5.9	108.83
8			6.5	108.23
+50			7.3	107.43
9			8.0	106.73
+50			8.5	106.23

		114.73		
10			9.0	105.73
+50			9.3	105.43
11	4.72	109.65	9.80	104.93
+50			5.5	104.15
12			5.5	104.15
+50			4.8	104.85
13			4.2	105.45
℄ Colima			3.9	105.75
TP			6.39	103.26

℄ Beaumont

TP	6.40	98.31		91.91
℄ Colima			5.0	93.31
13			5.2	93.11
+50			5.6	92.7
12			5.2	93.1
+50			5.2	93.1
11			4.8	93.5
+50			4.1	94.2
10			4.1	94.2
+50			3.9	94.4
9			3.4	94.9
+50			2.9	95.4
8	8.89	104.75	2.45	95.86
+50			8.1	96.65
7			7.5	97.25
℄ Midway			6.3	98.45
+50			6.3	98.45
6			6.1	98.65
+50			5.6	99.15
5			5.0	99.75
+50			4.1	100.65
4			3.1	101.65
+50			2.2	102.55
3			2.0	102.75

		104.75		
2+50			1.3	103.45
2	5.01	108.99	0.77	103.98
+50			4.60	104.39
1			3.60	105.39
+50			3.40	105.59
0+0 ℄ Forward			3.20	105.7
TP	0.51	96.04	13.26	95.53

20' East of W. Line Elec. Ave.

96.04

13+45 = N. Line Forward.				
℄ Forward.			7.5	88.5
14			7.3	88.7
+50			7.5	88.5
15			7.7	88.3
+50			7.9	88.1
16			8.2	87.8
+50	2.60	88.43	10.21	85.83
17			2.7	85.73
+50			2.9	85.5
18			3.1	85.3
+50			4.5	83.9
19			4.3	83.9
+50.			5.3	83.1
20			5.0	83.4
℄ Midway			5.0	83.4
+50			4.7	83.7
21			4.6	83.8
+50			5.3	83.1
22			5.3	83.1
+50			5.2	83.2
23	4.45	87.38	5.50	87.93
+50			4.1	83.28
24			4.6	82.78

		87.38		
24+50			4.4	82.98
25			5.1	82.28
+50			5.6	81.78
26			6.0	81.38
+50			6.3	81.08
℄ Colima			6.1	81.28
TP			6.71	80.67

Ticonderoga Additional Section

For Original. See Page 63

0+85

0+30

56.85

Lt. Rt.

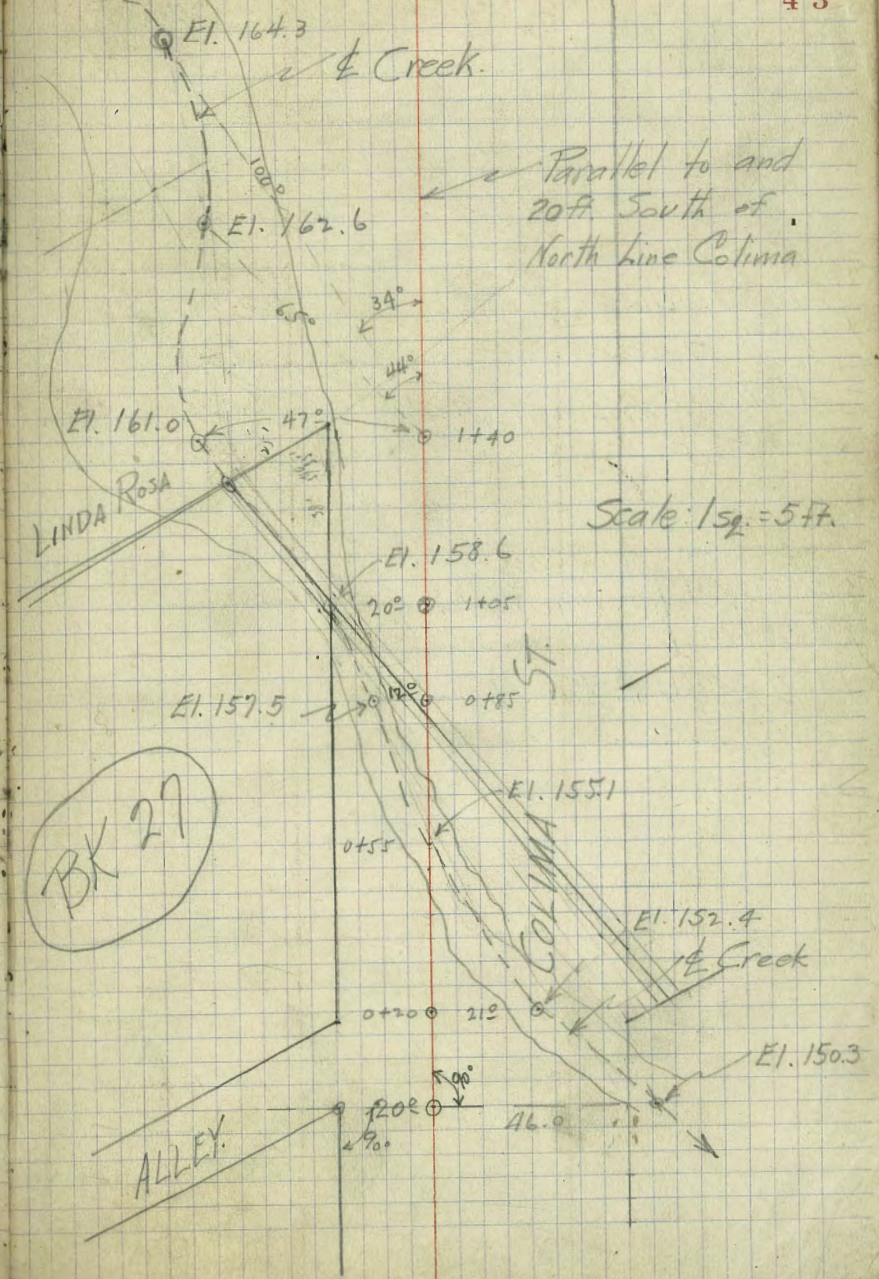
57.5	54.7	53.8	55.4	54.7	54.5
+0.6	8.7	3.1	1.5	2.7	2.4
	1	32	35	60	70

55.5	53.7	52.6	53.9	49.6	48.9	48.9
1.1	3.7	4.3	30	7.3	8.0	8.0
	1	32	38	39	60	70

56.85

Colv. at Linda Rosa

BM.	1.70	169.61		167.91
1			5.3	164.3
2			7.0	162.6
3			8.6	161.0
4			11.0	158.6
5			14.5	155.1
6			12.1	157.5
PP	3.55	161.28	11.88	157.73
7			8.9	152.4
8			11.0	150.3



Top of Rails on Elec. Ave.

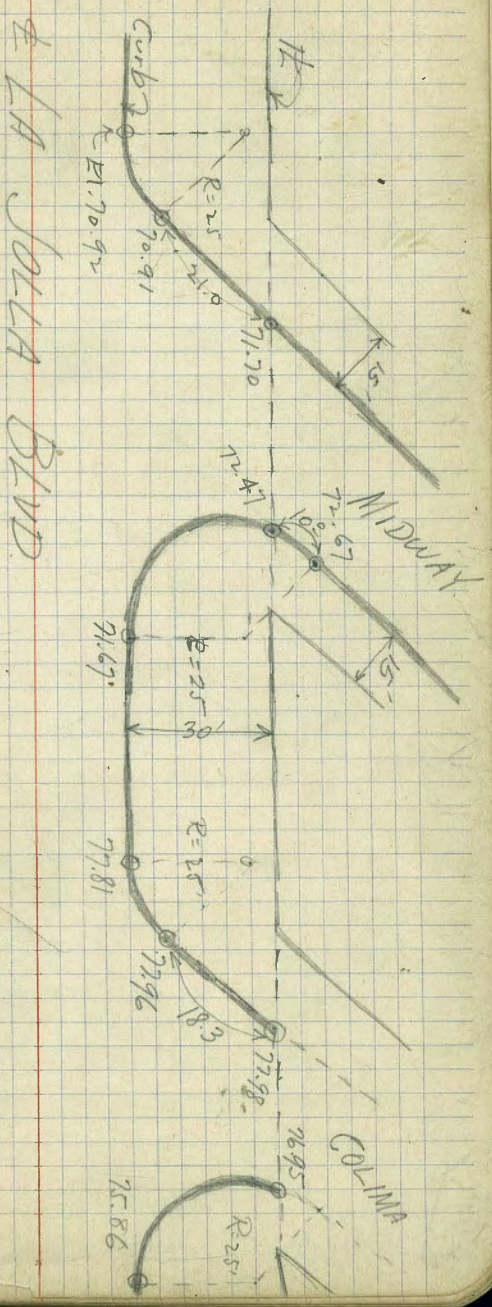
Aug. 27, 1916

BM.		2.42	88.29		80.87
				88.29	
T/R West Rail	So. Line Colima.			5.99	8+10 ✓
East "				5.99	8+30 ✓
West "	No. Line Colima			5.95	8+34 ✓
East "				5.95	8+34 ✓
West Rail	So. Line Midway			4.18	8+11 ✓
East "				4.16	8+13 ✓
West Rail	No. Line Midway			3.98	8+31 ✓
East "				4.00	8+49 ✓

CURB RETURNS - La Jolla
at Midway & Colima

B.M.	5.68	76.62		70.94
1			5.70	70.92
2			5.71	70.91
3			4.92	71.70
4			3.95	72.67
5			4.15	72.47
6			4.95	71.67
B.M.			4.90	71.72

B.M.	4.81	82.32		77.51
1			4.51	77.81
2			4.36	77.96
3			4.34	77.98
4			5.37	76.95
5			6.46	75.86



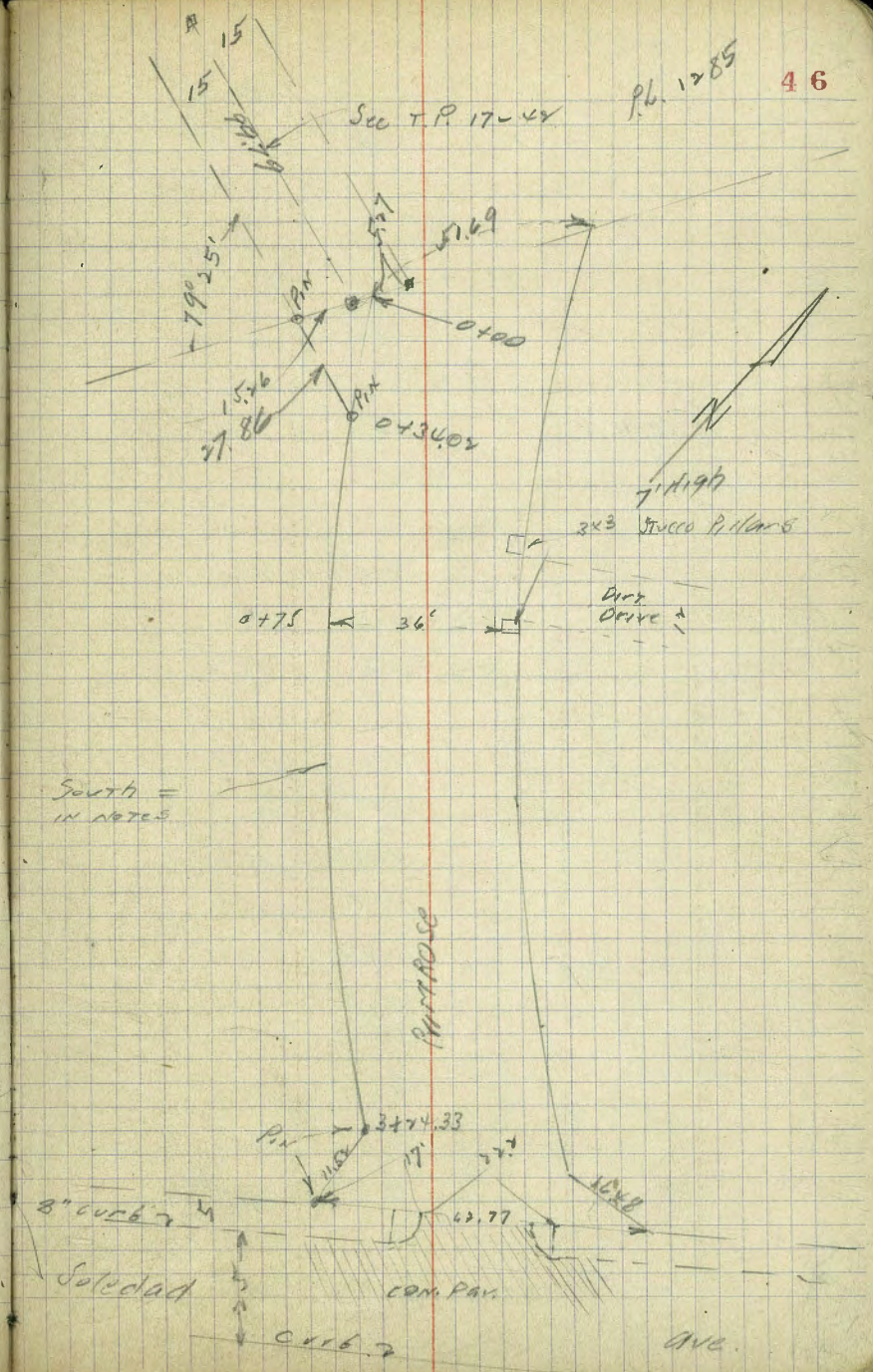
Moore

Xsec of Primrose
Soledad to Line of P.h. 1285

SWBP	1.61	192.06		190.45 Soledad Whitefield
T.P.	11.91	200.67	3.30	188.76

0 — 99.79 = E.C. See Tie Pt. 17-42

S Par = 3" oil Rock		10.8	189.9
C " on R.R. spike		10.35	190.32
N "		10.8	189.9
0 — 75			
N Par		10.7	190.0
C "		10.2	190.5
S "		10.7	190.0
0 — 50			
S Par		11.1	189.6
C "		10.5	190.2
N "		10.9	189.8
0 — 25			
N Par		11.9	188.8
C "		11.3	189.4
S "		11.8	188.9
0+00			
S end Par		12.5	188.2
+15.26 " " = ℄ to West		12.3	188.4



		200.67		
C +10 = SL Curve to E			12.5	188.2
+15 = NL to West			12.6	188.1
+ 46.69 = NL cly.			25.3	175.4
T.P.	146	189.59	12.54	188.13
	0+25	St. 40' Wide		
-10	1°07.14'		10.8	178.8
N			10.7	178.9
+11			10.6	179.0
C			4.6	185.0
+6			2.3	187.3
S			3.3	186.3
	0+34.04 1031.4'			
S	ON Pin		4.02	185.57
+18			3.2	186.4
C			3.7	185.9
+10			10.6	179.0
N			10.7	178.9
+10			10.6	179.0
	0+50 2014.28			
-10			10.2	179.4
N			9.8	179.8
+9			9.2	180.4
+16			4.5	185.2
C			4.6	185.0

		189.59		
S			5.0	184.7
	0+75			
S	3021.42		2.8	186.8
+6			4.8	184.8
C			5.1	184.5
N	eastedge Dr		6.4	183.0
+10	" " "		7.0	182.6
	1+00			
N -10	4°28.56'		5.9	183.7
N			5.9	183.7
+7	Row 5 Cypress trees		5.0	184.6
+13			3.1	186.5
C			3.6	186.0
+12			3.9	185.7
S			0.7	188.9
T.P.	127.2	201.36	0.95	188.64
	1+25 5°35.20'			
S			11.3	190.1
+7			13.1	188.3
C			13.0	188.4
+13	Cypress trees		13.3	188.1
N			13.5	187.9
+10			14.1	187.3

		201.36		
1+50				
−10	6042.84		12.5	188.7
N			12.5	188.9
+9			10.1	191.3
C			9.9	191.5
+10			10.2	191.2
S			8.0	193.4
1+75				
S	7449.98'		5.5	195.2
+9			5.9	194.8
+11			7.0	193.7
C			6.6	194.8
+18			6.4	194.8
+17			9.1	192.3
N			9.1	192.3
+10			9.7	191.7
2+00				
−10	8°57.12'		5.6	195.8
N			5.7	195.7
+6			2.7	198.7
C			3.0	198.4
+10			3.3	198.1
+11			2.3	199.1
S			2.3	199.1
T.P.	12.88	214.02	0.22	201.14

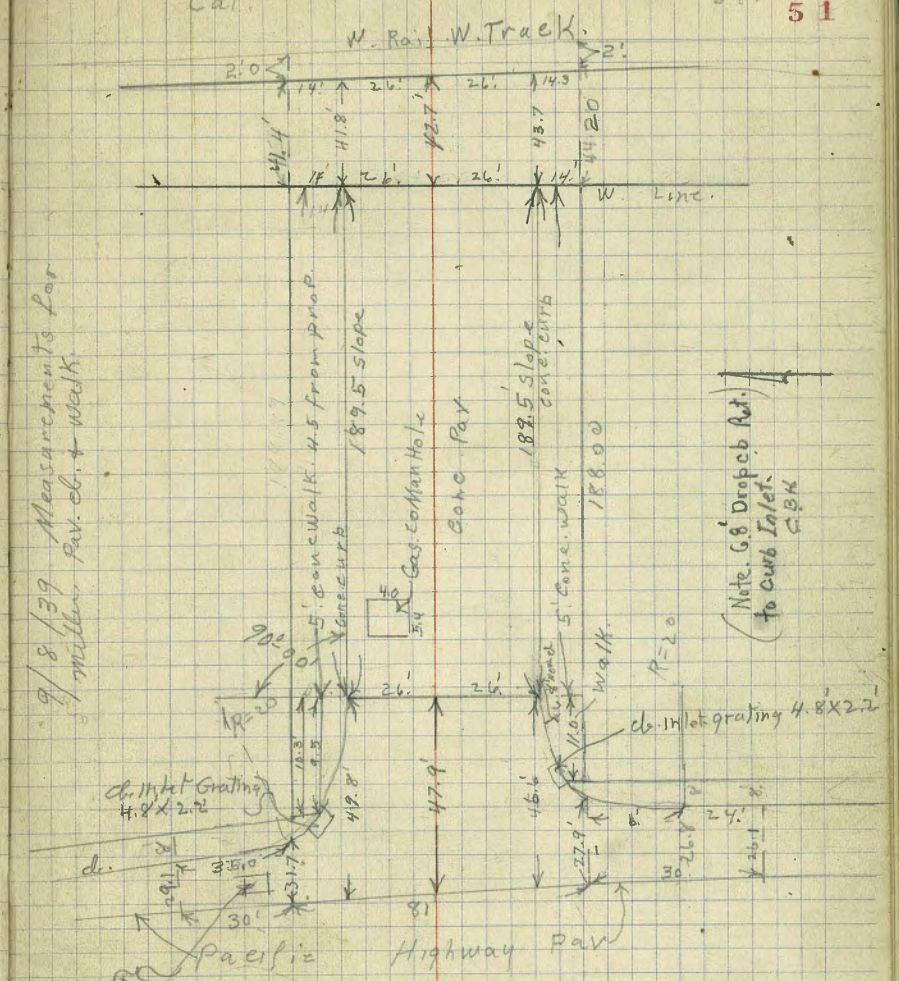
		214.02	
2+25			
S	10°04.20'	11.5	202.5
+6		12.2	201.8
C		12.1	201.9
+12		12.0	202.0
N		15.5	198.5
+10		16.5	197.5
2+50			
−10	11°11.40'	13.4	200.6
N		12.7	201.3
+10		8.1	205.9
C		8.3	205.7
+10		9.0	205.0
S		8.2	205.8
2+75			
S	12°18.54	4.5	209.5
+10		5.0	209.0
C		5.0	209.0
+11		4.6	209.4
N		9.6	204.4
+10		11.5	202.5
3+00			
−10	13°25.68	8.3	205.9
N		6.7	207.3
+		0.3	213.7
C		0.9	213.1

		214.07		
C + 13			0.9	213.1
T.P.	10.61	224.05	0.58	213.44
C + 18			8.2	215.9
S			8.2	215.9
3+24.83 E.C. 140 31.03'				
S	on Iron Pin		5.00	219.1
+4			5.5	218.6
+10			7.1	217.0
C			6.6	217.5
+10			6.2	217.9
N			12.9	211.2
+15			15.0	209.1
△ to △				
−15			14.1	210.0
N			11.4	212.7
+10			6.2	217.9
C			6.4	217.7
+10			6.9	217.2
+14			5.4	218.7
S	Iron Pin		5.00	219.1
	W/y Line Soledad Ave			
S	on Pin		3.98	220.07
+17	Top curb		4.60	219.45

	224.05	
+17	gut Pav	5.02	219.00
S + 39.2	gut	5.54	218.48
S + 39.2	Top cb	5.34	218.68
N		5.9	218.1
	W/y curb		
S−10	curb	3.46	220.59
" "	gut	3.87	220.18
S	curb	3.90	220.15
S	gut	4.27	219.78
S +12	PC Top cb	4.40	219.65
" "	gut	4.75	219.30
S + 44.2	PC curb	5.32	218.73
" "	gut	5.68	218.37
N	Top curb	5.73	218.32
"	gut Pav	6.14	217.91
	℄ Soledad Ave		
N		5.59	218.46
S		3.75	220.30
Top end cb N Cor Soledad + Hillside Dr.		10.29	213.76	OK
	See grade book for check			

6-27-39
Miller
Walker
Bess

	X. Sec	Cedar	St.	Calif. To Pacific	
BM. P.I. C.T	13.07	18.01		4.94	Pacific & Cedar.
	0+00 - 46.08 on S. Line } = W. Rail W. Track				
	0+00 - 43.58 on N " }				
S			2.23		
℄			2.04		
N.			1.95		
	0 0 - 44.08 on S. Line } Line 2' W. of W. Rail				
	0 0 - 41.58 " N. " }				
N - 5'			2.8	15.2	
N.			2.8	15.2	
cb			2.6	15.4	
1.4			2.1	15.9	
℄			2.1	15.9	
1.4			2.2	15.8	
cb			2.9	15.1	
S			2.8	15.2	
+			2.9	15.1	



18.01

00 - 27 E

S - 5.	3.0	15.0
S	2.9	15.1
el	3.2	14.8
¼	2.9	15.1
℄	2.8	15.2
¼	2.8	15.2
el	3.1	14.9
N	3.4	14.6
+ 5'	3.8	14.2

00 - 17 E

- 5.'	4.2	13.8
N	4.0	14.0
el	3.6	14.4
¼	3.3	14.7
℄	3.2	14.8
¼	3.5	14.5
el	4.2	13.8
S	4.6	13.4
+ 5	4.5	13.5

0+00 = W. Line California

- 2. = Bldg	5.4	12.6
S.	5.4	12.6
+ 5	4.3	14.7
el	4.5	13.5
¼	4.0	14.0
℄	3.8	14.2

18.01 cedar

¼	3.8	14.2
el	4.3	13.7
N	4.7	13.3
+ 2. = conc. walk. S.E. Cor.	4.92	13.09

0+01 Tel. Pole 14 N of N. el.

0+25 W

N - 1.5	5.22	12.79
N	5.2	12.8
el	5.3	12.7
¼	5.0	13.0
℄	4.9	13.1
¼	5.2	12.8
el	5.4	12.6
S	5.3	12.7
+ 1.5 Bldg.	4.9	13.1

0+50 W

S - 2.0'	5.9	12.1
S	6.4	11.6
el	6.6	11.4
¼	6.5	11.5
℄	6.2	11.8
¼	6.2	11.8
el	6.1	11.9
N	6.4	11.6
+ 5	6.4	11.6

18.01

0 + 72.5 W

1.0' S. of N = N.E. Cor. of S.D.C.G.&E.	7.09	10.92	{Conc. M.H. Iron Cover
3.5 " " " = S " " " " " " "	7.09	10.92	" " " "

0 + 75 W

−5.	7.4	10.6
N	7.2	10.8
+1.0 = N.W. Cor above M.H.	7.21	10.80
+3.5 = S " " " " "	7.21	10.80
cb	7.4	10.6
1/4	7.4	10.6
℄	7.5	10.5
1/4	7.8	10.2
cb	8.0	10.0
S	7.8	10.2
+2 = Bldg	7.8	10.2

0 + 96 Tel Pole 1.4 N. of N. cb

1 + 00 W

S − 2' = Bldg	8.7	9.3
S	8.7	9.3
cb	9.2	8.8
1/4	8.9	9.1
℄	8.9	9.1
1/4	9.0	9.0
cb	9.2	8.8
N E. of house.	9.7	8.3
+5. " " "	8.8	9.2

1 + 00 2

1.2' S. of N. Line = S.E. Cor House.

18.01 Cedar.

1 + 22 W.

1.5 S. of N. Line = S.W. Cor. above House

1.5 " " " " E. End Fence

1 + 25

−5.'	11.4	6.6
N	11.4	6.6
cb	10.7	7.3
1/4	10.4	7.6
℄	10.1	7.9
1/4	10.1	7.9
cb	10.3	7.7
S	10.0	8.0

1 + 47

2.' S. of N. Line = W. End above Fence.

1 + 50

S	10.5	7.5
+12	11.0	7.0
cb	11.6	6.4
1/4	11.6	6.4
℄	11.4	6.6
1/4	11.6	6.4
cb	11.7	6.3
N.	11.5	6.5
+5	11.5	6.5

1 + 61 W

1.4 N. of N. cb = Tel Pole

1 + 73 W

Elec. Pole 9' N. of S. Line = Elec Pole

18.01

1+75

— 5.			12.2	5.8
N.			12.2	5.8
cl			11.8	6.2
+2			12.8	5.2
1/4			12.5	5.5
℄			12.5	5.5
1/4			12.3	5.7
cl			12.7	5.3
+5			11.6	6.4
S			12.0	6.0
T.P.	5.06	10.56	12.51	5.50

1+85 W on S. Line = P.C. 20' Rad. cl Ret.
1+88.3 " " N " = " " " " "

S			4.6	6.0
S. conc. cl. E. End			5.01	5.55
gutter			5.7	4.9
1/4			5.1	5.5
℄			5.5	5.1
1/4			5.5	5.1
Gutter			5.8	4.8
N. conc. cl. E. End.			5.12	5.44
N			4.7	5.9

1+94.4 W

on N. cl. Ret. = E. End. cl. inlet cl	5.25	5.31
" " " " " " 1/4 gutter	6.22	4.34

8' E. of E. Line Pacific
6' S. " S cl. Cedar Elec Dead Man for Guy cable

10.56 Cedar

1+95 W

5.4

on S. cl. Ret = E. End cl. inlet cl.	5.25	
" " " " " " " gutter	6.21	4.35

Pacific Highway

30' S. of S. Line of Cedar see Plat

E	4.7	5.9
+8 = cl	5.0	5.6
+10 = gutter	6.8	4.6
E. Edge pav.	5.35	5.21

P.C. S. End 20' Rad. Ret.

S. End. conc. cl	6.20	4.36

out of place 3.7' N. of S. Line Cedar Produced.

on cl. Ret = S. End. cl. inlet = cl	5.33	5.23
" " " " " " " gutter	6.30	4.26

S. Line Cedar Produced.

E. cl. Line dirt	6.1	4.5
E. edge pav	5.45	5.11

℄ Cedar Produced

E. Edge pav	5.59	4.97
E. cl. Line	5.8	4.8
E. Line	5.8	4.8

3' S. of N. Line produced

cl. Ret. at N. End of cl. inlet cl	5.46	5.10
" " " " " " " gutter	6.47	4.09

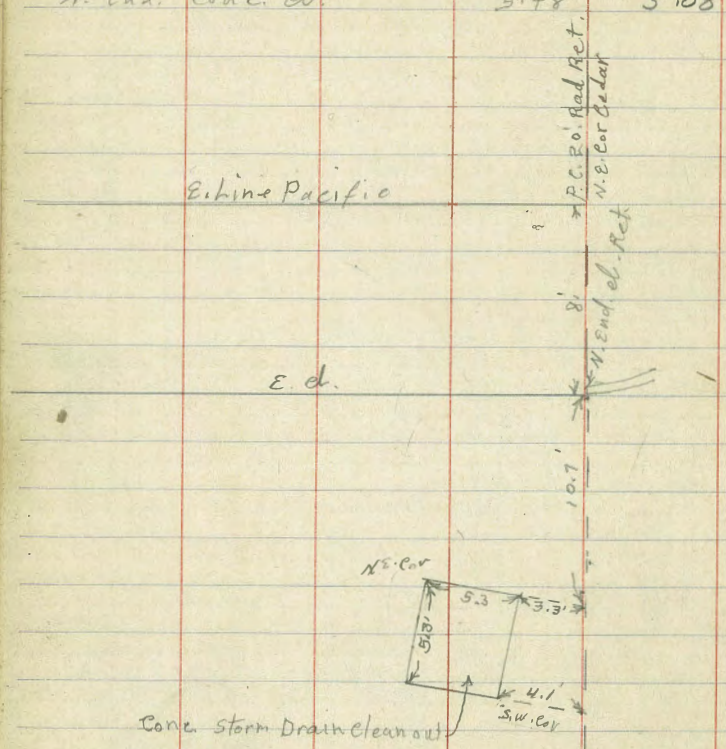
10.56

N. Line Cedar St. Produced

E. el. Line dirt gutter	6.3	4.3
E. edge Pav	5.71	4.85

N. End 20' Rad. Ret

N. End. conc. el.	5.48	5.08



Clean out. Box

S. E. Cor	5.94	4.62
S. W.	5.90	4.66
N. W.	5.90	4.66
N. E.	5.97	4.59

30' N of N. Line Cedar Produced
See Plat

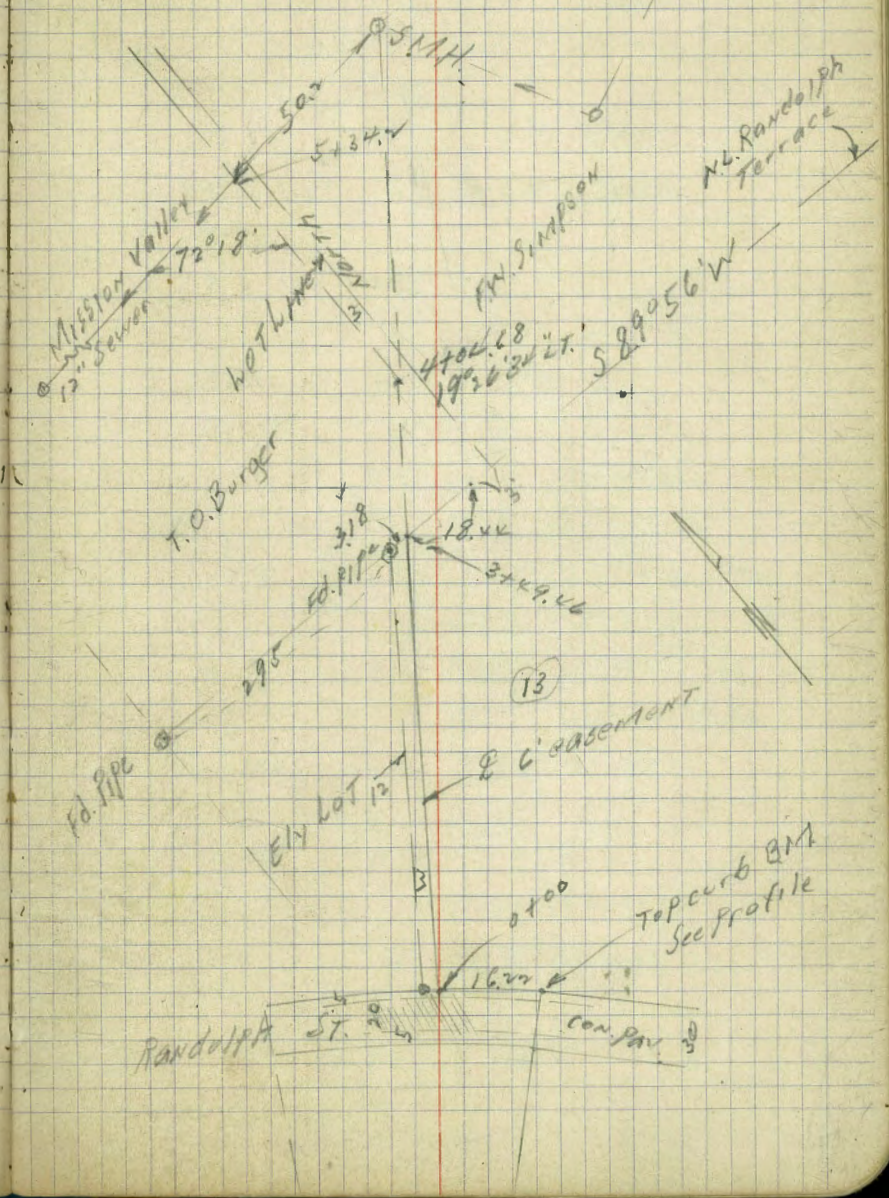
E. edge pav	5.84	4.72
2' W of E. el.	6.2	4.4
E. el.	5.6	4.9
7' E of E. el	5.4	5.2
8' E of E el = E. Line	5.0	5.5
Chk. BM Original	5.62	4.94

Moore
2-28-20

Location for Proposed
Water line Thru Lot 13
Randolph Terrace

	+	H.I.	−	El.	
B.M. Top curb	1.92	196.18		194.26	N. curb Randolph 162.2 E of 0+00
0-5	Top curb		2.16	194.02	
0-3.5	1' W=E SMH		2.18	194.00	Rim
"	"	"	9.00	187.18	F.L.
0+0 N.L. Randolph St			2.0	194.0	
+35			5.8	190.4	
+65			18.0	178.2	
T.P.	0.68	184.04	12.82	183.36	
1+00			15.8	168.2	
T.P.	0.75	171.77	13.02	171.02	
+30			12.5	159.3	
T.P.	0.36	159.44	12.69	159.08	
+60			8.9	150.5	
T.P.	0.33	146.76	13.01	146.43	

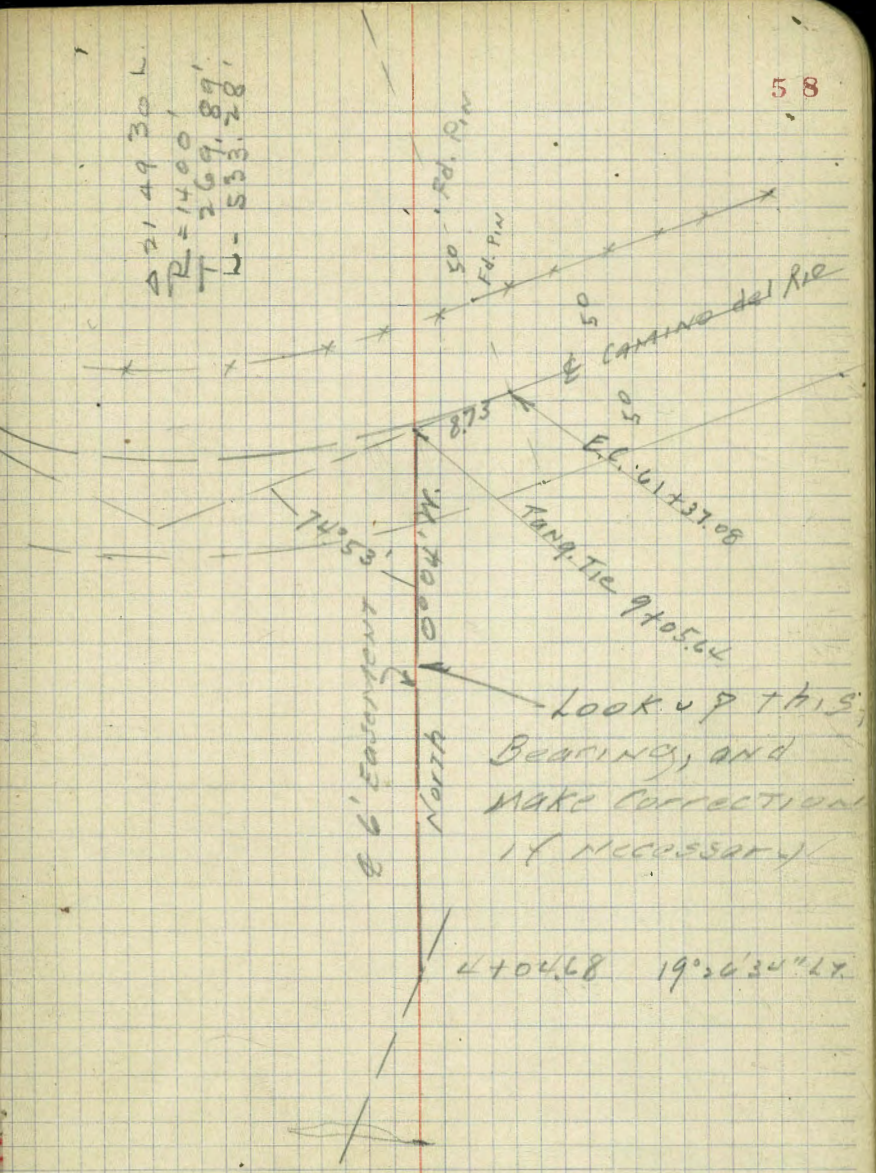
INDEXED
EFB



		146.76			
2+00			8.7	138.1	
T.P.	0.70	134.52	12.94	133.82	
+35			7.0	127.5	
T.P.	0.42	121.91	13.03	121.49	
+65			5.4	116.3	
2+79	1' w = ½ SMH.		4.05	115.26	RIM
"	" "	"	9.15	112.76	F.L.
"	ground		9.8	112.1	
T.P.	0.12	109.45	12.58	109.33	
3+00			5.4	104.0	
T.P.	0.13	96.70	12.88	96.57	
+25			2.2	94.5	
3+49.46	N.L. Randolph Ter.		9.9	86.8	
T.P.	0.33	84.28	12.75	83.95	?

	84.28			
3+60			0.0	84.3
3+90			8.9	75.4
4+04.68 Δ = 19°26'34" LT.			8.7	75.6 Top Mound
" 3' LT.			10.7	73.6
+20			11.4	72.9
" 3' LT.			13.4	70.9 " "
T.P.	0.35	71.89	12.74	71.54
+30			2.5	69.4
+45			5.7	66.2
+80			12.1	59.8
5+00			12.8	59.1
T.P.	0.06	59.05	12.90	58.99
5+34.23			2.7	56.3
" 50.2 RT			3.87	55.18 SMH RIM
" " "			9.15	49.90 F.L.
5+63 Top Cut			5.7	53.3
T.P.	0.51	46.94	12.62	46.43
T.P.	0.42	34.35	13.01	33.93
6+00 Bot. Borrow Pit			7.6	26.7
+50			9.2	25.1

		34.35			
7+00			10.2	24.1	✓
+50			11.5	22.8	✓
8			12.5	21.8	✓
T.P.	1.06	25.90	12.51	21.84	✓
+50			4.6	21.3	✓
+60			5.1	20.8	✓
+72			7.2	18.7	✓
+87			4.6	21.3	✓
9			5.0	20.9	✓
9+05.64	INT. E/P Tang. & Camino del Rio		5.3	20.6	✓

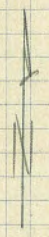


Measure alley Par
Blk 46 Park Villas
Moore 6-26-40

INDEXED
EFB

Lands

59



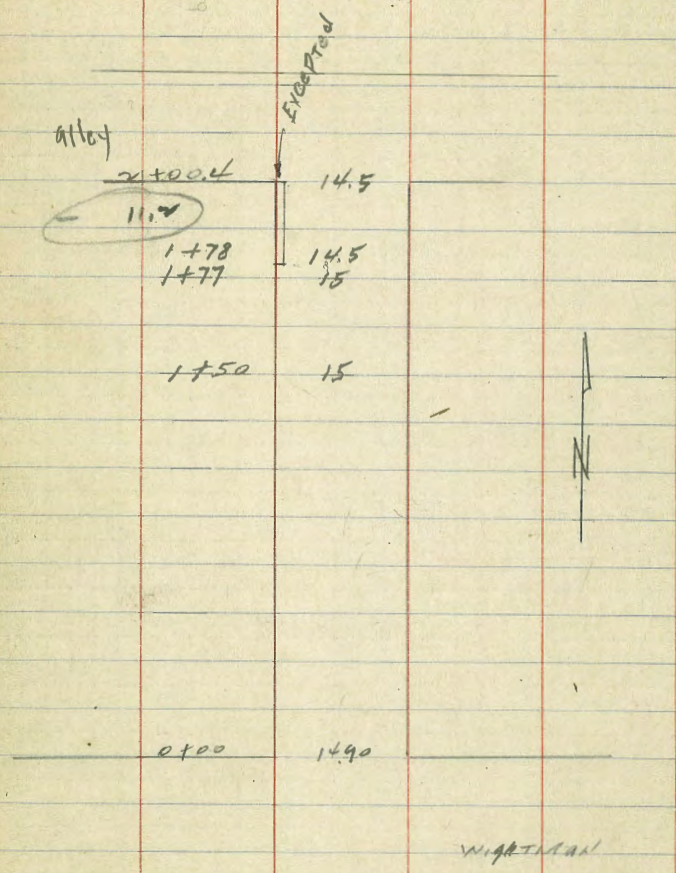
Paved June 12, 13, 14
1940

14.85	0+00	148.85
14.92	0+10	
14.90	0+50	596.40
		745.75
14.93	1	
		749.25
15.02	+50	
		751.00
15	2	
		746.25
14.85	+50	
		738.75
14.74	3	
		737.50
14.80	+50	
		738.75
14.75	4	
		728.75
14.60	+50	29.00
14.60	+52	
		706.80
14.85	5	147.75
14.70	5+10	
14.95	+50	593.00
		595.00
14.80	5+90	147.90
14.78	6+00	8900.70

Dwight

INDEXED
EFB

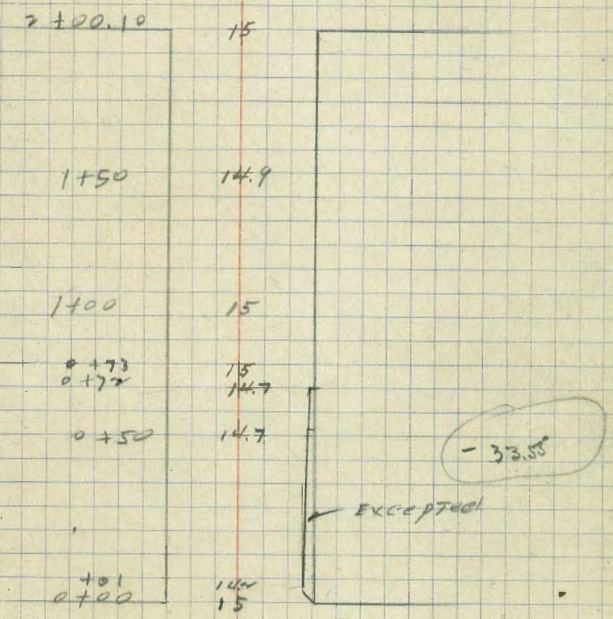
Slope Meas. alley Blk 4 Hartleys
North Park



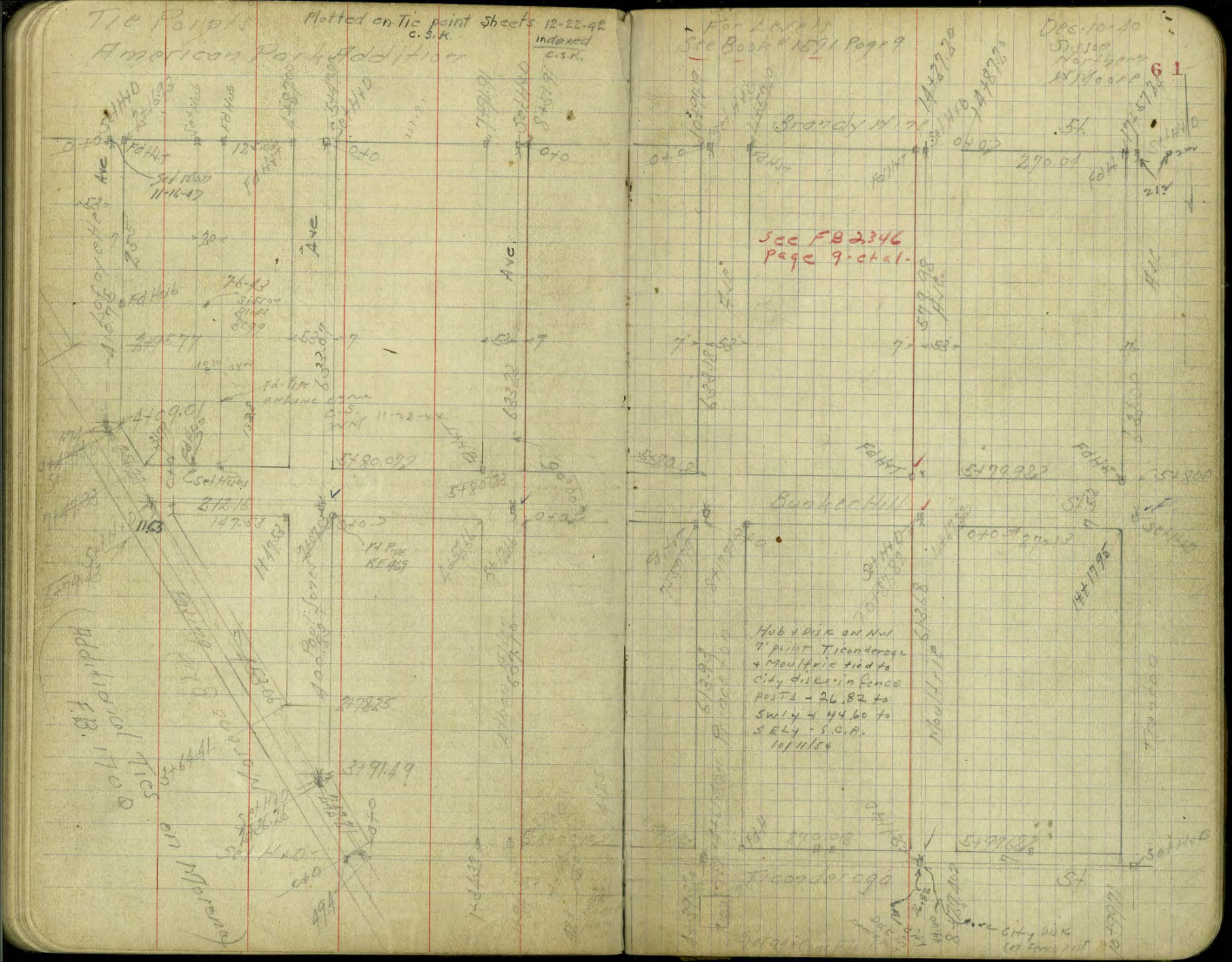
Paved 6-18-40

INDEXED
EFB

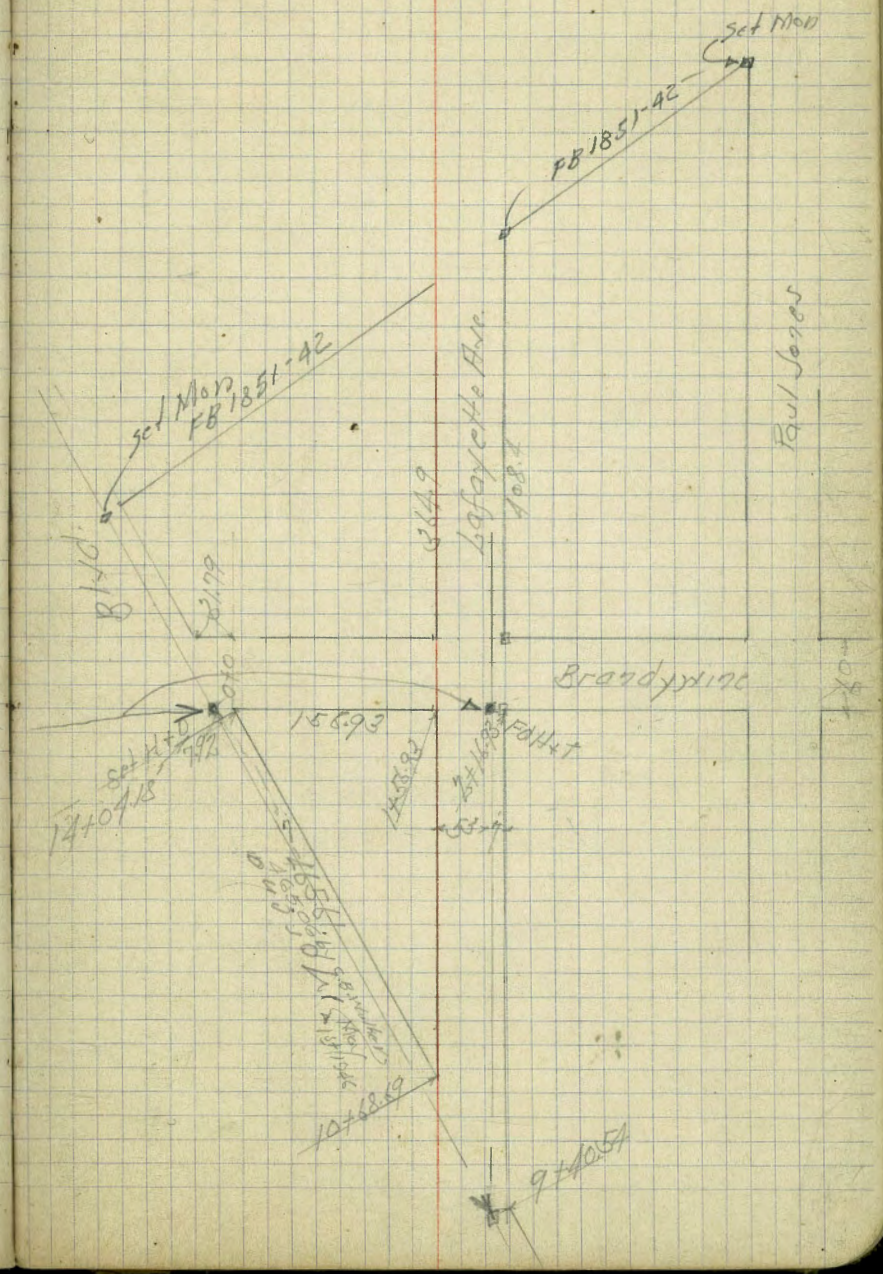
alley Blk 3 Hartleys N.P. 60



Paved 6-1-40


Tie Points
American Park Addition
Plotted on Tie point Sheets 12-22-42
C.S.K.
Indexed
C.S.K.
For Levels
See Book # 1591 Page 9
Dec. 10-40
Sisson
Northern
W Moore
61
Brandy Wine St.
See FB 2346
Page 9 - et al.
Bunker Hill
Hub + Disk on NW
7' point Ticonderoga
+ Moultrie tied to
city disks in fence
posts - 26.82 to
SWly + 44.60 to
SELy - S.C.A.
10/11/54
Moultrie
Ticonderoga St.
City Disk
Additional Ties on Morena
F.B. 1700

(Set Conc Mon
FB 1851-42)
C.B. Walker 11-16-49



Cross Section Ticonderoga St.
Moreno Blvd. to Trenton Ave.

0+50				
0+35	See Page 42 This Book			
TP	18.57	66.59	0.83	56.02
0+20	See Page 42			
0+0 =	E.L. Moreno Blvd on N			
0-37				
0-41	Taken on Dig			
0-49.4 =	E.L. Paving on North	Taken on Dig		
TP	8.62	56.85	4.13	48.73
TP	8.19	52.36	1.18	44.17
BM	10.40	45.55		34.95

B.B.P. Sodiaf RR Cut N.F. 261

Notes Reduced 1-13-41 C.B.H.

Dec 18-40

55.2
11.4 11.5
Rt = S 60 7 5 3

Lt Filling = Baseline

58.5	57.5	54.4	55.4	54.7	56.6	56.6	56.9
8.1	9.1	12.2	11.2	11.9	10.0	10.0	9.7
10		3	13	23	34	28.5	35

66.59

54.9	53.7	51.5	51.2	51.8	51.9	51.8
2.0	3.7	5.4	5.7	5.1	5.0	5.1
10		3	23	28.5	35	60 70

54.3	53.9	48.7	48.5	52.4	52.1
2.6	3.0	8.3	8.4	4.5	4.8
10		3	28.5	33	68

48.8	49.1	48.4	47.0	46.0
8.1	7.8	8.5	9.9	9.9
25		25	50	68

48.47	48.18	47.94	47.65	47.5	
8.38	8.67	8.91	9.20	9.40	9.72
25		25	50	68	93

56.85

	Lt	N.L		Rt			
2+20	59.8	59.6	59.8	58.1	57.4	57.7	
	6.8	7.0	6.8	8.5	9.2	8.9	8.4
	10		25	28.5	38	60	70
1+94.32 = E.L. Ethan Allen	59.3	58.29	59.4	57.4	56.2	55.6	
	7.3	8.30	7.2	9.2	10.3	11.0	10.7
	10	15 Outlet Sty Pipe	24	28.5	38	60	70
1+64	60.2	59.8	58.5	56.1	55.69	54.4	
	6.4	6.8	8.1	10.5	10.90	12.2	12.6
	10		23	28.5	32 Outlet 15 Steel Culv.	60	70
1+34.32 = N.L. Ethan Allen	60.5	59.8	58.4	56.9	55.8	53.6	
	6.1	6.8	8.2	9.7	10.8	13.0	13.6
	10		23	28.5	38	60	70
1+08	61.1	60.8	58.6	58.2	58.7	58.3	55.9
	5.5	5.8	8.0	8.4	7.9	8.3	10.7	11.5
	10	2		23	28.5	38	60	70
1+0	61.2	60.8	57.9	57.9	59.1	59.3	58.6	56.6
	5.4	5.8	8.7	8.7	7.5	7.3	8.0	10.0	10.8
	10		3	23	25	28.5	38	60	70

0+70 287 Sof N.L. = Sly Power Pole
66.59

66.59

Ticonderago

3+85 34' S of NL = ℄ 16" Olive Tree

3+75

3+69 34' S of NL = ℄ 10" Oliver Tree

TP 11.69 76.67 1.61 64.98

3+60 51' S of NL = ℄ 36" Palm Tree

3+46 28.5 S of NL = Sly Power Pole

3+42 = NW Cor Wire Fence 29.2 S of NL

3+30

3+0

2+80

2+50

66.59

Lt	NL			Rt		
68.7	68.0	67.1	64.7	65.0	64.8	63.7
8.0	8.7	9.6	12.0	11.7	11.9	13.0
10		7	10	28.5	40	60
	76.67					
67.6	67.1	66.1	64.0	64.3	63.8	62.3
+1.0	+0.5	0.5	2.6	2.3	2.8	4.3 4.8
10		7	10	28.5	40	60 70
66.6	63.9	63.4	63.9	63.4	61.7	
0.0	2.7	3.2	2.7	3.2	4.9	5.4
4		11	28.5	40	60	70
64.6	64.3	62.5	62.3	65.2	64.6	63.1
2.6	2.3	4.1	4.3	1.4	2.0	3.5 4.5
10		2	28.5	31	40	60 70
62.2	63.2	63.1	61.2	61.3	63.7	64.1 63.2
4.4	3.4	3.5	5.4	5.3	2.9	2.5 3.4 3.5
10		5	8	28.5	31	40 60 70
60.6	60.2	60.8	60.1	60.5	61.2	
6.0	6.4	5.8	6.5	6.1	5.4	5.5
10		13	28.5	38	60	70
	66.59					

6+0					
5+50	—				
TP	11.08	87.30	0.45	76.22	
4+99.32 = E.L. Princeton					
BM			9.06	67.61	N.W. Hub Ticonderoga & Prince West
4+71 = N.E. Cor Wire Fence 29.65 of N.L.					
4+69.32					
4+61 = ℄ Garage Conc Floor					
4+39.32 = N.L. Princeton					
4+07					
		76.67			

LT NL RT

85.3	84.0	83.3	81.5	80.5	77.6	76.0
7.0	3.3	4.0	5.8	6.8	9.7	11.3 12.8
10		6	10	28.5	40	60 70
81.3	80.3	79.3	77.7	76.8	74.6	72
6.0	7.0	8.0	9.6	10.5	12.7	15.1 15.9
10		7	11	28.5	40	60 70
	87.30					
	74.9	74.3	72.6	72.7	71.8	68.0
	1.8	2.4	4.1	4.0	4.9	8.7 9.1
		6	10	28.5	40	60 70
72.5	71.2	69.5	69.7	68.6	67.7	65.4
4.2	5.5	7.2	7.0	8.1	9.0	11.3 11.5
10		11	24	28.5	40	60 70
			65.72			
			10.95			
			53.35 = ℄ N. Garage Conc Floor			
	69.0	67.0	66.5	66.1	65.0	
	7.7	9.7	10.2	10.6	11.7	11.9
		11	28.5	40	60	70
68.9	67.9	65.4	65.5	65.49	65.45	
7.8	8.8	11.3	11.2	11.18	11.22	
10		10	28.5	29.3 - 47 Conc Walls	47 - 54 Footing 74 Pond	
	76.67					

Ticonderoga

7+99.40 = ℄					
7+69.40 = W.L. Moultrie					
BM	12.11	90.36	90.5	78.25	NW 7 Hub Ticonderoga + Moultrie
7+45					
7+10					
6+80					
6+50		87.30			

Lt W.L. Rt

79.7	78.9	77.4	78.7	79.2	79.0	
10.7	11.5	13.0	11.7	11.2	11.4	11.7
10		15	28.5	50	60	70

80.4	78.7	76.4	75.4	75.7	
10.0	11.7	14.0	15.0	14.7	14.4
10		28.5	40	60	70

90.36

81.8	78.3	76.6	75.4	74.8	
5.5	9.0	10.7	11.9	12.5	12.3
	9	28.5	40	50	70

86.7	80.7	79.7	78.3	75.3	74.6
0.6	6.6	7.6	9.0	12.0	12.7 13
	12	25	28.5	40	60 70

86.9	85.8	83.1	81.8	76.8	74.7
0.4	1.5	4.2	5.5	10.5	12.6 14.7
	7	11	28.5	40	60 70

87.8	86.4	85.5	84.0	82.1	79.5	75.5
10.5	0.9	1.8	3.3	5.2	7.8	11.8 13.5
10		6	8	28.5	40	60 70

87.30

Con't Page 75

9+50				
9+25				
TP	12.09	101.35	1.10	89.26
9+0				
8+50				

8+29.40 = FL Nov Hrie

90.36

Lt HL Rt

93.6	98.0	99.2	102.4	102.8	105.9	
7.8	3.4	2.2	+1.0	+1.4	+4.5	+6.6
20		11	17	28.5	60	70
85.4	89.5	91.4	96.0	96.9	100.3	
16.0	11.9	10.0	5.4	4.5	1.1	+1.4
20		8	17	28.5	60	70
	101.35					
82.4	83.5	85.2	90.9	91.4	95.9	
8.0	6.9	5.2	+0.5	+1.0	+5.5	+6.5
20		9	18	28.5	60	70
80.0	80.3	80.4	82.3	82.8	83.3	82.4
10.4	10.1	10.0	8.1	7.6	7.1	8.0 7.5
20		13	17	28.5	40	60 70
78.4	79.6	79.1	80.2	81.3	81.5	81.6
11.0	10.8	11.3	10.2	9.1	8.9	8.8 8.6
10		15	17	28.5	50	60 70
	90.36					

Cross Section Moultrie St.
Ticonderoga to Brandywine

5+0				
TP	11.93	114.08	0.12	102.15
5+25				
5+50				
TP	12.07	102.27	0.23	90.20
5+60				
5+85				
5+99.68	N.L. Ticonderoga			
BM	12.18	90.43		78.25

Notes Red. 1-13-41 CDK

HW 7 Mo. Ticonderoga & Moultrie

Dec 14-40

60 Yd.

N. ℄ E.

103.6	103.8	103.4	103.1	102.4	102.6	101.1
10.5	10.3	10.7	11.0	11.7	11.5	13.0
10	30	15		15	30	40

114.08

98.5	98.2	97.4	97.1	96.5	95.7	92.9
3.8	4.1	4.9	5.2	5.8	6.6	9.4
10	30	15		15	30	40

92.9	92.4	90.2	90.3	88.9	86.4	85.0
9.4	9.9	12.1	12.0	13.4	15.9	17.3
10	30	15		17	30	40

102.27

90.1	88.9	86.7	86.0	85.6	82.7	81.7
0.3	1.5	3.7	4.4	4.8	7.7	8.7
10	30	15		17	30	50

81.9	80.6	80.5	80.4	80.1	79.7	79.6
8.5	9.8	9.9	10.0	10.3	10.7	10.8
10	30	15		15	30	50

90.43

2+0				
TP	12.43	149.36	0.13	136.93
2+50				
3+0				
TP	11.93	137.06	0.25	125.13
3+50				
4+0				
TP	11.66	125.38	0.36	113.72
4+50				
		114.08		

135.1	136.9	139.6	141.0	142.2	144.1	145.1
7.3	1.5	9.8	8.4	7.2	5.3	4.3
40	30	15		15	25	30

149.36

131.6	132.8	134.6	136.6	136.6	137.1	139.7
5.5	4.3	2.5	0.5	0.5	+2.0	+2.6
40	30	15		20	25	30

126.9	127.8	128.1	130.6	130.9	133.0	133.9
10.2	9.3	8.0	6.5	6.2	4.1	3.2
40	30	15		18	21	30

137.06

122.6	123.1	123.8	125.4	126.1	127.7
2.8	2.3	1.6	0.0	+0.7	+2.3
40	30	15		15	30

116.7	117.0	116.6	118.6	119.0	119.6	120.5
8.7	8.4	8.8	6.8	6.4	5.8	4.9
40	30	15	7		15	30

125.38

110.6	111.4	111.7	112.4	112.3	113.3	113.1
3.5	2.7	2.4	1.7	1.8	0.8	1.0
40	30	10		15	30	20

114.08

Moultrie

5+79.98 = N.L. Bunkerhill				
L Bunkerhill				
BM		9.72	151.82	SW 7 Hub Bunker Hill & Moultrie
0+0 = S.L. Bunkerhill				
0+50				
1+0				
TP	12.38	161.54	0.20	149.16
1+50				
		149.36		

159.4	154.0	155.0	155.5	157.9	152.5	159.8	160.3
8.1	7.5	6.5	6.0	3.6	9.0	1.7	1.2
40	30	15		15	20	25	30

151.9	152.5	153.8	155.2	157.2	159.6
9.6	9.0	7.7	6.3	4.3	1.9
40	30	15		15	30

149.1	150.1	152.3	153.8	155.6	157.0	158.4
12.4	11.4	9.2	7.7	5.9	4.5	3.1
40	30	15		17	20	30

145.9	147.1	150.3	151.9	153.4	155.3	157.3
15.6	14.4	11.2	9.6	8.1	6.2	4.2
40	30	15		17	21	30

143.0	144.3	147.7	149.9	151.2	153.0	154.3
18.5	17.2	13.8	11.6	10.3	8.5	7.2
40	30	15		18	21	30

161.54

139.4	141.3	144.2	145.4	147.1	149.2	150.6
10.0	8.1	5.2	4.0	2.3	0.2	+1.2
40	30	15		18	21	30

149.36

TP	12.31	195.76	0.26	183.45
3+0				
3+50				
4+0				
TP	11.42	183.71	0.42	172.29
4+50				
5+0				
TP	11.32	172.71	0.15	161.39
5+50				
		161.54		

179.1	179.6	180.4	181.9	181.5	176.5	172.9	183.7
4.6	4.1	3.3	2.0	2.2	7.2	6.8	0.0
40	30	15		16	18	21	30

174.6	175.7	176.5	177.8	177.8	172.6	179.3	180.3
9.1	8.0	7.2	5.9	5.9	11.1	4.4	3.4
40	30	15		16	18	23	30

170.3	171.2	172.4	173.4	173.7	169.3	175.3	176.1
13.4	12.5	11.3	10.3	10.0	14.4	8.4	7.6
40	30	15		16	20	23	30

183.71

165.6	166.4	167.3	168.8	169.3	162.7	171.2	172.5
7.1	6.3	5.4	3.9	3.4	10.0	1.5	0.2
40	30	15		15	20	25	30

170.5	161.4	162.4	163.8		164.1	159.0	156.0	166.7
12.2	11.3	10.3	8.9		8.6	13.7	6.7	6.0
40	30	15			15	20	25	30

172.71

155.5	156.7	157.8	159.2	160.3	155.0	161.9	163.5
6.0	4.6	3.7	2.3	1.2	6.5	+0.4	+2.0
40	30	15		15	20	23	30

161.54

Moultrie

BM			7.70	199.54	Hub S.L. Brandywine W of L Moultrie
0+0 = S.L. Brandywine					
0+50					
1+0					
TP	12.09	207.24	0.61	195.15	
1+50					
2+0					
2+50					
		195.76			

N E

198.1	199.0	200.2	201.9	202.0	203.6
9.1	8.2	7.0	5.3	5.2	3.6
40	30	15		15	30

193.1	194.2	196.6	198.4	198.8	~~207.2~~ 200.2
14.1	13.0	10.6	8.8	8.4	7.0
40	30	15		15	30

191.9	192.9	194.4	196.1	196.2	197.7
15.3	14.3	12.8	11.1	11.0	9.5
40	30	15		15	30

207.24

190.6	191.5	192.3	194.0	193.3	195.1	195.7
5.2	4.3	3.5	1.8	2.5	0.7	0.1
40	30	15		19	21	30

187.9	188.2	188.7	190.0	189.4	190.5
7.9	7.6	7.1	5.8	6.4	5.3
40	30	15		15	30

183.3	183.9	184.8	185.9	185.6	186.6
12.5	11.9	11.0	9.9	10.2	9.2
40	30	15		15	30

195.76

Check Levels

BM	1.15	200.69		199.54	Hub S.L. Brandywine W 7 L Moultrie
TP	0.08 +	188.78	11.99	188.70	
TP	0.07	176.60	12.25 +	176.53	
BM			1.37	175.23	Hub S.L. Brandywine W 7 L Princeton
TP	0.19	164.40	12.39	164.21	
TP	0.22	152.33	12.29	152.11	
BM			11.00	141.33	SE Prop Cor Brandywine + Ethan Allen
TP	0.25 +	140.22	12.36	139.97	
TP	0.27 -	128.39	12.10	128.12	
BM			10.71	117.68	Hub SW Cor Brandywine + Paul Jones
TP	0.54	116.53	12.40	115.99	
TP	0.21	104.54	12.20 -	104.33	
BM			6.61	97.93	Hub SE Cor Brandywine + Lafayette

Dec 17-40
Sisson
W Moore

		104.54			
TP	0.10	92.22	12.42	92.12	
TP	0.22	80.01	12.43	79.79	
TP	0.35	68.05	12.31	67.70	
BM			7.42	60.63	Hub S.L. Brandywine E 7 L Morena
TP	1.08	63.68	5.45	62.60	
BM			3.96	59.72	Nail Pole SE Bunker Hill + Morena
TP	1.67	55.94	9.41	54.27	
TP	1.46	49.87	7.53	48.41	
TP	1.55	43.63	7.79	42.08	
BM			8.74	34.89	E.B.P. Santa Fe RR Culv. F261 34.95

Cross Section Ticonderoga St
Morena Blvd to Trenton Ave

TP	12.01	136.86	0.25	124.85	
10+50					
10+25					
10+0					
TP	11.95	125.10	0.0	113.15	
9+75					
TP	12.07	113.15	0.24	101.08	
TP	12.10	101.32	0.48	89.22	
BM	11.45	89.70		78.25	NW 7 Hub Ticonderoga & Moultrie P67

Ford From Page 68

Jan 6 4

Lt. N HL Rt. S

75

123.2	124.7		125.9	128.1	
1.9	0.4		+0.8	+3.0	+3.2
15			28.5	60	70
				123.9	
				1.2	0.8
				60	70
118.0	120.1	120.1	117.7	119.9	120.4
7.1	5.0	5.0	7.4	5.2	4.7
15		7	10	15	28.5
111.1	113.3	114.3	110.6	114.1	114.7
14.0	11.8	10.8	14.5	11.0	10.4
15		9	13	15	28.5
				119.4	
				5.7	6.0
	125.10			60	70
104.5	106.8	105.9	108.0	109.1	114.1
8.7	6.4	7.3	5.2	4.1	+0.9 +1.4
15		7	10	28.5	60 70
	113.15				

11+28					
BM			11.22	135.84	NW 7' Hub Ticonderoga & Trenton
TP	10.76	147.06	0.56	136.30	
10+99.71 = N.L. Trenton					
10+75					
		136.86			

Lt NL 5

142.1 141.7 141.4
5.0 5.4 5.7 6.2
28.5 60 70

147.06

135.9 135.1 135.5 136.9
1.0 1.8 1.4 0.0 -0.3
15 28.5 60 70

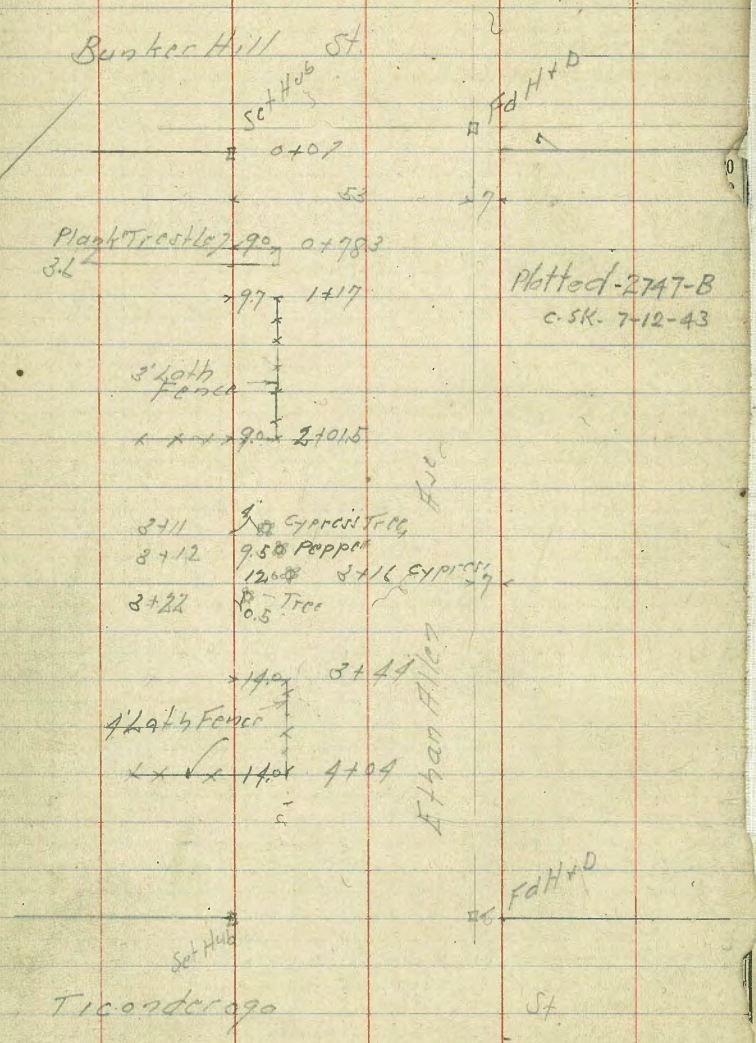
128.5 130.1 131.1 132.7
8.4 6.8 5.8 4.2 4.6
15 28 60 70

136.86

77 Location of Fences in Ethan Allen Ave Between Ticonderoga & Bunker Hill

Indexed C.S.K.

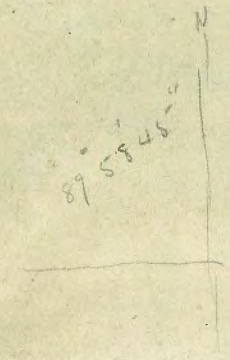
July 10-43
Sissor
Bliss
Begg



Plotted-2747-B
C.S.K. 7-12-43

180.07
75
255
120
135

75.03



ENGINEERING DEPARTMENT,
CITY OF EAST SAN DIEGO,
CALIFORNIA.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.