MINING
TRANSIT BOOK
363

F.B.570

KEUFFEL & ESSER CO.
DRAWING MATERIALS
AND
SURVEYING INSTRUMENTS.
NEW YORK.
CHICAGO. SAN FRANCISCO. ST. LOUIS.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EXCAVATION.

"Copyright, 1895, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MICROFILMED
JUL 11 1964

Alignment
East of Fairmount -

OFFICE OF THE CITY ENGINEER
EAST SAN DIEGO CAL.

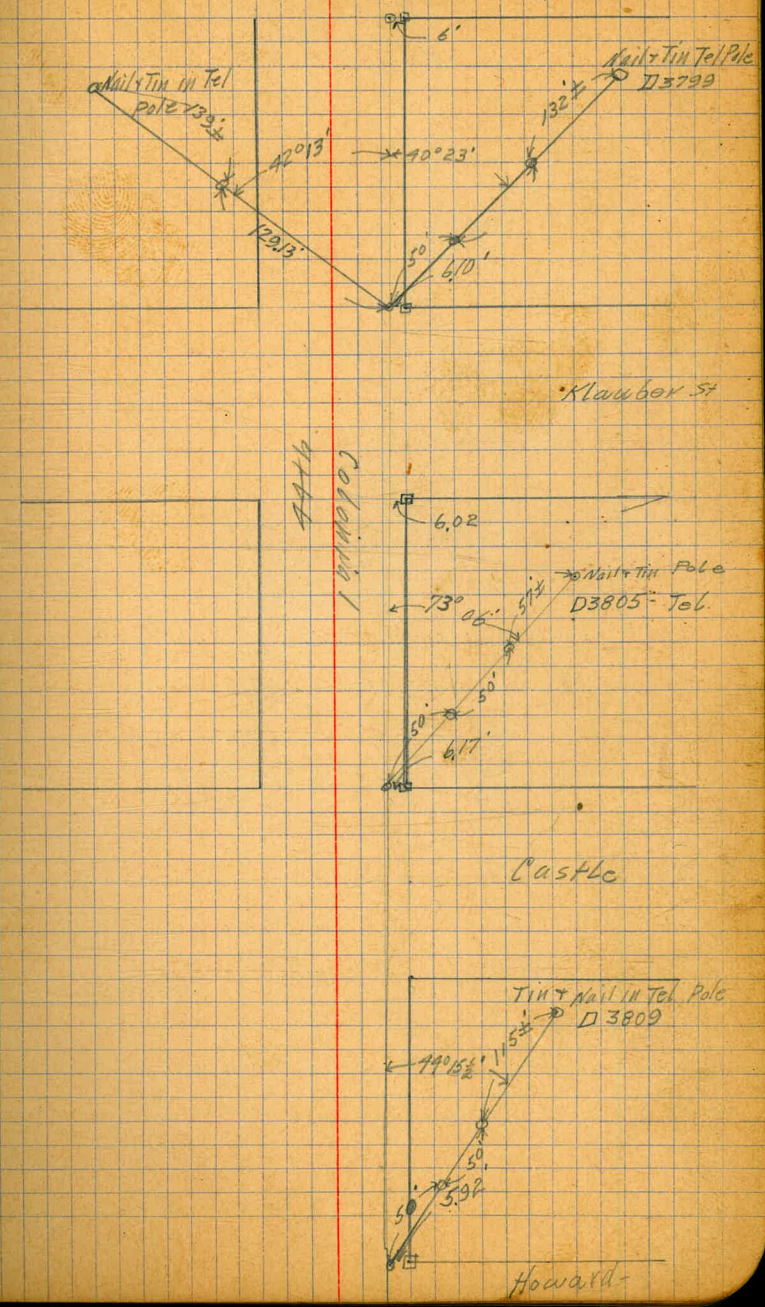
Indexed to date Feb 26, 1918.
Card " " " Mar 21, 1918

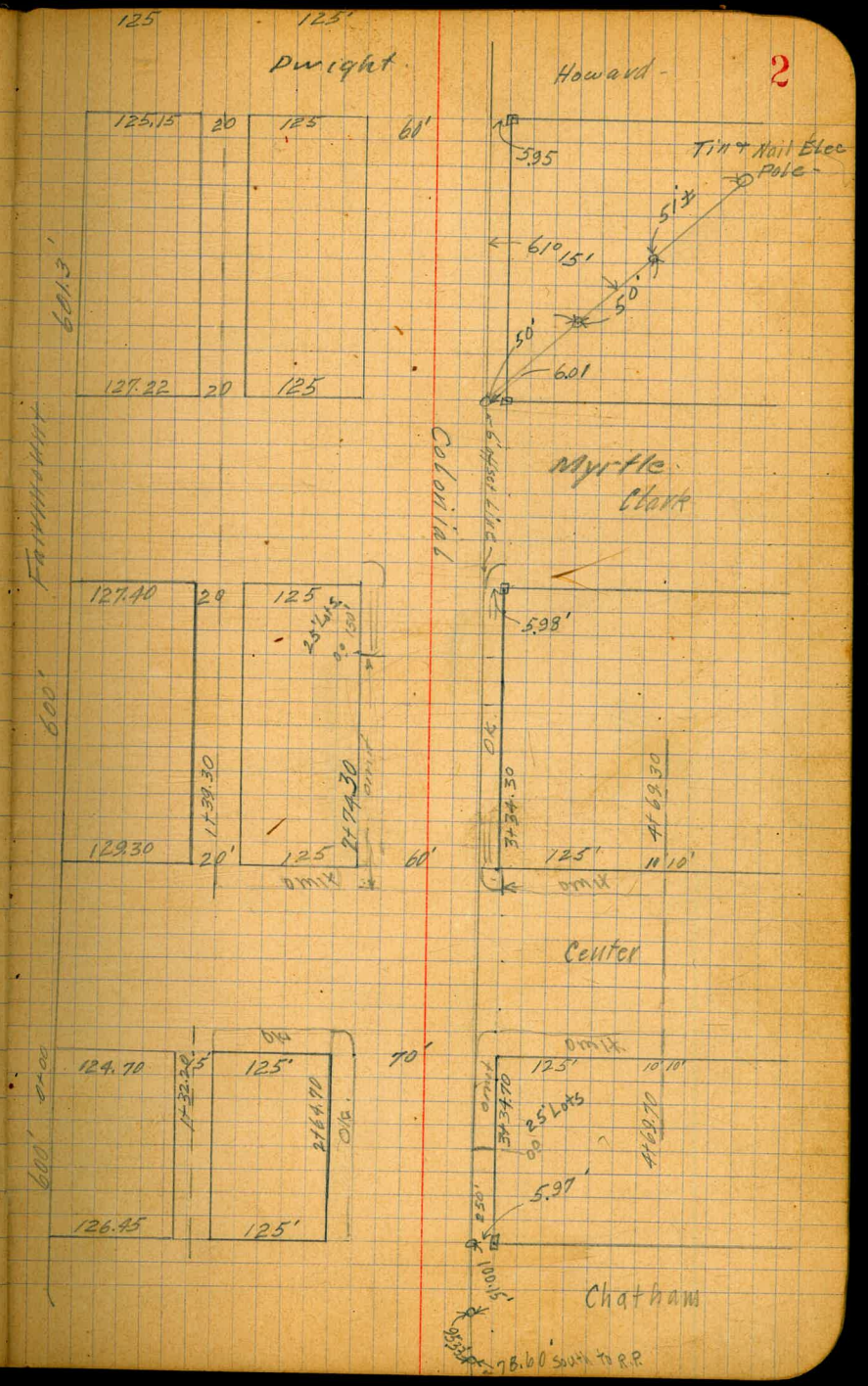
29.5
13

Index	Page
Alignment of Colonial	1-2
Diagram of Euclid	3-4
Alignment of Highland	5-6
Diagram of Chamoune	8
Alignment University	7+9
" Cabrillo	11-12

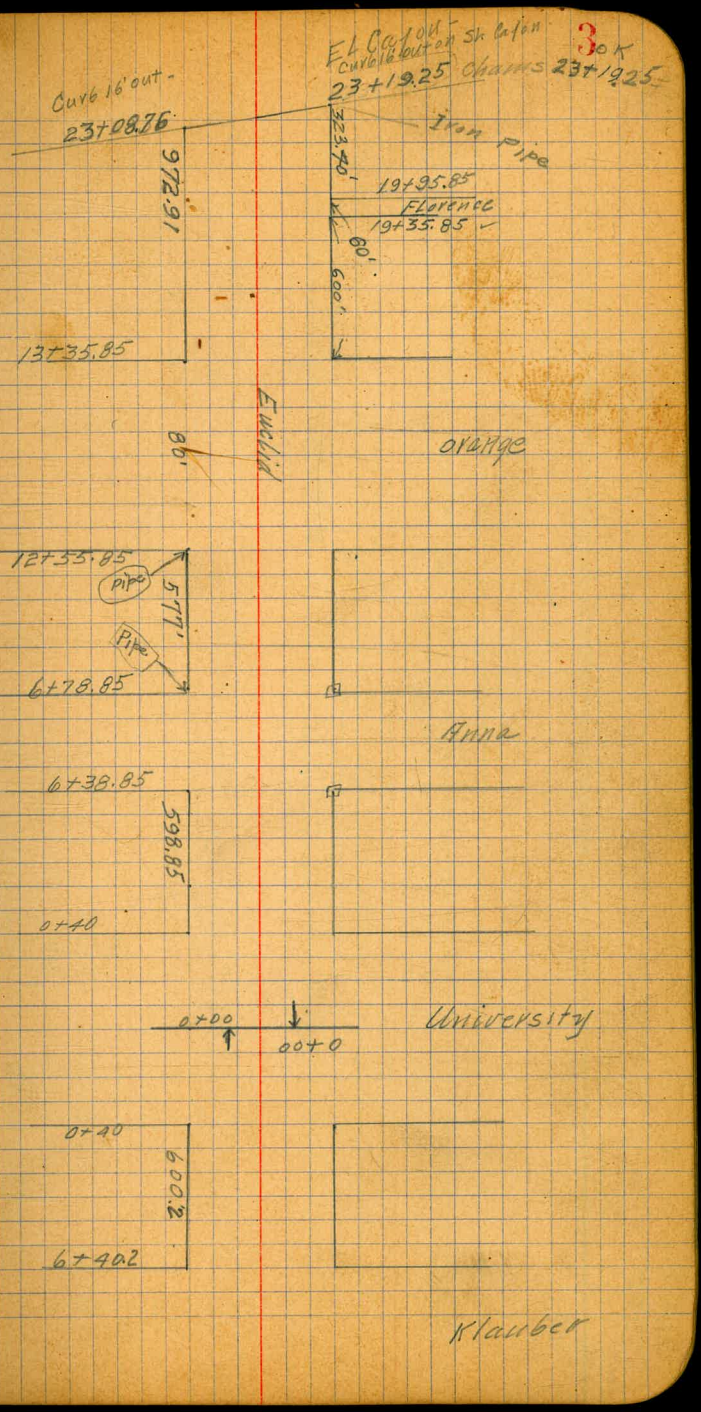
Sept 11-12-1914
Ford
Graf
Knudtson

1

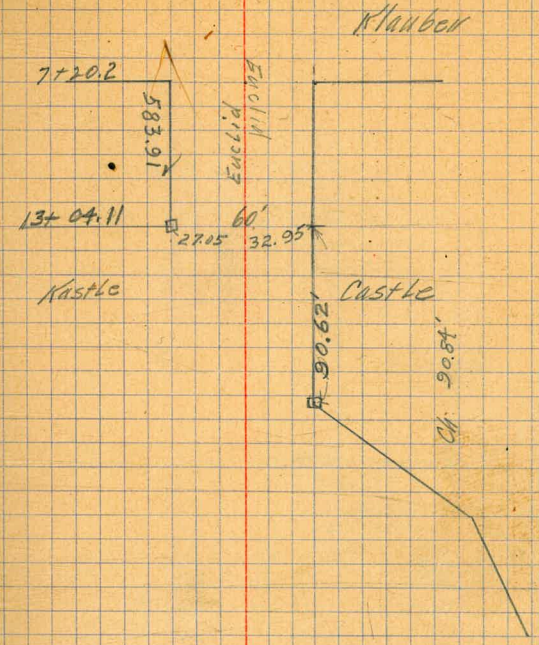




125
125'
Dwight
Howard
125.15
20
125
60'
5.95
Tin + Nail Elec Pole
51'±
61° 15'
50'
50'
6.01
601.3'
127.22
20
125
Fairmount
Colonial
Myrtle
Clark
127.40
20
125
25' Lots
5.98'
600'
1+39.30
2+74.30
3+34.30
4+69.30
129.30
20'
125
60'
125'
10' 10'
omit
Center
124.70
125'
70'
125'
10' 10'
1+32.20
2+64.70
3+34.70
25' Lots
4+69.70
600'
5.97'
126.45
125'
Chatham
78.60' south to R.P.

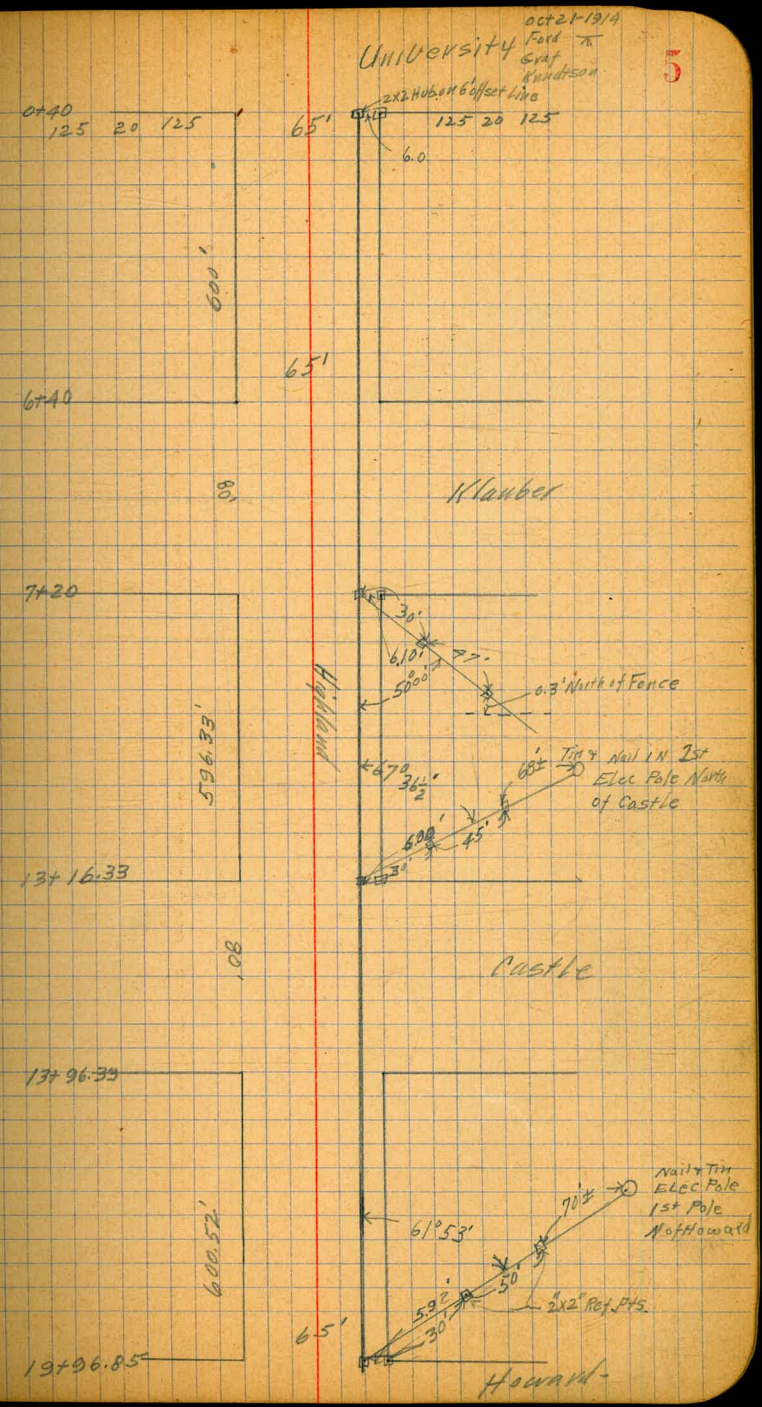


El Cajon
Curb 16' out on St. Cajon
3 OK
23+19.25 Chams 23+19.25
Curb 16' out
23+08.76
Iron Pipe
323.40'
19+95.85
Florence
19+35.85
972.91
80'
600'
13+35.85
Euclid
80'
Orange
12+55.85
Pipe
577'
Pipe
6+78.85
Anna
6+38.85
598.85
0+40
0+00
00+0
University
0+40
600.2
6+40.2
Klauber


Klauber
7+20.2
583.91
Euclid
Euclid
13+04.11
27.05
60'
32.95
Kastle
Castle
90.62'
Ch. 90.84'

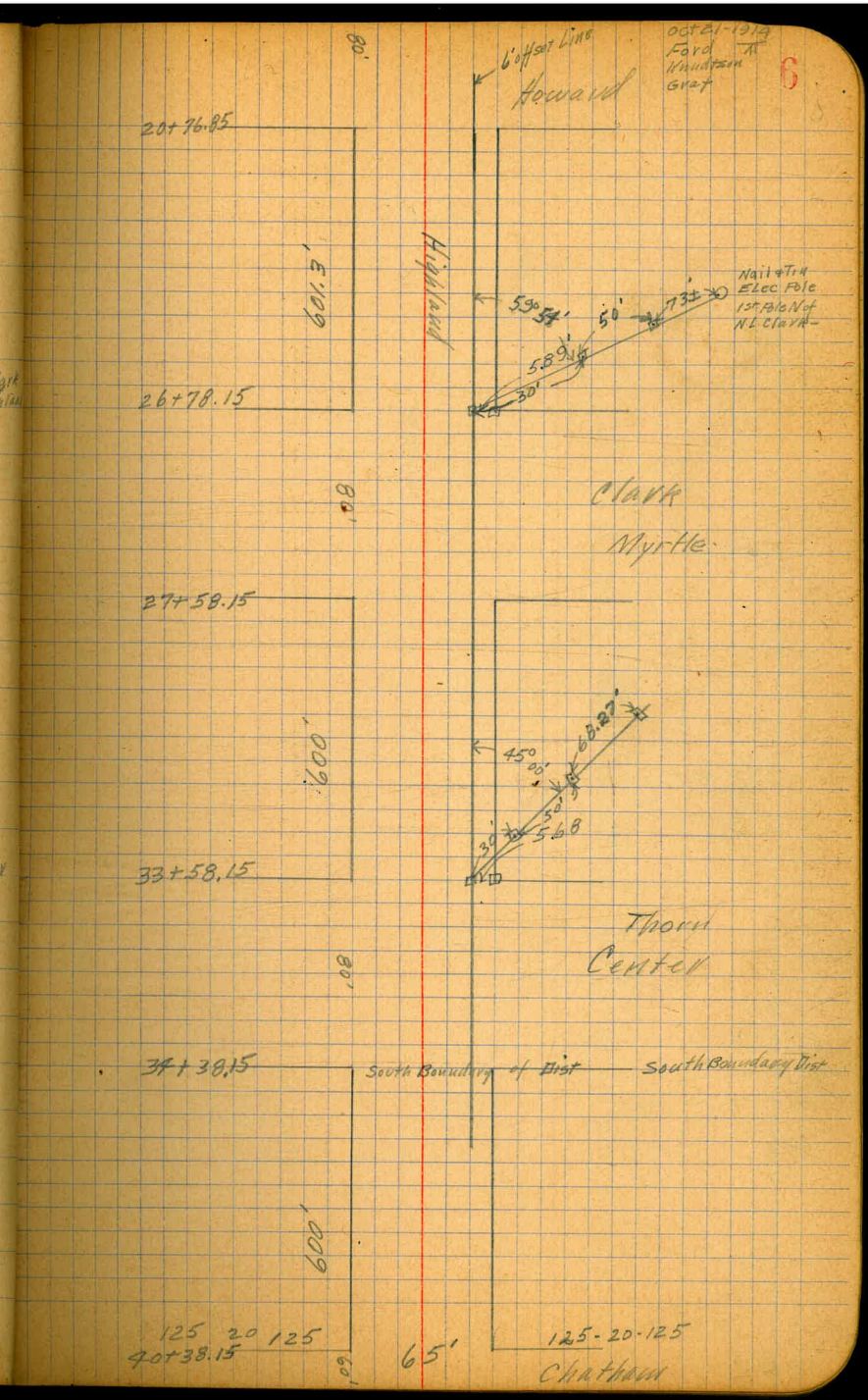
Pt Referenced Here is on a Line 6' W of EL. + .08's of SL Klauber

Pt. Ref is on New 6' Line 6' West + 0.11' N of NE. Howard + Highland



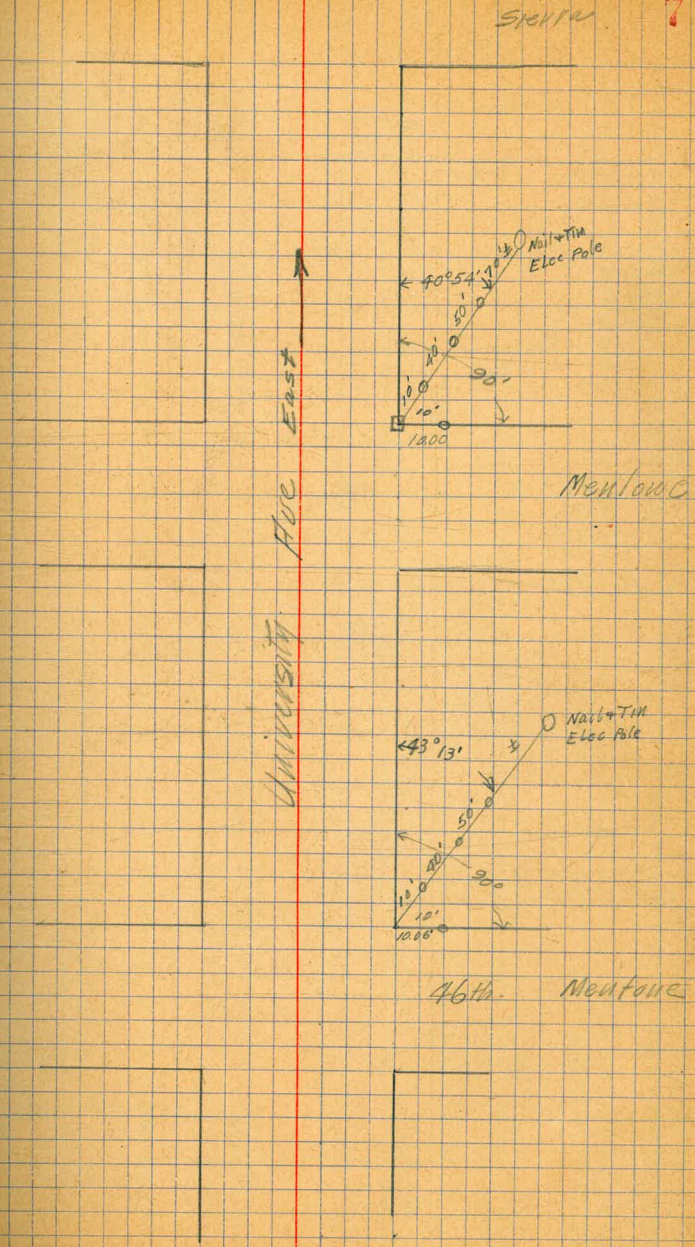
Pt Ref here is on a line 6' W of E.P.L & 0.42' N of NE Clark Highland

Pt Ref Here is on A line 6' W of E.P.L 8.38' N of N.L. Center

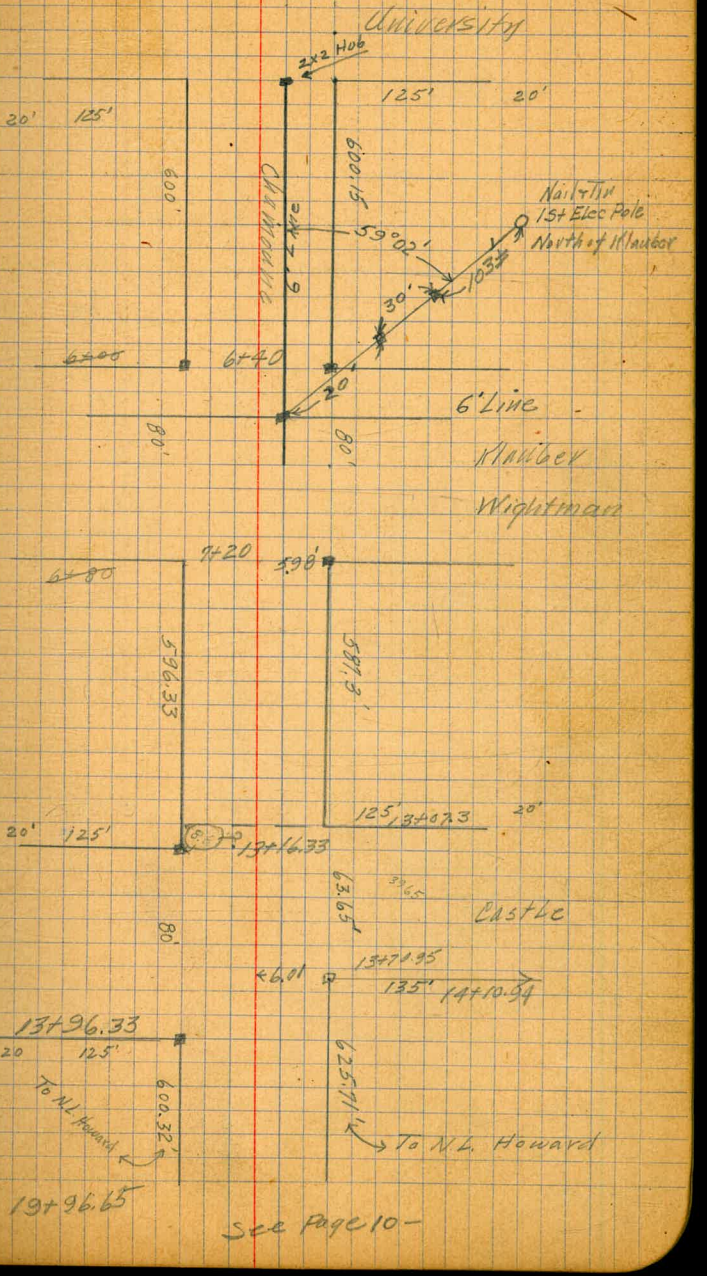


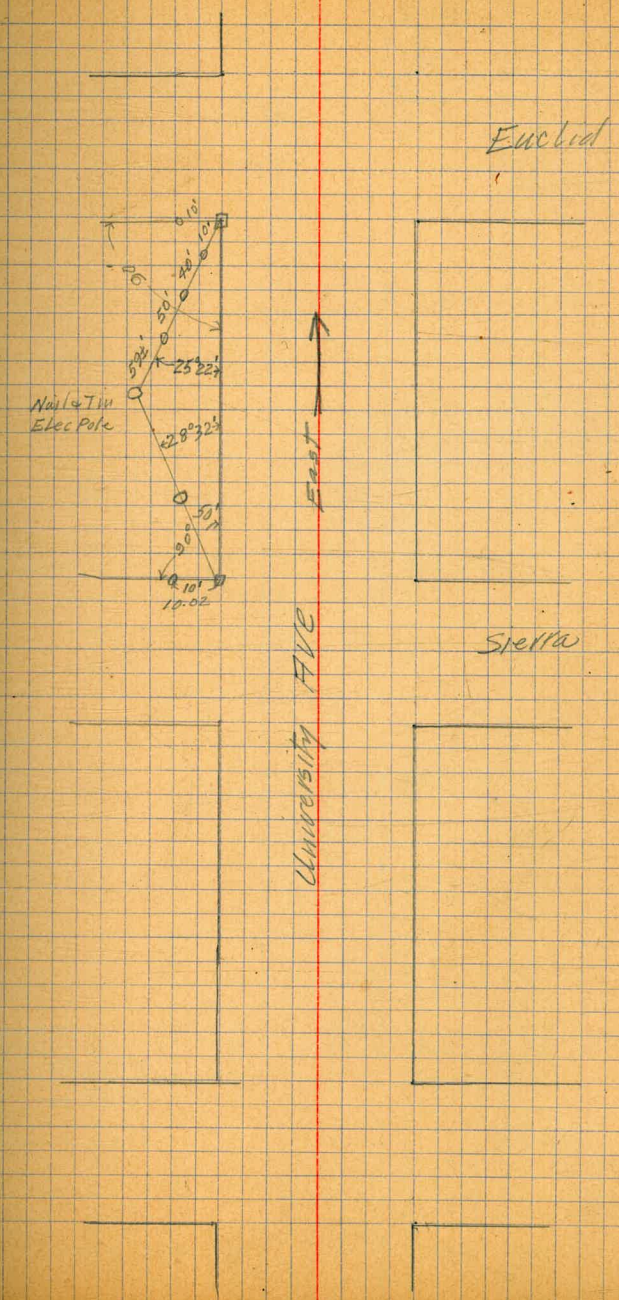
Oct 21-1919
Ford
Knudsen
Gray

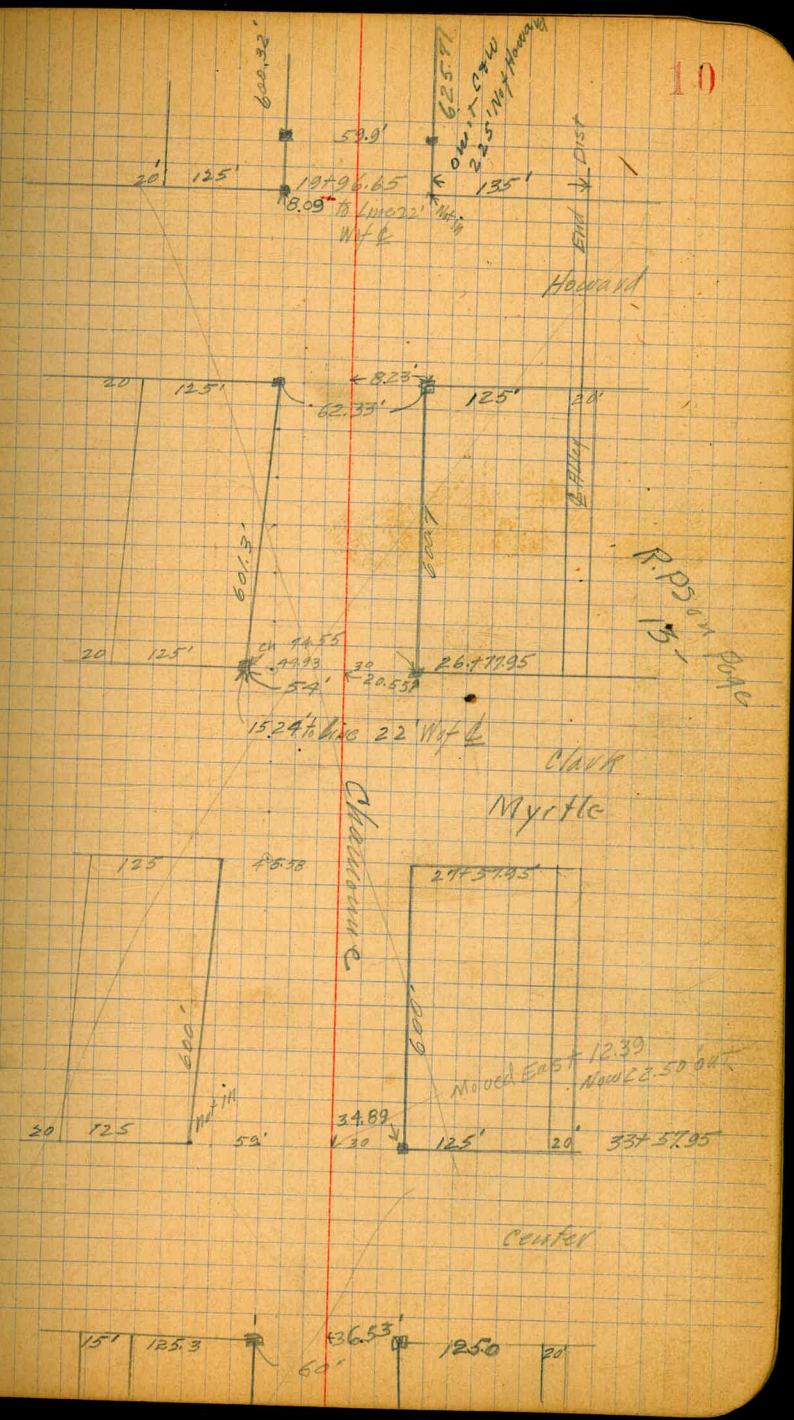
6

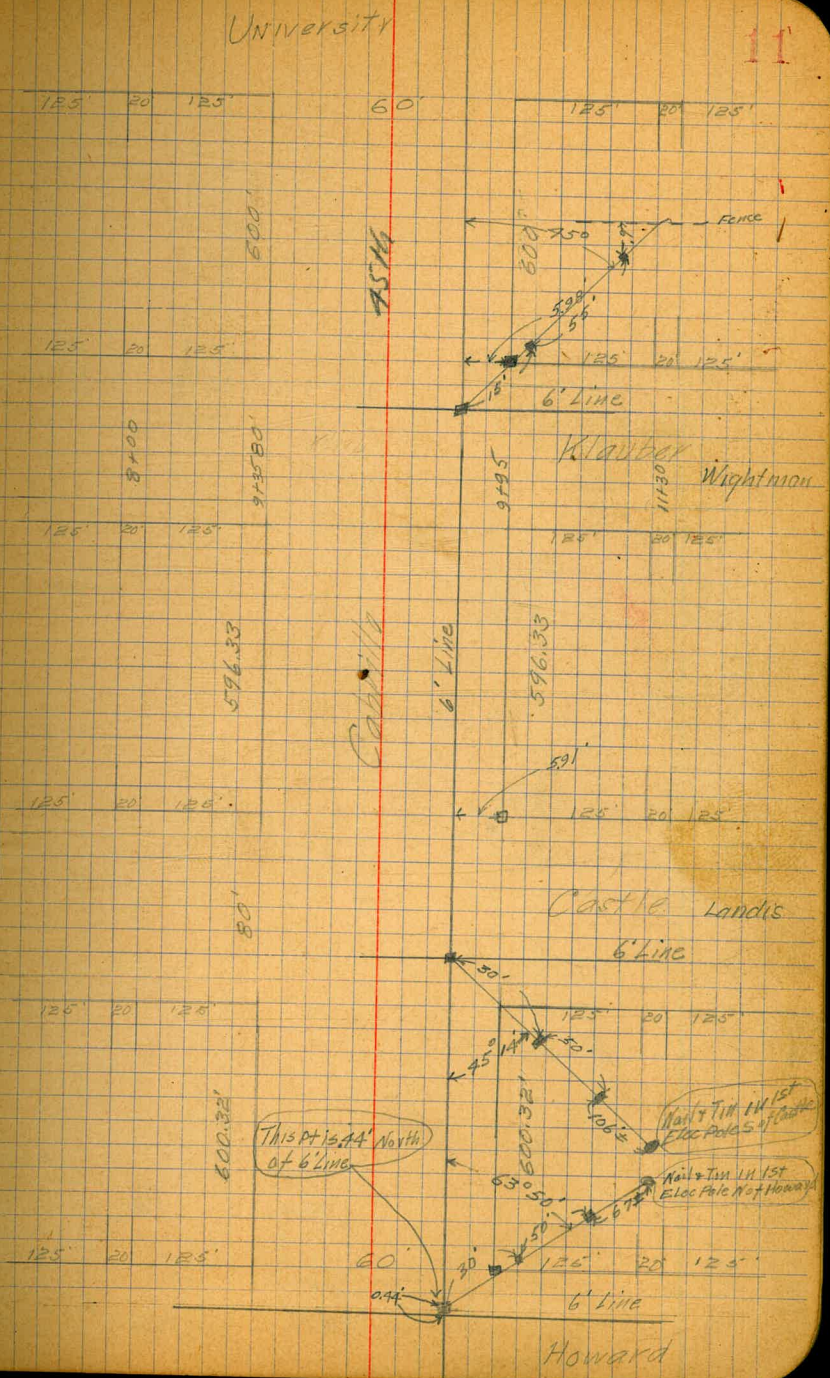

Sierra
Nail+Tin
Elec Pole
40°54'
70'
50'
40'
10'
90'
10'
10.00
Menlowe
University Ave East
Nail+Tin
Elec Pole
43°13'
50'
40'
10'
90°
10'
10.06'
46th
Menlowe

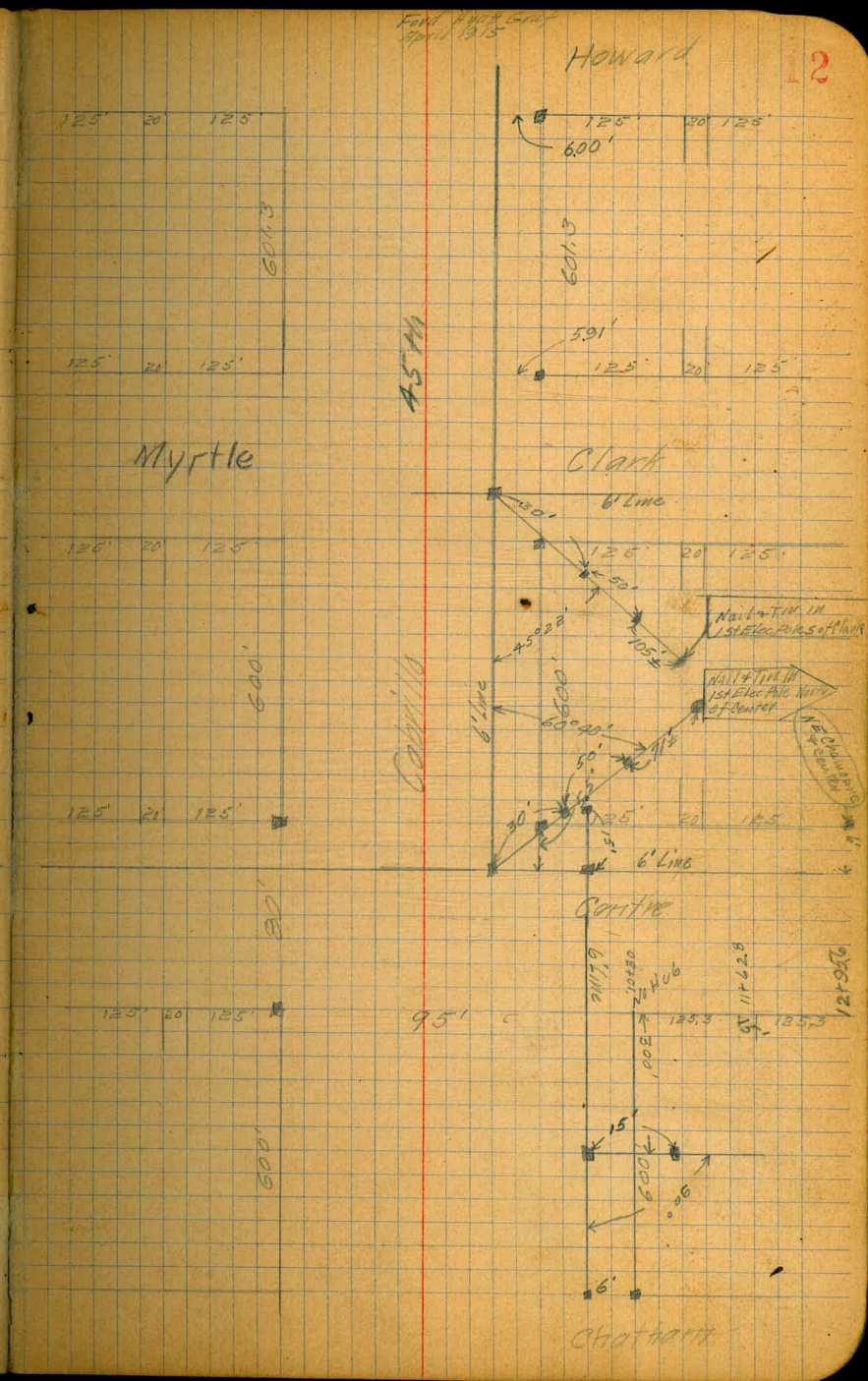
Chautauqua

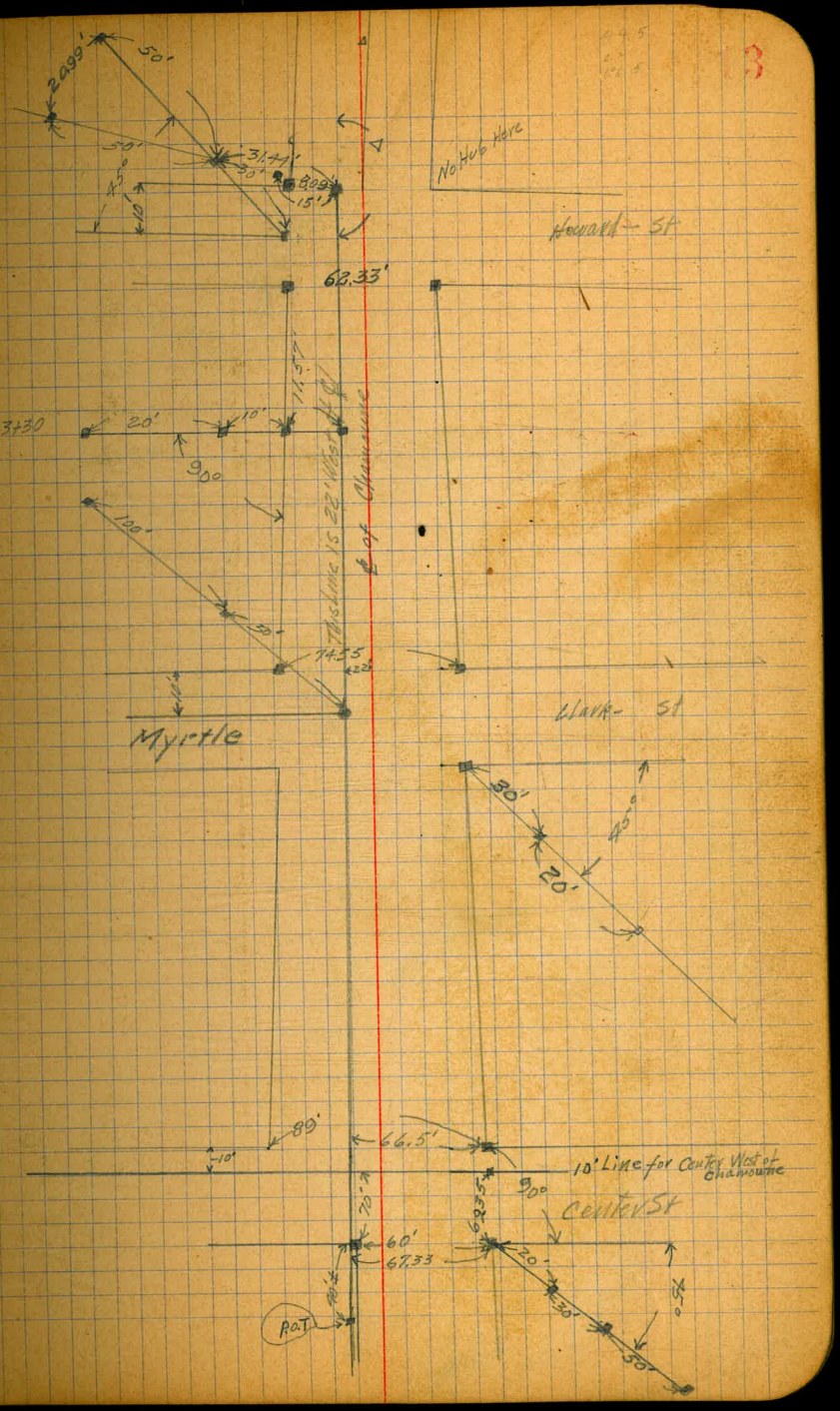

University
2x2 Hub
125'
20'
20'
125'
600'
600.15'
Chautauqua
59°02'
Nail & Tin
1st Elec Pole
North of Klauber
103'
30'
6+00
6+40
20
6' Line
Klauber
Wightman
80'
80'
7+20
5.98'
6+80
596.33'
596.3'
20'
125'
125'
13+73
20'
13+16.33
63.65'
Castle
80'
13+71.95
135'
14+10.94
13+96.33
20
125'
To N.L. Howard
600.32'
625.71'
To N.L. Howard
19+96.65
See Page 10-


Euclid
Sierra
University Ave
East
Nail & Tin
Elec Pole
10'
10'
40'
50'
25°22'
28°32'
50'
90°
10'
10.02


600.32'
625.71
59.9'
20'
125'
19+96.65
8.09' to line 22' W of ℄
135'
Dist
End
Howard
20
125'
8.23'
62.33'
125'
20'
601.3'
600.7
R. Pson Page 13
20
125'
ch 74.55
44.93
54'
30
20.55
26+77.95
15.24' to line 22' W of ℄
Clark
Myrtle
Chamoun C
125
46.58
27+57.95
600'
600'
Moved East 12.39
Now 22.50 out
20
125
59'
34.89
30
125'
20'
33+57.95
Center
15'
125.3
36.53'
125.0
20'
60'


University
125' 20' 125'
60'
600'
45 Ht
Fence
6' Line
Klauber
Wightman
8+00
9+35 80'
9+95
11+30
596.33
Cabrillo
6' Line
596.33
Castle
Landis
6' Line
80'
600.32'
This Pt is 44' North of 6' Line
Nail & Tin in 1st Elec Pole S of Castle
Nail & Tin in 1st Elec Pole N of Howard
6' Line
Howard


Ford Hyd & Grav
April 1915
Howard
Myrtle
Clark
Cabrillo
Centre
Chatham
45th
6' Line
Nail & Tin in 1st Elec Pole S of Clark
Nail & Tin in 1st Elec Pole North of Center
N.E. Chamberlin & Center
N.E. Fairmount & Center St.
125'
20'
601.3
600'
90'
95'
6.00'
5.91'
30'
50'
105'
45°22'
60°40'
15'
125.3
6'



No Hub Here
Howard St
62.33'
23+30
20'
10'
90°
This Line is 22' West of ℄ of Chamounix
74.55
Myrtle
Clark St
30'
20'
45°
89'
66.5'
10' Line for Center West of Chamounix
90°
Center St
60'
67.33
P.O.T.

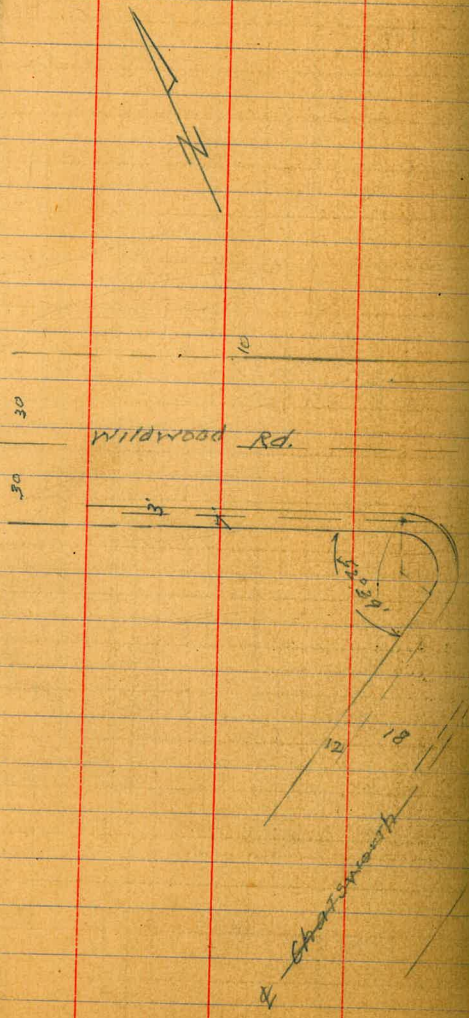
Moore
1-30-39.

Lowell St. Ext. 80' wide

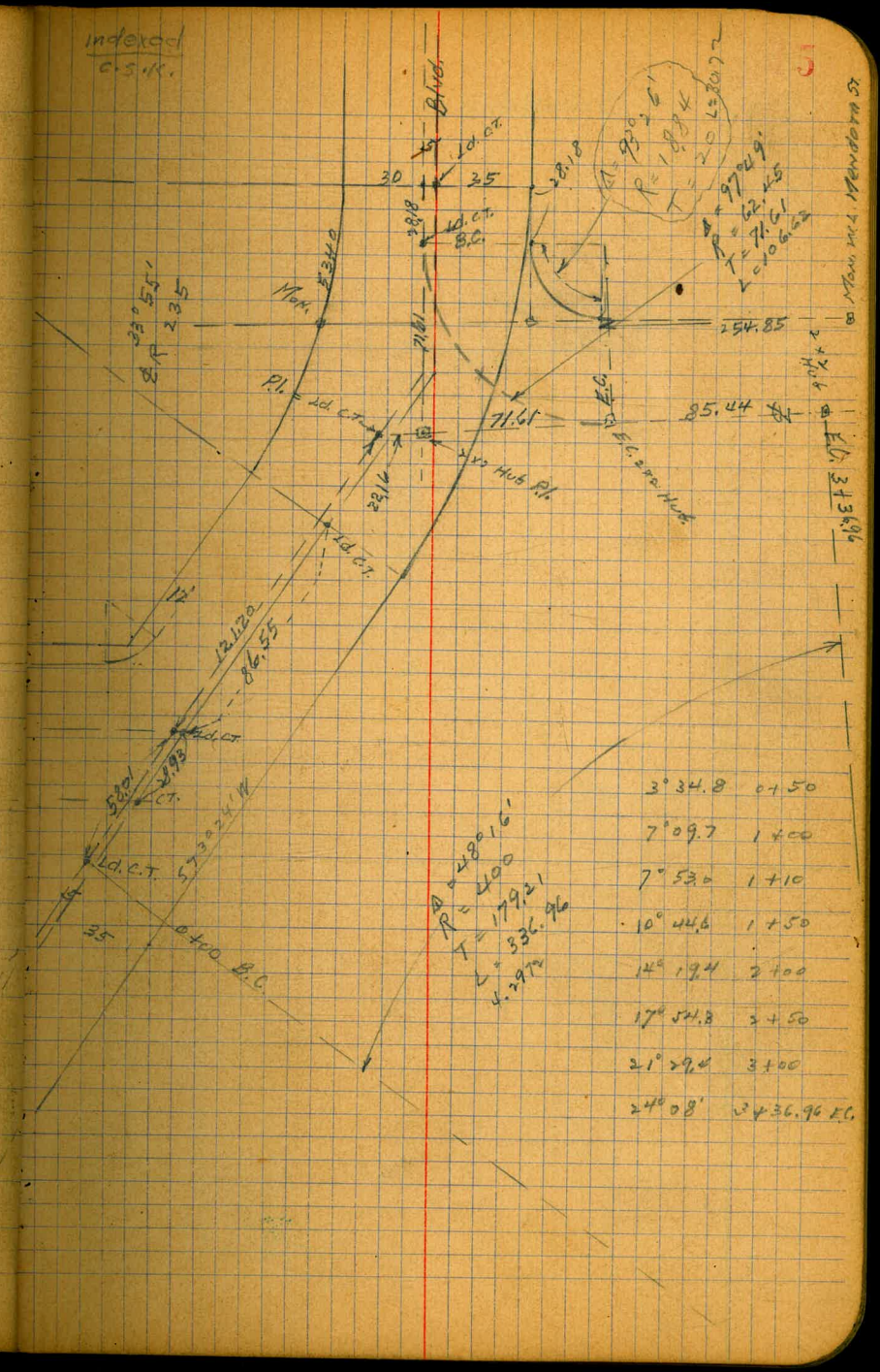
Chatsworth to Plum

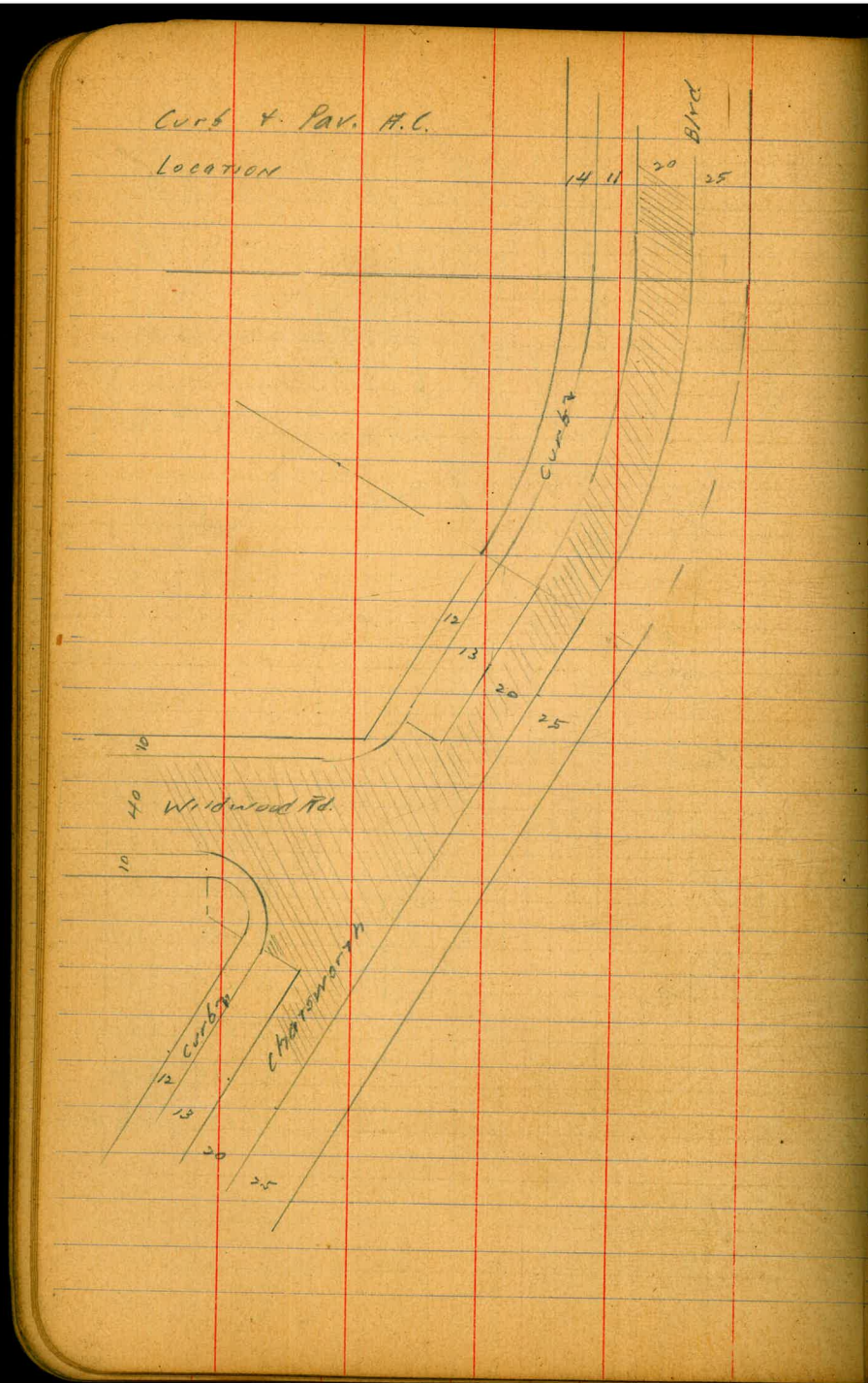
Via S.L. Pueblo Lot 200

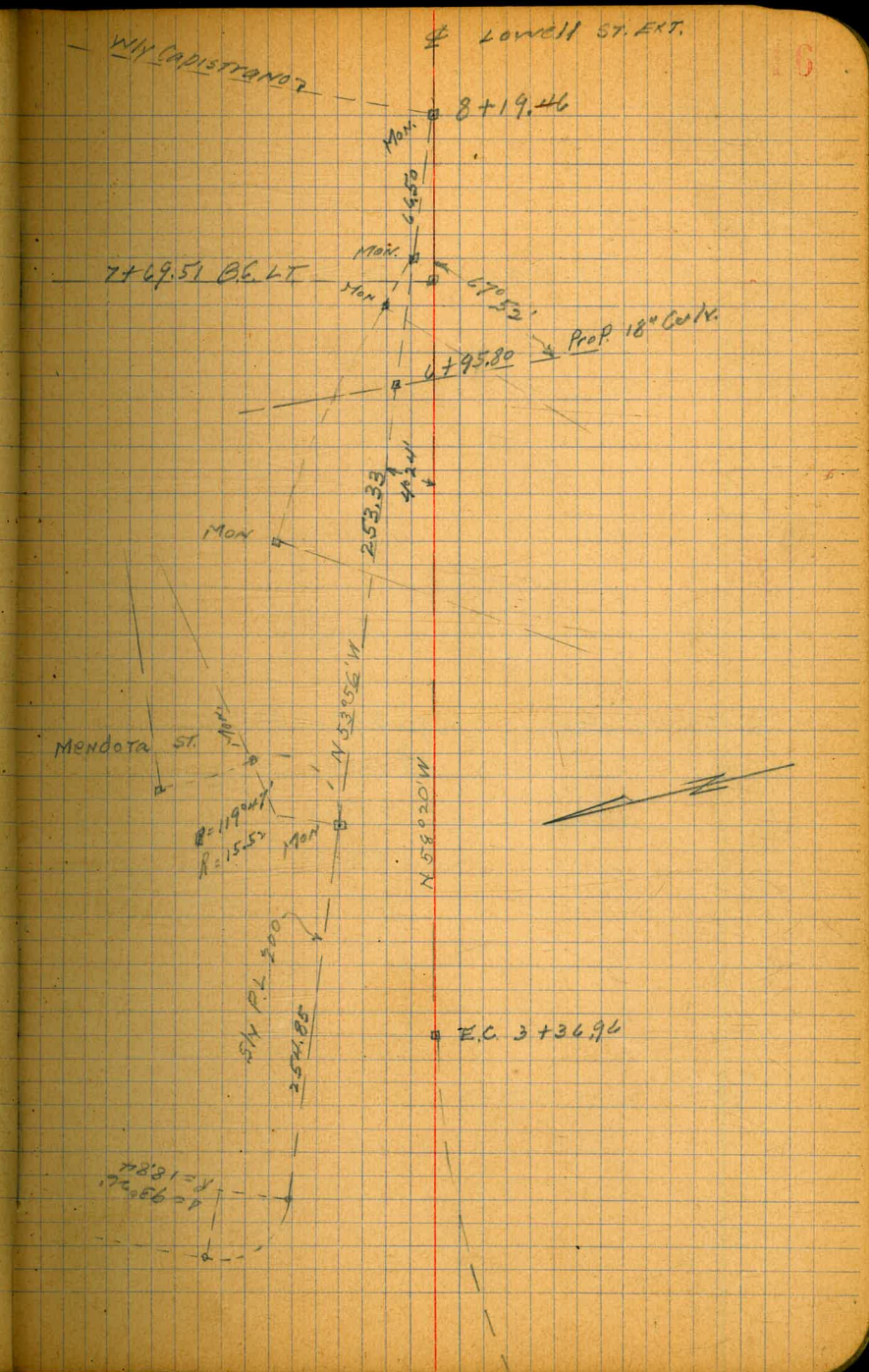
See Tie Pt. Bk. 26 P 44



Indexed
C.S.K.




Curb & Pav. A.C.
Location
Blvd
14
11
20
25
Curb
12
13
20
25
10
40
Wildwood Rd.
10
Curb
Chatsworth
12
13
20
25

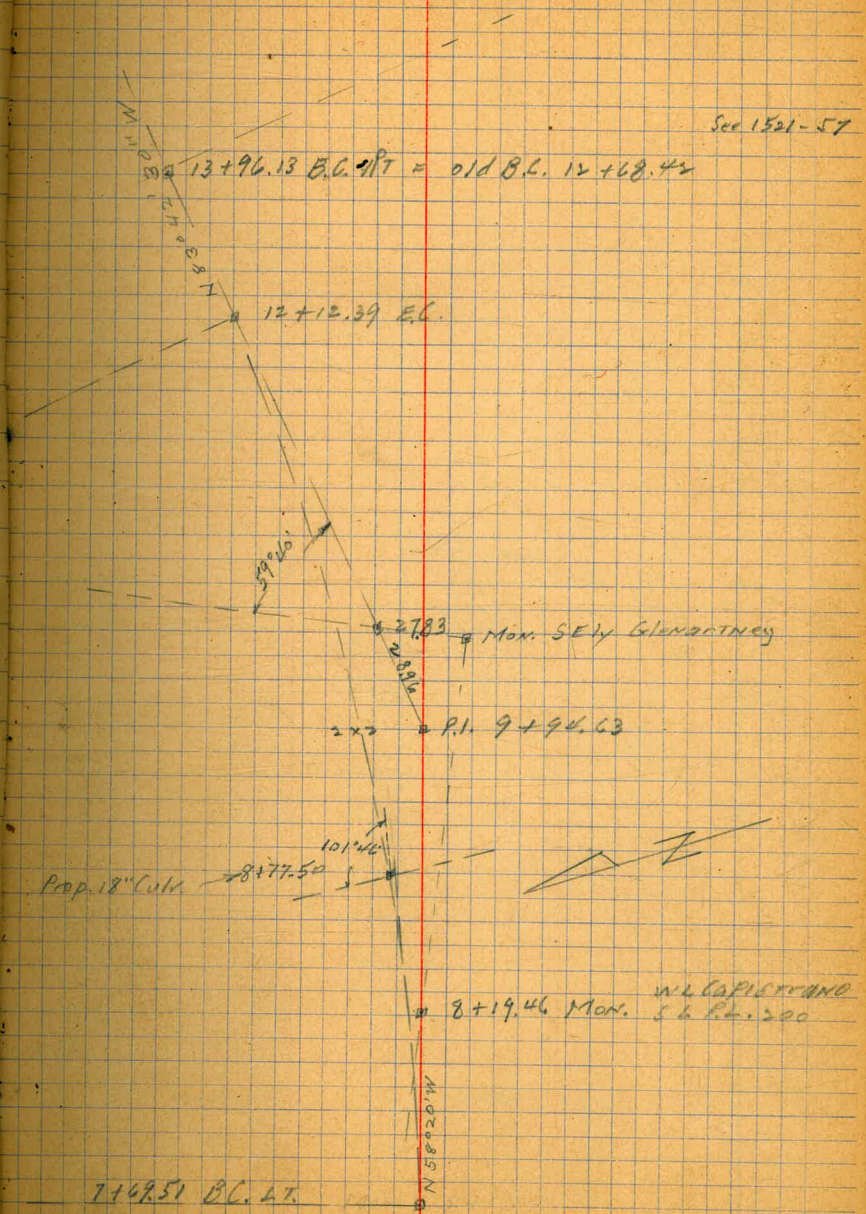

℄ Lowell St. Ext.
Wly Capistrano
8+19.46
Mon.
66.50
Mon.
7+69.51 B.C. LT.
Mon
67°52'
Prop. 18" Culv.
6+95.80
253.33
40°24'
Mon
N 53°56' W
Mendota St.
Mon
R=119°47'
R=15.52
Mon
N 58°20' W
Sly P.L. 200
254.85
E.C. 3+36.96
R=18.84
R=93°26'

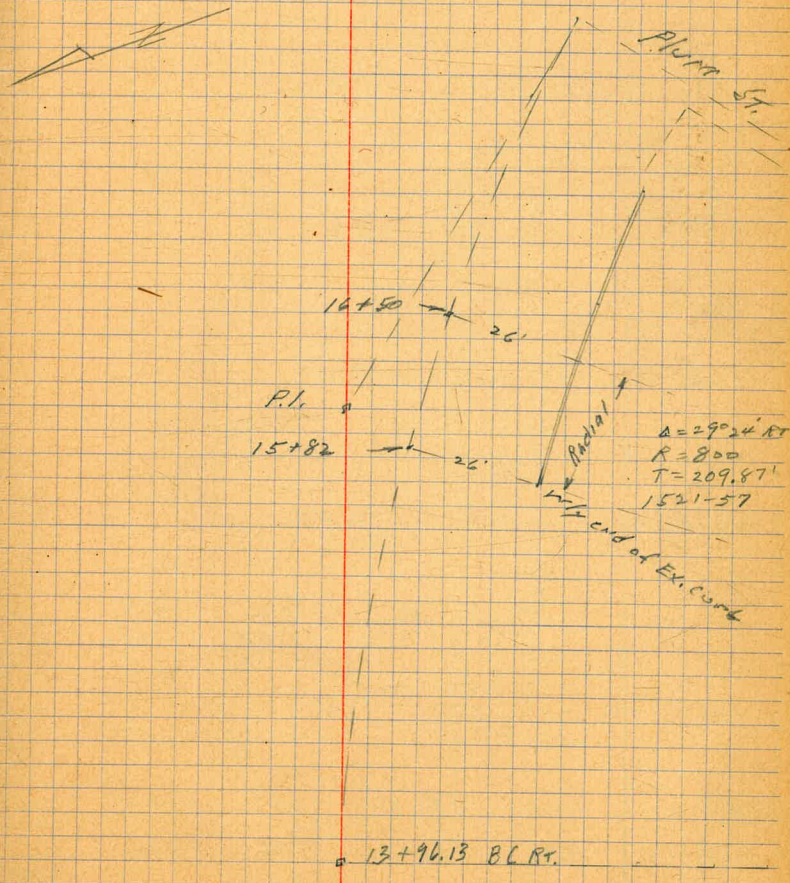
$\Delta = 25°22'30''$ LT

$R = 1000$

$T = 225.12$

$L = 442.88$




Plum St.
16+50
26'
P.I.
15+82
26'
Radial
End of Ext. Curve
Δ = 29°24' RT
R = 800
T = 209.87'
1521+57
13+96.13 BC Rt.

Levels on Lowell St. Ext.

Beg. at Chatsworth & Wildwood Rd.

1+50		10°44.6			
1+10	E. edge Pav.	7°53.0			
1+00		7°09.7			
0+50		3°34.8 Rt			
0+00 B.C. Rt. 5' W of ℄ Chatsworth					
0+00 — 42					
T.P.	1.55	174.83	12.69	173.28	
T.P.	0.91	185.97	12.98	185.06	
N.W.B.P.	0.37	198.04		197.67	Dixon Pl. Chatsworth

LT ℄ RT

167.49 7.34/37 W Pav.

168.03 6.80/13.5 E. Pav.

168.3 6.5

167.8 7.0/20

161.8 13.0/23

161.8 13.0/26

167.0 7.8/33

166.3 8.5/40

168.82 6.01

169.09 5.74/32 Cb

168.1 6.7/32 Gut

168.99 5.84/18 E.P.

169.24 5.59

169.20 5.63/2.6

169.4 5.4/10

170.0 4.8/13

170.0 4.8/29

171.6 3.2/31

172.0 2.8/40

170.31 4.57/23 Val. Gut

170.79 4.04

170.71 4.12/12 edge P.

170.5 4.3/20

171.1 3.7/22

171.0 3.8/38

174.1 0.7/40

171.98 2.85/25 Valley Gut

172.38 2.45 Ld C.T

172.31 2.52/15

171.8 3.0/24

172.5 2.3/40 = E.L.

173.78 1.05/18 Cb

173.02 1.81/18 Gut. Pav.

173.79 1.04/5 edge Pav to S

173.98 0.85

173.89 0.94/15 edge Pav.

174.83

0+53.30 #4

0+31.6 E edge Pav

0+26.65 4 equal Parts #1

0+00 B.C. LT ℄ 5' W of ℄ Chatsworth

B.C. -28.18 = P.C. W ℄ Chatsworth

B.C. -50

LT. Curve off Chatsworth R 62.45

2+00 14° 19.4

1+75

174.83

LT 163.8 11.0/50 163.2 11.6/40 166.0 8.8/25 ℄ 165.8 9.0 167.4 7.4/30 167.3 7.5/40 RT

166.32 8.51

165.2 9.6/40 165.4 9.4/13 166.12 8.71/4 E Pav 166.18 8.65 166.03 8.80/27 W Pav

165.7 9.1/40 164.9 9.9/35 164.4 10.4/25 165.39 9.44/13 edge P 165.09 9.74 164.73 10.10/10.4 E. Pav 164.33 10.50/9 UT 165.30 9.53/20 7 CG

E edge P 164.29 10.54/15 163.89 10.94 163.68 11.15/6.5 W edge Pav 163.27 11.56/9 UT 164.23 10.60/14 CG

163.24 11.59/15 163.05 11.78 162.86 11.97/5 W Pav

167.1 7.7/40 166.1 8.7/15 160.1 14.7 160.1 14.7/2 155.6 19.2/6 155.7 19.1/9 159.4 15.4/13 160.2 14.6/20 160.3 14.5/40 160.6 14.2/50

E. Pav. 167.53 7.30/28 167.9 6.9/20 167.1 7.7 163.6 11.2/10 162.9 11.9/16 158.1 16.7/20 158.1 16.7/25 163.9 10.9/30 164.1 10.7/40 164.2 10.6/50

174.83

T.P.	2.83	152.59	12.62	149.76
3+36.96 E.C.		24°08'		
3+00		21°29.4		
T.P.	0.66	162.38	13.11	161.72
2+50	Resume Rt Curve		17°54.3 Rt	
1+06.62 E.C.	#4			
0+79.95	#3			
		174.83		

LT ℄ RT

156.3 / 6.1 / 45 — 149.7 / 12.7 / 25 — 143.8 / 18.6 / 10 — 143.8 / 18.6 / 7 — 145.0 / 17.4 / 6 — 146.3 / 16.1 — 154.1 / 8.3 / 25 — 160.9 / 1.5 / 45

160.6 / 1.8 / 45 — 154.2 / 8.2 / 20 — 149.6 / 12.8 / 6 — 145.4 / 17.0 / 2 — 145.4 / 17.0 — 145.2 / 14.2 / 5 — 145.2 / 14.2 / 11 — 157.7 / 4.7 / 40

162.38

153.9 / 20.9 — 153.4 / 21.4 / 15 — 150.6 / 24.2 / 16 — 150.6 / 24.2 / 18 — 153.4 / 21.4 / 23 — 158.1 / 16.7 / 40 — 160.6 / 14.2 / 50

same

163.7 / 11.1 / 45 — 158.2 / 16.6 / 20 — 154.1 / 20.7

164.7 / 10.1 / 50 — 162.0 / 12.8 / 40 — 160.9 / 13.9 / 20 — 158.5 / 16.3 — 158.9 / 15.9 / 30

174.83

6+50				
T.P.	0.45	127.41	12.45	127.16
6+00				
5+50				
T.P.	0.08	139.81	12.86	139.73
5+00				
+50				
4+00				
		152.59		

LT ℄ RT

121.2 / 6.4 / 60 — 121.6 / 6.0 / 30 — 123.3 / 4.3 — 123.5 / 4.1 / 25 — 124.2 / 3.4 / 55

127.41 / 5

126.6 / 13.7 / 60 — 128.0 / 11.8 / 30 — 128.6 / 11.2 — 131.2 / 8.4 / 20 — 133.4 / 6.4 / 45

131.3 / 8.5 / 60 — 132.7 / 7.1 / 30 — 135.4 / 4.4 — 138.1 / 1.7 / 20 — 139.2 / 0.6 / 40

139.81 / 9

132.1 / 20.5 / 60 — 130.1 / 22.5 / 57 — 130.1 / 22.5 / 52 — 132.2 / 20.4 / 32 — 136.6 / 16.0 / 30 — 141.1 / 11.5 — 145.0 / 7.6 / 20 — 146.2 / 6.4 / 45

136.6 / 16.0 / 55 — 136.5 / 16.1 / 44 — 133.4 / 19.2 / 42 — 133.4 / 19.2 / 36 — 136.4 / 16.2 / 35 — 137.6 / 15.0 / 25 — 143.1 / 9.5 — 147.7 / 4.9 / 20 — 153.4 / +0.8 / 40

142.9 / 9.7 / 50 — 140.4 / 12.2 / 25 — 141.5 / 11.1 / 13 — 145.5 / 7.1 — 152.3 / 0.3 / 18 — 158.6 / +6.0 / 40

152.59 / 5

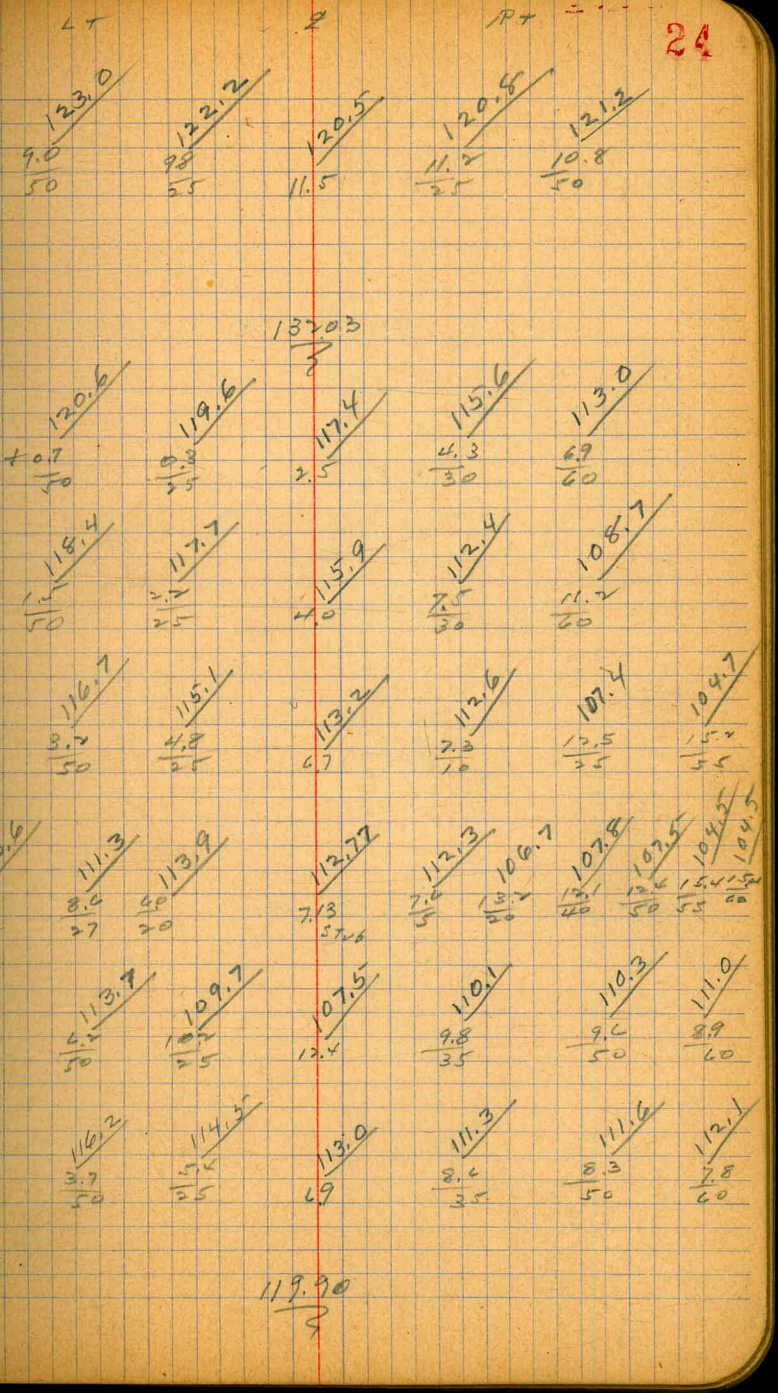
T.P.	473	119.90	12.44	115.17
8+50		2°18.3		
8+00		0°52.4		
7+69.51	B.C. Lt.			
7+50				
7+25				
6+95.8	Prop. Culv.	see ▲		
6+75				
		127.61		

LT		℄	RT		
118.1 / 9.5 / 50	116.3 / 11.3 / 25	114.6 / 13.0	112.4 / 15.2 / 35	112.4 / 15.2 / 55	
119.4 / 8.2 / 50	119.1 / 8.5 / 30	118.3 / 9.3	117.2 / 10.4 / 30	115.2 / 12.4 / 60	
120.5 / 7.1 / 50	119.9 / 7.7 / 25	119.40 / 8.21	117.4 / 10.2 / 25	110.6 / 17.0 / 60	
121.0 / 6.6 / 50	120.4 / 7.2 / 25	119.9 / 7.7	117.2 / 10.4 / 25	112.0 / 15.6 / 50	111.2 / 16.4 / 60
122.2 / 5.4 / 55	120.8 / 6.8 / 30	120.0 / 7.6	118.3 / 9.3 / 20	113.6 / 14.0 / 46	111.0 / 16.6 / 50
109.0 / 18.6 / 55	113.2 / 14.4 / 60				
118.0 / 9.6 / 65	117.8 / 9.8 / 50	116.2 / 11.4 / 25	115.84 / 11.77 Stub	114.8 / 12.8 / 35	109.9 / 17.7 / 50
113.6 / 14.0 / 65					
120.2 / 7.4 / 60	117.4 / 10.2 / 41	118.0 / 9.6 / 30	118.0 / 9.6	118.4 / 9.2 / 30	118.2 / 9.4 / 60

127.61

10+00		6°36.2			
T.P. Pl. Hub	13.01	132.03	0.88	119.02	2x2 Hub
9+50		5°10.2			
9+00		3°44.3			
8+80					
8+77.5	Culv Prop 18"		Sec A	3°05.6	
8+71					
8+63					
		119.90			

L+		℄	R+	
123.0 / 9.0 / 50	122.2 / 9.8 / 25	120.5 / 11.5	120.8 / 11.2 / 25	121.2 / 10.8 / 50
		132.03 / 8		
120.6 / +0.7 / 50	119.6 / 0.3 / 25	117.4 / 2.5	115.6 / 4.3 / 30	113.0 / 6.9 / 60
118.4 / 1.5 / 50	117.7 / 2.2 / 25	115.9 / 4.0	112.4 / 7.5 / 30	108.7 / 11.2 / 60
116.7 / 3.2 / 50	115.1 / 4.8 / 25	113.2 / 6.7	112.6 / 7.3 / 10	107.4 / 12.5 / 25	104.7 / 15.2 / 55
113.6 / 6.3 / 52	111.3 / 8.6 / 27	113.9 / 6.0 / 20	112.77 / 7.13 Stub	112.3 / 7.6 / 5	106.7 / 13.2 / 20	107.8 / 12.1 / 40	107.5 / 12.4 / 50	104.5 / 15.4 / 55	104.5 / 15.4 / 60
113.7 / 6.2 / 50	109.7 / 10.2 / 25	107.5 / 12.4	110.1 / 9.8 / 35	110.3 / 9.6 / 50	111.0 / 8.9 / 60
116.2 / 3.7 / 50	114.5 / 5.4 / 25	113.0 / 6.9	111.3 / 8.6 / 35	111.6 / 8.3 / 50	112.1 / 7.8 / 60
		119.90 / 8		



12+12.39	E.G	12° 41.25			
T.P.	4.29	146.77	0.12	142.48	
12		12° 19.9			
+50		10° 54.0			
11		9° 28.0			
T.P. old tie Hub	11.62	142.60	1.05	130.98	50' LT 10+60
10+50		8° 02.1			
10+30					
		132.03			

LT ℄ RT

143.5 / 3.3 / 40 — 143.2 / 3.6 / 20 — 142.65 / 4.12 Hub — 142.4 / 4.4 / 20 — 142.7 / 4.1 / 40

146.77 ℄

142.9 / +0.3 / 40 — 143.1 / +0.5 / 20 — 142.1 / 0.5 — 141.7 / 0.9 / 20 — 142.2 / 0.4 / 40

140.1 / 2.5 / 40 — 139.7 / 2.9 / 20 — 138.6 / 40 — 138.4 / 4.2 / 10 — 140.0 / 2.4 / 25 — 139.9 / 2.7 / 40

137.7 / 4.9 / 50 — 136.2 / 6.4 / 25 — 135.2 / 7.4 — 134.7 / 7.9 / 15 — 136.3 / 6.3 / 50

142.60 ℄

128.0 / 4.0 / 50 — 127.9 / 4.1 / 25 — 131.0 / 1.0 / 15 — 132.0 / 0.0 — 133.4 / +1.4 / 25 — 134.5 / +2.5 / 50

126.4 / 5.6 / 50 — 125.0 / 7.0 / 25 — 124.7 / 7.3 — 132.0 / 0.0 / 25 — 132.0 / 0.0 / 50

132.03 ℄

T.P.	0.51	143.47	12.51	123.16
15		3°43.4		
14+50		1°55.7		
13+96.13	BC. RT			
T.P.	0.99	135.67	12.09	134.68
+50				
13				
12+50				
		146.77		

LT ℄ RT

125.7 / 10.0 / 40
125.1 / 10.6 / 20
124.5 / 11.2
124.4 / 11.3 / 20
123.6 / 12.1 / 40

130.0 / 5.7 / 40
129.5 / 6.2 / 20
127.4 / 8.3
126.9 / 8.8 / 20
126.4 / 9.3 / 40

135.6 / 0.1 / 40
134.6 / 1.1 / 20
132.24 / 3.43 / 11.6
130.8 / 4.9 / 20
130.4 / 4.9 / 40

138.0 / 8.8 / 40
136.9 / 9.9 / 20
135.57
135.3 / 11.5
135.3 / 11.5 / 20
134.6 / 12.0 / 40

143.0 / 3.8 / 40
141.7 / 5.1 / 20
143.4 / 4.4
142.4 / 4.4 / 20
143.2 / 3.6 / 40

144.5 / 2.3 / 40
145.0 / 1.8 / 20
144.4 / 2.4
143.8 / 3.0 / 20
144.3 / 2.5 / 40

146.77

See F.B. 1521-64-65 for Curb El.
on Ranchitas Imprmts

16+50		9°06.5			
T.P.	0.06	111.04	12.69	110.98	
16		7°19.0			
+82		6°37.			
15+68					
check to cb. See 1521-65			4.51	119.16	119.13 / 0.03
15+50		5°31.6			
		123.67			

LT ℄ Rt

105.63 / 5.41 / 26 cb
105.04 / 6.00 / 26 gut Pav.
105.24 / 5.80 Pav
103.74 / 7.30 / 26 gut Pav
104.43 / 6.61 / 26 cb

111.04 ℄

112.74 / 10.93 / 40 cb
112.26 / 11.41 / 39 gut
111.77 / 11.90 / 22 Pav
111.47 / 12.20 Pav
110.7 / 13.0 / gut Pav
111.39 / 12.28 / 26 cb
111.0 / 12.7 / 35
112.9 / 10.8 / 40

114.07 / 9.60 / 40 Pav
113.7 / 10.0 / 20 Pav
113.17 / 10.50 Pav
112.7 / 11.0 / 21
113.10 / 10.57 / 26 gut
113.97 / 9.70 / 26 cb
113.7 / 10.0 / 35
115.6 / 8.7 / 40

Inlyend Curb

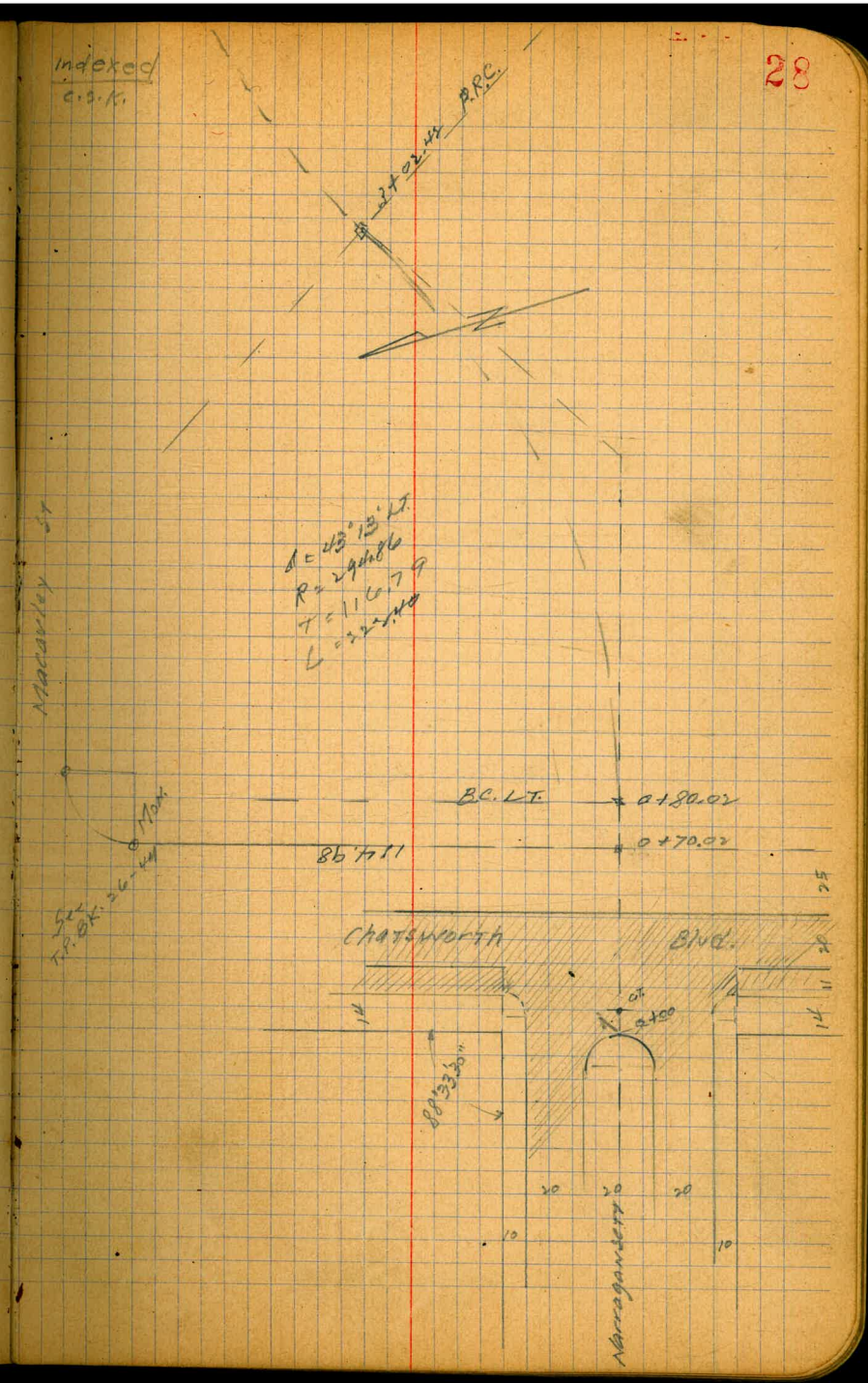
115.04 / 8.63 / 40 Pav
115.06 / 8.61 / 33 Pav
114.9 / 8.8 / 20
114.3 / 9.4 Pav
114.3 / 9.4 / 8
116.5 / 7.2 / 18
117.1 / 6.6 / 40

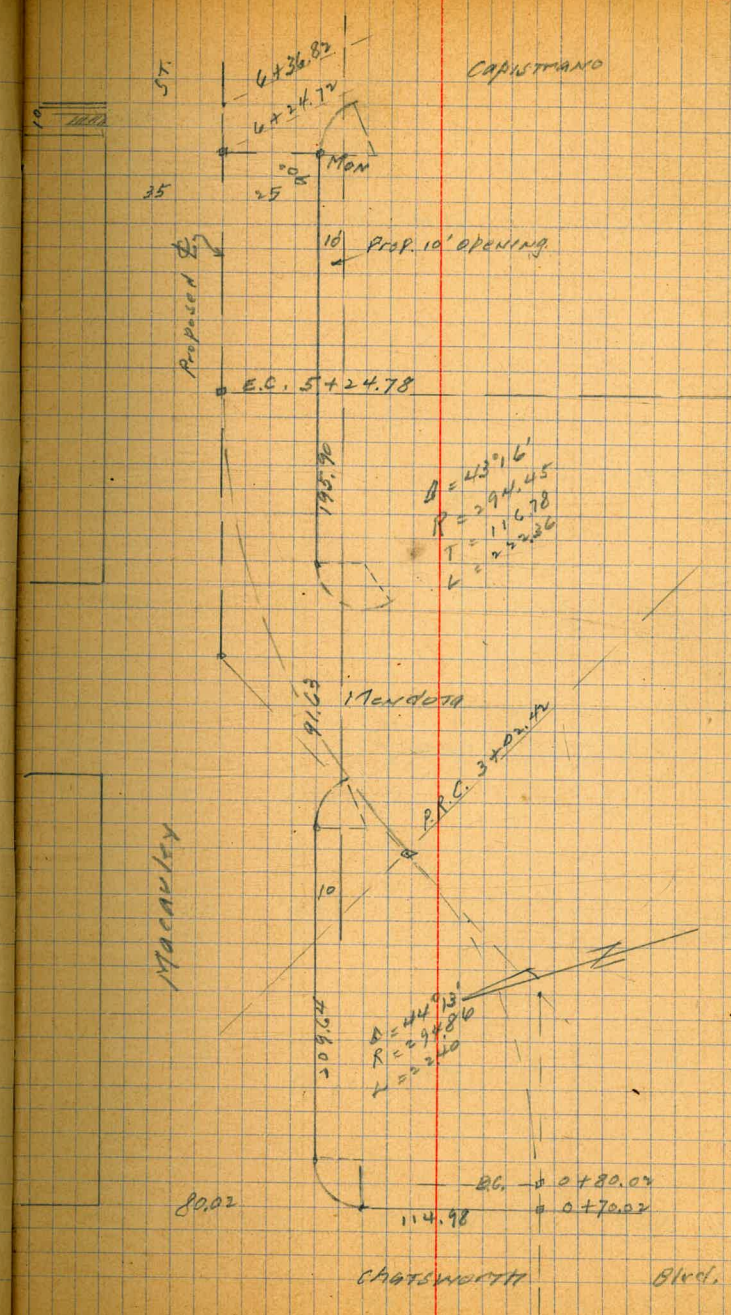
117.22 / 6.45 / 40 Pav
116.8 / 6.9 / 30
119.5 / 4.2 / 13
119.8 / 3.9
119.9 / 3.8 / 20
119.1 / 4.6 / 40

123.67 ℄

Proposed opening of Narragansett
Thru N. Cor. of Glenarthney
to Macauley St. 70' wide

Indexed
C.S.K.





Capistrano
St.
6+36.82
6+24.72
Mon
35
25
10
Prop. 10' opening
Proposed ℄
E.C. 5+24.78
195.90
Δ = 43°16'
R = 294.45
T = 116.78
L = 222.36
Mendota
91.63
P.R.C. 3+02.42
Macauley
10
209.64
Δ = 44°13'
R = 294.86
L = 224.0
80.02
114.98
B.C. 0+80.02
0+70.02
Chatsworth
Blvd.

4+18.60

Curve 4 equal Parts

3+58.01

3+02.42 PRC

2+46.82

Curve 4 equal Parts

1+91.42

1+35.62

0+80.02

NEBP	5.51	138.70	133.19

See 1521-58 for INT. Sec. Levels

24 2 R4

14.6/35	14.5/35	13.4/15	11.8	12.7/15	12.7/35
12.9/35	11.9/15		11.1	10.9/15	10.4/35
12.0/35	11.9/15		11.78 HW6	11.4/15	11.1/35
12.4/35	12.4/15		12.1	12.1/15	11.8/35
11.7/35	12.1/15		11.7	11.4/15	10.3/35
10.8/35	8.9/15		4.5	5.7/15	5.5/35
4.8/35	5.4/15		4.93 HW6	3.4/15	2.8/35

138.70/2

					LT			℄			RT
6+76.82	E ob Cap.	+ NL Macauley					4.36/35 Top ob				
6+36.82	W ob Capistrano	"					6.36/35 Top ob				
6+24.72	opposite Mon.	SL Macauley WL Capistrano			6.1/35	5.8/23	6.2/20	6.2	6.1/3	5.2/15	4.4/35
5+75					7.87/33	7.8/24	8.4/20	8.4	7.7/10	8.5/17	8.4/35
5+24.78	E.C.				9.9/35	9.6/24	9.8/19	9.98 Hub	9.5/15	9.1/35	
4+69.19					10.7/35	10.7/30	11.2/25	11.2/5	10.8	10.2/15	9.7/35
T.P.	10.34	136.30	12.74	125.96							
		138.70									

5' ice M. wall

136.30/2

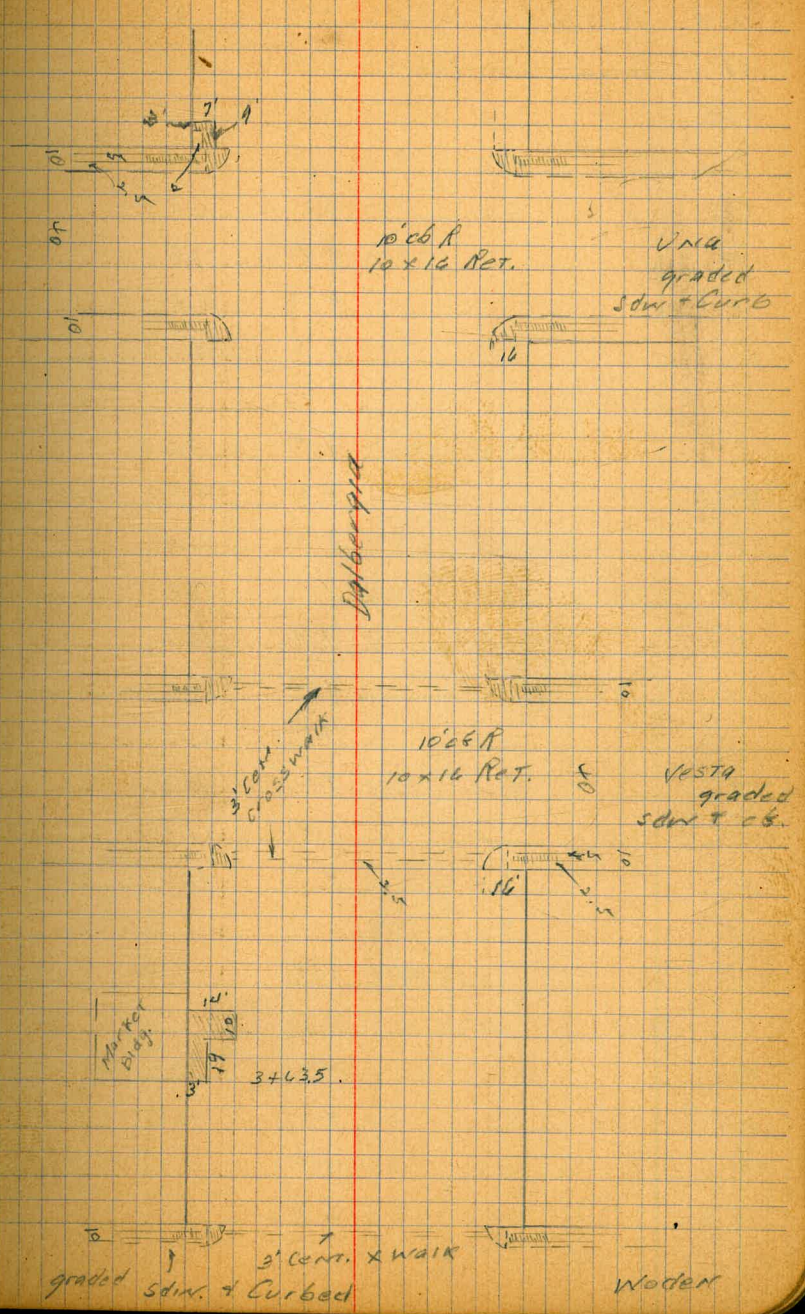
Indexed
C.S.K.

100' wide
16' obs
17' 1/4

Xsec Dalbergia St.
Woden to Thor

Wly. B.P.	2.06	22.71		20.65	Cottonwood Woden
	0+00 Wly Woden				
N			8.8	13.9	
cb cem			9.16	13.55	
qvt			10.2	12.5	
1/4			9.4	13.3	
c			9.4	13.3	
1/4			9.6	13.1	
qvt			10.1	12.6	
cb cem			9.63	13.08	
S			9.5	13.2	
	0+12				
S			7.2	15.5	
+13			7.1	15.6	
cb			9.8	12.9	
1/4			9.3	13.4	
c			9.1	13.6	
1/4			9.4	13.3	
cb			9.6	13.1	
+6			8.0	14.7	
N			7.1	15.6	
	0+50				
N			6.2	16.8	

Moore
3-5-39



22.71

+10			6.6	16.1
CO			9.0	13.7
1/4			8.1	14.6
C			7.9	14.8
1/4			8.1	14.6
C6			8.9	13.8
+3			6.4	16.3
S			6.8	15.9
1+00				
S			6.5	16.2
+13			6.0	16.7
C6			8.7	14.5
1/4			7.7	15.5
C			7.0	15.7
1/4			7.0	15.7
+13			7.7	15.5
C6			9.1	13.6
+5			5.6	17.1
N			4.9	17.8
T.P.	4.17	21.19	5.69	17.02
1+50				
N			4.2	17.0
+14			4.4	16.8
C6			6.7	14.5
+3			5.6	15.6

21.49

1/4		5.4	16.0
C		5.2	16.0
1/4		5.6	15.8
C6		6.7	15.0
+3		4.6	16.6
S		4.7	17.0
1+66			
N+1 3' Conc wall		3.26	17.99
1+87			
S-1 4' Brick +		4.33	16.86
2+00			
S		4.7	16.5
+13		5.0	16.2
C6		6.5	14.7
+2		5.4	15.8
1/4		5.1	16.1
C		4.9	16.3
1/4		5.1	16.1
+14		5.5	15.7
C6		6.4	14.8
+5		4.4	16.6
N		4.7	17.0
2+50			
N		4.1	17.1
+13		4.8	16.4
C6		6.5	14.7
+3		5.3	15.9

21.19

1/4		5.0	16.2
C		4.8	16.4
1/4		5.0	16.2
+14		5.5	15.7
CB		6.6	14.6
+3		4.6	16.6
S		5.3	15.9
	3+00		
S		5.2	16.0
+13		4.8	16.4
CB		6.6	14.6
+3		5.6	15.6
1/4		5.0	16.2
C		4.7	16.5
1/4		4.8	16.4
+14		5.4	15.8
CB		6.4	14.8
+5		4.2	17.0
N		4.5	16.7
	3+50		
N		4.8	16.4
+13		4.3	16.9
CB		6.4	14.6
+3		5.5	15.7
1/4		5.1	16.1
C		4.7	16.5

21.19

1/4		5.2	16.0
+15		5.6	15.6
CB		6.5	14.7
+3		5.2	16.0
S		5.4	15.6
	34635		
S	Floor El. Cent.	4.85	16.34
+3	Cent.	5.10	16.09
	3+835		
S	Floor "	5.09	16.12
+3	Cent	5.12	16.09
114	"	5.27	15.92
	2+92		
S	Fl. Cent.	5.04	16.15
+14	Cent.	5.14	16.03
	4+00		
S		5.5	15.7
+14		5.3	15.9
CB		6.4	14.8
+3		5.7	15.5
1/4		5.3	15.9
C		4.6	16.6
1/4		5.1	16.1
+14		5.4	15.8
CB		6.4	14.8
+5		4.5	16.7
N		5.0	16.2

4+50

N	4.6	16.6
+13	4.8	16.4
C6	6.4	14.8
+3	5.5	15.7
1/4	5.3	15.9
C	5.0	16.2
1/4	5.5	15.7
+15	5.7	15.5
C6	6.0	14.6
+3	4.8	16.4
S	5.7	15.5

5+00

S	5.8	15.4
+14	5.5	15.7
C6	6.6	14.6
+3	5.8	15.4
1/4	5.5	15.7
C	5.1	16.1
1/4	5.4	15.8
+15	5.7	15.5
C6	6.7	14.5
+2	5.4	15.8
N	4.9	16.3

5+32

N 4' CEM. WK.	4.96	16.23

5+50

N	5.3	15.9
+12	5.3	15.9
C6	6.4	14.8
+4	5.7	15.5
1/4	5.3	15.8
C	4.8	16.4
1/4	5.6	15.6
+14	5.8	15.4
C6	6.5	14.7
+7	5.1	16.1
S	5.9	15.3

5+77

N +2.5 3' CEM. WK.	5.12	16.07

6+00 ELY VESTA

S	5.4	15.8
C6 CEM	5.63	15.56
QUT	4.7	15.0
1/4	5.1	16.1
C	4.3	16.9
1/4	5.0	16.2
QUT	6.2	15.0
C6 CEM.	5.68	15.51
S	5.2	16.0

Note! Cross walks laid to grade of old R.R.

E/y Vesta +4 = E 3' Cent. X walk

N gut		6.24	14.95
1/4		5.03	16.16
C		4.22	16.97
1/4		5.02	16.17
S gut		6.05	15.14

Rails pulled now

E Vesta

S		5.6	15.6
CB		5.7	15.5
1/4		4.9	16.3
C		4.6	16.6
1/4		4.8	16.4
CB		5.1	16.1
N		5.3	15.9
T.P.	7.20	23.27	5.12	16.07

E Vesta +36 = E 3' Cent. X walk

N gut		7.74	15.53
1/4		6.84	16.43
C		6.05	17.22
1/4		6.70	16.57
S gut		7.66	15.61

W/y Vesta = 0+00

S		6.9	16.4
CB	Cent.	7.18	16.09
gut		7.6	15.7
1/4		6.7	16.6
C		6.2	17.1
1/4		6.8	16.5
gut		7.7	15.6
CB	Cent.	7.18	16.09
N		7.0	16.3

0+50

N		7.0	16.3
CB		6.8	16.5
1/4		7.0	16.3
C		6.4	16.9
1/4		6.6	16.7
CB		7.1	16.2
+3		6.1	17.2
S		6.0	17.3

1+00

S		5.1	18.2
+3		5.5	17.8
CB		6.5	16.8
1/4		4.3	17.0
C		6.1	17.2
1/4		6.5	16.8

c6	6.6	16.7	
+13	6.5	16.8	
N	7.2	16.1	
+5	8.2	15.1	
1+50			
-5	7.2	16.1	
N	6.4	16.9	
+2	5.7	17.6	
c6	5.8	17.5	
1/4	5.9	17.4	
C	5.4	17.9	
1/4	5.7	17.6	
c6	6.2	17.1	
+4	5.0	18.3	
S	5.0	18.3	
2+00			
S	4.9	18.4	
c6	5.6	17.9	
1/4	5.2	18.1	
C	5.0	18.3	
1/4	5.3	18.0	
c6	5.5	17.8	
+2	5.1	18.2	
N	5.2	18.1	
+5	6.4	16.9	

2+50		
N	5.0	18.3
+3	4.6	18.9
+14	4.6	18.7
c6	5.0	18.3
1/4	4.7	18.6
C	4.5	18.8
1/4	5.1	18.2
c6	5.3	18.0
S	5.0	18.3
2+66.5 E 6.6 Cen. Drive		
S	4.78	18.49
S +14 edge drive	5.06	18.21
c6	5.2	18.1
3+00		
S	4.6	18.7
c6	5.0	18.3
1/4	4.7	18.6
C	4.1	19.2
1/4	4.1	19.2
c6	4.4	18.9
+2	3.9	19.4
N	3.8	19.5
3+50		
N	3.2	20.1
+14	3.1	20.2
c6	4.0	19.3

		x3.27		
1/4			4.0	19.3
c			3.6	19.7
1/4			4.2	19.1
c6			4.8	18.5
+N			4.0	19.3
S			4.2	19.1
	4+00			
S			4.0	19.3
c6			4.5	18.8
1/4			4.3	19.0
c			3.6	19.7
1/4			3.7	19.6
c6			3.7	19.6
+3			3.0	20.3
N			3.0	20.3
	4+13.5	E 3' cen wk.		
S			3.92	19.35
+12.6			3.96	19.33
	4+31	E 6' cen drive		
S			4.09	19.18
+13			4.21	19.06
	4+50			
N			3.0	20.3
+13			3.1	20.2
c6			3.7	19.6
1/4			3.5	19.8

		x3.27		
c			3.8	19.5
1/4			4.2	19.1
c6			4.5	18.8
S			4.3	19.0
	4+53	E 3' cen wk		
S			4.14	19.13
+13			4.27	19.00
	5+00			
S			4.5	18.8
c6			4.7	18.6
1/4			4.3	19.0
c			3.6	19.7
1/4			3.5	19.8
c6			3.6	19.7
+4			3.1	20.2
N			3.2	20.1
T.O	5.15	24.80	3.67	19.65
	5+33			
S	E 4' cen wk		5.05	18.15
	5+50			
N			5.1	19.7
c6			5.0	19.8
1/4			5.3	19.5
c			5.3	19.5
1/4			6.0	18.8
c6			6.2	18.6
S			6.0	18.8

2480

6+00 Ely Una St graded

S	6.4	18.4
cb Cem	6.75	18.05
qvt	7.4	17.6
1/4	6.8	18.0
c	6.6	18.2
1/4	6.6	18.2
qvt	6.4	18.4
cb Cem.	5.87	18.98
N	5.4	19.2

W/y Una = 0+00

N	4.9	19.9
cb Cem.	5.30	19.50
qvt	6.0	18.8
1/4	6.1	18.7
c	6.1	18.7
1/4	6.4	18.4
qvt	7.0	17.8
cb Cem.	6.27	18.58
S	6.1	18.7

0+50

S	6.0	18.8
cb	6.1	18.7
1/4	5.7	19.1
c	5.4	19.4
1/4	5.4	19.4

2480

cb	5.2	19.6
qvt	4.4	20.2
N	4.7	20.1

1+00

N	4.3	20.5
cb	4.6	20.2
1/4	4.9	19.9
c	5.0	19.8
1/4	5.5	19.3
cb	5.9	18.9
S	5.5	19.3

1+50

S	4.9	19.9
cb	5.2	19.6
1/4	5.1	19.7
c	4.8	20.0
1/4	4.2	20.6
cb	4.0	20.8
N	3.3	21.5

1+57.5

S E 3' Cem. wk	4.50	20.30

2+00

N	2.7	22.1
cb	3.7	21.1
1/4	3.7	21.1
c	4.9	19.9
1/4	4.8	20.0

24.80

c6		4.7	20.1
+3		4.1	20.7
S		4.4	20.4
2+34 E 3' Cent wk			
N		2.31	22.49
2+50			
S		5.3	19.5
c6		5.3	19.5
1/4		5.0	19.8
C		5.2	19.6
1/4		3.9	20.9
c6		3.6	21.2
N		2.4	22.2
3+00			
N		4.2	20.6
+14		4.5	20.3
c6		5.1	19.7
1/4		5.1	19.7
C		6.0	18.8
1/4		6.2	18.6
c6		7.0	17.8
+3		6.4	17.4
S		6.8	17.0
3+19			
S E 3' cem. wk.		7.20	17.60

24.80

3+50		
S	8.7	16.1
+13	8.5	16.3
c6	8.9	15.9
1/4	8.0	16.8
C	7.4	17.4
1/4	7.0	17.8
c6	7.2	17.6
+2	6.3	18.5
N	6.1	18.7
3+77		
S E 3' Cem wk	9.07	15.73
3+94		
N E 2' " "	7.32	17.48
4+00		
N	7.7	17.1
+14	7.9	16.9
c6	8.8	16.0
1/4	8.6	16.2
C	8.4	16.2
1/4	8.7	16.1
c6	10.4	14.4
+3	9.7	15.1
S	10.2	14.6
T.P. 244	16.40	11.06	13.74

1640

4+50

S	2.9	13.5
+14	2.0	14.4
cb	3.0	13.4
1/4	3.4	14.0
C	1.5	14.9
1/4	1.6	14.8
cb	1.9	14.5
+2	1.1	15.3
N	1.4	15.0

5+00

N	2.6	13.8
+14	3.6	13.4
cb	4.1	12.3
1/4	3.5	12.9
C	3.7	13.2
1/4	3.7	12.7
cb	4.4	12.0
+4	3.7	12.7
S	3.4	13.0

5+50

S	5.1	11.3
cb	4.7	11.7
+2	6.0	10.4
1/4	5.3	11.1
C	4.8	11.6

1640

1/4	5.1	11.3
+11	5.9	10.5
cb	5.4	10.8
N	4.8	11.6

6+00 E/W Thor St 60' wide 10' cb Not graded

N-S	8.2	8.2
N	8.2	8.2
+10	7.4	9.0
cb	7.9	8.5
1/4	4.7	9.7
C	4.3	10.1
1/4	4.6	9.8
cb	4.8	9.6
+8	4.0	10.4
S	4.3	10.1

E cb.

S	4.9	9.5
cb	7.1	9.3
1/4	6.8	9.6
C	6.6	9.8
1/4	7.2	9.2
cb	8.0	8.4
+4	7.6	8.8
N	8.3	8.1
+5	8.3	8.1

16.40

E Thor

N	9.0	7.4
cb	8.4	8.0
1/4	7.7	8.7
c	7.5	8.9
1/4	7.5	8.9
cb	7.2	9.2
S	7.3	9.1

W cb

S	7.7	8.7
cb	7.5	8.9
1/4	7.1	9.3
c	6.6	9.8
1/4	8.4	8.6
cb	9.0	7.4
N	9.3	7.1

Willy Thor

N - S	10.1	6.3
N	10.5	5.9
cb	9.6	6.8
1/4	9.0	7.4
+6	9.0	7.4
+11	4.9	9.5
c	6.5	8.9
+8	6.4	10.0
1/4	8.0	8.4

16.40

cb			8.3	8.1
S			7.7	8.7
T.P.	3.45	12.47	7.58	8.82
check to BM 8P SE. curb		Main Thor	5.38	7.09

Indexed
C.S.K.

X sec alley Blk 26 Ocean Beach
20' wide
Moore
8-9-89

N in BP	12.98	38.01		25.03	Sup-set Saratoga
I.P.	12.64	49.97	0.68	37.33	

0-12 Ely c6 of Ebers

N Pav.	4.20	45.77
S "	4.06	45.91

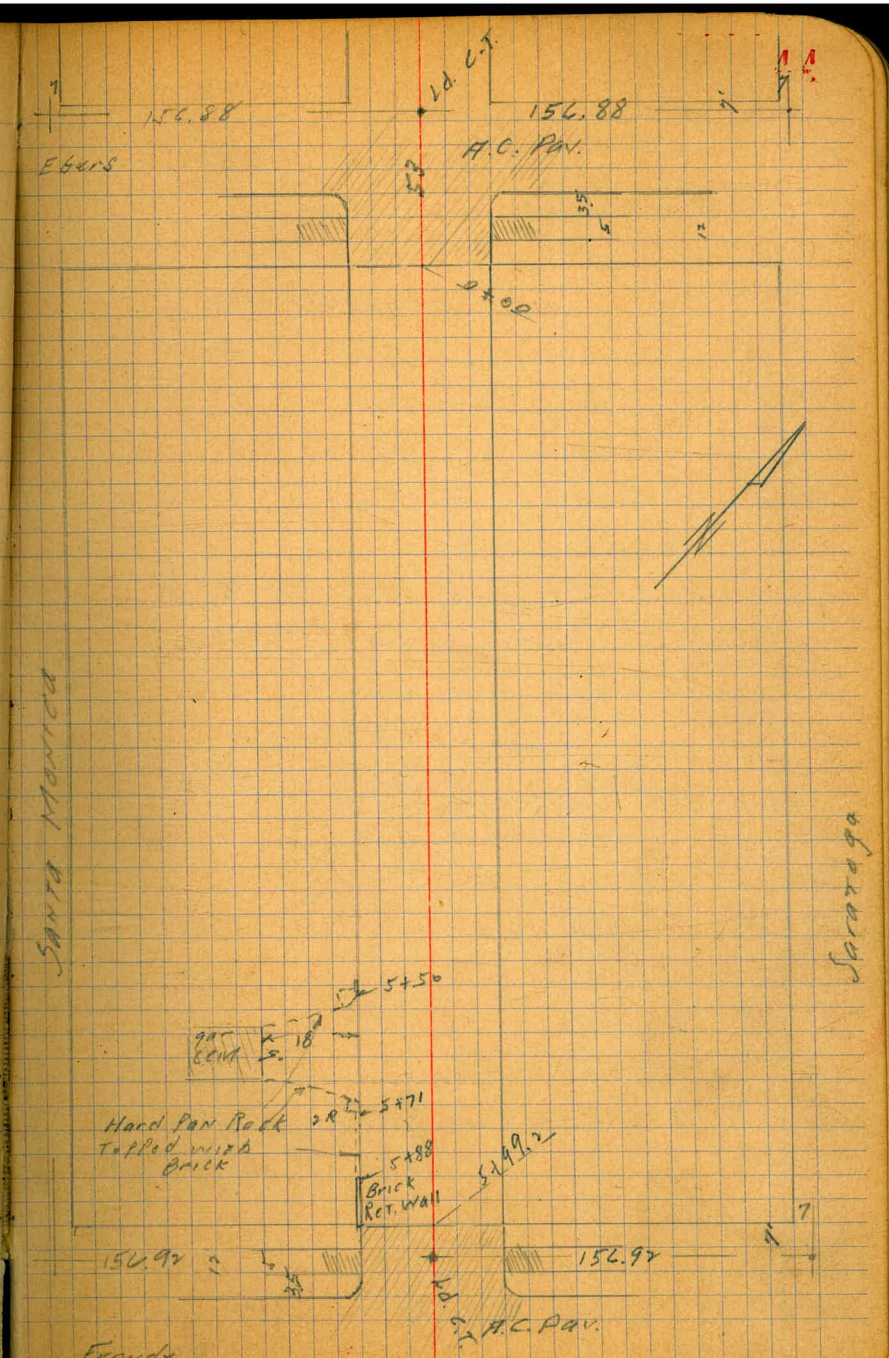
0+00 Ely Ebers

S c6	3.21	46.76
S Pav	3.47	46.50
C "	3.94	46.03
N "	3.55	46.42
N c6	3.45	46.52

0+01.5
N +0.7 12" Tel. Pole
0+03

N	0.4	49.57
+3	3.2	46.77
C	3.3	46.67
+6	3.2	46.77
S	0.0	49.97

I.P.	12.24	41.35	0.86	49.11



61.35

0+20		
S.	10.5	50.9
+0.7 W. end fence		
+2	10.6	50.8
+4	12.5	48.9
C	12.5	48.9
+7	12.2	49.2
+8	10.7	50.7
N	10.7	50.7
0+50		
N	9.5	51.9
+2	10.1	51.3
C	10.3	51.1
+6	10.2	51.2
+7	9.4	51.8
+9.3 fence in alley		
S	9.6	51.8
0+78		
S +0.8 14" Pow. Pole		
0+85		
S +0.4 E end fence		
0+94		
-3 Sin. 8' gar. Cem Cl.	7.70	53.65
S	8.00	53.35
+0.8 edge Cem. Apron	8.05	53.30
C	8.1	53.3
N	8.0	53.4

61.35

0+94			
N	7.9	53.5	
-3.5 Sin gar. dirt	7.8	53.6	
1+57			
N +0.5 Tel Pole 12" Dl.			
1+54			
N	4.7	56.7	
C	5.0	56.4	
+4	5.0	56.4	
S	4.2	57.2	
+8 Sin. 8' gar Cem Cl.	4.03	57.32	
2+00			
S	2.2	59.2	
+0.7 14" Power Pole			
C	2.7	58.7	
+9	2.6	58.8	
N.	2.0	59.4	
T.P. 12.54	73.79	0.10	61.25
2+50			
N fence on in alley	11.6	62.2	
+2	12.6	61.2	
C	12.7	61.1	
S	12.5	61.3	
3+00			
S	9.2	64.6	

Nail in Pole 2+00

C SMH RIM	9.59	64.20
+8	9.5	64.3
+9.1 fence in alley		
N	8.9	64.9
3+05		
N +1.1 12" Tel Pole		1.1 in alley
3+32		
N	7.3	66.5
+0.4 fence		
+2	8.0	65.8
C	8.0	65.8
S	8.1	65.7
+5 Sid. gar dirt fl.	8.2	65.6
3+41		
S +0.4 14" Pow. Pole		
3+50		
S	6.8	67.0
C	6.9	66.9
+7	6.7	67.1
+8.5 N edge Conc apron	6.19	67.60
+9.7 " " gar " fl	5.82	67.97
3+59		
N	5.76	68.03
+1.5 Conc apron	5.98	67.81

3+65			
N E edge gar. Conc fl	5.67	68.12	Line
C	5.9	67.9	
S E Sid. gar ? fl.	6.1	67.7	
3+89			
N -0.5 2' Conc. walk	3.51	70.28	
4+00			
S fence 0.3 in alley	2.6	71.2	
+2	3.1	70.7	
C	3.0	70.8	
N	2.8	71.0	
T.P. 12.57 86.10	0.26	73.53	
4+35			
-2.8 gar dirt	12.5	73.6	8' wide
N	12.4	73.7	
C	12.6	73.5	
+8	12.4	73.7	
+9.8 fence	12.1	74.0	
4+45			
S	11.1	75.0	
0.8 Earth fence			
+2	11.6	74.5	
C	11.6	74.5	
N	11.0	75.1	
+2.4 Sid. gar dirt fl.	11.0	75.1	

86.10

4+49

S 1" Pow. Pole on Line

4+83

N+1.2 12" Tel Pole

4+94

-2.3	Sin gar	cem. fl.	7.17	78.93	8' wide
N			7.2	78.9	
C			7.1	79.0	
S			7.2	78.9	

5+18

S			4.9	81.2	
C			4.9	81.2	
N			4.1	82.0	
+2	Sin gar	dirt	4.0	82.1	

5+29

N ℄ 10' Bd. Shed 0.4 in alley

5+51

N			1.3	84.8	
C			1.6	84.5	
S			1.2	84.9	
+0.4	Top wall		0.6	85.5	
T.P.	11.10	96.78	0.42	85.68	

96.78

47

5+62

-18	Bsmt Gar. Cem	10.80	85.98
-17	℄ Cem Apron	10.80	85.98
S		11.2	85.6
C		11.2	85.6
N		10.9	85.9
+5		10.9	85.9

5+71

N		9.8	87.0
C		10.2	86.6
S		10.0	86.8
+0.2	Top wall	9.29	87.49

5+88

S	Top Brick Ret wall	4.13	92.65
S		6.3	90.5
C		6.7	90.1
N		6.6	90.2

5+94

N		5.5	91.3
C		5.5	91.3
S		5.0	91.8
S	Top wall	4.20	92.58

5+99.2 = W/y Line Froude

S c6		4.26	92.52
S Pav		4.85	91.93
C "		5.08	91.70
N "		5.09	91.69
N c6		4.57	92.21

96.78

4' E of W ℄ Froude

N cb		4.58	92.20
N Pav		4.88	91.90
C "		4.70	92.08
S "		4.59	92.19
S cb		4.44	92.56
12' E of "	" ℄ W cb Froude		
S Pav		4.86	91.92
N "		5.18	91.60

Top cb. SW Froude ℄ Saratoga 4.81 89.97 90.00 Profile Grade

W cb Froude ℄

SL Saratoga

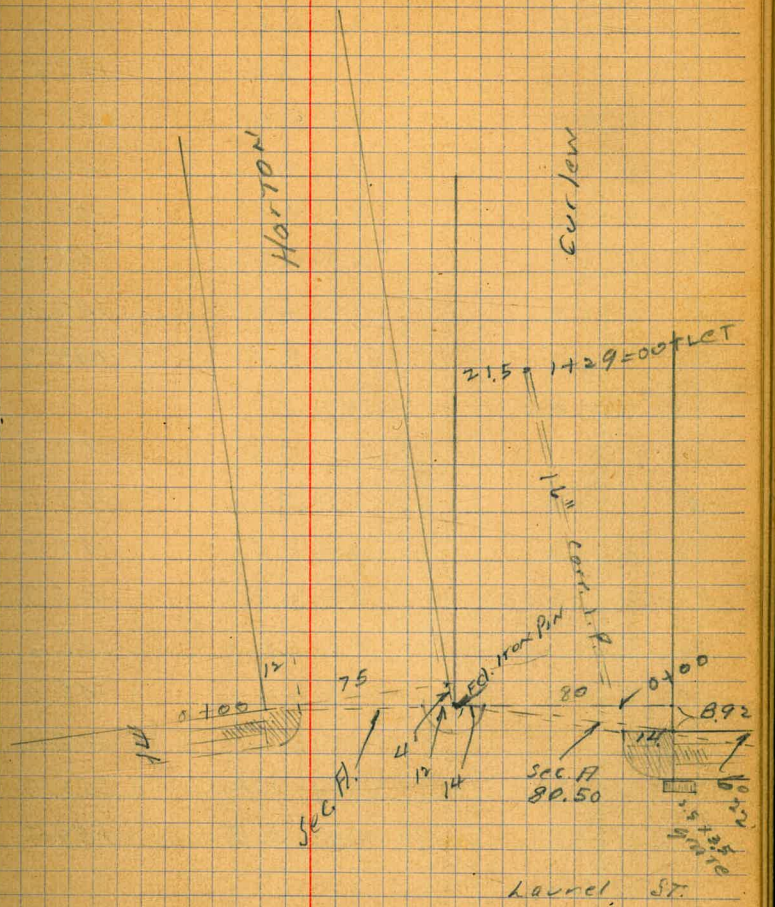
INDEXED
EFB

X Sec Curlew 80' wide 14' curbs 13' 1/4

Laurel N/y

6.14	15 x 21		146.07
	Sec A		
E		2.1	150.1
+4		4.0	148.2
cb	Top cb	4.18	148.03
gut	Pax	4.78	147.43
1/4	"	4.61	147.60
C	"	4.61	147.60
1/4	"	4.93	147.28
gut	"	5.41	146.60
cb	Top Ret	5.13	147.08
W	Iron Pin	5.0	147.2
	0+00		
W	Iron Pin	5.0	147.2
cb		5.1	147.1
1/4		4.9	147.3
C		4.5	147.7
1/4		4.5	147.7
cb		4.4	147.8
+9		4.0	148.2
E		2.0	150.2
+3	Top Bank	+2.4	154.6
	0+50		
-5		+6.0	158.2

Reduced Plot 2-21-90 CBH



152.21

0+50		
E	1.5	150.7
+4	4.0	148.2
cb	4.2	148.0
1/4	4.1	148.1
c	4.1	148.1
1/4	4.0	148.2
cb	4.2	147.8
W	4.5	147.7
1+00		
W	5.2	147.0
cb	5.1	147.1
1/4	3.5	148.7
c	3.5	148.7
1/4	3.7	148.5
cb	3.4	148.6
+4	3.6	148.6
E	+3.8	156.0
+5	+5.5	157.7
1+10		
-5	+2.0	154.2
E	+1.0	153.2
cb	1.4	150.8
1/4	3.3	148.9
c	2.6	149.6
1/4	3.2	149.0

152.21

cb	2.8	149.4
W	2.8	149.4
1+20		
W	4.5	147.7
cb	4.3	147.9
1/4	4.9	147.3
c	4.4	147.8
1/4	4.7	147.5
cb	4.1	147.1
E	0.8	151.4
1+29		
E	4.1	148.1
cb	5.4	146.6
1/4	5.6	146.6
c	7.4	144.8
1/4	9.2	143.0
+3 Bottom ditch	24.1	128.1
+5.5 FL. 16" outlet	11.57	140.64
+9 Bottom ditch	24.0	128.2
cb	9.4	142.8
W	9.8	142.4
1+40		
-10	17.9	134.3
W	17.1	135.1
+12	16.4	135.8
cb	25.4	126.8

1740	152.21		
c6 + 9		17.1	135.1
1/4		14.7	137.5
c		13.2	139.0
1/4		10.2	142.0
c6		8.4	143.8
E		7.2	145.0
+ 10		5.8	146.4

Xsec Horton

75' wide
12' cbs
12.75 1/4

Laurel N/y 152.21

Sec A = N L Laurel

E's	Iron Pin	5.0	147.2
cb	Top curb	5.13	147.08
qut	Pav	5.78	146.43
1/4	"	5.72	146.49
c	"	5.77	146.44
1/4	"	6.08	146.13
qut	"	6.62	145.59
cb	Top	6.20	146.01
W		5.9	146.3
	0+50		
W		5.8	146.4
cb		5.3	146.9
1/4		5.2	147.0
c		5.3	146.9
1/4		5.1	147.1
cb		4.8	147.4
E		4.5	147.7
	1+00		
E		4.4	147.8
cb		5.4	146.8
1/4		5.3	146.9
c		5.8	146.4
1/4		6.9	145.3

Reduced + Plot. 2-21-40 C.B.H.

152.21

INDEXED EFB

cb		7.3	144.9
W		7.3	144.9
	1+12		
W	& 3' Con. walk	10.06	142.15
	1+25		
W		10.9	141.3
cb		10.6	141.6
1/4		9.4	142.8
c		8.8	143.4
1/4		6.1	146.1
+6		6.2	146.0
cb		8.4	143.6
E		9.4	142.8
+10		9.0	143.2
	1+35		
-10		13.5	138.7
E		13.0	139.2
cb		12.0	140.2
+7		9.3	142.9
1/4		9.7	142.5
+8		12.4	139.8
c		16.7	135.5
+7		13.4	138.8
1/4		12.5	139.7
+4	Pepper Tree		
cb		12.4	139.8
W		12.3	139.9

15221

1750

W	17.0	135.2
cb	17.7	134.5
1/4	21.5	130.7
C	22.2	130.0
1/4	21.0	131.2
cb	22.4	129.8
E	23.2	129.0
+10	24.2	128.0

Moore
Sisson
Northern
Osborn
3-4-40

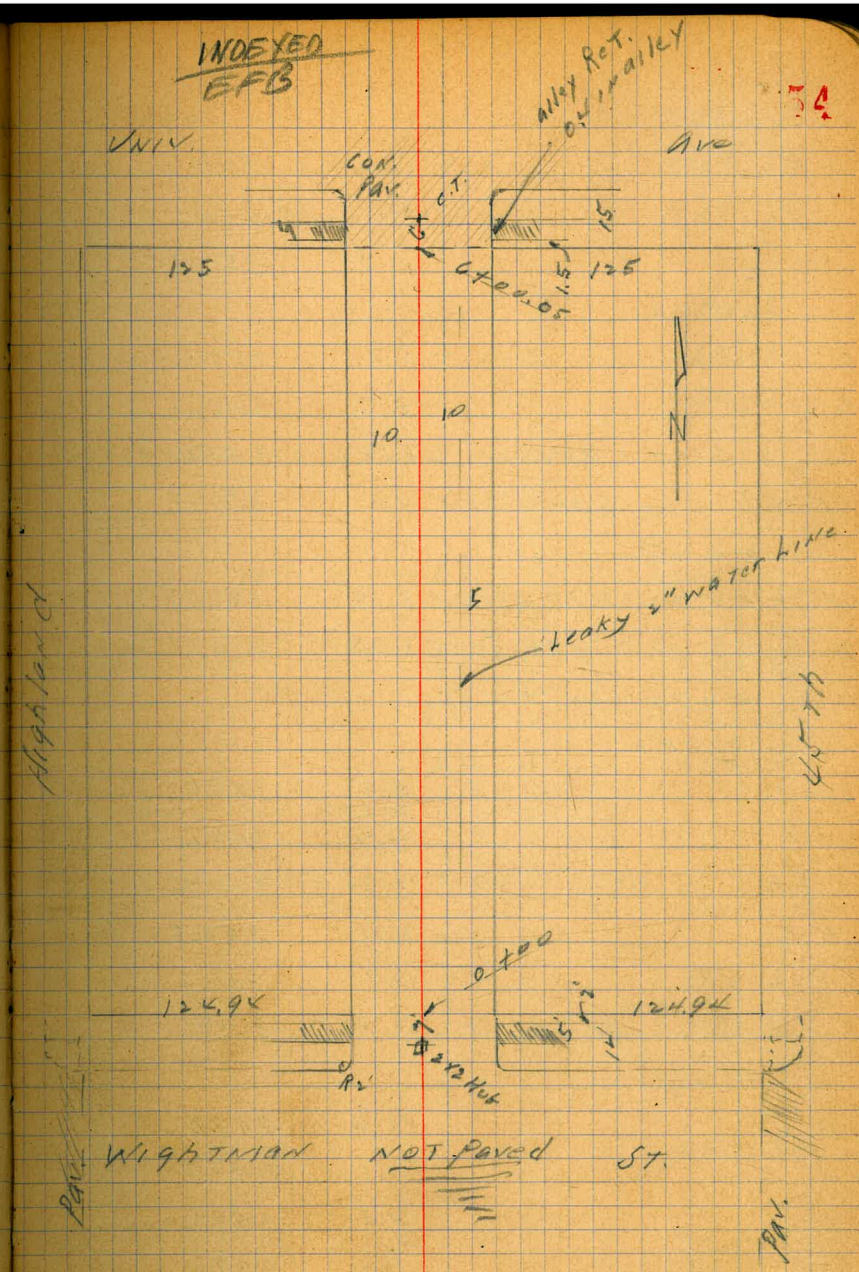
X sec. of Alley 20' wide
Blk 6 Subd. of Blk 3-6-9-12
City Hts. Annex #1.

					Wightman @ 45th
NWBP	6.42	353.79		347.37	
0-14 N cb Wightman					
E ~ 125 WL 45th			6.45	347.34	Top cb
" " " "			6.96	346.83	gut Pav
E.L. alley			5.05	348.74	Top cb.
" "			5.6	348.2	gut.
℄ "			5.4	348.4	"
W L "			5.3	348.5	"
" "			4.81	348.98	Top cb.
+ 125 E.L. Highland			3.56	350.23	" "
" " "			4.16	349.63	gut. Pav
0+00 NL Wightman					
W Top cb.			4.57	349.22	
W			4.4	349.4	
C			4.3	349.5	
E			4.7	349.1	
E " "			4.89	348.90	
0+06					
E			4.0	349.8	
E			4.2	349.6	
W			3.7	350.1	

Notes Reduced & Plot 3/5/40 on Profile 2715 C.B. Hough

INDEXED
EFB

34



353.79

0+25		
W	3.2	350.6
C	3.7	350.1
E	3.5	350.3
0+40		
E	3.7	350.1
C	3.7	350.1
W ℄ Cem. apron	3.12	350.67 g'wide
+2.8 Sin. gar. Cem	2.91	350.88
0+47		
E +0.2 ℄ Cem apron	3.74	350.05
E −2.7 Sin. gar. Cem	3.68	350.11
0+71 W +0.7	12" P.P.	
0+80		
−5	4.2	349.6
W	4.2	349.6
+3	3.4	350.4
C	3.7	350.1
E	3.9	349.9
+3 Sin. gar. cem.	3.83	349.96
1+00		
−5	4.6	349.2
E	4.1	349.7
C	4.2	349.6
W	4.2	349.6
+5	4.3	349.5

353.79

55

1+10		
W −2 Cem. apron	4.10	349.69
W −6 Sin gar cem	3.96	349.83
1+50		
W	4.0	349.8
C	4.0	349.8
E beg. fence	3.8	350.0 0.2 in alley
1+84 end above fence		on line
1+90		
E −3 Sin. gar dirt	3.6	350.2
2+00		
E	3.6	350.2
C	3.3	350.5
W	3.4	350.4
2+02 W +0.9	12" P.P.	
T.P. 5.79 356.14	3.44	350.35
2+25		
W	5.7	350.4
C	5.6	350.5
E	5.6	350.5
2+40		
C Rm S.M.H.	5.20	350.94
2+43		
E−12 Sin gar dirt	5.4	350.7
E	5.5	350.6
C	5.8	350.8

W		5.3	350.8
2+47			
W		4.7	351.4
C		5.2	350.9
E		5.0	351.1
+0.4 Cem. apron		5.01	351.03 13
+10.4 E Sin. gar.		4.91	351.23 Cem.
2+80			
W – 13 do. gar. dirt		4.7	351.4
3+02			
E		4.4	351.5
C		4.7	351.4
+9.8 12" P.P.			
W		4.5	351.6
3+44			
W E 13' shed Bd. + Bat.	could be gar. dirt	4.2	351.9 1N 0.5 alley
C		4.3	351.8
E		4.3	351.8
3+56			
E – 5.2 E Sin. gar. dirt		4.4	351.7
3+75			
E		3.9	352.2
C		4.1	352.0
W		3.9	352.2

3+94		
W – 2.8 Sin. gar. dirt	3.3	352.8
4+01		
W	3.3	352.8
+0.4 12" P.P.		
C	3.7	352.4
E	3.7	352.4
4+07		
E – 4 Sin. gar. dirt	3.7	352.4
4+40		
E	3.6	352.5
C	3.6	352.5
W	3.5	352.6
+1.0 apron Cem.	3.54	352.60
+4 Sin. gar. Cem.	3.35	352.79
4+75		
W	3.5	352.6
C	3.8	352.3
E	3.9	352.2
T.P. 4.45 356.57	4.02	352.12
4+90		
E – 5 Sin. gar. dirt	4.4	352.0
E	4.4	352.0
C	4.3	352.3
W	4.3	352.3
+17.6 do. gar. Cem.	3.45	353.12

		356.57			
5+02 W+0.5		12" P.P.			
5+42					
W			5.1	351.5	
C			5.4	351.2	
+ 9.9 ℄ 3' door to Bldg.		Cem. Tile	5.20	351.37	
5+71					
E + 0.10 against Bldg			5.5	351.1	
C			5.5	351.1	
+ 9.7	12" P.P.		5.2	351.4	5+37 SW Cor. of Cem. Tile Bldg 0.10 in alley
W			5.2	351.4	
6+00.05 S.L. Univ. Ave					
W	Top cb		5.68	350.89	
W	Pav.		5.82	350.75	
C	"		6.18	350.39	
+ 9.6	"		6.18	350.39	
+ 9.6	Top cb		6.13	350.44	
℄ cb Line Univ.					
E	Pav		6.80	349.77	
C	"		6.68	349.89	
W	"		6.60	349.97	
T.P.	5.81	356.29	6.09	350.48	
NWBP	46th Univ.		5.02	351.27	351.23

Cross Section Alley Block 257 Hayden's Sub.
Between Dalbergia + Main From Yama to Division

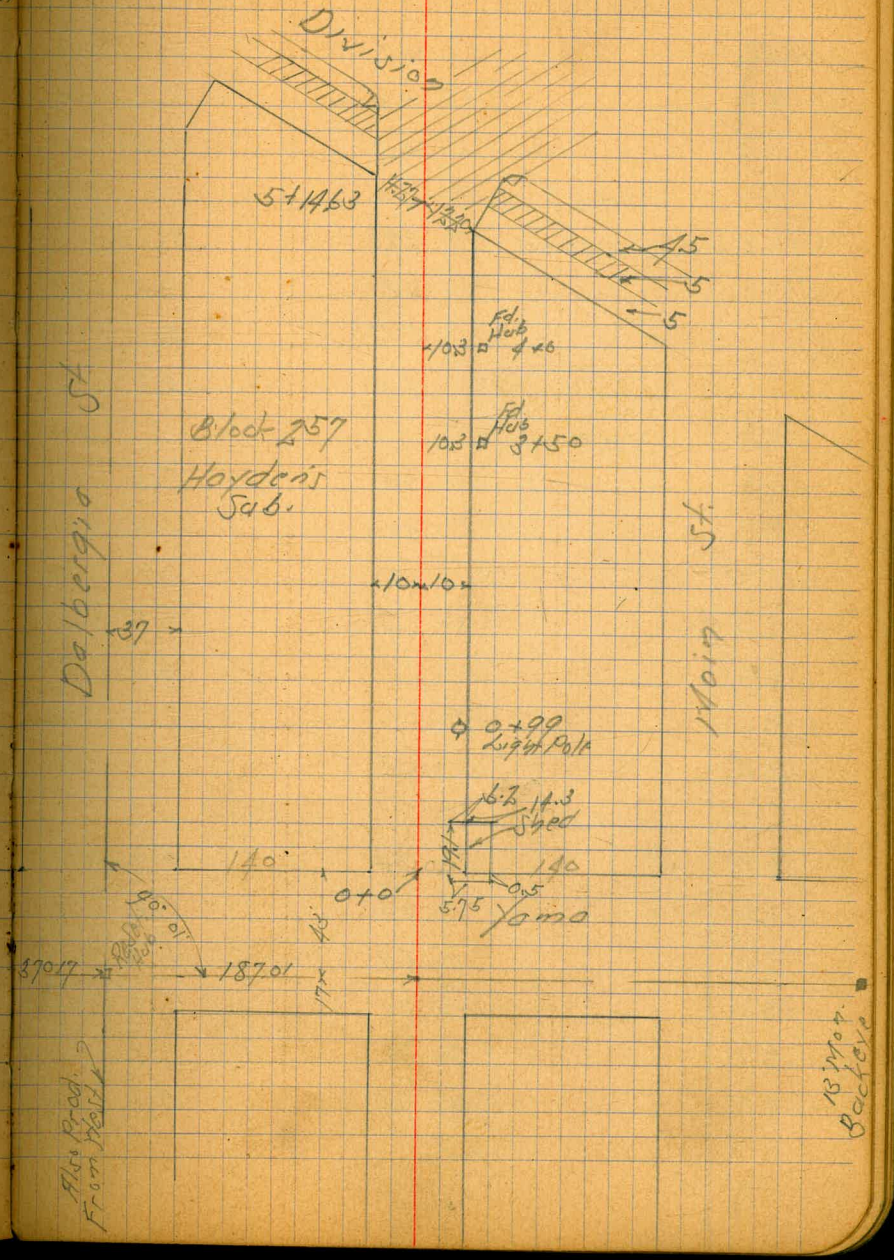
BM	4.39	13.37		8.98	H.W.B.P. Main + Division
TP	5.56	12.56	6.37	7.00	
	0-30 = ℄ Yama				
S			6.1		6.5
℄ on MH Rim			5.88		6.68
+6			5.6		7.0
+9 = Bot. Ditch From West			10.1		2.5
H			9.8		2.8
+3			5.6		7.0
	0-25				
H			10.1		2.5
℄			10.3		2.3
S			10.0		2.6
	0-17 = ℄ Wash				
S			10.9		1.7
℄			11.1		1.5
H			10.5		2.1
	0-10				
H			10.5		2.1
℄			10.2		2.4
S			10.6		2.0
	0+0 = E.L. Yama				
S			5.2		7.4
℄			5.0		7.6
H			4.9		7.7

Red. + Plot. on New profile May 31-40 C.B. Hough

INDEXED
EFB

May 28-40
Sisson
Northern
W. Moore

58



12.56

0+25

N	5.5	7.1
d	5.4	7.2
S	5.2	7.4

0+57

-04 = El 4.8 Concrete Walk	4.91	7.65
S	5.2	7.4
d	5.5	7.1
N	6.4	6.2

1+0

-10	7.0	5.6
N	7.1	5.5
+5	6.5	6.1
d	6.4	6.2
S	6.6	6.0
+2	5.1	7.5
+15	5.3	7.3

1+25

-15	7.4	5.2
S	7.4	5.2
d	6.9	5.7
+7	7.1	5.5
N	7.5	5.1
+15	7.5	5.1

12.56

1+70

-15			7.6	5.0
N			7.8	4.8
d			7.3	5.3
+7			7.1	5.5
S			7.5	5.1
+15			7.9	4.7
TP	10.61	15.92	7.25	5.31

2+0

-15	11.4	4.5
S	11.4	4.5
+2	10.9	5.0
d	10.6	5.3
+6	10.8	5.1
+8	11.5	4.4
N	11.4	4.5
+15	11.3	4.6

2+25

-15	11.6	4.3
N	11.8	4.1
+2	11.7	4.2
+4	11.3	4.6
d	10.9	5.0
+7	10.8	5.1
S	11.6	4.3
+15	11.8	4.1

15.92

2+50

-15	12.0	3.9
S	11.6	4.3
+5	10.9	5.0
D	10.8	5.1
+5	11.2	4.7
N	11.7	4.2
+15	11.7	4.2

2+75

-15	11.4	4.5
N	11.4	4.5
+5	10.8	5.1
D	10.6	5.3
+7	10.6	5.3
S	11.6	4.3
+15	11.8	4.1

3+0

-15	10.0	5.9
S	9.9	6.0
+3	9.3	6.6
D	9.2	6.7
+5	9.5	6.4
N	10.2	5.7
+15	10.6	5.3

15.92

3+50

-10	5.9	10.0
N	5.0	10.9
D	4.9	11.0
S	5.3	10.6
+10	5.8	10.1

3+75

-10	3.0	12.9
S	2.7	13.2
D	2.6	13.3
N	2.9	13.0
+10	2.8	13.1
TP	8.50 23.99	0.43 15.49

4+0

-10	8.2	15.7
N	8.5	15.5
D	8.5	15.5
S	8.5	15.5
+10	8.6	15.4

4+50

-10	6.8	17.2
S	6.4	17.6
+5	5.9	18.1
D	5.9	18.1
N	5.5	18.5
+10	5.3	18.7

23.99

4+75

-10	4.7	19.3
N	5.0	19.0
℄	5.3	18.7
+1	5.2	18.8
+4	4.4	19.6
S	5.0	19.0
+10	5.7	18.3

5+0

-10	4.0	20.0
S	2.9	21.1
+2	2.3	21.7
+5	4.8	19.2
℄	4.9	19.1
N	4.3	19.7
+10	3.8	20.2

5+14.63 Taken on Line of Paving

N Cb Top	2.88	21.11
Gutter on Paving	3.55	20.44
℄ " "	4.61	19.38
S Gutter " "	5.18	18.81
S Cb Top	4.99	19.00

N Cb Division

S on Paving opp Alley Return	5.60	18.39
℄ " "	3.92	20.07

23.99

N on Pav opp Alley Ret			3.17	20.82	
TP	2.70	14.34	12.35	11.64	
B.M			5.37	8.97	N.W. B.P. Main + Division 8.98

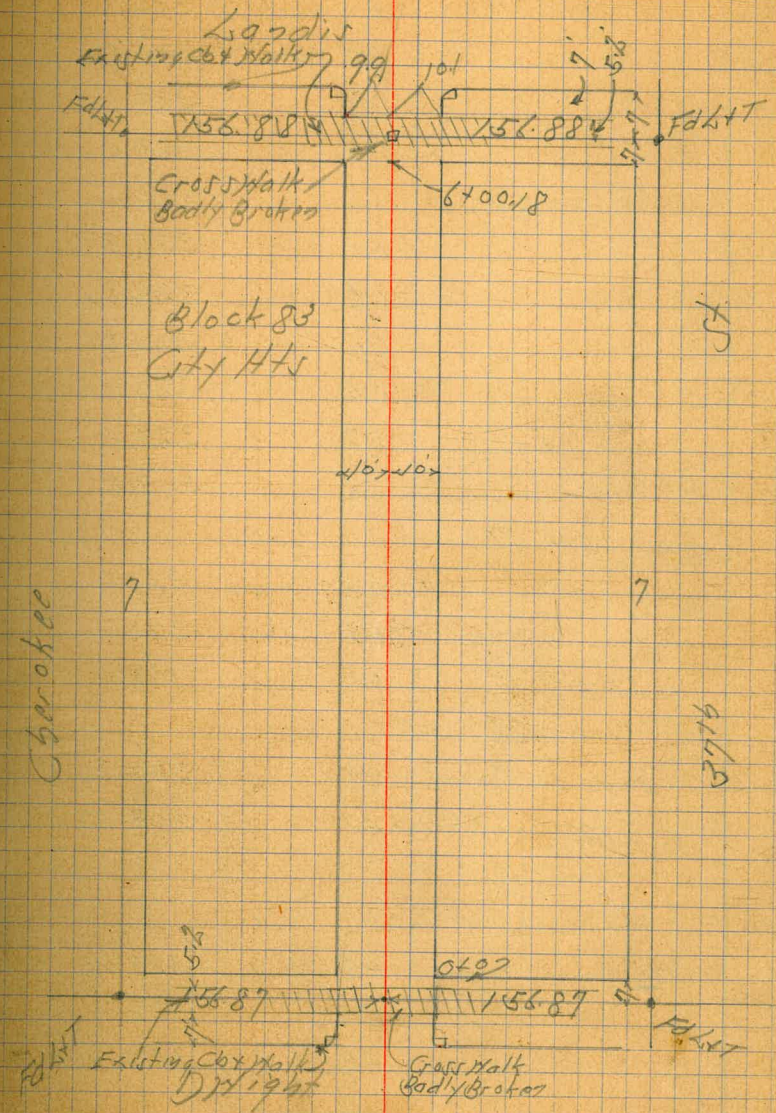
INDEXED
EPD

May 29-40
Sisson
Northern
H Moore

Cross Section Alley Block 83 City Hts.
Between Cherokee & 37th St. From Dwight to Landis

B.M.	5.88	325.87		319.99	N.W.B.P. Dwight & 37th St.
TP	8.71	333.37	1.21	324.66	
0-14 = N Cb Dwight					
E Cb Top			9.20	324.17	
E Ground			9.8	323.6	
℄ "			9.5	323.9	
W "			9.2	324.2	
W Cb Top			8.55	324.82	
0-7 = Sly Conc Walk					
W on Conc Walk			8.37	325.00	
E " " "			9.02	324.35	
0-1.8 = Nly Conc Walk					
E on Conc Walk			8.87	324.50	
W " " "			8.27	325.10	
0+0 = N.L. Dwight					
W			7.7	325.7	
+3			7.7	325.7	
+7			8.6	324.8	
℄			8.5	324.9	
+6			8.6	324.8	
E			8.1	325.3	
0+6					
E			6.3	327.1	
+2			6.5	326.9	
+5			8.1	325.3	

Reduced & Plot on Profile 2549
May 31-40. C.D.H.



	333.37				
℄			8.1	325.3	
+6			8.2	325.2	
+8			4.3	327.1	
W			6.0	327.4	
	0+25				
W			5.1	328.3	
+7			6.6	326.8	
℄			6.6	326.8	
+5			6.5	326.9	
+6			5.8	327.6	
E			5.6	327.8	
	0+45				
E			5.2	328.2	
℄			5.1	328.3	
W			5.0	328.4	
	0+56				
W-6.7 = Ely Conc Apron			4.71	328.66	✓
W-9.4 = ℄ Garage Conc Floor			4.10	329.27	✓
	0+74				
W-1.0 = Wly Power Pole					
W			4.2	329.2	
℄			4.5	328.9	
E			4.7	328.7	
TP	5.17	334.11	4.43	328.94	

	334.11			
	0+95			
-40 = ℄ Garage Conc Floor	5.99		328.12	✓
E	5.0		329.1	
℄	5.2		328.9	
W	4.8		329.3	
+6 = Ely Conc Apron	4.82		329.29	✓
+8.8 = ℄ Garage Conc Floor	4.32		329.79	✓
	1+25			
E -1.7 = ℄ Garage Dirt Floor	4.0		330.1	✓
	1+50			
W	3.5		330.6	
℄	3.9		330.2	
E	3.8		330.3	
+10	4.3		329.8	✓
	2+0			
-10	3.2		330.9	✓
E	2.6		331.5	
℄	2.8		331.3	
+3	3.4		331.7	
W	1.6		332.5	
+10	2.6		331.5	✓
	2+02			
W-0.4 = Wly Power Pole				
TP	6.17	337.95	2.83	331.78

337.95

2+25

-10	5.7	332.3 ✓
-1	5.9	332.1 ✓
W	5.4	332.6
+6	4.9	333.1
℄	5.5	332.5
+7	5.7	332.3
E	6.2	331.8
+10	6.6	331.4

2+45

E-8.8 = W℄ Conc Apron	6.25	331.70 ✓
E-10.8 = ℄ Garage Conc Floor 8' W. of	6.06	331.89 ✓
E	5.8	332.2
+3	5.5	332.5
℄	5.4	332.6
+2	5.4	332.6
+6	4.6	333.4
W	5.0	333.0
+1	5.6	332.4
+10	5.7	332.3

2+56

W-2.3 = E℄ 8' Conc Apron	5.38	332.57 ✓
W-5.8 = ℄ Garage Conc Floor	4.67	333.28 ✓

337.95

2+83

-10	4.8	333.2
W	4.3	333.7
℄	5.0	333.0
+2	5.0	333.0
E	5.7	332.3
+5.2 = ℄ Garage Conc Floor	5.73	332.22 ✓

2+94

W-1 = ℄ 8' Conc Apron	4.58	333.37 ✓
W-5.7 = ℄ Garage Conc Floor	3.72	334.23 ✓

340

W+0.2 = W℄ Power Pole

3+26

-10	5.3	332.7
E	4.8	333.2
℄	4.6	333.4
W	4.5	333.5
+04 = ℄ 3' Conc Walk	4.37	333.58 ✓

3+27

E-4.8 = S℄ Do. Garage Conc Floor	4.70	333.25 ✓

3+43

E-4.6 = W℄ Do Garage Conc Floor	4.66	333.29 ✓

3+60

W	4.2	333.8
℄	4.3	333.7

	337.95		
F		4.4	333.6
	3+68		
F = Δ 2' Conc Walk		4.26	333.69 ✓
+24 = W/y 2' " "		4.22	333.73 ✓
	3+96		
F = Δ 2' Conc. Walk		3.63	334.32 ✓
	4+0		
F		3.6	334.4
Δ		3.2	334.8
+8		3.3	334.7
+9.9 = W/y Power Pole			
W		3.5	334.5
+15		3.6	334.4
	4+50		
-15		2.8	335.2
W		3.1	334.9
Δ		3.0	335.0
F		2.8	335.2
+10		3.2	334.8
TP	6.07 341.04	2.98	334.97
	4+85		
W - 7.2 = Δ Garage Dirt Floor		5.4	335.6 ✓
	5+0		
-10		5.7	335.3
F		5.3	335.7

	341.04		
Δ		5.2	335.8
+9.7 = W/y Power Pole			
W		5.2	335.8
	5+30		
W		5.0	336.0
Δ		5.0	336.0
F		4.9	336.1
+10		5.3	335.7
	5+56		
F		4.3	336.7
Δ		4.2	336.8
+9.8 = E/y 4' Conc Apron		4.17	336.87
W " " "		4.14	336.90
+3 " " "		4.04	337.00
	5+68 = W/y Garage on E Entrance		✓
W		4.0	337.0
Δ		4.1	336.9
F		4.1	336.9
+3.6 W/y Conc Drive		3.98	337.06 ✓
	5+90		
-2.6 = W/y Conc Drive		4.23	336.81 ✓
F		4.5	336.5
+3		3.9	337.1
+5		4.6	336.4
Δ		4.6	336.4

		341.04			
W			4.4	336	6
	6+00.18 = S.L. Landis				
W			4.6	336	4
+5			5.3	335	7
℄			5.3	335	7
+4			5.4	335	6
+7			4.9	336	1
E			5.4	335	6
	6+02 = Sly Conc Walk				
E = Sly Conc Walk			5.77	335	27
W = Sly Conc "			5.34	335	70
	6+07.2 = Nly Conc. Walk				
W on Conc Walk			5.42	335	62
E " " "			5.84	335	20
	6+14.2 = Sly Cb Landis				
E Cb Top			6.08	334	96
E Ground			6.5	334	5
℄ "			6.2	334	8
W "			6.0	335	0
W Cb Top			5.64	335	40
TP	7.74	342.72	6.06	334.98	
BM			7.47	335.25	N.W. BP Landis + 36th 335.25

Cross Section Alleys Block 47
W.P. Herberts Subdivision

Indexed
LM

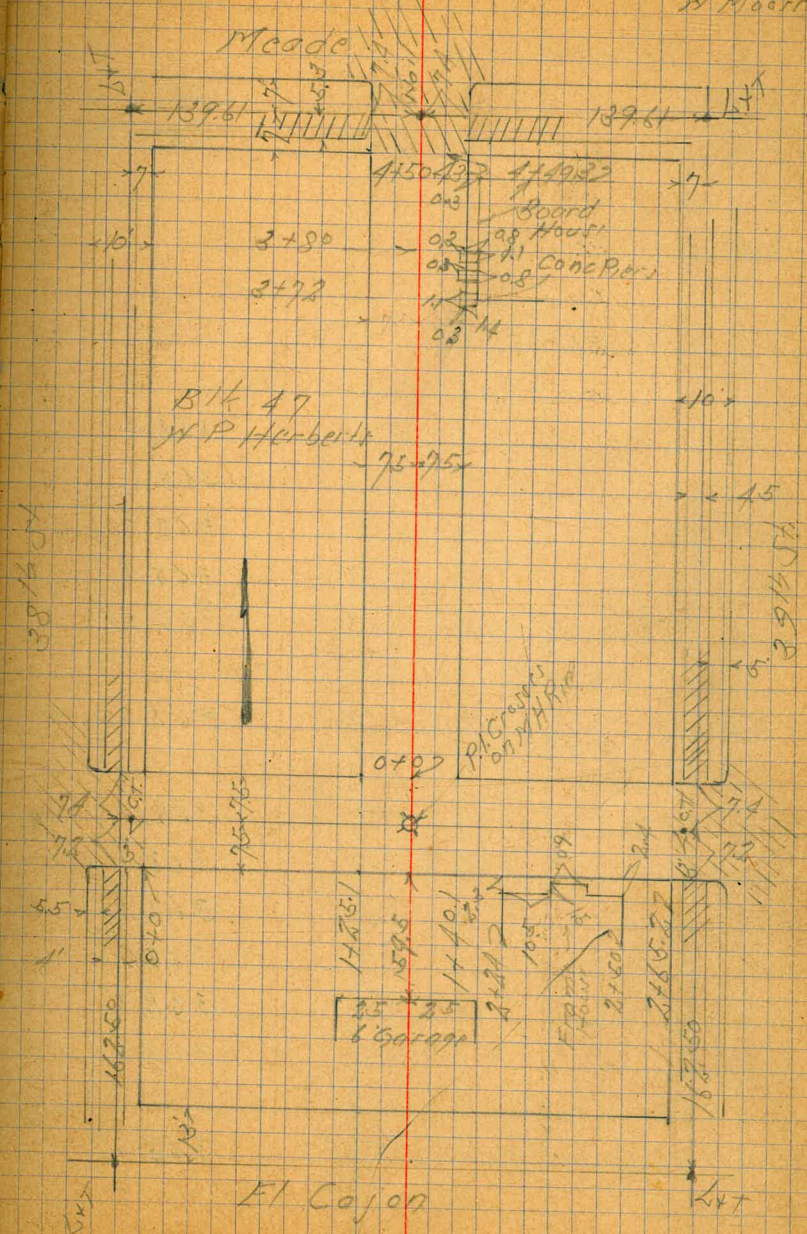
East & West Alley 15' Wide

BM	4.17	371.89		367.72	SWBP El Cajon & 39th St on MH & N&S Alley
TP	5.91	373.70	4.10	367.79	
	0-10 = ECb 38th St				
S on Paving			4.61	369 09	
℄ " "			4.56	369 14	
N " "			4.52	369 18	
	0+0 = EL 38th St				
N Top Cb			3.75	369 95	
Gutter on Paving			3.97	369 73	
℄ " "			4.24	369 46	
Gutter "			4.00	369 70	
S Top Cb =			3.81	369 89	
+0.5 = Wly & ℄ 2' Hedge					
	0+20				
-2.1 = Wly 2' Conc Walk			4.00	369.70	✓
-0.2 = Ely & ℄ 2' Wide Hedge					
S			4.2	369.5	
℄			4.7	369 2	
+5			4.7	369 2	
N			4.2	369.5	
+3.5 = Wly Frame House Ely Conc Porch			3.27	370 43	✓
	0+42				
-3' = Sly Frame House			5.0	368 7	✓
N			4.9	368.8	

Red & Plot on 2693 2-24-41 CBH

Feb. 20-41
Sisson
Northern
W Moore

69



373.70

℄	5.3	368.4
+6.3 = Wly ℄ 2.5 Wide Hedge		
S	4.8	368.9
+2' = Wly 2' Conc Walk	4.45	369.25 ✓
0+60		
N -3.5 = Ely Frame House		✓
0+62		
S +0.5 = ℄ & Ely 2.5 Wide Hedge		+
0+70		
-5	5.3	368.4
S	5.4	368.3
℄	5.4	368.3
N	5.3	368.4
+6.5 = Sly 2' Conc Walk	5.42	368.28 ✓
0+86		
S -10.3 = ℄ Garage Conc Floor 7' opening	5.20	368.50 ✓
1+0		
-5	5.7	368.0
N	5.6	368.1
℄	5.8	367.9
+5	5.7	368.0
S	5.4	368.3
+5	5.5	368.2
1+19		
N -4.8 = ℄ Garage Conc Floor	5.61	368.09 ✓

373.70

1+25.1 = N.L. N+S Alley

-5	5.6	368.1
S	5.4	368.3
℄	5.9	367.8
N	6.1	367.6
1+30		
S -0.2 = Sly Power Pole		×
1+32.6 = ℄ N+S Alley		
N	6.1	367.6
℄ on MH Rim	5.90	367.80 ✓
S	5.8	367.9
+59.5 = Wly + ℄ 6 Garages Conc Floor	4.76	368.94 ✓
1+40.1 = E.L. N+S		
-5	6.0	367.7
S	6.1	367.6
℄	6.1	367.6
N	6.0	367.7
+0.6 = Wly Fence		
1+64		
-5	6.2	367.5
N	6.1	367.6
℄	6.1	367.6
S	6.1	367.6
+6.5 = ℄ Garage Conc Floor	5.57	368.13 ✓

373.70

1+73			
S -0.1 = Wly Board Fence			
1+92			
N -2.6 = Sly + ℄ 2' Conc Walk	5.97	367.73	✓
2+0			
-5	5.9	367.8	
S	6.0	367.7	
℄	6.2	367.5	
N	6.2	367.5	
+0.7 = Fence			✓
+5	6.1	367.6	
2+03			
S = Ely Board Fence			✓
2+24			
-5	6.1	367.6	
N	6.2	367.5	
℄	6.3	367.4	
S	6.2	367.5	
+2.3 = N W Cor. Frame Ho.	6.2	367.5	✓
2+43			
N -0.6 = Ely Fence + Sly 2' Hedge			✓
2+50			
-2.4 = N E Cor House	6.5	367.2	✓
S	6.4	367.3	
℄	6.7	367.0	

373.70

N	6.3	367.4	
+5	5.8	367.9	
2+65.2 = W L 39th St			
-0.5 = Ely + Sly 2' Hedge			✓
N Top Ch	6.29	367.41	
Gutter on Paving	6.50	367.20	
℄ " "	6.74	366.96	✓
Gutter " "	6.60	367.10	
S Top Ch	6.37	367.33	
2+75.2 = W Cb 39th St			
S on Paving	7.13	366.57	
℄ " "	7.11	366.59	
N " "	7.12	366.58	
TP 4.96 372.75	5.91	367.79	

North & South Alley

372.75

0+0 = N-S East & West Alley

-025 = S'ly Fence			
E	4.8	368.0	
℄	5.2	367.6	
W	5.1	367.7	
0+27			
-10	5.0	367.8	
W	4.9	367.9	
℄	5.0	367.8	
E	4.9	367.9	
+0.6 = N'ly Fence			
+2 = SW Cor Bldg.	4.6	368.2	
0+30			
W+2.5 = W'ly Pow Pole			
0+44			
W-6.0 = ℄ Garage Conc Floor	4.37	368.38	
0+49			
E-2 = NW Cor Bldg	4.9	367.9	
E	4.8	368.0	
℄	4.7	368.1	
W	4.6	368.2	
+5	4.6	368.2	
0+54			
W+11 = S'ly Board Fence			
0+71			
-10	5.8	369.0	

Red Y Plot Dn 2693 3-24-41 CB/H

372.95

W	3.9	368.9
+13 = W'ly Board Fence		
℄	4.7	368.1
E	4.7	368.1
+10	4.6	368.2
0+81		
W-5.1 = S'ly Dr Garage Conc Floor	3.43	369.32 ✓
0+98		
W-5.0 = W'ly Dr Gar Conc Floor	3.27	369.48 ✓
1+0		
-10	4.4	368.4
E	4.3	368.5
℄	4.2	368.6
W	3.9	368.9
+5	3.7	369.1
1+01		
W+8.3 = W'ly Pow Pole		✓
1+10		
E-18 = W'ly Conc Ho-om	4.01	368.74 ✓
E-20 = ℄ Garage Conc Floor	3.89	368.86 ✓
W-5.8 = ℄ Garage Conc Floor	3.5	369.3 ✓
PP 583 37466	3.92	368.83
1+41		
-10	5.8	368.9
W	4.1	368.6

37466

℄	5.8	368.9
E	5.9	368.8
+1.7 = ℄ly Conc Apron	5.95	368.71 ✓
+7.6 = ℄ Garage Conc Floor	5.87	368.79 ✓
1+70		
E -1.0 = Sly Wire Fence		+
1+75		
-1.0	5.8	368.9
E	5.9	368.8
℄	5.7	369.0
ℳ	5.6	369.1
+10	5.3	369.4
2+0		
-10	5.2	369.5
ℳ	5.7	369.0
℄	5.6	369.1
E	5.9	368.8
+0.2 = Nly Wire Fence = Sly Board Fence	6.7	368.0 +
+10		
2+12		
ℳ +1.6 = Nly Power Pole		✓
2+50		
-10	6.0	368.7
-0.3 = Board Fence		
E	5.8	368.9

37466

℄	5.5	369.2
ℳ	5.5	369.2
+10	5.4	369.3
2+60		
ℳ -11.7 = ℄ Garage Conc Floor	4.95	369.91 ✓
2+66		
E -0.4 = ℄ 1.5 Conc Walk	5.87	368.79 ✓
2+75		
-10	4.8	369.9
ℳ	5.7	369.5
℄	5.7	369.5
E +0.3 = Board Fence	5.4	369.3 - E
+10	5.8	368.9
2+85		
ℳ -11.8 = ℄ Garage Conc F	4.30	370.36 ✓
3+0		
-10	5.3	369.4
E	4.9	369.8
+0.3 = Fence Failure		+
℄	4.9	369.8
ℳ	4.6	370.1
+10	4.6	370.1
3+09		
ℳ +11.5 = ℄ Garage Conc Floor	4.17	370.49 ✓
3+24		
E +1.0 = Nly Failure Fence + Sly Wire Fence		+

374.66

3+35

-11.7 = ℄ Garage Conc Floor	3.67	370.99	✓
W	4.3	370.4	
℄	4.3	370.4	
E	4.4	370.3	
+10	4.7	370.0	

3+48

E+0.3 = Nly Wire Fence			+
W = Wly Pow Pole			✓

3+63

-6.8 = ℄ Garage Conc Floor	4.17	370.49	✓
E	4.2	370.5	
℄	4.2	370.5	
W	4.1	370.6	
+10	4.0	370.7	

3+72

W-12 = ℄ Garage Conc Floor	3.65	371.01	✓
E+0.3 = Top Conc Pier	3.02	371.64	+

3+80

E+0.3 = Top Conc Pier	2.3	372.4	+

3+85

W-0.2 = Sly Lath Fence			+

4+0

-10 =	3.5	371.2	
W = Lath Fence	3.6	371.1	+

374.66

℄	3.8	370.9	
E	3.9	370.8	
+0.5 = Wly Board House			+

4+12

W+0.1 = Nly Lath Fence			+

4+21

W+0.3 = Ely 1.5 Conc Walk	3.11	371.55	✓

4+36

-0.2 = Wly Board House			+
E	3.7	371.0	
℄	3.5	371.2	
+7.2 = Nly + Ely 1.5 Conc Walk	3.20	371.46	✓
W	3.2	371.5	

4+50.43 = SL Meade

W Top Cb	3.47	371.19
Gutter on Paving	3.78	370.88
℄ " "	4.16	370.50
Gutter " "	3.94	370.72
E Top Cb	3.85	370.81

4+64.43 = SCb Meade

E on Paving		4.45	370.21
℄ " "		4.40	370.26
W " "		4.27	370.39
TP	4.20 374.47	4.39	370.27
BM		4.87	369.60

NW BP Meade +39.74

Field Book 36.9.65 Office → 369.75

BM	4.83	372.43		369.60	NW BP Meador 369.57
BM			4.74	367.69	SW BP Elcan 369.57 367.72

139.88 W 7 E

139.92 " F

17

ENGINEERING DEPARTMENT,
CITY OF EAST SAN DIEGO,
CALIFORNIA.

62
34
59

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44 2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.