

MINING  
TRANSIT BOOK  
363

F.B.570



# KEUFFEL & ESSER CO.

DRAWING MATERIALS  
AND  
SURVEYING INSTRUMENTS.  
NEW YORK.

CHICAGO. SAN FRANCISCO. ST. LOUIS.

## TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.  
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.  
FOR SINGLE TRACK EXCAVATION.

"Copyright, 1895, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

*Alignment  
East of Fairmount*

OFFICE OF THE CITY ENGINEER  
EAST SAN DIEGO CAL.

*Indexed to date Feb 26, 1918.  
Card " " " Mar 21, 1918*

*298  
143*



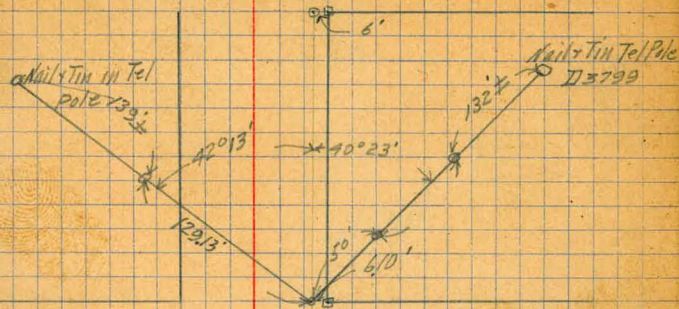
Index	Page
Alignment of Colonial	1-2 ✓
Diagram of Euclid	3-4
Alignment of Highland	5-6 ✓
Diagram of Chamoune	8 ✓
Alignment University	7-9 ✓
" Cabrillo	11-12 ✓



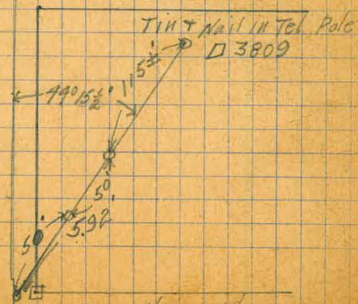
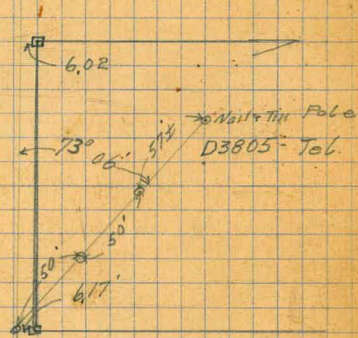
Sept 11-12-1914

Ford  
grat  
Krudtson.

1



4444  
Colonia 1





125

125'

Dwight

Howard

2

125.13 20 125 60'

127.22 20 125

127.40 20 125

129.30 20' 125 60'

124.70 125' 70'

126.45 125'

595  
Tin + Nail Elec Pole

61° 15'

50' 50' 601

598'

125' N 10' DMIX

DMIX 125' 10' 10'  
25' Lots  
5.97'

75.60 South to R.R.

Myrtle Clark

Center

Chatham

601.3  
600  
600  
600

Colonial

127.40  
127.40  
127.40

129.30  
129.30  
129.30

124.70  
124.70  
124.70

126.45  
126.45  
126.45

50' 50' 50' 50'

50' 50' 50' 50'

50' 50' 50' 50'

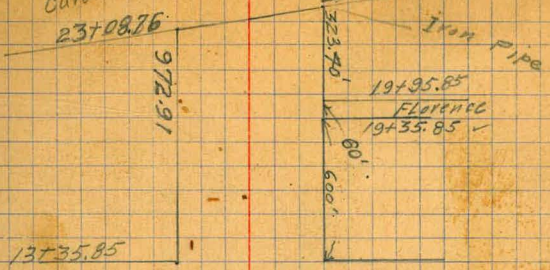
50' 50' 50' 50'

50' 50' 50' 50'

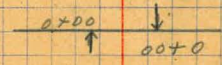


Curve 16' out -  
23+08.76

FL. Curve 10' out - Sh. 2' in  
Curve 16' out - Sh. 2' in  
23+19.25 chains 23+19.25 30K



Euclid  
80'  
Orange

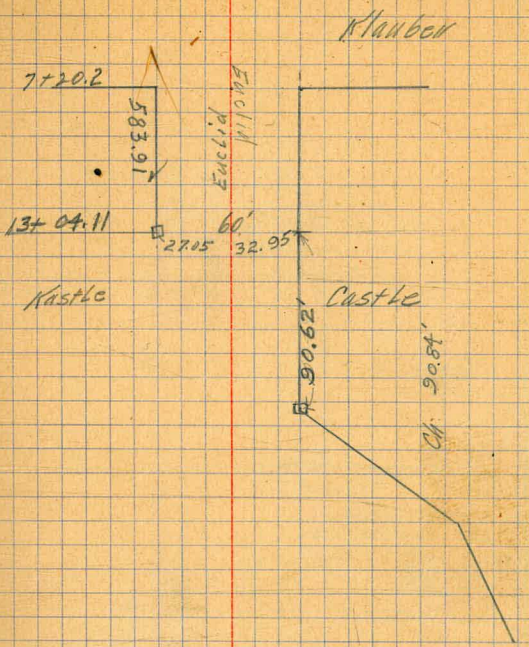


Anna

University

Klauber







University  
 Oct 21-1914  
 Ford  
 Gray  
 Knutson  
 2x2 Hub on 6' offset line  
 125' 20' 125'

0+40  
 125 20 125

65'  
 6.0

6+40

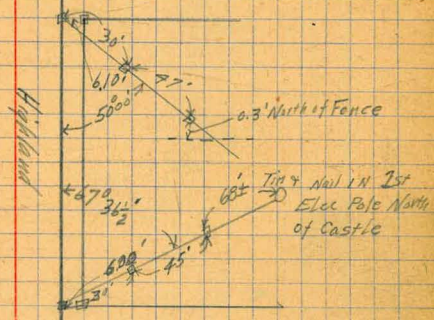
65'

8.0

Klumber

7+20

536.53'



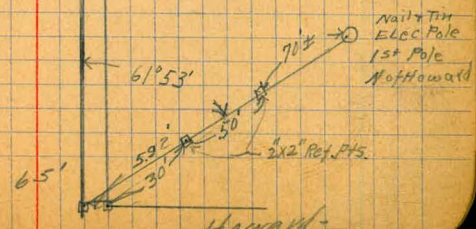
13+16.33

1.08

Castle

17+96.39

600.52'



19+96.85

Howard

Pt. Referenced Here is on a line 6' West of EL + 0.8' S of S. Line

Pt. Ref is on New 6' Line 6' West of 0.11' N of NE Howard + Highland



Pt Ref levels on a line 6' W of E.P.L. & 0.42' N of NE <sup>Corner</sup> ~~Highway~~

Pt Ref Here is on a line 6' W of E.P.L. & 38' N of N.E. Corner

20+76.85

1.5109

26+78.15

80'

27+58.15

1.6091

33+58.15

80'

34+38.15

1.6009

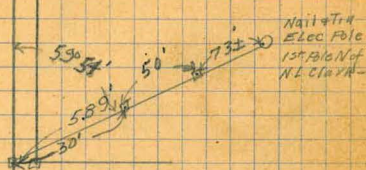
125 20 125  
40+38.15

80'

Oct 21-1914  
Ford  
Hudson  
Gray 6

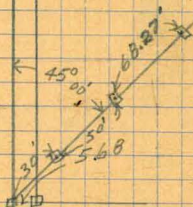
Clifford Line  
Howard

Highland



Clark

Myrtle



Thorn  
Center

South Boundary of Dist

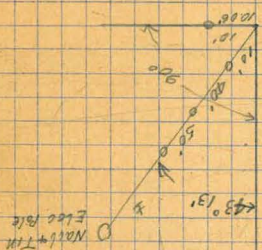
South Boundary Dist

65'

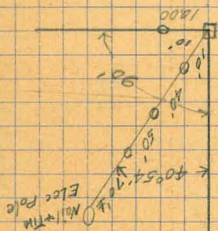
125-20-125  
Chatham



46th. Mentone



Mentone



51111

University

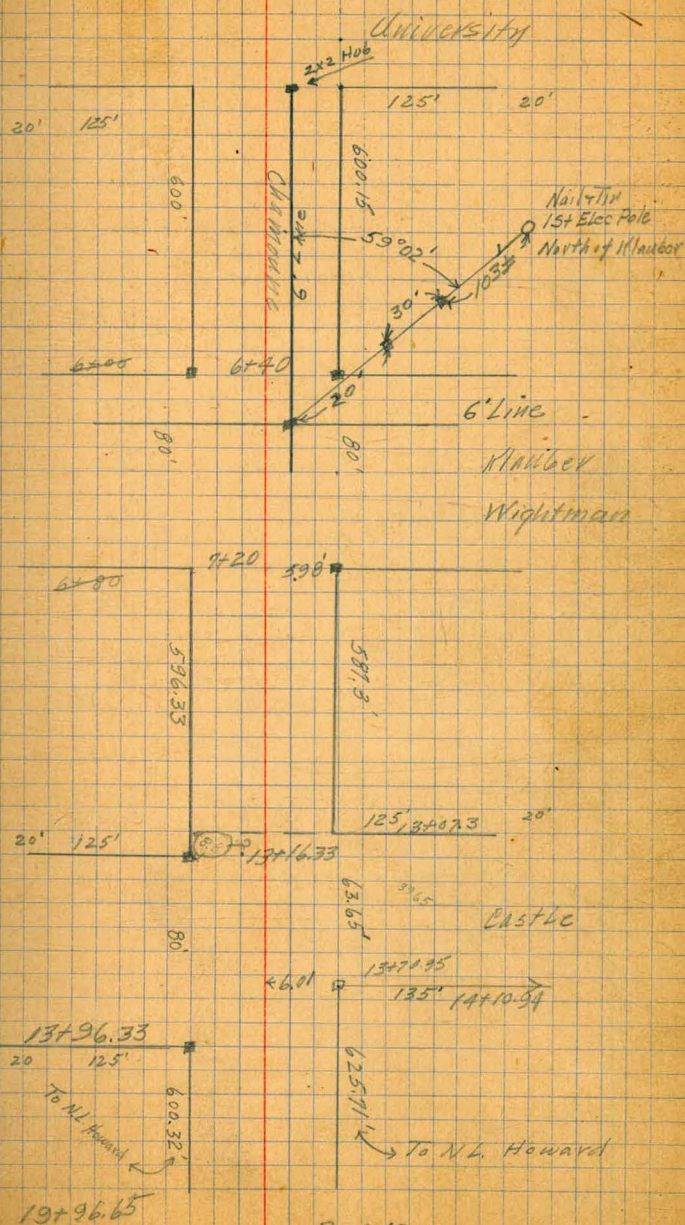
How East





Chamaine

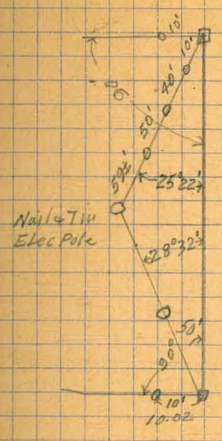
8



See Page 10-



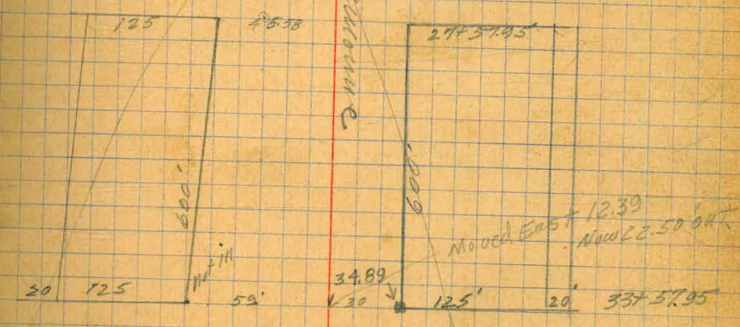
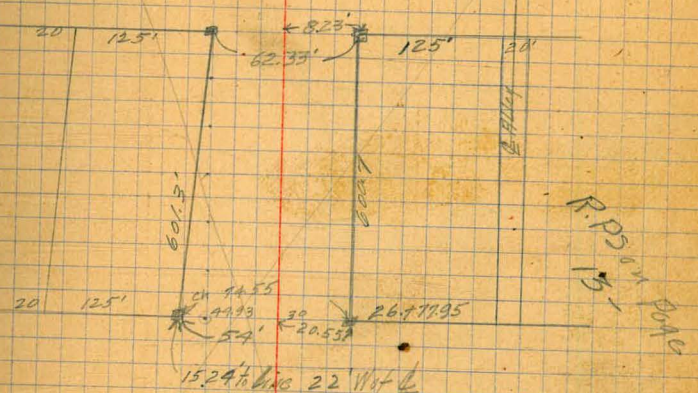
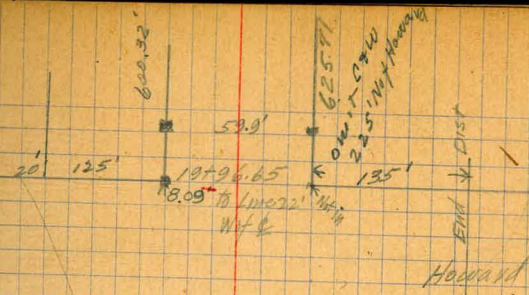
Euclid



University Ave

Stella





Howard

RPSON BOAC  
15-

CLARK  
Myrtle

Center



University

11

125° 20' 125° 60' 125° 20' 125°

500' 600' 250' 125° 20' 125°

125° 20' 125°

8400' 9450' 1180'

125° 20' 125° 125° 20' 125°

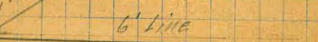
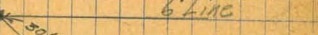
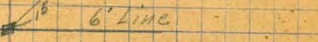
125° 20' 125°

125° 20' 125°

125° 20' 125° 125° 20' 125°

ASTA

COLLINA



This pt is 60' North of 6' Line

Nails in 11 1st Edge Pole of Road

Nails in 11 1st Edge Pole of Road

Howard



Ford Hill  
April 1913

Howard

12

125° 20' 125'

125° 20' 125'

6013

6013

125° 20' 125'

125° 20' 125'

591'

45 M

Myrtle

Clark

125° 20' 125'

125° 20' 125'

6' Line

NE Environment  
+ control etc

600'

Cabinda

Mail 4 T.M. II  
1st Electric Wks  
of Center

Mail 4 T.M. II  
1st Electric Wks  
of Center

125° 21' 125'

125° 20' 125'

6' Line

80'

Carrick

125° 20' 125'

125° 20' 125'

95'

6' Line

6' Line

6' Line

6' Line

6' Line

6' Line

6' Line

6' Line

6' Line

6' Line

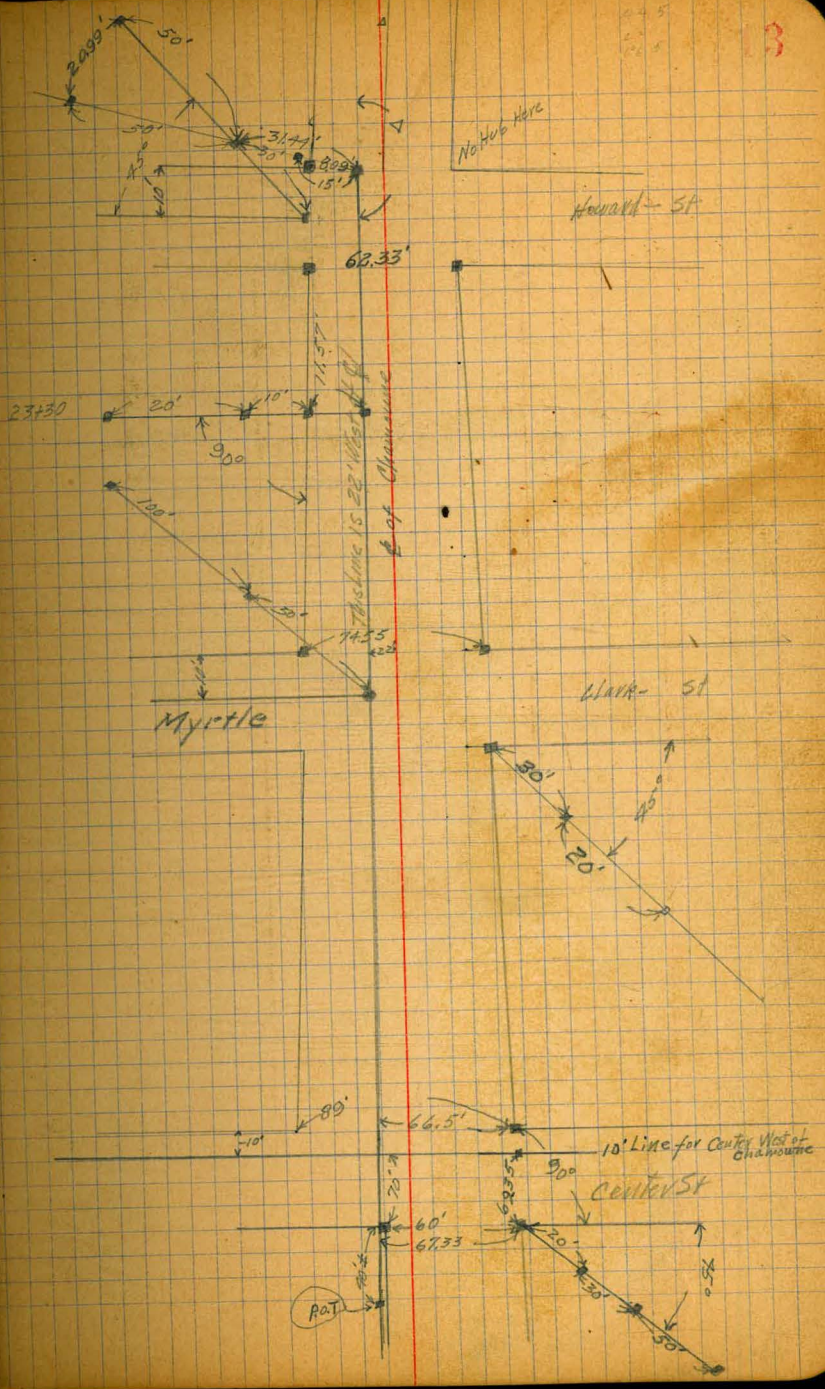
6' Line

6' Line

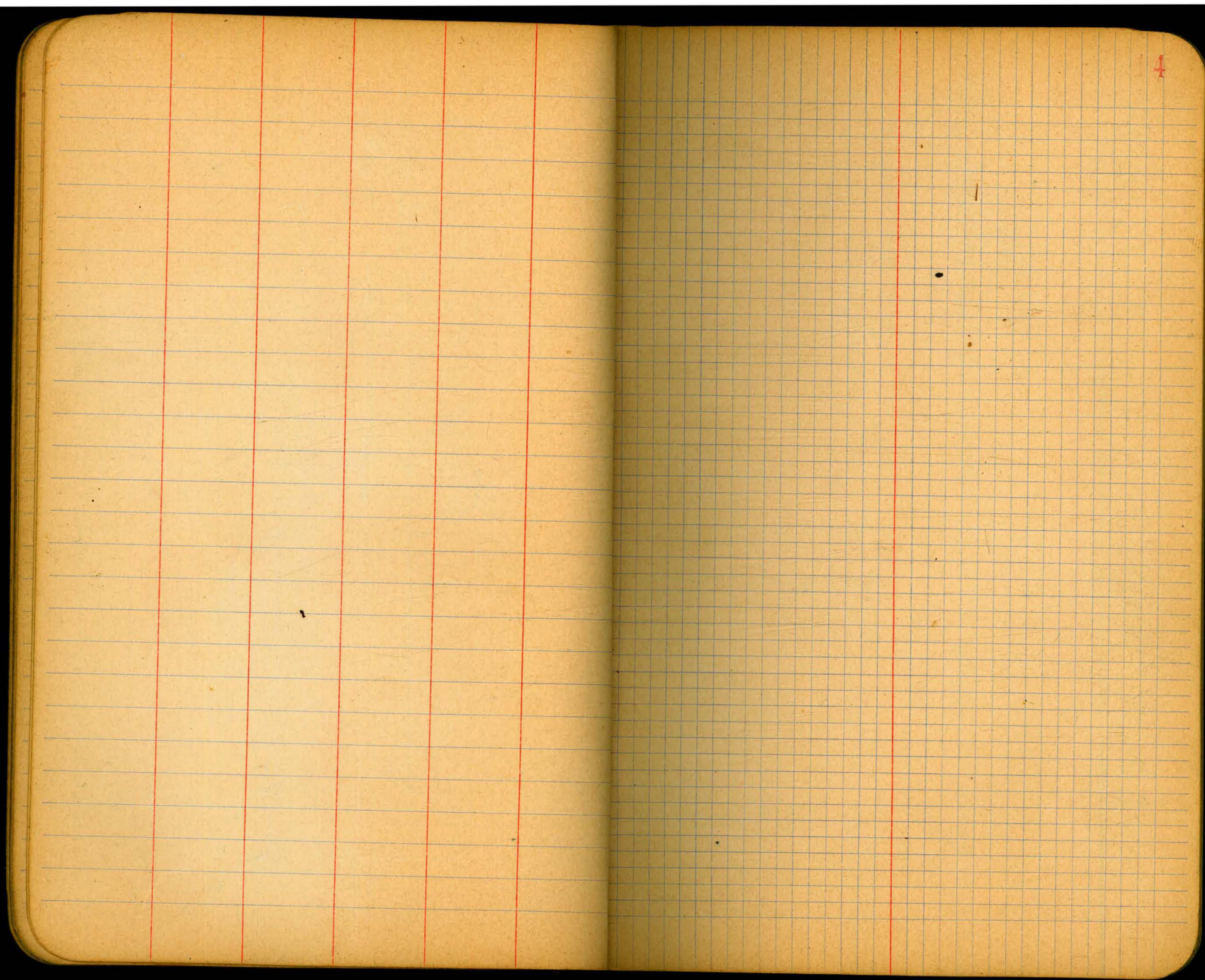
6' Line

Chatworth







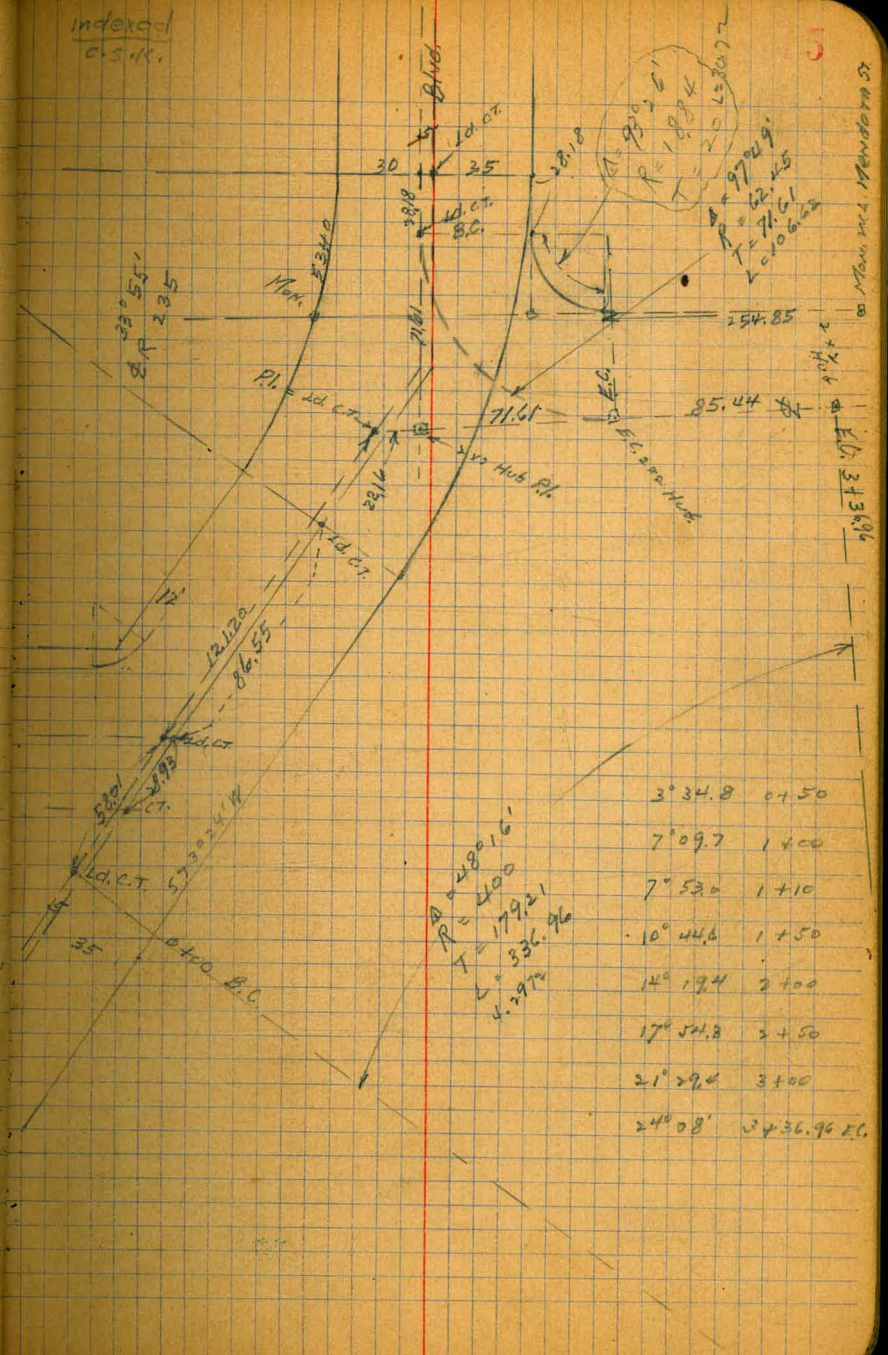
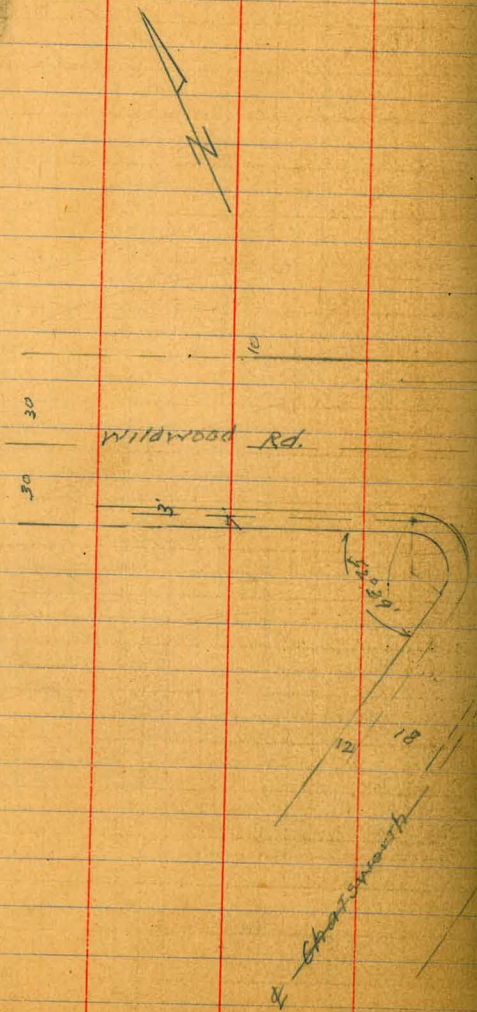




Lowell St. Ext. 80' wide  
 Chatsworth to Plum  
 Via S.L. Pueblo Lot 200  
 Sec T10 E7. BK. 26 P 44

Moore  
 1-30-39

indexed  
 C.S.K.

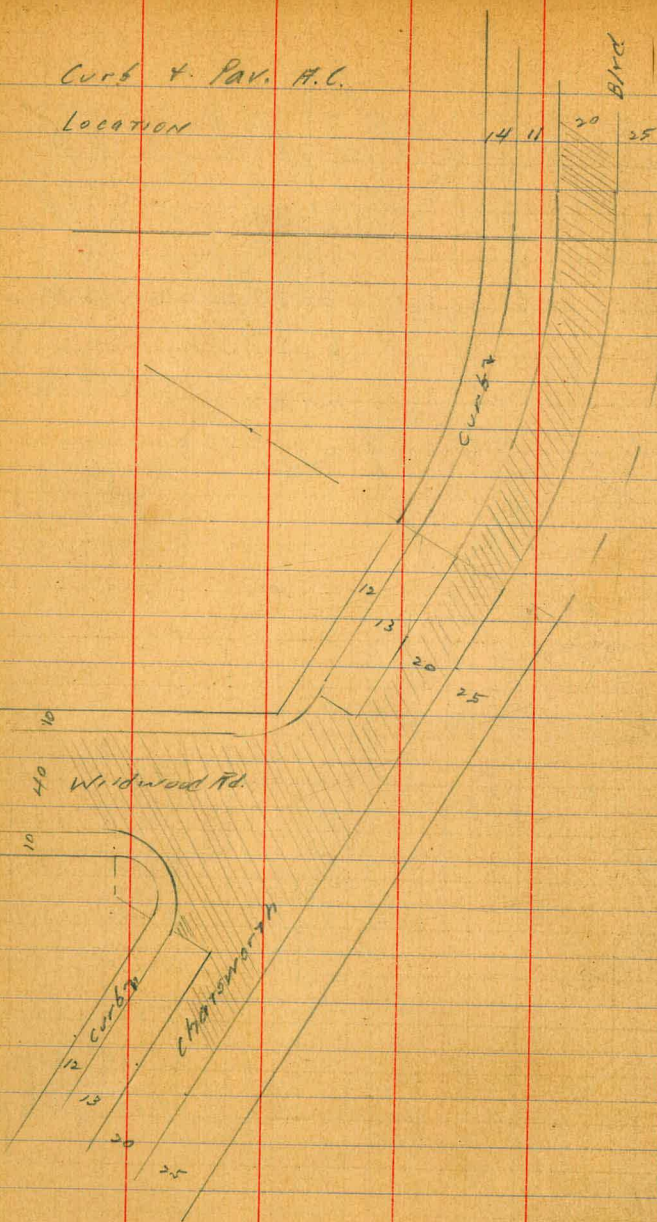


3436.96  
 3436.96



Curb & Pav. H.C.

Location



WIN CAPISTRANO 7

LOWELL ST. EXT.

8+19.46

7+69.51 BELT

67° 52'

6+95.80

PROP 18" CURB

MON

253.33

MON

MENDOTA ST.

R=119.44

R=15.55

MON

M. 250.50

N. 58.56

M. 250.50

N. 58.56

E.C. 3+36.96

SM PL 300

254.85

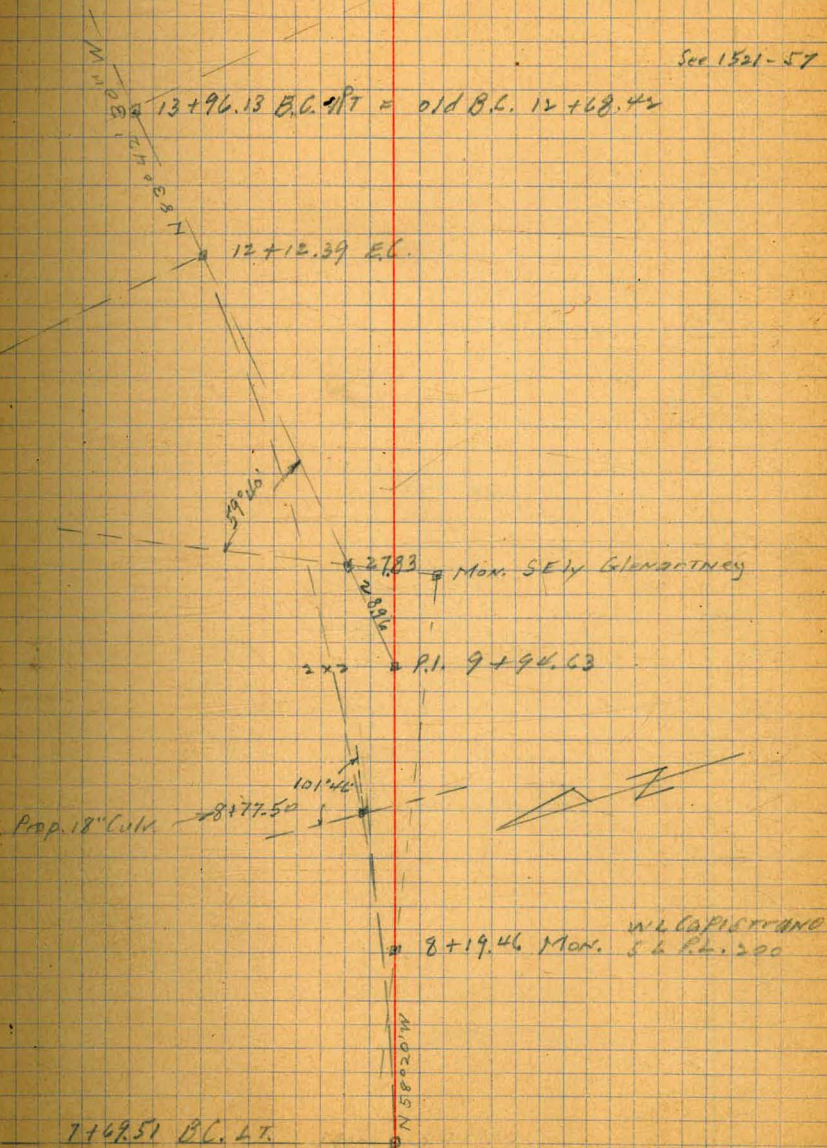
7231-1

176.66

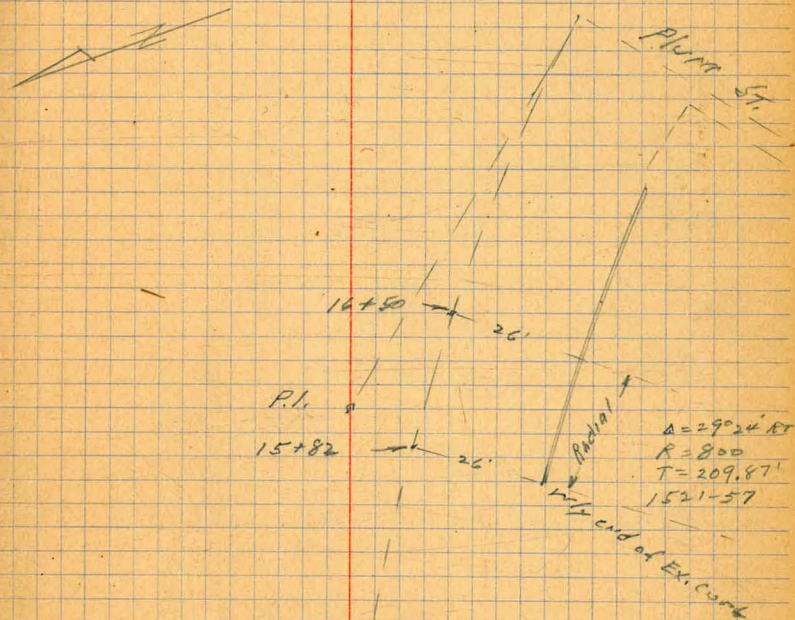




$\Delta = 25^{\circ} 22' 30''$  LT  
 $R = 1000$   
 $T = 225.12$   
 $L = 442.88$







13+96.13 B.C. RT.



Levels on Lowell St. EXT.

Beg. at Chatsworth & Wildwood Rd.

1+50 10°44.6

1+10 E edge Pav. 7°53.0

1+00 7°09.7

0+50 3°34.8 Rt

0+00 B.C. RT. S.W. of E CHATS WORTH

0+00 - 42

T.P. 1.55 174.83 12.69 173.28

T.P. 0.91 185.97 12.98 185.06

C.W.B.P. 0.37 198.04 197.67

Dixon Pl.  
Chatsworth

167.99  
7.24  
13.5  
W. Pav.

165.03  
6.80  
13.5  
E. Pav.

168.3  
6.15

167.8  
7.0  
13.0  
13.0  
13.0  
161.8  
161.8  
161.8  
161.0  
166.3

169.09  
5.74  
3.2

166.1  
0.7  
3.4  
9.2

168.99  
5.84  
3.8  
5.8

169.24  
5.59

169.20  
5.63  
3.0

169.4  
5.2  
11

170.0  
4.8  
13

170.0  
4.8  
13

171.6  
5.2  
11

172.0  
5.8  
10

170.31  
4.57  
2.3  
14.1  
9.2

170.79  
4.04

170.71  
4.2  
1.2  
12  
14.1

170.5  
4.2  
2.0

171.1  
3.5  
2.2

171.0  
3.2  
3.2

174.1  
0.7  
10

171.98  
3.85  
2.5  
14.1  
9.2

172.35  
4.5  
14.6

172.31  
2.3  
1.5

171.8  
3.0  
2.4

172.5  
2.3  
4.0 = E.L.

173.75  
1.05  
1.8  
10.6

173.02  
1.81  
1.8  
9.7  
Pav.

173.79  
1.04  
1.5  
10.6  
10.6

173.98  
0.85

173.89  
0.94  
1.5  
10.6  
10.6

174.83  
7



0 + 53.30

#1

0 + 31.6 E edge Pav

0 + 26.65

equal

4 PARTS #1

0 + 00 B.C. LT @ 5' W of E Chatsworth

B.C. - 2818 = P.C. W of Chatsworth

B.C. - 50

LT. Curve off Chatsworth R 68.45

2400

14° 19.4

1475

17483

$\frac{163.8}{1.0}$  LT  
 $\frac{163.2}{1.0}$   
 $\frac{166.0}{1.0}$   
 $\frac{165.8}{1.0}$   
 $\frac{167.4}{1.0}$   
 $\frac{167.3}{1.0}$  RT

$\frac{165.2}{9.4}$  40  
 $\frac{165.4}{9.4}$  73  
 $\frac{166.12}{8.71}$  4  
 $\frac{166.18}{8.45}$  27 W Pav  
 $\frac{166.32}{8.5}$

$\frac{165.7}{9.1}$  40  
 $\frac{164.9}{9.9}$  35  
 $\frac{164.4}{10.4}$  28  
 $\frac{165.39}{9.4}$  73 edge  
 $\frac{165.09}{9.4}$   
 $\frac{164.73}{10.0}$  81 Pav  
 $\frac{164.33}{10.50}$  94  
 $\frac{165.30}{9.53}$  207 ch

E edge P  
 $\frac{164.29}{10.52}$  15  
 $\frac{163.89}{10.94}$   
 $\frac{163.64}{11.5}$  4.5  
 $\frac{163.27}{11.58}$  94  
 $\frac{164.23}{10.40}$  14.06  
 Wedge Pav

$\frac{163.24}{11.59}$  15  
 $\frac{163.05}{11.78}$   
 $\frac{162.86}{11.97}$  5 W Pav

$\frac{167.1}{7.7}$  40  
 $\frac{166.1}{8.7}$  15  
 $\frac{160.1}{14.7}$   
 $\frac{160.1}{14.7}$   
 $\frac{155.6}{14.2}$  6  
 $\frac{155.7}{14.1}$  9  
 $\frac{159.4}{15.2}$  13  
 $\frac{160.2}{14.3}$  20  
 $\frac{160.3}{14.5}$  40  
 $\frac{160.6}{14.2}$  50

$\frac{167.53}{7.30}$  28  
 $\frac{167.9}{4.9}$  20  
 $\frac{167.1}{7.7}$   
 $\frac{163.6}{11.4}$  10  
 $\frac{162.9}{11.9}$  16  
 $\frac{161.9}{15.7}$  20  
 $\frac{158.1}{15.4}$  25  
 $\frac{163.9}{15.8}$  30  
 $\frac{164.1}{10.7}$  40  
 $\frac{164.2}{10.6}$  50

17483



T.P. 283 157.59 1262 149.76

3+36.96 EC. 24°08'

3+00 21°39.4

T.P. 0.66 162.38 13.11 161.73

2+50 Resume RT Curve 17°54.3 RT

1406.67 EC #4

0+79.95 #3

17483

$\frac{41}{45} \frac{156.3}{12.7}$   $\frac{149.7}{25}$   $\frac{143.8}{10}$   $\frac{143.6}{7}$   $\frac{145.0}{6}$   $\frac{146.3}{10.1}$   $\frac{154.1}{18.3}$   $\frac{160.9}{25}$   
 $\frac{160.6}{1.8}$   $\frac{154.2}{8.2}$   $\frac{149.6}{12.8}$   $\frac{145.4}{17.0}$   $\frac{145.4}{17.0}$   $\frac{145.2}{14.2}$   $\frac{145.2}{11}$   $\frac{157.7}{4.7}$

$\frac{164.7}{10.1}$   $\frac{162.0}{12.8}$   $\frac{160.9}{13.9}$   $\frac{162.38}{11.1}$   $\frac{158.2}{12.6}$   $\frac{153.9}{15}$   $\frac{153.4}{12}$   $\frac{150.6}{18}$   $\frac{150.6}{23}$   $\frac{153.4}{21.4}$   $\frac{158.1}{167}$   $\frac{160.6}{50}$   
 same  
 $\frac{154.1}{14.3}$   $\frac{158.5}{15.9}$   $\frac{158.9}{30}$   
 20.7  
 20.7  
 162.38  
 12483



4+50

T.P. 045 127.41 127.45 127.16

6+00

5+50

T.P. 008 139.81 1286 139.73

5+00

+50

4+00

152.59

$\frac{121.2}{60}$      $\frac{121.6}{30}$      $\frac{123.3}{43}$      $\frac{123.5}{25}$      $\frac{124.2}{55}$   
 2T    S    PT

$\frac{126.6}{60}$      $\frac{128.0}{30}$      $\frac{127.01}{3}$      $\frac{128.6}{11.2}$      $\frac{131.2}{20}$      $\frac{130.4}{45}$

$\frac{131.3}{60}$      $\frac{132.7}{30}$      $\frac{135.4}{4.4}$      $\frac{138.1}{20}$      $\frac{139.2}{60}$

$\frac{132.1}{20.5}$      $\frac{130.1}{22.5}$      $\frac{130.1}{22.5}$      $\frac{132.2}{20.4}$      $\frac{136.6}{16.6}$      $\frac{139.1}{2}$   
 $\frac{136.6}{60}$      $\frac{136.5}{57}$      $\frac{133.4}{24}$      $\frac{133.4}{36}$      $\frac{136.4}{30}$      $\frac{141.1}{11.5}$      $\frac{145.0}{20}$      $\frac{146.2}{6.5}$

$\frac{136.6}{140}$      $\frac{136.5}{101}$      $\frac{133.4}{192}$      $\frac{133.4}{162}$      $\frac{136.4}{15.0}$      $\frac{137.6}{15}$      $\frac{143.1}{9.5}$      $\frac{147.7}{20}$      $\frac{153.4}{108}$

$\frac{142.9}{9.7}$      $\frac{140.4}{12.2}$      $\frac{141.5}{11.1}$      $\frac{145.5}{7.1}$      $\frac{152.3}{0.3}$      $\frac{158.6}{+6.0}$   
 $\frac{142.9}{30}$      $\frac{140.4}{25}$      $\frac{141.5}{13}$      $\frac{145.5}{7.1}$      $\frac{152.3}{18}$      $\frac{158.6}{40}$

152.59



T.P. 473 119.90 12.40 115.17

8+50 2°18.3

8+00 0°52.0

7+69.51 B.C. LT.

7+50

7+25

6+95.8 Prop. Culu. sec A

6+75

127.61

$\frac{118.1}{95}$ 50	$\frac{116.3}{95}$ 25	$\frac{114.6}{13.0}$	$\frac{112.4}{95}$ 25	$\frac{112.4}{95}$ 25
$\frac{119.4}{95}$ 50	$\frac{119.1}{95}$ 30	$\frac{118.3}{95}$	$\frac{117.2}{10.0}$ 40	$\frac{115.2}{12.0}$ 20
$\frac{120.5}{95}$ 50	$\frac{119.9}{95}$ 25	$\frac{119.40}{82}$	$\frac{117.4}{10.0}$ 25	$\frac{110.6}{12.0}$ 60
$\frac{121.0}{95}$ 50	$\frac{120.4}{95}$ 25	$\frac{119.9}{27}$	$\frac{117.2}{10.0}$ 25	$\frac{112.0}{15.0}$ 50
$\frac{122.2}{95}$ 50	$\frac{120.8}{95}$ 30	$\frac{120.0}{7.0}$	$\frac{118.3}{9.5}$ 20	$\frac{113.6}{14.0}$ 40
$\frac{118.0}{9.0}$ 25	$\frac{117.8}{9.8}$ 50	$\frac{116.2}{11.4}$ 25	$\frac{115.84}{11.77}$ 5706	$\frac{109.9}{17.7}$ 50
$\frac{120.2}{24}$ 60	$\frac{117.4}{10.7}$ 41	$\frac{115.0}{9.6}$ 30	$\frac{118.0}{9.0}$	$\frac{113.6}{14.0}$ 65
				$\frac{118.2}{9.2}$ 80

127.61



10+00

6°36.7

T.P. Pl. Hub

1301

13203

0.88

119.02

xxx Hub

9+50

5°10.2

9+00

3°44.3

8+80

8+77.5

Cul. P.O.P 18"

500 &

3°05.0

8+71

8+63

119.90

$$\begin{array}{r} 9.0 \\ 50 \\ \hline 123.0 \end{array}$$

$$\begin{array}{r} 9.8 \\ 55 \\ \hline 122.2 \end{array}$$

$$\begin{array}{r} 120.5 \\ 11.5 \\ \hline \end{array}$$

$$\begin{array}{r} 120.8 \\ 11.2 \\ 55 \\ \hline \end{array}$$

$$\begin{array}{r} 121.2 \\ 10.8 \\ 50 \\ \hline \end{array}$$

$$\begin{array}{r} 120.6 \\ 10.7 \\ 50 \\ \hline \end{array}$$

$$\begin{array}{r} 119.6 \\ 9.8 \\ 55 \\ \hline \end{array}$$

$$\begin{array}{r} 117.4 \\ 2.5 \\ \hline \end{array}$$

$$\begin{array}{r} 115.6 \\ 4.3 \\ 30 \\ \hline \end{array}$$

$$\begin{array}{r} 113.0 \\ 5.9 \\ 20 \\ \hline \end{array}$$

$$\begin{array}{r} 115.4 \\ 1.1 \\ 50 \\ \hline \end{array}$$

$$\begin{array}{r} 117.7 \\ 2.2 \\ 25 \\ \hline \end{array}$$

$$\begin{array}{r} 115.9 \\ 4.0 \\ \hline \end{array}$$

$$\begin{array}{r} 112.4 \\ 2.1 \\ 22 \\ \hline \end{array}$$

$$\begin{array}{r} 108.7 \\ 11.1 \\ 20 \\ \hline \end{array}$$

$$\begin{array}{r} 116.7 \\ 8.2 \\ 50 \\ \hline \end{array}$$

$$\begin{array}{r} 115.1 \\ 4.8 \\ 25 \\ \hline \end{array}$$

$$\begin{array}{r} 113.2 \\ 0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 112.6 \\ 2.8 \\ 10 \\ \hline \end{array}$$

$$\begin{array}{r} 107.4 \\ 12.5 \\ 35 \\ \hline \end{array}$$

$$\begin{array}{r} 104.7 \\ 15.2 \\ 55 \\ \hline \end{array}$$

$$\begin{array}{r} 113.6 \\ 0.3 \\ 52 \\ \hline \end{array}$$

$$\begin{array}{r} 111.3 \\ 8.0 \\ 27 \\ \hline \end{array}$$

$$\begin{array}{r} 113.9 \\ 4.0 \\ 20 \\ \hline \end{array}$$

$$\begin{array}{r} 112.77 \\ 7.3 \\ 57.4 \\ \hline \end{array}$$

$$\begin{array}{r} 112.3 \\ 2.6 \\ 20 \\ \hline \end{array}$$

$$\begin{array}{r} 106.7 \\ 15.1 \\ 40 \\ \hline \end{array}$$

$$\begin{array}{r} 107.8 \\ 12.6 \\ 50 \\ \hline \end{array}$$

$$\begin{array}{r} 104.5 \\ 15.4 \\ 25 \\ \hline \end{array}$$

$$\begin{array}{r} 113.7 \\ 4.1 \\ 50 \\ \hline \end{array}$$

$$\begin{array}{r} 109.7 \\ 8.2 \\ 25 \\ \hline \end{array}$$

$$\begin{array}{r} 107.5 \\ 12.2 \\ \hline \end{array}$$

$$\begin{array}{r} 110.1 \\ 7.8 \\ 35 \\ \hline \end{array}$$

$$\begin{array}{r} 110.3 \\ 9.0 \\ 50 \\ \hline \end{array}$$

$$\begin{array}{r} 111.0 \\ 8.9 \\ 20 \\ \hline \end{array}$$

$$\begin{array}{r} 116.2 \\ 8.2 \\ 50 \\ \hline \end{array}$$

$$\begin{array}{r} 114.35 \\ 1.5 \\ 25 \\ \hline \end{array}$$

$$\begin{array}{r} 113.0 \\ 0.9 \\ \hline \end{array}$$

$$\begin{array}{r} 111.3 \\ 8.0 \\ 25 \\ \hline \end{array}$$

$$\begin{array}{r} 111.6 \\ 8.3 \\ 50 \\ \hline \end{array}$$

$$\begin{array}{r} 112.1 \\ 7.8 \\ 20 \\ \hline \end{array}$$

119.90



1241239 EG

12° 41.25

T.P.

429

146.77

0.2

142.48

12

12° 19.9

750

10054.0

11

9° 28.0

T.P. <sup>old tie</sup> Hub

11.62

142.60

105

130.98

50° LT  
10x60

10+50

8° 03.1

10+30

13203

$$\begin{array}{r} \text{LT} \\ 143.5 \\ \hline 3.3 \\ 40 \end{array}$$

$$\begin{array}{r} 143.2 \\ \hline 3.6 \\ 20 \end{array}$$

$$\begin{array}{r} 142.65 \\ \hline 4.14 \\ \text{Hub} \end{array}$$

$$\begin{array}{r} \text{RT} \\ 142.4 \\ \hline 4.4 \\ 20 \end{array}$$

$$\begin{array}{r} 142.7 \\ \hline 4.6 \\ 20 \end{array}$$

$$\begin{array}{r} 142.9 \\ \hline +0.3 \\ 20 \end{array}$$

$$\begin{array}{r} 143.1 \\ \hline +0.5 \\ 20 \end{array}$$

146.77

$$\begin{array}{r} 142.1 \\ \hline 0.5 \end{array}$$

$$\begin{array}{r} 141.7 \\ \hline 1.9 \\ 20 \end{array}$$

$$\begin{array}{r} 142.2 \\ \hline 1.6 \\ 20 \end{array}$$

$$\begin{array}{r} 140.1 \\ \hline 2.5 \\ 40 \end{array}$$

$$\begin{array}{r} 139.7 \\ \hline 2.4 \\ 20 \end{array}$$

$$\begin{array}{r} 138.6 \\ \hline 4.2 \end{array}$$

$$\begin{array}{r} 138.4 \\ \hline 4.4 \\ 10 \end{array}$$

$$\begin{array}{r} 140.0 \\ \hline 2.5 \\ 20 \end{array}$$

$$\begin{array}{r} 139.9 \\ \hline 1.5 \\ 20 \end{array}$$

$$\begin{array}{r} 137.7 \\ \hline 4.1 \\ 50 \end{array}$$

$$\begin{array}{r} 136.2 \\ \hline 4.5 \\ 50 \end{array}$$

$$\begin{array}{r} 135.2 \\ \hline 7.4 \end{array}$$

$$\begin{array}{r} 134.7 \\ \hline 1.2 \\ 20 \end{array}$$

$$\begin{array}{r} 136.3 \\ \hline 1.3 \\ 50 \end{array}$$

$$\begin{array}{r} 126.0 \\ \hline 4.0 \\ 50 \end{array}$$

$$\begin{array}{r} 127.9 \\ \hline 4.1 \\ 25 \end{array}$$

$$\begin{array}{r} 131.0 \\ \hline 7.6 \\ 15 \end{array}$$

14260

$$\begin{array}{r} 132.0 \\ \hline 0.0 \end{array}$$

$$\begin{array}{r} 133.4 \\ \hline 1.4 \\ 25 \end{array}$$

$$\begin{array}{r} 134.5 \\ \hline 1.5 \\ 50 \end{array}$$

$$\begin{array}{r} 126.4 \\ \hline 5.6 \\ 50 \end{array}$$

$$\begin{array}{r} 125.0 \\ \hline 7.0 \\ 25 \end{array}$$

$$\begin{array}{r} 124.7 \\ \hline 7.3 \end{array}$$

$$\begin{array}{r} 132.0 \\ \hline 0.0 \\ 25 \end{array}$$

$$\begin{array}{r} 132.0 \\ \hline 0.0 \\ 50 \end{array}$$

13203



T.P. 0.51 123.47 12.51 123.16

15 3043.2

14+50 1255.7

1349613 BC.Rt

T.P. 0.99 135.47 12.09 134.68

+50

13

12+50

146.77

$$\begin{array}{r} 100 \\ \hline 40 \end{array} \begin{array}{r} 125.7 \\ \hline 125.7 \end{array}$$

$$\begin{array}{r} 100 \\ \hline 80 \end{array} \begin{array}{r} 125.1 \\ \hline 125.1 \end{array}$$

$$\begin{array}{r} 112 \\ \hline 20 \end{array} \begin{array}{r} 124.5 \\ \hline 124.5 \end{array}$$

$$\begin{array}{r} 115 \\ \hline 20 \end{array} \begin{array}{r} 124.4 \\ \hline 124.4 \end{array}$$

$$\begin{array}{r} 121 \\ \hline 40 \end{array} \begin{array}{r} 123.6 \\ \hline 123.6 \end{array}$$

$$\begin{array}{r} 117 \\ \hline 20 \end{array} \begin{array}{r} 130.0 \\ \hline 130.0 \end{array}$$

$$\begin{array}{r} 112 \\ \hline 20 \end{array} \begin{array}{r} 129.5 \\ \hline 129.5 \end{array}$$

$$\begin{array}{r} 83 \\ \hline 3 \end{array} \begin{array}{r} 127.4 \\ \hline 127.4 \end{array}$$

$$\begin{array}{r} 118 \\ \hline 20 \end{array} \begin{array}{r} 126.9 \\ \hline 126.9 \end{array}$$

$$\begin{array}{r} 117 \\ \hline 20 \end{array} \begin{array}{r} 126.4 \\ \hline 126.4 \end{array}$$

$$\begin{array}{r} 101 \\ \hline 40 \end{array} \begin{array}{r} 135.6 \\ \hline 135.6 \end{array}$$

$$\begin{array}{r} 117 \\ \hline 20 \end{array} \begin{array}{r} 134.6 \\ \hline 134.6 \end{array}$$

$$\begin{array}{r} 113 \\ \hline 43 \end{array} \begin{array}{r} 132.24 \\ \hline 132.24 \end{array}$$

$$\begin{array}{r} 119 \\ \hline 20 \end{array} \begin{array}{r} 130.8 \\ \hline 130.8 \end{array}$$

$$\begin{array}{r} 119 \\ \hline 40 \end{array} \begin{array}{r} 130.8 \\ \hline 130.8 \end{array}$$

$$\begin{array}{r} 135.0 \\ \hline 28 \end{array}$$

$$\begin{array}{r} 136.9 \\ \hline 97 \end{array}$$

$$\begin{array}{r} 135.47 \\ \hline 115 \end{array}$$

$$\begin{array}{r} 135.3 \\ \hline 115 \end{array}$$

$$\begin{array}{r} 135.3 \\ \hline 11.5 \end{array}$$

$$\begin{array}{r} 134.8 \\ \hline 120 \end{array}$$

$$\begin{array}{r} 143.0 \\ \hline 38 \end{array}$$

$$\begin{array}{r} 147.7 \\ \hline 35 \end{array}$$

$$\begin{array}{r} 142.4 \\ \hline 44 \end{array}$$

$$\begin{array}{r} 142.4 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 143.2 \\ \hline 46 \end{array}$$

$$\begin{array}{r} 144.5 \\ \hline 13 \end{array}$$

$$\begin{array}{r} 145.0 \\ \hline 18 \end{array}$$

$$\begin{array}{r} 144.4 \\ \hline 3.4 \end{array}$$

$$\begin{array}{r} 143.8 \\ \hline 19 \end{array}$$

$$\begin{array}{r} 144.3 \\ \hline 17 \end{array}$$

146.77



See AB. 1521-64-65 for Curb E.  
on Ranchitas IMPRINTS

16750

90° 06.5

$$\begin{array}{r} 105.63 \\ 5.14 \\ \hline 26 \\ 06 \end{array}$$

$$\begin{array}{r} 105.04 \\ 6.00 \\ \hline 26 \\ 90T \text{ Par.} \end{array}$$

$$\begin{array}{r} 105.24 \\ 5.80 \\ \hline 26 \\ \text{Par} \end{array}$$

$$\begin{array}{r} 103.74 \\ 7.50 \\ \hline 26 \\ 90T \text{ Par} \end{array}$$

$$\begin{array}{r} 104.43 \\ 6.61 \\ \hline 26 \\ 06 \end{array}$$

T.P.

0.06

111.04

17.69

110.90

$$\begin{array}{r} 112.74 \\ 10.93 \\ \hline 26 \\ 06 \end{array}$$

$$\begin{array}{r} 112.26 \\ 11.41 \\ \hline 26 \\ 90T \end{array}$$

$$\begin{array}{r} 111.77 \\ 11.90 \\ \hline 26 \\ \text{Par} \end{array}$$

$$\begin{array}{r} 111.04 \\ 11.47 \\ \hline 26 \\ \text{Par} \end{array}$$

$$\begin{array}{r} 110.7 \\ 1.80 \\ \hline 26 \\ \text{Par} \end{array}$$

$$\begin{array}{r} 111.32 \\ 1.28 \\ \hline 26 \\ \text{Cf} \end{array}$$

$$\begin{array}{r} 111.0 \\ 1.27 \\ \hline 26 \\ 8.5 \end{array}$$

$$\begin{array}{r} 112.9 \\ 1.03 \\ \hline 26 \\ 00 \end{array}$$

16

7° 19.0

$$\begin{array}{r} 114.07 \\ 9.20 \\ \hline 26 \\ \text{Par} \end{array}$$

$$\begin{array}{r} 113.7 \\ 10.0 \\ \hline 26 \\ \text{Par} \end{array}$$

$$\begin{array}{r} 113.17 \\ 10.50 \\ \hline 26 \\ \text{Par} \end{array}$$

$$\begin{array}{r} 112.7 \\ 11.0 \\ \hline 26 \\ \text{Par} \end{array}$$

$$\begin{array}{r} 113.10 \\ 10.57 \\ \hline 26 \\ 90T \end{array}$$

$$\begin{array}{r} 113.97 \\ 9.70 \\ \hline 26 \\ 06 \end{array}$$

$$\begin{array}{r} 113.7 \\ 100.87 \\ \hline 35 \\ 10 \end{array}$$

$$\begin{array}{r} 115.8 \\ 11.5 \\ \hline 26 \\ 00 \end{array}$$

+ 82

6° 37.1

$$\begin{array}{r} 115.04 \\ 9.63 \\ \hline 26 \\ \text{Par} \end{array}$$

$$\begin{array}{r} 115.06 \\ 8.0 \\ \hline 33 \\ \text{Par} \end{array}$$

$$\begin{array}{r} 114.9 \\ 8.8 \\ \hline 26 \\ 00 \end{array}$$

$$\begin{array}{r} 114.3 \\ 9.4 \\ \hline 26 \\ \text{Par} \end{array}$$

$$\begin{array}{r} 114.3 \\ 9.4 \\ \hline 8 \\ \text{Par} \end{array}$$

$$\begin{array}{r} 116.5 \\ 7.2 \\ \hline 18 \\ \text{Par} \end{array}$$

$$\begin{array}{r} 117.1 \\ 6.0 \\ \hline 26 \\ 00 \end{array}$$

$$\begin{array}{r} 117.1 \\ 6.0 \\ \hline 26 \\ 00 \end{array}$$

15468

See 1531-65  
check to cb.

4.51

119.10

$$\begin{array}{r} 119.13 \\ 0.03 \end{array}$$

$$\begin{array}{r} 117.22 \\ 6.45 \\ \hline 26 \\ \text{Par} \end{array}$$

$$\begin{array}{r} 116.4 \\ 4.9 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 119.5 \\ 4.2 \\ \hline 73 \end{array}$$

$$\begin{array}{r} 119.6 \\ 3.9 \end{array}$$

$$\begin{array}{r} 119.9 \\ 3.8 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 119.1 \\ 4.6 \\ \hline 20 \end{array}$$

15450

5° 31.6

123.67

$$\begin{array}{r} 123.67 \\ 5 \end{array}$$



Proposed opening of Narragansett  
 thru N. Cor. of Glenartney  
 to Macaulay St. 70' wide

Indexed  
 C.S.K.

Macaulay St

52' 20" BK. 36-44' Max.

$\Delta = 43^{\circ} 13' \text{ LT}$   
 $R = 294.86$   
 $T = 116.79$   
 $L = 322.14$

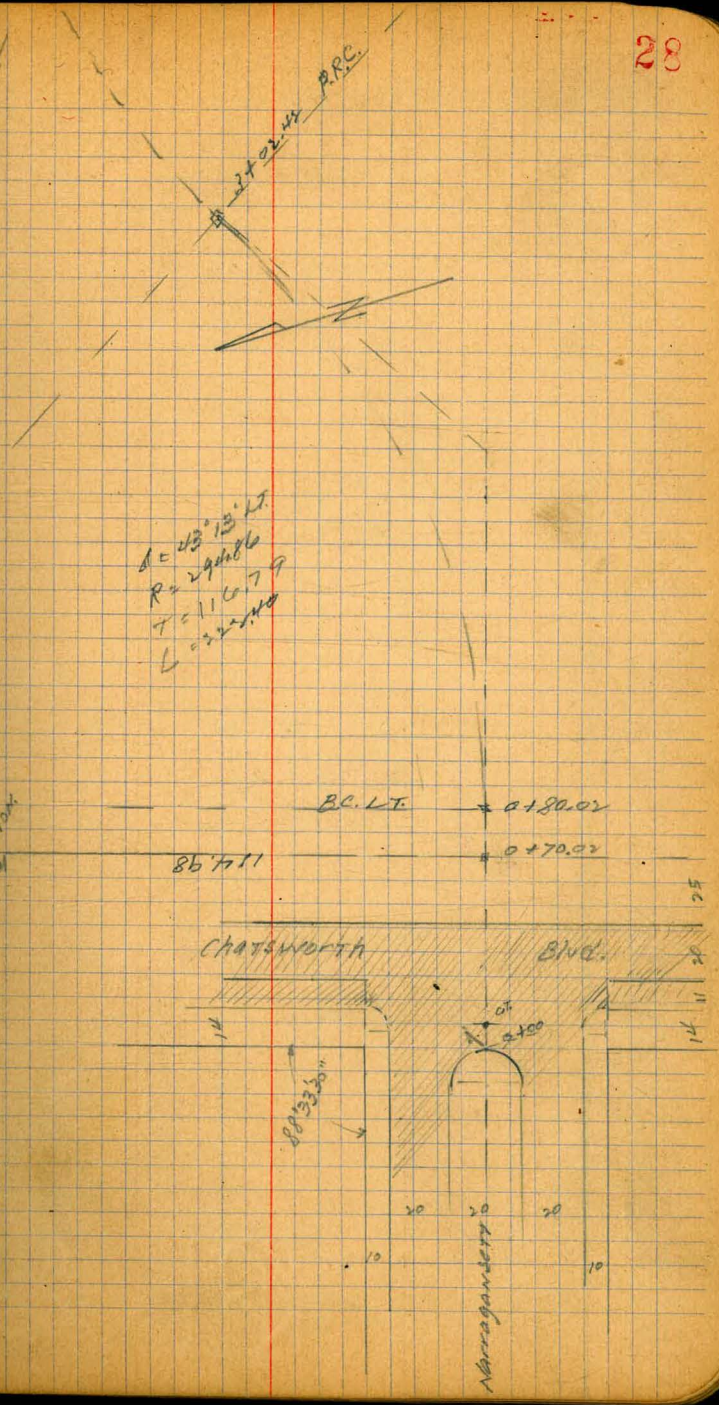
B.C. LT.  $\rightarrow 0+80.02$

86' 7" 11  $\rightarrow 0+70.02$

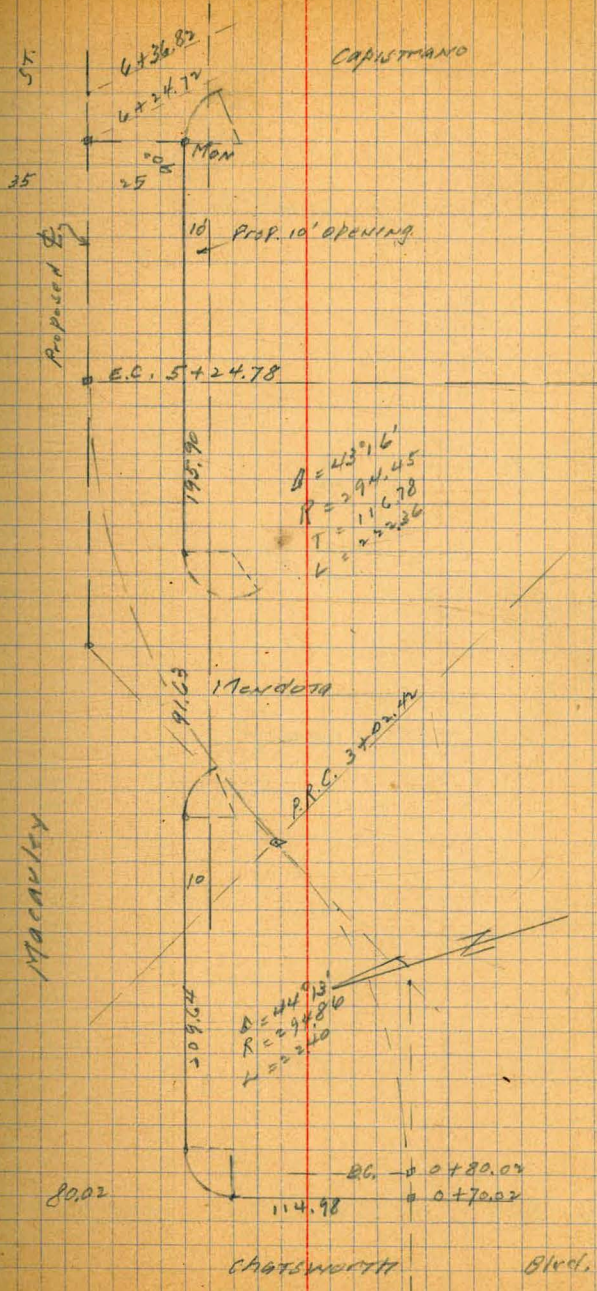
CRATSWORTH BNG.

88' 33.5"

Narragansett









4 + 18.60

Curve of equal parts

3 + 58.01

3 + 02.42 PRC

2 + 46.82

Curve of equal parts

1 + 91.22

1 + 35.62

0 + 80.02

NEBP

5.51

138.70

133.19

See 1521-56 for INT. Sec. Levels

24 8 27  
 $\frac{14.6}{35}$   $\frac{14.5}{33}$   $\frac{13.4}{15}$  11.8  $\frac{10.7}{15}$   $\frac{12.7}{35}$

$\frac{12.9}{35}$   $\frac{11.9}{15}$  11.1  $\frac{10.9}{15}$   $\frac{10.4}{35}$

$\frac{12.0}{35}$   $\frac{11.9}{15}$  11.7  
 11.7  
 11.7  
 $\frac{11.4}{15}$   $\frac{11.1}{35}$

$\frac{12.4}{35}$   $\frac{12.2}{15}$  12.1  $\frac{12.1}{15}$   $\frac{11.8}{35}$

$\frac{11.7}{35}$   $\frac{12.1}{15}$  11.7  $\frac{11.7}{15}$   $\frac{10.3}{35}$

$\frac{10.8}{35}$   $\frac{8.9}{15}$  6.5  $\frac{5.7}{15}$   $\frac{5.5}{35}$

$\frac{6.8}{35}$   $\frac{5.4}{15}$  4.93  
 4.93  
 $\frac{3.4}{15}$   $\frac{2.8}{35}$

138.70  
 2



TF  
 4+29.19  
 10.34  
 136.30  
 1274  
 12596  
 13870

S+24.78  
 EC

S+75

L+24.74 opposite Mon. SL Macouly  
 W.L. Capistrano

L+36.82 W of Capistrano

L+76.82 E of Cap. + NL Macouly

10.7  
 35  
 30  
 11.2  
 5  
 11.2  
 10.8  
 10.4  
 9.7  
 35

9.8  
 9.6  
 9.8  
 9.8  
 9.5  
 9.1  
 9.8  
 9.8  
 9.5  
 9.5

12.7  
 35  
 30  
 8.2  
 8.2  
 8.2  
 8.1  
 2.7  
 8.5  
 8.5

6.1  
 5.8  
 6.2  
 6.2  
 6.1  
 5.7  
 5.7  
 6.1  
 5.7  
 5.5

6.3  
 5.5  
 5.5  
 5.5

4.36  
 5.5  
 5.5  
 5.5

134.30



X sec Dalbergia St.

100' wide  
16' 063  
17' 1/4

Indexed  
C-S-R

Moore  
3-5-39

32

Woden to Thor

Wly. BP. 2.06 22.71 20.65 Woden

COTTONWOOD

0+00 Wly Woden

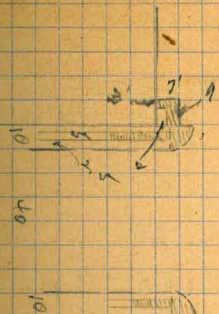
N	8.8	13.9
cb cem	9.16	13.55
907	10.2	12.5
1/4	9.4	13.3
C	9.4	13.3
1/4	9.6	13.1
907	10.1	12.6
cb cem	9.63	13.08
S	9.5	13.2

0+12

S	7.2	15.5
+13	7.1	15.6
cb	9.8	12.9
1/4	9.3	13.4
C	9.1	13.6
1/4	9.4	13.3
cb	9.4	13.1
+6	8.0	14.7
N	7.1	15.6

0+50

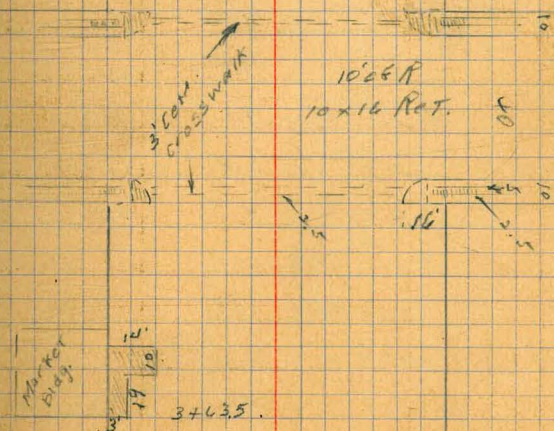
N	6.2	16.5
---	-----	------



10' cb R  
10x12 Ret.

Vista  
graded  
sdm + curb

Dalbergia



graded sdm. + Curbed  
3' cent. x walk

Woden



+10	8.8	16.1
cb	9.0	13.2
1/4	8.1	14.6
c	7.9	14.8
1/4	8.1	14.6
cb	8.7	13.8
+3	6.4	16.3
S	6.8	15.9

1700

S	6.5	16.2
+13	6.0	16.7
cb	8.2	14.5
1/4	7.2	15.5
c	7.0	15.2
1/4	7.0	15.2
+13	7.2	15.5
cb	9.1	13.6
+5	5.6	17.1
N	4.9	17.8

T.P.      4.17      21.19      5.69      17.02

1750

N	4.2	17.0
+14	4.4	16.8
cb	6.7	14.5
+3	5.6	15.6

1/4	5.2	16.0
c	5.2	16.0
1/4	5.2	15.8
cb	6.2	15.0
+3	4.4	16.6
S	4.2	17.0

1766

N-1 3' Cond work      3.20      17.99

1787

S-1 2' Brick +      4.33      16.86

2100

S	4.7	16.5
+13	5.0	16.2
cb	6.5	14.2
+2	5.4	15.7
1/4	5.1	16.1
c	4.9	16.3
1/4	5.1	16.1
+14	5.5	15.7
cb	6.4	14.8
+5	4.4	16.6
N	4.2	17.0

2150

N	4.1	17.1
+13	4.8	16.4
cb	6.5	14.7
+3	5.3	15.9



21.19

1/4	5.0	16.2
0	4.8	16.4
1/4	5.0	16.2
+14	5.5	15.7
06	6.6	14.6
+3	4.6	16.6
S	5.3	15.9
3400		
S	5.4	16.0
+12	4.8	16.4
06	6.6	14.6
+3	5.6	15.6
1/4	5.0	16.2
0	4.7	16.5
1/4	4.8	16.4
+14	5.4	15.8
06	6.4	14.8
+5	4.4	17.0
N	4.5	16.7
3450		
N	4.8	16.4
+13	4.3	16.9
06	6.4	14.6
+3	5.5	15.7
1/4	5.1	16.1
0	4.7	16.5

21.19

34

1/4	5.2	16.0	
+15	5.0	15.6	
06	6.5	14.7	
+3	5.4	16.0	
S	5.2	15.6	
3465.5			
S	Floor El. Cent.	4.85	16.34
+3	Cent.	5.10	16.09
3482.5			
S	Floor "	5.07	16.12
+3	Cent.	5.12	16.07
+14	"	5.27	15.92
3492			
S	Fl. Cent.	5.04	16.15
+14	Cent.	5.14	16.03
3400			
S		5.5	15.7
+14		5.3	15.9
06		6.4	14.8
+3		5.7	15.5
1/4		5.3	15.9
0		4.6	16.6
1/2		5.1	16.1
+14		5.4	15.8
06		6.4	14.8
+5		4.5	16.7
N		5.0	16.2



21.19

4+50

N	4.2	16.6
+13	4.8	16.4
06	6.4	14.8
+3	5.5	15.7
1/2	5.3	15.9
0	5.0	16.2
1/2	5.5	15.7
+15	5.7	15.5
06	6.0	14.6
+3	4.8	16.4
5	5.7	15.5

5+00

5	5.8	15.4
+14	5.5	15.7
06	6.6	14.6
+3	5.8	15.4
1/4	5.5	15.7
0	5.1	16.1
1/4	5.4	15.8
+15	5.7	15.5
06	6.7	14.5
+2	5.4	15.8
N	4.9	16.3

5+32

N	4' cent. wk	4.96	16.23
---	-------------	------	-------

21.19

35

5+50

N	5.3	15.9
+12	5.3	15.9
06	6.4	14.8
+2	5.7	15.5
1/4	5.3	15.8
0	4.8	16.4
1/2	5.2	15.6
+14	5.8	15.4
06	6.5	14.7
+2	5.1	16.1
5	5.9	15.3

5+77

N	+3.5	3' cent. wk	5.12	16.02
---	------	-------------	------	-------

6+00 Ely Vista

5	5.4	15.8	
06	cent	5.63	15.86
907	6.2	15.0	
1/2	5.1	16.1	
0	4.3	16.9	
1/4	5.0	16.2	
907	6.2	15.0	
06	cent	5.64	15.51
5	5.2	16.0	



21.19

Note! Crosswalks laid to grade of old R.R.

Ely VESTA +4 = E 3' Cent. X walk

N gut	6.24	14.95
1/4	5.03	16.16
C	4.22	16.97
1/4	5.02	16.17
S gut	6.05	15.14

E VESTA

S	5.0	15.6
CB	5.7	15.5
1/4	4.9	16.3
C	4.0	16.6
1/4	4.8	16.4
CB	5.1	16.1
N	5.3	15.9

T.P. 7.20 23.27 5.12 16.07

E VESTA +36 = E 3' Cent. X walk

N gut	7.74	15.53
1/4	6.84	16.43
C	6.05	17.22
1/4	6.70	16.57
S gut	7.66	15.61

Parts pulled now

23.27

Wly VESTA = 0+00

S	6.9	16.9
CB	7.18	16.09
gut	7.6	15.7
1/4	4.7	16.6
C	6.2	17.1
1/4	6.8	16.5
gut	7.7	15.6
CB	7.18	16.09
N	7.0	16.3
	0+50	
N	7.0	16.3
CB	6.9	16.8
1/4	7.0	16.3
C	6.4	15.9
1/4	6.6	16.7
CB	7.1	16.2
+3	6.1	17.2
S	6.0	17.3
	1+00	
S	5.1	18.2
+13	5.5	17.8
CB	6.3	16.8
1/4	6.3	17.0
C	6.1	17.2
1/4	6.5	16.8

36



23.27

cb	6.6	16.7
+13	6.5	16.8
N	7.2	16.1
+5	8.2	15.1
	1+50	
-5	7.2	16.1
N	6.4	16.9
+2	5.7	17.6
cb	5.8	17.5
1/4	5.9	17.4
c	5.4	17.9
1/4	5.7	17.6
cb	6.2	17.1
+4	5.0	18.3
S	5.0	18.3
	2+00	
S	4.9	18.4
cb	5.4	17.7
1/4	5.2	18.1
c	5.0	18.3
1/4	5.3	18.0
cb	5.5	17.8
+2	5.1	18.2
N	5.2	18.1
+5	6.4	16.9

23.27

37

	2+50	
N	5.0	18.3
+3	4.4	18.9
+14	4.6	18.7
cb	5.0	18.3
1/4	4.7	18.6
c	4.5	18.8
1/4	5.1	18.2
cb	5.3	18.0
S	5.0	18.3
	2+66.5 E 4.6 Comp. Drive	
S	4.78	18.49
S +14 edge drive	5.06	18.21
cb	5.2	18.1
	3+00	
S	4.6	18.7
cb	5.0	18.3
1/4	4.7	18.6
c	4.1	19.2
1/4	4.1	19.2
cb	4.4	18.9
+2	3.9	19.4
N	3.8	19.5
	3+50	
N	3.2	20.1
+14	3.1	20.2
cb	4.0	19.3



13.27

1/4		4.0	19.3
c		3.6	19.7
1/4		4.4	19.1
cb		4.8	18.5
+N		4.0	19.3
S		4.4	19.1
	4400		
S		4.0	19.3
cb		4.5	18.8
1/4		4.3	19.0
c		3.6	19.7
1/4		3.7	19.6
cb		3.7	19.6
+3		3.0	20.3
N		3.0	20.3
	4+13.5 E 3' cem wk.		
S		3.94	19.35
+12.6		3.96	19.33
	4+31 E 6' cem drive		
S		4.09	19.18
+13		4.21	19.06
	4+50		
N		3.0	20.3
+13		3.1	20.2
cb		3.7	19.6
1/4		3.5	19.8

23.27

38

L		3.8	19.5
1/4		4.7	19.1
cb		4.5	18.8
S		4.3	19.0
	4+53 E 3' cem wk		
S		4.14	19.13
+13		4.27	19.00
	5+00		
S		4.5	18.8
cb		4.7	18.6
1/4		4.3	19.0
c		3.6	19.7
1/4		3.5	19.8
cb		3.6	19.7
+4		3.1	20.2
N		3.2	20.1
	T.P. 5.5 24.80	3.64	19.65
	5+33		
S	E 4' cem. wk	5.05	18.15
	5+50		
N		5.1	19.2
cb		5.0	19.7
1/4		5.3	19.5
c		5.3	19.8
1/4		6.0	18.7
cb		6.2	18.6
S		6.0	18.8



24.80

600 Fly UNA St graded

S		6.4	18.4
cb	Cent	6.75	18.05
gur		7.2	18.6
1/2		6.8	18.0
c		6.6	18.2
1/4		6.6	18.2
gur		6.4	18.4
cb	Cent.	5.82	18.98
N		5.4	19.2

wily UNA = 0100

N		4.9	19.9
cb	Cent.	5.30	19.50
gur		6.0	18.8
1/4		6.1	18.7
c		6.1	18.7
1/2		6.4	18.4
gur		7.0	18.8
cb	Cent.	6.22	18.58
S		6.1	18.7

0 + 50

S		6.0	18.5
cb		6.1	18.7
1/2		5.7	19.1
c		5.4	19.4
1/4		5.4	19.4

24.80

39

cb		5.2	19.6
1/2		4.4	20.2
N		4.7	20.1
N	1+00	4.3	20.5
cb		4.6	20.2
1/4		4.9	19.9
c		5.0	19.5
1/2		5.5	19.3
cb		5.9	18.9
S		5.5	19.3

1 + 50

S		4.9	19.9
cb		5.3	19.6
1/2		5.1	19.7
c		4.8	20.0
1/4		4.2	20.6
cb		4.0	20.8
N		3.3	21.5
S &	14545 3' Cent. wtk	4.50	20.30

2100

N		2.7	22.1
cb		3.7	21.1
1/4		3.7	21.1
c		4.9	19.9
1/2		4.8	20.0



24.80

cb		4.7	20.1
+3		4.1	20.7
S		4.4	20.4
	2+34 E 3' Cem. WK		
N		2.31	22.49
	2+50		
S		5.3	19.5
cb		5.3	19.5
1/4		5.0	19.8
c		5.2	19.6
1/4		3.9	20.9
cb		3.4	21.2
N		2.4	22.2
	3+00		
N		4.4	20.6
+14		4.5	20.3
cb		5.1	19.7
1/4		5.1	19.7
c		6.0	18.8
1/4		6.4	18.6
cb		7.0	17.8
+3		6.4	17.4
S		6.8	17.0
	3+19		
S	E 3' Cem. WK.	7.70	17.60

24.80

40

	3+50		
S		8.7	16.1
+13		8.5	16.3
cb		8.9	15.9
1/4		8.0	16.8
c		7.4	12.4
1/4		7.0	12.8
cb		7.2	12.6
+2		6.3	18.5
N		6.1	18.7
	3+74		
S	E 3' Cem. WK	9.07	15.23
	3+94		
N	E 2' "	7.32	17.48
	4+00		
N		7.7	17.1
+14		7.9	16.9
cb		8.8	16.0
1/4		8.6	16.2
c		8.4	16.2
1/4		8.7	16.1
cb		10.4	14.4
+3		9.7	15.1
S		10.2	14.6
	T.P.	2.00	16.40
		11.06	13.74



1640

4+50

S	2.9	13.5
+14	2.0	14.4
cb	3.0	13.4
1/4	2.4	14.0
c	1.5	14.9
1/4	1.6	14.8
cb	1.9	14.5
+2	1.1	15.3
N	1.2	15.0

5+00

N	2.6	13.8
+14	3.6	13.4
cb	2.1	12.3
1/4	3.5	12.9
c	3.7	13.2
1/4	3.7	12.7
cb	4.6	12.6
+4	3.7	12.7
S	3.4	13.0

5+50

S	5.1	11.3
cb	4.7	11.7
+2	6.0	10.4
1/4	5.3	11.1
c	4.8	11.6

1640

41

1/4	5.1	11.3
+11	5.9	10.5
cb	5.6	10.8
N	4.8	11.6

6+00 Ely Thor St 60' wide 10' c60  
NOT graded

N-5	8.7	8.2
N	8.7	8.2
+10	7.4	9.0
cb	7.9	8.5
1/4	4.7	9.7
c	4.3	10.1
1/4	6.6	9.8
cb	6.8	9.6
+8	6.0	10.4
S	6.3	10.1

E c6.

S	6.9	9.5
cb	7.1	9.3
1/4	6.8	9.6
c	6.4	9.8
1/4	7.2	9.2
cb	8.0	8.4
+6	7.6	8.8
N	8.3	8.1
+5	8.3	8.1



16.40

E Thor

N	9.0	7.4
cb	8.4	8.0
1/4	7.7	8.7
0	7.5	8.9
1/4	7.5	8.9
cb	7.2	9.2
S	7.3	9.1

W cb

S	7.7	8.7
cb	7.5	8.9
1/4	7.1	9.3
0	6.6	9.8
1/4	8.4	8.6
cb	9.0	7.4
N	9.3	7.1

Willy Thor

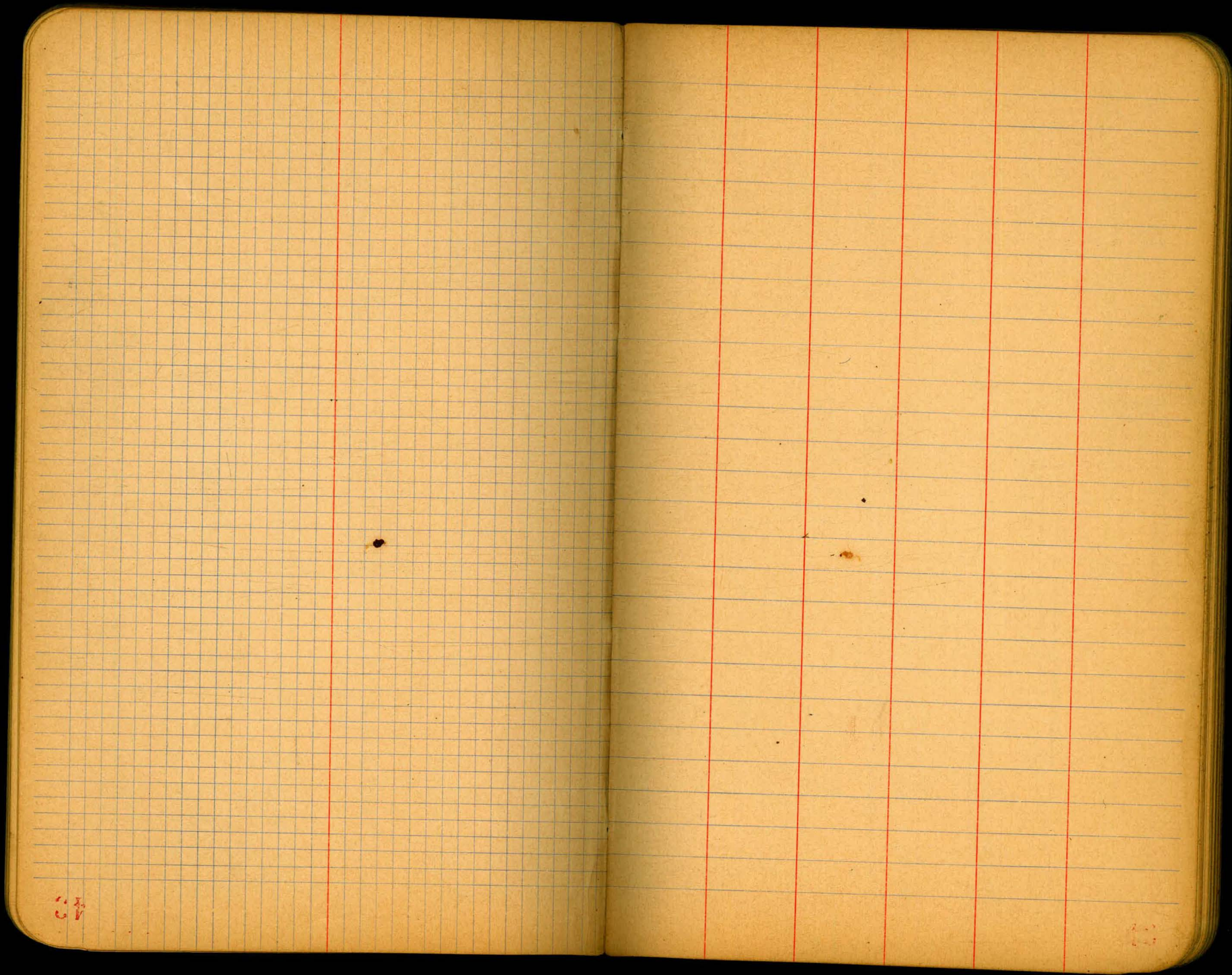
N-5	10.1	6.3
N	10.5	5.9
cb	9.0	6.8
1/4	9.0	7.4
f6	9.0	7.4
+11	6.9	9.5
0	6.5	9.9
+8	6.4	10.0
1/4	8.0	8.4

16.40

42

cb			8.3	8.1
S			7.7	8.7
T.P.	3.65	12.47	7.58	8.82
check to BITBP				
SE. curb			5.38	7.09
Main Thor				





57

58



Indexed  
C.S.K.

X sec alley BIK 26 Ocean Beach  
20' wide Moore  
8-9-29

NWB P	12.98	38.01		25.03	Sum set Saratoga
T.P.	12.64	49.97	0.68	37.33	

0-12 Fly ck of Ebers

N Pav.		4.20		45.77
S		4.06		45.91

0+00 Fly Ebers

S ck		3.21		46.76
S Pav		3.47		46.50
C "		3.94		46.03
N "		3.55		46.42
N ck		3.45		46.52

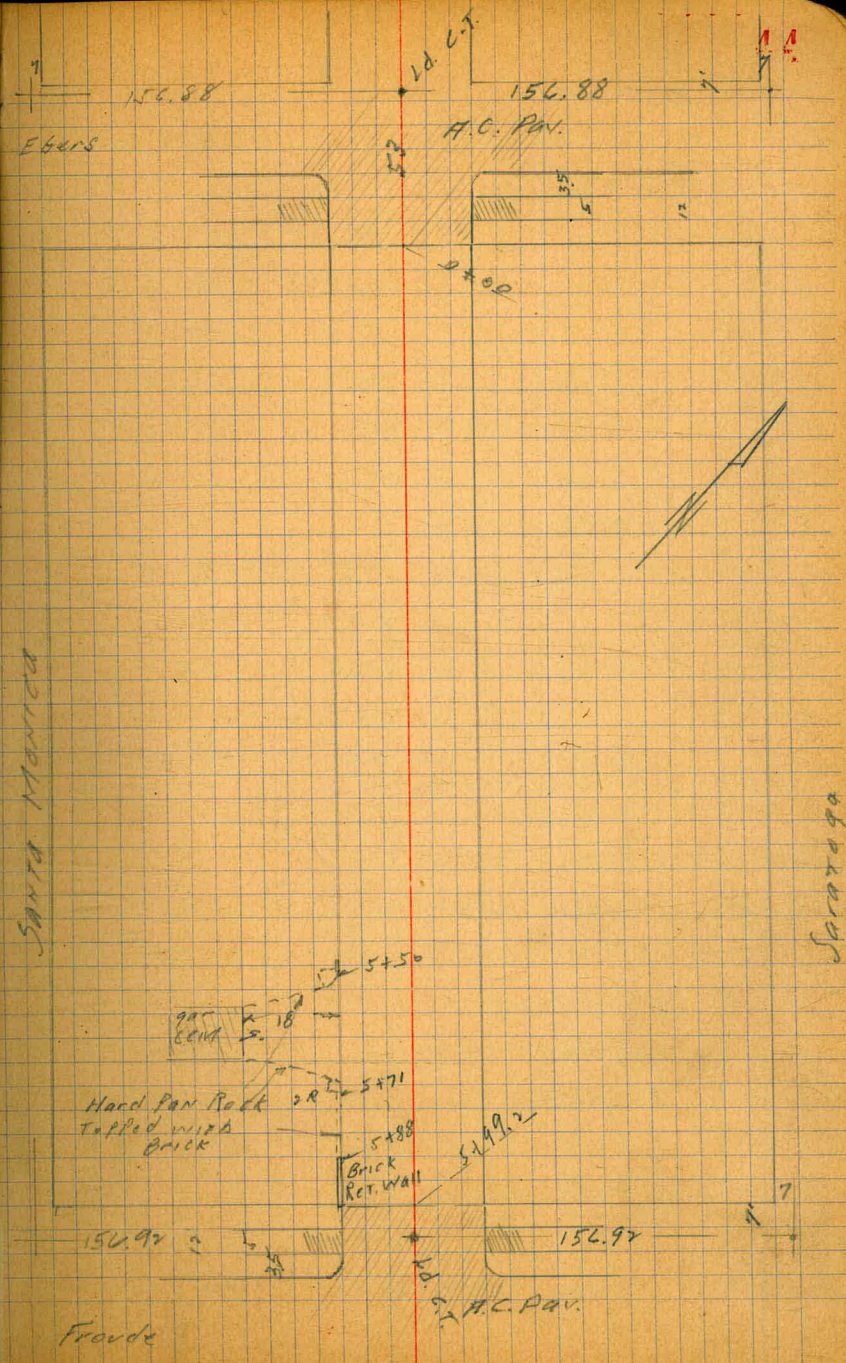
0+01.5

N + 0.7 12" Tel. pole

0+03

N		0.4		49.57
+3		3.7		46.77
C		3.3		46.67
+4		3.2		46.77
S		0.0		49.94

T.P.	12.24	41.35	0.86	49.11
------	-------	-------	------	-------





61.35

0 + 20

S	10.5	50.9
+ 0.7 W. end fence		
+ W	10.6	50.8
+ 4	12.5	48.9
C	12.5	48.9
+ 7	12.2	49.2
+ 8	10.7	50.7
N	10.7	50.7

0 + 50

N	9.5	51.9
+ 2	10.1	51.3
C	10.3	51.1
+ 6	10.2	51.2
+ 7	9.6	51.8
+ 9.3 fence in alley		
S	9.6	51.8

0 + 78

S + 0.8 14" Power Pole

0 + 85

S + 0.4 E end fence

0 + 94

- 3 Sin. 8' gar. cem cl.	7.70	53.65
S	8.00	53.35
+ 0.8. edge cem. apron	8.05	53.30
C	8.1	53.3
N	8.0	53.4

61.35

0 + 96

N	7.9	53.5
- 3.5 Sin. gar. dirt	7.8	53.6

+ 54

N + 0.5 Tel Pole 12" di.

+ 54

N	4.7	56.7
C	5.0	56.4
+ 4	5.0	56.4
S	4.2	57.2
+ 8 Sin. 8' gar. cem. fl.	4.03	57.32

2 + 00

S	2.2	59.2
---	-----	------

+ 0.7 14" Power Pole

C	2.7	58.7
+ 9	2.6	58.8
N	2.0	59.4

T.P. 12.54 73.79 0.10 61.25

mail in  
Pole  
2 + 00

2 + 50

N fence on in alley	11.6	62.2
+ W	12.6	61.2
C	12.7	61.1
S	12.5	61.3
3 + 00		
S	9.2	64.6



73.79

C	SMH Rim	9.59	64.20
+8		9.5	64.3
+9.1	fence in alley		
N		8.9	64.9
	3+05		
N	+ 1.1 12" Tel Pole		
	3+32		
N		7.3	66.5
+0.4	fence		
+2		8.0	65.8
C		8.0	65.8
S		8.1	65.7
+5	Sid. gar dirt fl.	8.2	65.6
	3+41		
S	+ 0.4 14" Pow. Pole		
	3+50		
S		6.8	67.0
C		6.9	66.9
+7		6.7	67.1
+8.5	N edge Cem apron	6.9	67.60
+9.7	" " gar " fl	5.82	67.97
	3+59		
N		5.76	68.03
+1.5	Cem apron	5.98	67.81

73.79

46

		3+65		
N	N edge gar. Cem fl	5.67	68.12	LINE
C		5.9	67.9	
S	E Sid. gar P. fl.	6.1	67.7	
	3+89			
N	0.5 2' Cem. Walk	2.51	70.28	
	H400			
S	fence 0.3 in alley	2.6	71.2	
+2		3.1	70.7	
C		3.0	70.8	
N		2.8	71.0	
T.P.	12.57 86.10	0.26	73.53	
	4+35			
-2.8	gar dirt	12.5	73.6	8' wide
N		12.4	73.7	
C		12.6	73.5	
+8		12.4	73.7	
+9.8	<sup>last</sup> fence	12.1	74.0	
	4+45			
S		11.1	75.0	
0.8	lath fence			
+2		11.6	74.5	
C		11.6	74.5	
N		11.0	75.1	
+2.6	Sid. gar dirt fl.		75.1	



86.10

4+69

S 1" Pow. Pole on Line

4+83

N 11.12" Tel Pole

4+94

-23 Sin gar comp 7.17 78.93 8' wide

N 7.2 78.9

C 7.1 79.0

S 7.2 78.9

5+18

S 4.9 81.2

C 4.9 81.2

N 4.1 82.0

+2 Sin gar dirt 4.0 82.1

5+29

N &amp; 10' Bd. Shed 04 in alley

5+51

N 1.3 84.8

C 1.4 84.5

S 1.2 84.9

+04 Top wall 0.6 85.5

T.P. 11.10 96.78 0.42 85.68

96.78

47

5+62

-18 BENT Cor. Comp 10.80 85.98

-17 ~~E~~ Cor. Apron 10.80 85.98

S 11.2 85.6

C 11.2 85.6

N 10.9 85.9

+5 10.9 85.9

5+71

N 9.8 87.0

C 10.2 86.6

S 10.0 86.8

+0.2 Top wall 9.29 87.49

5+88

S Top Brick Ret wall 4.13 92.65

S 6.3 90.5

C 6.7 90.1

N 6.6 90.2

5+94

N 5.5 91.3

C 5.5 91.3

S 5.0 91.8

S Top wall 4.20 92.58

5+99.2 - Wly Line Froude

Scb 4.20 92.52

S Pav 4.85 91.93

C " 5.08 91.70

N " 5.09 91.69

N cb 4.57 92.21



## 4' E of W L Froude

N	cb	4.58	92.20
N	PAV	4.88	91.90
E	"	4.70	92.08
S	"	4.59	92.19
S	cb	4.22	92.56

## 12' E of " " W L Froude

S	PAV	4.86	91.92
N	"	5.18	91.60

Top cb. Sw Froude 4  
 Saratoga 4.81 89.97 90.00 Profile Grade  
 W L Froude 4  
 St Saratoga



X Sec Curlew  
 Laurel City ✓  
 614 154.21 146.07

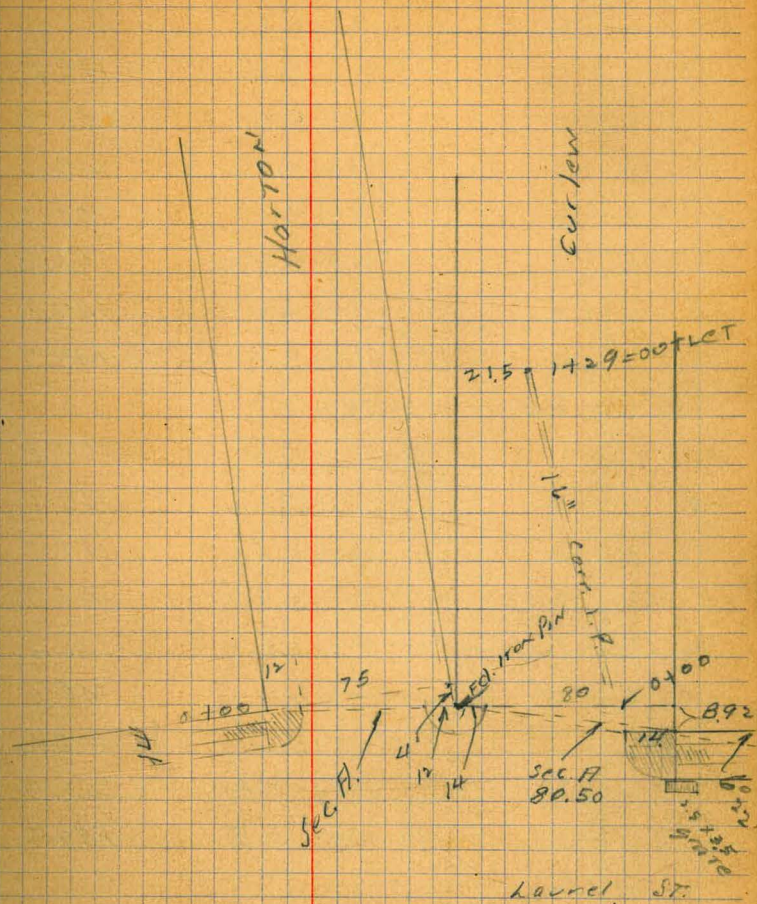
80' wide  
 14' curbs  
 13' 1/2

Sec A

F		2.1	150.1
+4		4.0	148.2
cb	TOP cb	4.18	148.03
gut	PAR	4.78	147.43
1/2	"	4.61	147.60
C	"	4.61	147.60
1/2	"	4.93	147.28
gut	"	5.41	146.60
cb	TOP RET.	5.13	147.08
W	IRON PIN	5.0	147.2
	0 + 00		
W	IRON PIN	5.0	147.2
cb		5.1	147.1
1/2		4.9	147.3
C		4.5	147.7
1/2		4.5	147.7
cb		4.4	147.8
+9		4.0	148.2
F		2.0	150.2
+8	TOP BANK	+2.4	154.6
	0 + 50		
-5		+6.0	158.2

Reduced Plot 2-21-90  
 CPH

INDEXED  
 EFB





152.21 ✓

	0+50		
E		1.5	150.7
+ 4		4.0	148.2
cb		4.4	148.0
1/2		4.1	148.1
c		4.1	148.1
1/2		4.0	148.2
cb		4.4	147.8
W		4.5	147.7
	1+00		
W		5.7	147.0
cb		5.1	147.1
1/2		3.5	148.7
c		3.5	148.7
1/2		3.7	148.5
cb		3.2	148.6
+ 4		3.6	148.6
E		+ 3.8	156.0
+ 5		+ 5.5	157.7
	1+10		
- 5		+ 2.0	154.2
E		+ 1.0	153.2
cb		1.4	150.8
1/2		3.3	148.9
c		2.4	149.6
1/2		3.2	149.0

152.21

50

cb		2.8	149.4
W		2.8	149.4
	1+20		
W		4.5	147.7
cb		4.3	147.9
1/2		4.9	147.3
c		4.4	147.8
1/2		4.7	147.5
cb		4.1	147.1
E		0.8	151.4
	1+29		
E		4.1	148.1
cb		5.6	146.6
1/2		5.6	146.6
c		7.4	144.8
1/2		9.2	143.0
+ 3	Bottom ditch	24.1	128.1
+ 5.5	Fl. 14" outlet	11.57	140.64
+ 9	Bottom ditch	24.0	128.2
cb		9.4	142.8
W		9.8	142.4
	1+40		
- 10		17.9	134.3
W		17.1	135.1
+ 12		16.4	135.8
cb		25.4	126.8



1740

152.21

51

cb + 9

17.1

135.1

1/4

14.7

137.5

c

13.2

139.0

1/4

10.2

142.0

cb

8.4

143.8

F

7.2

145.0

+ 10

5.8

146.4



Sec HORTON

75' wide  
12' cbs  
12.75 1/4

Laurel nly	152.21	
Sec H =		
E <sup>s</sup> Iron pin	5.0	147.2
cb Top curb	5.13	147.08
gut Pav	5.78	146.43
1/4 "	5.74	146.49
" "	5.77	146.44
1/4 "	6.08	146.13
gut "	6.62	145.59
cb Top	6.20	146.01
W	5.9	146.3
0 + 50		
W	5.8	146.4
cb	5.3	146.9
1/4	5.2	147.0
c	5.3	146.9
1/4	5.1	147.1
cb	4.8	147.4
E	4.5	147.7
1 + 00		
E	4.4	147.8
cb	5.4	146.8
1/4	5.3	146.9
"	5.8	146.4
1/4	6.9	145.3

Reduced to Plot 2-21-40  
C.B.H.

INDEXED  
EPB

cb	7.3	144.9
W	7.3	144.9
1 + 17		
W & 3' Con. walk	10.06	142.15
1 + 25		
W	10.9	141.3
cb	10.6	141.6
1/4	9.4	142.8
c	8.8	143.4
1/4	6.1	146.1
+ 6	6.2	146.0
cb	8.4	143.6
E	9.4	142.8
+ 10	9.0	143.2
1 + 35		
- 10	13.5	138.7
E	13.0	139.2
cb	12.0	140.2
+ 7	9.3	142.9
1/4	9.7	142.5
+ 8	12.4	139.8
c	16.7	135.5
+ 7	13.4	138.8
1/4	12.5	139.7
+ 4 pepper tree		
cb	12.4	139.8
W	12.3	139.9



15221

1750

W	17.0	135.2
cb	17.7	134.5
1/2	21.5	130.7
c	22.2	130.0
1/2	21.0	131.2
cb	22.4	129.8
F	23.2	129.0
+10	24.2	128.0







353.79

0+25			
W	3.2	350.6	
C	3.7	350.1	
E	3.5	350.3	
0+40			
E	3.7	350.1	
C	3.7	350.1	
W & Cem. apron	3.12	350.67	4' wide
+ 2.8 Six gar. Cem	2.91	350.88	
0+47			
E + 0.2 & Cem apron	3.74	350.05	
E - 2.7 Six gar. Cem	3.68	350.11	
0+71 W + 0.7	12" P.P.		
0+80			
- 5	4.2	349.6	
W	4.2	349.6	
+ 3	3.4	350.4	
C	3.7	350.1	
E	3.9	349.9	
+ 3 Six gar. Cem.	3.63	349.96	
1+00			
- 5	4.6	349.2	
E	4.1	349.7	
C	4.2	349.6	
W	4.2	349.6	
+ 5	4.3	349.5	

353.79

55

1+10			
W - 2 Cem. apron	4.10	349.69	
W - 6 Six gar. Cem	3.96	349.83	
1+50			
W	4.0	349.8	
C	4.0	349.8	
E big fence	3.8	350.0	on line
1+84 end above fence			
1+90			
E - 3 Six gar dirt	3.6	350.2	
2+00			
E	3.6	350.2	
C	3.3	350.5	
W	3.4	350.4	
2+02 W + 0.9	12" P.P.		
TP. 5.79	356.14	3.44	350.35
2+25			
W	5.7	350.4	
C	5.0	350.5	
E	5.6	350.5	
2+40			
C Run S.M.H.	5.20	350.94	
2+43			
E - 12 Six gar dirt	5.4	350.7	
E	5.5	350.6	
C	5.8	350.8	



356.14

W		5.3	350.8
	2+47		
W		4.7	351.4
C		5.2	350.9
E		5.0	351.1
	+ 0.4 Cent. approx	5.01	351.0 <sup>13</sup>
	+ 10.4 E Sim. gar.	4.91	351.2 <sup>23</sup> Cent.
	2+80		
W	- 13 do. gar. dirt	4.7	351.4
	2+02		
E		4.4	351.5
C		4.7	351.4
	+ 9.8 12° PP		
W		4.5	351.6
	3+44		
W	E 13' Shed Bd. + Bat. <small>could be gar. dirt.</small>	4.2	351.9 <sup>14</sup> in 0.5 alley
C		4.3	351.8
E		4.3	351.8
	3+56		
E	- 5.2 E Sim. gar. dirt	4.4	351.7
	3+75		
E		3.9	352.2
C		4.1	352.0
W		3.9	352.2

356.14

50

	3+94		
W	- 2.8 Sim. gar. dirt	3.3	352.8
	4+01		
W		3.3	352.8
	+ 0.4 12° PP		
C		3.7	352.4
E		3.7	352.4
	4+07		
E	- 4 Sim. gar. dirt	3.7	352.4
	4+40		
E		3.6	352.5
C		3.4	352.5
W		3.5	352.6
	+ 1.0 apron Cent.	3.54	352.60
	+ 4 Sim. gar. Cent.	3.35	352.79
	4+75		
W		3.5	352.6
C		3.8	352.3
E		3.9	352.2
	T.P. 4.45	350.57	402 352.12
	4+90		
E	- 5 Sim. gar. dirt	4.4	352.0
E		4.6	352.0
C		4.3	352.3
W		4.3	352.3
	+ 17.6 do. gar. Cent.	3.45	353.12



356.57

5102 W +0.5 12" PP

5142

W 5.1 351.5

C 5.4 351.2

+ 9.9 <sup>cem. tile</sup> 3' door to 81dg. 5.20 351.37

5171

E + 0.10 against 81dg 5.5 351.1

C 5.5 351.1

+ 9.7 12" PP 5.2 351.4

W 5.2 351.4

610005 S.L. UNIV. AVE

W Top cb 5.68 350.89

W Pav. 5.82 350.75

C " 6.18 350.39

+ 9.6 " 6.18 350.39

+ 9.6 Top cb 6.13 350.44

5' cb line UNIV.

E Pav 6.80 349.77

C " 6.68 349.89

W " 6.60 349.97

T.P. 5.81 356.39 6.09 350.48

NW&P <sup>46th</sup> UNIV. 5.04 351.27 351.23

57

5137 SW Cor. 10' Cent  
The 81dg 0.10 in ally



Cross Section Alley Block 257 Hayden Sub  
Between Dalbergia + Main From Yama to Division

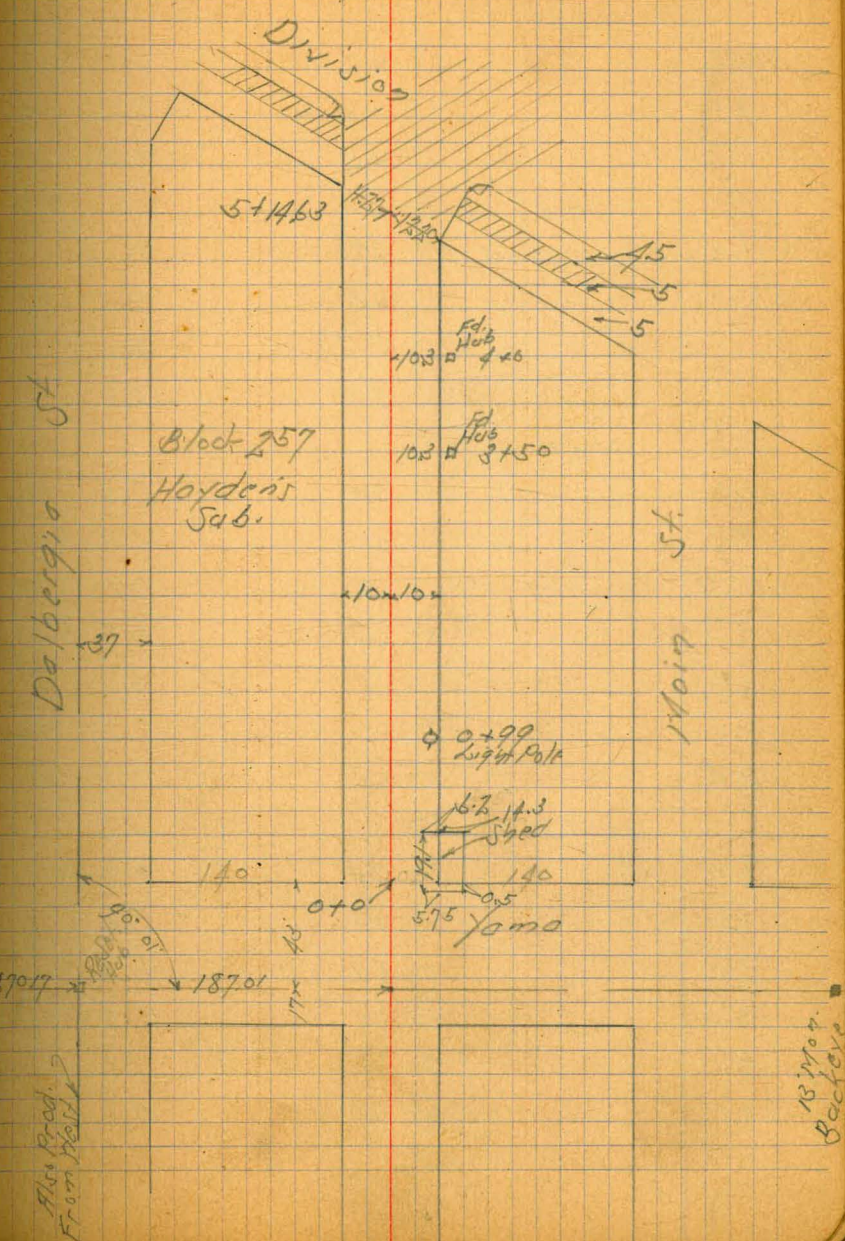
BM	4.39	13.37	8.98	HYD BP Near Division
TP	5.56	12.56	6.87	7.00
0-30-2 Yama				
S		6.1		6.5
2	on MH Rim	5.88		6.68
+6		5.6		7.0
+9	Bot Ditch From Start	10.1		2.5
H		9.8		2.8
+3		5.6		7.0
0-25				
H		10.1		2.5
2		10.3		2.3
S		10.0		2.6
0-17-2 Wash				
S		10.9		1.7
2		11.1		1.5
H		10.5		2.1
0-10				
H		10.5		2.1
2		10.2		2.4
S		10.6		2.0
0+0: F.L. Yama				
S		5.2		7.4
2		5.0		7.6
H		4.9		7.7

Red. Plot. on New Profile May 31-40 C.E. Hough

4 1/2 ft  
Cathedral

INDEXED  
E.F.S.

May 28-40  
Survey  
North of  
11/1000 58



13 Mon.  
Bockers



12.56

0+25

N	5.5	7.1
S	5.4	7.2
S	5.2	7.4

0+59

-0.4 - Fly A.8 Conerfolk	4.91	7.65
S	5.2	7.4
S	5.5	7.1
N	6.4	6.2

1+0

-10	7.0	5.6
N	7.1	5.5
+5	6.5	6.1
S	6.4	6.2
S	6.6	6.0
+2	5.1	7.5
+15	5.3	7.3

1+25

-15	7.4	5.2
S	7.4	5.2
S	6.9	5.7
+7	7.1	5.5
N	7.5	5.1
+15	7.5	5.1

12.56

1+70

-15	7.6	5.0		
N	7.8	4.8		
S	7.3	5.3		
+7	7.1	5.5		
S	7.5	5.1		
+15	7.9	4.7		
TP	10.61	15.9%	7.25	5.81

2+0

-15	11.4	4.5
S	11.4	4.5
+2	10.9	5.0
S	10.6	5.3
+6	10.8	5.1
+8	11.5	4.4
N	11.4	4.5
+15	11.3	4.6

2+25

-15	11.6	4.3
N	11.8	4.1
+2	11.7	4.2
+4	11.3	4.6
S	10.9	5.0
+7	10.8	5.1
S	11.6	4.3
+15	11.8	4.1



1592

3+50

-10	5.9	10.0
H	5.0	10.9
<del>S</del>	4.9	11.0
S	5.3	10.6
+10	5.8	10.1

3+75

-10	8.0	12.9
S	8.7	13.2
<del>S</del>	8.6	13.3
H	8.9	13.0
+10	8.8	13.1

8.50 23.99

4+10

-10	8.3	15.7
H	8.5	15.5
<del>S</del>	8.5	15.5
S	8.5	15.5
+10	8.6	15.4

4+50

-10	6.8	17.2
S	6.4	17.6
+5	5.9	18.1
<del>S</del>	5.9	18.1
H	5.5	18.5
+10	5.3	18.7

1592

2+50

-15	12.0	3.9
S	11.6	4.3
+5	10.9	5.0
<del>S</del>	10.8	5.1
+5	11.2	4.7
H	11.7	4.2
+15	11.7	4.2

2+75

-15	11.4	4.5
H	11.4	4.5
+5	10.8	5.1
<del>S</del>	10.6	5.3
+7	10.6	5.3
S	11.6	4.3
+15	11.8	4.1

3+0

-15	10.0	5.9
S	9.9	6.0
+3	9.3	6.6
<del>S</del>	9.2	6.7
+5	9.5	6.4
H	10.2	5.7
+15	10.6	5.3



23.99

4+75

-10	4.7	19.3
H	5.0	19.0
L	5.3	18.7
+1	5.2	18.8
+4	4.4	19.6
S	5.0	19.0
+10	5.7	18.3

5+0

-10	4.0	20.0
S	3.9	21.1
+2	3.3	21.7
+5	4.8	19.2
L	4.9	19.1
H	4.3	19.7
+10	3.8	20.2

5+14.63 taken on Line of Paving

H Cb Top	3.88	21.11
Gutter on Paving	2.55	20.44
L " "	4.61	19.38
S Gutter " "	5.18	18.81
S Cb Top	4.99	19.00

H Cb Division

S on Paving opp Alley	5.60	18.39
L " " Return	3.92	20.07

23.99

H on Pav opp Alley Ret	3.17	20.82
TP	2.70	14.34
	12.35	11.64
BM	5.37	8.97

 HX 80  
 MAT +  
 DIVISION  
 8.98



Cross Section Alley Block 83 City Hts.  
Between Cherokee & 37th St From Dwight to Landis

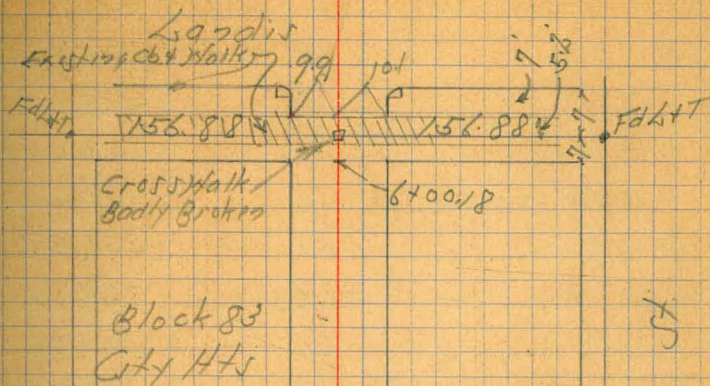
BM.	5.88	325.87		319.99	HW B.P. Dwight 37th St.
TP	8.71	333.37	1.21	324.66	
0-14-11 Cb Dwight					
F. Cb Top		9.20		324.17	
F Ground		9.8		323.6	
L "		9.5		323.9	
H "		9.2		324.2	
H Cb Top		8.55		324.82	
0-7-54 Conc Walk					
H on Conc Walk		8.57		325.00	
F " " "		9.02		324.95	
0-1.8-11 Conc Walk					
F on Conc Walk		8.87		324.50	
H " " "		8.27		325.10	
0+0-11.6 Dwight					
H		7.7		325.7	
+8		7.7		325.7	
+7		8.6		324.8	
L		8.5		324.9	
+6		8.6		324.8	
F		8.1		325.3	
0+6					
F		6.5		327.1	
+8		6.5		326.9	
+5		8.1		325.3	

Reduced to Plat. on Profile 2552  
May 31-46. C.B.H.

INDEXED  
E.P.S.

May 29-46  
Sisson  
Northern  
H Moore

62



Cherokee





333.37

S	8.1	325.3
+6	8.2	325.2
+8	6.3	327.1
H	6.0	327.4

0+25

H	5.1	328.3
+7	6.6	326.8
S	6.6	326.8
+5	6.5	326.9
+6	5.8	327.6
F	5.6	327.8

0+45

F	5.2	328.2
S	5.1	328.3
H	5.0	328.4

0+56

H-6.7 = Fly Conc Apron	4.71	328.66 ✓
H-9.4 = Garage Conc Floor	4.10	329.27 ✓

0+74

H-1.0 = Fly Power Pole		
H	4.2	329.2
S	4.5	328.9
F	4.7	328.7

TP	5.17	334.11	4.43	328.94
----	------	--------	------	--------

334.11

0+95

-40 = Garage Conc Floor	5.99	328.12 ✓
F	5.0	329.1
S	5.2	328.9
H	4.8	329.3

+6 = Fly Conc Apron	4.82	329.29 ✓
+8.8 = Garage Conc Floor	4.32	329.79 ✓

1+25

F-1.7 = Garage Dirt Floor	4.0	330.1 ✓
H	1+50	

H	2.5	330.6
---	-----	-------

S	3.9	330.2
---	-----	-------

F	3.8	330.3
---	-----	-------

+10	4.3	329.8 ✓
-----	-----	---------

2+0

-10	3.2	330.9 ✓
-----	-----	---------

F	2.6	331.5
---	-----	-------

S	2.8	331.3
---	-----	-------

+3	3.4	331.7
----	-----	-------

H	1.6	332.5
---	-----	-------

+10	2.6	331.5 ✓
-----	-----	---------

2+0.2

H-0.4 Fly Power Pole		
----------------------	--	--

TP	6.17	337.95	2.33	231.78
----	------	--------	------	--------



337.95

2+25

-10	5.7	332.3	✓
-1	5.9	332.1	✓
H	5.4	332.6	
+6	4.9	333.1	
⊗	5.5	332.5	
+7	5.7	332.3	
F	6.2	331.8	
+10	6.6	331.4	

2+45

F-8.8 = Hly Conc Apron	6.25	331.70	✓
F-10.8 = Garage Conc Floor	6.06	331.89	✓
F	5.8	332.2	
+3	5.5	332.5	
⊗	5.4	332.6	
+2	5.4	332.6	
+6	4.6	333.4	
H	5.0	333.0	
+1	5.6	332.4	
+10	5.7	332.3	

2+56

H-2.3 = Fly 8' Conc Apron	5.38	332.57	✓
H-5.8 = Garage Conc Floor	4.67	333.28	✓

337.95

2+83

-10	4.8	333.2	
H	4.3	333.7	
⊗	5.0	333.0	
+2	5.0	333.0	
F	5.7	332.3	
+5.2 = Garage Conc Floor	5.73	332.22	✓

2+94

H-1 = 8' Conc Apron	4.58	333.37	✓
H-5.7 = Garage Conc Floor	3.72	334.23	✓
	3+0		

H+0.2 = Hly Power Pole			
	3+26		

-10	5.3	332.7	
F	4.8	333.2	
⊗	4.6	333.4	
H	4.5	333.5	
+0.4 = 8' Conc Walk	4.37	333.58	✓

3+27

F-4.8 = Fly Do Garage Conc Floor	4.70	333.25	✓
----------------------------------	------	--------	---

3+43

F-4.6 = Hly Do Garage Conc Floor	4.66	333.29	✓
----------------------------------	------	--------	---

3+50

H	4.8	333.8	
⊗	4.3	333.7	



337.95

F		4.1	333.6
	3+68		
F	= 2' Conc Walk	4.26	333.69 ✓
+24	= 1 1/2' " "	4.22	333.73 ✓
	3+96		
F	= 2' Conc Walk	3.63	334.32 ✓
	4+0		
F		3.6	334.4
2		3.2	334.8
+3		3.3	334.7
+9.9	= 1 1/2' Power Pole		
11		3.5	334.5
+15		3.6	334.4
	4+50		
-15		2.8	335.2
11		3.1	334.9
2		3.0	335.0
F		2.8	335.2
+10		3.2	334.8
TP	6.07	341.04	334.97
	4+85		
11	-7.2 = 2' Garage Dir/Floor 54		335.6 ✓
	5+0		
-10		5.7	335.3
F		5.3	335.7

341.04

2		5.2	335.8
+9.7	= 1 1/2' Power Pole		
11		5.2	335.8
	5+30		
11		5.0	336.0
2		5.0	336.0
F		4.9	336.1
+10		5.3	335.7
	5+56		
F		4.3	336.7
2		4.2	336.8
+9.3	= Fly H Conc Apron	4.17	336.87
11	0.7 " "	4.14	336.90
+3	" " "	4.04	337.00
	5+68 = 1 1/2' Garage on F H Entrance ✓		
11		4.0	337.0
2		4.1	336.9
F		4.1	336.9
+2.6	= 1 1/2' Conc Drive	3.98	337.06 ✓
	5+90		
-2.6	= 1 1/2' Conc Drive	4.23	336.81 ✓
F		4.5	336.5
+3		3.9	337.1
+5		4.6	336.4
2		4.6	336.4



341.04

H		44	3366	
	6 + 0.18 = S.L. Lander			
H		46	3364	
+5		5.3	3357	
L		5.3	3357	
+4		54	3356	
+7		49	3361	
F		54	3356	
	6 + 0.2 = Sly Conc. Walk			
F = Sly Conc. Walk		5.77	33527	
H = Sly Conc. "		5.34	33570	
	6 + 0.72 = Sly Conc. Walk			
H on Conc. Walk		5.42	33562	
F " " "		5.84	33520	
	6 + 1.42 = Sly Cb Lander			
F Cb Top		6.08	33496	
F Ground		6.5	3345	
L "		6.2	3348	
H "		6.0	3350	
H Cb Top		5.64	33540	
TP	7.74	342.72	6.06	33498
BM		7.47	33525	14 M. BP Land 343616 33525



76

67







Cross Section Alley Block 47  
 W.P. Herberts Subdivision  
 East & West Alley 15' Wide

Indexed  
 LM

Feb. 20-11  
 Sisson  
 North 4th  
 W. Moore **59**

B.M. 4.17 371.89 367.73

TP 5.91 373.70 4.10 367.79

0+10 = FCB 38765

S on Pavings 4.61 369.09

L " " 4.56 369.14

N " " 4.52 369.18

0+0 = FL 38765

N Top cb 3.75 369.95

Gutter on Pavings 3.97 369.73

L " " 4.24 369.46

Gutter " 4.00 369.70

S Top cb = 3.81 369.89

+0.5 = 1/4 x 2 1/2 Hedge

0+26

-2.1 = 1/4 x 2 Conc Walk 4.00 369.70 ✓

-0.3 = 1/4 x 2 1/2 Wide Hedge

S 4.2 369.5

L 4.7 369.2

+5 4.7 369.2

N 4.2 369.5

+3.5 = 1/4 Frame House 3.27 370.43 ✓

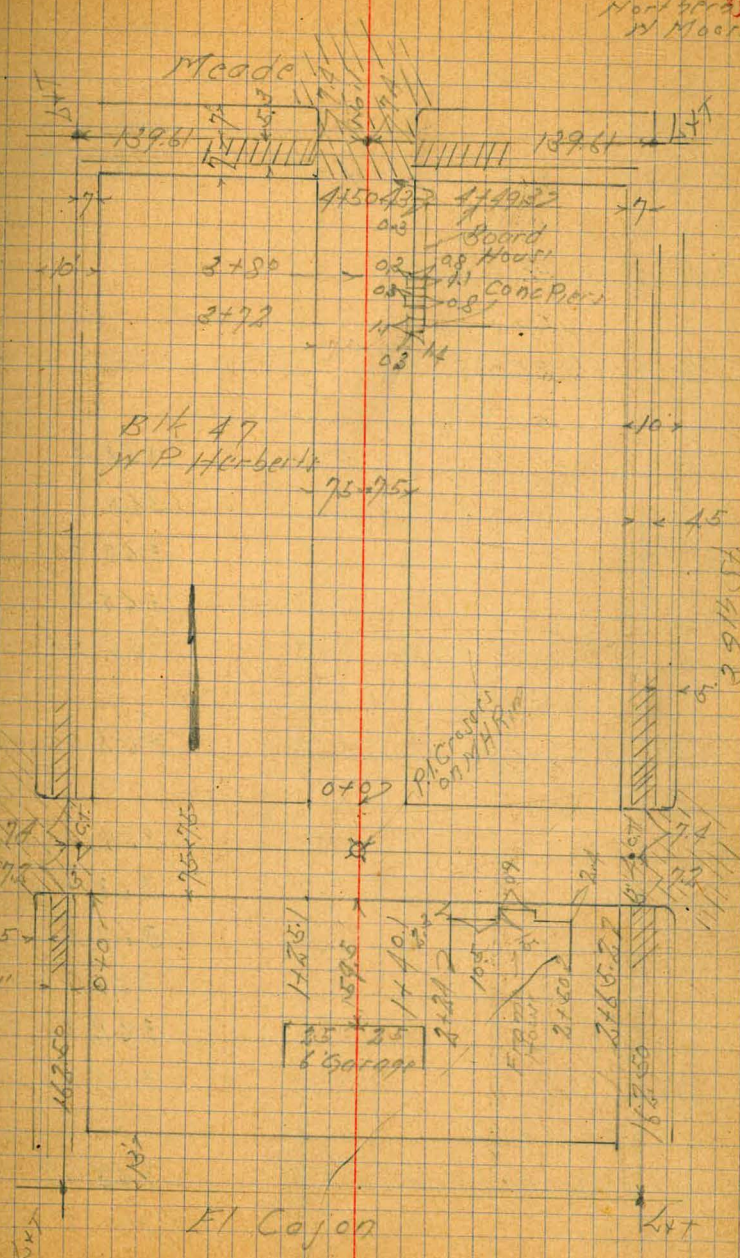
1/4 Conc Porch

0+42

-3 = 1/4 Frame House 5.0 368.7 ✓

N 4.9 368.8

Red X Plot on 2693 2-24-11





373.70

1/2	5.2	368.4	
+6.2 = 1/2 2.5 Wide Hedge			
S	4.8	368.9	
+2' = N 1/2 Conc Walk	4.5	369.25	✓
0+60			
H-2.5 = Fly From House			✓
0+62			
S+0.5 = 1/2 Fly 2.5 Wide Hedge			+
0+70			

-5	5.3	368.4	
S	5.4	368.3	
1/2	5.4	368.3	
H	5.3	368.4	
+6.5 = 1/2 2 Conc Walk	5.42	368.28	✓
0+86			
S-10.3 = 1/2 Garage Conc Floor	5.20	368.50	✓
7 opening			
1+0			

-5	5.7	368.0	
H	5.6	368.1	
1/2	5.8	367.9	
+5	5.7	368.0	
S	5.4	368.3	
+5	5.5	368.2	

1+19

H-48 = 1/2 Garage Conc Floor	5.61	368.09	✓
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373.70

1+251 = H 1/2 N 1/2 Alley			
-5	5.6	368.1	
S	5.4	368.3	
1/2	5.9	367.8	
H	6.1	367.6	
1+30			
S-0.2 = Fly Post or Pole			*
1+32.6 = 1/2 N 1/2 Alley			

H	6.1	367.6	
1/2 0.2 N 1/2 Rim	5.90	367.80	✓
1/2	5.8	367.9	
+5.95 = 1/2 1/2 6 Garage Conc Floor	4.76	368.94	✓

1+40.1 = 1/2 N 1/2			
-5	6.0	367.7	
S	6.1	367.6	
1/2	6.1	367.6	
H	6.0	367.7	

+0.6 = Fly Fence			
1+64			

-5	6.2	367.5	
H	6.1	367.6	
1/2	6.1	367.6	
S	6.1	367.6	
+3.5 = 1/2 Garage Conc Floor	5.57	368.13	✓



373.70			
	1+73		
S-0.1 =	Hly Board Fence		
	1+92		
H-2.6 =	Sly + 2.2 Cor. Posts	5.97	367.73 ✓
	2+0		
-5		5.90	367.8
S		6.0	367.7
1/2		6.2	367.5
H		6.2	367.5
+0.7 =	Fence		
+5		6.1	367.6
	2+03		
S =	Ely Board Fence		
	2+24		
-5		6.1	367.6
H		6.2	367.5
1/2		6.3	367.4
1/2		6.2	367.5
S		6.2	367.5
+2.3 =	Hly Cor. Frame Ho.	6.2	367.5 ✓
	2+43		
H-0.6 =	Ely Fence + Sly 2 Ho. dpt		
	2+50		
-2.4 =	Hly Cor. Ho. dpt	6.5	367.2 ✓
S		6.4	367.3
1/2		6.7	367.0

373.70			
H		6.3	367.4
+5		5.8	367.9
	2+65.2 =	M.L. 397.5 J	
-0.5 =	Ely + Sly 2 Ho. dpt		
H Topch		6.29	367.41
Gutter on Porch		6.50	367.20
S	" "	6.74	366.90 ✓
Gutter	" "	6.60	367.10
S Topch		6.37	367.33
	2+75.2 =	M.C.B. 397.5 J	
S on Porch		7.13	366.57
S	" "	7.11	366.59
H	" "	7.12	366.58
TP	4.96	292.75	591
			367.77



North + South Fly

372.75

-0.5 = Fly Fence	0+0 = N. 1/4 East + West Fly			
F	48	368.0	x	
1/2	5.2	367.6		
N	5.1	367.7		
	0+27			
-10	5.0	367.8		
N	4.9	367.9		
1/2	5.0	367.8		
F	4.9	367.9		
+0.6 = Fly Fence			x	
+2 = SW Cor Bldg	4.6	368.2	v	
	0+30			
N + 2.5 = N 1/4 Post Pole			v	
	0+44			
N - 6.0 = 1/2 Garage Conc Floor	4.37	368.38	v	
	0+49			
F - 2 = NW Cor Bldg	4.9	367.9	v	
F	4.8	368.0		
1/2	4.7	368.1		
N	4.6	368.2		
+5	4.6	368.2		
	0+54			
N + 1.1 = Fly Board Fence			x	
	0+74			
-10	3.8	369.0	x	

Red + Plot on 2693 2-24-41 BH

372.75

72

N	3.9	368.9		
+1.3 = Fly Board Fence				
1/2	4.7	368.1		
F	4.7	368.1		
+1.0	4.6	368.2		
	0+81			
N - 5.1 = Fly De Garage Conc Floor	3.43	369.32	v	
	0+98			
N - 4.0 = N 1/4 De Garage Conc Floor	3.27	369.48	v	
	1+0			
-10	4.4	368.4		
F	4.3	368.5		
1/2	4.2	368.6		
N	3.9	368.9		
+5	3.7	369.1		
	1+01			
N + 2.3 = N 1/4 Post Pole				v
	1+10			
F - 1.8 = NW Cor Bldg	4.01	368.74	v	
F - 7.0 = 1/2 Garage Conc Floor	3.89	368.86	v	
N - 5.8 = 1/2 Garage Conc Floor	3.5	369.3	v	
TP	5.83	374.68	3.92	368.83
	1+41			
-10	5.8	368.9		
N	6.1	368.6		



37466

$\frac{1}{2}$	5.8	368.9	
F	5.9	368.8	
+ 1.7 = $\frac{1}{4}$ Conc Apron	5.95	368.71	✓
+ 7.6 = $\frac{1}{2}$ Garage Conc Floor	5.87	368.79	✓
	1+70		
F - 1.0 = Sky Wire Fence			
	1+75		
-1.0	5.8	368.9	
F	5.9	368.8	
$\frac{1}{2}$	5.7	369.0	
M	5.6	369.1	
+ 1.0	5.3	369.4	
	2+0		
-1.0	5.2	369.5	
M	5.7	369.0	
$\frac{1}{2}$	5.6	369.1	
F	5.9	368.8	
+ 0.2 = $\frac{1}{4}$ Wire Fence = $\frac{1}{4}$ Board Fence	6.7	368.0	+
+ 1.0			
	2+12		
M + 1.6 = $\frac{1}{4}$ Porc Pole			✓
	2+50		
-1.0	6.0	368.7	
- 0.3 = Board Fence			
F	5.8	368.9	

37466

73

$\frac{1}{2}$	5.5	369.2	
M	5.5	369.2	
+ 1.0	5.4	369.3	
	2+60		
M - 1.7 = $\frac{1}{2}$ Garage Conc Floor	4.75	369.91	✓
	2+66		
F - 0.4 = $\frac{1}{2}$ 1.5 Conc Walk	5.87	368.79	✓
	2+75		
-1.0	4.8	369.9	
M	5.2	369.5	
$\frac{1}{2}$	5.2	369.5	
F	5.4	369.3	
+ 1.0	5.8	368.9	
	2+85		
M - 1.8 = $\frac{1}{2}$ Garage Conc	4.30	370.36	✓
	3+0		
-1.0	5.3	369.4	
F	4.9	369.8	
+ 0.2 = Fence Lattice			+
$\frac{1}{2}$	4.9	369.8	
M	4.6	370.1	
+ 1.0	4.6	370.1	
	3+0.9		
M - 1.8 = $\frac{1}{2}$ Garage Conc Floor	4.17	370.49	✓
	3+26		
F + 1.0 = $\frac{1}{4}$ Lattice Fence + $\frac{1}{4}$ Sky Wire Fence			x



374.66

3+35

-11.7 = $\frac{1}{2}$ Garage Conc Floor	3.67	370.99	✓
H	4.3	370.4	
$\frac{1}{2}$	4.3	370.4	
F	4.4	370.3	
+10	4.7	370.0	

3+48

F+0.3 = Nly Side Fence			+
H = Nly Post Pole			✓

3+53

-6.8 = $\frac{1}{2}$ Garage Conc Floor	4.17	370.49	✓
F	4.2	370.5	
$\frac{1}{2}$	4.2	370.5	
H	4.1	370.6	
+10	4.0	370.7	

3+72

H-12 = $\frac{1}{2}$ Garage Conc Floor	3.65	371.01	✓
F+0.3 = Top Conc Pipe	3.02	371.64	✓

3+80

F+0.3 = Top Conc Pipe	2.3	372.4	+
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3+85

H-0.2 = Sky Lat 4 Fence			+
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4+0

-10 =	2.5	371.2	
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H = Lat 4 Fence	3.6	371.1	+
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374.66

74

$\frac{1}{2}$	3.8	370.9	
F	3.9	370.8	

+0.5 = Nly Board House			+
	4+12		

H+0.1 = Nly Lat 4 Fence			+
	4+21		

H+0.3 = Fly 15 Conc Walk	3.11	371.55	✓
	4+36		

-0.2 = Nly Board House			+
F	3.9	371.0	

$\frac{1}{2}$	3.5	371.2	
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+2.2 = Nly Fly 15 Conc Walk	3.20	371.46	✓
H	3.2	371.5	

4+50-43 = Sh Meads

H Top 66	3.47	371.19	
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Gutter on Pavlog	3.78	370.88	
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$\frac{1}{2}$ " "	4.16	370.50	
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Gutter " "	3.94	370.72	
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F Top 66	3.85	370.81	
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4+64-43 = SCB Meads

F on Pavlog	4.45	370.21	
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$\frac{1}{2}$ " "	4.40	370.26	
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H " "	4.27	370.39	
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TP	4.20	374.47	4.39	370.27
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BH	4.87	369.60	
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Field 36.965 office 369.75  
 Meads  
 369.75



B.M	2.83	372.43	369.60	NW 8P Moodet 397987
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B.M		474	367.69	NW 8P E/Co 117 P 394851 367.76
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139.88 W 7 E

139.92 " " " "

5471  
5451  
5449

ENGINEERING DEPARTMENT,  
CITY OF EAST SAN DIEGO,  
CALIFORNIA.

67  
24  
29

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.