LOT SURVEYS

DIETZGEN

MINING

TRANSIT BOOK

No. 422

F.B. 584

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

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MICROFILMED
DEC 1 1954

Lot Surveys.

Card Index to Mar. 21, 1918
" " " Aug 20, 1918

3.4
25.9
8.1
37.0

89 56

OVERLOOK. OIL Pav. Ele. page 33 to 38

Blk. 49 Ocean Beach page 39 to 42

Diancia 43 - 45

Lewis & Albatross Curb levels 46 to 48

West Lewis 49 to 52

Dorcas 53 to 57

Hawthorn St. Felton to Gregory 58 to 60

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Survey Lots 1 & 16 Country Paradise 1.

Lot Survey for Mrs. M. E. King 2

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Lots 8-13 - Blk. 189 C Hts for E. G. Hoffman 3.

Lot 35 - Blk 15 - Teralta, for Daniel Dunn 4.

Lots 8 & 9 - Blk. 7. Bung. Pk. for O.E. Elwell 5.

Lots 33 & S. 8' of 34 - Blk. 39. Teralta, for Mrs. Bateman 6.

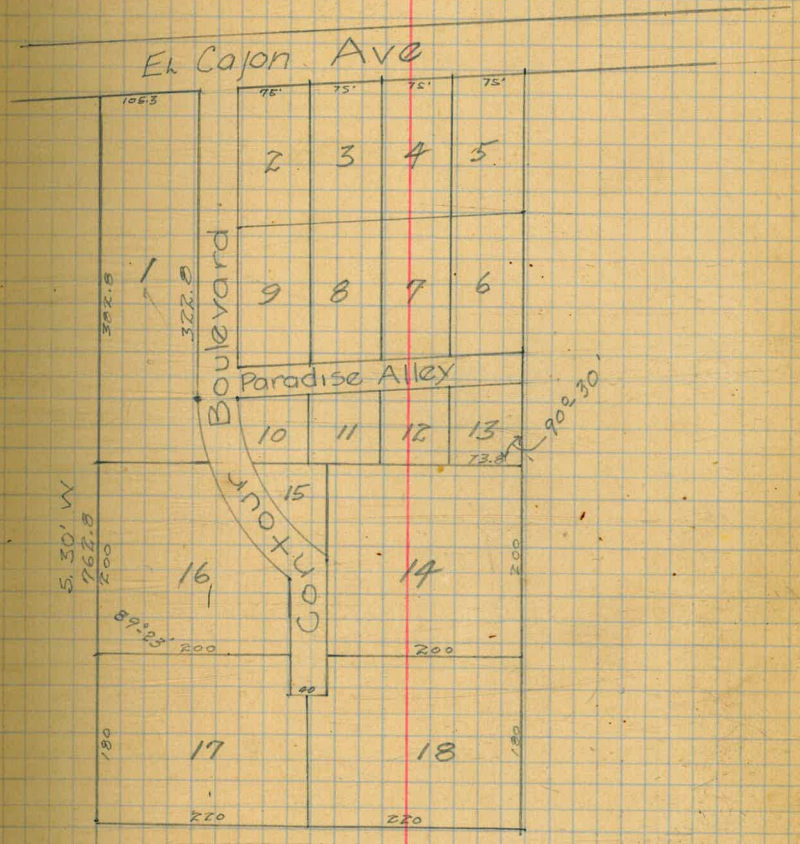
Lots 7 & 8 Blk 4 Res Sub. Blk 1-12 Fairmont Add. 10

Lots S ½ 14 all 15 Blk 5 Fairmont Annex No 2, 11

Lots 8, 9 & 10 Blk 2 Wilshire Place 12

Lots 9-10 Blk 4 City Hgts Annex #1 16

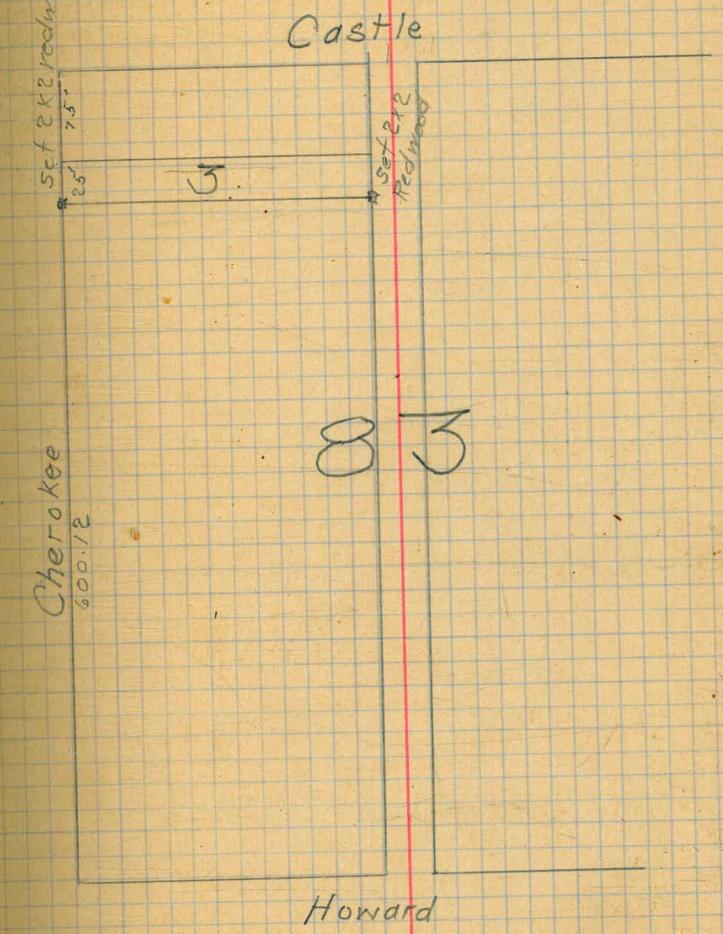
Survey Lots 1816. Country Paradise.



Lot Survey for Mrs. M.E. King

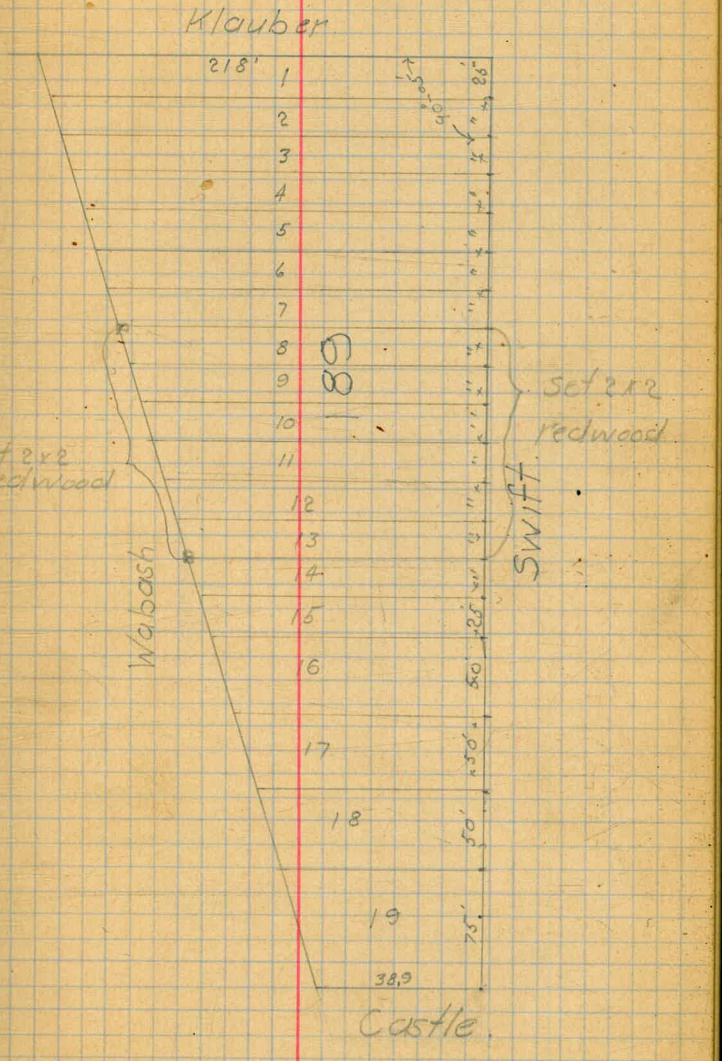
March 18, 18.
Hyatt
W. Brown

2



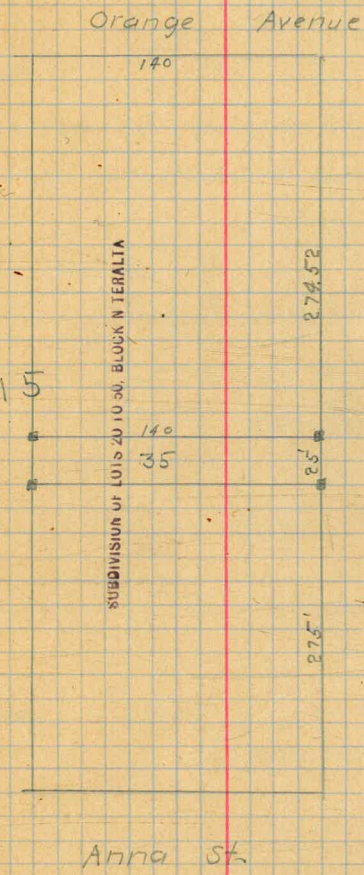
Lot Survey for
E. G. Hoffman.

Ayatt
Brown
Apr 5, 18.



Lot Survey for Daniel Dunn

Hyatt & Brown July 11, 18.

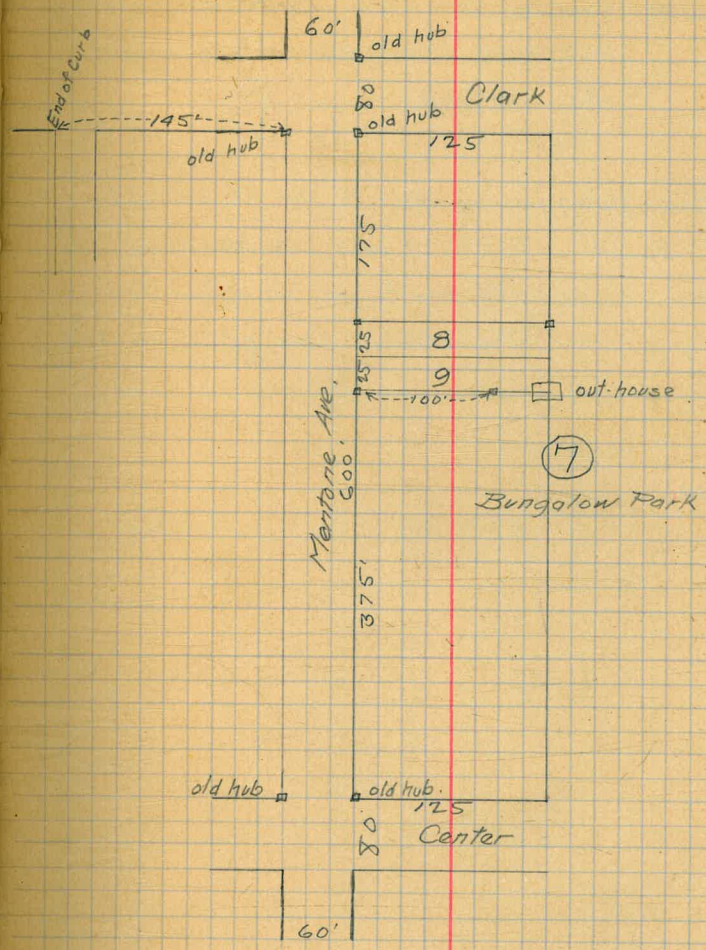


Lot Survey for O.E. Elwell.

Note: Out house is over S.E. corner.
Set stake on south line 100' back from front of lot.

W.C. Brown
J.D. Chandler

Oct. 18, 1918.



Set 2 x 2 Redwood hubs.

Lot Survey for Mrs. Bateman.

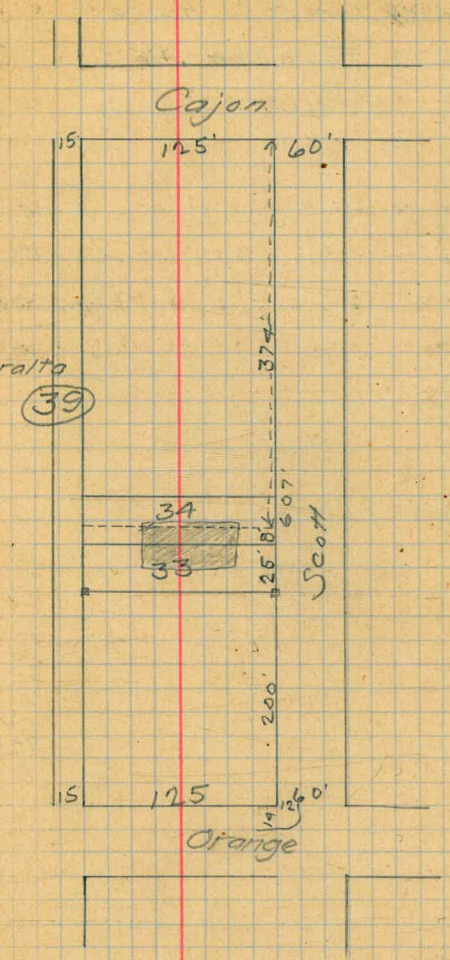
4238 Scott Ave.

Hc 2712-M.

Note: Mrs. Bateman has deed to lot 33 and south 8' of 34. North line outs into her house, and she is going to try to get an extra foot on the north. No stakes were set on north side. House is about a foot over the line.

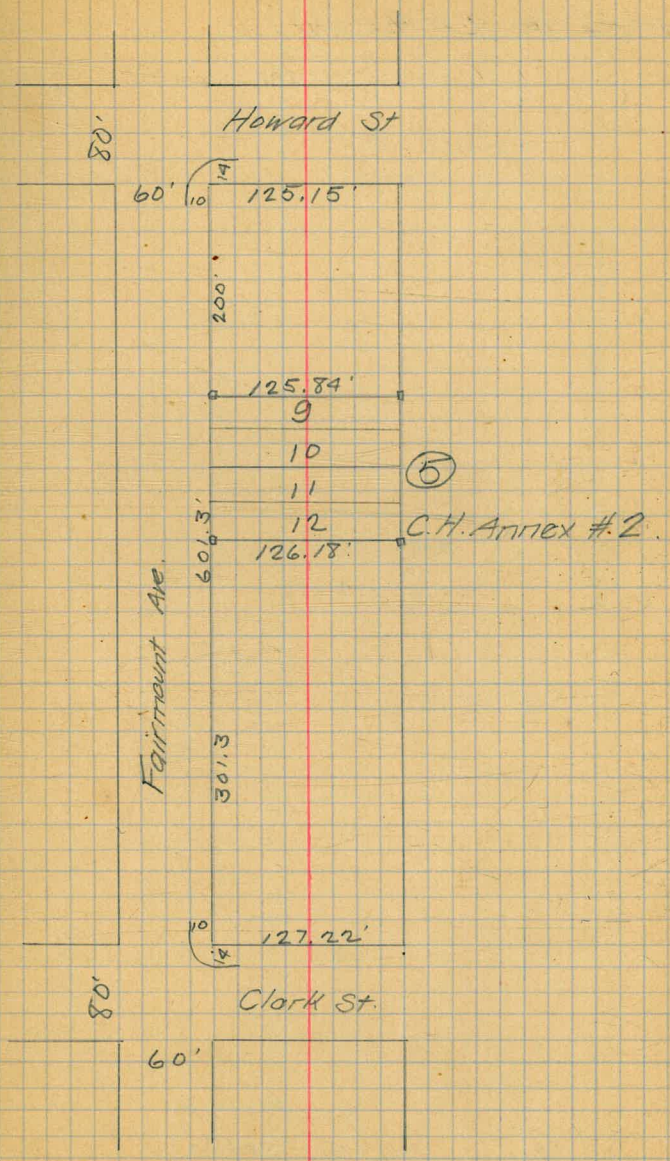
W.C. Brown.
J.D. Chandler.

Nov. 22, 1918

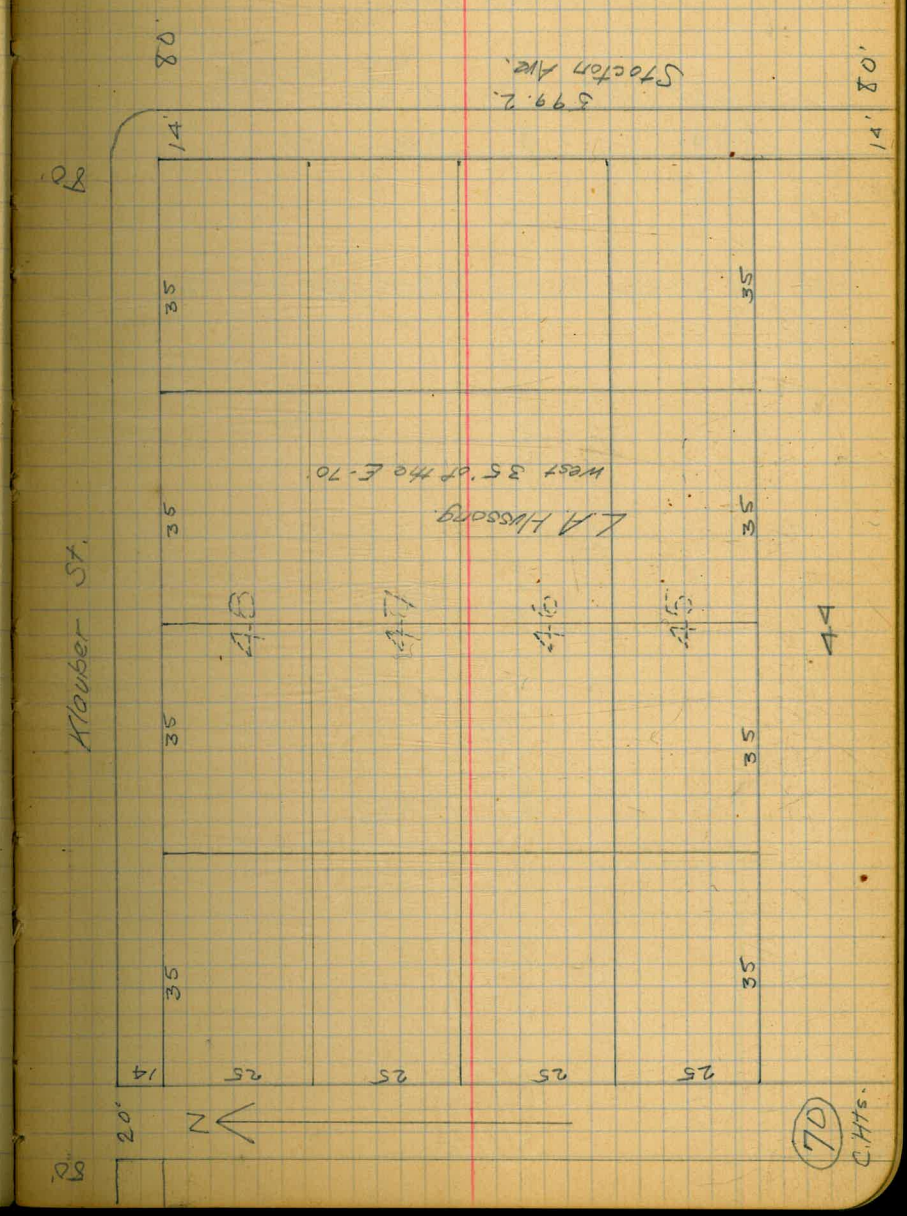


Lot Survey for H.M. Hodge
3557 Fairmount Ave.
Hc. 1527-J.

Note



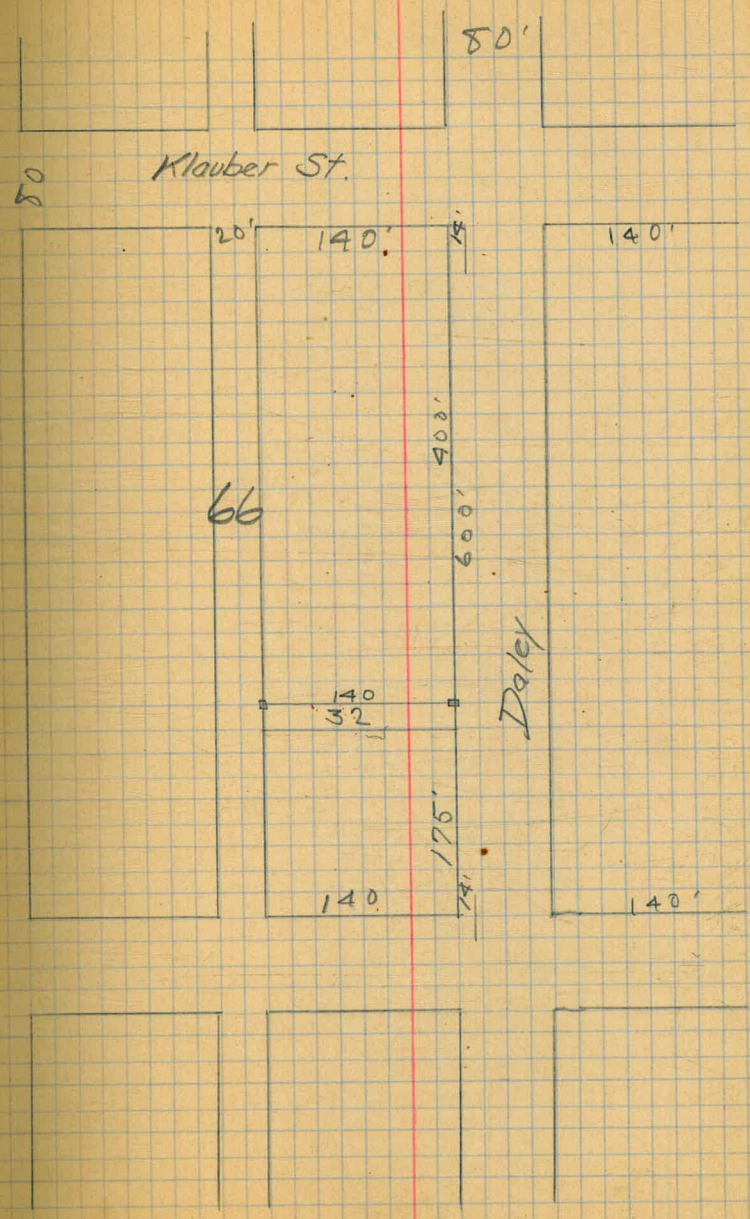
Survey for L.A. Hussong.



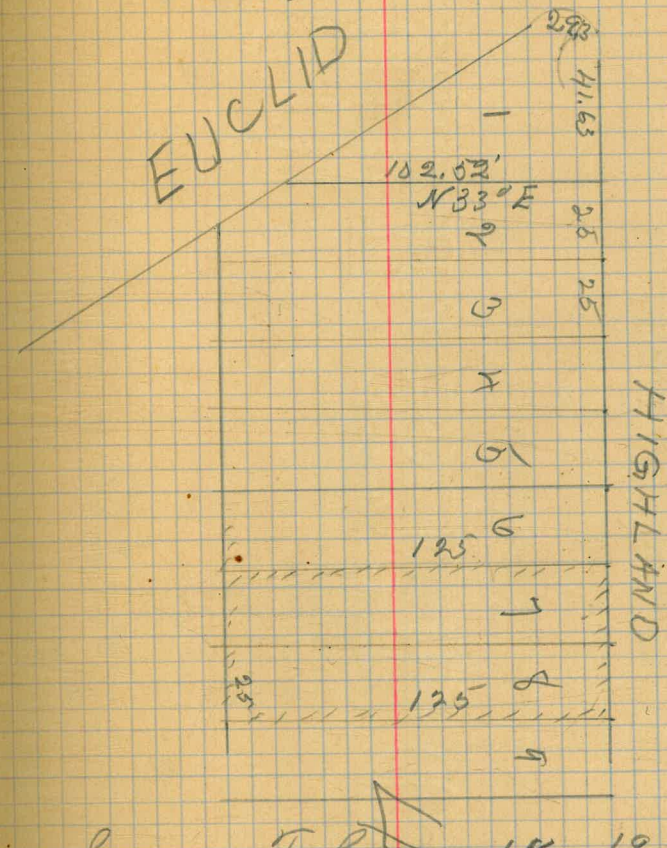
Survey for Roberts.
3718 Daley Ave.

Lot 32 Block 66 Cliffs.

Roof and window frames extend over north line

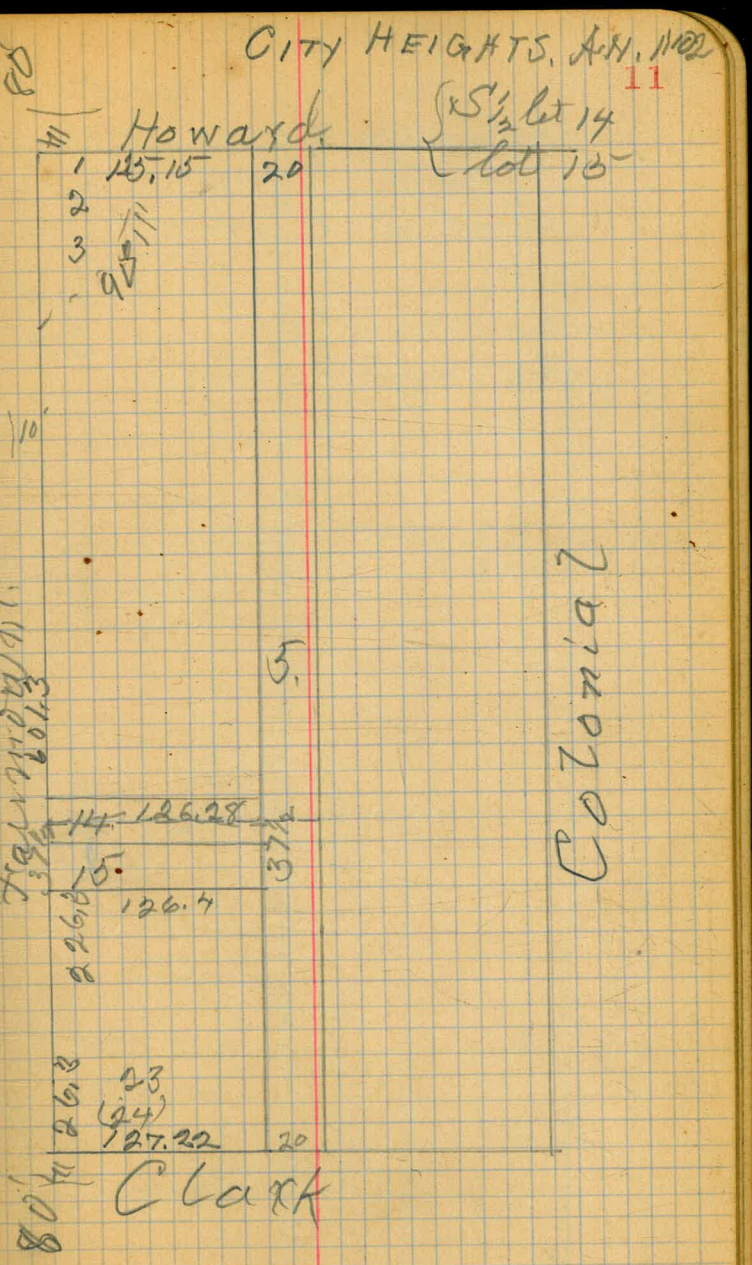


Resub. division of Bks 1-12
Fairmont Addition.



Survey Feb 15 - 1921
Merrill
Buckley

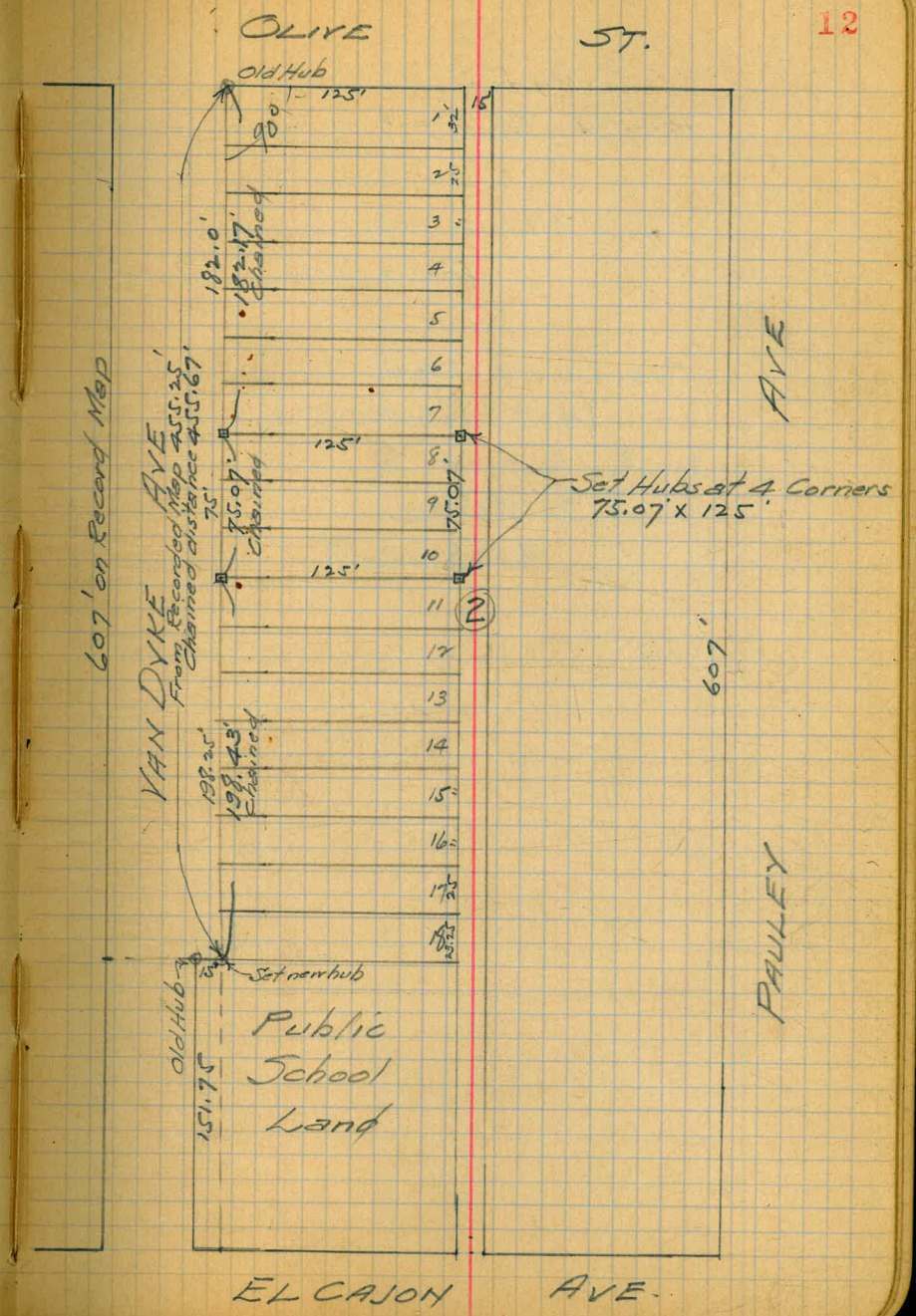
CITY HEIGHTS. A.M. 1102



March 2-21

Lot Survey for
Lots 8, 9 & 10
Block 2 - Willshire Place

Survey: Mar. 11th 1921
Ford, Ferguson & Fenton



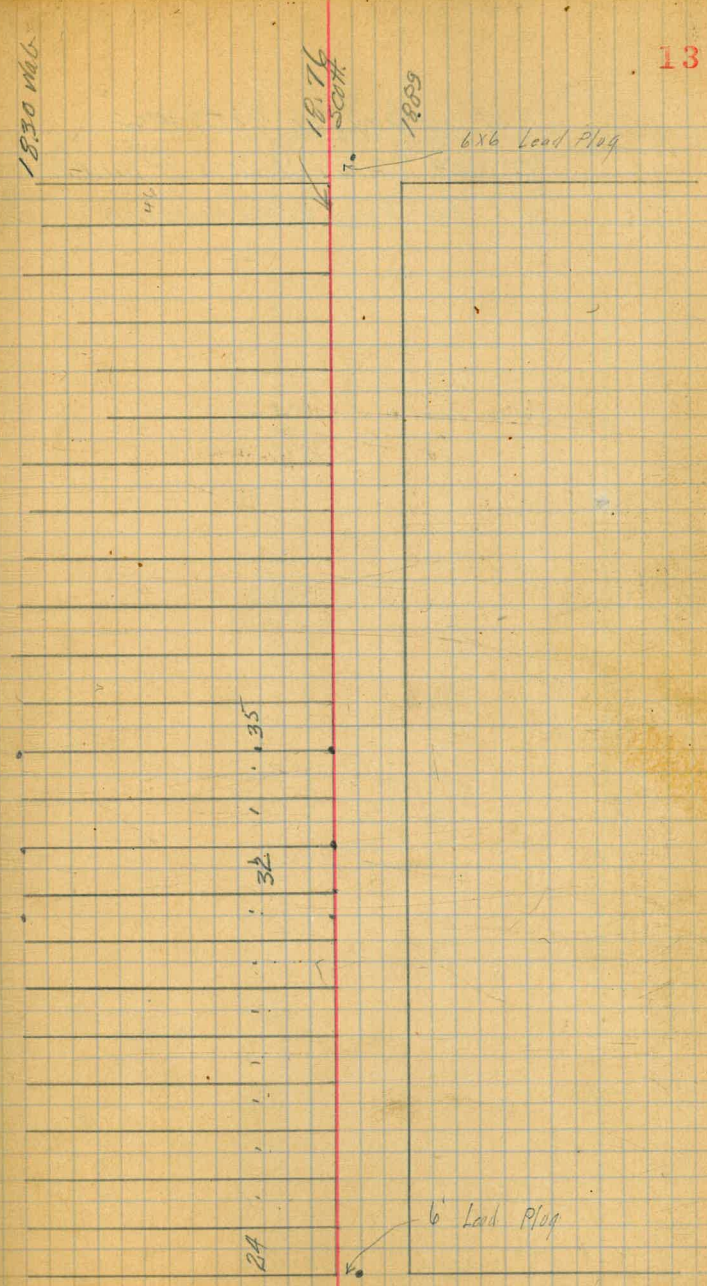
Lot Survey for Lots 33 & 34
Block #4 - Subdiv. 7-17- N. Peralta.

Survey Mar. 16, 1921
Ford & Fenton.

Mrs. Cordrey -
(4071 Kansas -)
Mail Reciipt to
F. S Walker.
4138 Scott -

300 80 140 - 20 140 80 300.3

300 563.30 568.76 569.96 Chained 300.3.

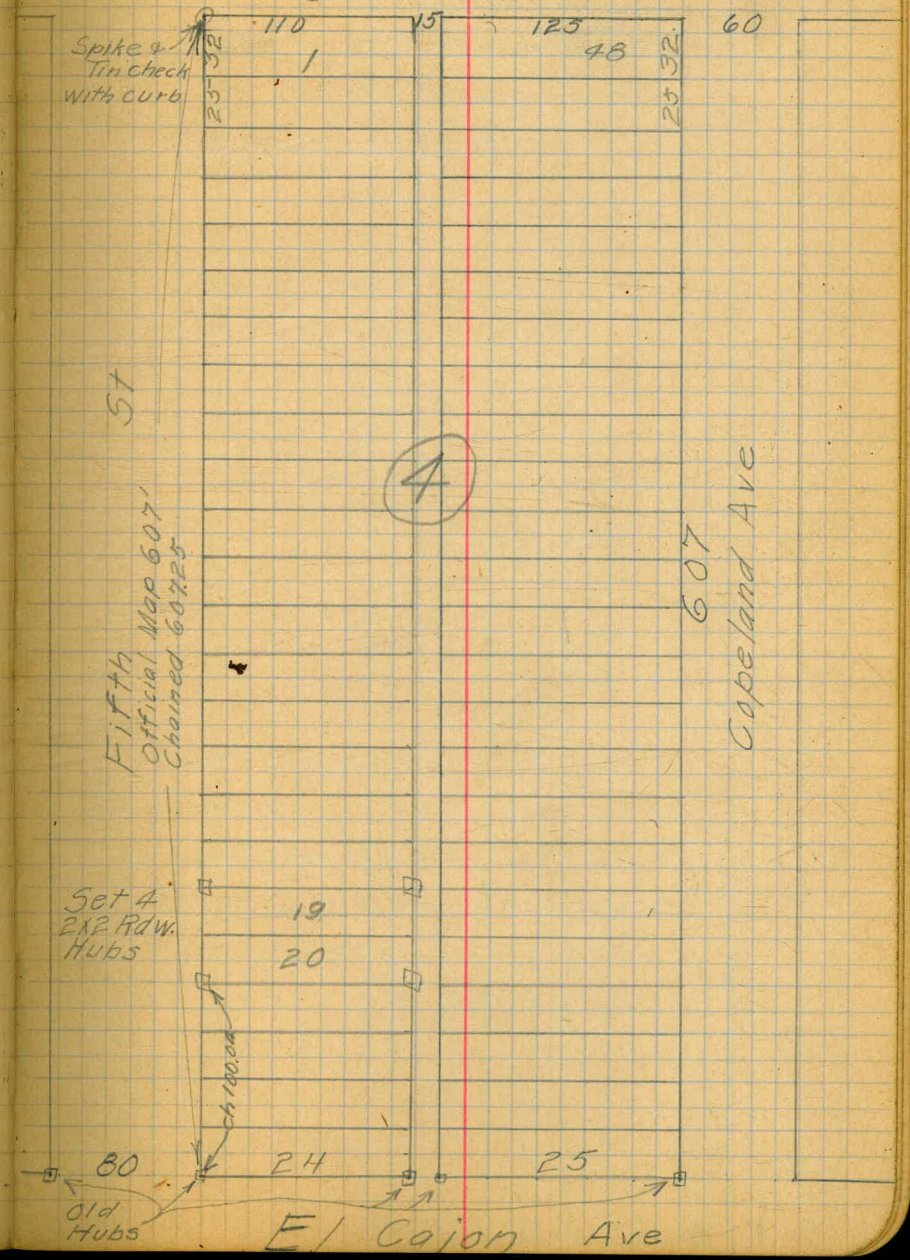


Lot survey for Lots 19&20
Block #4 Wilshire Place
for Frank Sebastian

June 29, 1921

Bartlett
Wittman

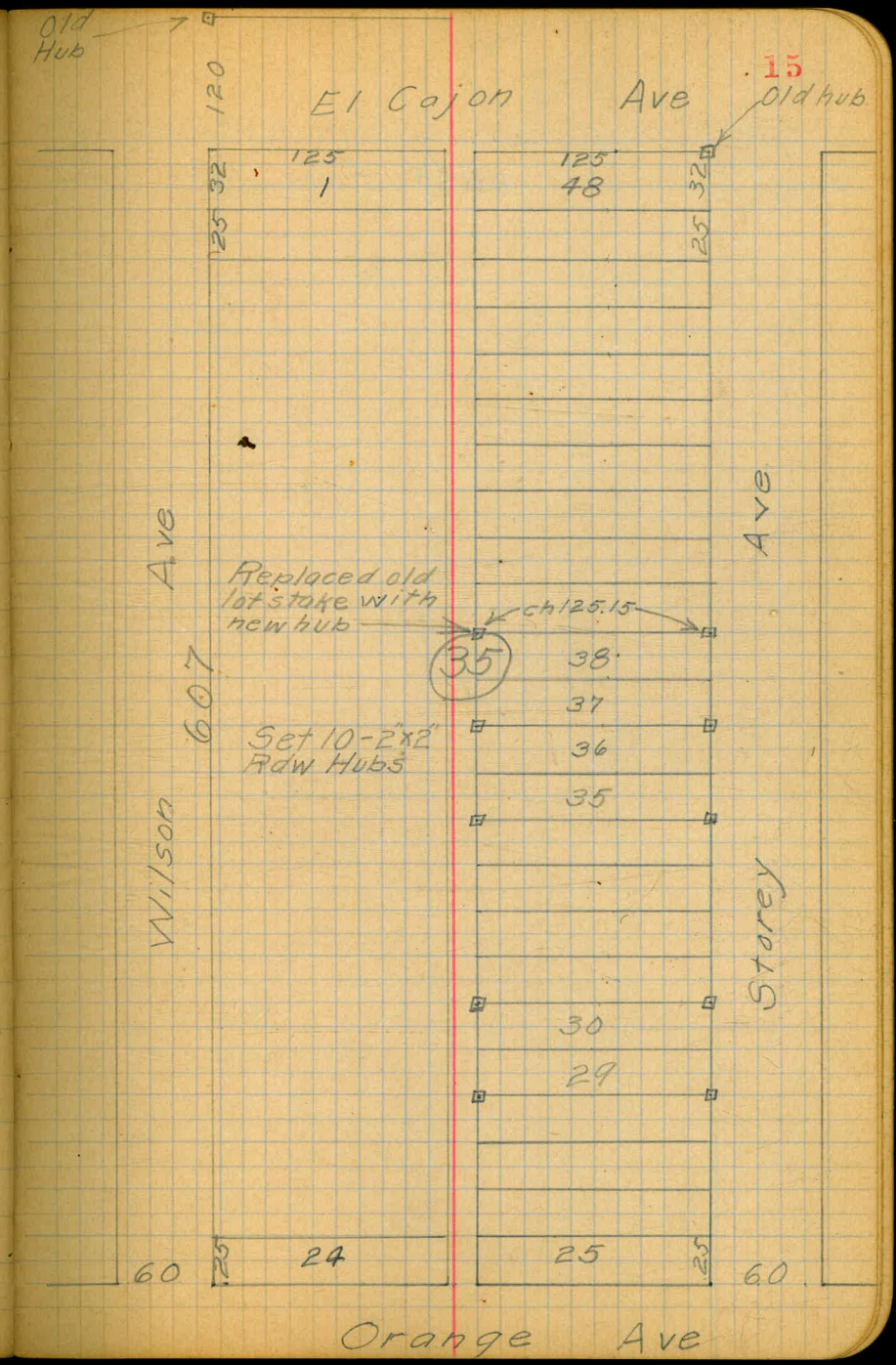
14



Lot Survey of Lots 29 & 30 and 35-38 inclu. of Block #35 Teralta for Thierza A Wright 4205 Wilson

Survey June 30, 1921 by Bartlett & Wittman

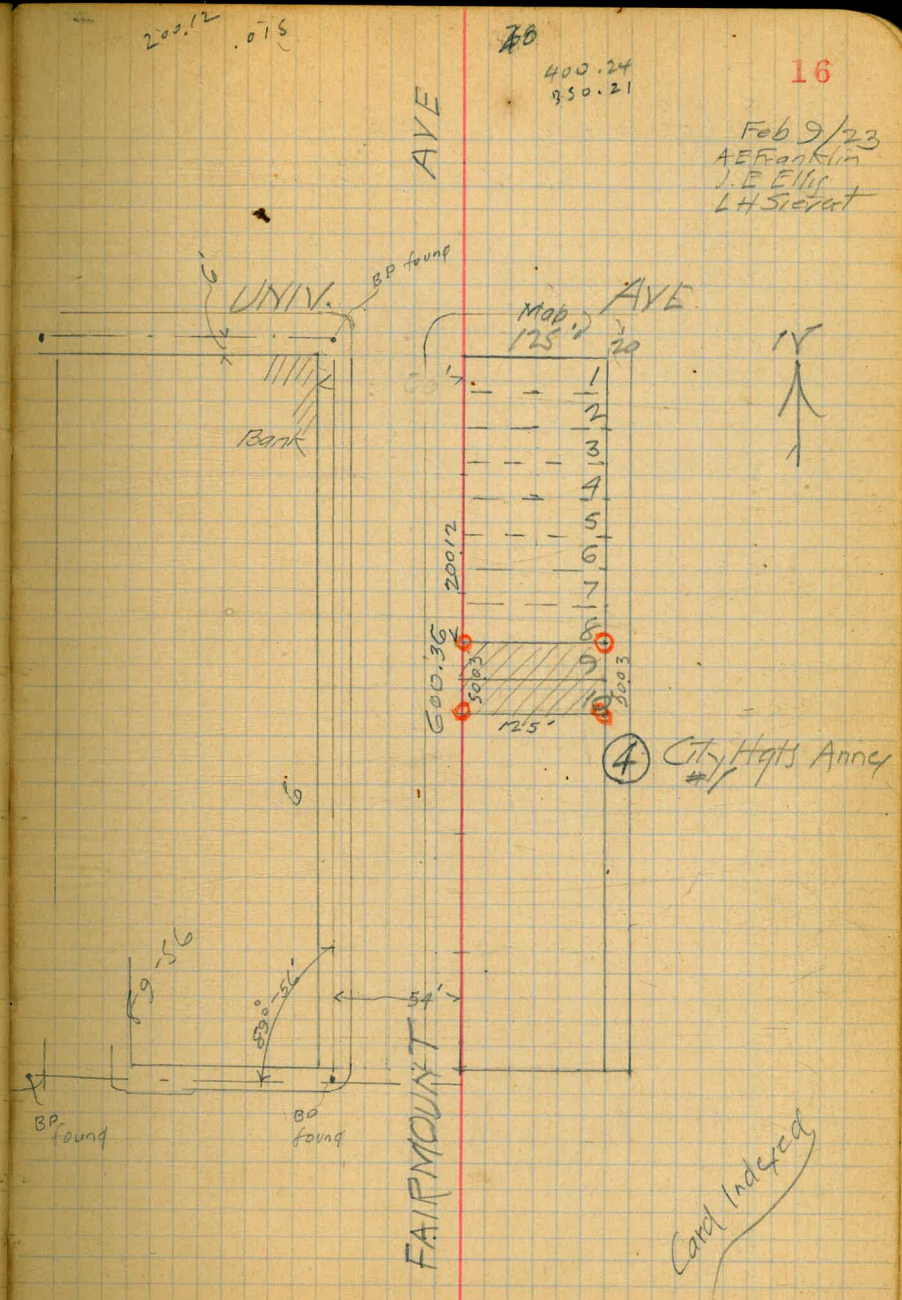
From face of curb at Orange to old hub at N.L. El Cajon. Ck 0.02
From face of curb at Orange to old hub at S.L. El Cajon. Ck 0.01
Curb between Storey & Wilson checked 0.30



Perm. #111

Lot Survey F.W.H Mayer
3859 Farmount

Feb 9/23
A E Franklin
J. E Ellis
L H Sievert

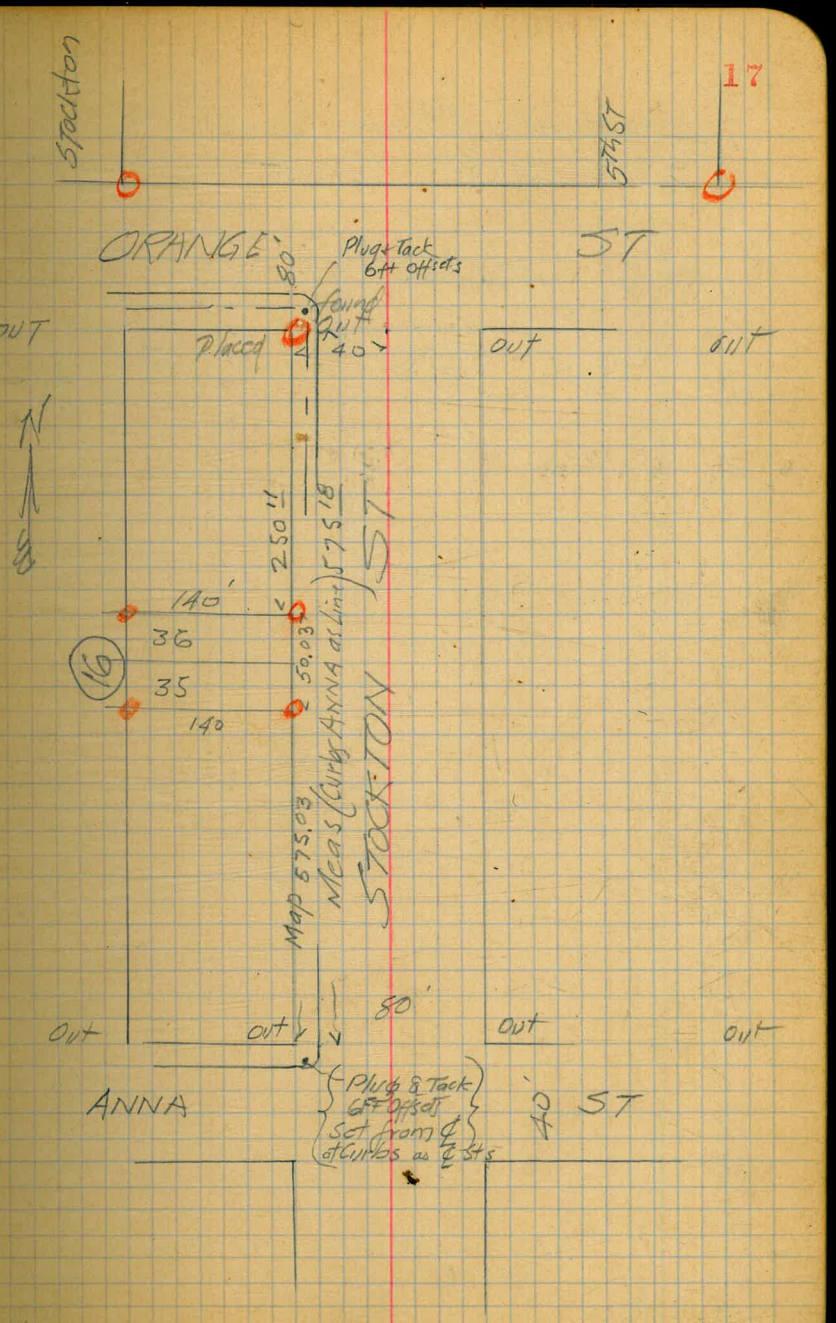


Card Indexed

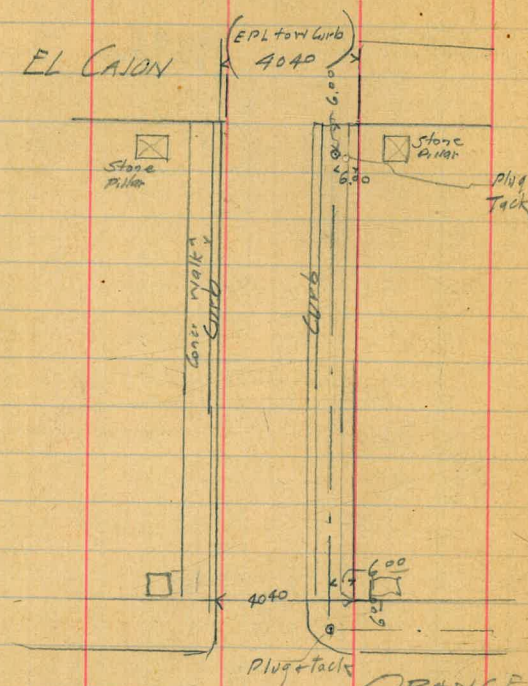
Mar 3/23
AE Franklin
JE Ellis
LH Sievert

Lot survey E.F. Bannerman
Blk 16 Lots 35 & 36 Tenalty

All Block corners out, set Cor NE Cor Blk 16 by using ℄ between curbs of Stockton thence 40' Ry as E line Blk 16 Intersected No. line (found) of Orange thence 80' South to NE Cor Block 16 A.E.F.



Lot Survey Clarence Palmiter { Permit
Lot 9 Block J Teralta { No 132

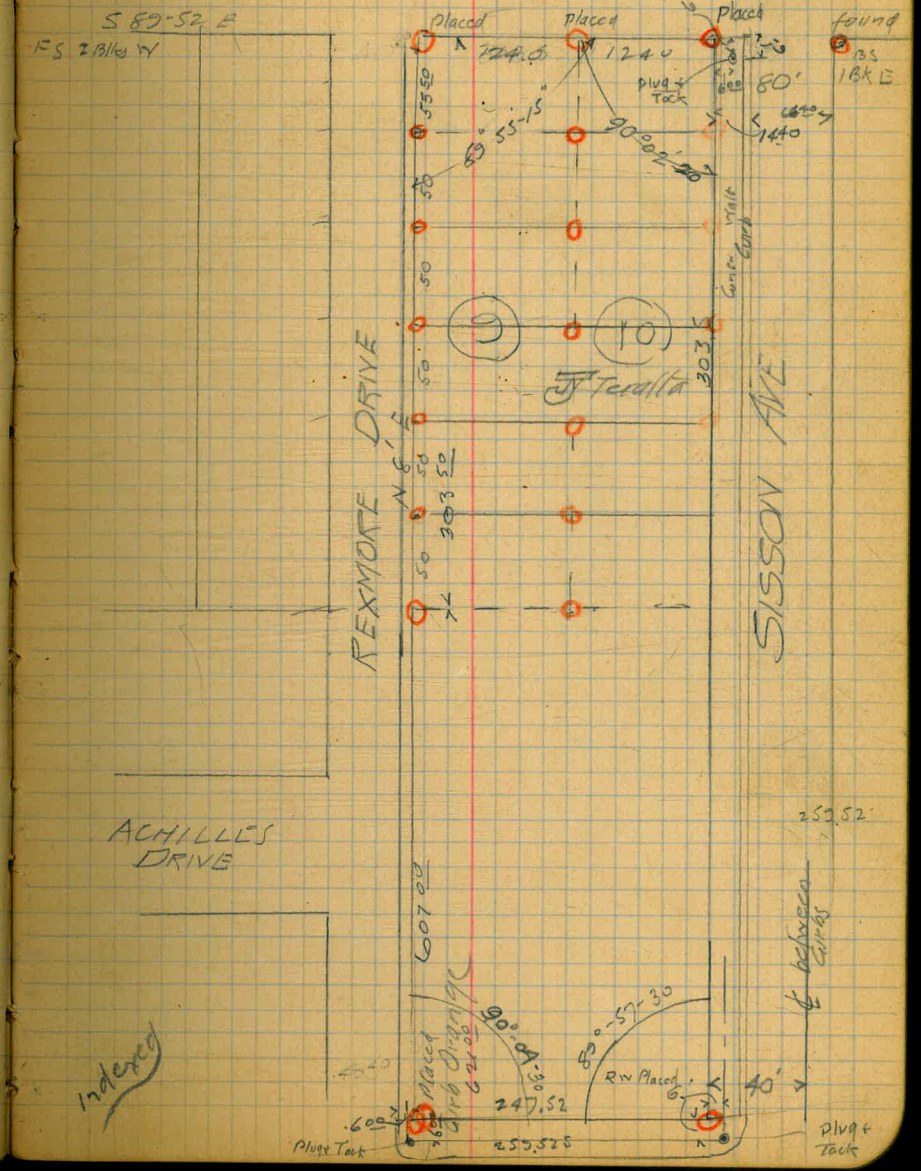


7
2-20

90-04-45

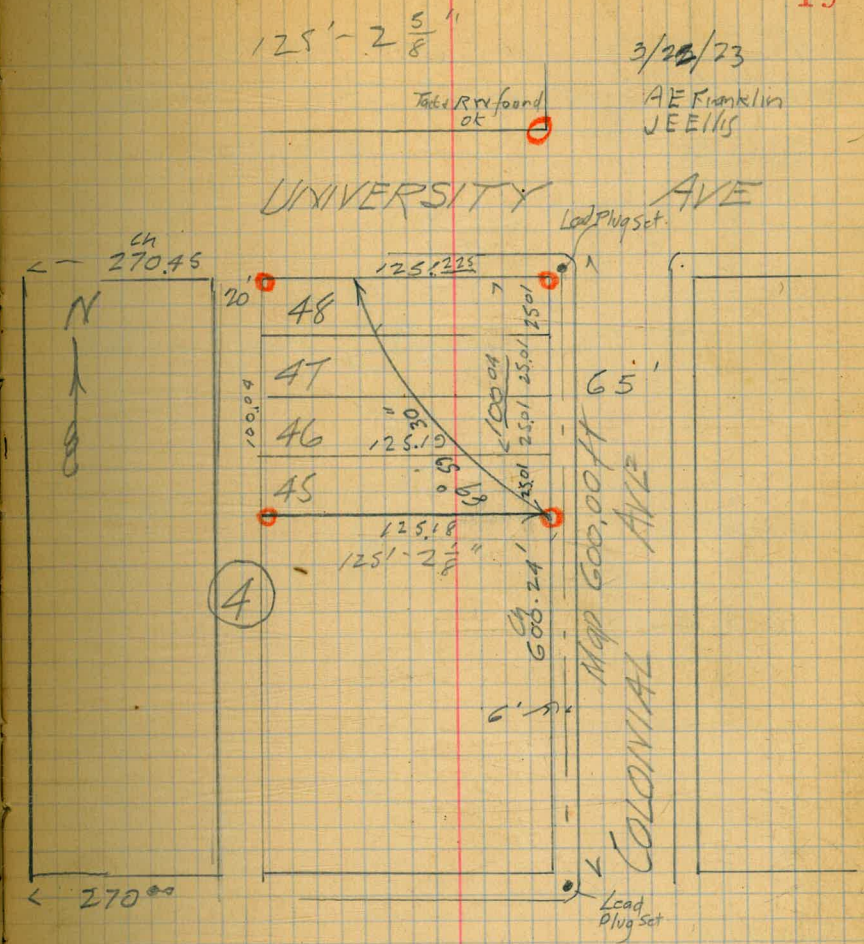
80-55-15
90-02 20
89 57 30
90-04 30
358-118 95
359-59 35

3/10/23
AE Franklin
JE Ellis
LH Sievert



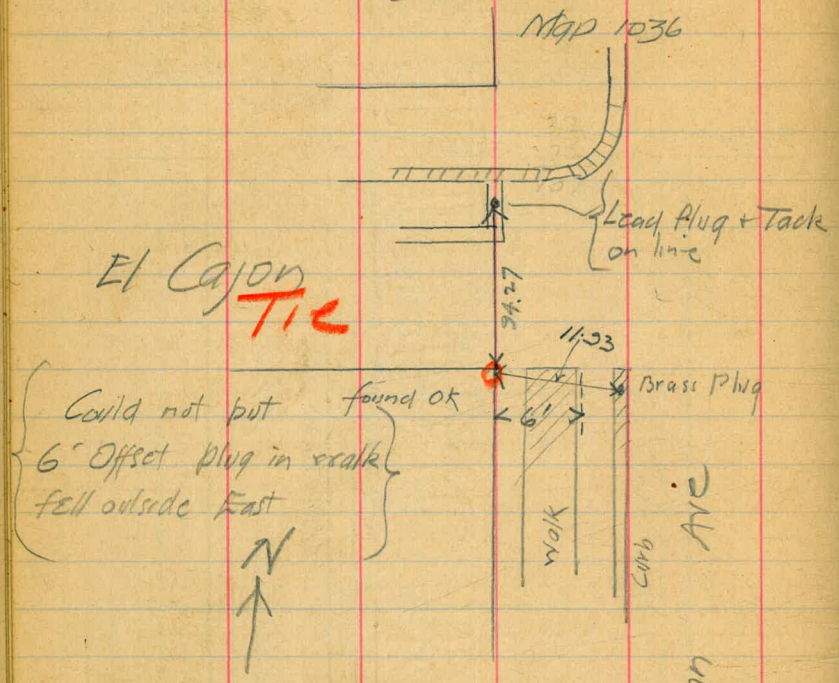
Lot Survey A A Carpenter
Permit #140 Lots 45-48 Block 4 CH Amy #1

3/22/23
AE Franklin
JE Ellis

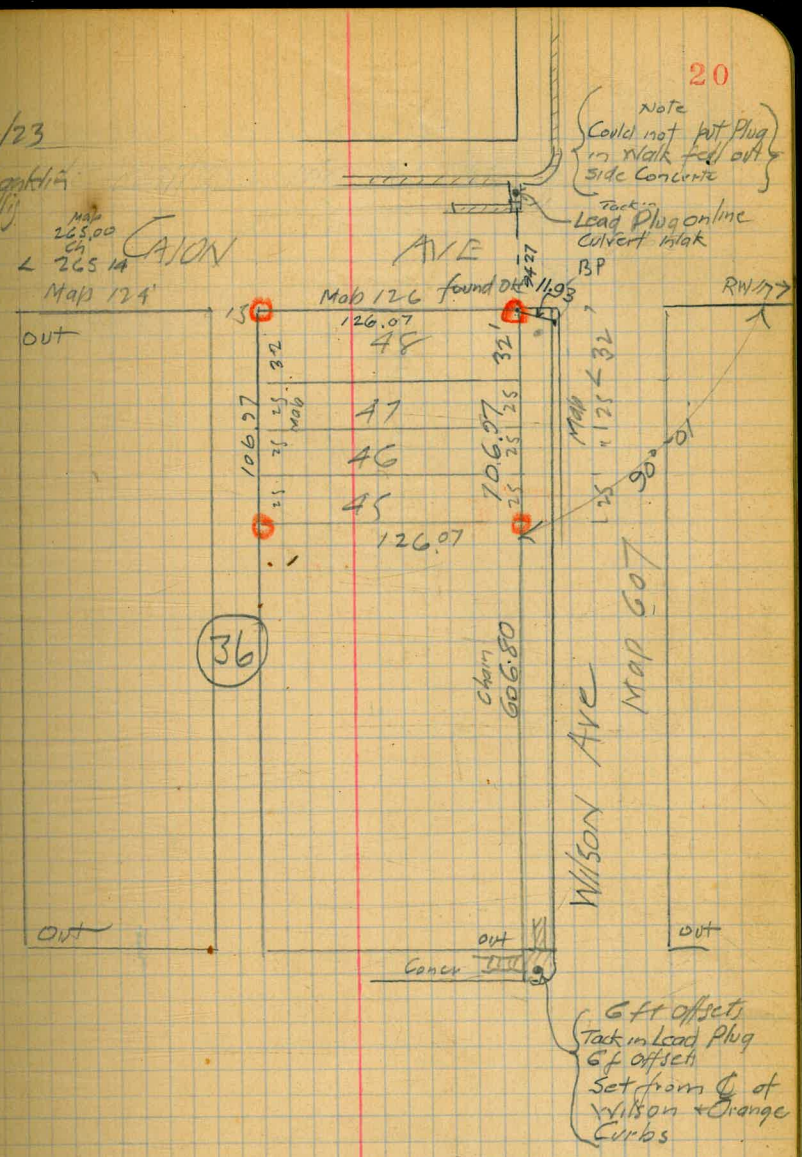


Indexed

Lot Survey H Frank Harmon
Permit #143 Lots 45-48 Teralta Blk 36



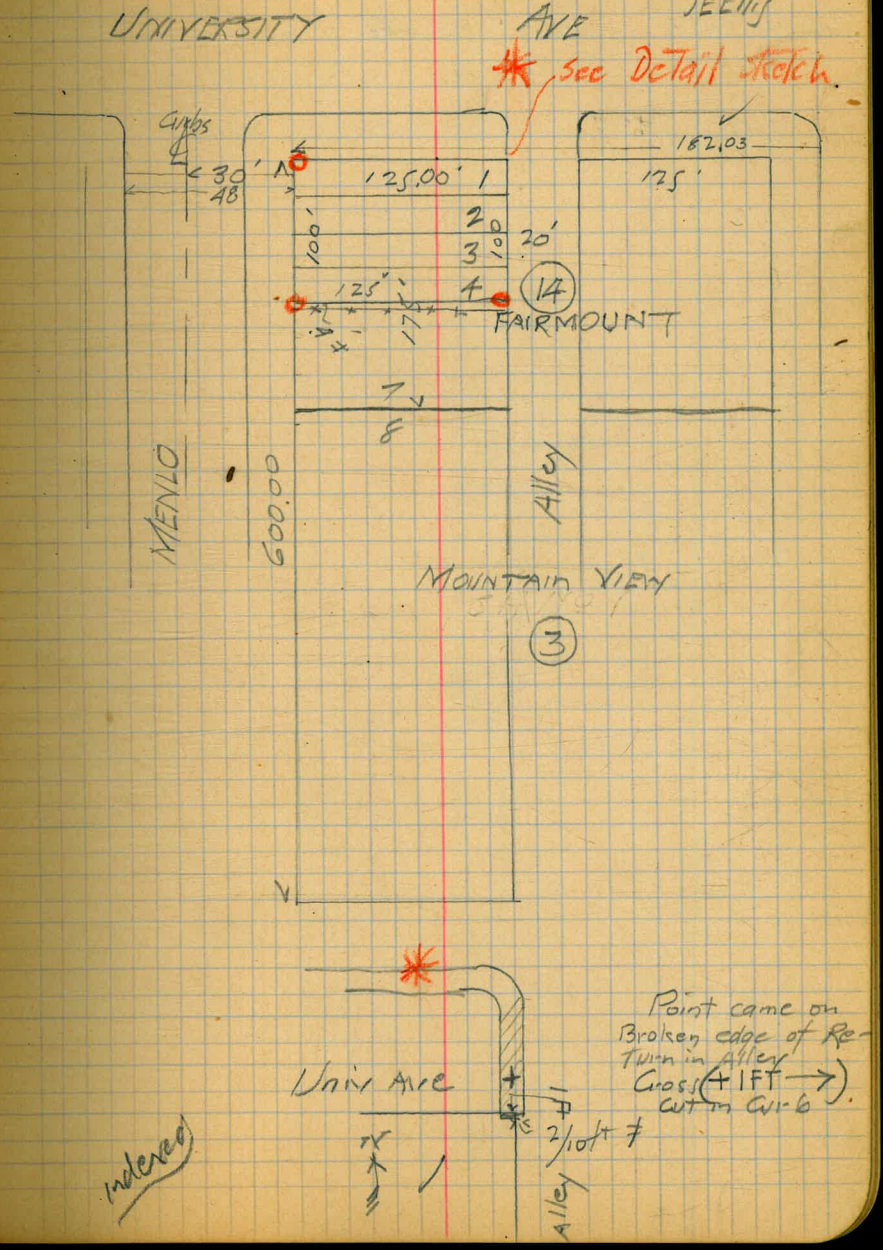
3/24/23
AE Franklin
J E Ellij



Indexed

Lot Survey East San Diego Lumber Co
Lots 1-2-3-4 Blk 14 Fairmount
SE Cor Univ. & Menlo Aves
Permit #147

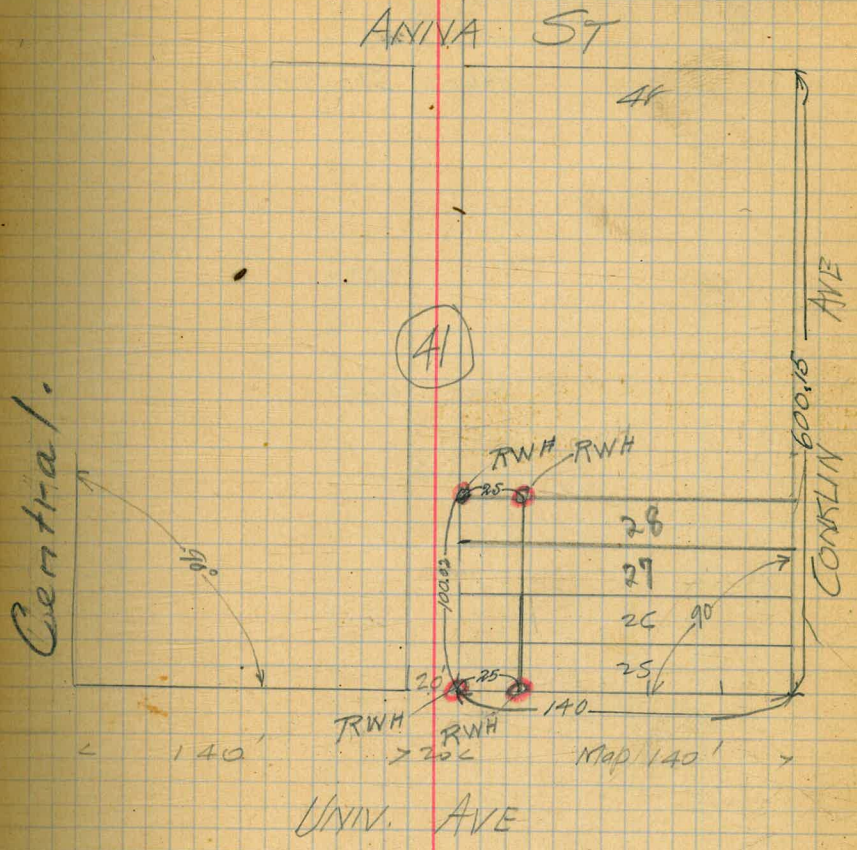
3/26/23
A.E. Franklin
J.E. Ellis



Lot Survey Harry G Truax
Permit # 154 Lots 25 to 28 W 25' of
Block 41 City Hghts
Univ Ave Betw. Conklin & Central

13,5

4/11/23 Time 3hr Weather Cloudy
J.E. Ellis
C.S. Kelley



Indexed

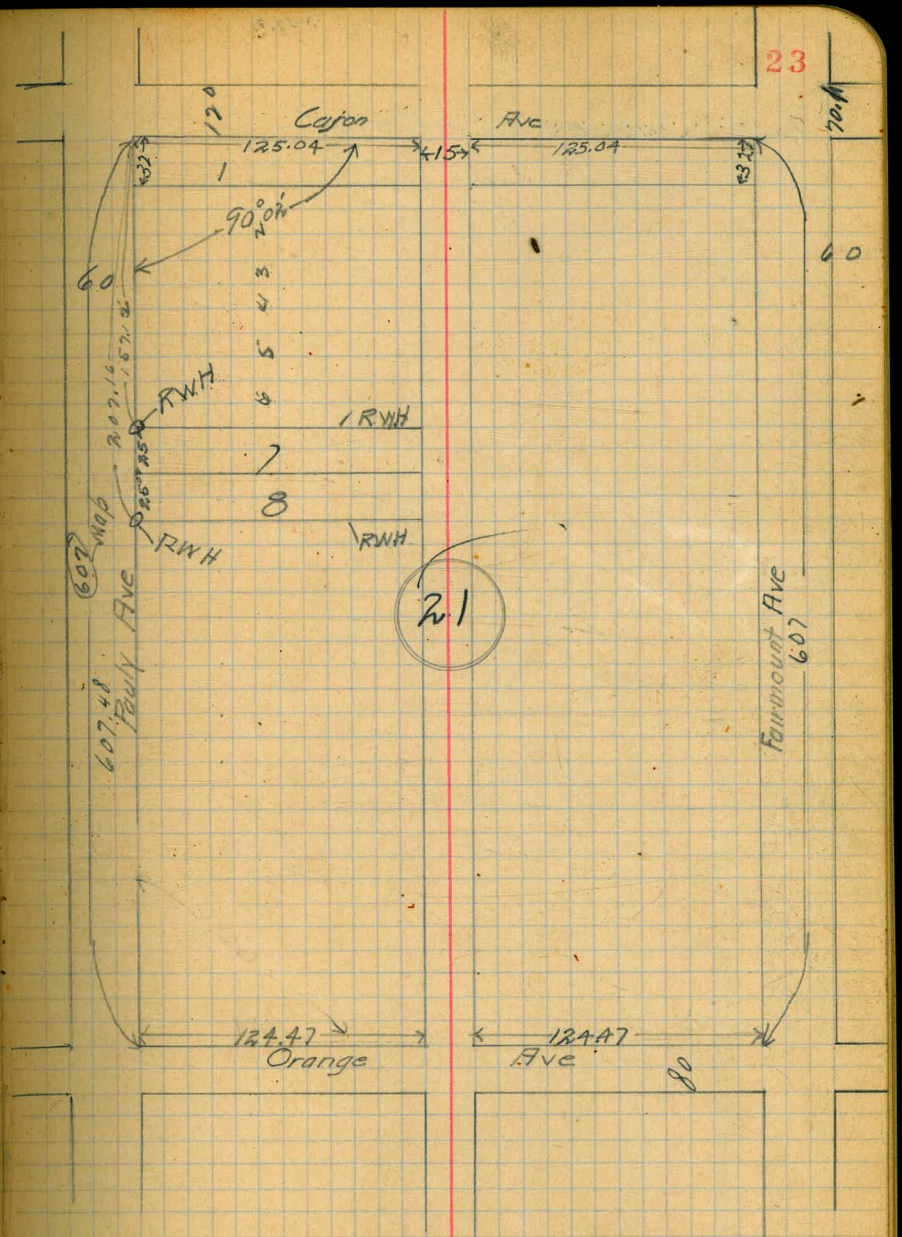
Staked By
J.E. Ellis
C.S. Kelley

4/16/23

Lot Survey of

Lots 7 and 8

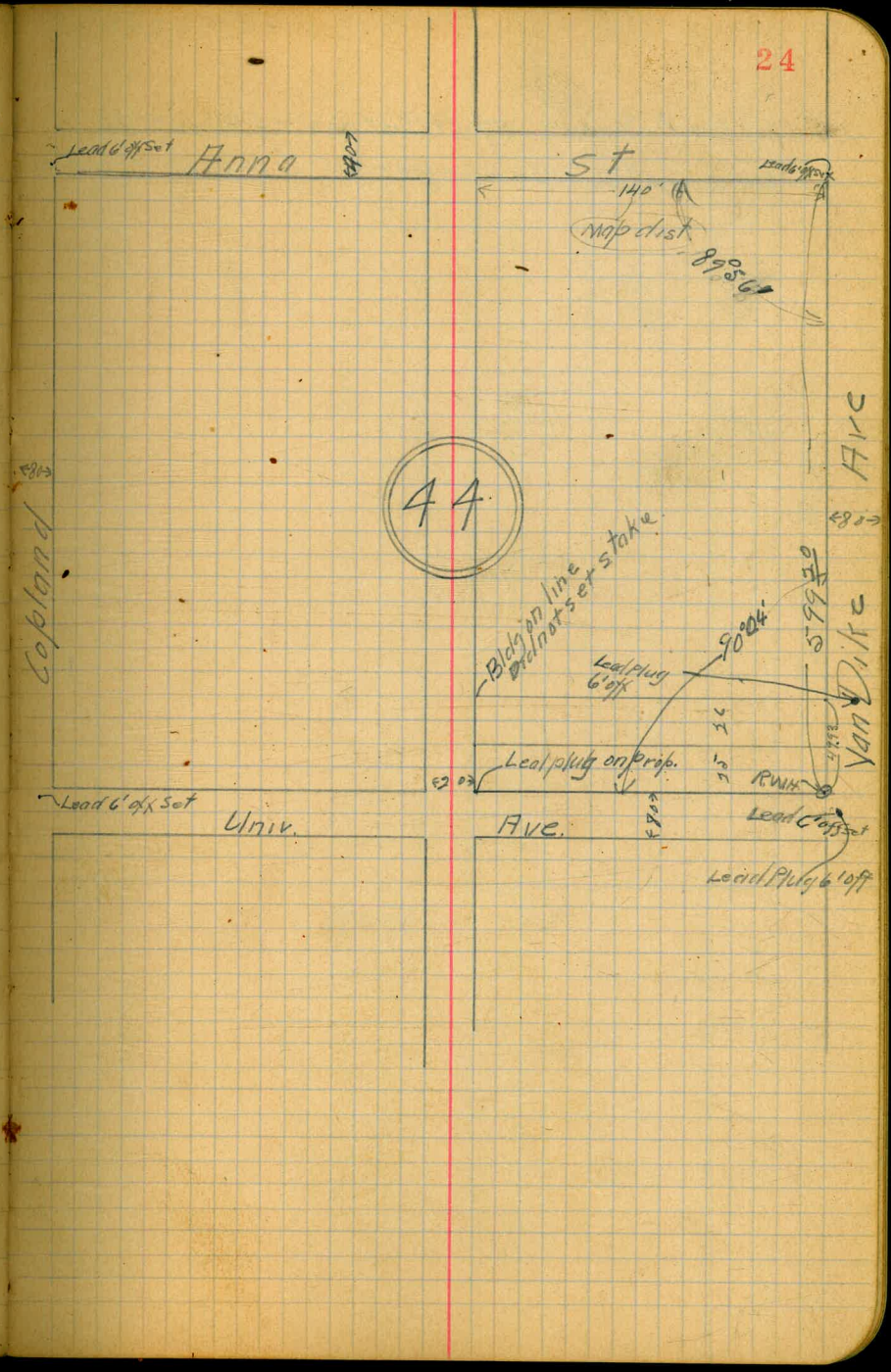
Block 21 Teralta



May 8, 1923
Ellis Kelley

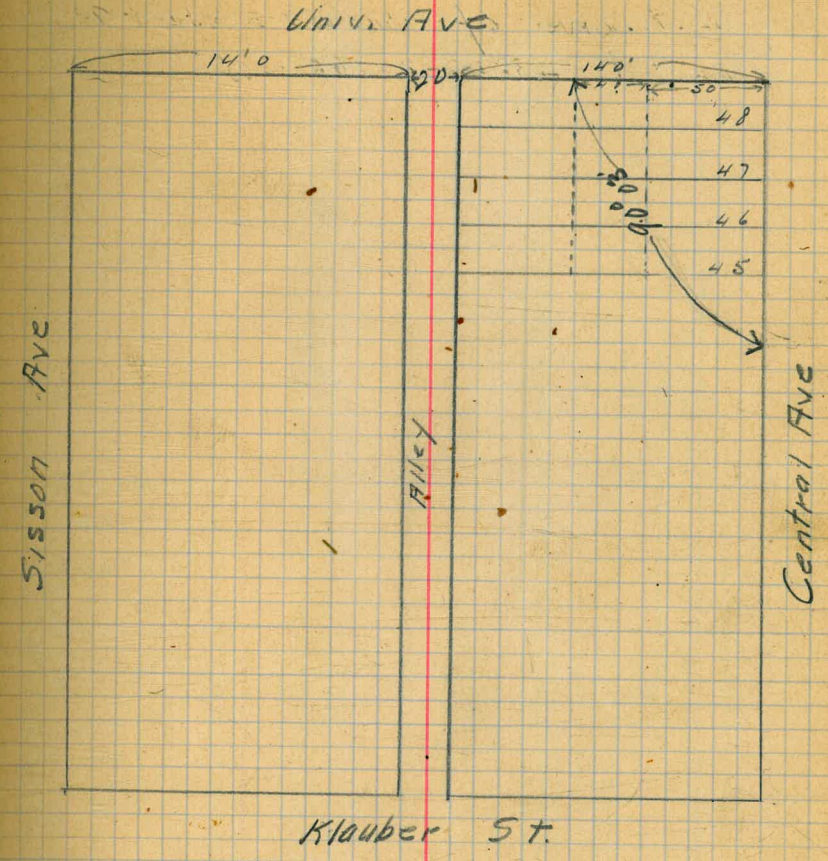
Weather. Hot

Lot Survey of Lots 25 + 26 Block 44.



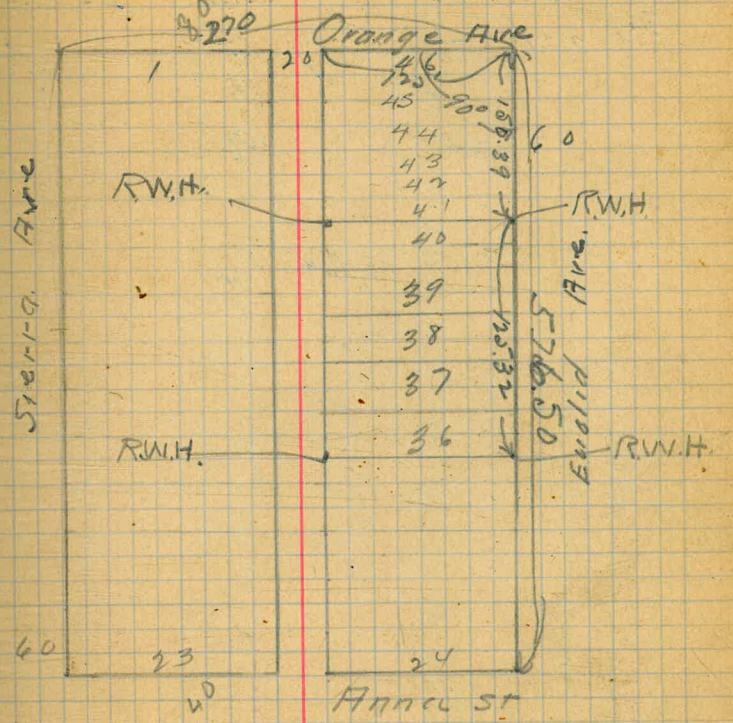
5-23-23

Lot Survey of East 40' of West 90' of Lots 48-47-46-45 - Block 5 3 C.H.



June 6-1923
Ellis
Walker
Preston

Lot Survey of Lots 36-37-38-39-40
Block 3 Chester Park



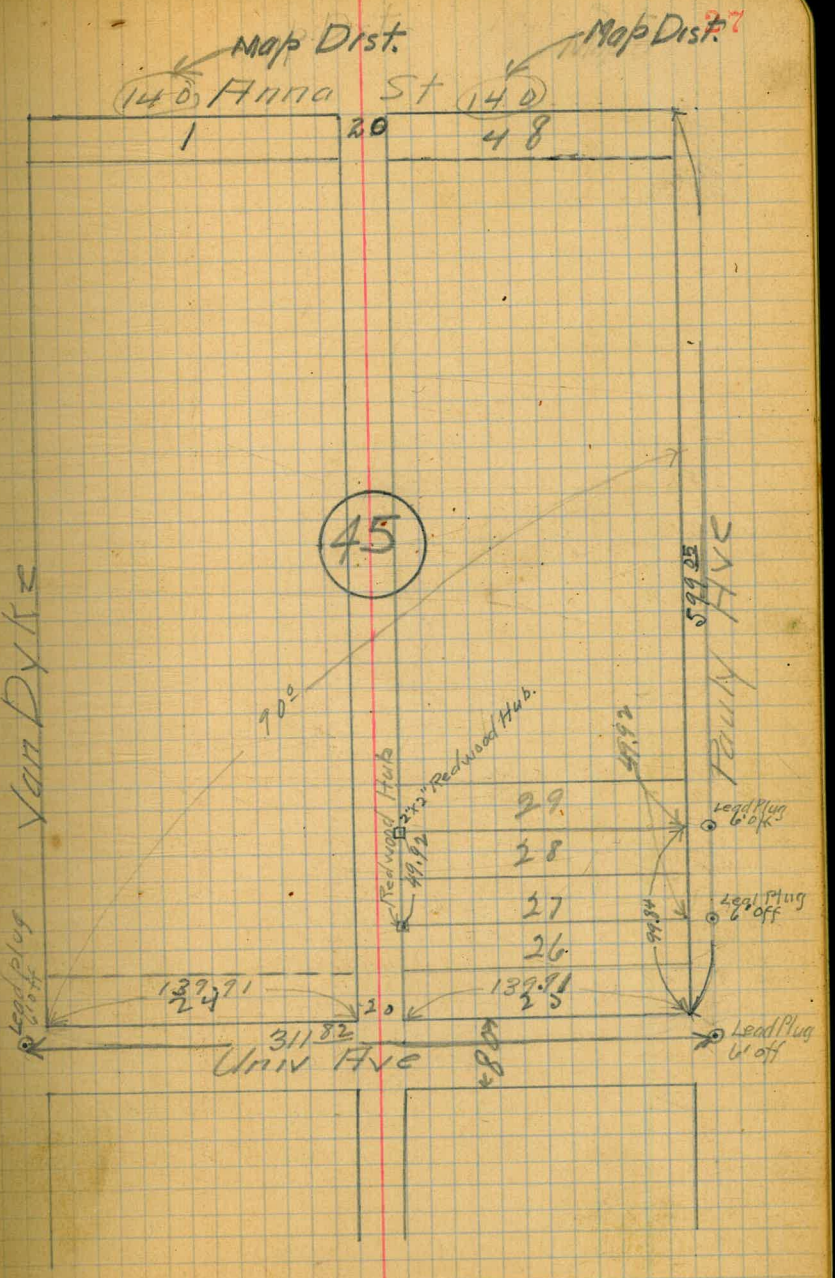
Ellis
Walker
Treston

June 15-1923

Lot Survey of Lots 25-26-27-28
Block 45 City Hights

99.84
49.92

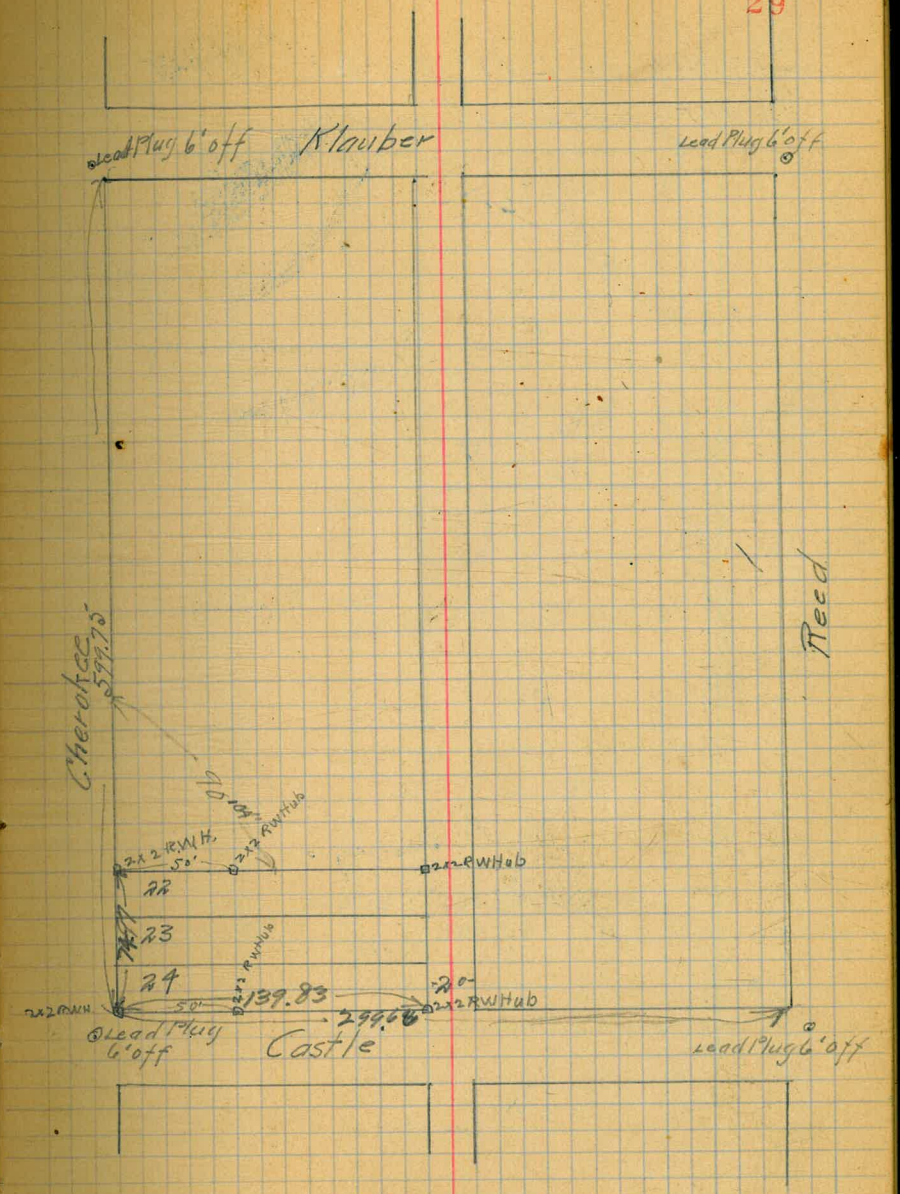
139.91
6
49.91



7-24-23

Lot Survey of Lots 22-24 Block 64 City Heights
For M.R. Essery

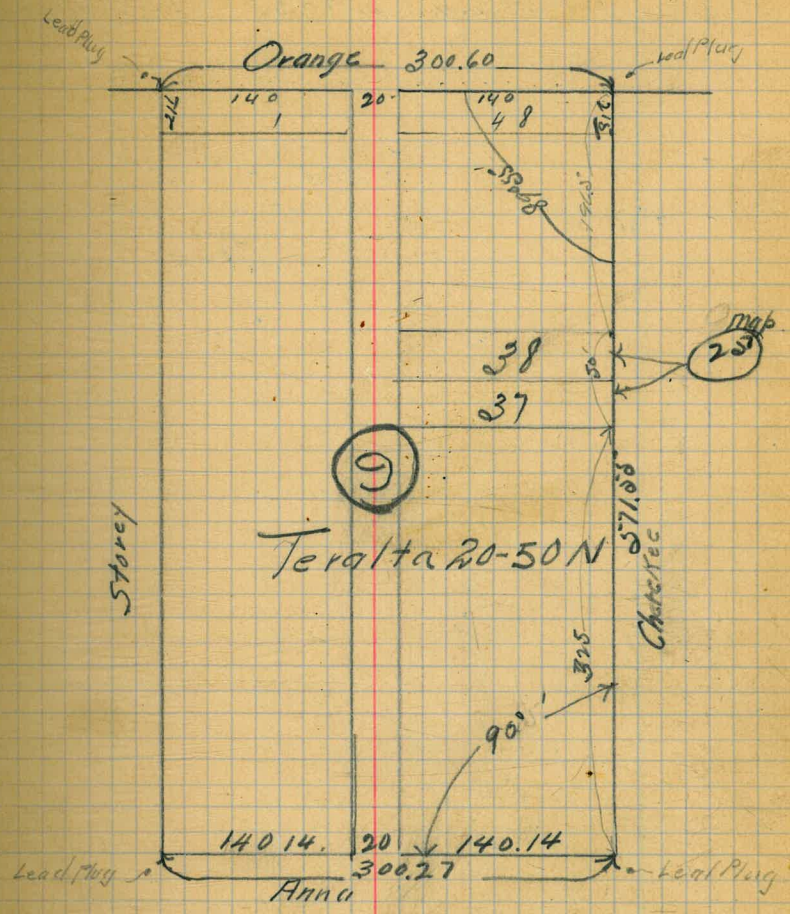
Ellis
Walker
Sack



8-16-23

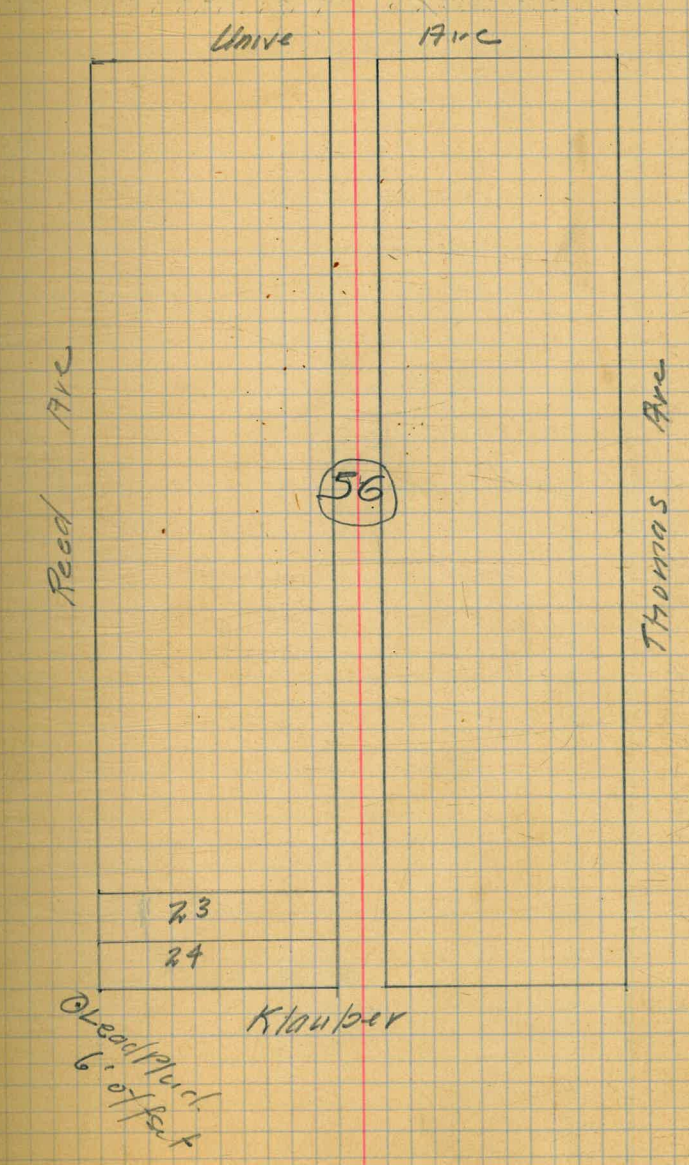
Survey of Lots 37-38- Blk 9
Teralta 20-50 N

Ellis
Walker
Steck



Lead Plugs set 6' offset at all 4 Corners

Lot Survey Block 56 - Lots 23-24 CH



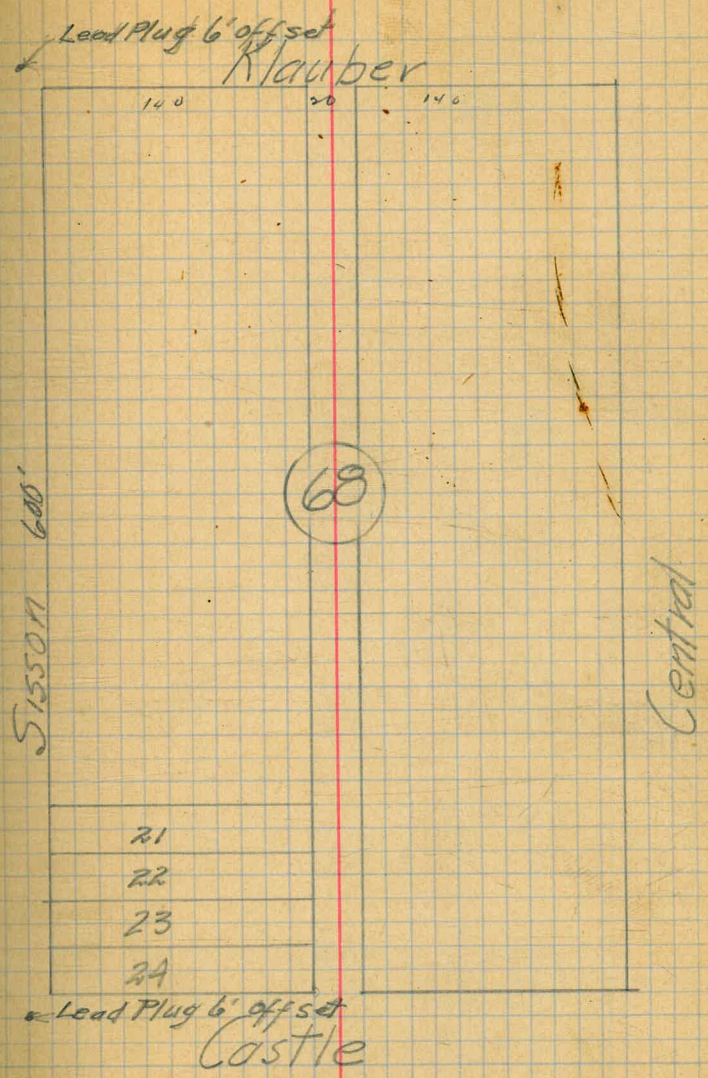
Lot Survey of Lots 21-24 Blk. 68 C.H.

Weather D. - Cold

Ellis
Walker
Preston

12-13-23

32



Moore
9-29-39.

Oil Pav. Elev.

Indexed
C.S.K.

Xsec of Hilda beg. at Dorcas

						LT	℄	RT
8						80.1 / 8.1 / 8	80.0 / 8.2	79.6 / 8.6 / 12
T.P.	11.61	88.21	0.15	76.60			88.21	
7+69.22	FC of 180° Curve					76.6 / 0.2 / 9	76.6 / 0.2	76.2 / 0.6 / 10
7+13.48	PRC on LT					73.2 / 3.6 / 15	72.2 / 4.6	71.4 / 5.4 / 11
6+71.04						69.9 / 6.5 / 15	68.5 / 8.3	67.5 / 9.3 / 11
6+21.95						64.0 / 12.8 / 15	63.2 / 13.6	62.4 / 14.4 / 11
5+72.87 = on Ely Dorcas Sec 1544 Center of 180° Curve						57.5 / 19.3 / 6	57.4 / 19.4	57.3 / 19.5 / 14
B.M. ℄ Hub	0.39	76.75		76.36	1544-7		76.75	

10 + 02.2N P.O.C.

9 + 77.48

T.P.	11.9N	111.9N	0.3N	100.00
9 + 52.75	B.C.			
9 + 25				
8 + 94.22				
8 + 69.22				
T.P.	12.43	100.32	0.32	87.89
8 + 49.22	B.C. to L.T.			

88.21

L.T.	℄	R.T.
104.6 / 7.8 / 4	104.3 / 7.6	107.5 / 8.4 / 14
102.7 / 9.2 / 4	102.8 / 9.4	101.8 / 10.1 / 13

111.9N

100.3 / 0.0 / 17	100.1 / 0.2	98.3 / 1.0 / 13
97.6 / 2.7 / 9	97.2 / 3.1	96.5 / 3.8 / 12
94.2 / 5.6 / 15	93.4 / 6.9	92.8 / 7.5 / 12
91.3 / 9.0 / 15	89.9 / 10.4	89.4 / 10.9 / 11

100.3N

87.5 / 0.7 / 10	87.0 / 1.2	86.6 / 1.6 / 11

88.21

12+86.98 PRC of 180° Curve

+71

17+89.52

+92.04

+44.60

11+25

+97.14

10+49.68

111.92

LT		℄	RT	
105.96	104.91	105.4	104.92	105.95
5.96	7.01	6.5	7.00	5.97
cb 15	15		15	15 cb
	90T		90T	
105.95	104.92	105.5	104.93	106.00
5.97	7.00	6.4	6.95	5.92
cb 15	15		15	15 cb
	90T		90T	
105.9		106.2	105.6	
6.0		5.7	6.3	
12			12	
106.9		107.1	106.7	
5.0		4.8	5.4	
15			12	
108.9		108.5	107.9	
3.1		3.4	4.0	
15			12	
109.1		108.7	108.1	
2.8		3.2	3.8	
15			12	
108.3		108.3	107.5	
3.6		3.6	4.4	
14			12	
102.1		106.7	105.9	
4.8		5.2	6.0	
15			12	

111.92

N E Cor. Hilda & Monitor
Upper Deck

#7 B.C. on Lt				
#6				
T.P.	12.01	122.19	1.74	110.18
#5				
#4				
#3				
#2				
#1				

Curve in 7 Parts
10+02.22 = P.O.C Beg. upper deck of N E Cor. Hilda & Monitor

111.92

Indexed
C.S.K.

℄	RT		
110.8 / 11.4	110.6 / 11.3 / 2	112.7 / 9.5 / 7	112.8 / 9.4 / 18
106.5 / 15.7	110.8 / 11.4 / 9	110.9 / 11.3 / 20	

122.19.

106.5 / 5.4	109.3 / 2.6 / 10	109.2 / 2.7 / 21
106.0 / 5.9	108.4 / 3.5 / 10	108.3 / 3.6 / 21
105.8 / 6.1	107.8 / 4.1 / 11	107.9 / 4.0 / 22
105.1 / 6.8	107.3 / 4.6 / 13	107.4 / 4.5 / 22
102.7 / 9.2	106.8 / 5.0 / 12	107.0 / 4.9 / 23
104.3 / 7.6	104.6 / 7.3 / 4	106.5 / 5.4 / 10	106.6 / 5.3 / 20

111.92

XSEC ON MONITOR.

from end of New Cb to Hilda

00 = End curve of 20 R NW Cor Hilda & Monitor

0+25

0+50

T.P. 0.20 110.17 12.22 109.97

0+75.4 = B.C.

1+00

1+29.6

1+39.6

Sta. backed up

122.19

LT	℄	RT
98.0 / 12.2 / 11	98.7 / 11.5	98.9 / 11.3 / 5
102.2 / 8.0 / 9	102.5 / 7.7	102.7 / 7.5 / 4
106.2 / 4.0 / 9	106.5 / 3.7	106.6 / 3.6 / 2
	110.17	
110.3 / 11.9 / 9	110.8 / 11.4	111.0 / 11.2 / 2
114.9 / 7.3 / 10	115.0 / 7.2	115.5 / 6.7 / 15

120.25 / 1.94 / 15 cb end	119.89 / 2.30 / 9 UT	120.3 / 1.9	119.74 / 2.45 / 9 UT	120.14 / 2.05 / 15 cb end
121.94 / 0.25 / 15 cb	121.44 / 0.75 / 15 / 9 UT	122.19 / 0.0	121.64 / 0.55 / 15 / 9 UT	122.12 / 0.07 / 15 cb

122.19

				LT	RT
check to B.M.			11.28	76.35	76.36
T.P.	1.58	87.63	12.41	86.05	
Center of Curve of NWly Cor Hilda & Monitor					
T.P.	0.80	98.46	12.33	97.84	
		110.17			

$\frac{92.8}{5.9}$ $\frac{93.0}{5.7}$

98.66

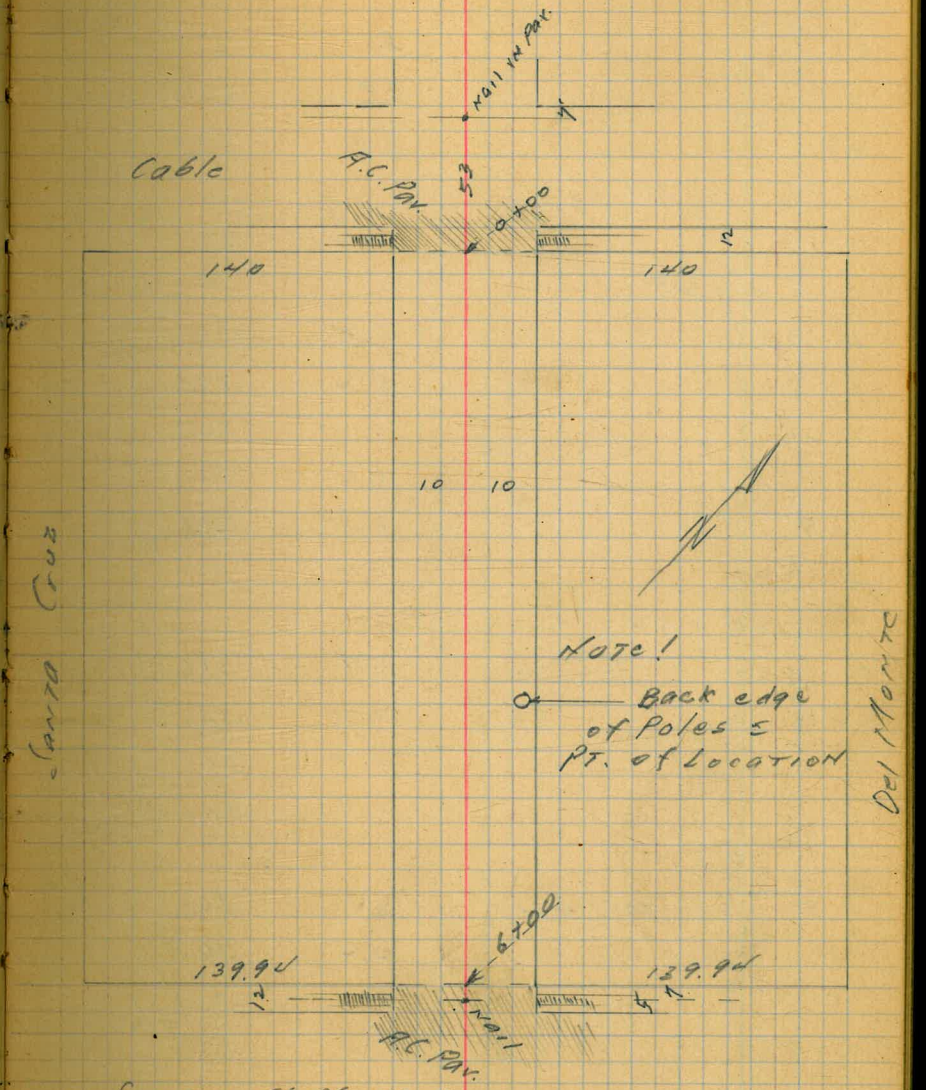
Indexed
C.S.K.

Moore
9-29-39

X sec Alley 20' wide
Blk 49 Ocean Beach
Bet. Del Monte & Santa Cruz
from Cable to Sunset Cliffs Blvd.

S.E.B.P.	10.21	35.37	25.11	Del Monte Cable
0-12 E c6				
N Pav		10.24	24.88	
S "		(10.37)	25.00	
0+00 Ely Cable				
S c6		9.43	25.89	
S Pav		9.63	25.69	
C "		10.12	25.20	
N "		9.51	25.81	
N c6		9.37	25.95	
0+3				
N		6.6	28.7	
+2		7.6	27.7	
+5		9.3	26.0	
C		9.4	25.9	
+8		8.8	26.5	
S		7.2	28.1	
0+14				
S		5.4	29.9	
+2		7.5	27.8	

Notes Reduced 10-3-39 CBH
and platted # 2377



35.37

C	8.1	27.2
+5	7.7	27.6
+7	5.9	29.4
+9.8 12" Tel Pole		
N	5.6	29.7
0+25		
N	5.7	30.1
+3	5.N	29.9
+6	6.6	28.7
C	6.6	28.7
+8	6.5	28.8
S	4.7	31.1
0+50		
S	3.7	31.6
+N	4.7	30.6
C	4.8	30.5
N	4.9	30.4
0+70		
−5 Sm. gar. dirt	4.4	30.9 ✓
N	4.4	30.9
C	4.N	31.1
S	4.0	31.3

0+80 C +9.3 14" P. Pole on S.

35.37

40

		Ele.
1+00		
S.	3.6	31.7
C	3.7	31.6
N	4.1	31.2
1+24		
C +9.5 12" Tel. Pole on N.		
1+37		
−4.8 do. gar. dirt.	3.8	31.5 ✓
N	3.8	31.5
C	3.6	31.7
S	3.N	32.1
1+54		
S	3.1	32.2
C	3.3	32.0
N	3.0	32.3
+1 Sm. gar. conc.	N.83	32.49 ✓
1+64		
−0.7 W.L do. gar conc.	3.00	32.32
N	3.1	32.2
C	3.3	32.0
S	3.1	32.2
1+80		
S	3.0	32.3
C	3.N	32.1 ✓
N	3.1	32.2
+0.7 E.L. do. gar. conc.	3.0N	32.30

35.32

1+86

N - 0.3 Sin. gar. wood 3.10 32.22 ✓

2+00

N 2.8 32.5

C 3.0 32.3

S 2.9 32.4

2+11

C + 9.4 12" P. Pole on S

T.P. 9.40 42.02 2.90 32.42 ✓

2+41

S 9.2 32.8

C 9.1 32.9

N 9.3 32.7

+2 Sin. gar. dirt 9.4 32.6 ✓

2+50

C + 9.5 10" Tel. P. on N

2+60

N. Side

- 2.5 Sin. gar dirt 8.8 33.2

2+95

N. 8.5 33.5

C 8.7 33.3

S 8.4 33.6

+ 0.8 Sin. gar. dirt 8.2 33.8 ✓

42.02

3+00

C on M.H. Rim. 8.53 33.49 ✓

3+30

S 8.4 33.6

C 8.4 33.6

N 8.4 33.6

+4.4 Sin. gar. conc. 8.33 33.69 ✓

3+48

12" P. Pole on Line on S

3+62

- 4.2 & 3 car gar. dirt 8.4 33.6 ✓

N 8.4 33.6

C 8.3 33.7

S 8.3 33.7

3+80

- 88 do. gar. conc. 4.67 35.35 ✓

S 7.9 34.1

C. 8.2 33.8

N 8.2 33.8

4+02

C + 9.8 10" Tel. Pole on N

4+30

N 7.9 34.1

C 7.8 34.2

S 7.7 34.3

42.02

4+57

S			7.4	34.6
C			7.5	34.5
N			7.9	34.1
+1.5	5 in. gar.	wood	7.8	34.2 ✓

4+63

Fence in alley 0.9

5+00

N			6.8	35.2
+0.8	12"	fence		
C			4.3	35.7
+9.5	12"	P. Pole		
S			5.9	36.1

5+30

S			4.4	37.8
C			4.3	37.7
N			4.5	37.5

5+45

N − 5			2.0	40.0 ✓
N			2.2	39.8
C			3.2	38.8
S			3.0	39.0
+5			2.6	39.4 ✓

5+50

S			2.7	39.3

42.02

42

C			2.8	39.2
+4			2.6	39.4
N			0.6	41.4
T.P.	656	47.64	0.94	41.08 ✓

5+80

N			4.9	42.7
+4			5.5	42.1
C			6.1	41.5
S			5.8	41.8

6+00 W/L Sunset Cliff Blvd.

S	C6		3.34	44.30
S	Par		3.76	43.88
C	"		4.05	43.59
N	"		4.07	43.57
N	C6		4.04	43.62

4+14 W/L curb

N	Par.		4.58	43.06
S	"		3.73	43.91

Ch to BMBP	SE Cor Del Monte + Sunset Cliffs Blvd.	10.65	36.99	37.05

0.06 curb pushed out

Indexed
C.S.K.

Bianca St. Pav. levels
℄ 180° Curve = beg.

7

6

5

4

3

2

1 = 1st Stake South of ℄ 180° Curve

or 1.58 59.26 57.68

N/V C.B.

48.29 / 10.97	48.36 / 10.90 / 15	48.25 / 11.01 / 19
48.59 / 10.67	48.59 / 10.67 / 15	48.61 / 10.65 / 18
49.02 / 10.24 / 1	49.12 / 10.14 / 15	49.02 / 10.24 / 19
49.87 / 9.39 / 1	49.96 / 9.30 / 15	49.82 / 9.44 / 20
51.15 / 8.11 / 2	51.36 / 7.90 / 15	51.17 / 8.09 / 22
52.98 / 6.28 / 2	53.14 / 6.12 / 15	53.02 / 6.24 / 22
55.18 / 4.08 / 2	55.31 / 3.95 / 15	55.23 / 4.03 / 21

59.26

14				
13				
12				
T.P.	2.55	50.29	11.52	47.74
11 = PC				
10				
9				
8 = P.C.				
		59.26		

Mly
of

48.41	48.02	47.11
1.88	2.27	3.18
4	15	27
48.83	48.44	47.59
1.46	1.85	2.70
3	15	27
48.95	48.52	47.81
1.34	1.72	2.48
3	14	25

50.29
9

48.89	48.42	47.82
10.37	10.86	11.44
1	15	24
48.59	47.86	47.36
10.85	11.40	11.90
	15	21
48.12	48.02	47.89
11.14	11.24	11.37
	15	22
48.13	48.21	48.12
11.13	11.05	11.14
	15	20

59.26
6

21 = 20' S of N/y Weeks

20 = E.C. on N/y Weeks

19

18

17

16

15

50.29

N/y
06.

37.91 / 12.38 / 5	37.96 / 12.23 / 19	37.70 / 12.59 / 30
39.64 / 10.65 / 7	39.76 / 10.53 / 20	39.50 / 10.79 / 31
41.92 / 8.37 / 10	41.83 / 8.48 / 20	41.38 / 8.91 / 32
43.64 / 6.65 / 8	43.49 / 6.80 / 20	42.89 / 7.40 / 31
45.34 / 4.95 / 8	45.04 / 5.25 / 20	44.34 / 5.95 / 31
46.69 / 3.60 / 6	46.27 / 4.02 / 19	45.39 / 4.90 / 29
47.68 / 2.61 / 5	47.30 / 2.99 / 17	46.29 / 3.90 / 29

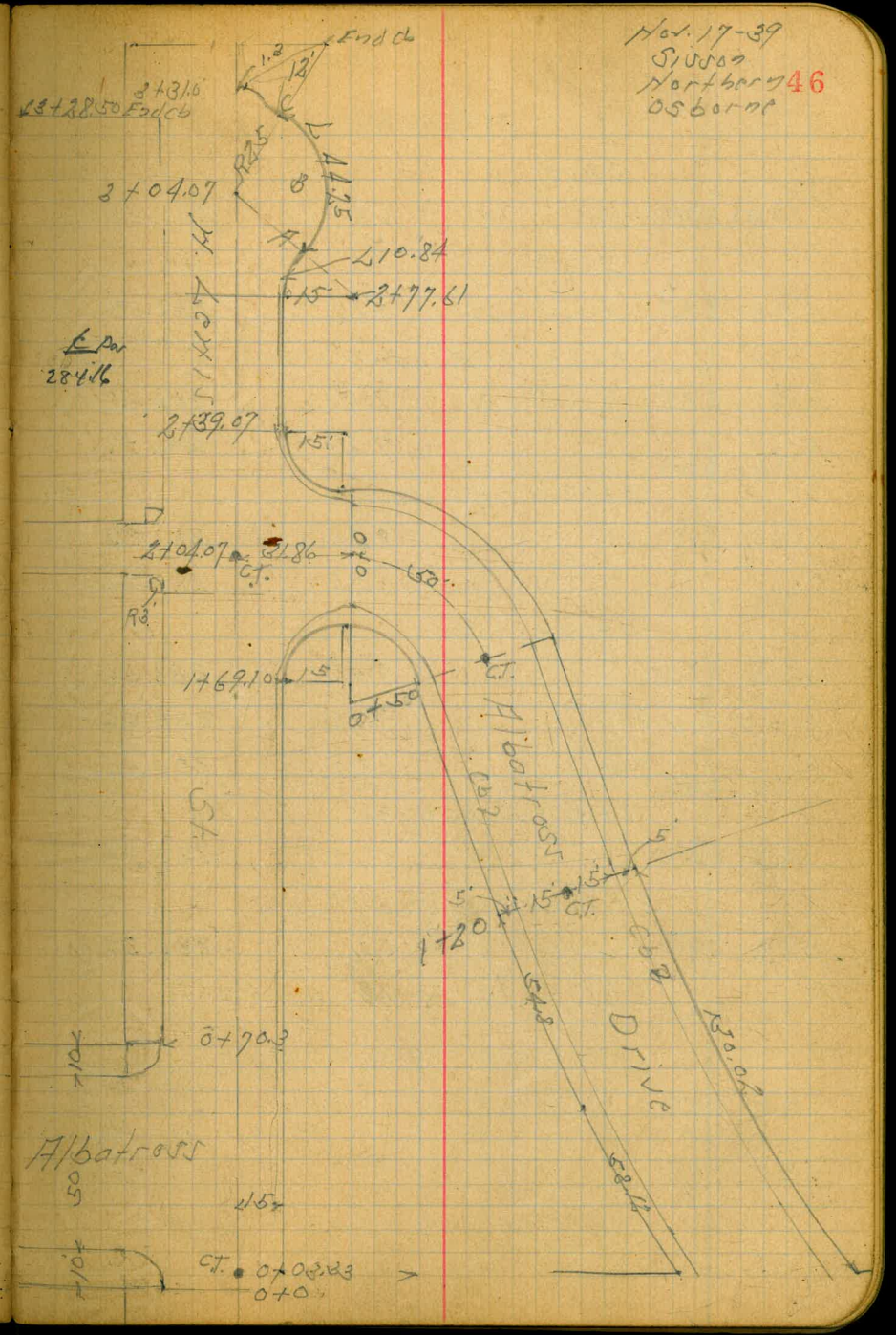
50.29

W. Lewis St & Albatross Dr. — Indexed C.S.R.

Curb Levels West of Albatross

BM	4.54	289.50	284.96	S.E.B.P. Lewis & Front
	0+0 = E.L. Albatross on S			
S Cb		5.53	283.97	
	0+0.33 = End Cb. on N			
N Cb		5.24	284.26.	
	0+10.3	5.74	283.76	
S.L. on Cb		5.57	283.93	
	0+60.3			
S.L. on Cb		5.97	283.53	
	0+70.3			
S Cb		5.94	283.56	
N Cb		5.97	283.53	
	1+0.			
N Cb		6.15	283.35	
S Cb		6.10	283.40	
	1+30			
S Cb		6.32	283.18	
N Cb.		6.28	283.22	
	1+69.10 = B.C. on N			
N Cb		6.63	282.87	
S Cb		6.58	282.92	
	1+97 = B.C. Alley Rt			
S Cb		6.67	282.83	
	2+0			
S.L. End Alley Rt.		6.79	282.71	

Reduced & Platted on profile "S" C&H. 11-18-39



Nov. 17-39
S. Sisson
Northern
Osborne

46

	289.50		
	2+15		
S.L. End Alley Rd		6.62	282.88
	2+18		
S Cb		7.15	282.35
	2+29.07 = E.C. on N		
S Cb		7.53	281.97
N Cb		7.58	281.92
	2+77.61 = B.C. on N		
N Cb		8.24	281.26
S Cb		8.25	281.25
	3+04.07 = Rad		
A		8.42	281.08
B = Δ Curve		8.84	280.66
C		9.08	280.42
	3+31 = End Cb on N		
N Cb		9.13	280.37
	3+28.50 End Cb on S		
S Cb		9.11	280.39
TP	6.88	288.52 7.86	281.64

Albatross Drive
Curb Levels

288.52		
0+0 = B.C.		
N Cb	5.92	282.60
E Cb	5.67	282.85
0+25 = Δ Curve		
E Cb	5.39	283.13
N Cb	4.91	283.61 ?
0+50 = E.C.		
N Cb	5.06	283.46
E Cb	5.01	283.51
0+85		
E Cb	4.46	284.06
N Cb	4.44	284.08
1+20 = B.C.		
N Cb	3.83	284.69
E Cb	3.83	284.69
54.8 N of B.C. on E		
E Cb	2.61	285.91
N Cb	2.79	285.73

			288.52		
	107.92' N of B.C. on E = Ely Beacon Hill Ter.				
W Cb			2.02	286.50	
E Cb			1.46	287.06	
	130.02' N of B.C. on W = Ely Beacon Hill Ter				
W Cb			1.54	286.98	
TP	4.52	292.3°	0.74	287.78	
B.M			7.34	284.96	SEBP Lewis & Frost

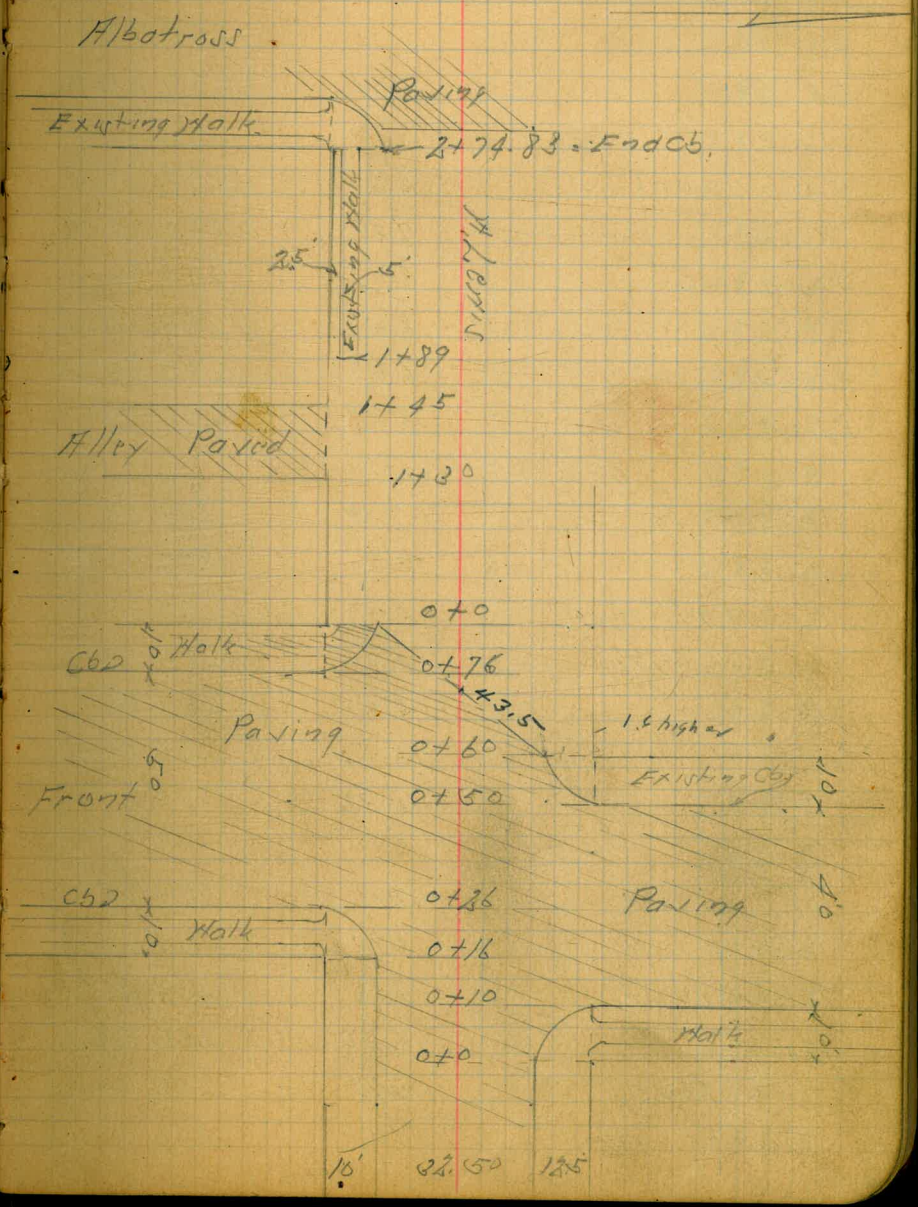
Cross Section N Lewis St.
Front to Albatross

Indexed
C.S.H.

BM	6.63	291.59	284.96	SEBP Lewis & Front
0+0 = E.L. Front From North				
S.L.		6.0	285.6	
10' N = Top Cb		6.07	285.52	✓
Gutter on Pav		6.51	285.08	✓
27.5' N " "		5.89	285.70	✓
42.5' N = Gutter "		6.06	285.53	✓
N Cb Top		5.53	286.06	✓
55' N on Conc Walk		5.29	286.30	
0+10 = E Cb From N				
S.L.		6.0	285.6	
10' N Cb Top		6.24	285.35	✓
Gutter on Pav		6.69	284.90	✓
27.5' N " "		6.25	285.34	✓
42.5' N " "		6.28	285.31	✓
55' N Cb Top		5.56	286.03	✓
Gutter		6.20	285.39	
105' N Cb Top		5.38	286.21	
Gutter		6.05	285.54	
155' N Cb Top		5.23	286.36	
Gutter		5.77	285.82	
0+16 = E.L. Front From S.				
S.L.		6.2	285.4	
10' N Cb Top		6.32	285.27	✓
Gutter on Pav		6.78	284.81	✓

Red. by & plotted on profile #596 CDH 11/24/39

Nov. 22-39
Sisson
Northern
Osborne



291.59

27.5 N on Pav		6.50	285.09 ✓
42.5 N " "		6.21	285.28 ✓
55' N " "		6.04	285.55 ✓
	0+26		
S.L. Top Cb		6.62	284.97 ✓
Gutter on Pav		7.20	284.39 ✓
10' N " "		6.93	284.66
27.5 N " "		6.43	285.16 ✓
42.5' N " "		6.09	285.50
55' N " "		5.82	285.77
	0+30 = ℄ Front From N		
S.L. on Pav.		7.19	284.45
10' N " "		6.86	284.73 ✓
27.5 N M.H. Rim		6.40	285.19 ✓
42.5 N on Pav		6.06	285.53
55' N " "		5.83	285.76
105' N " "		5.56	286.03
155' N " "		5.82	286.27
	0+50		
S.L. on Pav		7.11	284.48
10' N " "		6.94	284.65
27.5' N " "		6.66	284.93
42.5' N " "		6.55	285.04
55' N Top Cb		5.92	285.67 ✓
Gutter on Pav		6.50	285.09 ✓

291.59

105' N Cb Top		5.69	285.90
Gutter on Pav		6.29	285.30
155' N Cb Top		5.43	286.16
Gutter on Pav		5.98	285.61
	0+60		
S.L. on Pav.		7.42	284.17
10' N " "		7.32	284.27
27.5' N " "		7.05	284.54
45' N Gutter on Pav		6.54	285.05 ✓
45' N Cb Top		5.91	285.68 ✓
56' N		5.4	286.2
75' N	0+76	4.8	286.8
S.L. Cb Top		7.63	283.96 ✓
Gutter on Pav		8.18	283.41 ✓
10' N on Pav		7.82	283.77
24.1 N = M.H. Pav.		7.04	284.55
27.5 N		6.9	284.7
45' N		5.6	286.0
55' N		4.4	287.2
75' N	0+0 = M.L. Front From South	3.3	288.3
S.L.		7.3	284.3
10' N Cb Top		7.45	284.14
Gutter on Pav		7.96	283.63
27.5' N		6.5	285.1
40' N		5.6	286.0

291.59

55' N	4.4	287.2
75' N	3.3	288.3
0+03		
7.7' N of S.L. Sly Power Pole		
0+15		
S.L.	4.4	287.2
10' N	4.8	286.8
15' N	5.7	285.9
27.5' N	5.6	286.0
40' N	5.0	286.6
55' N	3.8	287.8
0+40		
S.L.	4.2	287.4
10' N	4.8	286.8
18' N	4.9	286.7
27.5' N	5.0	286.6
40' N	4.8	286.8
55' N	4.0	287.6
0+70		
S.L.	4.1	287.5
10' N	4.4	287.2
27.5' N	4.9	286.7
40' N	5.0	286.6
55' N	4.5	287.1
0+92 = ℄ 1.5 Conc Ribbon		
1.5' S of S.L.	4.11	287.48

291.59

0+97 = ℄ 1.5 Conc Ribbon		
1.5' S of S.L.	4.13	287.46
1+0		
S.L.	4.1	287.5
27.5' N	4.9	286.7
40' N	5.2	286.4
55' N	4.8	286.8
1+14 = ℄ 5.5' Conc Walk on South		
0.6' N of S.L.	3.99	287.60
1+30 = E.L. Alley		
S.L. on Conc Pav	4.88	286.71
27.5' N	4.9	286.7
40' N	5.2	286.4
55' N	4.1	287.5
1+37.5 = ℄ Alley		
S.L. on Paving	5.07	286.52
1+45 = W.L. Alley		
S.L. on Pav	4.90	286.69
27.5' N	5.1	286.5
40' N	5.3	286.3
55' N	4.8	286.8
1+47.5		
8.2' N of S.L. Sly Power Pole		
45.2' N of S.L. = N'ly Guy "		

291.59

1+89 = East End Conc. Walk on S

S.L on Ely Conc Or.	5.77	285.82
2.5' N = Sly Walk	5.77	285.82
7.5' N = Ely "	5.83	285.76
27.5 N	5.8	285.8
40' N	5.9	285.7
55' N	4.8	286.8
2+40		
S.L.	6.1	285.5
2.5' N = Sly Walk	6.70	284.89
7.5' N = Ely "	6.79	284.80
8' N = Sly Power Pole		
10' N	6.4	285.2
27.5' N	6.1	285.5
40' N	6.1	285.5
55' N	4.4	287.2
2+60		
S.L.	7.1	284.5
2.5' N = Sly Walk	7.06	284.53
7.5' N = Ely "	7.10	284.49
10' N	6.8	284.8
27.5' N	6.9	284.7
37' N	6.5	2851
55' N	4.3	287.3

291.59

2+74.83 = E.L. Albatross

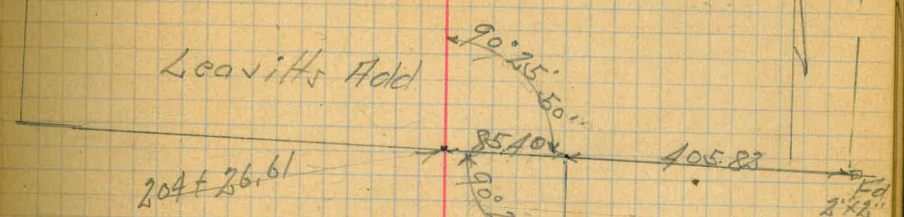
S.L on Conc. Walk	7.80	284.29
10' N = Ely Endlb.	7.52	284.07
Gutter	2.72	283
Gutter	7.7	283.9
27.5' N	7.3	284.3
40' N	7.3	284.3
55' N	5.2	286.4

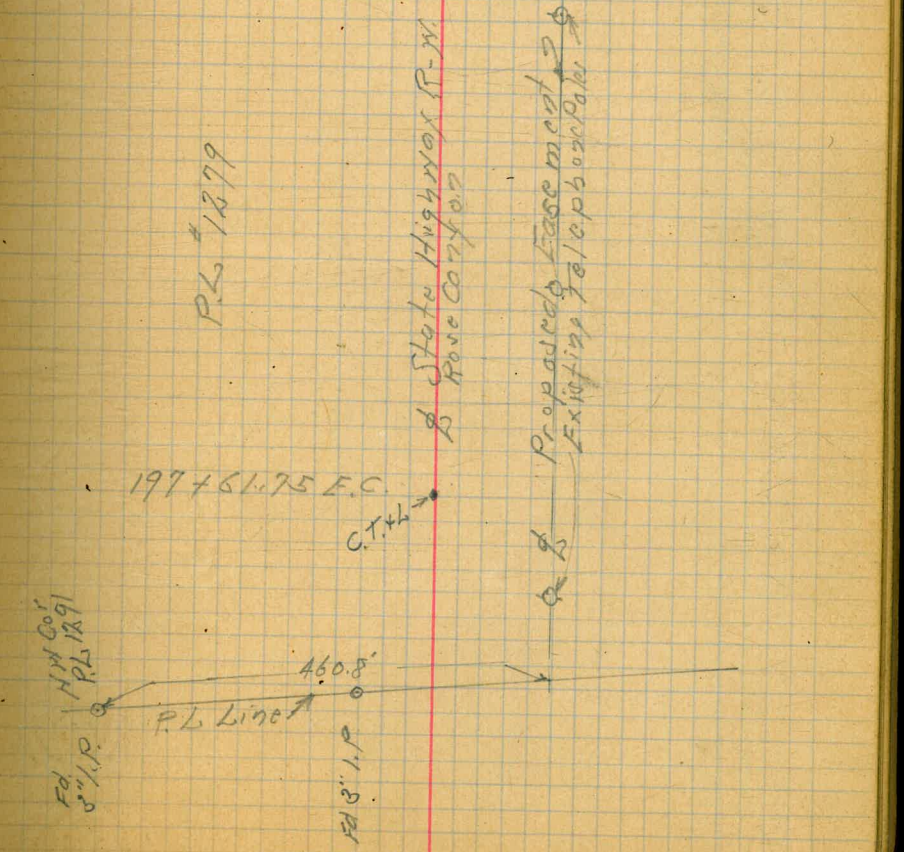
Proposed Easement in Pueblo Lot 1279
For Southern California Telephone Co.

Indexed
C.S.16

Nov 22 '89
Sisson
Northern
Osborne

53

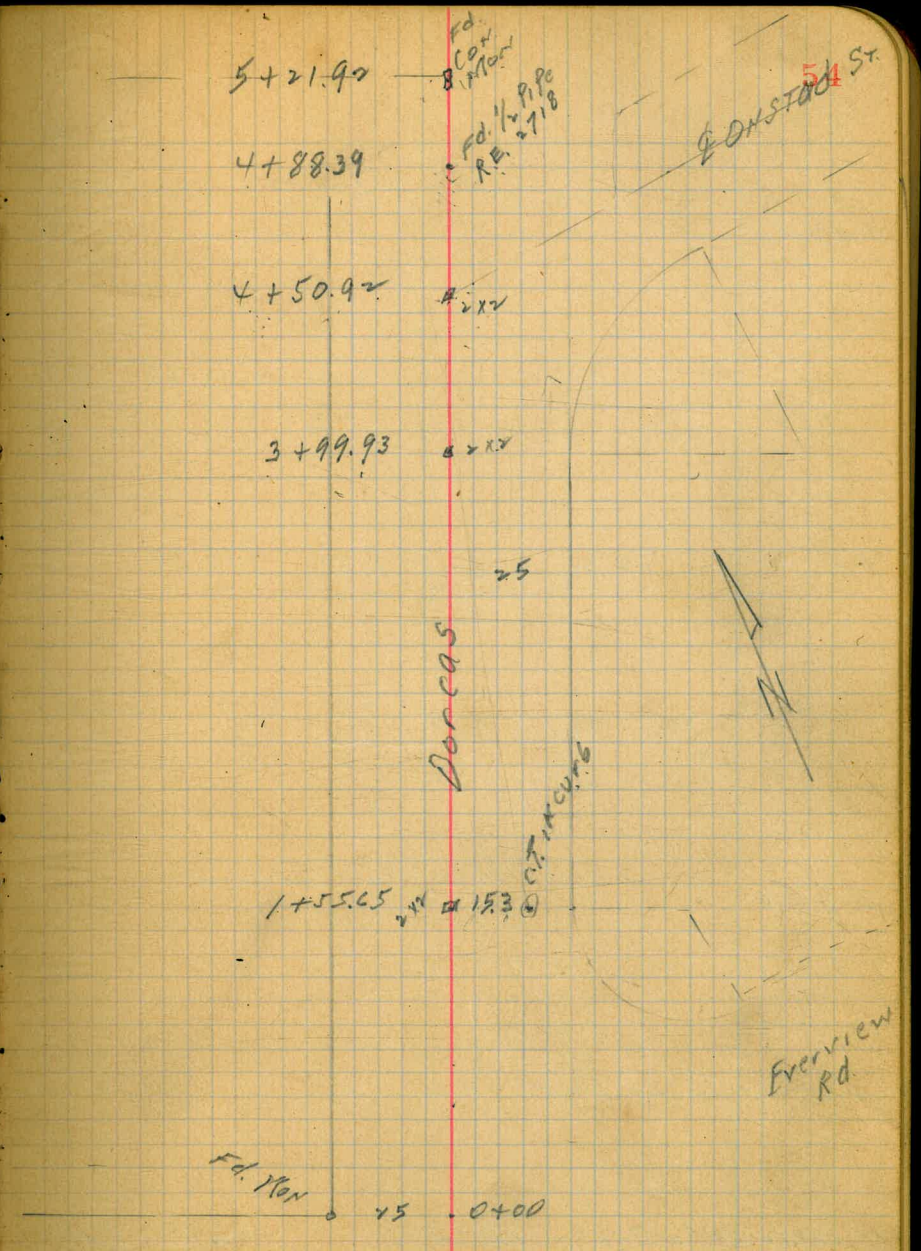




INDEXED 2-9-40
EFB

X sec of Dorcas St.
Lillian to Onstad St.

Moore
2-8-40.



1+25				
1+00				
T.P.	12.41	123.25	0.31	110.84
0+50				
0+06				
00 = N/y Lillian St.				
10+02.22 P.O.C. Hilda Rd.	7.20	111.15		103.95 E HUB

LT				℄		RT
111.3	112.3	114.0	115.2	116.1	116.7	118.4
12.0 / 5.5	11.0 / 4.5	9.3 / 2.5	8.1 / 1.2	7.2	6.6 / 1.2	5.1 / 2.5
109.5	110.2	111.4	112.3	113.1	113.4	114.8
13.8 / 5.5	13.1 / 4.5	11.9 / 2.5	11.0 / 1.2	10.2	9.9 / 1.2	8.5 / 2.5
				123.25 / 2		
104.7	105.1	105.6	106.0			
6.5 / 5.5	6.1 / 4.5	5.6 / 2.5	5.2 / 1.4	106.5	106.7	108.3
				4.7	4.5 / 1.2	2.9 / 2.5
	100.1	99.6	99.9	101.0		
	11.1 / 4.5	11.6 / 2.5	11.3 / 1.0	10.2		
	97.7	98.6	99.1	100.3	101.4	
	13.5 / 4.5	12.6 / 2.5	12.1 / 1.2	10.9	9.8 / 2.5	
				111.15 / 2		

3+50				
3				
)				
T.P.	12.44	146.69	1.16	134.25
+50				
2+00				
T.P.	12.56	135.41	0.40	122.85
1+55.65	PC on RT			
		123.25		

LT ℄ RT.

143.0

130.7 132.3 135.0 136.6 139.8 144.0 144.4 144.93 ✓
16.0 14.4 11.7 10.1 6.9 3.7 2.7 2.3 1.74
55 45 35 25 5 1 15 15 end C6

126.0 126.8 128.5 131.0 132.5 136.6 137.8 138.61
20.7 19.9 18.2 15.7 14.2 10.1 8.9 8.08
55 45 35 25 1 15 15 C6

146.69
5

121.9 123.1 124.0 125.3 126.7 129.9 131.4 132.34
13.5 12.3 11.4 10.1 8.7 5.5 4.0 3.07
55 45 35 25 1 15 15 C6

118.1 118.8 121.0 122.6 124.9 125.6 126.11
17.3 14.6 12.4 12.8 10.5 9.8 9.30
55 45 35 1 15 15 C6

135.41
5

114.6 115.1 117.2 118.9 120.2 120.5 120.94 ✓
8.7 8.2 6.1 4.2 3.1 2.8 2.31 8.11.
55 45 35 1 15 15 C6. on 40.
C. T.

123.25
5

check to BM			1.72	177.56
T.P.	9.52	179.28	0.03	169.76
35 + 21.92				
4 + 88.39				
T.P.	11.77	169.79	1.17	158.02
4 + 50.92	P.I. ℄ ONSTAD			
3 + 99.93	P.C. ON RT.			
T.P.	12.66	159.19 146.69	0.16	146.53

LT ℄ RT

57

177.64 BM BP in Cem. Porch House

N ly Cor Onstad Everview

157.7	158.7	159.8	161.51		
12.1	11.1	10.0	8.28 — on Con. Mon.		
55	45	25			
152.0	153.8	157.2	158.8	159.2	160.4
17.8	16.0	12.6	11.0	10.6	9.4
55	45	25	10		25

169.79
℄

147.7	148.7	151.3	152.7	156.9	158.0
11.5	10.5	7.9	6.5	2.3	1.2
55	45	25	10		25

137.6	38.5	140.6	143.2	147.4	150.9	151.2	152.2
21.6	20.7	18.6	16.0	11.8	8.3	8.0	6.9
55	45	35	25	3		15	25

159.19
℄

Cross Section Hawthorn St.
Felton to Gregory

INDEXED
EPB

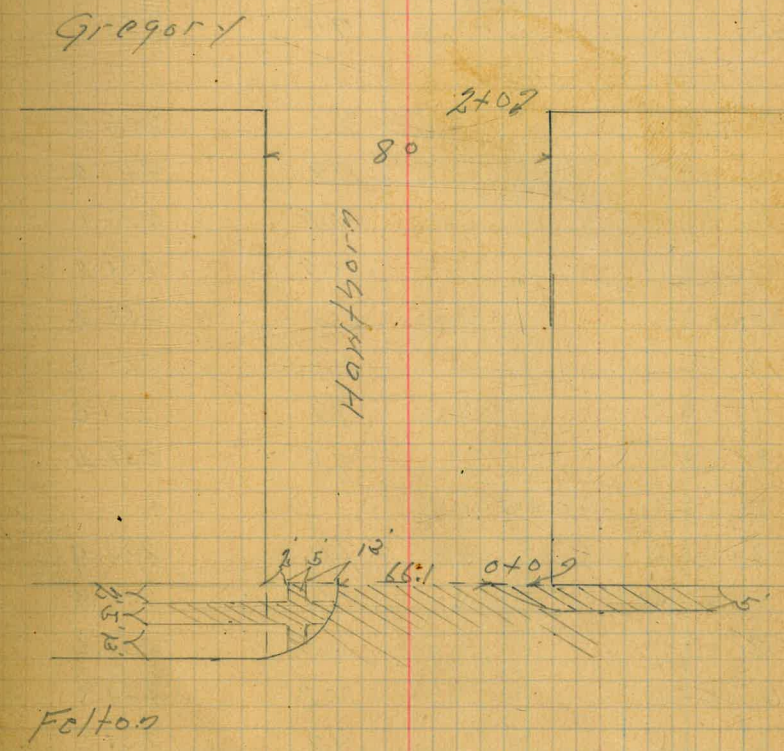
BM	6.00	261.48	255.48	SEBP Top Wall Jan Pier + Felton
	E Cb Felton From H			
H	Top Cb	10.28	251.20	
Gutter on Paving		10.91	250.57	
Cb	" "	11.23	250.25	
℄	" "	11.69	249.79	
Cb	" "	12.85	248.63	
S	" "	14.80	246.68	
	E Cb Felton From S			
S	Cb Top	14.40	247.08	
Gutter on Paving		14.85	246.63	
Cb	" "	12.90	248.58	
℄	" "	11.98	249.50	
Gutter	" "	11.65	249.83	
Cb	Top	11.09	250.39	
H	on Walk	10.13	251.35	
	0+0 = EL Felton			
H		10.1	251.4	
Cb	Top	11.14	250.34	
Gutter on Paving		11.71	249.77	
℄	" "	12.12	249.36	
Cb	" "	12.96	248.52	
+6.1	Gutter "	13.28	248.20	
+6.1	Cb Top = End	12.68	248.80	
S	on Walk	14.30	247.18	

Red + Plot 6-3-40 CBH
Profile 2139.

80' Wide
20' Cbs

May 31-40
Sisson
Northern
H Moore

58



261.48

0+3

-2		11.2	250.3
S		12.8	248.7
Cb		12.8	248.7
℄		11.9	249.6
Cb		11.2	250.3
N		9.4	252.1

0+25

N		9.3	252.2
Cb		9.9	251.6
+1		10.4	251.1
℄		10.7	250.8
Cb		11.3	250.2
+17		11.6	249.9
S		9.9	251.6
+3		9.0	252.5

0+50

-3		7.6	253.9
S		9.7	251.8
+2		10.7	250.8
Cb		10.2	251.3
℄		9.7	251.8
Cb		9.6	251.9
+2		9.1	252.4
N		9.4	252.1

261.48

0+75

N		9.1	252.4
Cb		8.7	252.8
+3		9.3	252.2
℄		9.0	252.5
Cb		8.9	252.6
S		9.5	252.0

0+92

S		8.9	252.6
Cb		8.6	252.9
℄		8.5	253.0
Cb		8.8	252.7
N		9.1	252.4

1+0

-10		13.5	248.0
N		12.2	249.3
+14		9.0	252.5
Cb		8.8	252.7
℄		7.8	253.7
Cb		8.0	253.5
+5		7.5	254.0
+10		4.1	257.4
S		4.3	257.2

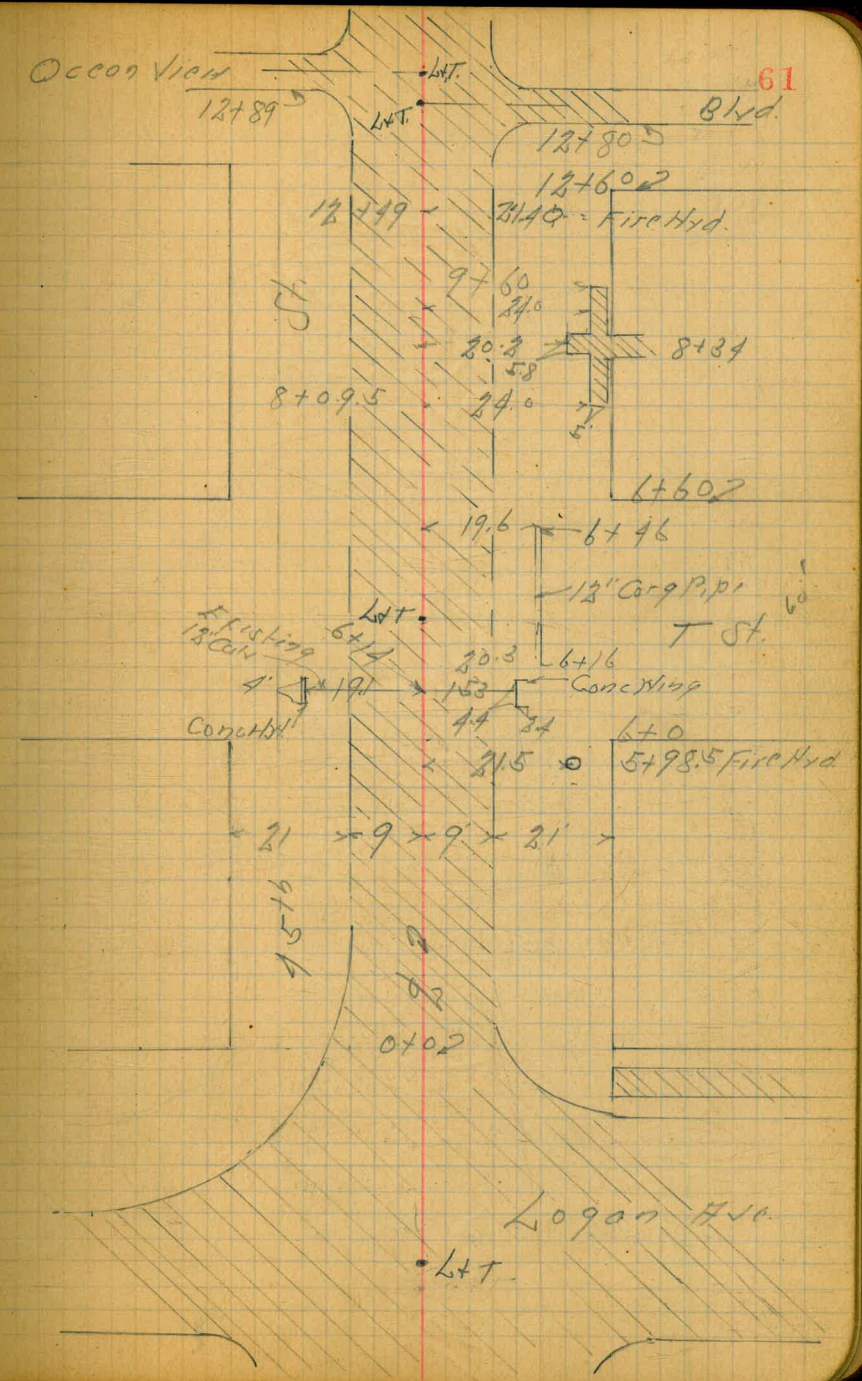
TP 0.24 257.82 3.90 257.58 Nail Pole 1+0 0750 ctr

		257.82		
	1+25			
S			2.6	254.2
Cb			3.1	254.7
+5			3.0	254.8
+15			6.5	251.3
℄			7.1	250.7
Cb			9.5	248.3
N			12.0	245.8
+15			15.0	242.8
	1+50			
-20			18.2	239.6
N			16.8	241.0
Cb			13.5	244.3
℄			11.0	246.8
Cb			9.1	248.7
S			7.4	250.4
+15			6.8	251.0
	1+75			
-15			10.5	247.3
S			11.3	246.5
Cb			13.2	244.6
TP	0.93	246.31	12.44	245.38
+5			2.3	244.0
+13			4.5	241.8
℄			5.2	241.1

		246.31		
Cb			7.4	239.9
N			9.9	236.4
+20			11.8	234.5
	2+0 = W.L. Gregory			
-20			17.8	228.5
N			14.6	231.7
Cb			11.8	234.5
℄			9.8	236.5
Cb			8.1	238.2
S			6.3	240.0
+10			5.6	240.7
TP	12.36	256.62	2.05	244.26
B.M.			1.15	255.47 S.E. B.P. Juniper + Felton 255.48

Cross Section 45th St.
Logan Ave to Imperial Ave.
Ocean View

INDEXED
EFB



Cross Section of 5th to 8th.
Logan Ave to Imperial Ave

Red. F.L.L.P. 11-2-40
Plot C.D.H. 11-6-40

0+75					
0+59 = Ely Tel. Pole 21.3 Rt.					
0+50					
0+25					
0+0 = N.L. Logan					
0-10 = HCb Logan					
0-30 = ℄ Logan					
TP	7.14	92.85	7.41	85.71	
BM	7.68	92.12		85.44	℄ 4th St. Ocean View Portland 2.5 mi.

Nov. 1-40
Sisson
Northern
Rt.-E-W Moore

62

St. W

84.2	84.4	84.8	84.15	84.79		85.61	85.85	85.6	86.1	86.4
8.7 10	8.5 30	8.1 41	8.7 19	8.06 12.5-Ep		7.24	7.00 9	7.2 15	6.8 19	6.5 30
84.0	84.2	83.9	84.47			85.80	86.70	85.6	86.3	86.5
8.9 40	8.7 30	9.0 26	8.68 19-EPav			7.05	7.15 9	7.3 15	6.6 20	6.4 30
84.05	84.46	85.97	85.92			86.61	85.5	86.1	86.2	
8.80 36-EdPav	8.39 30	6.88 8	6.89			7.24 9	7.4 14	6.8 20	6.7 30	
84.30	85.56	85.86	85.80 ✓			85.37	86.8			
8.55 50	7.29 30	6.99 16	7.05	7.48 12-EdPav		7.1 30				
84.76	85.44	85.66 ✓	85.83	85.67 ✓		85.10	85.16	85.63	85.38	86.00
8.09 50	7.41 38	7.16 30	7.02 20	7.18		7.75 20	7.69 30-Gut	7.25 30-Cb	7.49 50	6.45 80-Cb
85.27	85.29 ✓	85.20	85.03 ✓			84.97	85.22 ✓			
7.58 50	7.56 30	7.55 20	7.82			7.88 20	7.63 30			
			92.85 ✓							

2+75

2+50

2+10 = Ely To Pole 21.5 Rt ✓

2+0

1+50 = Ely Anes or Pole 21.5 Lt ✓

1+25

1+0

92.85

Lt Z Rt

84.7	84.9	84.3	84.6	86.4	86.7.1	86.81	86.75	86.3	86.5	86.2	86.5
8.5	8.0	8.6	8.3	6.5	6.14	6.04	6.10	6.6	6.4	6.7	6.4
40	30	26	20	15	9		9	15	20	30	40
84.8	84.5	84.7	86.3	86.58	86.69	86.67	86.4	86.8	86.3	87.9	
8.1	8.1	8.3	6.6	6.27	6.16	6.18	6.5	6.1	6.6	5.0	
40	30	20	16	9		9	17	21	30	40	
85.8	85.4	84.9	86.1	86.28	86.41	86.36	86.1	86.8	86.5	87.1	
7.1	7.5	8.0	6.8	6.57	6.14	6.19	6.8	6.1	6.4	5.8	
40	30	20	16	9		9	15	21	30	40	
84.4	84.6	84.5	85.6	85.65	85.97	85.97	85.9	86.0	86.4	86.4	
8.5	8.3	8.4	7.3	7.00	6.88	6.88	7.0	6.9	6.5	6.5	
40	30	22	15	9		9	15	22	30	40	
84.2	84.5	84.5	85.0	85.35	85.75	85.90	85.9	86.4	86.3	86.5	
8.7	8.1	8.4	7.9	7.50	7.14	6.95	7.0	6.5	6.6	6.4	
40	30	22	16	9.7 EP		9	16	20	30	40	
84.2	84.2	85.1	84.6	84.98	85.61	85.93	85.7	86.4	87.3		
8.7	8.7	7.8	8.3	7.87	7.24	6.93	7.2	6.5	5.6		
40	30	19	16	10.5 EP		9	16	20	30		

92.85

45th St

5+50

5+10 = Ely Tel Pole 21.5 Rt ✓

5+0

4+50

4+0

3+62 = Ely Tel Pole 21.9 Rt ✓

3+50

3+06

92.85

	Lt					℄			Rt		
	85.0	84.5	84.7	85.3	85.68	85.76	85.68	85.6	84.9	84.5	84.2
	7.9	8.4	8.2	7.6	7.17	7.09	7.17	7.3	8.0	8.4	8.7
	40	30	21	16	9		9	15	19	30	40
	86.2	86.1	84.9	85.8	85.97	86.06	85.96	85.7	85.0	84.7	
	6.7	6.8	8.0	7.1	6.88	6.79	6.89	7.2	7.9	8.2	
	40	30	22	17	9		9	19	30	40	
	87.2	86.4	85.5	86.2	86.30	86.45	86.40	86.2	86.1	85.7	
	5.7	6.5	7.4	6.7	6.55	6.40	6.45	6.7	6.8	7.2	
	40	30	20	15	9		9	21	30	40	
	86.4	86.1	85.2	86.3	86.63	86.79	86.72	86.8	87.4	87.6	87.1
	6.5	6.8	7.7	6.6	6.22	6.06	6.13	6.1	5.5	5.3	5.8
	40	30	19	16	9		9	20	22	30	40
	85.9	86.5	85.5	85.5	86.5	86.72	86.94	86.92	86.8	87.4	88.0	88.3
	7.0	6.4	7.4	7.4	6.4	6.13	5.91	5.93	6.1	5.5	4.9	4.6
	40	30	24	20	16	9		9	20	22	30	40
	84.6	85.5	84.9	86.5	86.70	86.82	86.80	85.3	86.9	86.9	88.02
	8.3	7.4	8.0	6.4	6.15	6.03	6.05	7.6	6.0	6.0	4.83
	40	30	19	15	9		9	19	24	30	43.7 ℄ 7 Cancel

✓

92.85

BM	334	90.51 ✓	5.68	87.17	S.E. Top Fire Hyd. T St + 45th
6+60	= N.L. T St	= Fly Tel Pole 22.0 Rt ✓			
6+46					
6+30	= ℄ T St				
6+16					
6+14	= Existing 1½" Culvert ✓				
6+0	= S.L. T St				
		92.85			

W Lt ℄ E Rt

83.8	83.7	84.3	85.2	85.58	85.65	85.56	85.6	84.7	85.6	85.4
9.1 40	9.2 30	8.6 20	7.7 16	7.27 9	7.20	7.29 9	7.3 16	8.2 19	7.3 30	7.5 40

83.91

8.94
19.6 = 1/2 lot 1½" Culv ✓

84.9	85.57	85.63	85.55	85.5
8.0 30	7.28 9	7.22	7.30 9	7.4 30

83.55 ✓

9.30
20.3 = Out lot 1½" Culv F.L.

83.0	83.1	82.83	84.50	85.4	85.59	85.66	85.58	85.43	83.50	84.4	84.9
9.9 40	9.8 30	10.02 19.1 = F.L.	8.35 19.1 Top Hyd	7.5 16	7.26 9	7.19	7.27 9	7.42 15.3 = Top Hyd	9.35 15.3 = F.L.	8.5 30	8.0 40

84.5	84.5	84.4	85.4	85.61	85.70	85.66	85.5	84.2	85.4	84.9
8.4 40	8.4 30	8.5 23	7.5 16	7.24 9	7.15	7.19 9	7.4 17	8.7 20	7.5 23	8.0 30

92.85

45th St.

8+43 16" Tree 22.9 Rt. ✓
8+34

8+22 = 14" Tree 22.2 Rt. ✓
8+09.5 = ℄ 5' Conc Walk on E ✓

8+0 = Palm Tree 22.8 Rt ✓
7+89. = Ely Tel Pole 22' Rt ✓
7+76 = Palm Tree 22.2 Rt ✓

7+50

7+37

7+19 = Palm Tree 21.0' Rt ✓
7+0

6+72 = Palm Tree 22' Rt ✓

90.51

Lt ℄ Rt

86.74
3.77
20.2 = ℄ 5.8 Conc Walk ✓

86.56
3.95
24.0 = ℄ 4.5 Conc Walk ✓

85.5	85.6	86.4	86.68	86.73	86.63	86.1	86.5	86.3	86.0
5.0	4.9	4.1	3.83	3.79	3.88	4.4	4.0	4.2	4.5
40	30	17	9		9	15	20	30	40

84.7	84.8	85.0	85.8	86.03	86.14	86.10	85.8	85.9
5.8	5.7	5.5	4.7	4.48	4.37	4.41	4.7	4.6
40	30	19	15	9		9	15	30

85.75
4.76
28.8 = ℄ 4' Conc Walk ✓

84.0	84.1	84.7	85.71	85.83	85.71	85.5	85.5
6.5	6.4	5.8	4.80	4.68	4.80	5.0	5.0
40	30	18	9		9	16	30

✓

90.51

TP	4.59	93.64	1.46	89.05
10+0				
9+60				
9+50				
9+38 = Wly 4' Palm 31 Lt				
9+36 = Ely Tel Pole 21.6 Rt				
9+10 = Wly 4' Palm Tree 31' Lt				
9+06 = 10" Tree 22.0' Rt				
9+0				
8+85 = 12" Tree 22' Rt				
8+64 = 10" Tree 22' Rt				
8+50				
		90.51		

Lt ℄ Rt

87.8	87.9	88.4	87.9	88.66	88.74	88.69	89.0	89.1	89.6
2.7 40	2.6 30	2.1 18	2.6 15	1.85 9	1.77	1.82 9	1.5 20	1.4 30	0.9 40

88.51
2.00
24 = Wly Conc Walk

87.6	88.0	88.5	88.13	88.24	88.22	88.0	88.5	88.42	88.5
2.9 40	2.5 30	2.0 15	2.38 9	2.27	2.29 9	2.5 14	2.0 18	2.09 24 = Wly Walk	2.0 30

87.8	87.9	87.66	87.74	87.65	87.6	87.85	87.8
2.7 40	2.6 30	2.85 9	2.77	2.86 9	2.9 14	2.67 24 = Wly Walk	2.7 30

86.8	86.9	87.3	87.23	87.27	87.16	87.35	87.15	87.0
3.7 40	3.6 30	3.2 17	3.28 9	3.24	3.35 9	3.16 18	3.36 24 = Wly Conc Walk	3.5 30

90.51

45th St.

11+50

11+12

11+0

10+86 = Tel Pole 21.8 Rt ✓

10+68 = ℄ 2 Ribbon Conc Dr. ✓

10+50

10+32 =

93.64

Lt. ℄ Rt.

88.8	89.1	88.7	89.19	89.33	89.22	89.1	90.1	92.0
4.8 / 30	4.4 / 17	4.9 / 15	4.45 / 9	4.31	4.42 / 9	4.5 / 20	3.5 / 30	1.6 / 36 = Top Cut

89.43

4.21 / 30 = ℄ 2' Conc Walk ✓

89.5	89.5	89.48	89.55	89.52	89.3	90.1	90.9
4.1 / 30	4.1 / 15	4.16 / 9	4.09	4.12 / 9	4.3 / 17	3.5 / 23	2.7 / 30

88.91

4.73 / 30 = 2 Rib. Conc Dr. ✓

88.0	88.2	89.19	89.28	89.26	89.3	89.6	90.0
5.6 / 40	5.4 / 30	4.45 / 9	4.36	4.38 / 9	4.3 / 20	4.0 / 30	3.6 / 40

90.09

3.55 / 29.7 = ℄ 3' Conc Walk ✓

93.64

BM		8.17	85.47 ✓	Starting 85.44
18+89 = Sly Paving to West				
12+80 = Sly Paving to East				
12+60 = S.L. Ocean View Blvd				
12+33 = Ely Tel Pole 221 Rt. ✓				
12+30				
12+13 = Anchor Pole Wly 22.6 ✓				
12+0				
	93.64			

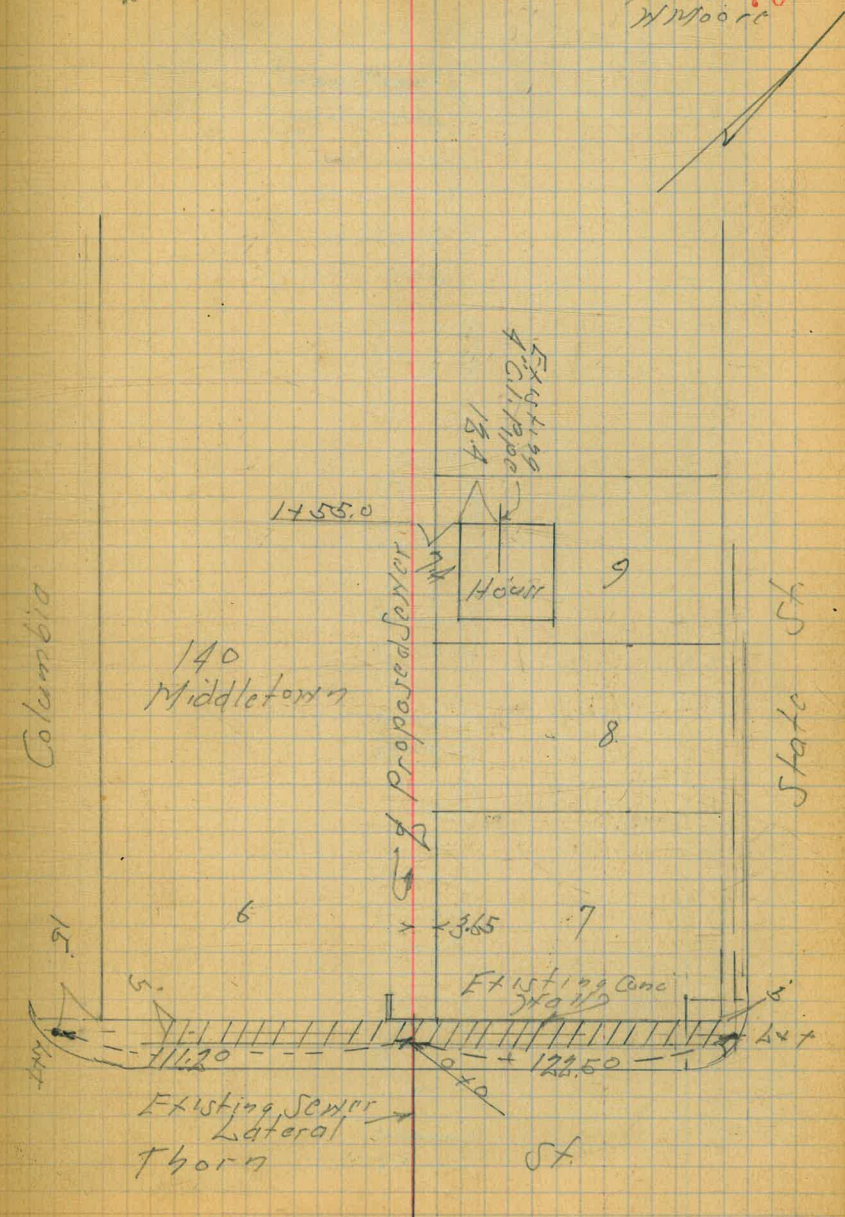
Lt.		℄		Rt.				
	84.87	85.53	85.78					
	8.77 30	8.11 9	7.86					
			86.02	86.03	85.88	86.07	86.34	
			7.62	7.61 9	7.76 22	7.57 30	7.27 40	
85.9	86.1	85.5	86.35	86.56	86.57	86.6	87.3	87.4
7.7 30	7.5 20	8.1 16	7.29 9	7.08	7.07 9	7.0 15	6.3 30	6.2 40
	86.6	86.5	87.29	87.45	87.39	87.3	88.8	91.0
	7.0 30	7.1 15	6.35 9	6.19	6.25 9	6.3 20	4.8 30	2.6 35
86.2	86.8	88.1	87.5	88.20	88.32	88.18	88.1	90.3	91.8
7.4 40	6.8 30	5.5 17	6.1 15	5.44 9	5.31	5.46 9	5.5 21	3.3 30	1.8 35
					✓ 93.64				

Proposed Sewer to Serve
Lot 9 Block 140 Middletown

BM	0.17	187.44		187.27	S.E. BP Thorn & State
TP	6.50	181.66	12.28	175.16	
0+0	= Sly 5' Conc Walk Top		7.65	174.01	
	Top 4" Sewer Lat.		12.60	169.06	
+05.2	on Walk		7.50	174.16	
	Top Conc Wall 47 Wide		4.12	177.54	
+06			4.3	177.4	
+25			2.7	179.0	
+50			1.3	180.4	
+75			0.8	180.9	
1+0			1.9	179.8	
+25			5.8	175.9	
+55 = Nly House			12.4	168.3	
TP	6.09	175.56	12.19	169.47	
19.8' E of ½ Top 4" C.I. Soil Pipe			3.57	171.99	
	Floor Basement		1.13	174.43	

INDEXED
EFB

Nov. 1-40
Sisson
Northern
W Moore



University

6+00.5°

18.0

5+0 18.0

4+0 18.0

3+0 18.0

Forward this Receipt Pro

DEPARTMENT OF

Receipt

REQ. NO. G 3519

University

6+00.5
1.4
599.1

6+00.5 18.0

5+0 18.0

4+0 18.0

3+0 18.0

2+0 18.0

1+0 18.0

0+50 18.0

0+01.4 18.0

0+0 19.8

Final Paving
Alley Block 6
City Hts Annex
No 1
Between
Highland & 45th St.

19,783.80
26.46
10,810.26

Hightman

Receipt

REQ. NO. G 35

Received on Requisition Number Specified the Following in Good Order:

DATE	RECEIVED FROM	QUANTITY	DESCRIPTION

Forward this Receipt Promptly to Purchasing Department After Delivery Completed.

DEPARTMENT OF PUBLIC WORKS By _____

Floor Elev.

	+	H.I.	−	Elev.		
B.M.	1.60	11.60		10.00		Kitchen floor
~~E.P.~~						
Stake			5.26	6.34	3.66	N.E Corner Hub.
			6.71	4.89	5.71	N.W " "
	4.15	10.72	5.03	6.57	3.43	S.E " " Terrace
			5.62	5.10	4.90	S.W. " " Terrace
			5.40	5.32	4.68	S.W. " " Corner Sun Porch.
			3.13	7.59	2.41	South end of jog on west side
	check		5.84	4.88		N.W.
			Checks	.01		

west side temp

0-6
12-0
-4
3-2
16-0
3-5
Sta 12-7 = 12.6
offset 15-6"
" 17-2
32-8" = 32.67 to N.E. cor. of inside wall

~~12-7~~
~~4~~
~~12-0~~
12-7
0-6
6-3
6-6
6-6
6-3
0-6
Sta 39-1 = 39.08
offset 15.6
"

12-7
26-6
39-1

7-11
7-11
~~1-4~~
17-2

to north line of inside found.
" " " " " " from NW temp

0-6
7-4
0.4
7-4
15-6

6-5
6-11
6-5
Sta 19-8 = 19.67
North line of wing wall

39.08
58.75

to South line, inside wall from NW temp

check
5
58-9
5-7
5-7
-10
-6
71-3

west side

23-5
-10
4-0
28-3 = 28.25

28-3
3-5
Sta 24-10 = 24.83
4-0 = 4.0
9-0

70-8
3-5
67-3 = 67.25
3-2
10
71-3 = 71.25

69-0

NW temp stake to offset on west
offset
length of offset

west side

" " to corner

South side

8-3
15-9
24-0 = ~~23.75~~ 24.0

outside (north)
7-1
5-4
7-0
4-0
23-5 = 23.42 to

39-7 = 39.6
55-7 = 55.6
16-0 = 16.0
3-5 = 3.42

4-3
7-6
4-3

offset 6-5 +15=21.5

3-5
2-1
2-6
8-0

3-10
2-7
6-5

N.E. cor.

to first jog

jog north
to west side
from jog to west side
offset north at jog

51.8
25.9
14.4
39.9
6
33.9
25.9
8.0

518
259
14
399
400
259
14.1

Profile across Road to alley
" " S. of Unio
" " at anna
400
269
13.1
6.55
Fnt at anna
Cabr. Kl
13.2
6.6
525
168
357
1.5565
177.6 BM BP cent Porch of House
NW Cor ANSTAD
EVERVIEW

43,560

57.68

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	25.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20—16)÷2 or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.

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