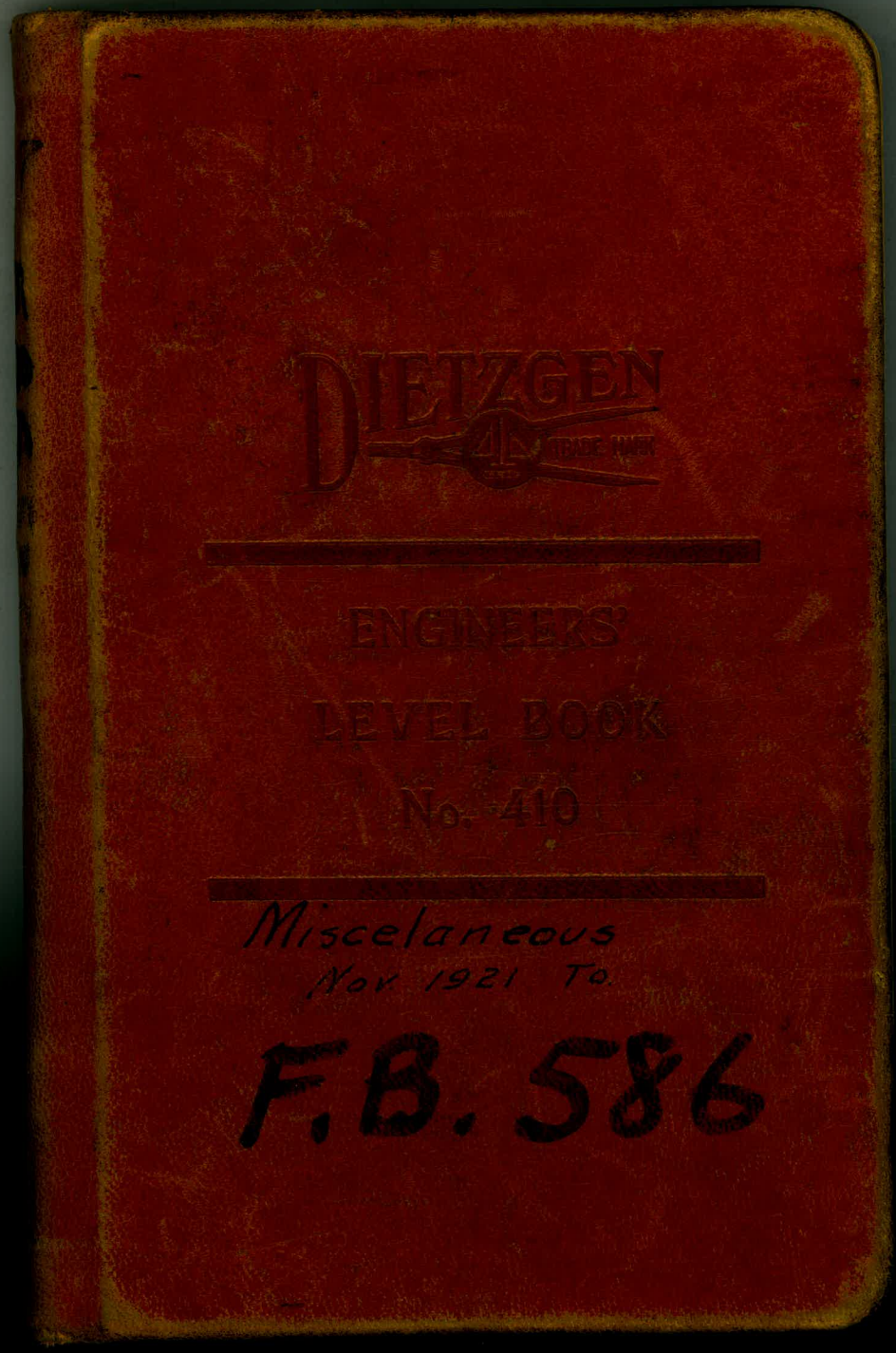
DIETZGEN
ENGINEERS'
LEVEL BOOK
No. 410
Miscelaneous
Nov 1921 To
F.B. 586

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

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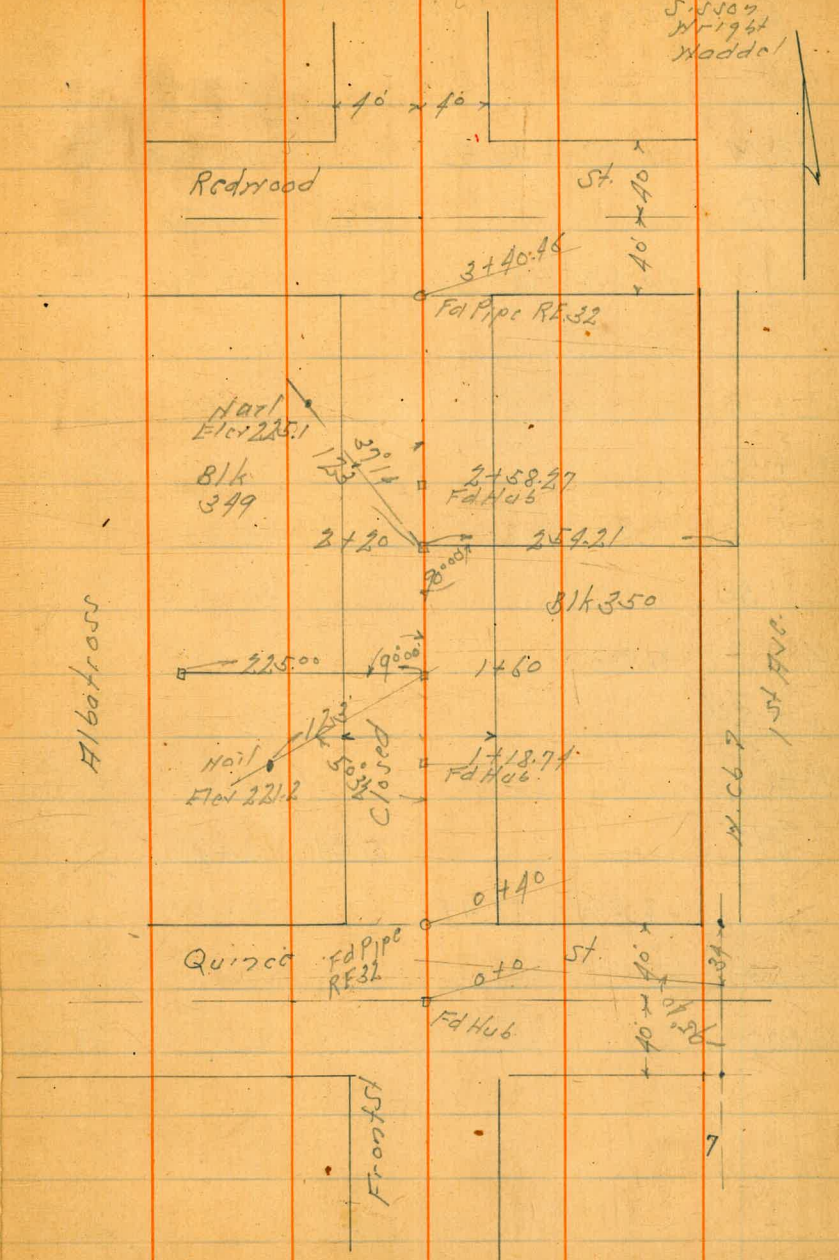
F.B. 586

Front St.	Palm to Quince	4 - 7
Tie cross-section	Front St	35 - 38
Alley Blk. 60 Univ. Hts	Monroe to Madison Ohio - Illinois	8 - 11
Palm	Kettner to Pacific sketch	12 - 19
Vine	Calif. to Pacific sketch. (13)	20 - 23
Maple	32 to 33 sketch	25 - 32
Oil Road proposed	Columbia South to Sassafrass	34
Narragansett Ave.	Warrington & Catalina	38 - 40
Final Paving Measurement's on Alley Blk 72 Ocean Beach		41
Alley Blk 106 Univ. Hts		50 - 55
Dupont	Catalina to Bow sketch	56 - 64
Silvergate	Dupont to Charles	65 - 71
BORN.	Dupont to Dudley	72 - 75

Topog. Quince St Front Block 349 + 350

BM	0.94	266.47		265.53	N.W. BP Redwood + 2nd St
TP	0.85	254.33	12.99	253.48	
BM			8.87	245.46	S.E. Top F Hyd Redwood + 1st Ave
TP	2.11	243.63	12.81	241.52	
Top Curb	W.L. 1st Ave + East ℄		1.77	241.86	
TP	1.06	232.48	12.21	231.42	
2+20	Base Line		3.43	229.05	on Stub
1+60	" "		7.48	225.00	on Stub
1+18.74	Base Line		11.58	220.90	on Hub
1+60	225 W of ℄		12.93	219.55	on Stub

April 19-46
Sisson
Wright
Waddel



Grades - Euclid N. of Klauber

Smale / Chisholm 11-10-21 1

	+	HI	−	Elev.
BM	1.99	42.62		340.63
TP			5.26	37.36
✓	10.68	48.04		37.36
2+00				
" +50				
3				
+50				
4				
+50				
5				
TP			3.81	44.23
✓	3.26	47.49		44.23
5+50				
6+00				

82/2

BP - N. W. Univ. & Euclid

W/S	Grade	Cut	E/S	Grade	Cut
10.68 / 37.36	38.33	F 0.97	—		
7.25 / 40.79	38.60	G - 2.19	11.44 / 36.60	38.60	F 2.00
6.24 / 41.80	38.87	✓ 2.93	8.42 / 39.62	38.87	G 0.75
5.23 / 42.81	39.14	✓ 3.67	6.67 / 41.37	39.14	✓ 2.23
4.54 / 43.50	39.41	✓ 4.09	5.69 / 42.35	39.41	✓ 2.94
3.74 / 44.30	39.68	✓ 4.62	4.54 / 43.50	39.68	✓ 3.82
3.81 / 44.23	39.96	✓ 4.27	3.88 / 44.16	39.96	✓ 4.20
4.38 / 43.11	40.23	✓ 2.88	3.43 / 44.06	40.23	✓ 3.83
5.21 / 42.28	40.5	✓ 1.78	3.81 / 43.68	40.50	✓ 3.18

Curb Grades Daley Ave Diagram

Univ. to Klauber

	West	M	M	East
0+00 SL Univ	346.8			347.2
2+40	338.4 X 4/4=1/16=		1/4=1/16=.035 1/2=1/4=.13 3/4=9/16=.30	X339.4
A°	337.0+.4=	M=+.4	M=+.52	338.0+.52=
2+80	337.4 X			X338.52
40'				
3+20	337.2 X			X338.3
N.L. Klauber 6+00	338.6			339.7
S.L. Klauber	338.0			339.0

Stake Lots

Block	Lots
5	48
	47
	46
	45

DEC 23 1921

DEC 23 1921 31+034

DEC 23 1921 29+30

DEC 23 1921 55 25-6-7-8

DEC 23 1921 Return

Lots	Block
11-12	
15-16	54
17-18	
21-22-23-24	54

DEC 23 1921

DEC 23 1921

DEC 23 1921

DEC 23 1921

Ford
Smale
Chisholm
Nov 12-21

SW Stakes Daley

Sta	+	HI	−	Elev	
BM				338.03	52/19
NE Klauber Daley	6.32	344.35	4.65	339.70	
BM				338.03	52/19
NW Klauber Daley	6.66	344.69	6.09	338.6	
				338.03	
NE Klauber Daley	6.15	344.18	4.48	339.70	
				338.03	
N.W. Klauber Daley	5.71	343.74	5.14	338.60	
330' N of NL Klauber NL Daley			6.34	337.40	
				338.03	
330' N of NL Klauber E L Daley	6.70	344.73	6.21	338.52	
			5.03	339.70	
BM				338.03	52/19
	5.41	343.44	4.84	338.60	M=4

B.P. SW Klauber Daley

P

N/S Klaub

11-28-21

Front St. Cross Section
Palm St to Quince St.

BM	1.10	249.39		248.29	HE BP Palm & 1st
TP	0.52	237.39	12.52	236.87	
TP	1.59	226.85	12.13	225.26	
		0+0 = N.L. Palm St.			
F Cb Top			3.00	223.85	✓
Gutter			3.77	223.08	✓
+2.5 = W.L. Conc Gutter			3.85	223.00	
¼ on Pav			3.90	222.95	
½ " "			4.17	222.68	✓
¼ " "			4.61	222.24	
Gutter " "			5.21	221.64	✓
Cb Top			4.52	222.33	✓
+10			4.5	222.3	
W			6.1	220.7	
		0+50			
W			9.0	217.8	
C			8.0	218.8	
¼			7.5	219.3	
½			7.3	219.5	

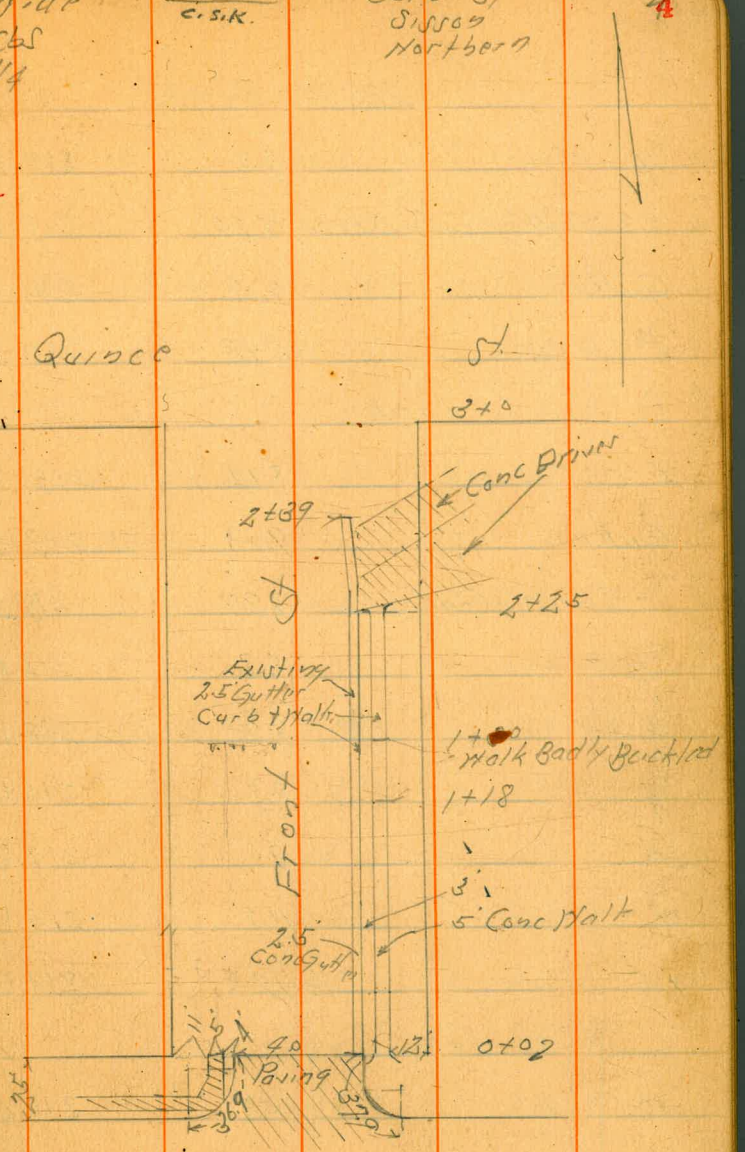
Reduced - plot 11-2-39 - Profile #351 CB Hough

80' Wide
20' C&S
10' ½

Indexed
C.S.K.

Oct 31-39
Sisson
Northern

4



		226.85	
¼		7.0	219.8
+7.5 = Wly Con Gutter		7.24	219.61
Gutter		7.19	219.66 ✓
E Cb Top		6.92	220.43 ✓
	0+75		
E Cb Top		8.14	218.71
Gutter		9.03	217.82
+2.5 = Wly Con Gutter		8.99	217.76
¼		8.8	218.0
℄		8.7	218.1
¼		8.2	218.6
Cb		9.6	217.2
W		11.7	215.1
+5		12.3	214.5
	1+0		
-10		15.2	211.6
W		14.9	211.9
Cb		12.3	214.5
¼		9.6	217.2

		226.85	
℄		10.3	216.5
¼		10.5	216.3
+7.5 = Wly Con Gutter		10.68	216.17
Gutter		10.74	216.11 ✓
E Cb Top		9.90	216.95 ✓
TP	1.28	216.33	11.80 215.05
	1+25		
E Cb Top		1.11	215.22 ✓
Gutter		1.95	214.38 ✓
+2.5 = Wly Con Gutter		1.89	214.44
¼		1.8	214.5
℄		1.6	214.7
¼		1.4	214.9
Cb		5.2	211.1
W		8.6	207.7
+15		9.6	206.7
	1+50		
-20		17.5	198.8 Tb ~~208.8~~
W		13.5	202.8

216.33

Cb	9.6	206.7
¼	3.6	212.7
℄	3.5	212.8
¼	3.6	212.7
+7.5 = N'ly Conc Gutter	3.68	212.65
Gutter	3.69	212.64
E Cb Top	3.86	213.47
1775		
E Cb Top	4.67	211.66
Gutter	5.53	210.80
+2.5 = N'ly Conc Gutter	5.42	210.91
¼	5.6	210.7
℄	5.2	211.1
+7	5.6	210.7
¼	7.1	209.2
Cb	13.0	203.3
W	20.3	196.0
+25	30.3	186.1

216.33

270

-85	43.3	173.0
W	26.8	189.5
Cb	19.0	197.3
¼	12.9	203.4
℄	7.0	209.3
¼	7.2	209.1
+7.5 = N'ly Conc Gutter	7.12	209.21
Gutter	7.18	209.15
E Cb Top	6.84	209.99
2+25 = N'ly End Cb & Walk on East		
E Cb Top	8.30	208.03
Gutter	9.11	207.22
+2.5 = N'ly Conc Gutter	9.11	207.22
¼	8.8	207.5
℄	8.3	208.0
¼	16.0	200.3
Cb	23.2	193.1
W	35.5	180.8

		216.83			
+45			58.3	163.0	
	2+50				
-50			62.0	154.3	2+39 = NW End Conc Drive 9.42
W			42.6	173.7	
cb			28.8	187.5	
¼			20.2	196.1	
℄			12.0	204.3	
¼			9.4	206.9	
cb			9.2	207.1	
E = Sly 6' Conc Dr.			8.85	207.48	✓
TP	3.86	211.63	8.56	207.77	
TP	3.18	208.74	11.07	200.56	
	2+75				
E			0.0	203.7	
cb			8.3	195.4	
¼			8.5	195.2	
℄			9.2	194.5	
¼			13.2	190.5	
cb			18.0	185.7	

	208.74			
W		38.0	170.7	
+15		40.8	162.9	
+55		44.0	159.7	
	3+0 = S.L. Quince			
-50		34.0	169.7	
-25		35.0	168.7	
W		42.2	161.5	
cb		30.5	173.2	
¼		26.2	177.5	
℄		23.0	180.7	
¼		18.6	185.1	
cb		16.0	187.7	
E		10.0	193.7	

Alley Block 60 Univ Hgts. Cross Section
Between Ohio + Illinois From
Monroe to Madison

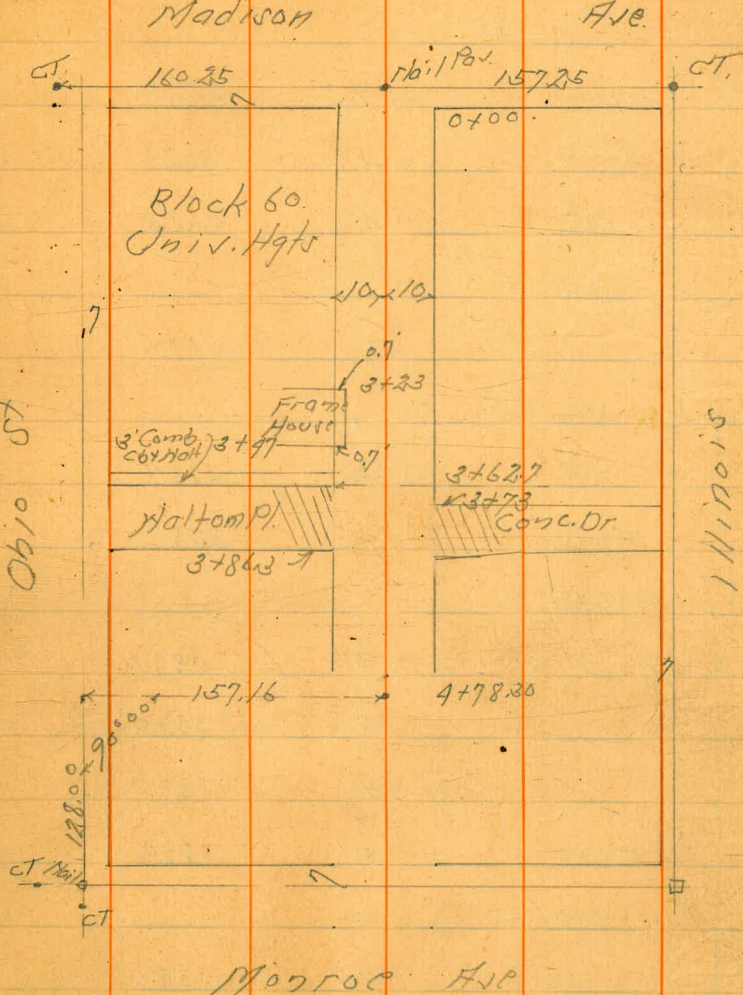
BM	6.91	392.91		386.00	S.E.B.P. Madison + 30th St
TP	3.82	393.51	3.22	389.69	
0 - 14 = S Cb of Madison					
W on Pav			4.46	389.05	✓
℄ " "			4.53	388.98	✓
E " "			4.40	389.11	✓
0+0 = S.L. Madison					
E Top Cb			3.92	389.59	✓
Gutter on Pav			4.22	389.29	✓
℄ " "			4.18	389.33	✓
Gutter " "			4.05	389.46	✓
W Top Cb			3.82	389.69	✓
0+22					
W			4.2	389.3	
℄			4.0	389.5	
E			3.8	389.7	
+5 = ℄ Garage N Ent Conc Floor			3.50	390.01	✓

Reduced plat on Profile 2251 11-2-39 CBH

Indexed
C.S.K.

Oct 31-39
Sisson
Northern

8



89351

0+50

E		4.2	389.3
℄		4.2	389.3
W		4.7	388.8

1+00

W		4.9	388.6
+0.5' = W/y Post Pole			
℄		4.6	388.9
E		4.7	388.8

1+34

-3.5 = ℄ Garage Dirt Floor		4.5	389.0
E		4.5	389.0
℄		4.8	388.7
W		5.1	388.4

1+65

W		5.5	388.0
℄		5.3	388.2
E		5.3	388.2

89351

1+79

-4.5 = N/y Do Garage Conc Floor		4.65	388.86
E		5.1	388.4
℄		5.4	388.1
W		5.7	387.8

1+98

W		5.4	388.1
℄		5.4	388.1
E		5.1	388.4
+4.5 = S/y Do Garage Conc Floor		4.62	388.89

1+99

0.6' E of W.L = Post Pole

2+0 - N/y 4 Garages on W

E		5.1	388.4
℄		5.4	388.1
W = N/y 4 Car Garage on Conc Apron		5.56	387.95
+2' = Garage Floor		5.49	388.02

	393.51		
2+37 = S1y 4 Garages			
-2' = Garage Floor Conc	5.43	388.08	✓
W on Conc Apron	5.62	387.89	✓
℄	5.41	388.10	
E	5.5	388.0	
2+76			
0.8' E of W.L. = Pav Pole			
2+87			
E	5.9	387.6	
℄	5.8	387.7	
W	5.9	387.6	
+1.7 = ℄ Garage Dirt Floor	5.7	387.8	✓
3+09			
W	6.2	387.3	
℄	5.9	387.6	
E	5.8	387.7	
+0.7' = Conc Apron	5.73	387.78	✓
+6.7 = Garage Floor Conc	5.63	387.88	✓

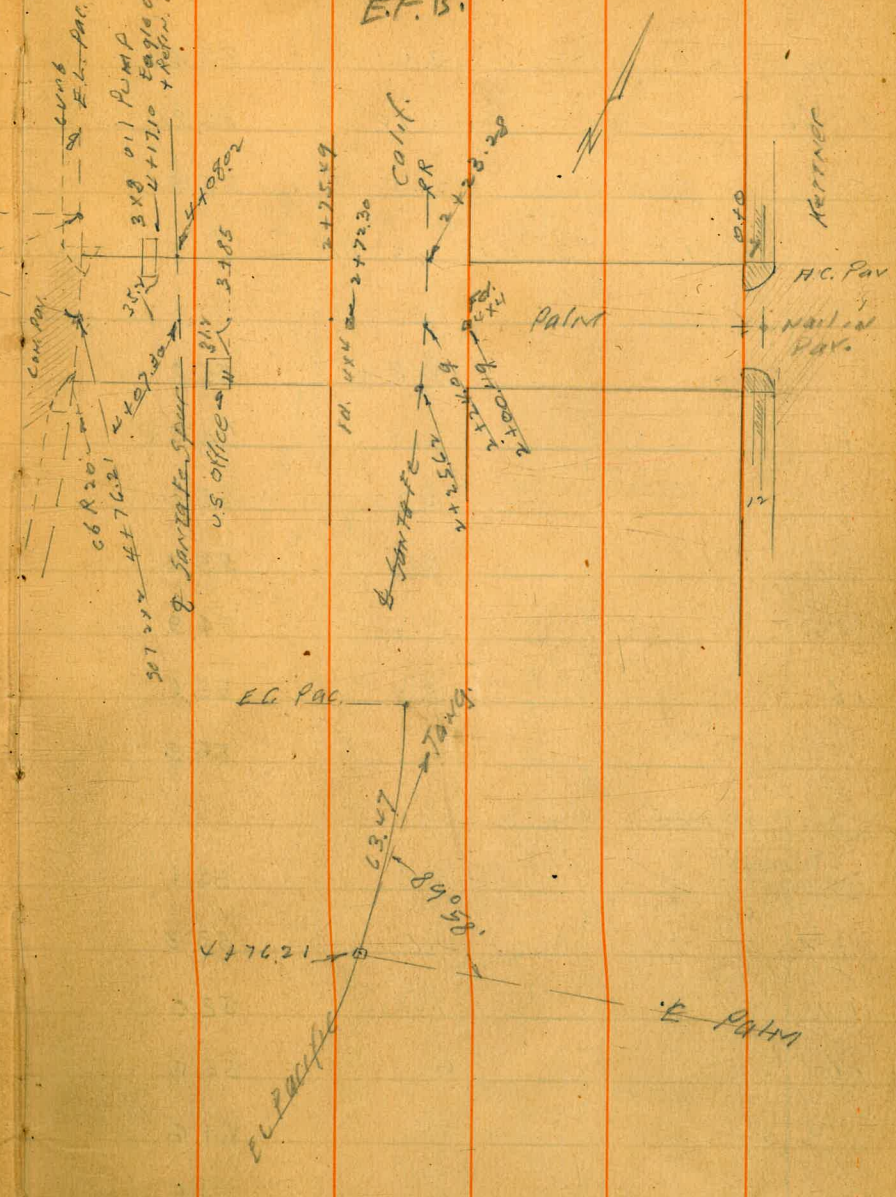
	393.51		
TP	4.25	392.01	5.75	387.76	
3+34					
E = ℄ 3' Conc Gutter			4.69	387.32	✓
℄			4.5	387.5	
W			4.4	387.6	
3+62.7 = NCb Walton Pl. on W					
W Top Cb			4.81	387.20	✓
Gutter on Pav.			5.07	386.94	✓
℄			4.9	387.1	
E			4.7	387.3	
3+73 = N1y Conc Drive on E					
E			4.92	387.59	✓
3+74.5 = ℄ Walton on W					
W on Pav			5.01	387.00	✓
3+86.3 NSCb Walton Pl on W					
E on Conc. Drive			4.48	387.53	✓
℄			4.7	387.3	
W Gutter			5.29	386.72	✓
W Top Cb			4.92	387.09	✓

	392.01						392.01			
	3+89				TP	4.92	391.50	5.43	386.58	
1.0' E of W.L = Power Pole					TP	2.82	386.61	7.71	383.79	
	4+30				BM			7.64	378.97	S.E. BP Monrock 30 ft 378.95
W		4.9	387.1							
℄		4.7	387.3							
E		4.7	387.3							
+12 = ℄ Garage		4.6	387.4	✓						
	4+59									
E		4.9	387.1							
℄		4.7	387.3							
W = W℄ Do. Garage Conc Floor		4.77	387.24							
	4+68									
E		4.7	387.3							
+13 = ℄ Garage 1st Floor		4.6	387.4	✓						
	4+74.3									
E		4.9	387.1							
℄		5.0	387.0							
+93 = W℄ Bm Blk										
W = S℄ Do. Garage Conc Floor		4.90	387.11	✓						

X sec Palm 80' wide 1-25-40
Ker. to Pac. 14 c66
13 1/4

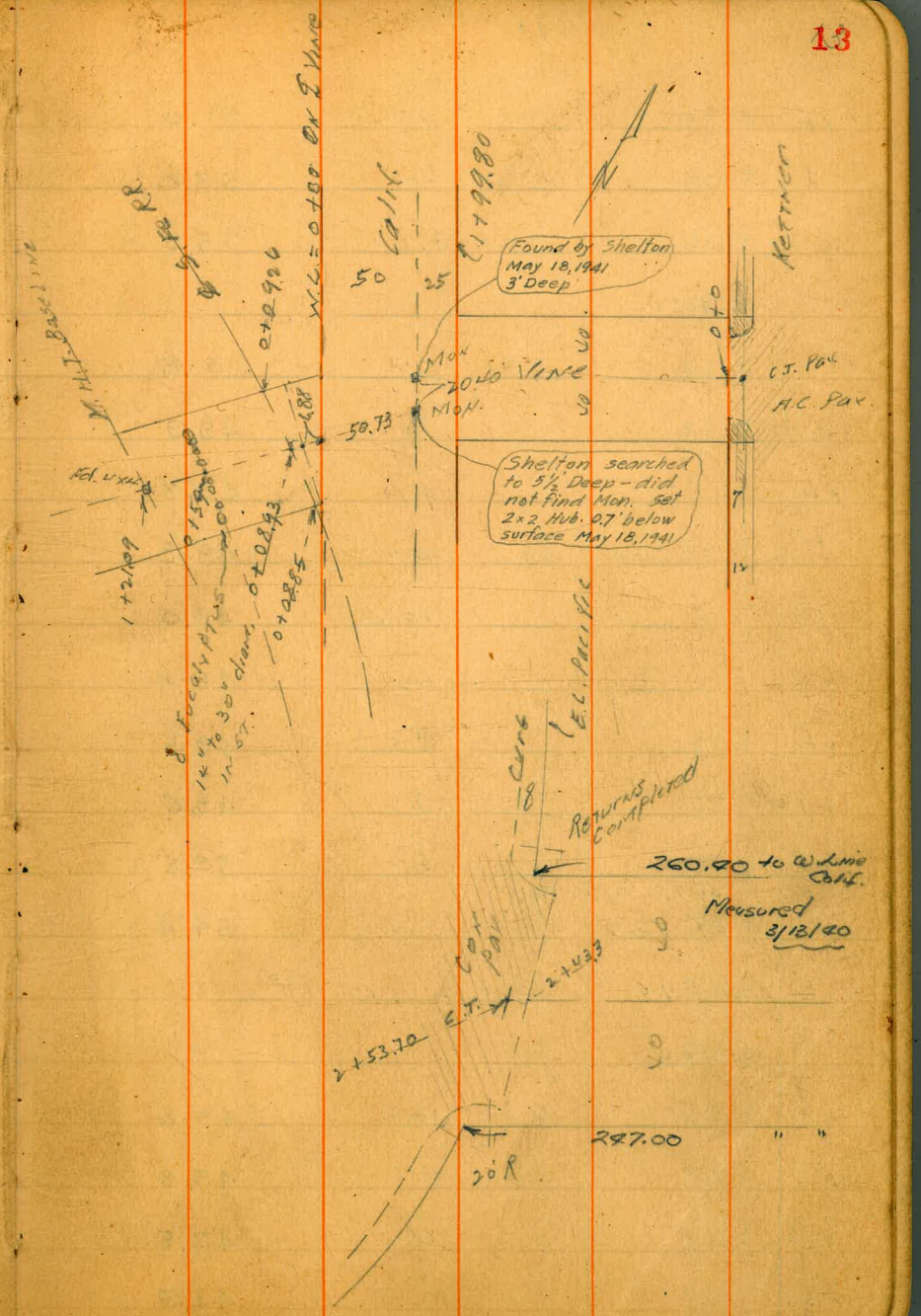
INDEXED
E.F.B.

S.E.B.P	1.52	59.01 ✓		57.49	Palm & Ker.
0-12 w. cb Ker.					
S cb			2.54	56.47	
S pav gut			3.20	55.81	
cb "			3.10	55.91	
1/4 "			3.01	56.00	
c "			2.96	56.05	
1/4 "			2.81	56.20	
cb "			2.74	56.27	
N " gut			2.69	56.32	
N cb			2.05	56.96	
0+0					
N			1.8	57.2	
N + 14.7			2.20	56.81	
gut pav			2.90	56.11	
1/4 "			2.61	56.40	
c "			2.66	56.35	
1/4 "			2.87	56.14	



59.01

S gut	par		3.41	55.60
S cb			-.74	56.25
S			2.5	56.5
	0+1.5	S+12	12" P.P	
	0+15			
S			2.8	56.2
cb			4.5	54.5
1/4			3.7	55.3
C			3.7	55.3
1/4			4.1	54.9
cb			3.4	55.6
N			2.1	56.9
	0+35			
N			2.9	56.1
1/4			5.7	53.3
1/4			7.0	52.0
cb			6.4	52.6
1/4			7.4	51.6
C			7.5	51.5
1/4			7.5	51.5



5901

c6	8.0	51.0	
+1½	6.0	53.0	
S	3.1	55.9	
0+50			
S	5.2	53.8	
+3	9.1	49.9	
c6	9.7	49.3	
1/c	10.2	48.8	
c	10.0	49.0	
1/c	10.6	48.4	
c6	9.5	49.5	
+1½	9.4	49.6	
N	6.2	52.8	
+1	OUTS are Top of Cut 4.6	54.4	
0+96	S+12 12" P.P.		
1+00			
-1	10.0	49.0	
N	3.1	45.9	
+6	14.5	42.5	
c6	14.7	42.3	

5901

1/c	17.3	41.7	
c	18.3	40.7	
1/c	18.3	40.7	
c6	18.0	41.0	
+10	17.4	41.6	
S	14.3	47.7	
T.P. 1.12	47.25	12.88	46.13
1+50			
-1	5.5	41.8	
S	7.5	39.8	
+2	10.3	37.0	
+4	13.0	34.3	
c6	13.1	34.2	
1/4	14.3	33.0	
c	13.6	33.7	
1/c	13.2	34.1	
c6	13.2	34.1	
+9	12.2	35.1	

		47.25 ✓			
cb + 13			9.9	37.4	
N			5.7	41.6	
+ 1			4.0	43.3	
T.P.	0.09	34.59 ✓	12.75 ✓	34.50	
T.P.	1.01	33.31 ✓	2.29	32.30	Nail in Pole
	1 + 75				
- 1			+ 8.0	41.1	
N			+ 6.1	39.4	
+ 4			+ 1.7	35.0	
+ 9			0.3	33.0	
cb			0.5	32.8	
1/4			2.2	31.1	
C			3.2	30.1	
1/4			3.4	29.9	
cb			2.1	31.2	
+ 2	14"	P.P.			
+ 7			2.1	31.2	
+ 12			+ 1.1	34.4	

		38.31 ✓		
S		+ 4.1	37.4	
+ 1		+ 5.5	38.8	
	1 + 86			
- 1		+ 3.7	37.0	
S		+ 2.4	35.7	
+ 6		3.0	30.3	
cb		3.8	29.5	
1/4		3.1	30.2	
C		3.2	30.1	
1/4		2.9	30.4	
+ 7		1.0	32.3	
+ 10		+ 1.7	35.0	
cb		+ 3.4	36.7	
N		+ 5.6	38.9	
	2 + 00.49 = EL Coll 4			
N		+ 6.0	39.3	
cb		+ 5.7	39.0	
+ 4		+ 5.7	39.0	
+ 8		1.0	32.3	
1/4		2.4	30.9	

33.31

C	3.8	29.5
1/4	4.9	28.4
C6	3.8	29.5
+9	2.0	31.3
S	+3.2	36.5
2+05		
S	0.3	33.0
+2	1.6	31.7
C6	2.1	31.2
+5	2.2	31.1
1/4	5.8	27.5
+9	2.0	31.3
C	1.9	31.4
1/4	1.4	31.9
C6	0.0	33.3
N	2.5	30.8
2+16		
N	6.4	26.9
C6	6.5	26.8
1/4	6.7	26.6

33.31

C	6.9	26.4
1/4	6.8	26.5
C6	6.8	26.5
S	6.8	26.5
2+24.09 = E rails		
S E rail	5.88	27.43
S E	6.2	27.1
S W "	6.04	27.27
C " "	5.70	27.61
C E	5.9	27.41
C E "	5.53	27.78
N " "	5.20	28.11
N E	5.7	27.61
N W "	5.39	27.92
2+32		
N	7.0	26.3
C6	7.0	26.3
1/4	7.2	26.1
C	7.3	26.0
1/4	7.4	25.9

33.31

c6	7.6	25.7	
9	7.8	25.5	
2 +38			
5	4.0	29.3	
c6	4.0	29.3	
1/4	4.7	28.6	
c	4.6	28.7	
1/4	4.1	29.2	
c6	4.4	28.9	
N	4.7	28.6	
+7 & Blk. Signal			
2 +75.49 WL Call			
-10	5.2	28.1	
N	5.4	27.9	
c6	5.8	27.5	
1/4	5.9	27.4	
c	6.2	27.1	
1/2	6.2	27.1	
c6	6.6	26.7	
+9	6.9	26.4	

33.31

5	4.9	28.4
2 +79		
5	5.0	28.3
+5	7.1	26.2
c6	6.9	26.4
1/4	6.7	26.6
c	6.3	27.0
1/4	7.0	26.3
c6	6.3	27.0
+11	5.9	27.4
N	8.6	24.7
+10	13.0	20.3
3 +00		
-10	13.8	19.5
N	9.8	23.5
+2	8.6	24.7
c6	8.6	24.7
1/4	9.6	23.7
c	9.3	24.0
1/4	9.5	23.8

		33.31		
c6			8.6	24.7
+7			10.3	23.0
S			6.0	27.3
3+05	14" P.P.	S +1N		
T.P.	0.98	21.68	17.41	20.70
3+40				
S			2.7	19.0
c6			2.8	18.9
1/4			2.8	18.9
c			2.7	19.0
1/4			2.9	18.8
c6			3.5	18.2
+6			3.5	18.2
+10			4.4	15.3
N			4.5	15.2
+7	SE Cor Span Stucco Bldg.		6.3	15.4

	27.68		
3+47			
-7 & 9' opening		6.57	15.11 Con. El. of Sp.
N		6.6	15.1 Stucco Co.
c6		6.7	15.0
1/4		6.3	15.4
c		6.3	15.4
1/4		6.6	15.1
c6		6.5	15.2
S		6.8	14.9
3+96	15" PP	S +11.8	
3+98	12" "	N +9.5	
4+07.30	& Span on & Path		
S & rail		6.70	14.98
S &		7.1	14.6
S W "		6.48	15.00
C " "		6.98	14.70
C &		7.1	14.6
C E "		6.93	14.75
N " "		7.34	14.34
N E		7.8	13.9
N W "		7.44	14.24

℄ +18 S +10 Sta. R.R. xing Post			
℄ +37			
N		7.5	14.2
cb		7.3	14.4
1/℄		7.2	14.5
C		7.3	14.4
1/℄		7.2	14.5
cb		7.2	14.5
+6.6 12" P.P. Guy Pole			
S		6.8	14.9
℄ +76.21 E.C. Pacific			
S		6.7	15.0
+10.7 Top cb end		6.93	14.75
" out Pav		7.61	14.07
cb	"	7.60	14.08
1/℄	"	7.59	14.09
C	"	7.73	13.95
1/N	"	7.95	13.73
cb	"	8.19	13.49

cb +3.2 Pav.		8.26	13.42	
cb + 4.7 out Pav		8.10	13.58	
" " ~~Top cb. end~~ cont. sdw.		8.10	13.58	
N Conc. drive		7.59	14.09	
8' West E cb Pacific				
N-17 Top cb		7.28	13.80	cb end
" out		8.44	13.24	beg. cont. S dw. of Drive 1x to 0.1 Sta.
N "		8.23	13.45	
C Pav		7.93	13.75	
S "		7.41	14.07	
S Top cb.		7.04	14.64	
B.P. Front of Lindberg Field Bldg		9.46	12.22	12.22 0.0N

1-25-40

Xsec Vine St.
Calif. to Pacific
See Sketch P 13
" FB 1258-40

80' wide
14' cbs
13' 1/4

SEBP	2.53	42.11		39.58	Vine + Ket.
T.P.	0.76	30.14	12.73	29.38	

0+00 W.L. Calif to North

S			7.6	22.5
cb			7.0	23.1
1/4			8.2	21.9
c			8.5	21.6
1/4			9.3	20.8
cb			8.3	21.8
N			7.0	23.1

0+06.88 = 90° with SW Cor.

N			7.6	22.5
cb			7.5	22.6
1/4			7.5	22.6
c			7.6	22.5

Notes Reduced + Plotted on Profile #913 1-27-40 EBH

30.14

INDEXED EFB

20

1/4			7.6	22.5
cb			7.1	23.0
S			7.5	22.6

0+08.93 Int. ℄ Vine + ℄ R.R.

S	E rail		6.99	23.15
S	W "		7.13	23.01
c	W "		7.17	22.97
c	E "		7.00	23.14
N	" "		7.03	23.11
N	W "		7.23	22.91

0+14

N			8.0	22.1
cb			8.1	22.0
1/4			8.1	22.0
c			7.9	22.2
1/4			7.8	22.3
cb			7.8	22.3
S			7.8	22.3
T.P.	0.41	18.20	12.35	17.79

1820 ✓

0+80			
-10		1.8	16.4
S		1.7	16.5
c6		1.7	16.5
1/4		1.6	16.6
C		1.4	16.8
1/4		1.1	17.1
c6		0.9	17.3
N		0.7	17.5
0+84			
-10		0.6	17.6
N		2.0	16.2
c6		2.0	16.2
1/4		2.1	16.1
C		2.1	16.1
1/4		2.1	16.1
c6		2.3	15.9
+3	12" R.P.		
S		2.4	15.8
+10		2.5	15.7

1820 ✓

0+73			
-10		4.4	11.8
S		4.9	13.3
c6		3.9	14.3
1/4		3.7	14.5
C		3.6	14.6
1/4		3.3	14.9
c6		3.2	15.0
N		3.2	15.0
+10		3.0	15.2
0+90			
-10		3.5	14.7
N		3.7	14.5
c6		3.7	14.5
1/4		3.7	14.5
C		4.0	14.2
1/4		4.8	13.4
c6		6.0	12.2
S		6.3	11.9
+10		6.4	11.8

18.20

1+09			
-10		4.5	11.7
S		4.4	11.8
cb		4.3	11.9
1/4		4.0	12.2
C		3.6	12.6
1/4		3.9	13.3
cb		3.8	13.8
N		3.8	13.8
+10		3.8	13.8
1+21.09 - MHT Sardine			
-10		3.9	13.3
N		3.9	13.3
cb		4.0	13.2
1/4		4.0	12.2
C		4.2	12.0
1/4		4.4	11.8
cb		4.5	11.7
S		4.6	11.6
+10		4.6	11.6

18.20

1+50			
S		7.0	11.2
cb		6.9	11.3
1/4		6.8	11.4
C		6.8	11.4
1/4		6.7	11.5
cb		6.8	11.4
N		6.9	11.3
1+72	S + 11.7	14" P.P.	
2+00			
N		7.7	10.5
cb		7.6	10.6
1/4		7.3	10.9
C		7.2	11.0
1/4		7.1	11.1
cb		7.0	11.2
S		7.0	11.2
2+43.3	end Pav. at Pac.		
S		7.7	10.5
cb	Top end	7.73	10.47

		1820		
S	qut pax		8.22	9.98
1/4	"		7.92	10.28
c	"		7.75	10.45
1/4	"		7.92	10.28
	qut "		8.20	10.00
N	cb Top end		7.55	10.65
N			7.8	10.4
C.T.	2+53.70, Int. Evine & El. Pac.			
N			7.9	10.3
+10	cb		7.88	10.32
"	qut Pav		8.45	9.75
cb	"		8.38	9.82
1/4	"		8.25	9.95
c	C.T. "		8.19	10.01
1/4	"		8.27	9.93
cb	"		8.46	9.74
+4	qut "		8.49	9.71
cb	Top		8.01	10.19
S			8.1	10.1

		1820			
E	cb Pac				
S	Top cb		8.21		9.99
S	qut pav		8.76		9.44
c	"		8.45		9.75
N+c	" "		8.43		9.57
"	Top cb. P.C.		8.03		10.17
T.P.	3.45	13.45	8.20	10.00	
T.P.	5.70	14.65	4.50	8.95	
NEBP Pac. & Harasthy			4.60	10.05	10.00

Cross Section Maple St 32nd St to 33rd St

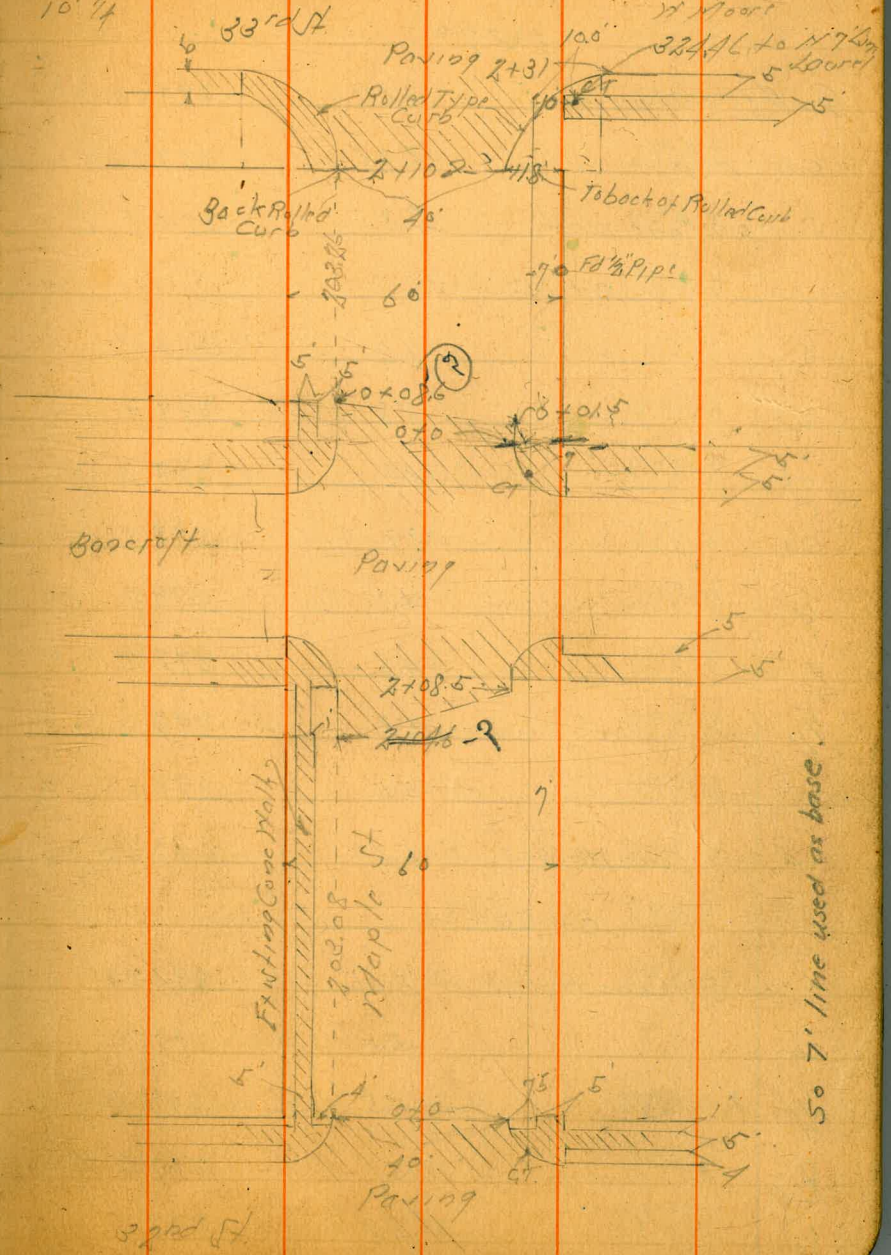
BM	1.59	302.70		301.11	SW. BP Maple & 32nd
		FCb 32nd St			
S	Cb Top		2.91	299.79	
S	Gutter on Paving		3.44	299.26	
Cb	" "		3.70	299.00	
1/4	" "		4.14	298.56	
1/2	" "		4.56	298.14	
1/4	" "		5.04	297.66	
Cb	" "		5.75	296.95	
H	" "		6.36	296.34	
H	Cb Top		5.60	297.10	
		0+0 = FL 32nd St			
H			5.37	297.33	
+6	= Sly Conc Walk		5.38	297.32	
Cb	Top		5.42	297.28	
Gutter on Paving			5.96	296.74	
1/4	" "		5.12	297.58	
1/2	" "		4.37	298.33	
1/4	" "		3.93	298.77	

Reduced & Plotted By H.M. Cole 7/5/40 Profile 620

60' Wide
10' Cbs
10' 1/4

INDEXED
EFB

July 3 - 40
Sisson
Northern
W Moore



So 7' line used as base.

	302.70		
Gutter on Paving		3.67	299.03
CL Top		2.94	299.76
S of Conc Walk		2.8	299.9
	0+35		
S		1.2	301.5
+2		2.8	299.9
+5		3.4	299.3
CL		3.9	298.8
¼		4.3	298.4
½		4.8	297.9
¼		5.2	297.5
CL		5.5	297.2
+4 = S/y Conc Walk		5.40	297.30
	0+50		
N +6 = S/y Conc Walk		5.45	297.25
CL		5.5	297.2
¼		5.5	297.2
½		5.1	297.6
¼		4.8	297.9

	302.70		
+8		4.7	298.0
CL		4.4	298.3
+4		4.0	298.7
+7		3.3	299.4
S		+1.5	304.2
	0+70		
S		0.9	301.8
+1		3.0	299.7
+7		4.6	298.1
CL		4.8	297.9
+4		5.2	297.5
¼		5.0	297.7
½		5.1	297.6
¼		5.6	297.1
CL		5.8	296.9
+4 S/y Conc Walk		5.51	297.19
	1+0		
N +6 = S/y Conc Walk		5.63	297.07
CL		6.1	296.6
¼		6.0	296.7

Maple St.

		302.70			
℄			5.5	297	2
1/4			5.5	297	2
+7			5.4	297	3
Cb			5.2	297	5
+6			4.4	298	3
S			2.9	299	8
TP	2.92	300.10	5.52	297.18	
	1+01				
-11.6	= Wly Do Garage Conc Floor		0.65	299	45
-0.3'	= N Wly Conc Apron		2.09	298	01
S			2.1	298	0
SCb			2.7	297	4
	1+17				
-11.6	= Ely Do. Garage C.F.		0.67	299	43
-0.2'	= N Ely Conc Apron		2.42	297	68
S			2.5	297	6
SCb			3.0	297	1
	1+25				
S			0.3	299	8

		300.10			
+6			2.7	297	4
Cb			3.1	297	0
+5			3.6	296	5
1/4			3.3	296	8
℄			3.3	296	8
1/4			3.7	296	4
Cb			3.7	296	4
+4 = Sly Conc Walk			3.51	296	59
	1+50				
N+6 = Sly Walk			3.99	296	11
Cb			4.2	295	9
+3			4.4	295	7
1/4			4.2	295	9
℄			3.9	296	2
1/4			3.8	296	3
+5			4.0	296	1
Cb			3.6	296	5
+7			3.0	297	1
S			1.7	298	4

Maple St.

300.10

270

S	4.0	2961
Cb	4.4	2957
+2	4.9	2952
¼	5.0	2951
½	5.1	2950
¼	5.2	2949
Cb	5.2	2949
+4 = S/y Conc Walk	4.84	29526
27046 on N		
27085 on S = W/y Edge Paving Bancroft		
N 76 = S/y Conc Walk	4.90	29520
Cb Top	4.99	29511
Gutter on Paving	5.54	29456
¼ " "	5.28	29482
½ " "	5.10	29500
¼ " "	5.10	29500
Gutter " "	5.29	29481
Cb Top	4.62	29548
S	4.3	2958

300.10

W Cb Bancroft

S Cb Top	4.57	29553
S Gutter on Paving	5.26	29484
Cb " "	5.38	29472
¼ " "	5.44	29466
½ " "	5.55	29455
¼ " "	5.69	29441
Cb " "	5.73	29437
N Gutter " "	5.82	29428
N Cb Top	5.15	29495

E Cb Bancroft

W Cb Top	6.15	29395
Gutter on Paving	6.77	29333
Cb " "	6.48	29362
¼ " "	6.09	29401
½ " "	5.88	29422
¼ " "	5.86	29424
Cb " "	6.00	29410
S Gutter " "	6.05	29405

	300.10		
S Cb Top	5.68	294	42
0+01.5 on S Cb 0+08.6 " N Cb = Fly Edgr. Paving			
S on Conc Walk	5.45	294	65
Cb Top	5.87	294	23
Gutter on Paving	6.48	293	62
1/4 " "	6.18	293	92
℄ " "	6.06	294	04
1/4 " "	6.35	293	75
Gutter " "	6.84	293	26
Cb Top	6.21	293	89
N	5.9	294	2
0+25			
N	7.2	292	9
+2	8.1	292	0
Cb	7.7	292	4
1/4	7.3	292	8
℄	7.1	293	0
1/4	7.1	293	0
Cb	7.0	293	1

	300.10		
S	7.0	293	1
0+50			
S	8.4	291	7
Cb	9.0	291	1
1/4	9.5	290	6
℄	9.3	290	8
1/4	10.0	290	1
Cb	10.2	289	9
+7	9.8	290	3
N	8.6	291	5
0+75			
N	11.0	289	1
+5	11.6	288	5
Cb	11.6	288	5
1/4	11.4	288	7
℄	11.1	289	0
1/4	10.9	289	2
Cb	10.8	289	3
+5	9.9	290	2

Maple St.

	300.10			
S		9.7	290.4	
	0+92			
N = S Wly Conc Apron		11.71	288.39	
N - 18 : Wly Do Garage C.F.		11.28	288.82	
	1+09			
S		11.5	288.6	
Cb		11.8	288.3	
¼		12.1	288.0	
Δ		12.4	287.7	
¼		12.7	287.4	
Cb		12.9	287.2	
N		12.7	287.4	
N = S Ely Conc Apron		12.32	287.78	
+18 : Ely Do Garage C.F.		11.23	288.87	
	1+22			
S - 13.3 = Δ Conc Apron		10.99	289.11	
S - 17.3 = Δ Do Garage Conc Floor		10.88	289.22	
TP	1.27	289.21	12.16	287.94

	289.21		
	1+34		
-16.4 = S Wly Do Garage Conc Floor	3.64	285.57	
-6.3 = S Wly Conc Apron	3.68	285.53	
N	3.8	285.4	
Cb	3.5	285.7	
¼	3.8	285.4	
Δ	3.6	285.6	
¼	3.3	285.9	
+6	3.2	286.0	
Cb	2.4	286.8	
+6	1.4	287.8	
S	1.3	287.9	
	1+50		
N -16.4 = S Ely Do Garage C.F.	3.65	285.56	
N -6.3 = S Wly Conc Apron	3.94	285.27	
	1+75		
S	2.7	286.5	
Cb	4.7	284.5	
+5	5.7	283.5	

	2+89.21		
¼	6.0	28 3 2	
½	6.3	28 2 9	
¼	6.4	28 2 8	
Cb	6.2	28 3 0	
N	6.2	28 3 0	
	2+0		
N	8.0	28 1 2	
Cb	8.2	28 1 0	
¼	8.5	28 0 7	
½	8.3	28 0 9	
¼	8.0	28 1 2	
Cb	6.5	28 2 7	
+5	6.1	28 3 1	
S	4.2	28 5 0	
	2+10 = N ¼ Imp. on 33rd St.		
S	5.6	28 3 6	
+4	7.3	28 1 9	
Cb	7.7	28 1 5	
+1.8 = Back Rolled Cb Top	8.73	28 0 48	

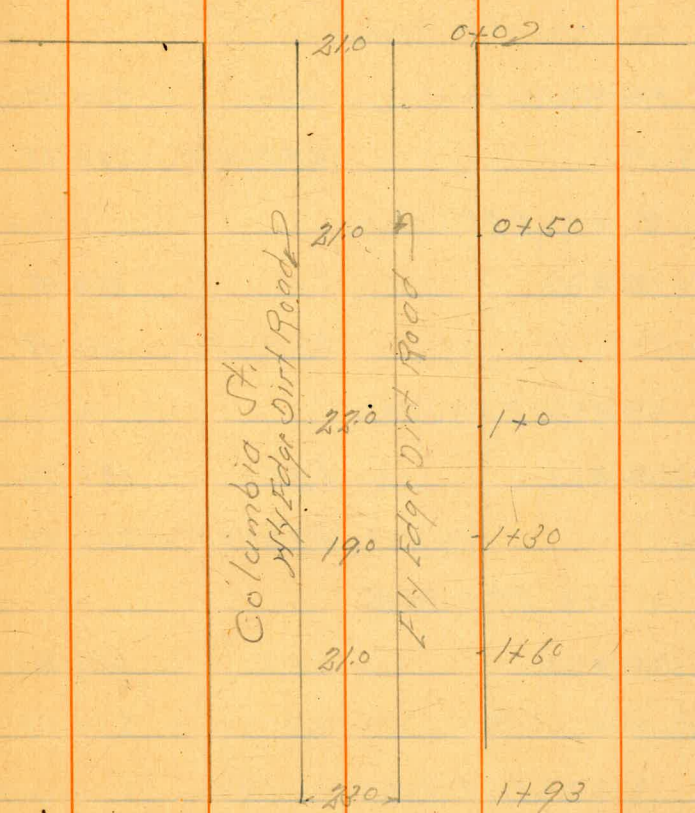
	2+89.21		
Gutter on Paving	9.07	280.14	
¼ " "	9.01	280 20	
½ " "	9.10	280 11	
¼ " "	9.27	279 94	
Cb " "	9.57	279 64	
+1.8 " "	9.58	279 63	
+1.8 = Back Rolled Cb Top	9.25	279 96	
+6.8 = N ½ (conc) walk	92	280 0	
N	8.8	280 4	
	2+31 = N Cb 33rd St		
-11 = Cb BC	8.76	280 45	
Gutter on Pav	9.02	280 19	
N " "	9.37	279 84	
Cb " "	9.68	279 53	
¼ " "	9.80	279 41	
½ " "	9.80	279 41	
¼ " "	9.79	279 42	
Cb " "	9.75	279 46	
S " "	9.85	279 36	

		289.21			
+10 = Gutter on Pav			9.43	279.78	
+10 = CL BC Top			8.67	280.54	
TP	10.90	299.40	0.71	288.50	
TP	529	302.74	1.95	297.45	S.W. B.P. MAP/4482 301.11
BM			1.62	301.12	

Proposed Oiled Road
Columbia St South of Sassafras

INDEXED
EPB

Sept 6-40
Sissa
Northern
N Moore



Re Cross Section Front St
Palm St North
See Sketch Page 4

BM	5.86	228.19		222.33	Top Curb N L Palm W Cb Front St Page 4
		N W Return			
N End Cb = N L Palm			5.86	222	33
Gutter			6.51	221.	68
		9.22 SW			
Cb Top			6.00	222	19
Gutter			6.61	221.	58
		18.45 SW			
Cb Top			6.25	221	94
Gutter			6.90	221	29
		27.67 SW			
Cb Top			6.57	221.	62
Gutter			7.21	221	98
		36.9 SW = W Cb E.C.			
Cb Top			6.87	221.	32
Gutter			7.61	220	58
		N E Return			
N Cb = N L Palm			4.34	223	85
Gutter			5.13	223	06

INDEXED
EFB

Nov 23-40
Sisson
Northern
W Moore

35

		228.19			
		9.47 SE			
Cb Top			4.47	223	72
Gutter			5.20	222	99
		18.95 SE			
Cb Top			4.40	223	79
Gutter			5.10	223.	09
		28.42 SE			
Cb Top			4.25	223.	94
Gutter			4.93	223.	26
		37.90 SE = E Cb E.C.			
Cb Top			4.00	224.	19
Gutter			4.65	223	54
		0-25 = N Cb Line Palm St.			
E Cb on Paving			5.38	222	81
℄ " "			6.09	222	10
W Cb " "			6.85	221	34
		0+0			
W			6.9	221.	3
Cb Top			5.86	222.	33

Red. & Yds Corrected.
11-25-40
C.B.H.

228.19		
Gutter	6.51	221.68
¼	5.94	222.25
℄	5.52	222.67
¼	5.26	222.93
Gutter	5.13	223.06
ECb Top	4.34	223.85
0+50		
ECb Top	7.77	220.42
Gutter	8.54	219.65
¼	8.4	219.8
℄	8.5	219.7
¼	8.7	219.5
+5 = Wly Oil Pox	8.9	219.3
Cb	9.5	218.7
W	10.1	218.1
+9 = Ely House	10.1	218.1
0+70		
16.6 E of ℄ = Wly Power Pole		

228.19		
0+75		
-10	12.7	214.5
W	11.0	217.2
Cb	9.5	218.7
+5	9.4	218.8
+8 = Wly Oil Pox	10.3	217.9
¼	10.2	218.0
℄	10.1	218.1
¼	10.1	218.1
Gutter	10.25	217.84
ECb Top	9.49	218.70
1+0		
ECb Top	11.23	216.96
Gutter	12.07	216.12
¼	11.8	216.4
℄	11.7	216.5
¼ = Wly Oil Pox	11.7	216.5
+2	11.0	217.2
Cb	11.6	216.6

		228.19		
+5			12.1	216.1
TP	1.80	217.66	12.33	215.86
+10			4.0	213.7
W			5.6	212.1
+10			6.3	211.4
	1+25			
-15			11.0	206.7
W			10.0	207.7
+10			8.4	209.3
Cb			6.8	210.9
+4			6.1	211.6
¼			2.8	214.9
+1 = W by Oil Pan			3.2	214.5
½			3.0	214.7
¼			3.1	214.6
Gutter			3.26	214.40
FCb			2.43	215.23

	217.66		
1+50			
FCb Top	4.19		213.47
Gutter	5.00		212.66
¼	4.9		212.8
½	4.9		212.8
+7 = W by Oil	5.0		212.7
¼	4.9		212.8
Cb	10.9		206.8
W	15.0		202.7
-20	19.0		198.7
1+75			
FCb Top	6.00		211.66
Gutter	6.85		210.81
¼	6.8		210.9
½	6.8		210.9
+3 = W by Oil Pan	6.8		210.9
+8	6.4		211.3
¼	8.3		209.4

Rest of Sec Same

Proposed Widening of Narragansett Ave. to 80' Bet. Warrington & Catalina

Moore
Osborne
Hale
1-7-41.

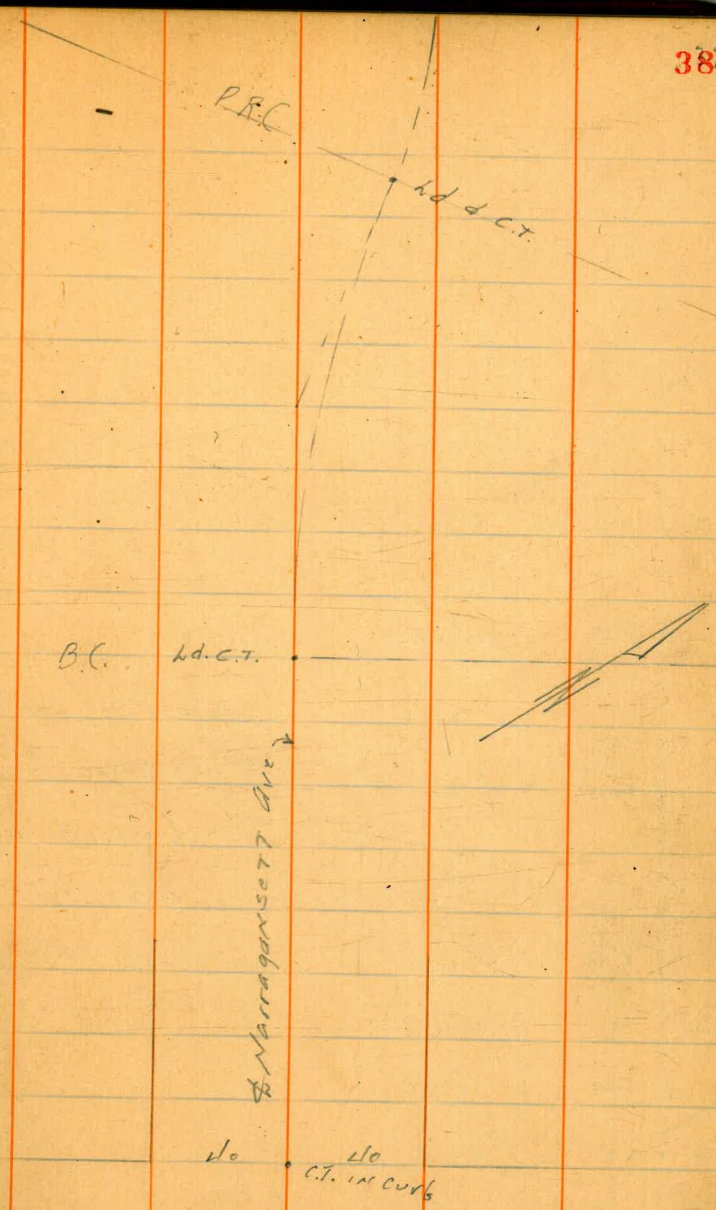
1+48.59 P.R.C. 10° 38.5

1+25	8° 57.2	Δ = 21° 17' 02" Rt.
1+00	7° 09.7	℄ R = 400
0+75	5° 22.3	T = 75.16
0+50	3° 34.8	L = 148.59
0+25	1° 47.4	d = 4.2972' [illegible] 8-7-51
0+00	B.C. = ℄ Sta.	

Existing Impmt. on Narragansett
width 46'
curbs 8'
Roadway 30'
6" Curb face
regular crown

See P 42 for X sec.

Indexed
L.M.



5+78.33 P.R.C. 32°23'21"

+50 30°15.6

5 26°29.5 Δ = 64°47'42" Rt.

+50 22°43.3 / D.R = 380

T = 241.13

4 18°57.1 L = 429.74

+50 15°11.0 Long chord = 407.23 bal 8-7.5'

3 11°24.8 d = 4.53'

+50 7°38.6

2+00 3°52.5

1+48.59 P.R.C.

P.R.C. Ld. C.T.

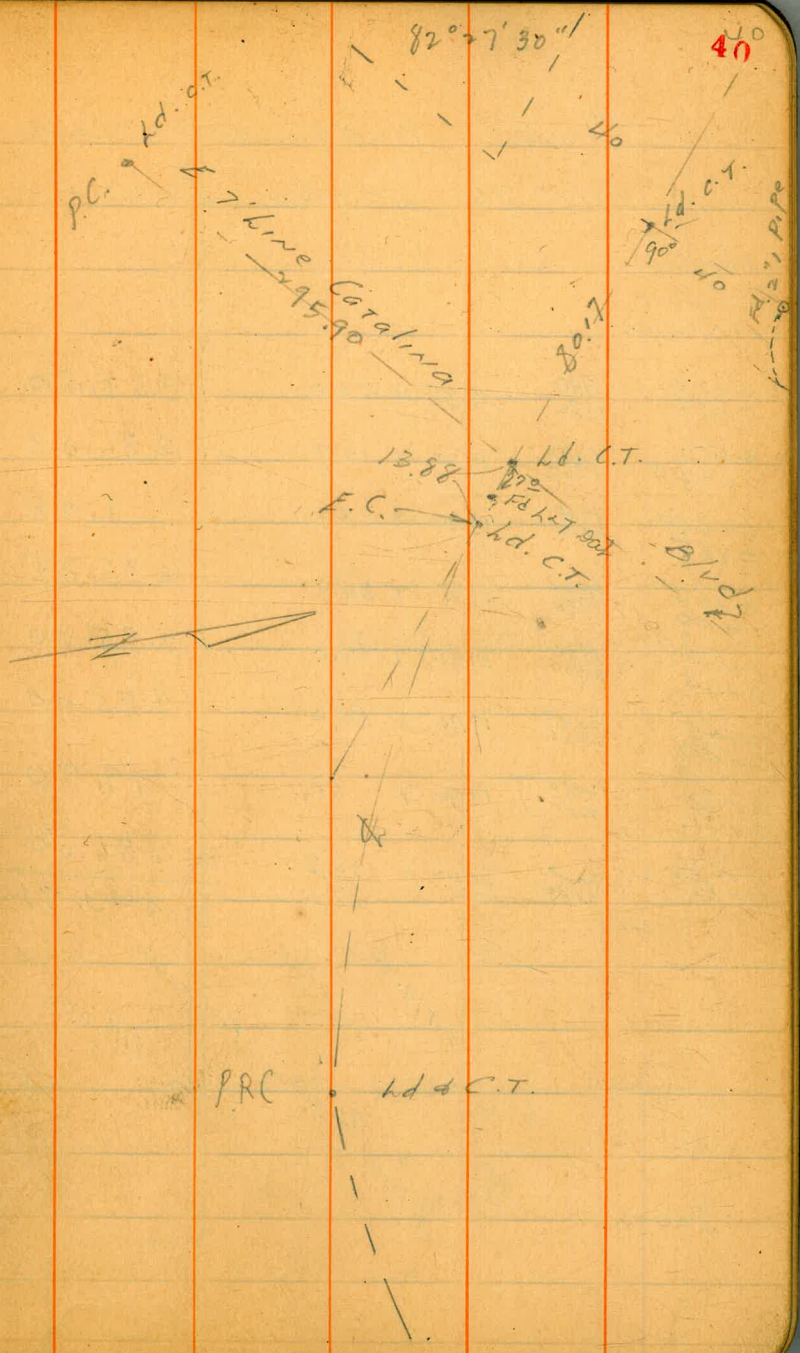
P.R.C. Ld. C.T.

8+62.38 = E/L 7' Line Catalina

8+48.50 E.C. N0°47.0 Ld. C.T.

8	17° 03.14	
+50	13° 12.36	Δ = 41° 34' Rt
		ER = 372.4
7	9° 21.58	T = 141.34 ✓
		L = 270.17
+50	5° 30.8'	d = 4.62' on 8-75'
6+00	1° 49.0 N	

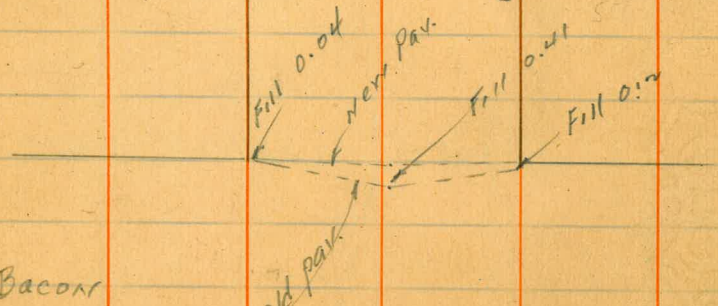
5+78.33 PRC



Final Meas. of alley
Blk 72 Ocean Beach

Moore
Osborne
1-7-41.

0+00 0+50	19.90 18.80	19.35 x 50.0	967.50
0+50 0+64.9	18.80 19.60	19.20 x 14.9	286.08
0+64.9 0+65	19.60 20.00	19.80 x 0.1	1.98
0+65 1+00	20.00 19.90	19.95 x 35.0	698.25
1+00 2+00	19.90 20.00	19.95 x 100.0	1995.00
2+00 2+50	20.00 19.80	19.90 x 50.0	995.00
2+50 2+51	19.80 20.00	19.90 x 1.0	19.90
2+51 4+25.3	20.00 20.00	20.00 x 174.3	3486.00
			8449.71



Bacon

Indexed L.M.

alley

Paved

41

4+25.3 — 20

2+51 20
2+50 19.8

2+44 2.2 x 3.5 iron grate

2+00 20

1+00 19.9 1.5

0+65 20.0
0+64.9 19.6

This paid by P.O. Maybe

0+50 18.8

0+00 9.95 9.95 3

60 sq ft

10 10

Bacon ST.

Moore
Osborne
Sommermeyer

1-28-11

Xsec Proposed align.
Narragansett 80' wide
West of Warrington
to Catalina Blvd

Indexed
L.M.

422

			LT	℄	RT
0+75			220.0 / 1.0 / 40	216.8 / 4.2 / 14	216.30 / 4.73 / 6.2 / C6
				216.11 / 4.9	216.35 / 4.68 / 24.7 / C6
					216.5 / 4.2 / 31
					217.2 / 3.8 / 34
					217.2 / 3.8 / 40
0+50			219.6 / 1.4 / 40	216.7 / 4.3 / 10	216.48 / 4.55 / 2.9 / C6
					216.08 / 4.95
					216.54 / 4.79 / 28.2 / C6
					216.8 / 4.2 / 40
0+00 ℄ T.P.	Ld+C.T.	4.54	~1.03	4.17	216.49 Ld. C.T. IN PAV.
			~1.03		
0+25			219.9 / 0.8 / 40	217.2 / 3.5 / 10	216.61 / 4.05 / 1.0 / C6
					216.09 / 4.57
					216.59 / 4.07 / 29.5 / C6
					216.9 / 3.8 / 40
0+00	B.C. RT	℄ Sta.			
			219.6 / 1.1 / 40	216.91 / 3.75 / 6.4 / C6	216.49 / 4.17
					216.59 / 4.07 / 30 / C6
					216.8 / 3.9 / 40
T.P.	12.91	~0.891	0.17	196.00	
				220.66	
TP	12.76	196.17	0.53	183.41	
T.P.	12.78	183.94	0.41	171.16	
T.P.	12.79	171.57	0.17	158.78	
T.P.	13.10	158.95	0.27	145.85	
NEBP	12.93	146.12		133.19 Chatsworth Narragansett	
T.P.	12.69	220.66	0.94	207.97 Narragansett La Cresta	
NW Ld plug			3.74	205.17	
		208.91			

	LT		℄		RT	
3+00	211.5 9.5 40	210.0 11.0 19	209.88 11.15 12 C6	209.80 11.23	209.98 11.05 18.7 C6	211.2 9.8 40
2+50		215.8 5.2 40	214.38 6.65 26.5 C6	213.77 7.26	214.03 7.00 4.6 C6	214.0 7.0 20
2+00	216.1 4.9 20	215.69 5.34 31.4 C6	215.66 5.37 1.50 C6	215.69 5.34 SDW	215.4 5.6 25	213.3 7.7 40
+48.59 P.R.C.	217.8 3.7 40	216.9 4.1 28	215.95 5.08 24.8 C6	215.77 5.26	216.01 5.02 4.3 C6	215.5 5.5 40
1+25	219.4 1.6 40	216.6 4.4 25	216.07 4.96 17.7 C6	216.01 5.02	216.11 4.92 13.4 C6	216.2 4.8 19
1+00	219.5 1.5 40	216.6 4.4 20	216.22 4.81 11.1 C6	216.09 4.94	216.25 4.78 19.8 C6	216.4 4.6 24
221.03			221.03			

217.2 215.3
3.8 5.7
22 40

217.5 216.3
3.5 4.7
28 40

5+00							
4+50							
4+38.5		W c6 Redondo ℄ N.L regular crown 6" curb face					
4+08.84	= INT. E c6 Redondo ℄ N.L.						
4+00							
T.P.	0.21	201.14	13.08	201.93			
3+50							
T.P. T.P.	0.54	215.01	6.56	214.47			
		221.03					

	LT.		℄		RT.	
191.8	188.6	188.64	189.29	189.66	190.2	194.9
10.3 / 40	13.5 / 27	13.50 / 21 c6	12.85	12.48 / 9.5 c6	11.9 / 18	7.7 / 40
197.6	194.8	194.84	194.81	194.95	196.2	
4.5 / 40	7.3 / 20	7.30 / 11.6 c6	7.33	7.19 / 21.1 c6	5.9 / 40	
			196.73	196.65	196.72	196.75 176.78
			5.71 / 40	5.49 / 45	5.42 / 50 c6	5.39 / 55 5.36 / 60
			197.95	197.54	197.18	197.18 197.18
			4.19 / 40	4.60 / 45	4.96 / 50 c6	4.96 / 55 4.96 / 60
202.1	199.9	199.12	198.79	198.99	198.8	
0.0 / 40	2.2 / 15	3.07 / 4.15 c6	3.35	3.15 / 20.3 c6	3.3 / 40	
		207.14				
207.0	204.3	204.12	203.91	204.53	205.2	
8.0 / 40	10.7 / 12	10.89 / 11.7 c6	11.10	10.48 / 26 c6	9.8 / 40	
		215.01				

6+50				
T.P.	0.33	178.02	12.99	177.69
6+35.45	SL Narr + W cb Redondo			
6+00				
5+78.33	PRC			
5+54.4	S.L. Narr. + E cb Redondo			
5+50				
T.P.	1.62	190.68	13.08	189.06
		202.14		

	LT		℄		RT
1769	176.57	176.03	176.06	175.4	173.7
1.1 / 40	1.45 / 32.5 / cb	1.99 / 2.3 / cb	1.96 / sdw	2.6 / 20	4.3 / 40

178.02

178.94	178.64	178.35	178.03	177.79
11.74 / 60 / cb	12.04 / 55 / cb	12.33 / 50 / cb	12.65 / 45 / cb	12.99 / 40 / cb

180.04	180.10	180.32	180.36	179.9
10.64 / 50 / Pav	10.58 / 40 / Pav	10.36 / 2.8 / cb	10.32 / sdw	12.8 / 40

180.89	181.21	181.42	181.49	181.7	179.9
9.79 / 50 / Pav	9.47 / 40 / Pav	9.26 / 2.3 / cb	9.19 / sdw	9.0 / 10	10.8 / 40

181.70	181.84	182.20	182.58	182.94
8.98 / 60 / cb	8.84 / 55	8.48 / 50	8.10 / 45	7.74 / 40 / cb

183.22	183.31	183.36	183.83	186.1	185.9
7.46 / 40 / sdw	7.37 / 37.5 / cb	7.32	6.85 / 0.5 / cb	4.6 / 20	4.8 / 40

190.68

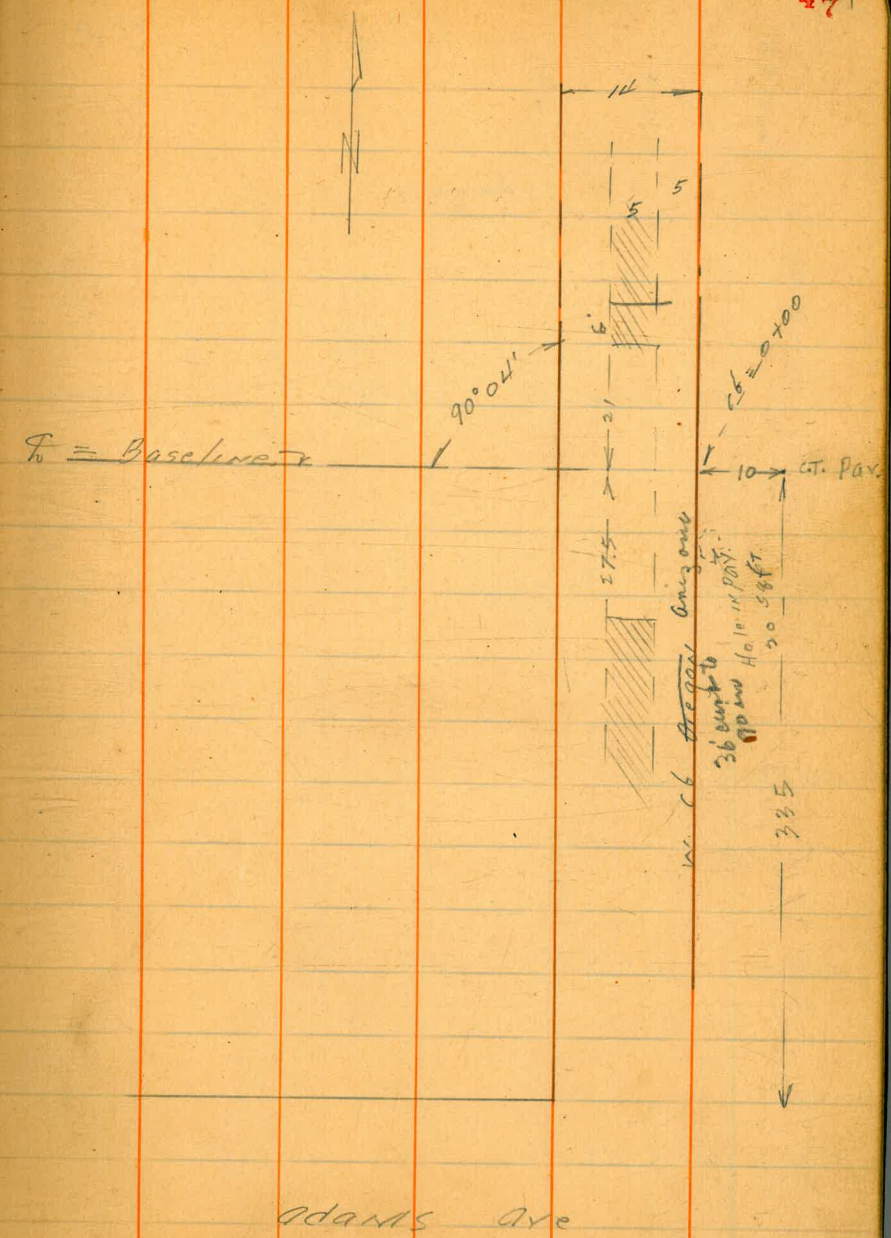
check to BMBP Narragansett Catalina		8.10	157.46	157.52 / 0.06	
T.P.	0.40	165.56	0.30	165.16	
8+62.38 = E 7' Line Catalina Blvd.					
E L Catalina Blvd					
+48.50 E.C.					
8					
T.P.	0.30	165.46	12.86	165.16	
7+50					
7+00					
		178.02			

	LT		℄		RT	
156.14	155.96	155.41	155.05	154.24	154.67	154.68
9.32 / 40 / sdw	9.50 / 27 / c6	10.05 / 27 / 9.47	10.41	11.22 / 36.7 / 9.47	10.79 / 36.7 / c6	10.78 / 40 / sdw
	156.3	155.91	155.49	154.99	155.0	
	9.2 / 40	9.55 / 21.2 / c6	9.97	10.47 / 27.6 / c6	10.5 / 40	
157.3	156.7	156.54	155.99	155.46	155.3	155.7
7.2 / 40	8.8 / 25	8.92 / 16.8 / c6	9.47	10.00 / 23.3 / c6	10.2 / 30	9.8 / 40
163.0	161.2	160.92	160.28	159.84	160.3	161.2
2.5 / 40	4.3 / 25	4.54 / 18.3 / c6	5.18	5.62 / 12 / c6	5.2 / 20	4.3 / 40
			165.46			
	167.7	166.15	165.28	165.36	164.8	164.4
	10.3 / 40	11.87 / 25 / c6	12.74	12.66 / 5.2 / c6	13.2 / 20	13.6 / 40
	172.2	171.38	170.46	170.92	169.9	168.8
	5.8 / 40	6.64 / 29.5 / c6	7.56	7.10 / 0.4 / c6	8.1 / 20	9.2 / 40
			178.02			

Moore
Osborne
S'Meyer
4-23-41.

Survey Washed out Fill
W side ~~Oregon~~ Arizona N. of Adams

S.E.B.P.	5.38	390.29		384.91	Adams Idaho
SW BP			6.34	383.95	Adams Oregon
T.P.	1.97	385.17	7.09	383.20	
SW BP Adams ~~Hamilton~~	=380.05	Brass plug out only head	5.20	379.97	
T.P.	5.55	382.68	8.04	377.13	



Levels on washout
West side ~~Oregon~~ Arizona
N of

Indexed
LM

Station														
							LT			℄		RT		
0+14 = w.L. Arizona (~~Oregon~~)						377.68 (5.0 / 30)		377.58 (5.1 / 18)	369.48 (13.5 / 10)	369.38 (13.3)	372.48 (10.2 / 9)	376.68 (6.0 / 11)		378.48 (4.2 / 21)
0+10 wedge	377.64 (5.04 / 67.1)	377.55 (5.13 / 67)	377.38 (5.30 / 55)	377.57 (5.11 / 47) walk	377.33 (5.35 / 41) walk	377.81 (4.87 / 27.5) end walk		377.88 (4.8 / 22)	369.68 (13.0 / 10)	371.68 (11.0)	372.58 (10.1 / 6)	376.88 (5.8 / 10)	377.88 (4.8 / 15)	378.83 (3.85 / 21) end on walk
0+02				377.58 (5.1 / 30)	377.68 (5.0 / 22)	373.38 (9.3 / 30)	373.18 (9.5 / 13)	376.68 (6.0 / 12)	375.48 (7.2 / 2)	378.18 (4.5)	378.68 (4.0 / 21)			
Curb = 0+0						377.81 (4.87 / 27.5)		378.10 (4.58 / 10)		378.29 (4.39)	378.62 (4.06 / 21)			
0+0 gutter						377.35 (5.33 / 27.5)		377.74 (4.92 / 10)		377.84 (4.84)	378.09 (4.59 / 21)			
00−10 = C.T. pav.										378.64 (4.04)				

Sunken

38r68

38r68

0 + 75	Toe of fill			
0 + 55				
0 + 43				
0 + 40				
T.P	0.16	358.03	12.72	357.87
0 + 30				
T.P	0.67	370.59	12.76	369.92
0 + 18				
		382.68		

LT ℄ RT

335.9 / 22.1 / 5 — 335.6 / 22.4 — 336.6 / 21.4 / 5

348.2 / 9.8 / 10 — 345.0 / 13.0 / 7 — 344.6 / 13.4 / 4 — 347.4 / 10.6 / 2 — 347.3 / 10.7 — 347.3 / 10.7 / 7

356.0 / 2.0 / 20 — 354.2 / 3.8 / 7 — 351.2 / 6.8 / 5 — 355.6 / 2.4 — 357.0 / 1.0 / 4 — 357.0 / 1.0 / 8

358.7 / +0.7 / 20 — 357.8 / 0.2 / 6 — 351.6 / 6.4 / 3 — 352.0 / 6.0 — 358.6 / +0.6 / 4 — 358.4 / +0.4 / 10

358.03

364.6 / 6.0 / 12 — 364.4 / 6.2 / 6 — 358.0 / 12.6 — 363.3 / 7.3 / 4 — 363.6 / 7.0 / 10

370.59

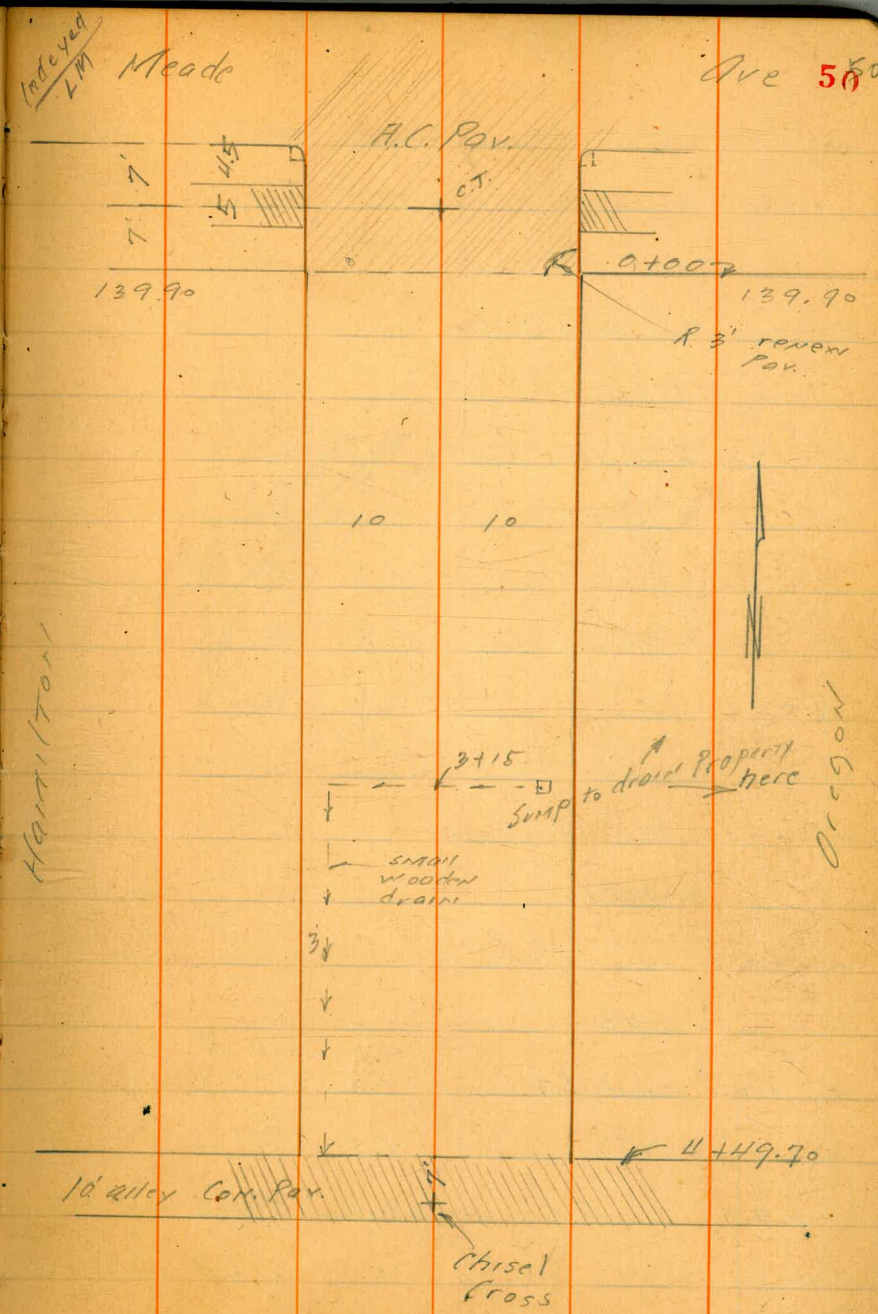
378.98 / 3.7 / 50 — 374.95 / 7.7 / 18 — 372.48 / 10.2 / 10 — 366.68 / 16.0 / 2 — 366.58 / 16.1 — 376.08 / 6.6 / 14 — 377.98 / 4.7 / 35

382.68

Moore
Osborne
S'Meyer
4-23-41.

Xsec. of N & S alley 20' wide
Blk 106 U.H.

SEBP	2.47	379.70		377.23	Meade Oregon
	0-14 = Scb Meade				
E	Pav.		5.14	374.56	
W	"		5.32	374.38	
	0+00 SL Meade				
W	cb	beg. Eugenia Hedge	4.80	374.90	Planted 1' back
W	pav		4.86	37484	
C	"		4.97	37473	
E	on old header		4.87	37483	
E	cb		4.56	37514	
	0+04				
E	-2 6" Cypress Tree				
	0+19				
E	-1.6 & 1.4 Brick Chimney		3.3	376.4	ground
E			3.3	376.4	
C			3.7	376.0	



		379.70			
W			4.0	375.7	5' width × 1.5
+2.3	Brick Chimney		4.2	375.5	
	0 + 42				
E +0.5	beg. Wooden slat fence				
	0 + 44				
W −1.3	℄ 3' Conc. walk		4.7	375.53	
W			4.2	375.5	
C			3.8	375.9	
E			3.8	375.9	
+5			3.9	375.6	
	0 + 50				
W +0.2	beg. 6d. Fence				
	0 + 94				
W +2.6	14" P.P.				
	1 + 00				
−5			4.7	375.0	
E +0.2	end slat Fence		4.3	375.4	
C			4.5	375.2	
+9.9	" 6d. "		4.6	375.1	
W +5			4.6	375.1	

51

51

		379.70			
T.P.	4.74	380.05	4.39	375.31	
	1 + 03				
E −6.3	N end 4 car gar.		4.60	375.4	Fl. El. according to Carpenter Gar. is under Const.
	1 + 20				
−5			5.2	374.8	
W			5.2	374.8	
C			4.9	375.1	
E			5.2	374.8	
	1 + 40				
E −6.2	S end 4 car gar.		4.55	375.50	Fl. El.
	1 + 50				
−5			5.1	374.9	
E −1.1	beg. picket fence				
E			5.2	374.8	
C			4.6	375.4	
W			5.1	374.9	
+1.3	beg. Picket fence				
+10			5.4	374.6	

Get Apron and Floor

38005

	1+65			
-5		5.0	375.0	
W		5.0	375.0	
C		4.3	375.7	
E		4.3	375.7	
+20	Low spot	5.3	374.7	
	1+85			
-20		5.2	374.8	
E		5.2	374.8	
C		4.8	375.2	
W		5.0	375.0	
+5		5.0	375.0	
	1+94			
W +2.6	9" P.P			
	2+03			
-5		5.1	374.9	
-1.2	end Picket Fence			
W		5.0	375.0	
C		4.9	375.1	
E		5.1	374.9	

38005

P2

E +1	Picket Fence			
+20		5.3	374.7	
	2+15			
W		5.0	375.0	
-7.8	E Sin gar.	4.83	375.22	Cem.
	2+29			
W -13	beg. Picket Fence			
	2+50			
E -20		5.7	374.3	
E -1	Picket Fence			
E		5.6	374.4	
C		5.7	374.3	
W		5.4	374.6	
+1	end Picket Fence beg wire "			
+5		5.2	374.8	
	2+80			
-5		5.2	374.8	
W		5.2	374.8	
C		5.7	374.3	
E		5.9	374.1	
+5		5.9	374.1	Try to
+30	Straw Berry Patch	6.1	373.9	drain this

		380.05			
	3+00				
−30	Strawberries		6.4	373.6	drain this
−7			6.5	373.5	
E −0,3	end piket fence				
E	beg. Lat. fence on line		6.1	373.9	
C			6.0	374.0	
W			5.7	374.3	
+0.6	end wire fence				
+5			5.7	374.3	
	3+02				
W +1.0	beg. Cypress hedge				
	3+15				
−10			5.9	374.1	
W			6.0	374.0	
+2			5.8	374.2	
C			5.8	374.2	
+7			5.9	374.1	
+7	Sump of wood drain		6.7	373.3	
E			5.8	374.2	
+20			5.9	374.1	

		380.05			
	3+17				
E −0.2	end Lat. fence				
E −0,5	NW Cor house		5.8	374.2	ground
"	floor El.		3.9	376.1	
"	Bot. Conc. fd.		6.4	373.6	
	3+25				
E −0.5	Cor. house		W +1.0 end Cypress hedge		
E −1.6	to N end porch				
	3+27				
E +0.3	6" Tree				
	3+34				
W +2.1	12" P.P.				
	3+40				
E −1.6	SW Cor Porch				
T.P.	5.02	379.71	5.36	374.69	Nail in Pole West side
	3+50				
−10			5.6	374.1	
E			5.02	374.5	

		379.71			
C			4.9	374.8	
W			5.4	374.3	
+15			5.6	374.1	
	3+65				
-10			5.5	374.2	
W			5.4	374.3	
C			5.5	374.2	
E			5.3	374.4	
+10			5.3	374.4	
	3+85				
E +0.5	NW Cor. Bd. shed				
	3+99				
E +0.3	SW Cor. "	"			
" "	beg. wire fence				
	4+00				
-10			5.1	374.6	
E			5.2	374.5	
C			5.0	374.7	
W			4.9	374.8	

	379.71			
W +0.7 beg. picket fence				
+10		5.1	374.6	
	4+15			
W +2.6 12" p.p.			Note!	2.6 in alley
	4+20			
W -0.9 end picket fence				
	4+25			
W -3.7 E. edge gar.		4.8	374.9	S/y entrance on 10' alley
W		4.5	375.2	
C		5.0	374.7	
E		5.0	374.7	
+10		5.0	374.7	
	4+43			
-10		4.9	374.8	
E		4.6	375.1	
C		4.8	374.9	
W		4.8	374.9	
+3.7 against gar.		5.3	374.4	
	4+49.70	N.L. E+W 10' alley		
W-5 pav.		6.7	373.44	

4+48.2 = End wire fence 0.5 in alley

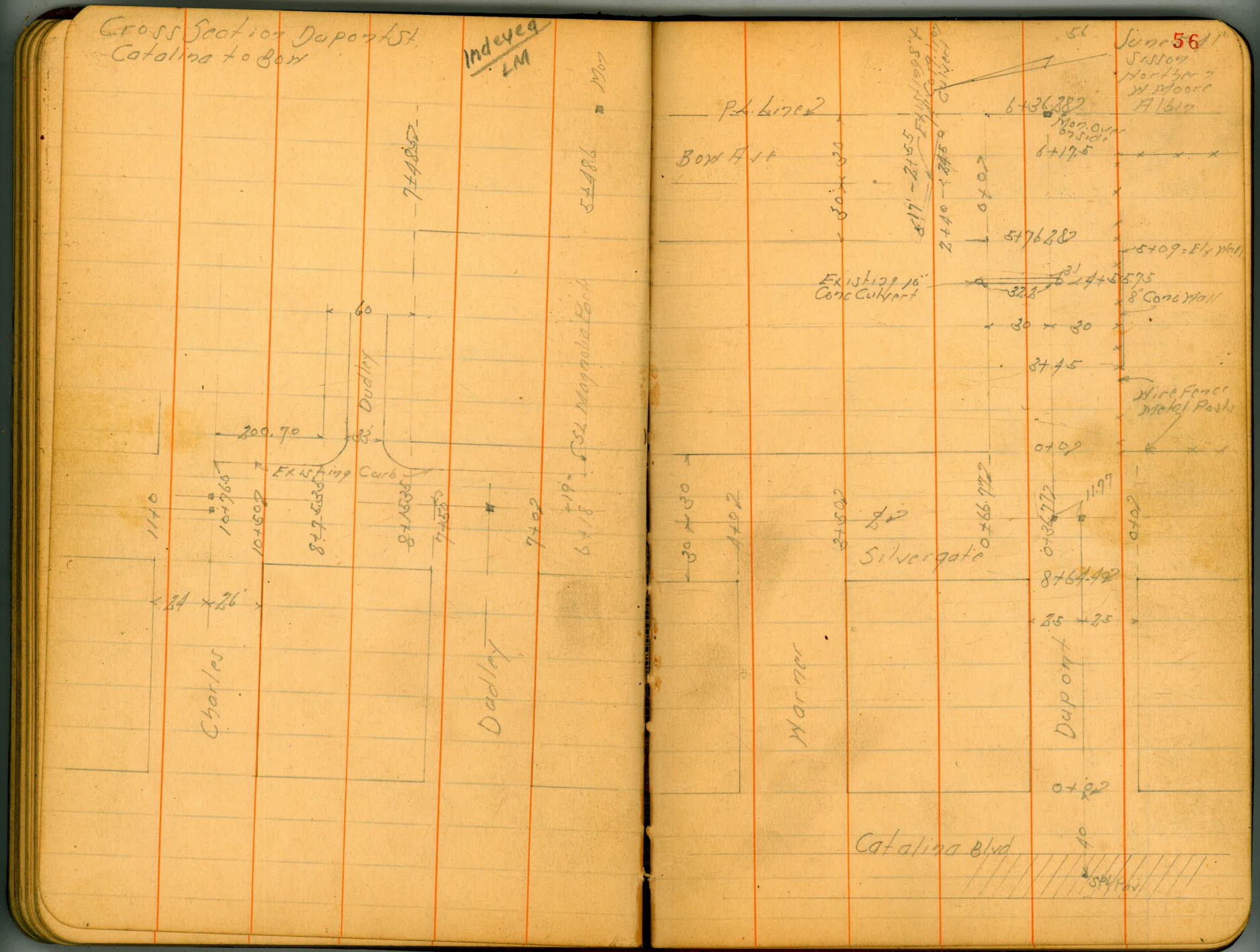
		379.71			
W	pav		6.75	373.46	
C	"		6.30	373.41	
E	"		5.99	373.72	
+5	"		5.90	373.81	
	E INT. of alleys on M.H.				
E of S.M.H			6.31	373.40	
T.P.	3.47	377.98	10.20	369.51	
SEBP			7.00	370.98	371.07
Meade & Hamilton					
	Brass Plugs Taken out & Kids in both B.M.'s				
T.P.	7.19	378.17	7.00	370.98	
check to orig. B.M.			0.95	377.22	377.23

C. Moore
G. Farrow
7-23-41

Add. Notes for New Garage Blk 10 L.U.H.

55

					Meade Oregon
SEBP	4.93	380.16		377.23	
T.P.	4.07	379.96	4.27	375.89	
	1+03				
E-0.3	NL Cem. apron		5.34	374.62	
E-6.3	" 4 Car gar. Cem. floor		4.53	375.43	
	1+21.5				
E-0.25	E Cem. apron		5.48	374.48	
E-6.25	" garage		4.57	375.39	
	1+40				
E-0.2	SL Cem apron		5.57	374.39	
E-6.2	" garage Cem.		4.49	375.47	


Cross Section Dupont St.
Catalina to Bow
Indexed
LM
Mon
7+48.52
5+48.6
60
Dudley
200.70
33
Existing Curb
SL Magnolia Park
11+0
10+76.0
10+50.2
8+75.35
8+15.35
7+50
7+0.2
6+18
24
26
Charles
Dudley
Sunset
Sisson
Northern
W Moore
Albin
P.L. Line
Bow Ave
6+36.28
Mon. Over on Side
6+17.5
5+76.28
5+09 = Elv Wall
Existing 10" Conc Culvert
4+55.75
8" Conc Wall
30
30
3+45
Wire Fence Metal Posts
0+0.2
11.77
Silvergate
8+64.42
25
25
Warner
Dupont
0+0.2
Catalina Blvd
40
Sph Pav

Cross Section Dupont St
Catalina to Bow

See Sketch Page 56

Reduced & Plotted 6-20-41 CBH

0+83 = ℄ 10 Conc Drive on Rt						Lt-N ✓		℄		Rt 5 ✓		
						301.0	301.0	301.0	300.7	301.29	301.98	302.23
						3.0	3.0	3.0	3.3	2.68	1.99	1.74
						25	15		15	21 = N'ly Conc Drive	25 on Dr.	40 on Dr.
0+50						300.4	300.2	300.0	299.7	299.7	300.7	
						3.6	3.8	4.0	4.3	4.3	3.3	
						25	15		15	20	25	
0+25						299.8	299.2	298.7	298.7	298.6	300.1	
						4.2	4.8	5.3	5.3	5.4	3.9	
						25	15		15	20	25	
0+0 = F.L Catalina						299.4	299.3	297.6	296.8	297.2	297.5	297.7	299.6
						4.6	4.7	6.4	7.2	6.8	6.5	6.3	4.4
						25	20	15	10		15	20	25
0-16							296.1		296.6		297.1		
							7.9		7.4		6.9		
							25				25		
0-40 = ℄ Catalina on Paving						296.22	296.65	297.05		297.40	297.70	
						7.75	7.32	6.92		6.57	6.27	
						50	25			25	50	
BM	8.07	303.97		295.90	Mon 20 N NW Cor Catalina & Dupont			303.97 ✓				

							Lt		℄		Rt		
3+0	24.3 Lt of ℄ = Sly 1.5x1.5 Brick Pilaster ✓					307.3	307.4	307.2	307.2	307.2	308.5	308.7	
						3.5	3.4	3.6	3.6	3.6	2.3	2.1	
						25	20	15		15	20	25	
2+50						305.8	306.3	305.7	305.9	305.9	307.1	307.5	
						5.0	4.5	5.1	4.9	4.9	3.7	3.3	
						25	20	15		15	20	25	
2+24.3	24.3 Lt of ℄ = Sly 1.5x1.5 Brick Pilaster ✓												
2+28	21.2 Rt of ℄ = Sly 24" Cypress Tree ✓												
2+0						304.6	305.1	304.4	304.5	304.4	304.6	305.8	306.1
						6.2	5.7	6.4	6.3	6.4	6.2	5.0	4.7
						25	20	15		15	18	20	25
1+50						303.2	303.3	303.6	302.8	303.0	302.8	303.0	304.0
						7.6	7.5	7.2	8.0	7.8	8.0	7.8	6.8
						35	25	20	15		15	20	25
TP	7.17	310.76	0.38	303.59					310.76				
1+27	= ℄ 3.5 Conc Walk on Rt										302.85	303.50	
											1.12	0.47	
											21' = Hly Conc Walk	25 = Top Step on Walk	
1+0						301.4	301.6	301.3	301.5	301.4	301.6	302.7	
						2.6	2.4	2.7	2.5	2.6	2.4	1.3	
						35	25	15		15	20	25	
		303.97							303.97				

Dupont

5+21	19.6 Rt of ℄ = Sly 10" Pepper Tree	✓		
5+02	19.8 Rt of ℄ = Sly 12" Pepper Tree	✓		
5+0				
4+82	20' Rt of ℄ = Sly 10" Pepper Tree	✓		
4+71	= ℄ 7' Conc Drive on Rt			
4+64	23.7 Rt of ℄ = Nly 1x1 Conc Post	✓		
4+50				
4+21	17' Rt of ℄ = ℄ 2' 12" Fac Trees	✓		
4+0	16.2 Rt of ℄ = ℄ 12" Fac Tree	✓		
3+91	17' Rt of ℄ = ℄ 3' 8" Fac Trees	✓		
3+83	21.3 Lt of ℄ = Sly 1.5x1.5 Brick Pilaster	✓		
TP	5.67	315.33	1.10	309.66
3+50				
		310.76		

59

	Lt	℄	Rt	
	310.3	310.4	309.9	310.0
	5.0	4.9	5.4	5.3
	25	20	15	
				311.41
				3.95
				23.5 = NLy Conc Drive
	310.2	310.3	310.4	310.5
	5.1	5.0	4.9	4.8
	25	25	15	
	309.5	309.7	309.7	310.0
	5.8	5.6	5.6	5.3
	25	25	15	
				315.33 ✓
	308.5	308.9	308.4	308.5
	2.3	1.9	2.4	2.3
	25	20	15	
				310.76

	Lt	℄	Rt	
	310.1	311.1	310.9	310.9
	5.2	4.2	4.4	4.4
	10	13	15	25
	311.85			
	3.48			
	30 conc.			
	310.6	311.0	311.6	
	4.7	4.3	3.7	
	12	15	25	
	309.7	310.5	310.9	
	5.6	4.8	4.4	
	12	15	25	
	308.6	309.4	309.6	
	2.2	1.4	1.2	
	15	20	25	

7+04	Ely Conc Dr. on Lt				
7+0					
6+90	= Wly Conc Dr on Lt				
6+65	25.0 Lt of ℄ = Sly 1.5×1.5 Brick Pilaster ✓				
6+50					
TP	0.85	304.89	11.29	304.04	
6+0					
5+65	25' Lt of ℄ = Sly 1.5×1.5 Brick Pilaster ✓				
5+62	20' Rt of ℄ = Sly 6" Pepper Tree ✓				
5+50					
5+42	19.5 Rt of ℄ = Sly 6" Pepper Tree ✓				
		315.33			

Lt.		℄		Rt	
300.95 3.94 25 = Sly Conc					
301.09 3.80 25 on Conc Drive	301.2 3.7 15	301.3 3.6	301.6 3.3 15	301.9 3.0 2.0	302.5 2.4 25
301.62 3.27 25 = Sly Conc Drive					
303.7 1.2 25 = Base 2' High Brick Wall	303.9 1.0 15	303.9 1.0	303.9 1.0 10	304.7 0.2 15	305.3 +0.4 25
		304.89 !			
306.2 9.1 25 = Base 1.3' High Brick Wall	306.4 8.9 20	306.2 9.1 15	306.3 9.0	306.3 9.0 10	307.3 8.0 15	307.7 7.6 25
307.8 7.5 35	308.3 7.0 25	308.5 6.8 20	308.3 7.0 15	308.3 7.0	308.3 7.0 10	309.6 5.7 15	310.0 5.3 25
			315.33		

Dupont

8+69 22.5 Rt of ℄ = Double Pepperidge 8" Diam ✓

8+64.40 = ℄ Silvergate

TP	0.18	293.38	11.69	293.20
8+50				
8+0				
7+80 = ℄ 10' Flag Stone Walk on Rt				
7+50				
7+19 = ℄ 15 Brick Drive on Rt				

304.89

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Lt	℄	Rt	
292.3	291.0	291.4	292.1
1.1 / 25	2.4 / 20	2.0 / 15	1.3
293.38 ✓			
293.2	292.7	292.5	293.1
11.7 / 25	12.2 / 19	12.4 / 15	11.8
296.7	295.3	295.5	296.0
8.7 / 25	9.6 / 18	9.4 / 15	8.9
298.14			
6.75 / 25 = ℄ 10' Flag Stone Walk			
298.4	298.3	298.5	298.4
6.25 / 25	6.6 / 15	6.4	6.5 / 10
301.41			301.79
3.48 / 25 = ℄ 14' Brick Drive			3.10 / 38 on Brick Dr.
304.89			

Lt	Rt	
293.3	293.4	293.6
1.1 / 25	0.0 / 20	+0.2 / 25
293.7	294.4	
11.2 / 15	10.5 / 25 = Base Rock Wall	
296.4	297.1	
8.5 / 15	7.8 / 25 = Base Rock Wall	
298.9	299.9	
6.0 / 15	5.0 / 25 = Base Rock Wall	

						Lt		℄			Rt		
2+50						278.9	278.9	279.1	279.0	278.1	280.4	280.4	280.4
						5.5	5.5	5.3	5.4	6.3	4.0	4.0	4.0
						40	30	20		7	10	20	30
2+0						280.7	281.1	280.9	280.7	279.0	282.1	282.0	282.2
						3.7	3.3	3.5	3.7	4.4	2.3	2.4	2.2
						40	30	20		7	10	20	30
TP	1.88	284.38	10.88	282.50					284.38 ✓				
1+50						282.6	283.1	282.4	282.8	282.4	282.0	284.0	283.8	284.1
						10.8	10.3	11.0	10.6	11.0	11.4	9.4	9.6	9.3
						40	30	25	20		10	12	20	30
1+0						285.2	284.7	285.0	285.0	284.8	284.3	286.0	285.9	286.1
						8.2	8.7	8.4	8.4	8.6	9.1	7.4	7.5	7.3
						30	25	20	10		10	12	20	30
0+50						287.0	287.1	286.9	287.1	287.3	287.0	286.3	288.5	288.1	288.3
						6.4	6.3	6.5	6.3	6.1	6.4	7.1	4.9	5.3	5.1
						40	30	23	20	10		10	12	20	30
0+0 = E.L. Silvergate						289.2	289.4	288.7	288.7	289.2	289.3	290.6	290.6	291.1
						4.2	4.0	4.7	4.7	4.2	4.1	2.8	2.8	2.3
						30	27	25	20		12	14	20	30 Wly Wire Fence
BM			2.84	290.54	℄ Mon Silvergate + Dupont From West									
		293.38							293.38					

Dupont

						Lt		℄		Rt		
4+55.75	℄ 10" Conc Culvert					270.31 6.16 32.2 = Outlet Culv F.L.				271.17 5.30 3.1 = Inlet 10" Conc Culv. Flow Line		
4+50						271.8 4.7 40	272.3 4.2 30	272.8 3.7 20	271.9 4.6	271.8 4.7 10	272.4 4.1 20	272.4 4.1 30	274.40 2.07 30 = Top Wall
								276.47 ✓				
TP	3.50	276.47	11.41	272.97								
4+0						274.0 10.4 40	273.5 10.9 30	273.7 10.6 20	273.4 11.0	273.4 11.0 10	273.6 10.8 20	273.5 10.9 30	275.73 8.65 30 = Top Wall
3+50						275.0 9.4 40	274.8 9.6 30	275.3 9.1 20	275.2 9.2	274.9 9.5 7	276.6 7.8 10	276.2 8.2 20	276.6 7.8 30	277.12 7.26 30 = Top Wall
3+0						277.0 7.4 40	277.7 6.7 30	277.2 7.2 20	277.1 7.3	276.4 8.0 7	278.7 5.7 10	278.6 5.8 20	278.5 5.9 30
		284.38						284.38				

							Lt		℄		Rt		
BM			5.50	270.97	Nail Pole SW Pole Dupont & Bolt		268.4	268.5	268.7	269.3	269.7	270.0	272.2
6+36.28	= E L Bow From N = P.L.						8.1 30	8.0 20	7.8	7.2 20	6.8 30	6.5 50	4.3 100
6+17.5	= Ely Wire Fence on Rt						268.8	268.8	268.8	269.0	269.5	270.2	273.1
							7.9 30	7.7 20	7.7	7.5 20	7.0 30	6.3 50	2.8 100
6+06.28	= ℄ Bow From N						269.0	269.0	268.7	269.3	269.8		
							7.5 30	7.5 20	7.8	7.2 20	6.7 30		
5+76.28	= W.L. Bow From N					269.3	269.1	269.3	269.9	270.3	271.3	271.6	
						7.2 40	7.4 30	7.2 20	6.6	6.2 10	5.2 20	4.9 30	
5+50						271.1	269.5	270.2	271.2	271.3	271.5	272.6	
						5.4 40	7.0 30	6.3 20	5.3	5.2 10	5.0 20	3.9 30	
5+0						271.4	271.2	271.5	271.6	272.0	272.8	272.7	272.91
						5.1 40	5.3 30	5.0 20	4.9	4.5 10	3.7 20	3.8 30	3.56 30 = Top Wall
		276.47							276.47				

Cross Section Silvergate Ave
Dupont to Charles

Indexed
LM

Sec Sketch Page 56

1+87	21.8 Rt of ℄ = Ely Tel Pole		25.3 Lt of ℄ = Wly Pow Pole		
1+50					
1+0					
0+66.77 = N.L. Dupont From E				Plot.	
0+50 = N.L. Dupont From W			30.2 Lt of ℄ = Sly Picket Fence		
0+25 = ℄ Dupont From West					
0+0 = S.L. Dupont From West					
B.M.	3.88	294.42		290.54	℄ Mon Silvergate & Dupont From W Page 62

Scine 9-41

65

Lt = W		℄		Rt = E			
291.4	290.6	289.5	289.4	288.6	289.1	288.5	288.1
3.0 / 30	3.8 / 20	4.9 / 18	5.0	5.8 / 20	5.3 / 22	5.9 / 30	6.3 / 40
291.7	291.2	289.8	289.5	289.9	289.8	289.1	288.4
2.7 / 30	3.2 / 20	4.6 / 18	4.9	5.5 / 20	4.6 / 23	5.3 / 30	6.0 / 40
291.6	291.2	290.1	289.8	288.9	289.3		
2.8 / 30	3.2 / 20	4.3 / 18	4.6	5.5 / 20	5.1 / 30		
	292.2	290.5	290.2	289.4	288.9		
	2.2 / 30	3.9 / 20	4.2	5.0 / 20	5.5 / 30		
	292.1	291.6	290.7	289.4	290.7		
	2.3 / 30	2.8 / 20	3.7	5.0 / 20	3.7 / 30		
293.9	293.5	291.8	291.4	291.2	291.7	291.0	
0.5 / 30	0.9 / 23	2.6 / 20	3.0	3.2 / 15	2.7 / 20	3.4 / 30	

294.42 ✓

						Lt.		℄		Rt.			
3+55	21.8 Rt of ℄ = Fly Tel Pole				✓	292.1	291.0	289.9	289.5	288.9	289.4	288.2	287.6
3+50	= S.L. Warner					5.6 30	6.7 20	7.8 15	8.2	8.8 19	8.3 20	9.5 30	10.1 40
3+36	25.3 Lt of ℄ = Wly Power Pole				✓	291.9	290.9	289.5	289.3	288.6	288.9	287.9	287.5
3+0						5.8 30	6.8 20	8.2 17	8.4	9.1 20	8.8 21	9.8 30	10.2 40
TP	8.40	297.68	5.14	289.28					297.68 ✓				
2+50						291.6	290.8	289.6	289.1	288.3	288.7	288.0	287.6
						2.8 30	3.6 20	4.8 17	5.3	6.1 18	5.7 20	6.4 30	6.8 40
2+06								289.58					
								4.84 16 = ℄ 3.8+3.8 Gas M.H.					
2+0						291.1	290.1	289.6	289.2	288.6	288.6	288.2	287.7
						3.3 30	4.3 20	4.8 17	5.2	5.8 20	5.8 22	6.2 30	6.7 40
1+89	30.2 Lt of ℄ = Wly Picket Fence				✓								
		294.42							294.42				

Silvergate

6+03 28.7 Lt of ℄ = Ely 24" Cypress Tree ✓

6+0

5+66 29.0 Lt of ℄ = Ely 24" Cypress Tress ✓

5+50

5+36 21.7 Rt of ℄ = Ely Anchor Pole ✓ 26.0 Lt of ℄ = Wly Pow Pole ✓

5+23 21.7 Rt of ℄ = Ely Tel Pole

5+0

4+50

4+15 29.3 Lt of ℄ = Ely 24" Cypress Tree ✓

4+0 = N.L. Warner

3+75 = ℄ Warner

29768

Lt.		℄			Rt.		
296.4	295.6	293.6	293.0	292.5	293.1	292.7	291.8
1.3 / 30	2.1 / 20	4.1 / 16	4.7	5.2 / 18	4.6 / 20	5.0 / 30	5.9 / 40
294.7	293.5	292.9	292.2	291.5	292.9	291.7	290.9
3.0 / 30	4.2 / 20	4.8 / 17	5.5	6.2 / 18	4.8 / 20	6.0 / 30	6.8 / 40
294.5	293.3	291.7	291.4	290.7	291.7	290.8	290.4
3.2 / 30	4.4 / 20	6.0 / 15	6.3	7.0 / 20	6.0 / 23	6.9 / 30	7.3 / 40
293.6	292.5	290.9	290.6	290.0	290.5	289.7	288.9
4.1 / 30	5.2 / 20	6.8 / 16	7.1	7.7 / 20	7.2 / 22	8.0 / 30	8.8 / 40
292.5	291.9	290.5	290.0	289.3	289.7	288.2	288.0
5.2 / 30	5.8 / 20	7.2 / 17	7.7	8.4 / 18	8.0 / 20	9.5 / 30	9.7 / 40
	291.6	290.7	289.8	289.2	289.5	288.4	287.7
	6.1 / 30	7.0 / 20	7.9	8.5 / 19	8.2 / 20	9.3 / 30	10.0 / 40

29768

7+30

7+25 = ℄ Dudley

7+01 20.7 Rt = Ely Tel Pole ✓

7+0 = S.L. Dudley From Wart

TP	6.42	301.52	2.58	295.10	
6+92	26.4 Lt of ℄ = Wly Power Pole				✓
6+85	28.8 Lt of ℄ = Ely 24" Cypress Tree				✓
6+50					
6+33	28.8 Lt of ℄ = Ely 24" Cypress Tree				✓
BM		409	293.59	B.P. Ecb Sl. Magnolia 18" Pine & Silverado 293.60	
6+18	= Sly Cb on Rt				
6+16	30.7 Rt of ℄ = Sly Wire Fence				✓

297.68

Lt		℄		Rt	
299.4	298.5	296.1	295.6	295.6	295.13	294.6
3.1 30	3.0 20	5.4 16	6.9 19	6.9 19	6.39 19	6.9 30
297.6		296.6	295.5	294.6	295.09	294.5
3.9 30		4.9 20	6.0	6.9 19	6.43 19	7.0 30
298.6	297.3	295.7	295.1	294.2	294.78	294.2
2.9 30	4.4 20	5.8 16	6.4	7.3 19.1	6.74 19.1 Cb	7.3 30
			30.52 ✓			
297.4	296.5	294.5	294.0	293.3	294.01	293.7	293.0
0.3 30	1.2 20	3.2 16	3.7	4.4 19	3.67 19 Cb	4.0 30	4.7 40
296.7	295.4	293.9	293.4	292.8	293.57	293.0	292.0
1.0 30	2.2 20	3.8 16	4.3	4.9 19 Gutter	4.11 19.5 Cb	4.7 30	5.7 40
			297.68				

Silvergate

8+53 = Conc Walk & Steps on Lt

8+45.35 = ℄ Dudley

8+28.85 = S Cb Dudley From East

8+15.35 = S.L. Dudley From East

8+0

7+50 = N.L. Dudley 31.4 Lt of ℄ = Sly Tile Wall ✓

301.52

Plot 6 - 1941 C.B.H.

	Lt		℄		Rt		
	299.79	299.01	297.51				
	1.73 30 = Wt 4' Walk	2.51 21.2 Top Steps	4.01 17.4 = ℄ Bot 4' Conc Step				
	299.7	298.8	296.7	296.4	295.5	295.1	
	1.8 30	2.7 20	4.8 16	5.1	6.0 19	6.4 30	
	299.7	299.1	296.7	296.4	295.5	295.3	296.11	292.39
	1.8 30	2.4 20	4.8 16	5.1	6.0 19	6.2 30	5.41 30 = Cb	9.13 8 = Cb
	299.9	299.1	296.7	296.4	295.5	296.42	295.8
	1.6 30	2.4 20	4.8 16	5.1	6.0 19	5.10 19	5.7 30
	299.8	299.1	296.7	296.3	295.2	296.13	295.4
	1.7 30	2.4 20	4.8 16	5.2	6.3 19	5.39 19	6.1 30
	299.3	298.7	296.3	295.7	294.8	295.32	294.8
	2.2 30	2.8 20	5.2 16	5.8	6.7 19 = Gut.	6.20 19 = Cb	6.7 30

301.52

9+99 20.5 Rt of Z = Ely Tel Pole ✓

9+78 = Z 5' Conc Step on Lt

9+50

9+10

9+0

8+90 30.8 Lt of Z = Wly Tile Wall ✓

8+88 21.3 Rt of Z = Ely Tel Pole 23.2 Lt of Z = Wly Pow Pole ✓

8+25.35 = NL Dudley From E

8+61.85 = NCL Dudley

30.52

Lt		Z		Rt	
297.62	296.35				
3.90	5.17				
26.2 = Z 5' Top Conc Step	20.2 = Z 6' Step Top Bot Step				
298.4	298.4	296.9	295.3	295.1	294.1	294.69	297.5
6.1 30	6.1 20	4.6 20	6.2 17	6.4	7.4 19	6.83 19	7.0 30
298.8	298.6	296.7	295.8				
4.7 30	4.9 20	4.8 20	5.7				
297.9	297.0	296.4	295.9	294.9	295.61	295.3	
5.6 30	4.5 20	5.1 15	5.6	6.6 19	5.91 19	6.2 30	
299.3	298.6	296.7	296.2	295.1	296.02	295.7	
3.7 30	4.9 20	4.8 16	5.3	6.4 19 = 6w Ht	5.50 19 cb	5.8 30	
299.5	298.8	296.8	296.3	295.4	295.2	296.01	292.08
3.0 30	3.7 20	4.7 16	5.2	6.1 19	6.3 30	5.51 30 cb	9.44 86 cb

30.52

Silvergate

						Lt		℄		Rt	
BM			7.92	292.68	B.P. E Cb Silvergate S.L. Magnolia Park 293.60						
BM	8.90	301.60		292.70	B.P. E Cb Silvergate ℄ Charles						
11+0 = N.L. Charles From W						292.5 9.0 30	291.9 9.6 20	291.2 10.3	291.0 10.5 19	290.8 10.7 30	
BM			8.90	292.62	B.P. E Cb Silvergate ℄ Charles 292.70						
10+76 = N End Cb on Rt						293.9 7.6 30	293.0 8.5 20	291.9 9.6	292.1 9.4 18.75	292.65 8.87 18.75 N.L. End Curb	291.5 10.0 30
10+50 = S.L. Charles From W						294.1 7.4 30	293.5 8.0 20	292.8 8.7	292.4 9.1 19	292.90 8.62 19	292.8 8.7 30
10+20						297.2 4.3 30	296.7 4.8 25	293.9 7.6 20	293.6 7.9		
10+18	25.8 Lt of ℄ = Wly Power Pole										
10+0						297.5 4.0 30	297.3 4.2 25	295.1 6.4 20	294.2 7.3 18	294.1 7.4	293.1 8.4 19 Gatter	293.77 7.75 19 Cb	293.8 7.7 30
		301.52							301.52		

Cross Section Bow Ave
Dupont to Dudley

Indexed
LM

See Sketch Page 56

2+40	= Existing Corg. Iron Culvert				✓
2+47	29.8 Rt of ℄ = Nly 2 Board Fence				✓
2+0					
1+95	20.8 Lt of ℄ = Wly Power Pole				✓
1+50					
1+0					
0+50					
0+07	31 Rt of ℄ = Sly 2 Board Fence				✓
0+0	= N.L. Dupont				
BM	1.24	272.21		270.97	SW Nail Pole Dupont & Bow P64

Sune 16 72

Lt. = W ℄ Rt. E

262.61 — 9.60 — 17 = Outlet 14" Corg Iron Culvert

264.55 — 7.66 — 24.5 = Inlet 8" Corg Iron Culvert

263.7	264.8	265.0	266.8	266.5	266.1	265.8	267.2	266.9
8.5	7.4	7.2	5.4	5.7	6.1	6.4	5.0	5.3
45	30	20	17		20	26	30	40
267.4	267.1	268.6	267.0	267.2	266.4	266.5	267.7	267.1
4.8	5.1	3.6	5.2	5.0	5.8	5.7	4.5	5.1
40	30	20	17		20	26	30	40
269.5	269.1	268.3	267.5	267.8	267.2	267.1	267.8	267.2
2.7	3.1	3.9	4.7	4.4	5.0	5.1	4.4	5.0
40	30	20	18		20	27	30	40
269.6	269.7	269.6	268.3	268.1	267.9	267.7	268.2	267.0
2.6	2.5	2.6	3.9	4.1	4.3	4.5	4.0	5.2
40	30	23	20		20	28	30	40
	269.1	269.2	268.9	268.5	268.3			
	3.1	3.0	3.3	3.7	3.9			
	30	20		20	30			

272.21

Box Arc.

4+50				
TP	0.82	261.60	11.43	260.78
4+12	28.0	Rt of ℄ = ℄ 1" Stand Pipe as Hyd		
4+0				
	31.5	Rt of ℄ = Ely Power Pole		
3+64	22.4	Lt of ℄ = Wly Power Pole		
3+50				
3+0				
2+75				
2+50				
		272.21		

Lt.			℄			Rt	
250.1	251.5	252.2	252.8	254.7	254.8	256.1	261.4
11.5 50	10.1 30	9.1 20	8.8 8	6.9	6.8 20	5.5 24	0.2 30
			261.60				
252.6	256.3	256.8	255.7	258.7	259.0	260.5	264.5
19.6 55	15.9 35	15.4 20	16.5 15	13.5	13.2 20	11.7 24	7.7 30
256.7	257.7	258.9	259.0	260.5	260.9	261.7	266.0
15.5 45	14.5 30	13.3 20	13.2 20	11.7	11.3 20	10.5 25	6.2 30
257.6	259.6	260.2	266.4	263.4	262.7	262.9	266.2
14.6 50	12.6 30	12.0 20	5.8 10	8.8	9.5 20	9.3 24	6.0 30
258.7	261.1	261.6	263.6	264.2	264.6	265.5	266.6
13.5 50	11.1 30	10.6 20	8.6 6	8.0	7.6 20	6.7 30	5.6 40 07 Dirt Drive
261.3	262.1	263.2	266.1	265.5	265.2	266.1	266.6	267.3
10.9 40	10.1 30	9.0 20	6.1 10	6.7	7.0 20	6.1 25	5.6 30	4.9 40
			272.21				

Bow Ave

						Lt		℄		Rt			
7+48.5 = S.L. Dudley From West						232.9	232.9	233.2	236.0	238.1	239.8	241.3	241.0
						19.0	19.0	18.7	15.9	13.8	12.1	10.6	10.9
						47	30	20		20	30	40	60
7+0						236.2	236.4	237.0	238.7	240.6	242.0	243.7	243.6
						15.7	15.5	14.9	13.2	11.3	9.9	8.2	8.3
						50	30	20		20	30	40	60
6+50						237.9	238.1	238.7	239.3	240.5	242.6	243.1	246.2	246.9
						14.0	13.8	13.2	12.6	11.4	9.3	8.8	5.7	5.0
						50	30	20	10		20	30	40	60
6+0						241.1	241.7	241.9	244.4	245.3	247.2	248.7	247.7	250.6
						10.8	10.2	10.0	7.5	6.6	4.7	3.2	4.2	1.3
						50	30	20	5		20	30	32	60
BM			2.00	249.93	Mon SW Cor PL 172									
TP	2-09	251.93	11.76	249.84					251.93					
5+48.6		40' Rt of ℄ = Ely 18" Cypress Tree ✓				243.1	243.6	244.8	246.6	248.0	249.4	249.6	252.1	254.0
						18.5	18.0	16.8	15.0	13.6	12.2	12.0	9.5	7.6
						50	30	20		8	13	30	40	60
5+0						247.6	249.4	249.9	250.8	251.8	251.8	251.8	252.4	258.1
						14.0	12.2	11.7	10.8	9.8	9.8	9.8	9.2	3.5
						50	30	20	5		5	20	23	30
		261.60							261.60					

BM			2.04	293.59	B.P.F. Cb of Silvergate St. Magnolia Park 293.60
TP	12.05	295.63	2.64	283.58	
TP	11.49	286.22	0.21	274.73	
TP	11.44	274.94	0.20	263.50	
TP	12.28	263.70	0.51	251.42	
		251.93			

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Table IX.—Calculation of Earthwork.

Width	HEIGHT														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	.02	.04	.06	.07	.09	.11	.13	.15	.17	.18	.20	.22	.24	.26	.28
2	.04	.07	.11	.15	.18	.22	.26	.30	.33	.37	.41	.44	.48	.52	.56
3	.06	.11	.17	.22	.28	.33	.39	.44	.50	.56	.61	.67	.72	.78	.83
4	.07	.15	.22	.30	.37	.44	.52	.59	.67	.74	.81	.89	.96	1.04	1.11
5	.09	.19	.28	.37	.46	.56	.65	.74	.83	.93	1.02	1.11	1.20	1.30	1.39
6	.11	.22	.33	.44	.56	.67	.78	.89	1.00	1.11	1.22	1.33	1.44	1.55	1.67
7	.13	.26	.39	.52	.65	.78	.91	1.04	1.16	1.30	1.42	1.55	1.68	1.81	1.94
8	.15	.30	.44	.59	.74	.89	1.04	1.19	1.33	1.48	1.63	1.78	1.92	2.08	2.22
9	.17	.33	.50	.67	.83	1.00	1.17	1.33	1.50	1.67	1.83	2.00	2.17	2.33	2.50
10	.18	.37	.56	.74	.93	1.11	1.30	1.48	1.67	1.85	2.04	2.22	2.41	2.59	2.78
11	.20	.41	.61	.82	1.02	1.22	1.43	1.63	1.83	2.04	2.24	2.44	2.65	2.85	3.06
12	.22	.44	.67	.89	1.11	1.33	1.56	1.78	2.00	2.22	2.44	2.67	2.89	3.11	3.33
13	.24	.48	.72	.96	1.20	1.44	1.68	1.92	2.16	2.41	2.65	2.89	3.13	3.37	3.61
14	.26	.52	.78	1.04	1.30	1.55	1.81	2.08	2.33	2.59	2.85	3.11	3.37	3.65	3.89
15	.28	.56	.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	3.06	3.33	3.61	3.89	4.17
16	.30	.59	.89	1.18	1.48	1.78	2.07	2.37	2.67	2.96	3.26	3.56	3.85	4.15	4.44
17	.31	.63	.94	1.26	1.57	1.89	2.20	2.52	2.83	3.15	3.46	3.78	4.09	4.41	4.72
18	.33	.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	3.67	4.00	4.33	4.67	5.00
19	.35	.70	1.06	1.41	1.76	2.11	2.46	2.82	3.17	3.52	3.87	4.22	4.57	4.92	5.28
20	.37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	4.07	4.44	4.81	5.18	5.56
21	.39	.78	1.17	1.55	1.94	2.33	2.72	3.11	3.50	3.89	4.28	4.67	5.06	5.44	5.33
22	.41	.81	1.22	1.63	2.04	2.44	2.85	3.26	3.67	4.07	4.48	4.89	5.30	5.70	6.11
23	.43	.85	1.28	1.70	2.13	2.56	2.98	3.41	3.83	4.26	4.68	5.11	5.54	5.96	6.39
24	.44	.89	1.33	1.78	2.22	2.67	3.11	3.56	4.00	4.44	4.89	5.33	5.78	6.22	6.67
25	.46	.92	1.39	1.85	2.31	2.78	3.24	3.70	4.17	4.63	5.09	5.56	6.02	6.48	6.94
26	.48	.96	1.44	1.92	2.41	2.89	3.37	3.85	4.33	4.82	5.30	5.78	6.26	6.74	7.24
27	.50	1.00	1.50	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00	6.50	7.00	7.50
28	.52	1.04	1.55	2.07	2.59	3.11	3.63	4.15	4.67	5.18	5.70	6.22	6.74	7.26	7.78
29	.54	1.07	1.61	2.15	2.68	3.22	3.76	4.30	4.83	5.37	5.91	6.44	6.98	7.52	8.06
30	.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.55	6.11	6.67	7.22	7.78	8.33
31	.57	1.15	1.72	2.30	2.87	3.44	4.02	4.59	5.17	5.74	6.32	6.89	7.46	8.04	8.61
32	.59	1.18	1.78	2.37	2.96	3.56	4.15	4.74	5.33	5.92	6.52	7.11	7.70	8.30	8.89
33	.61	1.22	1.83	2.44	3.05	3.67	4.28	4.89	5.50	6.11	6.72	7.33	7.94	8.55	9.17
34	.63	1.26	1.89	2.52	3.15	3.78	4.40	5.04	5.67	6.29	6.93	7.56	8.18	8.81	9.44
35	.65	1.30	1.94	2.59	3.24	3.89	4.53	5.18	5.83	6.48	7.13	7.78	8.42	9.08	9.72
36	.67	1.33	2.00	2.67	3.33	4.00	4.66	5.33	6.00	6.67	7.33	8.00	8.67	9.33	10.00
37	.68	1.37	2.06	2.74	3.42	4.11	4.79	5.48	6.17	6.85	7.54	8.22	8.91	9.59	10.28
38	.70	1.41	2.11	2.82	3.52	4.22	4.92	5.63	6.33	7.03	7.74	8.44	9.15	9.85	10.56
39	.72	1.44	2.17	2.89	3.61	4.33	5.05	5.78	6.50	7.22	7.95	8.67	9.39	10.11	10.83
40	.74	1.48	2.22	2.96	3.70	4.44	5.18	5.92	6.67	7.41	8.15	8.89	9.63	10.37	11.11

Table gives cu. yds. in 1 ft. of a triangle of given width and height. Corrections for tenths of width are one tenth the values found under each height considering the widths from 1 to 9 as tenths and similarly the corrections for tenths of height are one tenth the figures opposite width considering the heights from 1 to 9 as tenths. Thus if w =16.2 and h =5.3, cu. yds. =1.48+.028+.089 =1.597 cu. yds. or practically 160 cu. yds. per 100 ft. If w exceeds 40 ft., use one half and multiply result by 2, if both w and h are large use one half of each and multiply result by 4. Any cross-section may be divided into triangles by the following rule. To the triangle of the sum of the outside cuts (or fills) =h, and ½ the roadbed =w, add the triangles formed by taking the distance out to each break in turn (=w's) by the difference between the cuts (or fills) on each side of it (=h's) always subtracting the outer from the inner.

Distances from Center of Roadway for Cross-Sectioning.

Roadway 16 feet wide. Side Slopes 1 on 1½.

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	25.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20—16)÷2 or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.

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