F.B.
826

FIELD BOOK

No. 410

MICROFILMED

DEC 15 1964

RETURN TO CITY ENGINEER'S OFFICE
CITY HALL, SAN DIEGO, CAL.

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CITY HALL, SAN DIEGO, CAL.

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Connection between sta 12+45? 12+75 on alley between Alabama & Florida and sta 2+85 on Florida

Sta	+ R.	H.I.	- R.	elev	Grade
~~Sta~~	4.79	257.79		253.00	
0+0 = M.H. Alley					245.00
0+50			6.2	251.6	246.16
1+0	POSTED		5.4	252.4	247.33
1+50			5.6	252.2	248.49
2+0			6.2	251.6	249.66
2+15 = M.H. Florida			5.3	252.5	250.0

5

1

B.M. 253.00
4.13
257.13

cut				
	57.13	57.13	57.13	57.13
	46.16	47.33	48.49	49.66
	10.97 ✓	9.80 ✓	8.64 ✓	7.47 ✓
5.4 ✓				
5.1 ✓				
3.7 ✓				
1.9 ✓				
2.5				

1.17
1.14
1.7

2

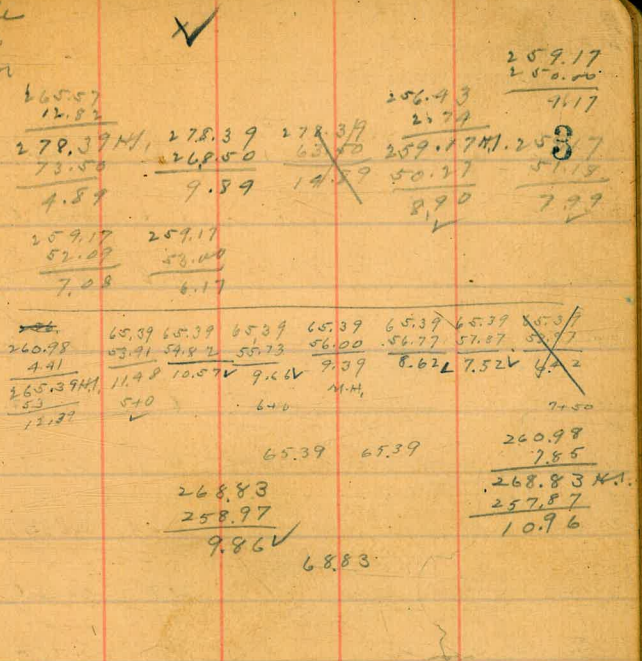
57.13
50
7.13

Levels on top stakes ℄ Florida St from 25 N of N.L. University to 25's of S.L. Alley between ℄ Cajon & Howard.

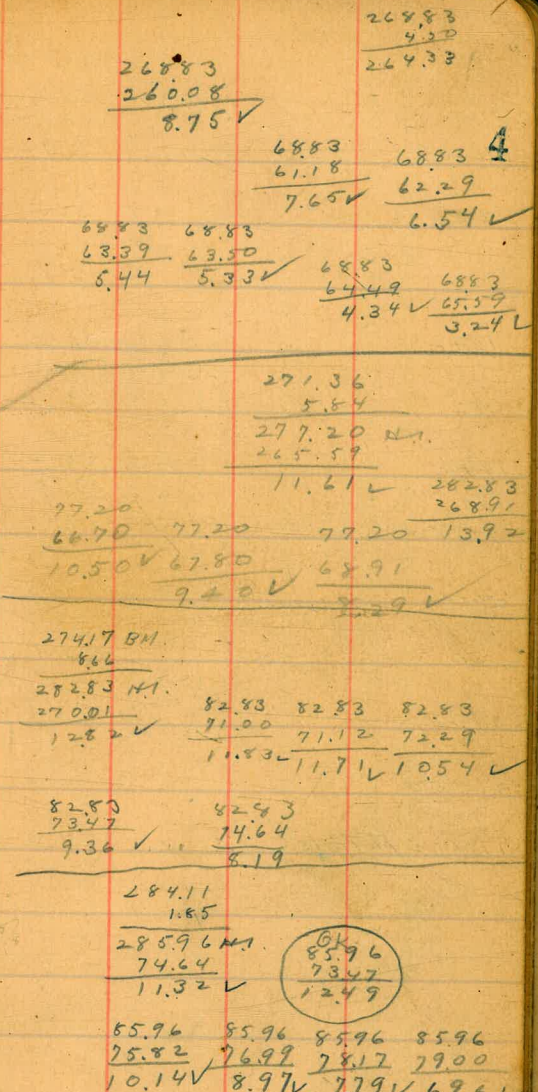
	+ R.	H.I.	− R	elev H.I. stake	Grade
B.M. Mon N.E. Alley Univ				265.57	
B.M.	12.96	278.53			
T.P.	7.05	285.54	0.04	278.49	
0+0 = dead end 25' N. of NL Univ			1.60	278.89	278.50
50			3.28	282.26	278.50
1+0			8.3	277.2	268.50
T.P.	1.20	278.01	12.73	272.81	
1+50			2.60	271.4	263.50
2+0			7.23	266.78	258.50
2+50			11.2	262.8	253.50
T.P.	3.22	269.91	12.32	261.69	
2+85 = N.H. when sewer goes to Main going down alley bet Florida & Alabama.			12.40	257.5	250.0
3+0			11.80	258.1	250.27
3+50			11.3	253.6	251.18
4+0			8.48	256.43	252.09
5+0			7.0	257.9	253.00
5+0			4.8	260.1	253.91
5+50			5.6	259.3	254.82
6+0			4.2	260.7	255.73
6+45 = N.H. & Lincoln			4.4	260.5	256.00
6+50			3.93	260.98	256.77
7+0			2.8	262.1	257.87
1+50			4.22	263.69	258.97
T.P.	11.31	274.00	4.22	263.69	

10/30/11 Dimple Evans. Medium

cut



		275.00				
8+0			10.9	264.1	260.08	4.0 ✓
8+50			10.6	264.4	261.18	3.2 ✓
9+0			18.8	266.2	262.29	3.9 ✓
9+50			6.8	268.2	263.39	4.8
9+55 — M.H.			6.8	268.2	263.50	4.7 ✓
10+0			9.3	270.7	264.99	5.2 ✓
10+50			3.64	271.36	265.57	5.8 ✓
11+0			2.9	272.6	266.70	5.9 ✓
50			1.6	273.4	267.80	5.6 ✓
12+0			1.6	273.4	268.91	4.5 ✓
50			0.83	274.17	270.01	4.2 ✓
T.P.	9.73	283.90	0.83	274.17		
12+95 ℄ Pole M.H.			8.5	275.4	271.00	4.4 ✓
13+0			5.4	275.8	271.12	4.4 ✓
50			7.9	276.0	272.29	3.7 ✓
14+0			6.2	277.7	273.47	4.2 ✓
50			5.3	278.6	274.64	4.0 ✓
15+0			4.2	279.7	275.82	3.9 ✓
50			2.4	281.5	276.99	4.5 ✓
T.P.	10.96	294.32	0.44	283.46		
16+0			10.21	284.11	278.17	5.9 ✓
16+35 — M.H.			8.4	285.9	279.00	6.9 ✓



		294.32				
16+50			7.9	286.4	279.35	7.0 ✓
17+0			5.5	288.8	280.53	8.3 ✓
50			2.8	291.5	281.70	9.8 ✓
18+0			0.62	293.70	282.88	10.8 ✓
T.P.	4.40	298.10	0.62	293.70	"	
50			3.9	294.2	284.05	10.2 ✓
19+0			5.2	292.9	285.23	7.7 ✓
19+50			6.0	292.1	286.40	5.7 ✓
19+75 ℄ Howard. M.H.			6.6	291.5	287.00	4.5 ✓
20+00			6.5	291.6	287.27	4.3 ✓
50			6.1	292.0	287.80	4.2 ✓
21+0			5.3	292.8	288.34	4.5 ✓
21+50			4.80	293.30	288.87	4.4 ✓
21+66 = P.T. = 25' S of Alley			4.4	293.7	289.05	4.7 ✓

293.30 B.M.
3.80
297.10 H.I.
288.87
8.23 ✓

97.10 97.10 97.10
89.05 88.34 87.80
8.05 ✓ 8.76 ✓ 9.30 ✓

97.10 97.10 97.10
87.29 87.28 87.00
9.30 9.83 10.10 ✓
9.78 ✓

97.10 97.10 97.10
86.40 85.23 84.05
10.70 11.87 ✓ 13.05

285.96 H.I.
279.35
6.61 ✓

85.96 85.96 85.96
80.53 81.70
5.43 ✓

293.70
3.35
297.05 H.I.
281.70
15.35 ✓

97.05 97.05 97.05
82.88 84.05 85.23
14.17 ✓ 13.00 ✓ 11.82

6" Sewer & Alley between Texas & Arizona from ℄ Alley between El Cajon & Howard, To E.T. 30' N of N.L. Polk,

Sta	+ R	H.I.	− R	elev top Stake	Grade
	0.47	333.70		333.23	
T.P.	5.38	328.85	8.20	325.50	
0+0					319.00
0+50			5.49	325.39	319.23
1+0			5.9	325.0	319.47
50			6.0	324.9	319.71
2+0			6.4	324.5	319.24
2+27.5 = M.H. ℄ Howard			6.2	324.7	320.07
2+50			5.8	325.1	320.18
3+0			5.8	325.1	320.92
50			5.0	325.9	320.65
4+0			5.0	325.9	320.89
50			4.98	325.90	321.13
5+0			4.8	326.1	321.36
5+27.5 = M.H.			4.9	326.0	321.49
5+50			5.3	325.6	321.60
6+0			5.0	325.9	321.89
6+50			4.4	326.5	322.07
7+0			3.4	327.5	322.31
7+50			3.3	327.6	322.54

POSTED

3

√

cut,

325.90 − 3.55 = 329.45 T.H. − 19.00 = 10.45

329.45 − 19.23 = 10.22 ✓

329.45 − 19.47 = 9.98 ✓

329.45 − 19.71 = 9.74 ✓

329.45 − 19.94 = 9.51 ✓

329.45 − 20.07 = 9.38 M.H. ✓

6

329.45 − 20.18 = 9.27 ✓

325.90 B.M. − 3.85 = 329.75 H.I. − 320.42 = 9.33 ✓

329.75 − 20.65 = 9.10 ✓

329.75 − 20.89 = 8.86 ✓

329.75 − 21.18 = 8.62 ✓

329.75 − 21.36 = 8.39 ✓

6.2 ✓

329.75 − 21.49 = 8.26 ✓

329.75 − 21.60 = 8.15 ✓

329.75 − 21.84 = 7.91 ✓

329.75 − 22.07 = 7.68 ✓

329.75 − 22.31 = 7.44 ✓

5.5 ✓

329.75 − 22.54 = 7.21 ✓

5.2 ✓

4.6 ✓

4.6 ✓

4.9 ✓

4.7 ✓

5.3 ✓

5.0 ✓

4.8 ✓

4.7 ✓

4.5 ✓

4.0 ✓

4.1 ✓

4.4 ✓

5.2 ✓

5.1 ✓

	330.98			cut	
8+0		3.0	327.9	322.78	5.1 ✓
8+37.2 = F.T. 30'W. of N.L. P&K		3.2	327.7	323.00	4.7

329.75 = P.T.
322.78
6.97 ✓

329.75
323.00
6.75

Sewer line ℄ Texas from ℄ Alley S of El Cajon to ℄ Alley N of El Cajon.

	+ R	H.I.	− R	elev. top Stake	Grade
B.M. Mon S.W. Texas & El Cajon				322.14	
B.M.	10.43	332.57			
0+0					315.00
50			11.5	321.1	316.33
1+0			10.5	322.1	316.67
50			9.6	323.0	316.66
2+0			8.5	329.1	316.34
2+25					316.51
50			6.5	326.1	316.67
2+75					316.84
3+0			8.4	324.2	317.00
50			8.5	324.1	317.34
4+0			8.0	324.6	317.67
A+45 = N.W.℄ Alley			7.6	325.0	318.00

POSTED

B.M. 322.14 + 4.78 = 326.92 H.I.

26.92 − 15.33 = 11.59	26.92 − 15.67 = 11.25	26.92 − 16.00 = 10.92	26.92 − 16.34 = 10.58	26.92 − 16.67 = 10.25	
26.92 − 17.00 = 9.92	26.92 − 17.34 = 9.58	26.92 − 17.67 = 9.25	26.92 − 18.00 = 8.92		

5.8 ✓ 6.4 ✓ 7.0 ✓ 7.8 ✓ 9.3 Not Set ✓ 7.2 ✓ 6.8 ✓ 6.9 ✓ 7.0 ✓

322.14 + 6.94 = 329.08 H.I. − 317.34 = 11.74

322.14 + 6.57 = 328.71 H.I. − 316.51 = 12.20 ✓ ; 28.71 − 17.00 = 11.71 ; 316.84 = 11.87 ✓

329.08 − 317.67 = 11.41 ✓ ; 329.08 − 318.00 = 11.08 ✓

329.08 = H.I. − 3.34 = 325.74 = B.M.

Sewer line & Line of Alley N of El Cajon from
F.T. 25' E of & Alley between Mississippi & Louisiana
To & Alley between Oregon & Idaho.

	+ R	H.I	− R	elev top of Rail	Grade
B.M. Mon S.W. El Cajon & Texas				322.14	
B.M.	10.43	332.57			
0+0 F.T.					328.00
50	POSTED		0.92	331.65	326.88
1+0			2.2	330.4	325.75
50			4.2	328.4	324.63
2+0			5.5	327.1	323.50
50			5.8	326.8	322.36
3+0			6.6	326.0	321.24
+50			7.9	324.7	320.11
+54.7 M.H. Alley			7.9	324.7	320.00
4+0			9.1	323.5	319.53
50			8.9	323.7	319.00
5+0			8.5	324.1	318.48
5+44.7 M.H. at Texas			7.6	325.0	318.00
+50			7.3	325.3	318.10
6+0			7.2	325.4	319.16
50			6.6	326.0	320.21
7+0			6.3	326.3	321.27
7+84.7 M.H. Alley			4.9	327.7	322.00

5

X

331.65 B.M.
1.33
332.98 H.I.
326.88
6.10 ✓

Cut

5.4	
4.8 ✓	
4.7 ✓	
3.8 ✓	
3.6 ✓	
4.2 ✓	.53
4.8 ✓	
4.6 ✓	
4.7 ✓	
4.0 ✓	
4.7 ✓	
5.16 ✓	
7.0 ✓	
7.2	
6.2 ✓	
5.8 ✓	
5.0 ✓	
5.7	

32.98 / 25.75 / 7.23 ✓
32.98 / 24.68 / 8.35 ✓
32.98 / 23.50 / 9.48 ✓
32.98 / 22.36 / 10.62 ✓

32.98 / 21.24 / 11.74 ✓
32.98 / 20.11 / 12.87 ✓
32.98 / 20.00 / 12.98 ✓

332.98 H.I.
4.30
324.68 T.P.
4.21
328.89

328.89 / 320.00 / 8.89
28.89 / 19.53 / 9.36
28.89 / 19.00 / 9.89
28.89 / 18.88 / 10.01

324.68
4.15
328.83 H.I.
320.00
8.83 ✓

28.83 / 19.53 / 9.30 ✓
28.83 / 19.00 / 9.83 ✓

28.83 / 18.48 / 10.35 ✓
28.83 / 18.00 / 10.83 ✓
28.83 / 18.10 / 10.73
28.83 / 19.16 / 9.67 ✓

28.83 / 20.21 / 8.62 ✓
28.83 / 21.27 / 7.56 ✓
28.83 / 22.00 / 6.83

Sec 474-50

		332.57				
2+50			4.5	328.1	322.79	5.3
8+00			1.4	331.2	325.42	5.8
T.P.	12.07	343.92	0.72	331.85		
50			10.4	333.5	328.05	5.5
9+00			6.5	337.4	230.68	6.7
9+24 M.H. E. Arizona			6.5	337.4	332.00	5.4
9+50			5.1	238.8	339.63	4.2
T.P.	12.94	356.76	0.10	343.82		
10+00			12.3	344.5	339.89	4.6
50			5.5	351.3	345.15	6.2
T.P.	12.30	368.68	0.38	356.38		
11+00			11.54	357.14	350.41	6.7
11+15 Alley			10.3	358.4	352.00	6.4
+50			7.0	361.7	354.21	7.5
12+00			3.9	365.8	357.37	8.4
T.P.	10.37	378.91	0.14	368.54		
50			9.8	368.1	360.52	7.6
13+00			9.1	369.8	363.68	6.1
13+05 15 Hamilton			9.5	369.4	364.00	5.4
13+50			8.1	370.8	364.71	6.1
14+00			6.0	372.9	365.50	7.4
14+50			4.7	374.2	386.29	7.9
14+95 3 M.H. Alley			4.0	374.9	367.00	7.9

	378.91			
15+0	3.6	375.3	367.03	8.3
50	4.5	374.4	367.29	7.1
16+0	5.0	373.9	367.55	6.4
50	4.8	374.1	367.81	6.3
17+0	4.5	374.4	368.08	6.3
50	3.7	375.2	368.34	6.9
18+0	3.7	375.2	368.60	6.6
18+50	3.4	375.5	368.87	6.6
18+75 ^{2} = M.H. & Alley	3.5	375.4	369.00	6.4

Sewer & Alley between Arizona & Texas from & Alley N of El Cajon To & Madison

St	+ R	H.I	- R	elev top stakes	Grade
B.M.	B.P. Mon S.W. Texas & El Cajon			322.19	
B.M.	12.56	339.70			
0+0 = M.H. & Alley N of El Cajon			7.0	327.7	322.00
0+50			5.4	329.3	322.81
1+0	POST		5.2	329.5	323.62
1+5			4.06	330.64	324.42
2+0			3.1	331.6	325.23
2+50 = M.H.			2.4	332.3	326.03
3			0.68	B.M. 334.02	326.84
T.P.	7.17	341.49	0.68	334.02	
+50			8.4	333.1	327.65
4+0			7.9	333.6	328.45
+50			7.4	334.1	329.26
4+94.7 = M.H. & Meade			4.5	337.0	330.00
5+0			4.5	337.0	330.05
+50			6.3	335.2	330.99
6+0			5.9	335.6	330.93
+50			5.1	336.4	331.37
7+0			4.5	337.0	331.81
50			4.3	337.2	332.25
			3.8	337.7	

12

cut

328.83 / 322.81 = 6.02 H.I.
28.83 / 23.62 = 5.21
34.34 / 21.27 = 13.07
330.64 / 3.70
334.34 / 322.00 = 12.34
334.34 / 22.81 = 11.53 ✓
34.34 / 23.62 = 10.72 ✓
34.34 / 24.42 = 9.92 ✓
34.34 / 25.23 = 9.11 ✓

5.7 ✓
34.34 / 26.03 = 8.31 ✓
34.34 / 26.84 = 7.50 ✓
34.34 / 27.65 = 6.69 ✓
34.34 / 28.45 = 5.89 ✓

6.4 ✓
334.02 / 5.56
39.57 / 28.45 = 11.12 chk

5.9 ✓
339.57 H.I. / 326.44 = 12.14
39.57 / 29.26 = 10.31 ✓
39.57 / 30.00 = 9.57 ✓
39.57 / 30.05 = 9.52

6.2 ✓
39.57 / 30.49 = 9.08 ✓
39.57 / 30.93 = 8.64 ✓
39.57 / 31.37 = 8.20 ✓
39.57 / 31.81 = 7.76 ✓
39.57 / 32.25 = 7.32 ✓

6.4 ✓
339.57 H.I. / 2.38
337.19 T.P. / 5.31
342.50

6.3 ✓
7.2 ✓
5.5 ✓
5.2 ✓
9.8 ✓
7.00 ✓
7.0
4.7 ✓
4.7 ✓
5.0 ✓
5.2 ✓
5.0 ✓

		341.49			
8+0			3.8	337.7	332.69
8+34 2 M.H.			3.9	337.6	333.00
+50			3.8	337.7	333.13
9+0			3.13	338.36	333.57
T.P.	9.28	347.64	3.13	338.36	
50			7.4	340.2	334.01
10+0			7.7	339.9	339.45
50			7.1	340.5	334.89
11+0			5.4	342.2	336.33
50			4.7	342.9	336.77
11+75 2 M.H. ℄ Monroe ✓			4.5	343.1	336.00
12+0			4.1	343.5	336.33
50			3.5	344.1	336.98
13+0			3.10	B.M. 344.54	337.65
50			2.7	344.9	338.81
14+0			2.5	345.1	338.97
50			2.1	345.5	339.63
15+0			1.63	B.M. 346.01	340.29
	9.20	355.21	1.63	346.01	
15+15 2 M.H ✓			9.0	346.2	340.50
T.P.					
50			8.8	346.4	340.96
16+0			8.1	347.1	341.62

347.58
344.54
3.04

En el Pelo de las riejas hace un mido los ratones

42.50
32.25
10.25 chk

342.50
338.36
4.14

5.0 ✓	342.50 H.I. 32.69 9.81 ✓			
4.6 ✓		42.50 33.00 9.50 ✓	42.50 33.13 9.37 ✓	42.50 33.57 8.93 ✓
4.6 ✓	338.36 9.22 347.58 334.01 13.57 ✓			
4.8 ✓		47.58 34.45 13.13 ✓	47.58 34.89 12.69 ✓	47.58 35.33 12.25 ✓
6.2 ✓				47.58 35.77 11.81 ✓
5.5 ✓	47.58 36.00 11.58 ✓	47.58 36.33 11.25 ✓	47.58 36.99 10.59 ✓	47.58 37.65 9.93
5.6 ✓	344.54 5.18 349.72 H.I. 337.65 12.07 ✓			47.58 38.31 9.27
6.9 ✓		49.72 38.31 11.41 ✓	49.72 38.97 10.75 ✓	49.72 39.63 10.09 ✓
7.1 ✓	49.72 40.01 9.71			49.72 40.29 9.43 ✓
7.1 ✓	49.72 40.50 9.22 ✓	49.72 40.96 8.76 ✓	49.72 41.62 8.10 ✓	49.72
7.2 ✓				
7.1 ✓				
6.9 ✓				
6.6 ✓				
6.1 ✓				
5.9 ✓				
5.7 ✓				
5.7 ✓				
5.4 ✓				
5.5 ✓				

355.21

16+50	7.4	347.8	342.28	
17+0	6.6	348.6	342.94	
50	5.5	349.7	343.60	
		B.M		
18+0	4.64	350.57	344.26	
50	2.9	352.3	344.93	
18+55 M.H. 4, Madison	2.6	352.6	345.00	

See Book 933-76 for contin. levels

5.5	✓
5.7	✓
6.1	✓
6.3	✓
7.4	
7.6	✓

49.72 − 42.28 = 7.44 ✓
49.72 − 42.94 = 6.78 ✓
49.72 − 43.60 = 6.12 ✓
355.87 − 343.60 = 12.27 ✓

14

350.57 + 5.30 = 355.87 N.1
355.87 − 44.26 = 11.61 ✓
55.87 − 44.93 = 10.94
55.87 − 45.00 = 10.87 ✓

Sewer beginning at M.H. ℄ Polk & Alley between Florida & Alabama Thence E To ℄ Alabama Thence N on ℄ Alb To F.T. 30's of Alley between El Cajon & Howard.

Sta	+ R	H.I.	− R	elev for 8 Tanks	Grade
B.M.				278.59	
B.M.	10.31	288.90			
0+0 = M.H. ℄ Polk & Alley					273.00
50			6.8	282.1	275.63
1+0			2.8	286.1	278.26
1+50			0.30	B.M. 288.60	280.90
T.P.	5.80	294.40	0.30	288.60	
1+90 = M.H. ℄ Polk & Alley			2.9	291.5	283.90
2+0			3.2	291.2	283.65
50			3.6	290.8	283.27
3+0			4.4	290.0	283.49
50			5.2	289.2	283.71
4+0			5.6	288.8	283.93
50			5.6	288.8	284.15
5+0			5.7	288.7	284.37
5+30 = M.H.			5.4	289.0	284.50
5+50			5.3	289.1	284.59
6+0			5.0	289.4	284.81
50			5.3	289.1	285.03
7+0			4.7	289.7	285.25

POSTED

5

cut

6.5 ✓
7.8 ✓
7.7 ✓
8.5 ✓
8.2 ✓
7.5 ✓
6.5 ✓
5.5 ✓
4.9 ✓
4.6 ✓
4.3 ✓
9.5 ✓
4.5 ✓
4.6 ✓
4.1 ✓
4.5 ✓

15

278.54 B.M.
9.16
287.70 H.I.
275.63
12.07 ✓

87.70 / 78.26 = 9.44 ✓
87.70 / 80.90 = 6.80

288.60
5.69
294.29 H.I.
280.90
13.39 ✓

94.29 / 83.00 = 11.29 ✓
94.29 / 83.05 = 11.24 ✓
94.29 / 83.27 = 11.02 ✓

94.29 / 83.49 = 10.80 ✓
94.29 / 83.71 = 10.58 ✓
94.29 / 83.93 = 10.36 ✓
94.29 / 84.15 = 10.14 ✓
94.29 / 84.37 = 9.92

249.89 = B.M.
3.94
293.83 = H.I.
284.37
9.46 ✓

93.83 / 84.50 = 9.33 ✓
93.83 / 84.59 = 9.24 ✓

93.83 / 84.81 = 9.02 ✓
93.83 / 85.03 = 8.80 ✓
93.83 / 85.25 = 8.58 ✓

		294.40				
7+50			4.51	289.89	285.47	4.4 ✓
T.R.	9.39	299.28	4.51	289.89		
8+00			9.2	290.1	285.69	4.4 ✓
7+50			7.3	292.0	285.91	6.1 ✓
8+70 M.H. @ Howard			7.5	291.8	286.00	5.8 ✓
9+00			6.9	292.9	287.12	5.8 ✓
50			5.1	294.2	288.99	5.2 ✓
10+00			3.0	296.3	290.86	5.4 ✓
50			2.3	297.0	292.73	4.3 ✓
10+57 = F.T. 30's of S.L. Alley			2.5	296.8	293.00	3.8 ✓

293.83 = H.I.

93.83 − 85.47 = 8.36 ✓
93.83 − 85.69 = 8.14 ✓
93.83 − 85.91 = 7.92 ✓
93.83 − 86.00 = 7.83
93.83 − 87.12 = 6.71

289.89 + 8.43 = 298.32 H.I.
298.32 − 285.91 = 12.41
298.32 − 287.12 = 11.20 ✓

98.32 − 86.00 = 12.32 ✓
98.32 − 88.99 = 9.33 ✓
98.32 − 90.86 = 7.46
98.32 − 92.73 = 5.59

289.89 + 9.60 = 299.49 H.I.
299.49 − 288.99 = 10.50

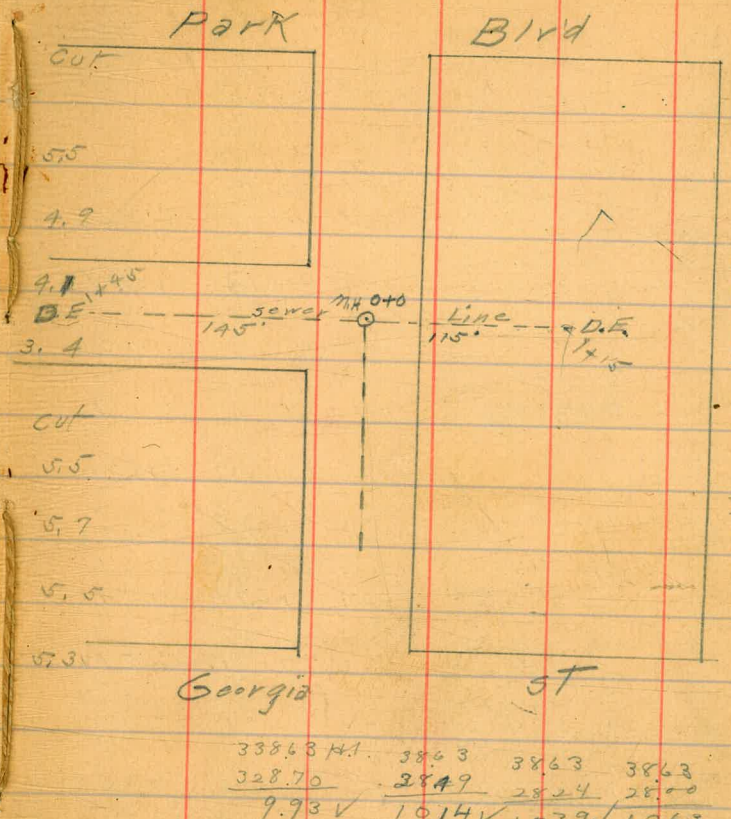
99.49 − 90.86 = 8.63
99.49 − 92.73 = 6.76

99.49 − 93.00 = 6.49

Sewer Line see opp Page

Sta	+ R	H.I.	- R	elev on stakes	Grade
B.M. = B.P. drive ways to normal	1.35	344.93		343.58	
B.M. T.P.	4.64	338.10	11.47	333.46	
0+05			4.6	333.5	328.00
0+50 S			4.99	B.M. 333.11	328.24 ✓
1+0	POSTED		5.5	332.6	328.49 ✓
1+45			6.0	332.1	328.70 ✓
		338.10			
0+0 N			4.6	333.5	328.00
0+50 N	Note stakes set 15' W of E.		4.0	334.1	328.43 ✓
1+0			3.7	334.4	328.87 ✓
1+15			3.8	334.3	329.00 ✓

5



338.68 H.I.

38.63	38.63	38.63	38.63
328.70	328.49	328.24	328.00
9.93 ✓	10.14 ✓	10.39 ✓	10.63

38.63	38.63	38.63	38.63
28.43	28.87	29.00	
10.20 ✓	9.76 ✓	9.63 ✓	

Sewer Line in ℄ Alley between El Cajon & Howard, from ℄ Alley E. of Park Blvd To 25' W. of W.L.

Mission Appl

Sta.	+ B.S.	H.I.	− F.S.	Elev. Top of Curb	Grade
B.M.- brass plg drive way to Normal				343.58	
B.M.	1.35	344.93			
T.P.	4.64	338.10	11.47	333.46	
0+0=M.H.			4.6	333.5	328.00
0+50			8.97	329.13	323.79
T.P.	1.43	326.82	12.71	325.39	
1+0			3.9	322.9	319.58
1+50	POSTED		7.2	319.6	315.37
1+90 M.H. ℄ Georgia			8.3	318.5	312.00
2+0			9.1	317.7	311.36
T.P.	1.44	315.30	12.96	313.86	
2+50			2.51	312.79	308.19
3+0			4.2	311.1	305.01
3+50			5.7	309.6	301.84
3+78.5 M.H. ℄ Alley bet. Florida & Ga.			9.3	306.0	300.00
4+0			11.12	B.M. 304.18	298.78
T.P.	0.89	303.31	12.88	302.42	
4+50			2.4	300.9	295.89
5+0			4.1	299.2	292.99
5+50			8.6	294.7	290.10
5+69 M.H. ℄ Florida			9.1	294.2	289.00
6+0			9.4	293.9	288.35
6+50			13.8	289.5	287.30

18

Cut

329.13
9.50
338.63 H.I.
2379
38

5.5 ✓
5.3 ✓
3.3 ✓
4.2 ✓
6.5
6.3 ✓
4.6 ✓
6.1 ✓
7.8 ✓
6.0
5.4 ✓
5.0 ✓
6.2 ✓
4.6 ✓
5.2 ✓
5.6 ✓
2.2 ✓

329.13
2.99
331.92 H.I.
323.79
8.13 ✓

331.92
328.00
3.92 M.H. ✓

331.92
319.58
12.34 ✓

322.83 H.I.
315.37
7.46 ✓

2283 2283
11.36 08.19
11.47 ✓ 14.64 ✓

3.17

304.18
9.03
311.21
305.01
6.20 ✓

311.21 11.21 311.21
301.84 298.75
9.37 ✓ 11.21 12.93 ✓

304.18
0.20
304.38
292.99
8.49 ✓

304.38 304.38
292.99 290.10
11.39 ✓ 14.28

292.99
2.98
300.97
290.10
10.87 ✓

300.97
289.00
11.97

290.10
8.22
298.32
289.00
9.32

294.20 = H.I.
288.35
5.85 ✓

94.20
87.30
6.90 ✓

		303.31				
7+0			13.00	290.3	286.25	4.0 ✓
7+50			13.00	290.3	285.20	5.1
7+59 ? = M.H. & Alley			12.9	290.6	285.00	5.6 ✓
8+0			11.4	291.9	286.81	5.1 ✓
+50			9.2	294.1	289.07	5.0 ✓
9+0			6.8	296.5	291.33	5.2 ✓
9+50			4.4	298.9	293.60	5.3 (Not in)
10+0			2.43	B.M. 300.88	295.86	5.0 ✓
T.P.	11.98	312.86	2.43	300.88		
+50			9.2	303.7	298.12	5.6 ✓
11+0			5.9	307.0	300.39	6.6 ✓
11+39 ? M.H. & Alley			5.8	307.1	302.20	4.9 ✓
11+50			5.9	307.0	302.83	4.2
T.P.	9.39	321.04	1.21	311.65		
12+0			8.4	312.6	305.99	6.6
+50			3.16	B.M. 317.88	309.15	8.7
12+64 = R.E. 75 W. of W.L. Miss.			2.5	318.5	310.00	8.5

300.88
1.63
302.51 H.I.

5) 2.27
45

2.26

2.26
2.27

302.51
291.33
11.18 ✓

302.51
293.60
8.91

8.91
.45
8.46

19

302.51
295.86
6.65 ✓

302.51
294.12
4.39 ✓

302.51
300.39
2.12 ✓

302.51
302.20
0.31 ✓

291.33
2.87
294.20 = H.I.
286.25
7.95 ✓

94.20
85.20
9.00

94.20
85.00
9.20

94.20
86.81
7.39 ✓

94.20
89.07
5.13 ✓

Sewer ℄ Alley between Texas & Louisiana. From ℄ Alley N of El Cajon To ℄ Monroe

Sta	+ R	H.I.	- R	elevation stakes	Grade
B.M. Con. Mon cor El Cajon & Texas				322.14	
B.M.	6.94	329.08			
T.P.	7.06	332.80	3.34	325.74	
0+0 = M.H. ℄ alley E & west			8.1	324.7	320.00
0+50			8.0	324.8	320.40
1+0			7.04	B.M. 325.76	320.81
1+50			6.6	326.2	321.21
2+0			5.8	327.0	321.62
2+50 = M.H.			5.8	327.0	322.02
3+0			5.4	327.4	322.42
3+50			4.7	328.1	322.83
4+0			4.5	328.3	323.23
4+50			4.3	328.5	323.63
4+97 = M.H. ℄ Meade			3.8	329.0	324.00
5+0			3.8	329.0	324.07
5+0			3.3	329.5	324.73
6+0			2.9	329.9	325.39
6+50			1.9	330.9	326.05
7+0			0.68	B.M. 332.12	326.72
T.P.	9.41	341.53	0.68	332.12	

POSTED

cut.

325.76 + 6.48 = 332.24 H.I. − 321.62 = 10.62 ✓

32.24 − 22.02 = 10.22 ✓ | 32.24 − 22.42 = 9.82 ✓ | 32.24 − 22.83 = 9.41 ✓

32.24 − 23.23 = 9.01 ✓ | 32.24 − 23.63 = 8.61 ✓ | 32.24 − 24.00 = 8.24 ✓

32.24 − 24.07 = 8.17 | 32.24 − 24.73 = 7.51 ✓ | 32.24 − 25.39 = 6.85 ✓

4.7 ✓

4.4 ✓

5.0 ✓

332.12 + 6.42 = 338.54 H.I. − 326.72 = 11.82 ✓

32.24 − 26.05 = 6.19 ✓

5.0 ✓

5.4 ✓

38.54

5.0 ✓

325.74 + 4.58 = 330.34 H.I. − 321.21 = +9.13 ✓

30.34 − 20.81 = 9.53 ✓ | 30.34 − 20.40 = 9.94 ✓

5.0 ✓

5.3 ✓

5.1 ✓

30.34 − 20.00 = 10.34 ✓

4.9 ✓

5.0 ✓

4.9

4.8 ✓

4.5 ✓

4.9 ✓

5.4 ✓

341.53

7+50	8.3	333.2	327.38
8+0	8.9	333.1	328.04
8+34.7 M.H.	7.5	334.0	328.50
+50	7.5	334.0	328.70
9+0	6.9	335.1	329.37
+50	6.2	335.3	330.03
10+0	5.6	335.9	330.69
+50	4.2	337.3	331.35
11+0	1.6	339.9	332.02
+50	3.8	337.7	332.68
11+75 = M.H. @ Monroe	3.0	338.5	333.00

338.54 = H.I.
327.38
11.16 ✓

21

5.8 ✓
5.1 ✓
5.5 ✓
5.3 ✓
5.7 ✓
5.3 ✓
5.2 ✓
6.0 ✓
7.9 ✓
5.0 ✓
5.5 ✓

38.54	38.54	38.54	38.54
28.04	28.50	28.70	29.37
10.50 ✓	10.04 ✓	9.84 ✓	9.17 ✓
38.54	38.54	38.54	38.54
30.03	30.69	31.35	32.02
8.51 ✓	7.85 ✓	7.19 ✓	6.52
	38.54	38.54	
	32.68	33.00	
	5.86	5.54	

331.35
1.72
343.07 H.I.
932.02
11.05 ✓

43.07	43.07
32.68	33.00
10.39 ✓	10.07 ✓

Sewer & Alley between Louisiana & Miss. from & Alley N of El Cajon to & Monroe

Sta	+ R.	H.I.	− R	elev top stakes	Grade
B.M.				331.65	
B.M.	6.75	338.40			
0+0 = M.H. & Alley N. of El Cajon			4.9	333.5	327.60
0+50			5.04	B.M. 333.36	327.24
	POSTED				
1+0			4.8	333.6	327.98
1+50			3.9	334.5	327.72
2+0			3.9	334.5	327.97
2+50 = M.H.		5	3.7	334.7	328.20
3+0			3.6	334.8	328.99
3+50			3.9	334.5	328.68
4+0			3.57	B.M. 334.83	328.98
T.P.	4.82	339.65	3.57	334.83	
4+50			4.7	335.0	329.17
4+94.7 = M.H. & Meade			4.6	335.1	329.90
5+0			4.6	335.1	329.42
5+50			5.0	334.7	329.65
6+0			4.7	335.0	329.89
6+50			4.5	335.2	330.12
7+0			4.4	335.3	330.36
7+50			4.1	335.6	330.59

cut.

6.5 ✓
6.1 ✓
6.1 ✓
6.8 ✓
6.5 ✓
6.5 ✓
6.4 ✓
5.8 ✓
5.9 ✓
5.8 ✓
5.7 ✓
5.7 ✓
5.0 ✓
5.1 ✓
5.1 ✓
4.9 ✓
5.0 ✓

333.36 B.M.
5.41
338.77 H.I.
327.00
11.77 = M.H. ✓

22

38.77 − 27.24 = 11.53 ✓
38.77 − 27.48 = 11.29 ✓
38.77 − 27.72 = 11.05
38.77 − 27.97 = 10.80
38.77 − 28.21 = 10.56 ✓
38.77 − 28.44 = 10.33 ✓

38.77 − 28.68 = 10.09 ✓
38.77 − 28.93 = 9.84 ✓
38.77 − 29.17 = 9.60

334.83
4.71
339.54 H.I.
29.17
10.37 ✓

339.54 − 28.93 = 10.61

39.54 − 29.40 = 10.14 ✓
39.54 − 29.42 = 10.12 ✓
39.54 − 29.65 = 9.89 ✓
39.54 − 29.89 = 9.65 ✓

39.54 − 30.12 = 9.42 ✓
39.54 − 30.36 = 9.18 ✓
39.54 − 30.59 = 8.95 ✓

49 ✓

339.65

8+0			3.4	336.3	330.83
8+34.7 = M.H.			3.2	336.5	331.00
				B.M.	
+50			2.82	336.83	331.05
T.P.	6.12	342.95	2.82	336.83	
9+0			5.7	337.3	331.31
+50			5.1	337.9	331.55
10+0			4.6	338.4	331.78
+50			4.1	338.9	332.02
				B.M.	
11+0			4.40	338.55	332.25
+50			4.6	338.4	332.49
11+75 M.H. & Monroe			5.0	338.0	332.60

339.54 H.I.

5.5 ✓	39.54	39.54	39.54
	30.83	31.00	31.08
	8.71 ✓	8.54 ✓	8.46 ✓

26

5.5 ✓ 336.83 − 3.80 = 332.63 H.I.

4263 − 31.08 = 11.55

5.8 ✓ 331.31

11.32 ✓

6.0 ✓	4263	4263	4263
	31.55	31.78	32.02
	11.08 ✓	10.85 ✓	10.61

6.4 ✓	42.63	42.63	42.63
	32.25	32.49	32.60
	10.38	10.14	10.03

6.6 ✓ 338.55 + 4.44 = 342.99 H.I.

6.9 ✓ 342.99 − 332.02 = 10.97 ✓

42.99 − 32.25 = 10.74 ✓

42.99 − 32.49 = 10.50 ✓

6.3 ✓

5.9 ✓ 42.99 − 32.60 = 10.39 ✓

5.4 ✓

Sewer beginning ℄ Georgia 12' N of Howard. N to ℄ El Cajon
W on El Cajon To ℄ Alley bet. Georgia & Park Blvd Thence N
To F.F. 20' S. of S. Line Meade

	+ R.	H.I.	− R	elev Top of Plates	Grade
B.M.	11.28	324.07		312.79	
B.M.				B.M.	
0+0 = 12 N. of Howard.			5.07	319.00	314.00
0+13 = end of Sewer D.E					313.85 ✓
0+50			5.5	318.6	313.43
1+0			5.7	318.4	312.86
				POSTED	
+50			5.7	318.4	312.29 ✓
1+74 = M.H. ℄ Alley.			5.6	318.5	312.00
2+0			5.5	318.6	312.20 ✓
+50			5.8	318.3	312.90
3+0			6.0	318.1	313.50 ✓
50			6.7	317.4	314.10
4+0 = M.H. ℄ El Cajon			5.4	318.7	314.70
+50			6.2	317.9	315.70
5+0			5.90	B.M. 318.17	316.70
+50			2.8	321.3	317.70
+65 M.H. ℄ Alley bet Georgia & Park Blvd	7.96	330.31	1.22	322.85	318.00
T.P.			1.22	322.85	
6+0			7.27	B.M. 323.59	318.39 ✓
+50			10.8	320.0	318.94
7+0			9.5	321.3	319.50
7+45 T.P.			5.5	325.3	320.00
	11.98	342.59	0.20	330.61	

cut

24

319.00
4.44
323.44 H.I.
313.43
10.01 ✓

23.44
13.85
9.59 ✓

	323.44	23.44	23.44	23.44	23.44
	12.86	12.29	12.00	12.30	12.90
5.0	10.58 ✓	11.15	11.44	11.14	10.54
	319.00	322.83	322.83	322.83	322.83
	3.83	14.70	14.10	13.50	12.90
5.2 ✓	322.83 H.I.	8.13 ✓ M.H.	8.73 ✓	9.33 ✓	9.93 ✓
5.5 ✓	322.83	322.83	322.83	322.83	322.83
	12.30	12.00	12.29	12.86	12.90
6.1 ✓	10.53 ✓	10.83 ✓	10.54 ✓	9.97	
6.5 ✓					
		318.17			
		4.14			
6.3 ✓		322.31 H.I.	22.31	22.31	22.31
		315.70	16.70	17.70	
5.4 ✓		6.61 ✓	5.61 ✓	4.61 ✓	
4.6		22.31			
		18.00			
3.3 ✓		4.31 ✓			
	323.59				
	6.66				
4.0 ✓	330.25 H.I.				
	318.39				
2.2 ✓	11.86 ✓	30.25	30.25	30.25	
		18.94	19.50	20.00	
1.5 ✓		11.31 ✓	10.75 ✓	10.25 ✓	
3.6 ✓					
4.9 ✓					
5.2 ✓					
1.1 ✓					
1.8 ✓					
5.3 ✓					

		342.59				
8+0			9.98	B.M. 332.61	325.15	✓ 7.5
+50			4.4	338.2	329.83	✓ 8.4
9+0			2.2	340.4	334.52	✓ 5.9
9+05=M.H			2.3	340.3	335.00	✓ 5.3
+50			0.84	B.M. 341.75	335.57	✓ 6.2
T.P.	6.89	348.64	0.84	341.75		
10+0			6.9	342.2	336.20	✓ 6.0
+50			5.8	342.8	336.84	✓ 6.0
11+0			5.6	343.0	337.47	✓ 5.5
+50			5.20	B.M. 343.44	338.11	✓ 5.3
12+0			4.7	343.9	338.75	✓ 5.2
12+20=F.T. 20' S. of Meade			4.5	344.1	339.00	✓ 5.1

330.25 = H.I.
325.15
5.10 ✓

30.25
29.83
00.42

341.75
3.53
345.28 H.I.
334.52
10.76 ✓

45.28 45.28 45.28
35.00 35.57 36.20
10.28 ✓ 9.71 ✓ 9.08 ✓

343.44
3.92
347.36 H.I.
336.84
10.52 ✓

O.K.
47.36
36.20
11.16

.43
.68
C4

47.36 47.36 47.36
37.47 38.11 38.75
9.89 ✓ 9.25 ✓ 8.61 ✓

47.36
39.00
8.36 ✓

Sewer & Alley between El Cajon & Meade from 20' E of E Line of Georgia to & Alley between Mississippi & Louisana

Sta	+ R	H.I.	- R	elev Top Stakes	Grade
B.M.				318.17	
B.M.	4.22	322.39			
T.P.	6.01	323.86	4.54	317.85	
0+0 = D.E			0.64	B.M. 323.22	318.00
+50			2.6	321.3	16.85
1+0			3.8	320.1	15.69
1+30 = M.H. & Alley			4.8	319.1	315.00
+50			6.8	317.1	313.11
2+0			8.69	B.M. 315.17	308.38
+50			10.9	313.0	303.64
T.P	0.75	312.36	12.25	311.61	
3+0			4.6	307.8	298.90
3+20 M.H. & Florida			7.8	305.1	297.00
+50			10.71	B.M. 301.65	296.84
4+0			14.0	298.4	296.58
+50			11.7	300.7	296.32
5+0			10.62	B.M. 301.74	296.05
5+10 M.H. & Alley Cor Florida & Alley			10.5	301.9	296.00
+50			10.1	302.3	297.58
6+0			8.0	304.4	299.55
T.P.	10.72	318.28	4.80	307.56	

POSTED

A

Cut					
	323.22				
	0.94				
	329.16 H.I.	24.16	24.16	24.16	24.16
	318.00	16.85	15.69	15.00	13.1
	6.16 ✓	7.31 ✓	8.47 ✓	9.16 ✓	11.05 ✓
			4.74		
	315.17				
	1.40				
	316.57 H.I.	316.57	16.57	16.57	
5.2 ✓	308.38	303.64			
	8.19 ✓	12.93 ✓			
4.5 ✓	301.74				
	5.94				
	307.68 H.I.	307.68	307.68	307.68	307.68
4.4 ✓	297.00	296.84	296.58	296.32	296.05
	10.68 ✓	10.84 ✓	11.10 ✓	11.36 ✓	11.63
4.1 ✓ X					
		307.68	307.68	307.68	
4.0 ✓ X		296.00			
	301.74				
	5.01				
6.8 ✓ X	306.75 H.I.	306.75	306.75	306.75	
	296.32	296.05	296.00	296.58	
9.4 ✓	10.43	10.70 ✓	10.75 ✓	9.17 ✓	
8.9					
	306.75				
	299.55				
8.1 ✓ X	7.20 ✓				
4.8 ✓					
1.8 ✓					
4.4 ✓					
5.7 ✓					
5.9 ✓					
4.7 ✓					
9.9 ✓					

28

		318.28					
6+50			10.6	307.7	301.53	6.2 ✓	
7+0			10.47	B.M. 307.81	303.50	4.3 ✓	
+50			2.5	310.8	305.48	5.3 ✓	
8+0			4.0	314.3	307.45	6.9 ✓	
8+50			3.16	315.12	309.42	5.7 ✓	
8+90 M.H. & Alleybet Alley & Miss.			2.1	316.2	311.00	5.2 ✓	
9+0			1.10	B.M. 317.18	311.42	5.8 ✓	
T.P.	11.08	328.26	1.10	317.18			
+50			7.0	321.3	313.52	7.8 ✓	
10+0			5.7	322.6	316.63	7.0 ✓	
10+50			3.4	324.9	317.73	7.2	
11+0			1.44	326.82	319.84	7.0	
T.P.	9.23	336.05	1.44	326.82			
+50			6.8	329.3	321.94	7.4	
12+0			5.0	331.1	324.05	7.0 ✓	
12+50			2.72	B.M. 333.33	326.16	7.2 ✓	
12+70=M.H. & Alleybet Miss. & L.B.			2.52	333.53	327.00	6.5	

307.81
5.12
312.93 H.I.
294.55
13.38

312.93 312.93 312.93
301.53 308.50 305.48
11.70 ✓ 4.43 ✓ 7.45

307.81
11.25
319.06 H.I.
307.45
11.61

319.06
305.48
13.58

319.06
309.42
9.64 ✓

319.06 319.06
311.00 311.42
8.06 ✓ 9.64 ✓

317.18 = B.M.
9.75
327.13 H.I.
313.52
13.61 ✓

327.13
315.63
11.50 ✓

327.13
317.73
9.40

326.82
3.68
330.50 H.I.
326.16
4.34 ✓

30.50 30.50 30.50
24.05 21.94 19.84
6.45 ✓ 8.56 10.66 ✓

Sewer Alley between Miss. & Ala. Sts from Alley N of El Cajon to ℄ Madison

Sta	+R	H.I.	−R	elev top stakes	Grade
B.M.	12.13	327.25		315.12	
0+00 = M.H. ℄ Alley N of El Cajon			11.1	316.2	311.60
0+50			8.74	B.M. 318.51	312.59
1+00			6.6	320.7	314.18
1+50			5.6	321.7	316.78
1+80					316.73
2+00					
2+20 = M.H. Drop			3.7	323.6	317.00
2+50			3.3	324.0	318.22
3+00			1.31	B.M. 325.94	318.58
T.P.	10.12	336.06	1.31	325.94	
3+50			8.9	327.1	318.94
4+00			8.9	327.2	319.31
4+50			9.0	327.1	319.67
4+94 = M.H. ℄ Meade no Frank			6.0	330.1	320.00
5+00			6.1	330.0	320.03
5+50			5.6	330.5	320.32
6+00			5.2	330.9	320.61
6+50			5.5	330.6	320.91
7+00			6.4	329.7	321.20

POSTED

cut.

5.9 ✓
6.5 ✓
5.9 ✓
brick
5.6 ✓
5.8 ✓
7.4 ✓
8.2 ✓
7.9 ✓
7.4 ✓
10.1 ✓
10.0 ✓
10.2 ✓
10.3 ✓
9.7 ✓
8.5 ✓

		336.06			
7+50			7.90	B.M. 328.66	321.99
8+0			7.4	328.7	321.79
8+34.8 = M.H. break			6.9	329.2	322.3
8+50			6.7	329.4	322.13
9+0			6.2	329.9	322.57
9+50			5.8	330.3	323.01
10+0			5.0	331.1	323.95
10+50			3.9	332.2	323.89
11+0			2.6	333.5	329.13
11+50			1.47	B.M. 334.59	329.77
T.P.	3.70	338.29	1.47	334.59	
11+74.8 = M.H. Manhole break			4.1	334.12	325.00
12+0			3.7	334.6	325.15
12+50			4.0	334.3	325.44
13+0			4.7	333.6	325.73
13+50			5.8	332.5	326.03
14+0			6.2	332.1	326.32
14+50			5.9	332.4	326.61
15+0			5.6	332.7	326.90
15+14.8 = M.H. break			5.5	332.8	327.00

337.59 = H.I.

7.2	✓	37.59	37.59	37.59	37.59	37.59	37.59
		27.00	26.90	26.61	26.32	26.03	25.78
6.9	✓	10.59 ✓	10.69 ✓	10.98 ✓	11.27 ✓	11.56	11.86
7.2	✓	37.59	37.59	37.59			
		25.44	25.15	25.00			
		12.15	12.44	12.59			
7.3	✓	334.59			336.46	11.87	
		1.87			25.44		
		336.46 = H.I.			11.02	11.16	
7.3	✓	326.03	36.46	36.46	36.46	36.46	36.46
		10.43 ✓	25.73	25.44	25.15	25.00	
7.3	✓	336.46	10.73 ✓	11.02 ✓	11.31 ✓	11.46 ✓	
		325.59					
		10.87					
7.7	✓	36.46	36.46	36.46	36.46	36.46	36.46
		24.77	24.33	23.89	23.45	23.01	22.57
		11.69	12.13	12.57	13.01	13.45	13.89
8.3	✓	328.66		333.70			
		5.04					
9.2	✓	333.70					
		321.49	33.70	33.70	33.70	33.70	
9.8	✓	12.21 ✓	21.79	22.00	22.13	22.57	
			11.91 ✓	11.70	11.57 ✓	11.13	
9.2	✓	333.70					
		323.70	33.70	33.70	33.70	33.70	
9.4	✓	10.00	23.01	23.45	23.89	24.33	24.77
			10.69	10.25	9.81	9.37	8.93
8.9	✓	36.30			328.66		
		25.00	33.70		7.64		
7.9	✓	11.30	25.00		336.30 = H.I.	36.30	
			8.70		323.45	23.89	
6.5	✓	325.66			12.85	12.41 ✓	
		6.30		34.96	36.30	36.30	
5.8	✓	334.96 = H.I.		22.13	24.77	24.33	
		322.00		12.83	11.53 ✓	11.97 ✓	
5.8	✓	12.96 ✓					
					34.96	34.96	
5.8	✓				22.57	23.01	
					12.39 ✓	11.95 ✓	
5.8	✓	34.96	34.96		34.96	34.96	
		23.45	23.89		24.33	24.77	
		11.51 ✓	11.07		10.63	10.19	

338.29

15+50	5.8	332.5	327.20
16+0	4.9	333.4	327.99
+50	4.7	333.6	327.79
17+0	3.5	334.8	328.08
+50	3.80	B.M. 334.49	328.37
18+0	4.1	334.2	328.66
18+50	3.2	335.1	328.96
18+54.8 M.H. ℄ Madison	3.2	335.1	329.00

334.49 B.M.
3.10
337.59 H.I.
328.37
9.22 ✓

5.3 ✓	37.59	37.59	37.59
5.9 ✓	28.66	27.80	28.08
5.8 ✓	8.93 ✓	8.59 ✓	9.51 ✓
6.7 ✓	37.59	37.59	37.59
6.1 ✓	27.49	27.20	27.79
5.5 ✓	10.10 ✓	10.39 ✓	9.80 ✓
6.1			
6.1 ✓			

34 92 29

Sewer Alley between Georgia & Florida from Alley between El Cajon & Meade 70 F.T. 25' S. of Adams

Sta	+ R	H.I.	- R	elev top sta rks	Grade
B.M.				323.22	
B.M.	3.65	326.87			
0+00 M.H. ℄ Alley					315.00
0+50			6.5	320.4	315.81
1+00			5.29	321.58	316.62
T.P.	10.99	332.57	5.29	321.58	
1+50			10.2	321.4	317.93
2+00	POSTED		8.2	324.4	318.24
2+50 = M.H.			5.4	327.2	319.105
3+00			3.1	329.5	319.86
3+50			1.56	331.01	320.67
T.P.	10.50	341.51	1.56	331.01	
4+00			10.0	331.8	321.48
4+50			8.2	333.6	322.29
4+94.3 = M.H. ℄ Meade			8.3	333.5	323.00
5+00			7.5	334.3	323.10
5+50			4.8	337.0	324.105
6+00			5.1	336.7	325.01
6+50			3.6	338.2	325.96
7+00			1.13	340.68	326.92
T.P.	7.00	348.28	1.13	340.68	

cut

321.58
4.30
325.88 H.I.
315.81
10.07 ✓

25.88 25.88
16.62 17.43
9.26 ✓ 8.45 ✓

.81 .81

31

4.1 — 321.58 / 8.89 / 330.38 = H.I. / 318.24 / 12.14 ✓ — 30.38 30.38 30.38 / 19.05 19.86 / 11.33 ✓ 10.52 ✓

4.6 ✓

5.0 ✓

5.0 ✓ — 331.01 / 5.60 / 336.61 = H.I. / 320.67 / 15.94 ✓ — 36.61 36.61 36.61 / 21.48 22.29 23.00 / 15.13 ✓ 14.32 ✓ 13.61 ✓

6.2 ✓

8.2 ✓ — 36.61 / 23.10 / 13.51

9.6 ✓

95 96 95

10.3 ✓ — 331.01 / 10.81 / 341.82 H.I. / 323.10 / 18.72 — 41.82 41.82 41.82 / 24.05 25.01 25.96 / 17.77 ✓ 16.81 ✓ 15.86 ✓

10.3 ✓

11.3 ✓ — 41.82 41.82 41.82 / 26.92 / 14.90

10.5 ✓

11.2 Mtn — 340.68 / 4.65 / 345.33 H.I.

13.0 ✓

~~326.92~~ 340.68 / 4.72 / 345.40 = H.I. / 326.92 / 18.48 ✓ — ~~4068~~ 4540

11.9 ✓

12.2 ✓

13.8 ✓

	348.28			
9+50		6.5	341.8	327.87
8+0		5.8	342.5	328.83
8+39 M.H. break		5.6	342.7	329.50
8+50		5.3	343.0	329.57
9+0		9.7	338.6	329.79
+50		10.2	338.1	330.01
10+0		9.62	B.M. 343.66	330.23
+50		5.0	343.3	330.45
11+0		5.8	342.5	330.67
11+10		5.9	342.4	330.71
11+40		6.0	342.3	330.85
11+74=M.H. & Monroe break		7.8	340.5	331.00
12+0		7.9	340.4	331.31
+50		8.77	339.51	331.90
13+0		9.7	338.6	332.49
+50		8.7	339.6	333.07
14+0		7.6	340.7	333.66
14+50		6.3	342.0	334.25
15+0		7.30	B.M 340.98	334.83
T.P. 9.20	350.28	7.30	340.98	
15+14 M.H. break		9.7	340.6	335.00

340.98 = B.M.
5.02
346.00
333.07
12.93

345.33 M.H.
329.50
15.83

343.66
1.25
344.91
330.01
14.90

345.40 = M.H.
327.87
17.53

345.40 M.H.
7.42
337.98 T.P.
3.22
347.20 = M.H.

339.51
5.46
344.97 = M.H.
331.00
13.97

339.51
3.60
343.11 M.H.
332.49
10.62

34366
3.42
347.08
330.23
16.85

13.9				
13.7				
13.2				
13.4				
8.8				
8.1				
13.4				
12.9				
11.7				
11.7				
11.4				
9.6				
9.1				
7.6				
6.1				
6.5				
7.0				
7.8				
6.2				
5.6				

46.00 / 33.66 / 12.34 | 46.00 / 34.25 / 11.75 | 46.00 / 34.89 / 11.11

46.00 / 35.00 / 11.00 | 46.00 / 35.21 / 10.79 | 46.00 | 46.00

45.40 / 28.83 / 16.57 | 45.40 / 29.50 / 15.90 | 45.40 / 29.57 / 15.83

45.40 / 29.79 / 15.61

41.20 / 29.79 / 11.41 | 41.20 / 30.01 / 11.19

43.11 / 31.90 / 11.21 | 43.11 / 31.31 / 11.80

47.08 / 30.45 / 16.63 | 47.08 / 30.71 / 16.37 | 47.08 / 30.85 / 16.23

32

			350.28			
15+50			8.9	341.4	335.21	
16+0			8.0	342.3	335.50	
+50			7.6	342.7	335.80	
17+0			6.71	B.M. 343.57	336.09	
+50			5.9	344.9	336.39	
18+0			5.1	345.12	336.68	
~~+50~~			4.8	345.5	336.98	
18+54 M.H. E. Madison brook			4.8	345.5	337.00	
19+0			3.8	346.5	337.77	
19+60			3.7	346.6	338.79	
20+0			2.9	347.4	339.44	
+50			1.87	B.M. 348.41	340.27	
T.P.	7.10	355.61	1.87	348.41		
20+79 M.H.			7.6	348.0	340.67	
21+00			6.2	349.4	341.10	
+50			6.1	349.5	341.94	
22+0			5.6	350.0	342.77	
+50			5.3	350.3	343.61	
23+0			6.0	349.6	344.44	
23+33 = F.T. 25" y Adams			6.5	349.1	345.00	

346.0 = 41.

6.2 ✓ 46.00 / 35.50 / 10.50 ✓ — 46.00 / 35.80 / 10.20 — 46.00 / 36.09

6.8 ✓

6.9 ✓ 343.57 / 5.27 / 348.84 H.I. / 335.80 / 13.04 ✓ — 48.84 / 36.09 / 12.75 ✓ — 48.84 / 36.39 / 12.45 ✓ — 48.84 / 36.68 / 12.16 ✓

7.5 ✓

8.0 ✓ 48.84 / 37.00 / 11.84 — 48.84 / 38.77 / 10.07 ✓ — 48.84 / 39.44 / 9.40 ✓ — 48.84 / 40.27 / 8.57

8.5 ✓

~~8.5~~ 348.41 / 5.65 / 354.06 H.I. / 340.27 / 13.79 ✓ — 54.06 / 40.67 / 13.39 ✓ — 54.06 / 41.10 / 12.96 ✓ — 54.06 / 41.94 / 12.12 ✓

9.5 ✓

8.7 ✓

7.8 ✓ 54.06 / 42.77 / 11.29 ✓ — 54.06 / 43.61 / 10.45 ✓ — 54.06 / 44.44 / 9.62 ✓ — 54.06 / 45.00 / 9.06 ✓

8.0 ✓ 343.57 / 5.46 / 349.03 H.I. / 337.00 / 12.03

8.1 ✓ 343.57 / 5.50 / 349.07 H.I. / 336.68 / 12.39 ✓ — 49.07 / 37.00 / 12.07 ✓

7.3 ✓ 49.07 / 37.77 / 11.30 ✓

8.3 ✓

7.6 ✓

7.2 ✓

6.7 ✓

5.2 ✓

4.1 ✓

Sewer Florida st from ℄ Alley between El Cajon and Meade to M.H. ℄ Madison

Sta	+ R	H.I.	− R	elev for stakes 301.79	Grade
B.M.					
B.M	10.78	312.57			
0+0 = M.H. ℄ Alley					297.00
0+50			7.7	304.8	297.60
1+0			8.5	309.0	298.21
1+50			8.7	303.8	298.81
2+0			8.8	303.7	299.42
2+50 = M.H.			8.9	303.6	300.02
3+0			7.7	304.8	300.63
3+50			6.55	305.97	301.78
4+0			5.4	307.1	301.89
4+50			4.2	308.3	302.99
4+95 = M.H. ℄ Meade			3.3	309.2	303.00
5+0			3.3	309.2	303.10
5+50			2.0	310.5	304.13
6+0			1.2	311.3	305.16
6+50			0.42	B.M. 312.10	306.19
T.P.	11.42	323.52	0.42	312.10	
7+0			10.5	313.00	307.23

POSTED

N

Cut
7.1 ✓
5.8 ✓
5.0 ✓
9.3 ✓
3.6 ✓
4.2 ✓
4.7 ✓
5.3 ✓
5.9 ✓
6.2 ✓
6.1
6.4 ✓
6.1 ✓
5.9 ✓
5.8 ✓

305.97 B.M.
2.63
308.60 = H.I.
297.60
11.00 ✓

308.60 298.21 = 10.39 ✓
308.60 298.81 = 9.79 ✓
308.60 299.42 = 9.18 ✓
308.60 300.02 = 8.56 ✓

308.60 300.63 = 7.97 ✓
308.60 301.23 = 7.37 ✓
308.60 301.84 = 6.76 ✓
308.60 302.44 = 6.16 ✓

312.10 B.M.
4.30
316.40 H.I.

316.40 302.44 = 13.96 ✓
316.40 303.80 = 13.40 ✓
316.40 303.10 = 13.30
316.40 304.13 = 12.27 ✓
316.40 305.16 = 11.24 ✓

316.40 306.19 = 10.21 ✓
316.40 307.23 = 9.17 ✓
316.40
316.40

		323.52				
7+50			9.6	313.9	308.26	5.6 ✓
8+0			8.9	314.6	309.29	5.3 ✓
8+35 M.H.			7.8	315.7	310.00	5.7 ✓
8+50			7.2	316.3	310.32	6.0 ✓
9+0			5.7	317.8	311.35	6.5 ✓
+50			4.2	319.3	312.38	6.9 ✓
10+0			2.8	320.7	313.41	7.3 ✓
+50			1.5	322.0	314.49	7.6 ✓
11+0			1.5	322.0	315.47	6.5 ✓
+50			1.1	322.4	316.50	5.9 ✓
11+73 = M.H. & Monroe			0.9	322.6	317.00	5.6 ✓
12+0			0.74	B.M. 322.78	317.15	5.6 ✓
T.P.	9.90	332.68	0.74	322.78		
12+50			10.1	322.6	317.94	5.2 ✓
13+0			9.9	322.8	317.73	5.1 ✓
+50			9.8	322.9	318.02	4.9 ✓
14+0			9.7	323.0	318.32	4.7 ✓
+50			8.9	323.8	318.61	5.2 ✓
15+0			8.1	324.6	318.90	5.7 ✓
15+13 = M.H.			7.8	324.9	319.00	5.9 ✓

Cut

316.40 = M.H.
308.26
8.14 ✓

316.40 316.40 316.40 316.40
309.29 310.00 310.32 311.35
7.11 ✓ 6.40 ✓ 6.08 ✓ 5.05

35

322.78
4.65
327.43 = M.H.
312

322.78
1.97
324.75 M.H.
311.35
13.40

24.75
12.38
12.37 ✓

24.75 24.75 24.75 24.75 24.75
13.41 14.47 15.47 16.50 17.25
11.34 ✓ 10.34 ✓ 9.28 ✓ 8.25

322.78
3.19
325.97 = M.H.
315.47
10.50

25.97 25.97 25.97 25.97
16.50 17.00 17.15 17.32
9.47 ✓ 8.97 ✓ 8.82 ✓ 8.65 ✓

25.97 25.97 25.97 25.97
17.44 17.73 18.02 18.32
8.53 ✓ 8.24 ✓ 7.95 ✓

25.97 25.97 25.97 25.97
18.61 18.90 19.00
7.36 ✓ 7.07 ✓ 6.97 ✓

	332.68				
15+50		7.38	B.M. 325.30	319.65	5.7 ✓
16+0		6.9	325.8	320.58	5.3 ✓
+50		6.1	326.6	321.40	5.2 ✓
17+0		5.2	327.5	322.28	5.2 ✓
+50		3.9	328.8	323.15	5.7 ✓
18+0		2.46	B.M 330.22	324.03	6.2 ✓
18+55.5 M.H. @ Madison		1.2	331.5	325.00	6.5 ✓

32.15
18.90
13.25

325.30 = B.M.
6.55
332.15 = H.I.
319.65
12.50 ✓

88
87
88

36

32.15 32.15 32.15
20.53 21.40 22.28
11.62 ✓ 10.75 ✓ 9.87 ✓

32.15 32.15 32.15
23.15 24.03 25.00
9.00 ✓ 8.12 ✓ 7.15 ✓

BM 250.87 Hub N.E. Cor Hickory & Hortensia Sts.
+ 3.89
254.76 H.I.
- 4.22
BM 250.54 Mon west Line Witherby & Cen Chestnut Sts,

Crossection of Chestnut St (50 wide), Witherby West 10 courses 7½ quarters

	+	H.I.	−	
	1.38	251.92		250.54
00 = West line of Witherby Street.				
00				
M.L.			+0.2	252.1
cl			0.6	
1/4			1.0	
c			1.1	250.8
1/4			1.3	
cl			1.1	
D.L. +25			1.1	250.8
D.L.			4.1	247.8
cl			3.6	
1/4			3.4	
c			3.2	248.7
1/4			3.0	
cl			2.6	
M.L. +50			2.1	249.8
M.L.			3.3	248.6
cl			4.2	
1/4			5.1	

3 11 12 Dornan Shaw Devine

	+	H.I. 251.92	−	
c			5.5	246.4
1/4			6.2	
cl			6.5	
D.L.			7.0	244.9
At +75 Slope 25' North of North line.			8.5	243.4
" " " 13' " " " " +75			10.5	241.0
D.L.			17.2	234.7
cl			19.1	
1/4			19.8	
c			16.5	235.4
1/4			11.9	
cl			7.6	
M.L.			5.6	246.3
At 1+00 Slope 15' North of north line 1+00			7.6	
M.L.			11.9	240.1
#	0.29	239.57	12.63	239.29
cl			3.0	
1/4			6.4	
c			19.8	229.5
1/4			15.5	

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+	H.I. 229.07	−	Chestnut St (50' wide)
cl		10.6	
V.L.		5.8	233.8
at 1+00 slope 15' South of South line		1.0	238.6
at 1+25 slope 20' South of South line 1+25		1.9	
V.L.		7.7	231.9
cl		12.6	
1/4		18.9	
+2		19.8	
c		17.1	222.5
1/4		12.6	
cl.		10.7	
N.L.		8.2	231.4
at 1+25 slope 15' North of North line		4.4	
#	0.11	226.98	12.70 226.87
at 1+50 slope 20' North of North line 1+50		0.3	
N.L.		5.6	221.4
cl		9.6	
1/4		11.4	
c		9.4	217.6
1/4		5.7	

+	H.I. 226.98	−	
cl		2.5	
V.L.		+1.0	228.0
at 1+50 slope 25' south of south line		+7.2	234.2
at 1+75 " 20' " " " " 1+75		+0.4	227.4
V.L.		3.1	223.9
cl		5.9	221.1
1/4		8.1	218.9
c		11.4	215.6
1/4		13.6	213.4
cl		14.5	212.5
N.L.		12.9	214.1
at 1+75 slope 20' north of north line		7.7	219.3
#	0.93	216.04	11.87 215.11
at 2+00 slope 45' north of south line 2+00		3.6	
N.L.		8.1	207.9
cl		8.1	
1/4		6.0	
c		3.6	212.4
1/4		1.3	
cl		0.1	

	+	H.I. 216.04	−	Chestnut St (62')
N.L.			+0.8	216.8
at 2+00 slope 25' South of North line			+2.3	213.3
" 2+25 " 40' " " " "			11.3	
" " " 25' " " " " 2+25			8.9	
N.L.			13.4	202.6
ch			13.6	
1/4			13.0	
C			11.7	204.3
1/4			10.4	
ch			9.5	
N.L.			8.4	207.6
at 2+25 slope 40' North of North line			9.9	
" 2+50 " 25' " " " " 2+50			+1.6	217.6
N.L.			2.4	213.6
ch			4.0	
1/4			5.5	
C			7.2	208.8
1/4			9.1	
ch			10.7	
N.L.			12.5	203.5

	+	H.I. 216.04	−	
at 2+50 slope 40' south of South line,			17.8	
" 2+75 " 25' " " " " 2+75			3.1	
N.L.			1.6	214.4
ch			0.5	
#	12.76	228.78	0.02	216.02
1/4			12.1	
C			11.0	217.8
1/4			10.0	
ch			9.1	
N.L.			7.3	221.6
at 2+75 slope 25' North of North line			3.3	
#	10.71	239.41	0.08	228.70
3+00 = East line of Hastings St (50' wide) 3+00				
N.L.			8.9	230.5
ch			10.2	229.2
1/4			11.4	228.0
C			11.8	227.6
1/4			12.4	227.0
ch			13.1	226.3
N.L.			14.0	225.4

	+	H.I. 239.41	−	
				Chestnut St (50') wide 10' curbs 7½ quarters
at 3+00 slope 25' south of South line			15.9	
East curb of Hortensia Street (10').				
M.L.			9.4	230.0
cb			9.0	230.4
¼			9.6	229.8
c			8.0	231.0
¼			7.5	231.9
cb			6.3	233.1
M.L.			5.0	234.4
East ½ of Hortensia St. (7½)				
M.L.			3.0	236.4
cb			4.2	235.2
¼			4.6	234.6
c			5.7	233.7
¼			6.4	233.0
cb			6.6	
M.L.			7.4	232.0
Center of Hortensia St (50' street).				
M.L.			6.4	233.0
cb			5.4	234.0

	+	H.I. 239.41	−	
¼			4.5	234.9
c			3.8	235.6
¼			3.1	236.3
cb			2.0	237.4
M.L.			1.2	238.2
West ½ of Hortensia St (7½ quarters).				
M.L.			+1.0	240.4
cb			+0.4	239.8
¼			0.7	238.7
c			1.7	237.7
¼			3.1	236.3
cb			4.3	235.1
M.L.			5.4	234.0
West curb of Hortensia St. (50' street).				
M.L.			4.2	235.2
cb			2.6	236.6
¼			1.4	238.0
c			0.0	239.4
#	11.14	249.75	0.80	238.61
¼			9.7	240.1

	+	H.I.	−	Chestnut St (30' wide)
		249.8		
c l			8.9	N 0.9
N.L.			8.3	241.5
00 = West line of Hortensia St.				
00 N.L.			5.8	244.0
c l			7.2	242.6
1/4			8.1	241.7
c			9.0	240.8
1/4			10.0	239.8
c l			11.6	238.2
N.L. +25			12.9	236.9
N.L.			9.0	240.8
c l			7.9	
1/4			7.2	
c			6.2	243.6
1/4			5.5	N 4 4.3
c l			4.4	N 4 5.4
N.L. +50			3.1	246.7
N.L.			1.0	248.8
c l			2.0	N 47.8
1/4			1.7	N 48.1

	+	H.I.	−	
		249.8		
c			3.5	246.3
1/4			4.1	N 45.7
c l			5.0	N 44.8
N.L. +75			6.0	243.8
N.L.			2.6	247.2
c l			1.9	
1/4			1.4	
c			0.9	248.9
1/4			0.4	N 49.4
#	9.48	258.17 258.2	0.06	249.69
c l			8.0	N 50.2
N.L. 1+00			7.3	250.9
N.L.			4.7	253.5
c l			5.7	N 52.5
1/4			6.4	N 51.8
c			7.0	251.2
1/4			7.3	N 50.9
c l			7.6	N 50.6
N.L. 1+25			8.0	250.2
N.L.			6.2	252.0

	+	H.I. 258.17 258.2	−	Chestnut St 50' wide
cl			5.5	
1/4			5.3	
c			5.2	253.0
1/4			4.8	253.4
cl			4.2	254.0
M.L. 1+50			3.3	254.9
M.L.			1.6	256.5
cl			3.0	255.2
1/4			3.5	254.7
c			4.0	254.2
1/4			4.1	
cl			4.5	
M.L. 1+75			4.9	253.3
M.L.			4.2	254.0
cl			4.0	
1/4			3.6	
c			3.5	254.7
1/4			2.9	255.3
cl			2.2	256.0
M.L.			1.5	256.7

	+	H.I. 258.17 258.2	−	
2+00 M.L.			1.8	256.4
cl			2.5	255.7
1/4			2.7	255.5
c			3.4	254.8
1/4			3.4	
cl			3.6	
M.L. 2+25			4.2	254.0
M.L.			3.9	254.3
cl			3.6	
1/4			3.4	
c			3.2	255.0
1/4			2.7	255.5
cl			2.4	255.8
M.L. 2+50			1.8	256.4
M.L.			2.1	256.1
cl			2.2	256.0
1/4			3.0	255.2
c			3.2	255.0
1/4			3.5	
cl			3.6	

+	H.I.	−	Chestnut St (50' wide)
	258.17		
	258.2		
N.L.			
247.5			
		3.9	254.3
N.L.		3.9	254.3
cl		3.7	254.5
1/4		3.5	254.7
c		3.4	254.8
1/4		3.0	255.2
cl		2.8	255.4
N.L.		2.5	255.7
3+00 = East line of Trias St (50' wide)			
3+00			
N.L.		2.7	255.5
cl		2.8	255.4
1/4		3.0	255.2
c		3.5	254.7
1/4		3.7	
cl		3.7	
N.L.		4.0	254.2
#	3.06 257.31	3.92	254.25 BM Mon Center Chestnut & Trios.
East end of Trias St (10' wide)			
N.L.		3.0	254.3
cl		2.9	

+	H.I.	−	
	257.31		
1/4		2.9	
c		2.7	254.6
1/4		2.4	
cl		2.2	
N.L.		2.0	255.3
East 1/4 of Trias St (7½' wide)			
N.L.		2.0	255.3
cl		2.3	
1/4		2.5	
c		2.6	254.7
1/4		2.8	
cl		2.9	
N.L.		3.0	254.3
Center of Trias St.			
N.L.		3.1	254.2
cl		3.0	illegible
1/4		2.8	illegible
c		2.6	254.7
1/4		2.3	illegible
cl		2.2	illegible

	+	H.I. 257.31	−	Chestnut St (50' wide)
N.L.			2.2	255.1
West ½ Friar St (7½ quarters).				
N.L.			2.5	254.8
cb			2.5	255.8
¼			2.2	255.1
c			2.6	254.7
¼			2.8	255.6
cb			2.9	255.5
N.L.			3.1	254.2
West side Friar St.				
N.L.			3.3	254.0
cb			3.0	255.3
¼			2.9	255.5
c			2.4	254.9
¼			2.7	255.6
cb			2.7	255.6
N.L.			2.0	255.3
00 = West line of Friar St.				
00				
N.L.			2.1	255.2
cb			2.3	255.0

	+	H.I. 257.31	−	
¼			2.8	255.6
c			2.7	254.6
¼			2.9	255.5
cb			3.2	255.1
N.L. +25			3.2	254.1
N.L.			3.9	253.4
cb			3.3	255.0
¼			3.0	255.3
c			3.0	254.3
¼			2.7	255.6
cb			2.6	255.7
N.L. +50			2.3	255.0
N.L.			2.5	254.8
cb			2.8	255.5
¼			2.5	255.8
c			3.8	253.5
¼			3.8	255.3
cb.			3.8	255.3
N.L. +75			4.2	253.1
N.L.			4.7	252.6
cb			4.3	253.0

+	HI 25?.31	− Chestnut St (cont'd)
1/4	4.3	252.0
c	4.3	253.0
1/4	3.4	254.9
cl	3.0	254.3
M.L. 1+00	2.9	254.4
M.L.	2.9	254.4
cl	3.1	254.2
1/4	3.8	254.5
c	4.3	253.0
1/4	4.3	252.0
cl	4.2	252.1
D.L. 1+25	4.3	253.0
M.L.	4.0	253.3
cl	3.7	252.6
1/4	3.6	252.7
c	3.9	253.4
1/4	3.0	254.2
cl	3.1	254.2
M.L. 1+50	2.8	254.5
M.L.	2.9	254.4

+	HI 25?.31	−
cl	3.1	254.2
1/4	2.9	254.5
c	3.6	253.7
1/4	3.5	254.8
cl	3.8	254.6
M.L. 1+75	3.8	253.6
D.L.	4.2	253.1
cl	4.0	252.3
1/4	4.0	252.3
c	4.4	252.9
1/4	3.7	254.6
cl	3.5	254.8
M.L. 2+00	3.2	254.1
M.L.	3.9	253.4
cl	4.2	254.1
1/4	4.3	254.0
c	5.1	252.2
1/4	4.9	254.2
cl	4.8	254.3
D.L.	4.7	252.6

	+	H.I. 257.81	−	Chestnut St (50')	
# 2+25	1.86	254.76	4.41	252.90	
M.L.			3.8	251.0	
cb			3.5	N 1.3	
1/4			3.6	N 1.2	
c			3.5	251.3	
1/4			2.7	N 2.1	
cb			2.5	N 2.3	
M.L. 2+50			2.3	252.5	
M.L.			3.1	N 1.7	
cb			3.2	N 1.6	
1/4			3.2	N 1.6	
c			4.1	250.6	
1/4			4.4	N 0.1	
cb			4.3	N 0.5	
M.L. 2+75			4.5	250.3	
M.L.			4.7	250.1	
cb			4.8	N 0.0	
1/4			4.9	N 0.9	
c			4.8	250.0	
1/4			4.0	N 0.8	

	+	H.I. 254.76	−		
cb			3.8	N 1.0	
M.L.			3.6	251.2	
3+00 = East line of Ampudia St (50' street), 3+00					
M.L.			4.1	250.6	
cb			4.5	250.3	
1/4			4.7	250.1	
c			5.4	249.4	
1/4			5.6	249.2	
cb			5.8	249.0	
M.L.			5.8	249.0	
East curb of Ampudia St (10' curb),					
M.L.			5.9	248.9	
cb			6.2	248.6	
1/4			6.0	248.8	
c			5.5	248.3	
1/4			5.0	249.8	
cb			4.6	250.0	
M.L.			4.3	250.5	
East 1/4 of Ampudia St. (7½' quarter)					
M.L.			4.6	250.8	

+	H.I. 25 4.76	−	Chestnut St (50)'	
cl		4.7	N50.1	
1/4		5.2	N49.6	
c		5.9	248.9	
1/4		6.1	N48.7	
cl		6.4	N48.4	
M.L.		6.0	248.8	
Center of Ampudia St.				
M.L.		6.05	248.3	
cl		6.7	247.7	
1/4		6.05	248.3	
c		6.1	248.7	
1/4		5.4	249.4	
cl		5.3	249.5	
M.L.		5.2	249.6	
West 1/4 of Ampudia St.				
M.L.		5.6	249.2	
cl		6.0	N48.8	
1/4		5.9	N48.9	
c		6.1	248.7	
1/4		6.6	N48.2	

+	H.I. 25 4.76	−		
cl		7.2	N47.6	
M.L.		7.3	247.5	
West curb of Ampudia St.				
M.L.		7.9	246.9	
cl		7.4	N47.4	
1/4		7.1	N47.7	
c		6.4	248.4	
1/4		6.4	N48.4	
cl		6.2	N48.6	
M.L.		5.6	249.2	
00= West line of Ampudia St.				
M.L.		6.1	248.7	
cl		6.3	248.5	
1/4		7.0	247.8	
c		7.3	248.3	
1/4		7.5	247.3	
cl		7.8	247.0	
M.L. +25		8.6	246.2	
M.L.		10.4	244.4	
cl		9.4	N45.4	

+	H.I. 254.76	−	Chestnut St (60)
1/4		9.2	N 46.6
c		8.7	246.1
1/4		9.2	N 46.6
cb		7.7	N 47.1
M.L. +50		7.3	247.5
M.L.		9.4	246.4
cb		8.8	N 46.0
1/4		9.7	N 45.1
c		10.1	244.7
1/4		11.0	N 43.8
cb		11.5	N 43.3
M.L. +75		12.1	242.7
M.L.		14.3	240.5
cb		13.4	N 41.6
1/4		12.6	N 42.4
c		11.3	243.5
1/4		11.3	N 43.3
cb		10.1	N 44.7
M.L.		9.5	245.3
#	8.33 : 245.08	13.01	241.75

+	H.I. 248.08	−
1400 M.L.		1.0 244.1
cb		1.6 N 43.5
1/4		3.0 N 42.1
c		3.3 241.8
1/4		4.3 N 40.8
cb		5.0 N 40.1
M.L. 1425		5.8 239.3
M.L.		6.6 238.5
cb		5.5 N 39.6
1/4		5.0 N 40.1
c		3.7 241.4
1/4		4.0 N 41.1
cb		2.7 N 42.4
M.L. 1450		1.9 243.2
M.L.		2.3 242.8
cb		3.2 N 41.9
1/4		4.3 N 40.8
c		4.8 240.3
1/4		5.2 N 39.9
cb		6.2 N 38.9

+	H.I. 24°08	−	Chestnut St (50')
St. 1+75		7.0	238.1
St.		7.0	238.1
cl		5.9	239.7
1/4		5.2	239.9
c		4.8	240.3
1/4		4.0	241.1
cl		3.1	241.0
m.l. 2400		2.6	242.5
m.l.		2.3	242.8
cl		2.8	241.3
1/4		3.6	241.9
c		4.4	240.7
1/4		5.0	241.1
cl		5.4	239.7
St. 2+25		6.6	238.5
St.		6.0	239.1
cl		4.9	241.0
1/4		4.6	241.9
c		3.8	241.3
1/4		3.0	241.1

+	H.I. 24°08	−	
cl		2.2	241.9
m.l. 2400		1.9	243.2
m.l.		2.1	243.0
cl		2.4	241.7
1/4		2.9	241.2
c		3.8	241.3
1/4		4.6	241.9
cl		5.0	241.1
St. 2+75		5.8	239.3
St.		6.6	238.5
cl		5.7	239.6
1/4		5.3	239.8
c		4.7	240.4
1/4		4.0	241.1
cl		3.3	241.8
m.l.		3.0	242.1
300 = East line of Cristo St (50' wide).			
m.l.		4.6	240.5
cl		5.1	241.0
1/4		5.9	239.2

	+	H.I. 245.08	−	
Chestnut St (cont)				
c			6.8	238.3
1/4			7.5	237.6
cl			7.6	237.5
M.L.			8.4	236.7
East curb of Arista St (10' curb)				
M.L.			8.9	236.2
cl			8.2	
1/4			8.0	
c			7.7	237.4
1/4			7.0	
cl			6.2	
M.L.			5.5	239.6
East 1/4 of Arista St (7 1/2 quarters)				
M.L.			6.8	238.3
cl			7.1	
1/4			7.7	
c			8.2	236.9
1/4			8.4	
cl			8.9	
M.L.			9.3	235.8

	+	H.I. 245.08	−	
Center of Arista St.				
M.L.			10.5	234.6
cl			9.8	
1/4			9.3	
c			9.0	236.0
1/4			8.4	
cl			8.1	
M.L.			7.7	237.4
West 1/4 of Arista St				
M.L.			8.1	232.0
cl			8.9	
1/4			9.2	
c			9.5	235.6
1/4			10.2	
cl			11.0	
M.L.			11.6	233.5
West curb of Arista St.				
M.L.			12.6	232.5
cl			11.8	
1/4			11.1	

Chestnut St (50')

	+	H.I. 245.08	−	
c				
			10.2	234.9
1/4			9.9	
cl			9.4	
N.J.			9.7	236.4
00 = West line of Arista St.				
00 N.J.			9.9	230.2
cl			10.6	
1/4			11.5	
c			12.3	232.8
1/4			12.6	
cl			13.1	
N.J.			14.2	230.9
# +25	0.45	232.75	12.78	232.30
N.J.			4.3	228.5
cl			3.5	
1/4			2.9	
c			2.5	230.3
1/4			1.8	
cl			1.0	
N.J.			0.7	232.1

	+	H.I. 232.75	−	
+50 N.J.			4.5	228.3
cl			3.1	
1/4			4.2	
c			4.6	228.2
1/4			5.1	
cl			5.5	
N.J. +75			6.3	226.5
N.J.			9.4	224.4
cl			7.9	
1/4			7.3	
c			6.7	226.1
1/4			6.7	
cl			6.9	
N.J. 1400			6.6	226.2
N.J.			6.8	226
cl			7.6	
1/4			8.1	
c			8.5	224.3
1/4			9.1	
cl			8.9	

	+	HI	−	Chestnut VH (50')
		232.75		
R.T. 1+25			10.0	222.8
R.T.			10.2	222.6
cl			10.0	
1/4			9.7	
c			9.5	223.3
1/4			9.2	
cl			8.7	
m.T. 1+50			8.2	224.6
m.T.			9.3	222.5
cl			9.3	
1/4			9.5	
c			9.7	223.1
1/4			10.0	
cl			10.4	
R.T. 1+75			10.9	221.9
R.T.			10.3	222.5
cl			10.1	
1/4			10.0	
c			9.6	223.2
1/4			9.7	
cl			9.4	

	+	H.I. 232.75	−		
m.T. 2+00			9.7	223.1	
m.T.			11.1	221.7	
cl			10.7		
1/4			10.6		
c			10.3	222.5	
1/4			10.2		
cl			10.0		
R.T. 2+25			9.6	223.2	
R.T.			10.2	222.6	
cl			11.3		
1/4			11.8		
c			12.0	220.8	
1/4			12.5		
cl			12.9		
m.T.			13.2	219.6	
H 2+50	7.28	227.48	12.54	220.21	Rock T.P.
m.T.			10.5	217.0	
cl			9.6		
1/4			8.8		
c			7.9	219.6	

	+	HI.	−	
		227.49		Chestnut St (50')
1/4			6.9	
cb			5.3	
N.L. 2+75			3.2	224.3
R.L.			2.0	225.5
cb			3.7	
1/4			9.8	
c			9.3	218.2
1/4			9.4	
cb			10.4	
N.L.			12.0	215.5
3+00 = East line of Conde St (60' wide)				
N.L.			14.8	212.7
cb			13.0	
1/4			11.8	
c			8.6	218.9
1/4			6.2	
cb			5.6	
N.L.			2.5	225.0
East curb of Conde St (10' curb).				
N.L.			5.4	222.1

	+	HI.	−	
		228.49		
cb			7.5	
1/4			9.5	
c			11.6	216.9
1/4			14.3	
cb			14.5	
N.L.			17.8	209.7
East 1/4 of Conde St (7 1/2' quarters)				
#		3.67	12.99	214.50
N.L.			8.6	209.6
cb			6.2	
1/4			4.7	
c			4.2	214.0
1/4			2.9	
cb			0.8	
N.L.			+ 2.6	220.8
Center of Conde St				
N.L.			2.2	216.0
cb			4.1	
1/4			4.6	
c			5.20	212.9

55

Mon Cen Conde & Chestnut.

	+	H.I. 218.17	−	
			Chestnut St (00')	
½			7.2	
cl			8.4	
M.L.			10.2	208.0
		West ¼ of Conde St.		
M.L.			11.0	207.2
cl			10.5	
¼			9.5	
c			7.6	210.6
¼			6.6	
cl			4.3	
M.L.			3.5	214.7
		West curb of Conde St.		
M.L.			4.0	214.2
cl			6.6	
¼			8.6	
c			10.0	208.2
¼			10.7	
cl			11.6	
M.L.			11.6	206.6
00 = West line of Conde St.				

	+	H.I. 218.17	−	
00 M.L.			12.3	205.9
cl			12.0	
¼			12.0	
c			11.7	206.3
¼			11.0	
cl			9.9	
M.L.			8.2	210.0
#	3.09	209.71	12.55	205.62
425 M.L.			4.2	205.5
cl			4.0	
¼			3.8	
c			4.1	204.6
¼			4.2	
cl			4.7	
M.L.			5.0	203.7
155 M.L.			5.8	202.9
cl			5.8	
¼			5.8	
c			5.4	203.3
¼			5.2	
cl			5.1	

	+	H.I. 208.71	−	Chestnut St (60')
N.L. 1+75			5.1	203.6
N.L.			6.9	201.8
cl			7.0	
1/4			7.0	
c			6.9	201.8
1/4			6.9	
cl			7.1	
M.L. 1+00			7.2	201.8
M.L.			7.8	200.9
cl			7.9	
1/4			7.9	
c			7.7	201.0
1/4			7.6	
cl			7.8	
N.L. 1+25			7.7	201.0
N.L.			8.1	200.6
cl			8.2	
1/4			8.2	
c			8.2	200.5
1/4			8.2	

	+	H.I. 208.71	−	
cl			8.3	
M.L. 1+50			8.3	200.4
M.L.			7.6	201.1
cl			7.6	
1/4			7.6	
c			7.6	201.1
1/4			7.6	
cl			7.7	
N.L. 1+75			7.6	201.1
N.L.			6.4	202.3
cl			6.1	
1/4			6.1	
c			6.0	202.7
1/4			6.1	
cl			6.0	
M.L. 2+00			6.1	202.6
M.L.			4.8	203.9
cl			5.0	
1/4			5.0	
c			5.4	203.3

55

	+	H.I. 208.71	−	
				Chestnut St (60')
1/4			5.4	
cb			5.5	
N.L. 2+25			5.9	202.8
N.L.			5.0	203.7
cb			4.8	
c			4.5	204.2
1/4			4.2	
cb			4.1	
N.L. 2+50			4.2	204.5
N.L.			4.0	204.7
cb			3.6	
1/4			3.7	
c			3.7	205.0
1/4			3.9	
cb			3.8	
N.L. 2+75			4.4	204.3
N.L.			3.1	205.6
cb			3.0	
1/4			3.0	
c			3.0	205.7

	+	H.I. 208.71	−	
1/4			2.9	
cb			2.9	
N.L.			2.4	206.3
#	6.80	215.48	0.03	208.68
3+00 = 3+00	East line of Harney St (50' wide),			
N.L.			6.7	208.8
cb			6.7	
1/4			7.0	
c			7.1	208.4
1/4			7.2	
cb			7.0	
N.L.			7.4	208.1
	East curb of Harney St (10' curb)			
N.L.			6.2	209.3
cb			6.2	
1/4			6.1	
c			5.8	209.7
1/4			5.7	
cb			5.7	
N.L.			5.4	210.1

+	H.I. 210.48	−	
			Street unit 1H (50')
East ½ of Harney St. 7½ quarters			
M.L.		4.5	211.0
cl		4.5	
¼		5.4	
c		5.3	210.2
¼		4.9	
cl		6.0	
M.L.		5.5	210.0
Center of Harney St.			
M.L.		5.2	210.3
cl		5.2	
¼		4.0	
⊙		4.78	210.70 Mon Center
c		3.6	211.9
¼		3.3	
cl		3.3	
M.L.		3.0	212.5
West ½ of Harney St.			
M.L.		1.3	214.2
cl		2.2	
¼		2.0	

+	H.I. 210.48	−	
c		2.0	213.5
¼		2.0	
cl		2.8	
M.L.		2.2	213.3
West curb of Harney St.			
M.L.		2.1	213.4
cl		2.0	
¼		1.9	
c		1.6	213.9
¼		1.6	
cl		1.5	
M.L.		0.7	214.8
00 = West line of Harney St.			
M.L.		0.6	214.9
cl		1.9	
¼		2.0	
c		2.3	213.2
¼		2.7	
cl		2.5	
M.L.		2.4	213.1

	+	H.I. 210.48	−	Chestnut Mt (60')
+20 M.L.			5.0	210.5
cl			4.6	
1/4			4.4	
c			4.0	211.5
1/4			4.0	
cl			3.8	
M.L. +50			3.3	212.2
M.L.			5.9	209.6
cl			5.9	
1/4			6.4	
c			6.5	209.0
1/4			6.9	
cl			7.4	
M.L. +70			7.8	207.7
M.L.			11.0	204.5
cl			10.7	
1/4			10.4	
c			10.4	203.1
1/4			10.3	
cl			10.0	

	+	H.I. 210.48	−	
M.L.			10.3	205.2
# +100	0.26	203.09	12.65	202.83
M.L.			2.9	200.2
cl			2.5	
1/4			2.5	
c			2.5	200.6
1/4			2.4	
cl			2.4	
M.L. +20			2.3	200.8
M.L.			7.9	195.2
cl			8.7	
1/4			8.1	
c			8.8	194.3
1/4			9.2	
cl			9.6	
M.L.			10.3	192.8
# +50	0.06	190.55	12.60	190.49
M.L.			4.6	186.0
cl			5.0	
1/4			5.7	

	+	HI 190.55	−	Chestnut St (50')			+	HI 178.08	−		
c			5.9	184.7		cl			11.2		
1/4			6.1			1/4			11.3		
cl			5.8			c			11.4	166.7	
M.L. 1+75			5.6	185.0		1/4			11.9		
M.L.			12.6	178.0		cl			12.1		
cl			12.2			M.L.			12.5	165.6	
1/4			12.1			# 2+50	0.16	165.40	12.84	165.24	
c			12.2	178.4		M.L.			4.3	161.1	
1/4			12.0			cl			4.2		
cl			12.0			1/4			3.8		
M.L.			11.7	178.9		c			3.6	161.8	
# 2+00	0.29	178.08	12.76	177.79		1/4			3.2		
M.L.			6.0	172.1		cl			2.8		
cl			5.8			M.L. 2+75			2.6	162.8	
1/4			5.7			M.L.			5.9	159.5	
c			5.6	172.5		cl			6.5		
1/4			5.9			1/4			7.0		
cl			5.9			c			7.1	158.3	
M.L. 2+25			5.8	172.3		1/4			7.6		
M.L.			10.6	167.5		cl			8.0		

	+	H.I. 165.40	−	Chestnut St.
m.L.			8.2	157.2
3+00 = East line of Triggs St.				
00				
m.L.			9.2	156.2
ct			9.1	
I/J			9.0	
c			8.6	156.8
I/J			8.5	
ct			8.5	
m.L.			8.3	157.1
#			10.58	154.82 Mon Cen of Chestnut & Triggs

BM 254.25 Mon Con Tracks & Chestnut, Sts. 4-9-12 {Bowman Shaw Devine
+2.69
256.94
-8.37
248.57 Mon Con Chestnut & Annunciata Sts.

Crossection of Annunciata Av (50' wide), Chestnut to Bay Ct.
10' curbs 7½' quarters.

	+	H.I.	−	
	1.43	250.00		248.57
00 = South line of chestnut street				
00				
E.L.			0.9	249.1
ct			1.1	248.9
1/4			1.2	248.8
c			1.7	248.3
1/4			2.5	247.5
ct			3.1	246.9
W.L. +25			3.8	246.2 ✓
W.L.			4.9	245.1
ct			4.2	245.8
1/4			3.8	246.2
c			3.4	246.6
1/4			3.2	246.8
ct			2.6	247.4
E.L. +50.			2.2	247.8
E.L.			3.9	246.1
ct.			4.3	245.7
1/4			4.6	245.4
c			4.9	245.1
1/4			5.8	244.2
ct			5.7	244.3
W.L. +75			6.1	243.9
W.L.			6.9	243.1
ct			6.6	243.4
1/4			6.6	243.4
c			6.4	243.6
1/4			6.0	244.0
ct			5.8	244.2
E.L. 1+00			5.6	244.4
E.L.			7.4	242.6
ct			7.6	242.4
1/4			7.8	242.2
c			8.0	242.0
1/4			8.7	241.3
ct			9.4	240.6
W.L.			10.0	240.0
At 1+00 Alpe 20' W. W. L.			11.2	238.8
" 1+25 " 20' " " "			14.3	235.7

Amphidia St (50' wide)

	+	H.I. 250.00	−	
1+25				
W.L.			13.4	236.6
cl			12.4	237.6
1/4			11.6	238.4
c			11.1	238.9
1/4			10.8	239.2
cl			10.4	239.6
E.L.			9.9	240.1
1+50				
E.L.			11.9	238.1
cl			12.4	237.6
1/4			13.0	237.0
c			13.4	236.6
1/4			14.5	235.5
H	6.73	238.03	12.70	237.30
cl			3.1	234.9
W.L.			4.3	233.7
at 1+50 slope 20' West of West Line			5.7	232.3
" 1+75 " 25' " " " "			8.2	229.8
1+75				
W.L.			6.9	231.1
cl			5.9	232.1
1/4			5.1	232.9

	+	H.I. 238.03	−	
c			4.5	233.5
1/4			4.0	234.0
cl			3.2	234.8
E.L.			1.3	235.7
2+00				
E.L.			4.4	233.6
cl			5.7	232.3
1/4			6.8	231.2
c			7.5	230.5
1/4			9.2	228.8
cl			9.0	229.0
W.L.			9.7	228.3
at 2+00 slope 25' W. of W.L.			11.5	226.5
" 2+25 " 25' " " "			15.1	222.9
2+25				
W.L.			12.8	225.2
cl			11.2	226.8
1/4			10.7	227.3
c			9.7	228.3
1/4			8.8	229.2
cl			7.7	230.3
E.L.			5.6	232.6

+	H.I. 238.03	−	Ampudia St (50' wide)
2+50 E.L.		6.2	231.8
cl		8.1	229.9
1/4		9.5	228.5
c		10.3	227.7
1/4		11.2	226.8
cl		12.7	225.3
W.L.		14.8	223.2
at 2+50 slope 25' West of West Line		17.5	220.5
# 3.15	231.63	9.55	228.48 Mon Center Ampudia & Whitman
at 2+75 slope 25' West of West line		13.6	218.0
2+75			
W.L.		8.8	222.8
cl		6.5	225.1
1/4		5.0	226.6
c		3.4	228.2
1/4		2.3	229.3
cl		1.3	230.3
E.L.		0.0	231.6
3+00 = North line of Whitman St (50' wide),			
3+00 E.L.		0.1	231.5
cl		1.0	230.6

+	H.I. 231.63	−	
1/4		2.0	229.6
c		2.8	228.8
1/4		3.6	228.0
cl		5.4	226.2
W.L.		8.0	223.6
at 3+00 slope 25' W. of W. Line		14.0	217.6
North curb of Whitman St (50' wide),			
W.L.		8.1	223.5
cl		5.4	226.2
1/4		3.7	227.9
c		2.7	228.9
1/4		1.8	229.8
cl		1.2	230.4
E.L.		0.6	231.0
North 1/4 of Whitman St (24')			
E.L.		1.1	230.5
cl		1.6	230.0
1/4		1.8	229.8
c		3.0	228.6
1/4		4.0	227.6

+	H.I. 231.63	−	Ampudia (50' wide)
c.l.		5.5	226.1
W.L.		8.1	223.5
Center Line of Whitman St.			
At Center line slope 25' West W.L.		15.4	216.2
W.L.		8.1	223.5
c.l.		5.6	226.0
1/4		4.2	227.4
c		3.1	228.5
1/4		2.2	229.4
c.l.		2.1	229.5
E.L.		1.8	229.8
South 1/2 Whitman St (7½ wide).			
E.L.		2.5	229.1
c.l.		2.6	229.0
1/4		2.7	228.9
c		3.4	228.2
1/4		4.4	227.2
c.l.		6.0	225.6
W.L.		8.4	223.2
South curb of Whitman St.			

+	H.I. 231.63	−	
W.L.		8.2	223.4
c.l.		6.2	225.4
1/4		4.5	227.1
c		3.5	228.1
1/4		3.1	228.5
c.l.		3.1	228.5
E.L.		2.9	228.7
00 = South line of Whitman St.			
00 E.L.		3.4	228.2
c.l.		3.3	228.3
1/4		3.5	228.1
c		4.0	227.6
1/4		5.0	226.6
c.l.		6.5	225.1
W.L.		8.4	223.2
At 00 Slope 25' West of West line		16.0	215.6
" +25 " 25' " " " "		16.0	215.6
W.L.		9.5	222.1
c.l.		7.4	224.2
1/4		6.4	225.2

Ampudia (50' wide)

	+	H.I. 231.63	−
c			5.6
¼			5.7
cb			7.5
E.L.			8.9
at +25 slope 15' East of East line			10.5
at +40 " 20' " " " "			19.5
+40			
E.L.			14.7
cb			12.8
¼			11.4
c			10.3
¼			9.6
cb			9.9
W.L.			10.7
at +40 slope 25' West of West line			19.5
#	0.42	219.15	12.90
at +50 slope 25' West of West line			7.1
+50			
W.L.			2.4
cb			1.7
¼			2.4
c			2.7

	+	H.I. 219.15	−
¼			3.8
cb			5.5
E.L.			7.5
at +50 slope 25' East of East line			14.3
#	0.29	206.67	12.77
at +75 slope 40 East of East line			6.7
" " " 27' " " " "			12.8
" " " 19 " " " "			19.6
" " " 10 " " " "			15.9
+75			
E.L.			10.9
cb			9.2
¼			9.5
c			6.4
¼			5.8
cb			5.8
W.L.			6.4
at +75 slope 25' West of West line			7.9
" +90 " " " " " "			15.8
#	0.14	194.66	12.15
+90			
W.L.			2.3

	215.4
	213.7
	211.7
	204.9
	206.38
	200.0
	193.9
	187.1
	190.9
	195.9
	197.5
	197.2
	200.3
	200.9
	200.9
	200.3
	198.8
	190.9
	194.52
	192.4

	+	H.I. 194.66	−	Ampudia (50')
c.l.			3.2	191.5
1/4			4.4	190.3
c			5.9	188.8
1/4			8.3	186.4
c.l.			8.8	185.9
E.L.			12.3	182.4
at 1+50 Slope 40' East of East line			+12.0	206.7
" 1+00 " 40' " " " "			+17.2	211.9
E.L.			5.7	188.0
c.l.			9.4	185.3
1/4			16.2	178.5
c			11.2	183.5
1/4			9.7	185.0
c.l.			8.7	186.0
W.L.			9.6	185.1
at 1+00 Slope 25' West of West line			10.9	183.8
" 1+20 " 50' " " " "			18.4	176.3
" " " 25' " " " " 1+20			25.5	169.2
W.L.			24.8	169.9
c.l.			22.8	171.9

	+	H.I. 194.66	−	
1/4			14.7	180.0
c			11.1	183.6
1/4			8.0	186.7
c.l.			5.5	189.2
E.L.			0.8	193.9
at 1+20 Slope 20 East of East line 1+50			+10.8	205.5
# 1+50	5.24	199.76	0.14	194.52
E.L.			+9.2	209.0
c.l.			+4.8	204.6
1/4			+2.0	201.8
c			1.1	198.7
1/4			3.9	195.9
c.l.			7.6	192.2
W.L.			11.2	188.6
at 1+50 Slope 40' West of West line			32.5	167.3
" " " 50 " " " "			43.4	156.4
" " " 75 " " " "			37.8	162.0
" " " 100 " " " "			41.0	158.8
" 1+75 " 100 " " " "			52.0	147.8
" " " 50' " " " "			34.7	168.1

194.7
10.6
2.16.4
19
33
52

	+	H.I. 199.76	−	Amphidia (50')
1+75 W. L.			7.9	191.9
cl			3.5	196.3
1/4			0.0	199.8
c			+2.9	202.7
1/4			+6.4	206.2
cl			+9.0	208.9
E.L. 2+00			+12.8	212.6
E.L.			+9.5	209.3
cl			+6.4	206.2
1/4			+4.1	203.9
c			+1.4	201.2
1/4			1.6	198.2
cl			4.7	195.1
W. L.			8.7	191.1
at 2+00 Slope 50' West of West line			26.1	173.7
" 2+25 " 50' " " " "			28.2	171.6
" " " 35' " " " "			19.5	180.3
2+25 W. L.			11.6	188.2
cl			8.6	191.2
1/4			5.5	194.3

	+	H.I. 199.76	−	
c			2.5	197.3
1/4			+0.5	200.3
cl			+2.9	202.7
E.L.			+6.0	205.8
# 2+50	2.20	189.70	12.26	197.50
E.L.			+11.9	201.6
cl			+8.0	197.7
1/4			+5.6	195.3
c			+2.1	191.8
1/4			1.0	188.7
cl			3.5	186.2
W. L.			5.6	184.1
at 2+00 Slope 25' West of West line			11.6	178.1
" " " 50' " " " "			21.2	168.5
" 2+75 " 50' " " " "			29.1	160.6
" " " 20' " " " "			17.0	172.7
2+75 W. L.			10.2	179.5
cl			8.2	181.5
1/4			6.0	183.7
c			4.1	185.6

	+	H.I. 189.70	−	Amprndia (50')
½			1.2	
cb			+1.8	191.5
E.L.			+6.0	195.7
3+00 = North line of Boyd St (66' wide)				
3+00				
E.L.			5.0	184.7
cb			8.0	181.7
½			10.0	179.7
c			11.3	178.4
½			13.1	176.6
cb			14.1	175.6
W.L.			15.4	174.3
At 3+00 slope 26' West of West line			21.9	167.8
" " " 50' " " " "			32.2	157.5
#			6.67	183.03 Old Iron NE Cor of Amprndia & Boyd.

Fraction of Hortensia H. 50' wide — ~~East~~ line ~~Fort~~ N. 4th. Stockton Drive & West line Chestnut.

BM 250.87 Hub NE Cor, Hortensia & Hickory.

4-15-12 {Domain about Being.

	+	H.I.	−	
	12.38	263.25	250.87	
		~~Fort~~ Stockton drive		
00 = Nestle line of ~~Hort~~ Street.				
00				
W.L.			1.6	261 2
cl			1.8	
gutter			2.5	
1/4			2.4	
c			2.5	60 7
1/4			2.9	
gutter			3.2	
cl			2.7	
E.L.			2.5	60 7
0+1				
E.L.			2.5	60 7
cl			2.9	
+1			3.4	
1/4			2.8	
c			2.6	60 6
1/4			2.5	
+5			2.5	
+6			1.1	
cl			1.1	

	+	H.I. 263.25	−	
W.L. +25			0.9	262 3
W.L.			2.3	60 9
cl			2.3	
+2			2.7	
+3			3.4	
1/4			3.5	
c			3.6	59 6
1/4			3.9	
+6			4.4	
cl			3.4	
E.L. +50			3.5	59 7
E.L.			4.9	58 3
cl			5.0	
+1			5.8	
1/4			5.7	
c			5.2	58 0
1/4			4.9	
+5			4.7	
cl			4.0	
W.L.			3.8	59 4

	+	H.I. 263.25	−	Hortensia St 50 inside
+75 W. 2.			5.1	58 1
cl			5.5	
1/4			6.3	
c			6.7	56 5
1/4			7.1	
+6			7.3	
cl			6.5	
E. 2.			6.0	57 2
1+00 E. 2.			7.7	55 5
cl			8.0	
+1			8.7	
1/4			8.6	
c			8.3	54 9
1/4			7.9	
cl			7.1	
W. 2.			6.6	56 6
1+25 W. 2.			8.1	55 1
cl			8.8	
1/4			9.4	
c			9.7	53 5

	+	H.I. 263.25	−		
					70
1/4			10.0		
+6			10.0		
cl			9.3	53 9	
E. 1.			9.1	54 1	
H 1+50	5.07	25-5 84	12.38	25-0 87	
E. 2.			2.9	53 0	
cl			2.2		
+1			3.7		
1/4			3.6		
c			3.5	52 4	
1/4			3.1		
cl			2.3		
W. 2. 1+75			2.2	53 7	
W. 2.			2.7	53 2	
cl			3.0		
1/4			3.7		
c			4.0	51 9	
1/4			4.3		
cl			4.0		
E. 2.			3.6	52 3	

	+	H.I. 255.94	−	Hortensia St 80' wide
2+00				
E.L.			4.5	51 4/5
cl			4.5	
1/4			4.5	
c			4.2	51 7/5
1/4			3.9	
cl			3.0	
W.L. 2+25			2.3	53 1/5
W.L.			2.3	53 8/5
cl			2.8	
1/4			3.5	
c			3.8	52 1/5
1/4			4.4	
cl			4.6	
E.L. 2+50			5.0	50 9/5
E.L.			5.0	50 9/5
cl			4.1	
1/4			3.9	
c			3.4	52 5/5
1/4			3.0	
cl			2.2	

	+	H.I. 255.94	−	
W.L. 2+75			1.4	54 5/5
W.L.			1.4	54 5/5
cl			2.1	
1/4			3.1	
c			3.2	52 7/5
1/4			3.8	
cl			4.0	
E.L. 2+89.2			4.8	51 1/5
= North line of Hickory St.				
2+89.2				
E.L.			5.0	50 9/5
cl			4.1	
1/4			4.0	
c			3.1	52 8/5
1/4			3.0	
cl			2.2	
W.L.			1.7	54 2/5
#	3.78	254.65	5.07	250.87
00 = South line of Hickory St.				
00				
W.L.			1.4	253 2/5
cl			2.0	252.6

+	H.I. 254.65	−	Hortensia St 60' wide
¼		2.5	252.1
c		3.0	N51 6
¼		3.6	251.0
cb		4.2	250.4
E.L. +25		4.9	N49 7
E.L.		6.3	N48 3
cb		5.2	N49.4
¼		4.6	250.0
c		3.9	N50 7
¼		3.5	251.1
cb		3.0	251.6
W.L. +50		2.0	N52 6
W.L.		2.9	N51 7
cb		3.9	N50.7
¼		4.4	250.2
c		4.9	N49 7
¼		5.7	N48.9
cb		6.5	N48.1
E.L.		7.6	N47 0
at +50 Slope 15 East of East line		10.0	244.0

+	H.I. 254.65	−	
at +75 Slope 15 East of East line +75		11.4	N43.2
E.L.		9.1	N45 5
cb		7.7	N46.9
¼		6.8	N47.7
c		6.0	N48 6
¼		5.2	N49.4
cb		4.8	N49.8
W.L. 1+00		3.8	N50 8
W.L.		4.6	N50 0
cb		5.3	N49.3
¼		5.8	N48.8
c		6.8	N47 8
¼		7.9	N46.7
cb		8.8	N45.8
E.L.		10.4	N44 2
at 1+00 Slope 15 East of East line		13.8	N40.8
" 1+25 " 15 " " " " 1+25		16.4	N38.2
E.L.		11.8	N42 8
cb		9.8	N44.8
¼		8.5	N46.1

	+	H.I. 254.65	−	Hartenia Dr 30' wide
c			7.3	N47 3
1/4			6.6	N48.0
cl			6.2	N48.4
W.L. 1+50			4.7	N49 9
W.L.			5.4	N49 2
cl			6.6	N48.0
1/4			7.0	N47.6
c			9.1	N46 5
1/4			9.5	N45.1
cl			11.0	N43.6
E.L.			13.5	N41 1
#	5.14	249.23	10.56	244.09
At 1+50 slope 15' East of East line			12.6	N36.6
" 1+75 " " " " " "			14.7	N34.5
E.L.			9.7	N39 5
cl			6.3	N47.9
1/4			4.6	N44.4
c			3.3	N45 9
1/4			2.5	N46.7
cl			2.0	N47.2

	+	H.I. 249.23	−	
W.L. 2+00			0.6	N48 6
W.L.			1.0	N48 2
cl			2.7	N46.5
1/4			3.2	N46.0
c			4.3	N44 9
1/4			5.5	N43.7
cl			7.0	N47.2
E.L.			10.2	N39 0
At 2+00 slope 15' East of East line			14.7	N34.5
" 2+25 " " " " " " 2+25			14.6	N34.6
E.L.			10.5	N38 7
cl			7.3	N41.9
1/4			5.9	N43.4
c			5.0	N44 2
1/4			4.0	N45.2
cl			3.6	N45.6
W.L. 2+50			1.9	N47 3
W.L.			2.6	N46 6
cl			4.5	N44.7
1/4			5.1	N44.1

	+	H.I. 249.23	−	Horlonia St 30' wide		+ −	H1 244.26	−	
c			6.6	N42.6					
1/4			9.3	N40.9	cl		− −	10.0	234.3
cl			10.3	N39.9	E.L.			13.8	N30.5
E.L.			12.7	N36.5					
at 2+50 Slope 15' East of East line			16.6	N31.6					
" 2+75 " 20' " " " "			22.1	N27.1					
2+75									
E.L.			10.0	N34.2					
cl			11.8	N32.4					
1/4			10.1	N39.1					
c			8.5	N40.7					
1/4			6.8	N42.4					
cl			6.1	N43.1					
W.L.			4.5	N44.7					
3+00 = North line of Chestnut St.									
# 3+00	7.63	244.26	12.60	236.63					
W.L.			0.1	N44.2					
cl			2.9	N41.4					
1/4			3.8	N40.5					
c			6.1	238.2					
1/4			7.9	236.4					

ON	From	To	Page
Sta 12+65 on Alley bet Florida & Alabama and Sta. 2+85 Ft. or - 2			
Florida Alley bet Texas & Ariz	Urn	Howard	3-5
	Howard	Polk	6-7
Texas Alley North of El Cajon	Alley S El Cajon	Alley N El Cajon	8
Alley bet Ariz & Texas	Mississippi Alley Not	Idaho	9-11
Alley bet Florida Alabama	El Cajon	Madison	12-14
	Polk	El Cajon	15-16
Park Blvd	Georgia	El Cajon	17
Alley bet El Cajon & Howard	Park Blvd	Mississippi	18-19
Alley bet Texas Louisiana	El Cajon	Monroe	20-21
Alley bet Louisiana Mississippi	"	"	22-23
Georgia	El Cajon Park Blvd	St. Meade	24-25
Alley bet El Cajon & Meade	Georgia	Louisiana	26-27
Alley Bet. Mississippi Alabama Sts	El Cajon	Madison	28-30
Alley bet. Georgia Florida	"	Meade	31-33
Florida	"	Madison	34-36
Chestnut St			37-60
Ampudia			61-

18.00

242.90
1.85
244.75

25-11, 26 An Chestnut to Trini
262.90 an Inland History.

BM 255.00 N.W. Cor 1st & Thorn.

256.00
+ 3.38
259.38 HI.
- 6.91
251.47
+ 0.81
252.28 HI.
- 12.82
239.46
+ 1.05
240.51 HI.
- 6.56
233.95
+ 3.97
237.92 HI.

237.92 / 4.42 / 233.50
237.92 / 3.75 / 234.17
237.92 / 3.56 / 234.36
237.92 / 4.23 / 233.69
237.92 / 4.27 / 233.65
237.62 / 2.27 / 235.35
237.62 / 1.34 / 236.28

237.92 / 1.04 / 236.88

Ele on cement walk 3.3' East curb Line = 235.35

" " " " 12' " " " = 236.28

" " " " 20 " = Prop " = 236.88

No regular walk in but curb is standard stuff.

Mar 5th - 1912
Doman
Shaw,
Devine

3.36

80

Spruce St.

Check Ele 233.50

Curb Line, 20' from Prop.

St.

Cement walk running from curb to building. Walk 4' wide & has 3 steps at & above curb with 6" risers - all of cement.

Curb Ele to South Sprucé = 234.17

15'

20'

20

A

Building 53' front flush with Prop line.

" " 123' " " = 234.36
" " 124' " " = 233.69

" " 140' " " = 233.65

20'

Front

Prop Line.

Redwood St.

2+66 on Florida 25 S. of alley

332.57
0.92
331.65
337.47
4.10
333.37
328.00
5.4

378.88
7.80
371.08

945

425
150
275
137.5

225
75
150

312.86
4.70
307.16

347.64
8.22
339.42

341.53
2.13
339.40

299.28
291.50
7.78

342.28
3.61
338.67

325.79 S.W. 2 nails N.W. cor alley

347.06

348.44
11.38
337.06

4.2
8.3
12.7

332.29
1.02
331.27
2.20
329.07
0.50
328.57

328.55

11
11
136
13
150

2.72
8.08
64

332.68
9.29
323.39 52250

240.61
7.60
232.91

303.31
7.96
295.35

314.46

324.07
9.07
315.00
311.50
3.50
26
16250
313.75

224.07
13.57
210.50

Grade

20 | 700 | 3.18
60
100
120
180

318
336

1.2

3.5
4
1,272

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318
954

317.00
1.27
315.73

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