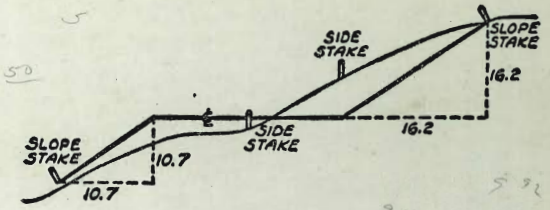
G-313



Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

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APR 15 1965

Table XIII—Corrections for Tangents and Externals

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

For Tangents Add

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	.26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

For Externals Add

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

Stake Alley Blk 109 Central Park (31 to 32 K to L) sts p1

Stake drainage ditch Friars Rd. 2

4358 Hill St.

Stake Sewer Riviera Villas Lot 23 3

Stake Laurel & Harbour Laurel St 4-8

Stake Gloria St Ocean View to Franklin 9-11

Sunset Cliffs & Ebers omit (12)

Stake Alley Blk 37 Ocean Beach Coronado & Santa Cruz 13-14

Stake Harbor Dr. 15-29

Stake Armstrong St wly cs only 30-31

Stake Poinsettia & Curtis Sts 32-35

Stake Del Rey St 36-38

Stake Storm Drain Jamacha Rd & Glencoe St 39-40

Stake Storm Drain Talbot St & Canyon & Albion 41-42

Stake Sewer Camino Del Collado 43

Stake Ely ½ 45th St Market St 623' Sly 44-45

Stake Alley Blk 45 Normal Hts 46 ✓

Stake Alley Blk 176 Univ Hts 47-48 ✓

Stake Sewers Water Winchester & Morning side 49

Stake Alley Blk 83 Pt Loma Hts 50-51

Stake Storm Drain Bellevue 52

Stake Alley Blk 30 Park Villas Univ Myrtle Stat & Drain 53

Stake Alleys Blk 43 Normal Hts 60-62

Stake Storm Drain Nly "B" St Btwn 30th & 31st Sts 63

(78-79) (64-75)

Stake La Jolla Blvd Colima to De la Costa Back of Book ✓

Stake Martin St 35th to Wabash curbs (76-77) Back of Book

Stake Storm Drains Midway & La Jolla Blvd 78 ✓

Stake Muirlands Sewer Outfall Sly 54-59

D. Smith
J. Rorer
R. Taylor
B. Fish

Plan # 10310-L

INDEXED

Alley Blk 109

Please Note: Alley is 20' wide but is paved only 18' according to plan

	Lt = Nly	℄	Rt = Sly 2' Bk pav. edge
2+60	CO 90 80 25 79 35		79 35 80 27 CO 92 1' Bk
2+20	Nail 1' Bk CI 66 80 89 79 23		79 23 80 72 CI 49 0 22 Bk
1+80	1' Bk CO 49 79 60 79 11		79 11 80 76 CI 65 0 74 inside pav
	stake 5' Bk Prop 79 38 CI 4 15		
1+65 ① Rt	Nail 1 68 in 80 26 CI 5 03		75 23 ie prop
1+40	CO 37 79 36 78 99		78 99 80 35 CI 36 0 17 Bk
1+00 Brk	CO 37 79 24 78 87		78 87 79 93 CI 06 .02 inside pav
0+80	CO 25 78 99 78 74		78 74 78 88 CO 14 1' inside pav
0+60 Brk	CO 03 78 50 78 47		78 47 78 73 CO 26
0+20	CO 33 78 13 77 80		77 80 78 71 CO 91
0+00 Ely 31st.	77 41		77 36
BM			78 48 NEBP 31st & K

Central Park

WO# 31566 ①
9/17/53

	Lt = Nly	℄	Rt = Sly
6+01 22 Wly 32nd.	79 68		79 68
5+65	FO 21 79 54 79 75		79 75 79 50 FO 25 1' Bk
5+30	FO 16 79 65 79 81		79 81 79 50 FO 31 2 02 Bk
4+95	FO 33 79 55 79 88		79 88 79 95 CO 07
4+60 Brk	0 59 Bk CO 30 80 25 79 95		79 95 79 62 FO 33 1' Bk
4+20	1' Bk CO 23 80 06 79 83		79 83 79 58 FO 25 1' Bk
3+80	FO 14 79 57 79 71		79 71 79 05 FO 66
3+40	CO 28 79 87 79 59		79 59 79 79 CO 20
3+15 ② Lt	75 83 ie prop		79 92 CI 4 09 5' Bk Prop
3+00	Nail 0 34 Bk CI 61 81 08 79 47		79 47 80 75 CI 28 0 45 Bk

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JUN 7 1954

Stake Drainage Ditch

2+29.5	-0.4	79.6		77.4		79.8	+0.3	6+32.5	-0.1	70.1		69.0		70.1	-0.2		
	5'RP	5.9				6.3			5'RP	3.2				3.2			
		C2.2				C2.4	5'RP			C1.1				C1.1	5'RP		
1+84.5	+0.2	80.7		80.1		81.5	+0.2	6+04.5	-0.1	70.5		69.7		71.1	-0.2		
	5'RP	2.7				4.3			5'RP	4.1				5.3			
		C0.6				C1.4	5'RP			C1.3				C1.9	5'RP		
1+39.5 Brk	-2.4	85.2		82.7		84.2	-0.3	5+64.5	+0.1	70.3		69.4		70.7	+0.1		
	5'RP	6.5				4.5			5'RP	4.3				4.1			
		C2.5				C1.5	5'RP			C1.4				C1.3	5'RP		
1+14.5 Brk	-2.8	88.3		85.3		87.1	+0.7	5+24.5	+0.1	70.8		69.6		70.7	-0.2		
	5'RP	7.5				5.1			5'RP	3.9				3.7			
		C3.0				C1.8	5'RP			C1.3				C1.1	5'RP		
0+72.4 E.C.	-0.9	95.5		91.6		94.9	+1.2	4+84.5	+0.1	70.9		69.8		71.0	-0.2		
	5'RP	9.3				8.1			5'RP	3.2				3.9			
		C3.9				C3.3	5'RP			C1.1				C1.2	5'RP		
0+52.3 Mid P.	-1.0	98.1		94.0		96.8	-0.2	4+44.5	+0.2	71.2		70.0		71.1	+0.1		
	5'RP	9.6				7.1			5'RP	3.9				3.7			
		C4.1				C2.8	5'RP			C1.2				C1.1	5'RP		
50' Rad																	
0+33.1 BC	+0.3	99.3		96.6		97.9	0.0	4+04.5	+0.1	71.4		70.2		71.4	-0.1		
	5'RP	6.9				4.1			5'RP	3.9				3.9			
		C2.7				C1.3	5'RP			C1.3				C1.2	5'RP		
0+21.6 EC	+0.7	99.7		97.8		99.7	-0.2	3+64.5 Brk	0.0	71.7		70.4		70.6	0.0		
	5'RP	5.3				5.3			5'RP	4.1				3.9			
		C1.9				C1.9	5'RP			C1.3				C1.2	5'RP		
20' Rad																	
0+09.3 BC	5'RP	100.3		99.0		100.3	-0.1	3+39.5	0.0	72.0		70.9		72.0	+0.1		
	+0.2	4.1				4.1			5'RP	3.7				3.7			
	5'RP	C1.3				C1.3	5'RP			C1.1				C1.1	5'RP		
0+00	+0.1	101.7		100		101.9	+0.4	3+14.5 Brk.	+0.1	73.6		72.1		73.6	+0.2		
	5'RP	4.7				5.3			5'RP	4.5				4.5			
		C1.6				C1.9				C1.5				C1.5	5'RP		
				2:1				2+74.5	-0.2	76.7		74.7		76.8	+0.2		
				3 5					5'RP	5.5				5.2			
										C2.0				C2.1	5'RP		

6785 Friars Rd
address

WO# R1059
10-7-53

Stake Sewer
4358 Hill St.

Lot 23
stake 3' wly

Riviera Villas Map # 1929

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JUN 7 ...

Ref FB2272

1+57.9 Brk 45° L.		210.46	~~211.56~~ 212.99	C2.53 ~~C1.43~~
1+40		210.82	~~211.80~~ 213.94	C3.12 ~~C2.14~~
1+20		211.22	~~212.06~~ 215.72	C4.50 ~~C3.66~~
1+00		211.62	~~212.32~~ 216.08	C-4.46 ~~C3.76~~
0+80	.0200 rate ~~.013 rate~~	212.02	~~212.58~~ 216.34	C-4.32 ~~C3.76~~
0+60		212.42	~~212.84~~ 216.23	C-3.81 ~~C3.39~~
0+40		212.82	~~213.10~~ 215.55	C-2.73 ~~C2.45~~
0+20		213.22	~~213.36~~ 215.72	C2.50 ~~C2.36~~
0+00 Meet existing pipe	School prop		213.62 Meet elv.	
BM Lect.			216.63	

P3 FB2272

1+87.9 MH #1			199.53	meet 204.21 C4.68
1+67.9 cut off wall	~~.4007 rate~~ .3643 rate	206.82	207.55	212.55 6' wll C-5.73 ~~C5.00~~

Stake Storm Drains
Laurel & Harbour Dr.
staked 6' off into st.

1+56 92		-4 94	1 64 C6 58
35'			
1+21 92 EC pipe	37° 46.50'	-4 76	1 54 C6 30
1+01 92	31° 24.459	-4 66	1 72 C6 38
0+81 92	25° 02.487'	-4 56	1 61 C6 17
0+61 92	18° 40.515'	-4 46	1 61 C6 07
0+41 92	12° 18.543'	-4 36	1 75 C6 11
20			
0+21 92	5° 56.571'	-4 26	2 04 C6 30
18 67			
0+03 25 B.C. pipe	0° 00'		
0+00 ℄ inlet B.C. ℄	-0 33 cb -1 16 grate -4 15 1e		2 04 C-2 37 C-3 20 C-6 19
BM Osborne ℄ Nail			4 41 59

.005061 rate

Δ = 75° 33'
℄ R = 90
offset 96
T = 69 75
L = 118 67
d = 19.0986

all staked 5' BK cb face

1+60 ℄ Cleanout	7 25 BK ℄ pipe	-4 00 1e 18"	3 60	C-7 64
1+20	6 95 BK	-3 25	4 02	C-7 27
0+80	6 66 BK	-2 50	3 60	C-6 10
0+40	6 37 BK	-1 75	3 45	C-5 20
0+00 = cb inlet ℄	6 08 BK ℄ pipe	3 56 cb 2 73 grate -1 00 1e	3 13	F0 43 C0 40 C-4 13
2+59 22 ℄ existing inlet		-7 00 1e new	1 41 C-8 41	-8 24 1e 54"
2+47 ℄ cleanout		-5 40	1 36 C-7 76	0 50 top C-0 86
2+26 92		-5 30	1 44 C-6 74	
1+91 92		-5 12	1 58 C-6 70	

	cb		wall
0°00' (stake - is tie deflection back to cb beam joint)		1.92 C2.24	
1+66.52 83/100 1°20.765'	-0.32	-1.15 gut	2.47 F0.55
0°00.00 2'BKcb c=5.73			
1+59.18 ℄ BC 0°00' (℄ catch basin)			
2'BKcb c=9.90		-1.33 F1.03	
		~~C2.12~~ ~~1.81~~	
1+46.5 74/100 face POC 3°40.368'	-0.31	-1.05 gut	2.32 F0.51
		-1.47 ~~2.51~~ F1.20	
1+26.5 7°20.736'	-0.27	~~C2.78~~	2.20 C0.31
		-1.48 ~~2.23~~ F1.35	
1+06.5 11°01.104'	-0.13	~~C2.36~~	1.86 C0.37
		-1.02 ~~2.34~~ F1.07	
0+86.5 14°41.472' end wall	0.05	~~C2.29~~	1.10 C1.24
		-0.68 ~~1.83~~	
0+66.5 18°21.840'	0.31	~~C1.52~~	F0.99
		-0.31 ~~1.66~~	F0.93
0+46.5 22°02.208'	0.62	~~C1.04~~	
2'bk cb c=15.63		1.62 ~~1.78~~	C0.65
0+26.5 25°42.576'	0.97	~~C0.81~~	
2'bk cb c=5.09		1.42 ~~1.84~~	C0.34
0+20.3 26°54.40' end cb begin Berm POC	1.08	~~C0.76~~	

	cb		wall
		2.17 F0.50 ~~3.37~~	
3+61.90 end wall	2.67	~~C0.72~~	3.75 F0.36
3+46.53	2.24	1.43 F0.81	
		~~3.41~~ 0.92	
3+31.16 31°34.945'	1.81	~~C1.60~~ F0.89	3.50 F0.09
2'BKcb c=3.64			
3+26.52 30°43.709			
		0.06 ~~3.08~~ F1.20	
3+06.5 27°03.341'	1.26	~~C1.79~~	3.35 F0.30
		0.59 ~~2.70~~ F0.04	
2+86.5 23°22.973'	0.63	~~C2.27~~	3.22 F0.32
		0.78 ~~2.70~~ C0.47	
2+66.5 19°42.605'	0.31	~~C2.39~~	3.09 F0.39
		-0.82 ~~2.52~~ F0.97	
2+46.5 16°02.237 POC	0.15	~~C2.37~~	2.96 F0.44
		-1.21 ~~2.46~~ F1.24	
2+26.5 12°21.869	0.03	~~C2.43~~	2.83 F0.37
		-1.32 ~~2.28~~ F1.21	
2+06.5 8°41.501' POC	-0.11	~~C2.39~~	2.70 F0.42
		-0.87 ~~2.08~~ F0.64	
1+86.5 5°01.133'	-0.23	~~C2.29~~	2.61 F0.53
1+69.18 end new throat 85/100 cb face	gut -1.15	cb -0.30	2.49 C2.79 cb

	Stake of Laurel Wly Side Only	5'BK of Face
5+19.91	4.00	3.72 F0.28
4+98.16	3.91	3.61 F0.30
4+76.41	3.82	3.48 F0.34
4+54.66	3.74	3.43 F0.31
4+32.91	3.65	3.29 F0.36
4+11.16 Inlet	3.56	3.13 F0.43
3+76.46	3.62	3.48 F0.14
3+61.90	3.73	3.29 F0.44
3+31.14 EC. &	4.10	3.35 F0.75
3+07.16 Begin	4.39	3.32 F1.07

	of Wly Side Laurel St 5'BK of Face	
7+37.41	4.86	4.35 F0.51
7+15.66	4.78	4.31 F0.47
6+93.91	4.69	4.26 F0.43
6+72.16	4.60	4.18 F0.42
6+50.41	4.52	4.08 F0.44
6+28.66	4.43	4.05 F0.38
6+06.91	4.34	3.97 F0.37
5+85.16	4.26	3.84 F0.42
5+63.41	4.17	3.75 F0.42
5+41.66	4.08	4.08 G

	Wly Cb Laurel 5' Bk cb face			Ely Cb Laurel stake 8' Bk cb face	
9+71 cbend inlet	4.89 grate	5.90	1' cb face	6+05.66	4.11 3.84 FO.27
9+60.53 obegutend	5.18	5.85	5.06 FO.79 .67 cb face	5+77.87	4.00 3.90 FO.10
				5+50.09	3.88 3.95 CO.07
8+89.03 obendgut	4.97 gut	5.55	4.48 FI.07 .58 cb face		
				5+22.30	3.77 4.02 CO.25
23					
8+66.03 cbend		5.43	4.41 FI.02 ~~4.53 FO.90~~	4+94.52	3.66 4.00 CO.34
8+46.03		5.30	4.38 FO.92	4+66.73	3.55 3.93 CO.38
8+24.41		5.21	4.41 FO.80	4+38.95	3.44 3.93 CO.49
8+02.66		5.12	4.29 FO.83	4+11.16 EVC	3.33 3.68 CO.35
7+80.91		5.04	4.68 FO.36	3+71.16	2.87 3.34 CO.47
7+59.16		4.95	4.44 FO.51	3+31.16 EC 2.5 BK	1.81 3.41 CI.60 2.50 BK

	Stake Ely Cbs Laurel 8' BK cb face		Stake Ely Cbs Laurel St 8' BK cb face	
8+83^{51}	5^{22}	5^{19} F.0^{03}		
8+55^{72}	5^{11}	5^{37} C0^{26}		
8+27^{94}	5^{00}	5^{21} C0^{21}	Prop Cb end	6^{54} 5^{80} F 0^{74}
8+00^{15}	4^{88}	5^{07} C0^{19}	10+36^{85} 8' Rad BC cb	6^{38} 5^{80} F0^{58}
7+72^{37}	4^{77}	3^{82} F.0^{95}	10+26^{85}	6^{29} 5^{54} F.0^{75}
7+44^{58}	4^{66}	3^{42} F-1^{24}	10+06^{85}	5^{99} 5^{25} F.0^{74}
7+16^{80}	4^{56}	3^{20} F-1^{35}	9+86^{85}	5^{70} 4^{96} F.0^{74}
6+89^{01}	4^{44}	3^{15} F-1^{29}	9+66^{85} BVC	5^{55} 4^{88} F.0^{67}
6+61^{23}	4^{33}	3^{02} F-1^{31}	9+39^{08}	5^{44} 4^{70} F.0^{74}
6+33^{44}	4^{27}	3^{19} F-1^{03}	9+11^{29}	5^{33} 4^{73} F.0^{60}

D. Smith
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B. Fish

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Stake Gloria St

Wo# 31731

Ocean View to Franklin

	Rough 5' BK	Cb grade	Cb	℄	Cb	Cb grade	5' BK Rough
2+09 R	C-1 73 2 21	140 48	40 76 CO 28	140 19	CO 51 40 49	139 98	(W) 7 14 F-2 84
1+80	C-1 95 2 15	140 20	40 73 CO 53	139 91	CO 44 40 14	139 70	7 52 F-2 18
1+67 Plug							133 32 7 56 C-4 24
1+65 (4) R							134 48 (4) 7 49 C-3 01
1+60	C-2 26 2 22	139 96	40 31 CO 35	139 67	CO 14 9 60	139 46	7 25 F-2 21 133 29 C-3 96
1+50 (W) R							(W) 139 35 6 40 F-2 95
1+40 B.V.C.	C-2 40 2 15	139 75	40 07 CO 32	139 46	CO 01 9 26	139 25	6 38 F-2 87 133 13 C-3 25
1+15 (3) R							134 01 (3) 6 71 C-2 70
1+09	C-1 74 1 20	139 46	9 69 CO 23	139 17	CO 03 8 99	138 96	6 91 F-2 05 132 92 C-3 99
1+00 (W) L	C-1 79 1 16 139 37 (W)						
0+78	C-1 56 40 73	139 17	9 27 CO 10	138 89	FO 05 8 62	138 67	F-2 10 132 70 6 57 C-3 87
0+67 5 (W) R							(W) 139 59 6 53 F-3 06
0+47	C-1 79 40 68	138 89	9 01 CO 12	138 60	FO 07 8 32	138 39	6 81 F-1 58 132 48 C-4 33
0+40 (2) R							(2) 133 32 6 42 C-3 10
0+25 (W) R							(W) 138 19 5 23 F-2 96
0+16 B.K	C-2 06 40 66	138 60	8 83 CO 23	138 31	FO 30 7 80	138 10	4 33 F-3 77 132 26 C-2 07
0+10 (1) R							(1) 133 04 4 64 C-1 60
Cb E.C. 0+10	C-1 94 40 48	138 54	8 77 CO 23	138 26	FO 18 7 86	138 04	4 38 F-3 66
OCEAN VIEW Nly 0+00	CO 04 8 53	138 49	8 53 CO 04	138 20	FO 04 7 67	137 71	132 15 4 97 C-2 82
BM			138 16 ℄ Int Hub Gloria + Ocean View				

Rt = Ely

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	Lt = Wly				Rt = Ely		
	Rough 5' BK	Cb grade	Cb	℄	Cb	Cb grade	Rough 5' BK
4+50	C2^{56} 7^{93}	145^{37}	5^{36} F0^{01}	145^{12}	C0^{07} 5^{01}	144^{94}	5^{15} C0^{21}
4+30	C2^{13} 7^{33}	145^{20}	5^{41} C0^{21}	144^{93}	C0^{08} 4^{81}	144^{73}	5^{08} C0^{35}
4+10	C2^{07} 6^{97}	144^{90}	5^{37} C0^{47}	144^{62}	C0^{15} 4^{56}	144^{41}	4^{82} C0^{41}
4+00 (W) R							4^{73} C0^{51} 144^{22} (W)
3+90 B.V.C.	C2^{46} 6^{95}	144^{49}	5^{04} C0^{55}	144^{20}	C0^{17} 4^{16}	143^{99}	4^{08} C0^{09}
3+45	C2^{25} 5^{68}	143^{43}	3^{67} C0^{24}	143^{14}	C0^{48} 3^{41}	142^{93}	4^{30} C1^{37}
3+00 E.V.C.	C2^{02} 4^{40}	142^{38}	2^{68} C0^{30}	142^{09}	C0^{53} 2^{41}	141^{88}	2^{23} C0^{35}
2+80	C2^{32} 4^{25}	141^{93}	2^{13} C0^{20}	141^{64}	C0^{74} 2^{17}	141^{43}	2^{02} C0^{59}
2+60	C2^{15} 3^{66}	141^{51}	2^{02} C0^{51}	141^{22}	C0^{32} 1^{33}	141^{01}	40^{12} F0^{89}
2+50 (W) R							140^{83} (W) 9^{00} F1^{83}
2+40	C2^{10} 3^{23}	141^{13}	1^{59} C0^{46}	140^{84}	C0^{47} 1^{10}	140^{63}	7^{60} F3^{03}
2+20	C1^{9} 2^{7}	140^{78}	1^{11} C0^{33}	140^{49}	C0^{44} 0^{72}	140^{28}	7^{17} F3^{11}

144^{32} cbend Franklin Northside

	Rough 5'BK	Cb grade	Cb	℄	Cb	Cb grade	Rough 5'BK
Sly Franklin 6+05^{03}		144^{08}	4^{41} CO^{33}	143^{70}	$C1^{11}$ 5^{46}	144^{35}	
Cb Rad 5+95^{03} B.C.	$C2^{91}$ 7^{11}	144^{20}	3^{92} FO^{28} ~~4^{05} FO^{15}~~	143^{79}	CO^{48} 4^{88}	144^{40}	5^{18} CO^{78}
5+75 (W) L	$C3^{10}$ 7^{55} 144^{45}						
5+52^{5}	$C2^{73}$ 7^{43}	144^{70}	5^{14} CO^{44}	144^{64}	CO^{07} 4^{77}	144^{70}	4^{88} CO^{18}
5+25 (W) L	$C3^{35}$ 8^{38} 145^{03}						
5+10 E.V.C.	$C2^{67}$ 7^{87}	145^{20}	5^{51} CO^{31}	145^{06}	FO^{01} 4^{98}	144^{99}	4^{73} FO^{26}
4+90	$C2^{16}$ 7^{54}	145^{38}	5^{44} CO^{06}	145^{19}	FO^{24} 4^{83}	145^{07}	4^{94} FO^{14}
4+70	$C2^{01}$ 7^{45}	145^{44}	5^{35} FO^{09}	145^{21}	CO^{04} 5^{10}	145^{06}	5^{30} CO^{24}

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Stake Alley Blk 1 Ocean Front

Btwn Mission Blvd & Bayard, Missouri + Chalcedony

wo# 3-5-54

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1+40		47.29	46.99	6.92 FO.07			
1+45 @ Lt				6.87 41.94 C 4.93			
1+80		46.94	46.64				
2+20		46.59	46.29				
2+60		46.24	45.94				
					BM		53.10 NE BP Chalcedony + Bayard
3+00	.0087 rate	45.90	45.60				
						47.84	
3+40		45.55	45.25		Wly Bayard St 0+00	47.94	47.64
3+70 @ Lt				39.98			
3+80		45.20	44.90		0+20 EVC	48.08	47.78
4+20		CO 40 5.25 44.85	44.55		0+40	48.09	47.79
4+60		CO 32 44.50	44.20	3.95 FO.25	0+60 EVC	47.98	47.68 8.42 C-0.74
	Mission Blvd	44.03	43.77				
5+00	Ely	44.15	43.85		1+00	47.64	47.34
BM			40.49	NW 7 Lt Mission + Missouri			

D. Smith 3-10-54
J. Rorer Wo# 32070
B. Fish

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Stake Alley BK 37 Ocean Beach

Btwn Sunset Cliffs & Ebers, Coronado & Santa Cruz

Lt = Nly — Rt = Sly

2' BK unless noted

	Lt = Nly	Rt = Sly
1+80	CO 70 90 40 89 70	89 71 90 03 CO 32 (1' BK)
1+60	0.90 BK CO 71 7 95 87 24	87 24 7 57 CO 33
1+30	CO 42 3 68 83 26	83 25 3 12 FO 13
1+00 (1.95 changes alley width 18°)	0.94 BK Nly, 0.98 BK Ely CO 60 9 88 79 28	79 26 9 63 CO 37 (1.50 BK Nly, 0.72 BK Ely)
0+80	CZ 60 8 22 76 22	76 16 7 43 CI 27
6+60	CO 70 3 10 72 40	72 16 2 32 CO 16
0+55	FO 15 1 20 71 35	71 05 ~~70 74~~ 70 72 FO 31 (1=0 33)
0+27.5	CI 92 8 10 66 18	66 01 8 20 CZ 19
Ely Sunset Cliffs 0+00	61 01	60 97
BM		54 23 SE BP Santa Cruz & Sunset Cliffs

	Lt = Nly	Rt = Sly
4+20	FO 62 3 19 93 81	94 11 4 82 CO 71
3+80	FO 30 5 02 95 32	95 62 6 25 CO 63
3+40	CO 02 6 85 96 83	97 13 7 47 CO 34
3+20	Grade CO 11 7 48 ~~97 77~~ 97 48	97 89 8 56 CO 67
3+00	FO 40 ~~FO 15~~ 7 33 ~~97 48~~ 97 73	98 31 8 42 CO 11
2+80 on curve	Grade ~~CO 13~~ 7 28 ~~97 45~~ 97 28	98 07 8 12 CO 05
2+60	CO 43 6 83 96 40	97 17 7 25 CO 08
2+40	CO 99 6 19 95 20	95 60 5 66 CO 06
2+20	0.40 BK CI 72 5 30 93 58	93 81 4 24 CO 43
2+00	0.27 BK CI 56 3 30 91 74	91 80 1 63 FO 17

Note: use plan grade due to fact owner of W end

Storm Drain 12" R.C.P. Between Lots 30 + 31 Blk 37 Ocean Beach.

	Lt = Nly	Rt = Sly 2' BK unless noted	5' Ely
5+98.71 wly Ebers	101.58	101.78	
5+80	CO.03 1.31 101.28	101.48 1.89 CO.41	1+70 cb outlet "X's 10" E&W — 90.02 ✓ meet 88.98
5+60	CO.02 0.15 100.13	100.35 0.65 CO.30	1+50 Brk End pipe + Sly wall Box. — ~~89.08~~ 12 90.34 C-1.22
5+30	CO.58 8.36 97.78	98.02 8.20 CO.18 0.44 BK	1+20 Brk — ~~89.23~~ 90.88 ~~C-1.65~~
5+00 0.88 BK	CO.34 5.77 95.43	95.70 5.91 CO.21	0+90 C-1.65 1.33 89.68 — ~~90.17~~ 1.33 ~~C-1.16~~
4+80	CO.24 4.40 94.16	94.44 4.88 CO.44 1' BK	0+60 C-1.49 2.62 90.13 — ~~91.11~~ 2.62 ~~C-1.51~~ erroneous
4+60	CO.38 3.84 93.46	93.75 4.61 CO.86	0+30 C-2.56 3.14 90.58 — ~~92.05~~ 3.14 ~~C-1.09~~
4+40	6' BK FO.56 2.79 93.35	93.65 4.52 CO.87	0+00 ℄ type "D" catch basin stake 5' E&W 93.07 CO.08 C 2.04 ie — 92.99 grate wly 3.36 CO.37 91.03 ie 3.36 C 2.33 Ely 3.45 CO.46 grate C 2.42 ie

D. Smith
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B. Fish

Stake Harbor Dr
Sta. 332+50 N wly to 381+68 ℄

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JUN

		Rt staked 3' BK.
334+50		2^{16} 2^{03} FO^{13}
334+25		2^{15} 1^{97} FO^{18}
334+00		2^{15} 2^{05} FO^{10}
333+75		2^{14} 2^{01} FO^{13}
333+50		2^{14} 2^{00} FO^{14}
333+25		2^{13} 1^{98} FO^{15}
333+00		2^{13} 2^{00} FO^{13}
332+75		2^{12} 2^{01} FO^{11}
332+56 Begin dovetail cb		2^{12} 1^{86} FO^{26}
332+50 ℄ existing catch basin		
BM		1^{59} Ely Osbourn's Nail Laurel + Harbor.

State Hwy plans Roll Map #6159

WO #21162
3-16-54
Rt

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	Lt.	Rt
336+60	B.C. FO^{93} 1^{31} 2^{24}	2^{23} 1^{31} FO^{92}
336+50	FO^{93} 1^{29} 2^{22}	2^{21} 1^{29} FO^{92}
336+25	FO^{83} 1^{38} 2^{21}	2^{20} 1^{38} FO^{82}
336+00	FO^{86} 1^{34} 2^{20}	2^{19} 1^{34} FO^{85}
335+75	FO^{82} 1^{37} 2^{19}	2^{18} 1^{37} FO^{81}
335+50	FO^{58} 1^{61} 2^{19}	2^{18} 1^{61} FO^{57}
335+25	FO^{68} 1^{51} 2^{19}	2^{17} 1^{51} FO^{66}
335+00	FO^{32} 1^{87} 2^{19}	2^{17} 1^{87} FO^{30}
334+75	FO^{18} 2^{00} 2^{18}	2^{16} 2^{00} FO^{16}
334+68 ^{56} E.C.		2^{16} 2^{00} FO^{16}

337+86				
337+75		FO^{78} 1^{73} 2^{51}	2^{45} 1^{63} FO^{82}	
337+50		FO^{62} 1^{86} 2^{48}	2^{44} 1^{61} FO^{83}	
337+25		FO^{63} 1^{77} 2^{40}	2^{38} 1^{45} FO^{93}	
337+10		E.C. FO^{53} 1^{83} 2^{36}	2^{34} 1^{39} FO^{95}	
337+00			2^{31} 1^{42} FO^{89}	FO^{46} 2^{21} 2^{67}
336+97^{50}	L	FO^{44} 1^{89} 2^{33}		338+46 6' Mod 17 FO^{53} 2^{19} 2^{72} 2^{62} 2^{11} FO^{51}
336+85	P.R.C.	FO^{48} 1^{82} 2^{30}		338+16 FO^{86} 1^{79} 2^{65} 2^{52} 1^{82} FO^{70}
336+75			2^{26} 1^{72} FO^{54}	338+00 2^{54} 2^{47} 1^{72} FO^{75}
336+72^{50}		FO^{79} 1^{45} 2^{24}		337+92^{82} B.C. FO^{79} 1^{74} 2^{53} 2^{46} 1^{63} FO^{83}

Rt Outside Cb near Laurel St

Note used 50 cb face

	CON pav. edge	CON pav edge	10' AC	gut grade	Stake 3' Bk Rt
337+27 end	1 80	1 56	1 48	1 43	2 20 GO 27
337+02				1 41	1 39 FO 52
336+77	1 74	1 48	1 40	1 40	1 34 FO 56
336+52				1 39	1 24 FO 65
336+27	1 62	1 41	1 37	1 38	1 25 FO 63
336+02				1 37	1 24 FO 63
335+77	1 64	1 40	1 47	1 36	1 28 FO 58
335+52				1 35	1 25 FO 60
335+27	1 65	1 61	1 43	1 33	1 21 FO 62

7 ¢' outside gut Pt. Lt

342+00	8°19.00	2 ~~69~~ 72 FO ~~48~~ 45	3 17	
341+75	7°48.304	2 ~~67~~ 70 FO ~~49~~ 44	3 14	
341+50	7°18.614	2 ~~67~~ 71 FO ~~44~~ 40	3 11	
341+25	6°47.921	2 ~~62~~ 69 FO ~~46~~ 39	3 08	
341+00	6°17.228	2 ~~59~~ 65 FO ~~46~~ 40	3 05	
340+75	5°46.535	2 ~~62~~ 61 FO ~~40~~ 41	3 02	
340+50	5°15.842	2 ~~57~~ 60 FO ~~42~~ 39	2 99	
340+16	4°34.100	2 ~~56~~ 59 FO ~~37~~ 34	2 93	
339+86	3°57.169	2 ~~50~~ 53 FO ~~38~~ 35	2 88	
339+56	6' Rad 3°20.336	2 44 FO 39	2 83	
337+92	82 BC 0°00'			

Rt 7' ~~5'~~ outside gut pt.

2 96 BC	2 ~~39~~ 43	FO ~~57~~ 53	
2 93	2 37	FO 56	
2 90 BC	2 ~~36~~ 38	FO ~~54~~ 52	
2 87	2 ~~33~~ 35	FO ~~54~~ 52	
2 84	2 ~~33~~ 34	FO ~~51~~ 50	
2 81	2 ~~27~~ 29	FO ~~54~~ 52	
2 78	2 ~~27~~ 28	FO ~~51~~ 50	
2 74 EC	2 ~~20~~ 23	FO ~~44~~ 41 51	←
2 70 BC	2 ~~20~~ 21	FO ~~50~~ 49	8' out
	FO 40		
	2 33 ON 6' Rad Pt.		
	2 73		
2 62	2 22	FO 40	

345+00	ES 14°28.25'	8' off Road Pt. 2 88 49 F0 54 3 42				
344+80	14°03.76	7' off Road Pt. 2 93 97 F0 50 46 3 43	11' off Pt out Pt. 341 F0 49 44			
344+50	13°25.930'	2 94 98 F0 51 47 3 45	Centerline 9' off Pt out Pt. 343 F0 49 45			
344+25	12°55.237'	2 90 96 F0 54 48 3 44				
344+00	12°24.544	2 90 97 F0 53 46 3 43				
343+75	11°53.851	2 89 93 F0 50 46 3 39				
343+50	11°23.158	2 86 92 F0 49 43 3 35				
343+25	10°52.465	2 88 87 F0 50 45 3 32				
343+00	10°21.772	2 74 83 F0 55 46 3 29				
342+75	9°51.079	2 75 81 F0 51 45 3 26				
342+50	9°20.386	2 75 80 F0 48 43 3 23	10' out 2 31 46 3 06 cbend F0 45 60			
342+25	8°49.693	2 74 77 F0 46 43 3 20	7' out 2 38 45 3 01 F0 43 56			
348+00		2 88 F0 52 3 39			12' off 3 43 cbend 2 81 F0 61	
347+75		2 88 F0 52 3 40				
347+50		2 86 F0 54 3 40				
347+25		2 85 F0 55 3 40				
347+00		2 85 F0 55 3 40				
346+75		2 84 F0 56 3 40				
346+50		2 86 F0 54 3 40				
346+30		2 85 F0 55 3 40			9' off 3 40 2 85 F0 55	
346+10		7' out 2 85 F0 53 3 38			11' off out 3 38 2 85 F0 53	
345+90		2 86 F0 56 3 40			8' off Road Pt.	

			4 17' off 15' off Rt	11' off 4' c6 Rad Pt
				3 23 2 85 Fo 38
350+50	2 59 Fo 59 3 18	3 18 2 60 Fo 58	352+72 0°30.761' 2 50 Fo 68 3 18	3 27 2 85 7' off Fo 42
350+25	2 66 Fo 55 3 21	3 21 2 63 Fo 58	352+52 0°13.9792' 11 44 off Fo 61 2 53 3 14	3 24 2 79 Fo 45
			352+35 34 B.C. 0°00'	
350+00	2 68 Fo 57 3 25	3 25 2 66 Fo 59	352+32 2 54 8 11 off Fo 59 3 13	3 22 2 75 Fo 47
349+75	2 70 Fo 57 3 27	3 27 2 68 Fo 59	352+12 2 53 Fo 59 B.C. 3 12	3 19 2 70 Fo 49
349+50	2 76 Fo 54 3 30	3 30 2 76 Fo 54	352+00 2 54 Fo 58 3 12	3 18 2 66 Fo 52
349+25	2 76 Fo 56 3 32	3 32 2 76 Fo 56	351+75 2 50 Fo 62 3 12	3 18 2 60 Fo 58
349+00	2 80 Fo 54 3 34	3 34 2 79 Fo 55	351+50 2 49 Fo 63 3 12	3 18 2 57 Fo 61
348+75	2 83 Fo 53 3 36	3 36 2 81 Fo 55	351+25 2 51 Fo 61 3 12	3 17 2 55 Fo 62
348+50	2 83 Fo 54 3 37	3 37 E.C. 2 83 7' off Fo 54	351+00 2 54 Fo 59 3 13	3 16 2 55 Fo 61
348+25	2 84 Fo 54 3 38	3 40 2 84 8 25 off Fo 56	350+75 2 56 Fo 59 3 15	3 17 2 57 Fo 60

		7' offsets Lt.	7' offsets Rt
355+00	3°42.0732'	F0 59 2 83 3 52	3 69 3 24 F0 45
354+75	3°21.0960	F0 60 2 88 3 48	3 64 3 19 F0 45
354+50	3°00.1188'	F0 62 2 82 3 44	3 60 3 12 F0 48
354+25	2°39.1414	F0 61 2 78 3 39	3 55 3 06 F0 49
354+00	2°18.1644	F0 60 2 74 3 34	3 51 3 03 F0 48
353+92	2°11.4517	F0 61 2 72 3 33	3 50 3 03 PCC 7' off F0 48
353+72	1°54.6697	F0 62 2 67 3 29	3 45 2 99 7.55' off F0 46
353+62	1°46.2790'	F0 63 2 65 9' off P.R.C. 3 28	
353+52	1°37.8881		3 39 2 94 9.22' off F0 45
353+32	1°21.1063'	F0 63 2 61 12' off 3 30	3 36 2 91 12' off F0 45
			3 33 2 91 16' off Rad Pt F0 42

	Lt.	Rt
357+50	7°11.8452 F0 68 3 14 3 82	3 99 3 46 F0 53
357+25	6°50.8680 F0 69 3 10 3 79	3 95 3 42 F0 53
357+00	6°29.8908' F0 67 3 09 3 76	3 92 3 40 F0 52
356+75	6°08.9136' F0 70 3 04 3 74	3 89 3 38 F0 51
356+50	5°47.9364 F0 67 3 04 3 71	3 86 3 36 F0 50
356+25	5°26.9592' F0 65 3 02 3 67	3 83 3 32 F0 51
356+00	5°05.9820 F0 62 3 02 3 64	3 80 3 28 F0 52
355+75	4°45.0048 F0 62 2 98 3 60	3 77 3 27 F0 50
355+50	4°24.0276' F0 61 2 96 3 57	3 75 3 27 F0 48
355+25	4°03.0504 F0 62 2 92 3 54	3 72 3 27 F0 45

	Lt.	Rt.
		11' off Rad Pt (4') 4.05 3.52 F0.53
359+23	17' off F0.70 3.35 PCC. 4.05	7' off 4.05 3.52 BC. F0.53
358+93	9.50' off F0.63 3.35 3.98	4.07 3.58 F0.49 ←
358+76.02 F.C.	F0.66 3.36 8°57.5874 3.96	4.08 3.61 F0.47 ←
358+63 8°46.6622	7' off F0.59 3.35 PRC. 3.94	
358+50 8°35.7540	F0.64 3.29 3.93	4.09 3.58 F0.51
358+25 8°14.7768	F0.66 3.25 3.91	4.07 3.54 F0.53
358+00 7°53.7996	F0.67 3.21 3.88	4.04 3.51 F0.53
357+75 7°32.8224	F0.67 3.18 3.85	4.02 3.49 F0.53

	Lt	Rt
361+13		4.14 3.58 F0.56
361+00		4.13 3.58 F0.55
360+75		4.10 3.48 F0.62
360+63	cbend 13.50' off F0.57 3.48 4.05	
360+58		7' off 4.08 3.52 F0.56
360+38	8.63' off F0.59 3.43 3.98	
360+33		7.55' off 4.07 3.56 F0.51
360+13	7' off F0.57 3.46 4.03	
360+08		9.22' off 4.07 3.51 F0.56
359+83	12' off F0.62 3.46 4.08	12' off 4.08 3.50 F0.58
		4.08 16' off 4.06 Rad Pt. F0.58

	Lt	Rt
		8' off 1' cb Rad.
363+10		4 58 3 98 F0 60
362+90	21' off on 11' off → F0 66 3 93 4 59	7' off 4 58 3 93 F0 65
362+70		4 51 3 89 F0 62
362+60	23' off on 9' off cbend F0 72 3 87 4 59	4 48 3 87 F0 61
362+50		4 45 3 87 F0 58
362+25		4 44 3 85 F0 59
362+00		4 42 3 81 F0 61
361+75		4 35 3 76 F0 59
361+63		4 31 3 74 F0 57
361+38		4 23 3 67 F0 56

	Lt	Rt
365+50		4 90 4 30 F0 60
365+25		4 89 4 28 F0 61
365+00		4 87 4 25 F0 62
364+89	cbend 13' 50' off F0 68 4 20 4 88	
364+84		7' off 4 87 4 25 F0 62
364+64	8' 63' off F0 67 4 18 4 85	
364+59		7' 55' off 4 85 4 22 F0 63
364+39	7' off F0 68 4 07 4 75	
364+34		9' 22' off 4 79 4 18 F0 61
364+09	12' off F0 71 4 03 4 73	12' off 4 73 4 09 F0 64
		4 73 16' off 4' Rad 17. F0 64

	Lt	Rt
368+05	11' off → FO 5.57 5.32	7' off 5.30 4.75 FO 5.55
367+85	5.28	10' off 1' Radlt. 5.28 4.70 FO 5.58
		5.28
		5.12
366+94	5.12	8' off 1' Radlt. 5.12 4.53 FO 5.59
366+74	11' off → FO 6.62 5.12	7' off 5.09 4.50 FO 5.59
366+44	cbend. 9' off → FO 6.61 5.10	7' off 5.06 4.49 FO 5.57
366+25		5.04 4.44 FO 6.60
366+00		5.01 4.42 FO 5.59
365+75		4.96 4.41 FO 5.55

	Lt	Rt
370+50		5.70 5.14 FO 5.56
370+25		5.71 5.14 FO 6.60
370+00		5.71 5.13 FO 5.58
369+75		5.67 5.06 FO 6.61
369+50		5.64 5.04 FO 6.60
369+25		5.61 5.00 FO 6.61
369+00		5.48 4.92 FO 5.56
368+75		5.46 4.90 FO 5.56
368+50		5.44 4.87 FO 5.57
368+35	cbend. 9' off → FO 5.57 5.40	7' off 5.39 4.83 FO 5.56

	Lt	Rt
372+35	17.50 off 14.50 off F0.45 5.45 F0.54 5.90	5.84 5.36 F0.48
372+10		5.83 5.30 F0.53
371+85	10.50 off F0.49 5.40 5.89	
371+75		5.82 5.29 F0.53
371+60	7.88 off F0.50 5.36 5.86	
371+50	7' off F0.52 5.33 5.85	5.81 5.28 F0.53
371+35	7' off F0.54 5.28 5.82	
371+22.50	8.75 off F0.55 5.26 5.81	5.78 5.24 F0.54
371+10	cb end 14' off F0.56 5.22 5.78	
370+85		5.74 5.21 F0.53
370+75		5.73 5.18 F0.55

	Lt	Rt
374+85	11' off F0.52 6.27	6.26 7' off 5.76 F0.50
374+65		10' off 1' above pt. 6.22 5.69 F0.53
373+83	6.05	6.05 8' off 1' Rad pt. 6.05 5.59 F0.46
373+63	cb B.C. 11' off F0.47 6.05	6.04 7' off 5.58 F0.46
373+50	11' off F0.47 6.05	6.03 7' off 5.58 F0.45
373+25	11' off F0.47 5.98	6.01 5.51 F0.50
373+00	11' off F0.46 5.90	5.88 5.44 F0.44
372+85	cb E.R. 11' off F0.46 5.89	5.87 5.43 F0.44
372+60	11.88 off F0.48 5.88	5.85 5.40 F0.45

	Lt	Rt
377+25	11' off → F0 50 6 54	7' off 6 52 6 04 F0 48
377+00	11' off → F0 52 6 53	6 51 6 01 F0 50
376+75	11' off → F0 53 6 53	6 51 6 00 F0 51
376+50	11' off → F0 51 6 52	6 50 6 01 F0 49
376+25	11' off → F0 54 6 49	6 47 5 95 F0 52
376+00	11' off → F0 52 6 45	6 43 5 93 F0 50
375+75	11' off → F0 53 6 43	6 41 5 90 F0 51
375+50	11' off → F0 57 6 40	6 38 5 83 F0 55
375+25	11' off → F0 54 6 36	6 34 5 80 F0 54
375+00	11' off → F0 58 6 33	7' off 6 31 5 70 F0 54

	Lt	Rt
379+25	7' off F0 50 5 89 6 39	6 39 5 89 F0 50 7' off
379+00	F0 50 5 92 6 42	6 42 5 92 F0 50
378+75	F0 48 5 98 6 46	6 46 5 95 F0 51
378+50	F0 49 6 01 6 50	6 50 6 00 F0 50
378+15	7' off F0 51 6 00 6 51	6 51 6 02 F0 49 7' off
378+02 50	8.75' off F0 50 6 01 6 51	6 51 6 03 F0 48 7' off
377+90	14' off F0 50 6 01 6 51	
377+77 50	19.25' off 6 09 F0 52 11' off → 12.25' off F0 48 6 52	6 52 6 04 F0 48 7' off
377+65	11' off → F0 48 6 52	6 52 6 04 F0 48 7' off
377+50	F0 50 6 54	6 52 6 04 F0 48

	Lt.	Rt
		13' off 6' cb Rad. Pt. 6^{02} 5^{53} FO^{49}
end Project		
381+62	13' off FO^{49} 5^{55} 6^{04}	6^{00} 5^{53} 7' off BC FO^{47}
381+32	8.50 off FO^{48} 5^{59} 6^{07}	6^{07} 5^{58} 7' off FO^{49}
381+02	7' off FO^{51} 5^{61} 6^{12}	6^{12} 5^{62} 7' off FO^{50}
380+75	FO^{52} 5^{64} 6^{16}	6^{16} 5^{68} FO^{48}
380+50	FO^{52} 6^{20}	6^{20} 5^{68} FO^{52}
380+25	FO^{50} 5^{73} 6^{23}	6^{23} 5^{75} FO^{48}
380+00	FO^{51} 5^{76} 6^{27}	6^{27} 5^{78} FO^{49}
379+75	FO^{51} 5^{80} 6^{31}	6^{31} 5^{80} FO^{51}
379+50	7' off FO^{51} 5^{84} 6^{35}	6^{35} 5^{85} 7' off FO^{50}

Cb Near Coast Guard
3' BK

342+00	3^{62} 2^{85} FO^{77}
+75	3^{59} 2^{98} FO^{61}
+50	3^{56} 2^{93} FO^{63}
+25	3^{53} 2^{87} FO^{66}
341+00	3^{50} 2^{98} FO^{52}
+75	3^{47} 2^{78} FO^{69}
+50	3^{44} 2^{69} FO^{75}
340+25	3^{41} 2^{64} FO^{77}
340+04 BC	3^{38} 2^{63} FO^{75}
1/3	3^{21} 2^{67} FO^{54}
2/3	3^{04} 2^{56} FO^{48}
EC	2^{85} 2^{45} FO^{40}
End. Prop	2^{34} 1^{94} FO^{40}

+80	3^{63}	2^{93} $F0^{70}$
+50	3^{83}	2^{74} $F1^{09}$
+25	3^{89}	2^{66} $F1^{23}$
344+00	3^{89}	2^{67} $F1^{22}$
+75	3^{86}	2^{67} $F1^{19}$
+50	3^{83}	2^{66} $F1^{17}$
+25	3^{80}	2^{81} $F0^{99}$
343+00	3^{76}	2^{87} $F0^{89}$
+75	3^{73}	2^{91} $F0^{82}$
+50	3^{70}	2^{87} $F0^{83}$
342+25	3^{66}	2^{83} $F0^{83}$

Prop end,	3^{00}	2^{59} $F0^{41}$
EC	3^{30}	2^{47} $F0^{83}$
1/2	3^{40}	2^{79} $F0^{61}$
345+00 BC	3^{50}	2^{92} $F0^{58}$
345+00 EC	3^{56}	2^{95} $F0^{61}$

INDEXED Stake Cbs Armstrong St Sly of Baltic wly cb only for School. staked 3' BK

1+00		359^{56}	60^{14} CO^{58}
0+80		359^{75}	60^{42} CO^{67}
0+60		359^{83}	60^{31}_{17} CO^{48}
0+40		359^{88}	60^{03} CO^{15}
0+20		359^{87}	9^{79} FO^{08}
0+12^{83} cb E.C.		359^{84}	9^{68} FO^{16}
0+00		359^{80}	
0-04 P.R.C. type G cb end		359^{78}	9^{45} FO^{33}
0-08 E.C.		559^{85}	9^{45} FO^{40}
Prop end cb 0-08.		360^{01}	9^{06} FO^{95}
Prop end cb 0-23		360^{00}	8^{02} FI^{98}
E.C.		359^{73}	9^{69} FO^{04}
BM		359^{67}	Chisel (X) on wly cb top Alley Nly & wly Armstrong.

2+88^{63}		357^{48} 7^{87} ~~CO^{39}~~ CO^{59}
E.C. 2+58^{63}	357^{65}	357^{85} 8^{34}_{11} ~~CO^{49}~~ CO^{69}
4' Rad		
B.C.	357^{69}	357^{87} 8^{36}_{31} ~~CO^{49}~~ CO^{67}
E.C.	357^{91}	357^{94} 8^{71}_{6} ~~CO^{77}~~ CO^{80}
10' Rad		
Mid Pt.	357^{94}	357^{92} 8^{64} ~~CO^{72}~~ CO^{70}
2+32^{83} B.C.		357^{97} 8^{62} CO^{65}
2+10		358^{25} 8^{92} CO^{67}
1+80		358^{62} 9^{22} CO^{60}
1+50		358^{99} 9^{29} CO^{30}
1+20 E.V.C.		359^{36} 9^{79} CO^{63}

FB 2228-34

E.C.	354^{80}	4^{73}	$F0^{07}$
4/5	354^{82}	4^{78}	$F0^{04}$
3/5	354^{88}	5^{00}	$C0^{12}$
2/5	354^{93}	4^{70}	$F0^{23}$
1/5	355^{00}	5^{08}	$C0^{08}$
P.C.C. 4+62	355^{10}	5^{07}	$F0^{03}$
Mid Pt. 10' Rad	353^{16} 355^{21}	5^{22}	~~$C0^{01}$~~ $C0^{06}$
P.R.C.	355^{23} ~~355^{23}~~	5^{15}	~~$F0^{18}$~~ $F0^{08}$
Mid Pt. 10' Rad.	355^{29} 355^{44}	5^{42}	~~$F0^{02}$~~ $C0^{13}$
4+42 B.C.	353^{35} → 355^{55}	5^{45}	~~$F0^{10}$~~ $C0^{10}$
4+08 ^{63}	356^{00}	5^{82}	$F0^{18}$ $C0^{02}$
3+78 ^{63}	356^{37}	5^{89}	~~$F0^{48}$~~ $F0^{28}$
3+48 ^{63}	356^{74}	6^{57}	$F0^{17}$ $C0^{03}$
3+18 ^{63}	357^{11}	7^{13}	$G0^{02}$ $C0^{22}$

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Lt. Wly. Stake Poinsettia & Curtis St. Rt. Ely WO # 31817 4/13/54

INDEXED

		2' BK grading Rough	Cb grade	Cb		Cb	Cb grade	2' BK grading Rough
1+80.09	2°23.640	Fo 43 7 56	147 99	8 06 Co 07		8 62 Fo 07	148 69	9 34 Co 65
1+60.09	BVC, 2°07.154	Fo 48 7 90	148 38	8 41 Co 03		8 98 Fo 14	149 12	9 20 Co 08
1+50	1°59.14	Fo 37 8 19	148 56	8 49 Fo 07		9 26 Co 02	149 24	9 50 Co 26
1+25	1°39.18	Fo 35 8 73	149 08	8 87 Fo 21		9 63 Fo 11	149 74	0 02 Co 28
1+00	1°19.40 .0208	Co 28 9 88	149 60	9 56 Fo 04		0 14 Fo 10	150 24	1 10 Co 86
0+75	0°59.66	Co 74 0 86	150 12	0 22 Co 10		Fo 11 0 63	150 74	1 29 Co 55
0+50	0°39.72	Co 80 1 44	150 64	0 66 Co 02		1 36 Co 12	151 24	1 92 Co 68
0+30.39	PCC, 0°24.08' Wly Prop	2' BK grading Co 50 1 55	151 05	1 04 Fo 01		1 77 Co 03	151 74	2 58 Co 84
0+26.29	cb PCC		151 12	0 95 Fo 17				
0+00	PRC, Ely Prop 0°00'					2 35 Co 01	152 34	3 37 Cl 03
			151 43	1 09 Fo 34	0-07 38 PRC cb	2 54 Co 03	152 51	
			1 74			2 74 Fo 06	152 80	
			1 74				153 11	

	0° 00' ↗ 5° 34.75 ↘	Rough	cb grade	cs	Lt = Wly	Rt = Ely	cs	cb grade	Rough 6' Bt grading
4+21.44	E.P.C.C.	CO^{01} 5^{79}	145^{78}	6^{00} CO^{22}			CO^{14} 7^{02}	146^{88}	8^{05} $C1^{17}$
4+00	5°17.71	CO^{4} 6^{3}	145^{94}	6^{33} CO^{39}			CO^{04} 7^{04}	147^{00}	9^{0} $C2^{0}$
3+75	4°57.89	CO^{40} 6^{54}	146^{14}	6^{39} CO^{25}			CO^{07} 7^{22}	147^{15}	9^{13} $C2^{0}$
3+50	4°38.00	FO^{14} 6^{20}	146^{34}	6^{58} CO^{24}			FO^{05} 7^{24}	147^{29}	9^{7} $C2^{4}$
3+25	4°18.15	FO^{22} 6^{32}	146^{54}	6^{70} CO^{16}	Δ = 11° 09' 30"		FO^{02} 7^{42}	147^{44}	9^{72} $C2^{28}$
	.008				ΣR = 2164			.0057	
					d = .79 4302				
3+00	3°58.30	CO^{01} 6^{75}	146^{74}	6^{87} CO^{13}			FO^{09} 7^{49}	147^{58}	9^{4} $C1^{8}$
2+75	3°38.42	CO^{05} 6^{99}	146^{94}	7^{21} CO^{27}			FO^{05} 7^{67}	147^{72}	0^{38} $C2^{66}$
2+50	3°18.575	FO^{55} 6^{59}	147^{14}	7^{26} CO^{12}			CO^{22} 8^{08}	147^{86}	9^{95} $C2^{09}$
2+40.09	3°10.698 E.V.C.	FO^{57} 6^{65}	147^{22}	7^{26} CO^{04}			8^{18} CO^{26}	147^{92}	0^{06} $C2^{14}$
2+20.09	2°54.812	FO^{42} 6^{99}	147^{41}	7^{48} CO^{07}			8^{11} CO^{02}	148^{09}	0^{25} $C2^{16}$
2+00.09	2°38.926	FO^{54} 7^{13}	147^{67}	7^{71} CO^{04}			8^{27} FO^{07}	148^{34}	8^{25} FO^{09} 2' Bt grading

					cb	cb grade	Rough 6' BK grading
℄ P.R.C. 0+00 0°00' 7°18'					FO^{14} 1^{46}	141^{60}	2^{12} CO^{52}
0-20^{26} 6°52' cb dist CS P.R.C.					FO^{31} 2^{19}	142^{50}	2^{83} CO^{33}
0-47^{93}					FO^{13} 3^{37}	143^{50}	4^{00} CO^{50}
27^{67}							
0-75^{60} cb dist						144^{50} meet	✓ 4^{58}
						146^{69} meet	
5+43^{02} Ely cb P.R.C.					6^{61} CO^{22}	146^{39}	
5+35^{97} Bop P.R.C. Ely					6^{66} CO^{52}	146^{14}	
				$\Delta = 14°36'$ $\Sigma R = 1330.47$ $d_1 = 1.2928$			
5+25 2°13.79'					FO^{11} 6^{14}	146^{25}	8^{33} $C2^{08}$
5+00 1°41.48'					CO^{15} 6^{55}	146^{40}	8^{36} $C1^{96}$
4+75 1°09.20'					CO^{12} 6^{67}	146^{55}	8^{49} $C1^{94}$
Meet →		145^{49}					
4+50 0°36.90'	FO^{5} 5^{1}	145^{54}	5^{61} CO^{07}		FO^{05} 6^{65}	146^{70}	8^{61} $C1^{88}$

Curtis St

Lt = Nly

0+80 meet 128 94

0+50 Fo 45 5 43 125 88

0+25 Fo 66 2 68 123 34

Nly Line of P.
0+00 Point Loma Villas Co 35 1 05 120 80

Curtis St

1°58.815'
0+87 97 26 meet

0+75 9°41.215'

0+50 1°07.510'

0+25 0°33.755'

139 92 meet

Fo 12 9 88 140 00 1 35 Co 75

Fo 08 0 22 140 30 0 27 Co 47

Fo 14 0 28 140 92 1 05 Co 13

Staked Sewer Del Rey St

D. Smith
J. Rorer
R. Taylor
B. Fish

Staked 5' Ely

INDEXED
MER
JAN 18 1965

2+90		13.18	20.67 C-7.49	5+95 (2)	
2+85 (8)			14.93 22.45 C-7.52	5+90	15.05
2+60	.567%	13.01	20.31 C-7.30	5+60	15.30
				5+45 (3)	1.222%
2+30		12.84	20.04 C-7.20	5+30	14.93
2+10 (9)			14.55 21.45 C-6.90		
2+00		12.67	19.97 C-7.30	5+00	14.57
				4+95 (4)	
1+70 S.M.H.		12.50	20.25 C-7.75 7.07 dia 14.14	4+70 SMH #1	14.20
1+36		11.14	18.93 C-7.79	4+40	14.03
				4+20 (5)	
1+02		9.78	17.76 C-7.98	4+10	13.86
0+68		8.43	16.74 C-8.31	3+80	13.69
				3+70 (6)	
0+34		7.07	15.91 C-8.84	3+50	13.52
0+00 Meet existing S.M.H.	6" stub.	1e 5.72 meq 5.90		3+20 (7)	13.35
BM			17.89 N wly Prop Mon Rosewood & Del Rey		

Staked 5' Ely

17.57 24.32 32.16 C-6.75 5/6/54

22.77 C-7.11

22.40 C-7.10

16.97 24.02 C-7.05

21.99 C-7.06

21.57 C-7.00

16.36 23.42 C-7.06

21.00 C-6.80 5' Ely & 10' Ely

20.89 C-6.86

15.61 22.28 C-6.67

20.84 C-6.98

20.79 C-7.10

15.36 22.16 C-6.80

21.11 C-7.59

21.07 C-7.72 15.11 22.45 C-7.34

6" Water Line
Staked 5' Ely

2+80	17^{69}	1^{52} C 3^{88}
2+40	17^{27}	1^{27} C 4^{00}
2+00	17^{00}	0^{90} C-3^{90}
1+60	16^{80}	1^{13} C 4^{33}
1+20	16^{60}	1^{31} C 4^{71}
0+80	16^{40}	20^{72} C 4^{32}
0+40	16^{20}	20^{53} C 4^{33}
0+00	16^{00}	✓
6+50 Plug	16^{40}	23^{49} C 7^{09}
6+45 ①		18^{18} 25^{33} C 7^{15}
6+20	16^{03}	23^{11} C-7^{08}
	16^{03}	

5' BK of face

W 0+20	18^{85}	9^{87} C-1^{02}
E 0+30	19^{61}	0^{72} C 1^{11}
W 0+55	19^{04}	9^{67} C 0^{63}
E 1+35	20^{16}	1^{65} C 1^{49}
E 1+85	20^{44}	1^{11} C 0^{67}
W 2+63	20^{29}	0^{31} C 0^{02}
W 3+85	21^{70}	1^{50} F 0^{20}
4+97	20^{20}	4^{52} C-4^{32}
4+80	19^{99}	4^{27} C-4^{28}
4+40	19^{53}	3^{63} C 4^{10}
4+00	19^{07}	3^{31} C 4^{24}
3+60	18^{61}	2^{78} C-4^{17}
3+20	18^{15}	2^{34} C 4^{19}

E 4+10	22^{68}	4^{20} C 1^{52}
W 4+35	22^{28}	2^{06} F 0^{22}
W 4+85	22^{74}	2^{62} F 0^{12}
E 5' BK E Hyd. 4+92	23^{67}	4^{98} C 1^{31}

Stake Del Rey

		Lt = Wly Rough	Cb	Cb	Rt = Ely	Rough
2+20		19.92	20.44 Co.52	20.61 Fo.01	20.62	
2+00 BVC	19.57 Fo.23	19.80	20.13 Co.32	20.29 Fo.21	20.50	22.22 Cl.72
1+90	19.79 Co.03	19.76	20.08 Co.32	20.22 Fo.24	20.46	22.20 Cl.74
1+60	20.18 Co.58	19.60	9.55 Fo.05	20.20 Fo.10	20.30	22.19 Cl.89
1+30	19.80 Co.36	19.44	9.93 Co.49	20.09 Fo.05	20.14	22.46 Cl.32
1+00	19.34 Co.06	19.28	9.86 Co.58	20.08 Co.10	19.98	22.43 Cl.45
0+70	18.95 Fo.17	19.12	9.76 Co.64	9.67 Fo.15	19.82	22.1 Cl.3
0+40	18.96 G	18.96	9.68 Co.72	9.89 Co.23	19.66	21.67 Cl.01
0+10 Cb BC	18.88 Co.08	18.80	20.15 Cl.35	20.66 Cl.16	19.50	21.34 Cl.84
Nly Rosewood 0+00		18.70	9.93 Cl.23	20.74 Cl.19	19.55	
BM				17.89		NW Cor Rosewood & Del Rey Prop. Mon.

Glendora 5+00 Sly	Lt = Wly Rough	23.05	Cb 3.29 Co.24	Rt = Ely Cb 4.94 Cl.19	23.75	Rough
4+97 BC	22.74 Fo.26	23.00	3.26 Co.26	4.84 Cl.14	23.70	25.21 Cl.20
4+60	22.34 Fo.23	22.57	2.88 Co.31	3.64 Co.37	23.27	25.40 Cl.1
4+30	21.86 Fo.36	22.22	2.59 Co.37	3.21 Co.29	22.92	24.43 Cl.51
4+00	21.45 Fo.42	21.87	2.26 Co.39	2.71 Co.14	22.57	24.2 Cl.6
3+70	20.93 Fo.60	21.53	1.91 Co.38	2.26 Co.03	22.23	24.18 Cl.95
3+40	20.77 Fo.41	21.18	1.70 Co.52	2.04 Co.16	21.88	23.29 Cl.41
3+10	20.48 Fo.36	20.84	21.39 Co.55	1.66 Co.12	21.54	23.50 Cl.96
2+80 FVC	20.21 Fo.28	20.49	21.03 Co.54	1.34 Co.15	21.19	22.79 Cl.60
2+60		20.26	20.84 Co.58	1.12 Co.16	20.96	
2+40	19.40 Fo.67	20.07	20.78 ~~Co.61~~ Co.71	20.91 Co.14	20.77	22.37 Cl.60

WO # 20824
6-16-54

	Stake	Storm Drain 48" stake 5' Nly	Jamacha Rd & Glencoe		
2+58 76	25 65 C4 41 321 24		5+05'		316 83 21 82 C4 99 stake 5' Sly
2+28 76	26 17 C4 30 321 87		4+70		317 30 22 80 C4 70
1+98 76	27 14 C4 64 322 50		4+36 81 EC		317 74 22 95 C5 21
1+68 76	27 41 C4 28 323 13		4+25 14		317 90 22 97 C5 07
1+38 76	28 36 C4 60 323 76		4+13 46 BC Lt	24 76 C6 11	318 05 23 18 C5 13
1+08 76	28 83 C4 44 324 39		4+03 ℄ Cleanout	24 38 C6 21	318 17 stake 5' Nly
0+78 76	29 47 C4 45 325 02		3+78 76	24 82 C5 84	318 68
0+48 76 2.5° Lt	29 39 C3 75 325 64		3+48 76	24 80 C5 48	319 31
0+24 38	29 46 C3 33 326 13		3+18 76	24 91 C4 97	319 94
0+00 1.5° Rt	326 63		2+88 76	25 48 C4 91	320 57

INDEXED
MER
JAN 18 1955

Stake 5' Sly

8+55	312^{13}	17^{77} C 5^{64}
8+20	312^{60}	17^{97} C 5^{37}
7+85	313^{07}	17^{90} C 4^{83}
7+50	313^{54}	19^{49} C 5^{95}
7+15	314^{01}	19^{81} C 5^{80}
6+80	314^{48}	19^{80} C 5^{32}
6+45	314^{95}	20^{40} C 5^{45}
6+10	315^{42}	20^{99} C 5^{57}
5+75	315^{89}	21^{37} C 5^{48}
5+40	316^{36}	21^{71} C 5^{35}

Stake 5' Sly

11+52^{81} end	308^{13}	11^{86} C 3^{73}
11+35	308^{37}	14^{89} C 6^{52}
11+00	308^{84}	12^{26} C 3^{42}
10+65	309^{31}	12^{85} C 3^{54}
10+30	309^{78}	13^{51} C 3^{73}
9+95	310^{25}	14^{59} C 4^{34}
9+60	310^{72}	16^{24} C 5^{52}
9+25	311^{19}	16^{55} C 5^{36}
8+90	311^{66}	17^{03} C 5^{37}

WO# R0658
6/29/54

Stake Drain 48"
Talbot & Cannon St. stake 10' wly

INDEXED
JJ ER
JAN 18 1955

0+99 38		198 85 209 17 C 10 32	
0+63 38 Nly Prop talbot.		199 10 207 53 C 8 43	
Ely 213 24	C-1 21 Cb	C-2 04 gut	C-13 94 ie
25' wly 30' Ely 0+53 38 Nly Cb Line stk & inlet (212 66)	212 03 C0 63	211 20 C1 46	199 30 C-13 36
0+52 22 E.C.			
0+37 56 B.C.			
0+29 16 grade Drk		199 90	212 19 C12 29
0+21 56 E.C.			
	Cb	gut	ie. out.
0+07 3 & inlet Cb stk. & pipe (212 47)	212 50 F0 03	211 67 C-0 80	202 50 C9 97
		207 30 ie in C-5 17	
0+00 sly inlet	207 30 ie	211 76 C.4 46	
BM		217 82 albion & Talbot & wall	

2+47 87	187 60 196 67 C-9 07
2+30 62 & cutoff wall E.V.C.	194 50 201 50 C7 00
2+26 62	195 75 202 52 C-6 77
2+22 62	196 30 203 52 C7 22
2+18 62 B.V.C. E.C.	196 50 204 48 C.7 98
2+02 Mid Pt.	197 23 205 71 C8 48
1+89 38 E.V.C. B.C.	197 95 206 51 C-8 56
1+79 38	198 20 206 74 C8 54
1+71 38 B.V.C.	198 35 206 83 C8 48
1+35 38	198 60 207 76 C9 16

		8' off		
3+85 48		173 35 177 36 C 4 01		
3+61 48 E.V.C.		173 60 178 66 C 5 06		
3+53 48		173 80 178 99 C 5 19		
3+45 48 B.V.C. E.C.		174 10 179 34 C 5 24		
3+29 86		174 80 180 64 C 5 84		
1/3				
3+14 24		175 50 186 74 C 11 24		
2+98 62 B.C.		176 20 187 77 C 11 57		
2+81 12 E.V.C.		177 10 189 21 C 12 11		
2+73 12		178 20 191 02 C 12 82		7' off
			4+09 48 End	173 10 176 88 C 3 78
2+65 12 8 cut off wall B.V.C.		180 70 191 98 C 11 28		

Sewer Camino Del Collado

INDEXED
JER
JAN 18 1955

2+40	39.82	44.13 C 4.31 (5 Lt. n L split)		
2+10	38.32	44.78 C 6.46	4+95.10 D.E. plug	54.35 C 8.18 (62.53)
			4+90 ③ 57.26 C 5.35 (62.61)	
1+80	36.82	43.93 C 7.11	4+66.15	52.47 C 7.92 (60.39)
1+50	35.32	43.73 C 8.41	4+36.15	50.52 C 8.07 (58.59)
			4+26 ② 53.14 C 5.27 (58.41)	
1+35 SMH	34.56	43.20 C 8.64 (707 14.14 tie dia)	4+06.15	48.57 C 8.16 (56.73)
1+20	34.41	43.29 C 8.88	3+76.15 SMH	46.62 54.52 C 7.90 (506 10.12 dia)
			3+72 ④ 49.52 C 5.75 (55.27)	
0+90	34.11	42.87 C 8.76	3+60	45.83 C 7.32 (53.15)
0+60	33.81	42.53 C 8.72	3+30	44.33 C 6.38 (50.71)
			3+20 ① 44.46 C 8.83 (53.29)	
0+30	33.51	42.31 C 8.80	3+00	42.82 5.57 (48.39)
0+00	33.21	42.01 C 8.80	2+70	41.32 C 4.59 (45.91)
BM		42.99 US C&G BM Sw cor La Jolla Shores & Collado		

INDEXED
JAN 18 1945

Stake Ely ½ 45th St Market St Sly for 623'

3' BK Ely unless noted

			4+60	149.68 0.10 CO.42	149.78 9.48 FO.30
2+20	154.70 4.56 FO.14	154.81 4.44 FO.37			
			4+40	149.87 0.09 CO.22	149.95 9.60 FO.35
2+00	155.12 5.01 FO.11	155.25 4.98 FO.27			
			4+20	150.11 0.37 CO.26	150.17 9.94 FO.23
1+80	155.50 5.44 FO.06	155.64 5.36 FO.28			
			4+00	150.40 0.55 CO.15	150.45 0.18 FO.27
1+60 BVC	155.89 5.76 FO.13	155.99 5.70 FO.29			
			3+80	150.75 0.81 CO.06	150.79 0.43 FO.36
1+20	156.60 6.41 FO.19	156.58 6.32 FO.26			
			3+60	151.15 1.12 FO.03	151.19 0.80 FO.32
0+80	157.32 7.13 FO.19	157.16 6.95 FO.21			
			3+40	151.60 1.52 FO.08	151.64 1.20 FO.44
0+50	157.86 7.84 FO.02				
0+40		157.75 7.60 FO.15	3+20 BVC	152.08 1.97 FO.11	152.14 1.64 FO.50
0+20	158.39 8.37 FO.02				
			2+80	153.12 3.14 CO.02	153.21 2.80 FO.41
0+00	158.75 8.88 CO.13 2' BK	158.33 8.27 FO.06			
0-10	158.93 exists meet	158.45 meet	2+40 EVC	154.16 4.16 Grade	154.28 3.92 FO.36
		158.85 NWBP 45th & Market			

		℄
6+13 end	150^{24} 9^{63} FO^{61}	150^{12} 9^{78} FO^{34}
5+80 ^{10}t	149^{91} 9^{83} FO^{08}	149^{77} 9^{52} FO^{25}
5+60	149^{67} 9^{83} CO^{16}	149^{60} 9^{30} FO^{30}
5+40	149^{56} 9^{79} CO^{23}	149^{53} 9^{19} FO^{34}
5+20	149^{47} 9^{88} CO^{41} $\frac{56}{150}$ ch face	149^{51} 9^{13} FO^{38}
5+04 ℄ 15" RCP 5 BK 10 BK & type H inlet	149^{46} ch 148^{80} grate 147^{00} ie 9^{96} CO^{50} $C1^{16}$ $C2^{96}$	9^{52} $C3^{02}$ 146^{50} ie outlet.
5+00	149^{45} 9^{84} CO^{39}	149^{50} 8^{99} FO^{51}
4+80	149^{53} 9^{88} CO^{35}	149^{67} 9^{24} FO^{43}

3' BK unless Noted

Stake Alley Blk 45
Normal Hts.
Btwn 39th & E Mtn View Adams & Edna Pl.

INDEXED
JAN 18 1956

	Lt-Sly	Rt-Nly
1+90	FO^{36} 4^{05} 374^{41}	374^{41} 4^{52} CO^{11}
1+60 Brk	FO^{42} 3^{58} 374^{00}	374^{00} 4^{08} CO^{08}
1+40 Brk	FO^{30} 3^{50} 373^{80}	373^{80} 3^{66} FO^{14}
1+10	FO^{03} 3^{43} 373^{46}	373^{51} 3^{27} FO^{24}
0+80 E.V.C. 2° BK	FO^{03} 3^{10} 373^{13}	373^{23} 3^{26} CO^{03}
0+60 1° BK	CO^{09} 2^{82} 372^{73}	372^{83} 3^{16} CO^{33}
0+40 1.06 BK	CO^{47} 2^{63} 372^{16}	372^{21} 2^{71} CO^{50}
0+20	CO^{07} 1^{67} 371^{60}	371^{60} 2^{19} CO^{59}
0+00 W/y 39th St	CO^{21} 1^{35} 371^{14}	371^{10} 1^{22} CO^{12}
BM		370^{87} SEBP Adams & 39th

	Lt-Sly	Rt-Nly
2+77.7	372^{45}	
2+71.91		372^{56}
2+60	0.77 BK C-0^{96} 4^{65} 373^{69}	373^{50} 4^{85} CI^{35}
2+40	FO^{01} 4^{67} 374^{68}	374^{63} 4^{95} CO^{32}
2+20 B.V.C.	CI^{67} 6^{50} 374^{83}	374^{83} 4^{87} CO^{04} 7° BK

D. Smith
J. Moree
R. Fish
D. Rissley

Stake Alley BK 176 Univ. Hts

Btwn Georgia & Florida, Polk & Lincoln.

Lt = Wly

Rt = Ely

5'BK pav
2.3 BK prior } Rt
unless stated

Lt 3'BK pav unless stated

1+50	C1 39 6 24 285 35	285 05 4 45 F0 60
1+20	C1 68 6 82 285 14	4'BK pav. 284 84 5 75 C0 91
1+10 SL ⊗	282 40 7 50 C5 10	
1+07 Shot encase R.		
0+90	C2 08 7 01 284 93	80 45 F4 18 284 63 80 98 F3 65
0+60	C2 69 7 41 284 72	80 47 F3 90 284 42 80 25 F4 17
0+54 Shot, encase		
0+40 end con encase ment Lt		
0+30	C1 82 6 33 284 51	80 43 F3 78 284 21 80 63 F3 58
0+00 Nly Lincoln	C1 04 5 34 284 30	284 00 81 19 F2 81
2805² top wall		
BM		Nail in tel Pole #411292 284 42 0-04 Start

WO # 318.53 47

Rt = Ely 8-30-54

3+30	3'BK 8'BK pav. C2 87 6 59 293 72	293 42 92 04 F1 38
2+90	C2 01 2 87 290 86	290 56 87 56 F3 00
2+5 DEVC.	end encase SL 4 5'BK pav. 4.2 BK prior C2 19 91 19 288 00	287 70 5 76 F1 94
2+40	C2 12 89 46 287 33	287 03 4 99 F2 04
2+30	C1 88 8 66 286 76	286 48 3 81 F2 67
2+23 Shot encase Lt		
2+20	C2 71 89 04 286 33	286 03 3 38 F2 65
2+10	C2 21 88 20 285 99	285 69 3 50 F2 19
2+00	6'BK pav. C3 28 89 03 285 75	285 45 4 62 F0 83
1+90 BVC.	6'BK C3 18 88 81 285 63	2.3 BK pav. 285 33 6 33 C1 00
1+60 Shot, ⊙	283 14 7 30 C4 16	
FB 2312-11		

	Lt = Wly	Rt = Ely		
5+00	F0 01 5 06 305 07	304 29 300 75 F3 54		
4+90	C0 29 4 95 304 66	304 05 300 31 F3 74		
4+80	C0 64 4 82 304 18	303 71 299 10 F4 61 7'8K pav.		
4+70	C1 24 4 87 303 63	303 25 298 74 F4 51		
4+60	C2 03 5 04 303 01	302 69 298 73 F3 96		
4+50 BVC.	C1 83 4 15 302 32	302 02 297 52 F4 50		
4+32 Lt end wall	304 55 top 301 05 pav 300 77 footing 4 36 New 4 40 F0 15 C3 35 C3 63	C3 56 4 40 300 84 pav	6+00 33 Sly Polk 308 22	305 20
4+10	299 45	299 15 297 64 F1 51	5+70 F0 28 7 00 307 28	304 94 4 93 F0 01 2'8K pav.
4+02 Lt Begin wall	302 38 top 298 88 pav 298 21 footing 3 38 C1 00 C4 50 C5 17	3 38 C4 71 298 67 pav	5+40 C0 15 6 50 306 35	304 69 3 41 F1 28
3+70	C0 19 6 77 296 58	296 28 5 10 F1 18	5+10 EVC. F0 54 4 87 305 41	4 18 F0 25 304 43 4 49 C0 06

D. Smith
J. Rarer
R. Taylor
B. Fish

Stake Sewer & Water Mains
Morningside & Winchester Sts.

INDEXED
MER
JAN 18 1955

Sewer Rachael
Winchester Sly

Staked 5' Ely

		sewer 5' Wly	wo# 21141 9-13-54 water 5' Ely	1+76 16 end plug	144 65 164 05 C-19 40
4	0+78 75 W&S end plug	218 53 200 675 C17 86	212 219 26 C-7 26	1+60	143 89 163 07 C-19 18
4	0+61 25 W		211 5 218 61 C-7 11	1+40	142 95 161 49 C-18 54
4	0+60	217 94 200 60 C17 34		1+20	142 01 159 72 C-17 71
4	0+43 75 W Brk		211 0 217 59 C6 59	1+00	141 07 159 25 C-18 18
4	0+40	217 19 200 52 C16 67		0+80	140 13 157 85 C-17 72
4	0+26 25 W .004 rate		211 6 216 68 C5 08	0+60 047 rate	139 19 155 37 C-16 18
4	0+20	216 01 200 44 C-15 57		0+40	138 25 152 59 C-14 34
4	0+08 75 make H_2O connection		212 2 215 89 C369 approx	0+20	137 31 149 73 C-12 42
3	0+00 SMH #1	214 78 200 36 C-14 42	~~[illegible]~~	0+00 existing SMH	136 37
	BM		213 68 N.W.B.P. Winchester & Morningside	BM	147 04 N.E.B.P. Rachel & Winchester

D. Smith
J. Rover
R. Taylor
B. Fish.

INDEXED
JUN 7 1954

Stake Alley BLK 83 Wo# 31800 10/14/54

Lt = Sly Pt Loma Hts Rt = Nly

1+80	38 BK	CO^{73} 51^{85} 251^{12}	251^{12} 51^{32} CO^{20}
1+60		CO^{04} 51^{80} 251^{76}	251^{76} 52^{40} CO^{64}
1+40	4' BK	CO^{20} 52^{32} 252^{12}	252^{12} 53^{68} $C1^{56}$ 1.15 BK
1+20		CO^{11} 52^{31} 252^{20}	252^{20} 52^{94} CO^{74}
1+00		CO^{26} 52^{26} 252^{00}	252^{00} 53^{10} $C1^{10}$
0+80		CO^{29} 51^{83} 251^{54}	251^{54} 52^{94} $C1^{40}$
0+60		CO^{93} 51^{72} 250^{79}	250^{79} 52^{66} $C1^{87}$
0+40		CO^{20} 49^{97} 249^{77}	249^{77} 52^{37} $C2^{60}$
0+20		$C1^{20}$ 49^{52} 248^{32}	248^{48} 50^{98} $C2^{50}$
0+00	Wly Prop Santa Barbara	✓ 246^{40} 246^{26} plan	Notes 246^{98} ✓ 246^{91}
BM			240^{17} SW B.P. Coronado Santa Barbara

Lt = Sly Rt = Nly

staked 3' BK pav. edge unless noted

4+60	1.50 BK	CO^{85} 35^{99} 235^{14}	235^{14} 35^{07} FO^{07}
4+40 BVC		$C1^{06}$ 37^{48} 236^{42}	236^{42} 36^{23} FO^{19}
4+07.5		CO^{38} 38^{77} 238^{39}	238^{39} 38^{22} FO^{17}
3+75	4' BK	CO^{40} 40^{76} 240^{36}	240^{36} 41^{27} CO^{91}
3+42.5		CO^{03} 42^{36} 242^{33}	242^{33} 43^{26} CO^{93}
3+10 EVC		CO^{30} 44^{59} 244^{29}	244^{29} 44^{65} CO^{36}
2+90		CO^{80} 46^{26} 245^{46}	245^{46} 46^{36} CO^{90}
2+70 BVC		CO^{10} 46^{65} 246^{55}	246^{55} 47^{16} CO^{61}
2+35		CO^{51} 48^{89} 248^{38}	248^{38} 48^{78} CO^{40}
2+00 EVC		CO^{48} 50^{69} 250^{21}	250^{21} 51^{20} CO^{99}

	Lt = Sly	Rt = Nly
	staked 3' BK pav. unless otherwise specified	
	✓ 223^{31} (Notes)	222^{54} ✓
$5+99^{95}$ Ely / ~~6+00~~ Guizot St	223^{35} (Plan)	222^{58}
		2^{06} BK
5+80	C-3^{67} 28^{80} 225^{13}	224^{93} 26^{81} C-1^{88}
5+60 B.V.C.	C-3^{16} 30^{06} 226^{90}	226^{90} 27^{41} C-0^{51}
5+20 E.V.C.	C-1^{50} 31^{95} 230^{45}	230^{45} 32^{28} C-1^{83}
		0^{25} BK
5+00	C-0^{60} 32^{75} 232^{15}	232^{15} 33^{47} C-1^{32}
4+80	C-0^{90} 34^{62} 233^{72}	233^{72} 34^{01} C-0^{29}

D. Smith
J. Rorer
R Taylor
B Pisk

Stake Storm Drain
Bellevue Ave & Nly Line
Bird Rock Add

Staked 5' Lt on Nly

WO#2/255
10/19/54

INDEXED
JAN 18 1955

0+52.68		156.77	58.60 C1.83	
0+26.70	E.V.C.	155.73	57.97 C2.24	
0+22.90		155.24	58.07 C-2.83	
0+19.16	B.V.C.	154.42	57.82 C3.40	
0+03.64	E.V.C.	149.67	53.89 C4.22	
0-00.27		148.82	52.26 C3.44	
0-04.24		148.31	50.74 C2.43	
0-08.24	B.V.C. Headwall	148.15	Lt 9.43 C1.28 / Rt 50.93 C2.78	
BM			148.40 top Fire Hyd Bellevue, Sub Line pg 3 FB 2326	

1+20.40	Headwall E.C.	172.78	77.54 C-4.76
1+14.51	Mid Pt. Δ=30° R=22.50 L=11.78 T=6.03	170.35	76.51 C6.16
1+08.62	B.C. Rt	167.91	174.80 C6.89
0+90.36	E.V.C.	160.36	70.82 C10.46
0+86.54		159.17	70.03 C10.86
0+82.63	℄ Cutoff wall	158.32	68.97 C10.65 (5' Rt)
0+78.66	B.V.C.	157.81	8' Lt 58.93 C1.12 / 5' Rt 68.88 C11.07

Stake Alley Blk 30 Park Villas

D. Smith
J. Rorer
R Taylor
D. Black

plan #1165-L

WO #32407
2/7/55

Btwn Upas & Myrtle Grim & 31st St

	Lt-Wly		Rt-Ely	
2+40	FO 11 30 34	330 45	330 75	30 67 FO 08
2+20 BVC	FO 04 30 16	330 20	330 50	30 54 4' BK CO 04
2+00	FO 23 9 64	329 87	330 12	30 21 CO 09
1+60	CO 02 9 22	329 20	329 39	30 23 CO 84
1+20 .016 grade	4' BK CO 01 8 53	328 52	328 65 .0183 grade	9 36 CO 21
0+80	FO 55 7 29	327 84	327 92	8 11 CO 19
0+40 Full 35/100 & valley here & Bk	1' BK CO 28 7 44	327 16	326 83 327 19	1' BK 7 27 CO 08
0+20 (Bk Lt-wly)	1' BK CO 42 7 24	326 82	326 83	1' BK 7 00 CO 17
0+00 Nly Upas	Meet	326 63	326 46	Meet
BM			328 99	NW BP 31st & Upas

Staked 3' Bk pav. edge unless noted

3+00 Myrtle 21 Sly	Meet	326 84	326 99	Meet
2+80 Full 35/100 & valley here & Bk	CO 77 30 12	329 35	329 15 329 65	2' BK 31 12 CO 47
2+60	CO 25 30 45	330 20	330 50	1' BK 31 35 CO 85

Stake Muirlands Ely Sewer Outfall

WO# 21234
2/17/55

BM		Chisel ☐ top headwall 178.43	Staked 5' Lt
2+01.75	176.91	86.19	C 9.28
1+71.75 SMH #2	175.61	84.67	C 9.06 5' Lt
1+55	175.54	84.06	C 8.52
1+30	175.44	82.45	C 7.01
1+05	175.34	81.10	C 5.76
0+80	175.24	80.76	C 5.52
0+55	175.14	80.87	C 5.73
0+30 SMH #1	175.04	80.57	C 5.53 5.24 dia
0+00 existing SMH #3 (Ely end Van Nuys)	174.92	174.96	
BM		180.73	0+30 Hub
BM		168.60	SW 7' con Mon Coss + Van Nuys

.004 rate

∠ 34° 50' Lt

5+01.75	189.96	98.65	C 8.69
4+71.75	188.66	97.76	C 9.10
4+41.75	187.35	97.86	C 10.51
4+11.75	186.05	98.05	C 12.00
3+81.75	184.74	96.94	C 12.20
3+51.75	183.44	95.58	C 12.14
3+21.75	182.13	94.00	C 11.87
2+91.75	180.83	92.21	C 11.38
2+61.75	179.52	90.09	C 10.57
2+31.75	178.22	87.97	C 9.75

.04352 rate

			Staked 5' Lt
7+81.75		200.90	208.45 C.7.55
7+51.75		199.78	207.51 C.7.73
7+21.75		198.66	206.60 C.7.94
6+91.75		197.54	205.57 C.8.03
6+61.75	.0374 rate	196.41	204.48 C.8.07
6+31.75		195.29	203.42 C.8.13
6+01.75		194.17	202.01 C.7.84
5+71.75		193.05	201.15 C.8.10
BM 200.74 on Hub ↓		L. 13° 08' Lt	
5+41.75 ahead =s			5.03 dia
5+46.75 Back	SMH #3	191.93	200.56 C.8.63
5+31.75		191.27	200.01 C.8.74

			Staked 5' Lt
10+71.75		215.24	223.80 C.8.56
10+41.75		213.54	223.81 C.10.27
10+11.75		211.83	223.01 C.11.18
9+81.75		210.13	221.25 C.11.12
9+51.75		208.42	218.38 C.9.96
9+21.75		206.72	215.61 C.8.89
8+91.75	SMH #4	205.02	213.88 C.8.86 Stake 5' Lt
8+71.75		204.27	212.74 C.8.47
8+41.75		203.14	211.57 C.8.43
8+11.75		202.02	210.01 C.7.99
BM		210.41	Chisel X on Rock 10' Rt 8+10 gone

			stake 5' Lt	BM 248.09 25' RP Rt		
				L 29°33' Lt		
13+56.75		229.38	236.18 C 6.80	16+44.65 SMH #6	239.21	248.19 C 8.98
13+26.75		228.36	235.50 C 7.14	16+26.75	238.59	247.28 C 8.69
12+96.75		227.34	234.42 C-7.08	15+96.75	237.57	245.50 C-7.93
			stake 5' Lt			
12+66.75	SMH #5	226.32	232.57 C 6.25	15+66.75	236.54	244.05 C-7.51
12+51.75		225.46	231.45 C 5.99	15+36.75	235.52	242.52 C 7.00
12+21.75		223.76	229.90 C 6.14	15+06.75 .0341 rate	234.50	241.27 C 6.77
11+91.75		222.05	229.20 C-7.15	14+76.75	233.48	240.80 C-7.32
11+61.75	.0568 rate	220.35	228.00 C-7.65	14+46.75	232.45	239.38 C 6.93
11+31.75		218.65	226.77 C 8.12	14+16.75	231.43	238.71 C-7.28
11+01.75		216.94	225.13 C 8.19	13+86.75	230.41	237.68 C 7.27
				BM		233.07 Chisel Rd on Rock zone 12+73

19+44.65		256.75	262.60 C-5.85	22+34.65 & SMH #8	269.02 277.63 C-8.61
19+14.65		255.48	261.90 C-6.42	22+14.65	268.18 276.36 C-8.18
18+84.65	SMH #7	254.21	261.80 C-7.59	21+84.65	266.91 274.33 C-7.42
18+54.65		252.34	259.41 C-7.07	21+54.65	265.64 273.32 C-7.68
18+24.65		250.46	257.41 C-6.95	21+24.65	264.37 272.18 C-7.81
17+94.65		248.59	255.77 C-7.18	20+94.65	263.10 269.95 C-6.85
17+64.65	.0625 rate	246.71	255.55 C-8.84	20+64.65	261.83 270.92 C-9.09
17+34.65		244.84	254.40 C-9.56	20+34.65	260.56 268.98 C-8.42
17+04.65		242.96	251.30 C-8.34	20+04.65	259.29 266.87 C-7.58
16+74.65		241.09	249.52 C-8.43	19+74.65	258.02 264.85 C-6.83
BM			253.85 253.87 ⊡ on Rock 17+25 4' Rt		

.0423 rate

25+84 18 ℄ Hub BM tie out 25' Lt RP		293 46		
25+34 65	282 76	290 91 C-8 15	28+19 18 SMH #10	295 70 303 59 C-7 89
25+04 65	281 39	290 27 C-8 88	27+94 18	294 56 302 89 C-8 33
24+74 65	280 02	289 17 C-9 15	27+64 18	293 20 301 45 C-8 25
24+44 65	278 64	287 47 C-8 83	27+34 18	291 83 299 70 C-7 87
24+14 65	277 27	285 55 C-8 28	27+04 18	290 47 297 98 C-7 51
23+84 65	275 90	284 02 C-8 12	26+74 18	289 11 297 45 C-8 34
23+54 65	274 52	283 56 C-9 04	26+44 18	287 75 296 85 C-9 10
23+24 65	273 15	282 17 C-9 02	26+14 18	286 39 294 75 C-8 36
22+94 65	271 77	280 65 C-8 88	25+84 18 SMH #9 (L. 18°37' Rt.)	285 03 293 38 C-8 35
22+64 65	270 40	279 72 C-9 32	25+64 65	284 13 292 36 C-8 23

.0458 rate

.0454 rate

30+41.53 SMH #11	ewb	304.91	314.80 C-9.89
30+29.18		304.39	313.68 C-9.29
29+99.18		303.15	312.07 C-8.92
29+69.18		301.91	310.63 C-8.72
29+39.18		300.66	307.84 C-7.18
29+09.18		299.42	306.58 C-7.16
28+79.18		298.18	305.56 C-7.38
28+49.18		296.94	304.94 C-8.00

D. Smith
J Rover
R Taylor

INDEXED

Stake "T" Alleys

	Lt = Nly	Rt = Sly
1+70	Co^{16} 6^{74} 386^{58}	386^{58} 6^{94} Co^{36}
1+55	Co^{54} 7^{34} 386^{80}	386^{80} 6^{92} Co^{12}
1+40 ^{17} Ely N+S Alley	Co^{47} 7^{53} 387^{06}	387^{06} 7^{18} Co^{12}
1+25 ^{17} Wly N+S Alley	BVC; Co^{09} 7^{48} 387^{36}	387^{36} 8^{04} Co^{68}
1+02 ^{21}	0.50 BK Co^{37} 8^{21} 387^{84}	387^{84} 8^{38} Co^{44}
0+80 EVC;	1.05 BK Co^{88} 90^{21} 388^{33}	388^{33} 8^{53} Co^{20}
0+60	1' BK Co^{53} 9^{18} 388^{65}	388^{66} 9^{03} Co^{37}
0+40	Co^{65} 9^{39} 388^{74}	388^{76} 9^{18} Co^{42} 6' BK
0+20	Co^{52} 9^{11} 388^{59}	388^{65} 9^{23} Co^{58}
0+00 Ely 36^{14}	388^{23}	388^{33}
F+W Alley		
BM		388^{06} Spike in Guy Pole 1st Alley S BK 42

BK 43 Normal Hts

stakes 3' BK unless noted

	Lt = Nly	Rt = Sly
2+65 ^{34} Wly Chero Kee	385^{88}	385^{85}
2+45	1' BK Co^{28} 6^{23} 385^{95}	385^{95} 6^{30} Co^{35}
2+22	Co^{64} 6^{76} 386^{12}	386^{12} 6^{62} Co^{50}
2+00 EVC;	Co^{20} 6^{49} 386^{29}	386^{29} 6^{82} Co^{53}
1+85	Co^{06} 6^{48} 386^{42}	386^{42} 6^{83} Co^{41}

W.O. # 32173
5/10/54

	Lt = Wly	Rt = Ely	Staked 3' Bk unless noted	Lt = Wly	Rt = Ely
2+60	1.08 BK C1 20 90 18 388 98	388 98 9 74 C0 76	5+60	C1 22 9 12 387 90	387 75 7 91 C0 16
2+22	C0 11 9 21 389 10	389 10 9 32 C0 22	5+30 EVC	85/100 BK C2 69 90 78 388 09	387 98 8 08 C0 10
1+84	0.78 BK C0 99 90 20 389 21	389 21 9 22 C0 01	5+10	92/100 BK C2 49 90 67 388 18	388 12 8 28 C0 16
1+46	C0 09 9 42 389 33	389 33 9 38 C0 05	4+90	370/100 BK C1 40 9 67 388 27	388 24 8 93 C0 69 2 BK
1+08	C0 18 9 62 389 44	389 44 9 70 C0 26	4+70	C1 26 9 60 388 34	388 34 9 11 C0 77
0+70 EVC	1.94 BK C1 36 90 92 389 56	389 56 9 78 C0 22	4+50 BVC	0.17 BK C1 22 9 63 388 41	388 41 9 27 C0 86 1 BK
0+50	C0 48 9 91 389 43	389 40 90 21 C0 81 1 BK	4+12	0.28 BK C1 60 90 12 388 52	388 52 9 42 C0 90 1 BK
0+30	C1 28 90 21 388 93	388 80 90 10 C1 30	3+74	C0 74 9 38 388 64	388 64 90 38 C1 74 0.50 BK
0+10	C1 13 9 18 388 05	387 75 9 58 C1 83	3+36	2.50 BK C1 34 90 09 388 75	388 75 9 53 C0 78
0+00 N/y Madison Ave N&S Alley	C0 42 7 94 387 52 C0 30 7 94 387 64 C6	387 12 8 18 C1 06 387 19 8 18 C0 99 C6	2+98	C1 10 9 97 388 87	388 87 9 37 C0 50

6+50 ^{67} sly of E+W Alley	Co ^{68} 8 ^{04} 387 ^{36}	387 ^{06} 7 ^{18} Co ^{12}
6+20 1BK	Co ^{42} 7 ^{96} 387 ^{54}	387 ^{29} 7 ^{62} Co ^{33}
5+90	Co ^{74} 8 ^{46} 387 ^{72}	387 ^{52} 7 ^{49} Fo ^{03}

D. Smith
D. Chipman
R. Taylor
C.

Stake Storm Drain
Nly "B" St Btwn. 30th & 31st Sts.

WO# 21274
4/4/53

Staked 10' Ely

INDEXED
JUN 7 1955

1+19.38 End.	190.07	93.63	C 3.56
0+88.53	188.88	90.98	C 2.15
0+57.78 P.C.	187.58	88.05	C 0.46
0+39.74 Mid Pt.	186.86	87.05	C 0.19
0+21.71 B.C.	186.14	88.78	C 2.64
	185.27 ↑		
0+00 end existing pipe	185.07 ↓		
30" V.C. make connection			
with 18" R.C.P.			

INDEXED
JUN 7 1954

La Jolla Blvd
Colima to Midway

CO^{10}	5^{20}	75^{60}		2+35
CO^{07}	6^{08}	76^{01}		2+00
CO^{06}	6^{17}	76^{41}		1+65
FO^{03}	6^{78}	76^{81}		1+30
FO^{05}	7^{17}	77^{22}		0+95
FO^{14}	7^{48}	77^{62}		0+60
FO^{28}	7^{74}	78^{02}		0+25
FO^{27}	7^{85}	78^{22}		0+00
FO^{52}	7^{25}	78^{27}	$\frac{67}{100}$ cb	$0-28^{06}$ cb B.C.
FO^{28}	7^{96}	78^{24}	$\frac{67}{100}$	1/4
CO^{02}	8^{19}	78^{17}	$\frac{58}{100}$ dip & Lip	1/2
CO^{03}	8^{14}	78^{11}	$\frac{52}{100}$	3/4
	8^{07}	78^{11}	$\frac{50}{100}$	E.C. Colima

Ely Cb		73^{24}	$\frac{57}{100}$	E.C. Midway
Fo^{44}	2^{35}	72^{79}	$\frac{63}{100}$	3/4
Cl^{10}	3^{43}	72^{33}	$\frac{67}{100}$	1/2
Cl^{06}	3^{07}	72^{01}	$\frac{67}{100}$	1/4
Fo^{15}	1^{96}	72^{11}	$\frac{67}{100}$	$5+37^{57}$ BC
Fo^{20}	2^{18}	72^{38}		5+15
Fo^{20}	2^{58}	72^{78}		4+80
Fo^{16}	3^{02}	73^{18}		4+45
Fo^{15}	3^{44}	73^{59}		4+10
Fo^{04}	3^{95}	73^{99}		3+75
Fo^{11}	4^{28}	74^{39}		3+40
Fo^{10}	4^{70}	74^{80}		3+05
Fo^{08}	5^{12}	75^{20}		2+70

INDEXED

La Jolla Blvd — Midway to Forward — Ely Cb

		Wly Cb 3'bk	Nail top Sub grade bot.	℄					
8+25	2°09.4191'	72 15 72 02 FO 13					FO 39 2 17	72 56	8+25
8+00	1°51.5043'	71 91 71 82 FO 09	71 69 71 33 CO 36	72 44		7 83 71 35 CO 48	FO 06 2 31	72 37	8+00
7+75	1°37.5895'	71 55 71 06 FO 49					FO 11 2 07	72 18	7+75
7+50	1°21.6747'	71 18 71 08 FO 10	71 28 70 51 CO 77	72 09		1 32 70 90 CO 42	FO 25 1 75	72 00	7+50.
C= (± 34/100)									
7+25	1°05.7599'	70 75 CO 20 70 95					FO 21 1 60	71 81	7+25
	0°47.617'		70 83 70 28 CO 55	71 67		70 88 70 55 CO 33	FO 23 1 39	71 62	7+00
6+96 5 Cb PRC	67/100	70 25 40 960 FO 65							
2/3 Mid Pt.	67/100	~~70 00~~ 69 85/16 925 FO 60					FO 24 1 20	71 44	6+67 5 Brk
1/3	67/100	~~69 69~~							
Culvert end. Meet	67/100	69 27					FO 24 1 08	71 32	6+44 80 Brk
								71 30 67/100	6+30 3 PCC.
							FO 25 1 05	71 30 65/100	3/4
							FO 29 1 03	71 32 58/100	1/2
							FO 27 1 13	71 40 61/100	1/4
								71 60 83/100	Midway EC

NOTE: Grades Wly Cb. from Bird Rock to Camino De La Costa See G-319

		Wly Cb 3'BK	Nail	℄		Ely Cb	
11+00	5°04.4819'	74.12 73.90 FO.22	73.95 73.46 CO.49	74.54	387 73.35 CO.52	FO.33 4.19 74.52	11+00
10+75	4°48.5671	73.97 73.80 FO.17				FO.32 4.05 74.37	10+75
10+50	4°32.6523	73.81 73.55 FO.26	73.55 73.15 CO.40	74.22	350 73.10 CO.40	FO.25 3.95 74.20	10+50
10+25	4°16.7375'	73.63 73.36 FO.27				FO.09 3.93 73.02	10+25
10+00	4°00.8227'	73.45 73.19 FO.26	73.39 72.82 CO.57	73.90	316 72.80 CO.36	FO.06 3.78 73.84	10+00
9+75	3°44.9079	73.27 73.42 CO.15				CO.41 4.07 73.66	9+75
9+50	3°28.9931'	73.09 72.62 FO.47	72.81 72.45 CO.36	73.53	280 72.45 CO.35	FO.17 3.31 73.48	9+50
9+25	3°13.0783	72.92 72.51 FO.41				CO.04 3.33 73.29	9+25
9+00	2°57.1635'	72.74 72.27 FO.47	72.47 72.10 CO.37	73.18	242 72.02 CO.40	CO.06 3.17 73.11	9+00
8+75	2°41.2487'	72.56 72.09 FO.47				FO.04 2.89 72.93	8+75
8+50	2°25.3339'	72.39 71.96 FO.43	72.06 71.76 CO.30	72.83	207 71.65 CO.42	FO.10 2.64 72.74	8+50

		Wly Cb 3' bk	Nail	℄
PRC cb 13+10⁵	7°18.4845'	67/100 74⁹⁶ 3⁸³ F1¹³	4⁸⁸ 74¹⁸ CO⁷⁰	75⁴³
3/4		66/100 74⁷¹ 4⁰¹ FO⁷⁰		
1/2		63/100 74⁰⁵ 2⁷⁵ F1³⁰		
1/4		60/100 73³⁵ 3⁰⁴ FO³¹		
Foward E.C.	72²⁹ gutter exists	55/100 72⁶² 2⁴⁹ FO³³		
Forward E.C.		58/100 74.00 73⁶⁰ FO.85 73¹⁵ FO⁴⁶	A.C. Gut. 73.52	
3/4		59/100 74.24 73⁸⁸ 72⁴⁴ F1⁵⁴ F1.80		
1/2		63/100 74.47 74³⁴ 73¹⁷ F1⁴⁷ F1.30		
1/4		66/100 74⁵⁹ 73⁶⁴ FO⁹⁵		
12+29	6°26.602' cb PRC.	67/100 74⁶⁵ 74⁰² FO⁶³		
12+00	6°08.1411'	74⁵⁴ 74⁶⁵ CO¹¹	74⁵⁹ 74⁰⁶ CO⁵³	75¹⁹
11+75	5°52.263'	74⁴⁴ 74⁴⁰ FO⁰⁴		
11+50	5°36.3115'	74³⁵ 74³⁷ CO⁰²	74⁵² 73⁷⁵ CO77	74⁸⁵
11+25	5°20.3967'	74²⁴ 74¹¹ FO¹³		

	Ely cb	
492 74⁴⁰ CO⁵³	7°11.8003' FO²⁷ 5⁰⁴ 75³¹	13+00
	6°56.904' FO¹⁴ 5⁰⁹ 75²³ 67/100	PCC cb 12+76⁶
	FO⁶⁹ 4⁵⁶ 75²⁵ 44 67/100	3/4
	FO⁰⁵ 5³¹ 75³⁶ 67/100	1/2
	FO²⁵ 5³⁸ 75⁶³ 67/100	1/4
477 74³⁵ CO⁴² ℄ Forward	FO⁴⁹ 5⁶¹ 76¹⁰ 67/100	Forward EC
	FO⁶¹ 6⁷⁹ 77⁴⁰ +20 78⁴⁸	
	7⁹⁶ meet +15	
	FO³² 6³⁸ 76⁷⁰ 67/100	Forward EC.
	FO¹³ 5⁹⁵ 76⁰⁸ 67/100	3/4
	CO⁵³ 6⁰⁴ 75⁵¹ 67/100	1/2
	CO⁵¹ 5⁶¹ 75¹⁰ 67/100	1/4
443 74⁰⁶ CO³⁷	CO¹⁴ 5⁰⁷ 74⁹³ 67/100 6°02.4118'	PCC cb 11+90⁹
	FO⁰² 4⁸⁴ 74⁸⁶	11+75
420 73⁸⁵ CO³⁵	CO⁰⁴ 4⁷⁹ 74⁷⁵	11+50
	FO¹⁶ 4⁴⁸ 74⁶⁴	11+25

	Wly Cb	Nail	℄		Ely Cb
15+25	75 78 5 90 CO 12				FO 46 5 65 76 11 15+25
15+00	75 69 5 59 FO 10	5 60 75 02 CO 58	76 05	5 42 74 90 CO 52	FO 04 5 99 76 03 15+00
14+75	75 60 5 54 FO 06				CO 07 6 01 5 96 75 94 14+75
14+50	75 50 4 91 FO 59	5 35 74 67 CO 68	75 90	5 29 74 80 CO 49	CO 18 6 03 5 97 75 85 14+50
Alley B.C. 14+24 8	75 41 5 10 FO 31				CO 05 5 81 5 76 75 76 14+25
E.C.	75 47 5 10 FO 37			5 20 74 60 CO 60	CO 13 5 86 75 73 E.C. 8° 18.6424
Prop Alley	75 69 4 15 FI 54				CO 30 5 99 67/100 75 69 Alley B.C. 14+04 9
Prop Alley	75 63 4 40 FI 23				CO 24 5 99 64/100 75 75 E.C.
E.C.	75 40 5 19 FO 21			CO 87	FO 13 6 82 17/100 75 95 Alley Prop
Alley B.C. 14+00 8°15.4595'	75 30 5 19 FO 11	5 36 74 52 CO 84	75 74		FO 41 5 48 17/100 75 89 Alley Prop
					FO 87 4 81 64/100 75 68 E.C.
13+75 7°59.5447'	75 21 4 30 FO 91				FO 77 4 81 67/100 75 58 Alley B.C. 13+77 86 8° 01.5124
13+50 7°43.6299'	75 11 4 03 FI 08	4 91 74 30 CO 61	75 57	5 09 74 50 CO 59	FO 93 4 56 75 49 13+50
13+25 7°27.7151'	75 02 3 88 FI 14				FO 50 4 90 75 40 13+25

	Wly Cb	Nail	℄		Ely Cb	
18+00	77^{26} 6^{59} FO^{67}	6^{78} 76^{20} CO^{58}	77^{34}	6^{70} 76^{15} CO^{55}	FO^{36} 6^{80} 77^{16}	18+00
17+75	77^{07} 6^{81} FO^{26}				FO^{25} 6^{77} 77^{02}	17+75
17+50	76^{89} 6^{71} FO^{18}	6^{37} 75^{81} CO^{56}	76^{89}	6^{27} 75^{75} CO^{52}	FO^{31} 6^{59} 76^{90}	17+50
17+25	76^{75} 6^{36} FO^{39}				FO^{28} 6^{54} 76^{82}	17+25
17+00	76^{62} 6^{15} FO^{47}	6^{09} 75^{45} CO^{64}	76^{61}	6^{09} 75^{57} CO^{52}	FO^{46} 6^{27} 76^{73}	17+00
16+75	76^{48} 5^{91} FO^{57}				FO^{21} 6^{43} 76^{64}	16+75
16+50	76^{35} 5^{30} FI^{05}	6^{05} 75^{35} CO^{70}	76^{50}	5^{92} 75^{47} CO^{45}	CO^{01} ~~FO^{04}~~ 6^{56} 76^{55}	16+50
16+25	76^{23} 5^{44} FO^{79}				FO^{14} 6^{32} 76^{46}	16+25
16+00	76^{11} 5^{16} FO^{95}	5^{96} 75^{26} CO^{70}	76^{36}	5^{70} 75^{20} CO^{50}	CO^{12} 6^{50} 76^{38}	16+00
15+75	75^{99} 5^{43} FO^{56}				FO^{07} 6^{22} 76^{29}	15+75
15+50	75^{88} 5^{69} FO^{19}	5^{75} 75^{05} CO^{70}	76^{22}	5^{63} 75^{10} CO^{53}	FO^{25} 5^{95} 76^{20}	15+50

NW 25' Rad Pt BM 80 58	W/y Cb 3' BK	Nail	℄
1/4	79 27 8 98 F0 29		
BC. Bird Rock	78 91 8 92 C0 01		
EC. Bird Rock 55/100	78 62		38° 14'
3/4 58/100	78 85 8 81 F0 04		28° 40' 30"
1/2 69/100	79 07 7 77 F1 30	C: 7 31	19° 07'
1/4 65/100	79 21 8 27 F0 94		9° 33' 30"
BCob 19+70 96 67/100	79 21 8 86 F0 35		0° 00'
19+50	79 01 8 50 F0 51	8 71 / 78 17 / C0 54	79 15
19+25	78 74 8 32 F0 42		
19+00	78 44 8 09 F0 35	8 09 / 77 40 / C0 69	78 58
18+75	78 12 7 79 F0 33		
18+50	77 80 7 74 F0 06	7 44 / 76 98 / C0 46	77 98
18+25	77 52 7 22 F0 39		

913 78 60 C0 53	℄ Bird Rock	Ely Cb		
		79 67	BC.	
C0 28	9 92	67/100	79 64	3/4
F0 65	9 13		79 78	1/2
F0 68	9 24		79 92 / ~~79 97~~	1/4
			80 01 / ~~80 11~~	
Meet			EC Bird Rock	
F0 09	9 44	60/100	79 53	Bird Rock EC
F0 82	8 45	63/100	79 27	3/4
F1 09	7 91	65/100	79 00	1/2
F1 27	7 49	67/100	78 76	1/4
F0 50	8 09	67/100	78 59	BCob 19+42 96
F0 22	8 18		78 40	19+25
F1 65	6 49		78 14	19+00
F0 28	7 59		77 87	18+75
F1 35	6 25		77 60	18+50
F0 85	6 51		77 36	18+25

	Wly Cb 3'bK	Nail	℄		Ely Cb	
22+50	79^{64} 8^{95} Fo^{69}	9^{40} 78^{67} Co^{73}	79^{83}	916 78^{70} Co^{46}	Fo^{09} 9^{74} 79^{83}	22+50
22+25	79^{76} 9^{12} Fo^{64}				Fo^{20} 9^{79} 79^{99}	22+25
22+00	79^{88} 9^{71} Fo^{17}	9^{85} 79^{10} Co^{75}	80^{22}	958 79^{15} Co^{43}	Co^{33} 80^{47} 80^{14}	22+00
21+75	79^{97} 9^{50} Fo^{47}				Co^{45} ~~Co^{39}~~ ↓ ↗ 80^{24} Co^{42} 80^{69} 80^{27}	21+80 21+75
21+50	80^{06} 9^{76} Fo^{30}	9^{99} 79^{30} Co^{69}	80^{42}	977 79^{22} Co^{55}	Fo^{02} 80^{38} 80^{40}	21+50
21+25	80^{07} 9^{49} Fo^{58}				Fo^{11} 80^{31} 80^{42}	21+25
21+00	80^{09} 9^{62} Fo^{47}	9^{92} 79^{20} Co^{72}	80^{36}	965 79^{30} Co^{35}	Fo^{36} 80^{08} 80^{44}	21+00
20+75	80^{00} 9^{24} Fo^{76}				Fo^{47} 79^{78} 80^{25}	20+75
E.C. 20+53 ^{23}	79^{86} 8^{90} Fo^{96}	9^{53} 78^{90} Co^{63}	80^{11}	943 78^{90} Co^{53}	Fo^{33} 79^{67} 80^{00}	20+50
3/4	79^{74} 9^{01} Fo^{73}					
1/2	79^{54} 9^{48} Fo^{06}			929 78^{75} Co^{54}	Fo^{17} 9^{50} 79^{67}	EC 20+24 ^{74}

	Wly Cb 3'BK	Nail	2		Ely Cb	
25+00	77^{52} 6^{94} FO^{58}	7^{19} 76^{47} CO^{72}	77^{59}	6^{87} 76^{50} CO^{37}	CO^{04} 7^{20} 77^{66}	25+00
24+75	77^{73} 6^{92} FO^{81}				CO^{19} 8^{08} 77^{89}	24+75
24+50	77^{95} 7^{05} FO^{90}	7^{65} 76^{93} CO^{72}	78^{02}	7^{38} 76^{95} CO^{43}	FO^{01} 8^{10} 78^{11}	24+50
24+25	78^{17} 7^{03} FI^{14}				FO^{02} 8^{31} 78^{33}	24+25
24+00	78^{39} 7^{53} FO^{86}	8^{13} 77^{43} CO^{70}	78^{50}	7^{79} 77^{35} CO^{44}	FO^{06} 8^{49} 78^{55}	24+00
23+75	78^{61} 7^{68} FO^{93}				FO^{32} 8^{45} 78^{77}	23+75
23+50	78^{83} 7^{89} FO^{94}	8^{54} 77^{75} CO^{69}	78^{95}	8^{25} 77^{80} CO^{45}	FO^{32} 8^{67} 78^{99}	23+50
23+25	79^{05} 8^{02} FI^{03}				FO^{17} 9^{04} 79^{21}	23+25
23+00	79^{27} 8^{49} FO^{78}	9^{00} 78^{27} CO^{73}	79^{39}	8^{76} 78^{25} CO^{51}	FO^{16} 9^{27} 79^{43}	23+00
22+75	79^{43} 8^{63} FO^{80}				CO^{05} 9^{69} 79^{64}	22+75

	Wly Cb 3'BK	Nail	℄			Ely Cb 3'BK	
27+50	73^{85} 7^{87} CO^{02}	4^{06} 73^{30} CO^{76}	74^{36}	4^{11} 73^{71} CO^{40}	FO^{37}	5^{04} 75^{41}	BC $27+29^{05}$
27+25	74^{31} 4^{36} CO^{05}				FO^{35}	5^{10} 75^{45}	27+25
27+00	74^{77} 4^{30} FO^{47}	4^{89} 74^{10} CO^{79}	75^{24}	4^{56} 74^{35} CO^{21}	FO^{05}	5^{66} 75^{71}	27+00
26+75	75^{24} 5^{21} FO^{03}				FO^{23}	5^{75} 75^{98}	26+75
26+50	75^{70} 5^{51} FO^{19}	5^{73} 74^{95} CO^{78}	76^{07}	5^{37} 75^{10} CO^{27}	FO^{09}	6^{15} 76^{24}	26+50
26+25	75^{87} 6^{90} CI^{03}				FO^{11}	6^{40} 76^{51}	26+25
26+00	76^{51} 6^{18} FO^{33}	6^{29} 75^{55} CO^{74}	76^{74}	6^{06} 75^{70} CO^{36}	FO^{28}	6^{49} 76^{77}	26+00
25+75	76^{83} 6^{47} FO^{36}				FO^{48}	6^{51} 76^{99}	25+75
25+50	77^{08} 7^{03} FO^{05}	6^{77} 76^{05} CO^{72}	77^{17}	6^{44} 76^{10} CO^{34}	CO^{08}	7^{29} 77^{21}	25+50
25+25	77^{30} 7^{48} CO^{18}				FO^{05}	7^{38} 77^{43}	25+25

	Wly Cb 3'bk			Ely Cb 75
NECT De La Costa & La Jolla Blvd				
BM	73^{04}			
De La Costa	70^{27} 70^{03} FO^{04}			De La Costa
EC,				Meet 75^{80} $\frac{43}{100}$ EC,
				FO^{65} 4^{75} 75^{40} $\frac{48}{100}$
3/4	71^{39} 1^{24} FO^{15}			FO^{70} 4^{42} 75^{12} $\frac{52}{100}$ 3/4
				FO^{66} 4^{40} 75^{06} $\frac{55}{100}$
1/2	72^{36} 2^{27} FO^{09}			FO^{56} 4^{45} 75^{01} $\frac{58}{100}$ 1/2
				FO^{82} 4^{28} 75^{10} $\frac{62}{100}$
1/4	73^{11} 2^{96} FO^{15}			FO^{93} 4^{27} 75^{20} $\frac{65}{100}$ 1/4
				FO^{56} 4^{74} 75^{30}
$27+63^{77}$ BC,	73^{59} 3^{74} CO^{15}	3^{81} 73^{00} CO^{81}	74^{11}	FO^{37} 5^{04} 75^{41} $\frac{67}{100}$ BC,

D. Smith
J Rover
R Taylor
B. Fish

Martin St 35th to Wabash

Curb Stakes 3' BK Cb Face.

WO # 31399
1/5/54
76

	Lt = Sly	Rt = Nly		Lt = Nly	Rt = Nly
2+45	F0.01 6.19 36.20	36.70 6.62 F0.08	4+60	F0.07 6.58 16.65	16.91 6.86 F0.06
2+25 BVC.	F0.17 7.04 37.21	37.71 7.66 F0.05	4+40	C0.06 7.80 17.74	18.00 7.96 F0.04
1+88	F0.02 8.87 38.89	39.39 9.70 C0.31	4+20	C0.28 9.48 19.20	19.47 9.44 F0.03
1+51	C0.25 0.82 40.57	41.07 1.43 C0.36	4+00	C0.09 1.12 21.03	21.32 20.75 F0.57
1+14	C0.44 2.69 42.25	42.75 2.99 C0.24	3+80 BVC.	F0.04 3.18 23.22	23.54 3.86 C0.32 2' BK
0+77	C0.07 4.00 43.93	44.43 4.31 F0.12	3+45 EVC.	C0.09 7.47 27.38	27.76 8.47 C0.71
0+40 BrK	F0.40 5.20 45.60	46.10 5.98 F0.12	3+25	C0.13 9.76 29.63	30.05 30.59 C0.54
0+20	F0.02 5.78 45.80	47.35 7.42 C0.07	3+05	C0.04 1.68 31.64	32.09 2.33 C0.24
0+10 Cb EC.	C0.33 5.75 45.42	48.10 8.12 C0.02	2+85	C0.35 3.75 33.40	33.87 4.02 C0.15
0+00 w/y 35th Cb end	C0.63 5.43 44.80	48.90 9.10 C0.20	2+65	C0.21 5.12 34.91	35.41 5.55 C0.14

	Lt = Sly	Rt = Nly
5+42.71 cb end Lt	meet 14.87 existing 15.07	
5+40.28 cb end Rt		15.59 meet 15.28 existing
5+32.04 cb BC, Lt.	FO.23 ~~FO.38~~ 4.87 15.10 ~~15.25~~	
5+28.93 cb BC, Rt		15.40 ~~15.64~~ 5.46 GO.06
5+00 EVC.	GO.08 5.63 15.55	15.85 5.78 FO.07
4+80	GO.10 6.01 15.91	16.19 6.20 GO.01

Stake Storm Drains
Midway & La Jolla Blvd

INDEXED
JER
JAN 18 1955

BM		70^{32} SWBP Midway & La Jolla		
	18" R.C.P.		42" R.C.P.	
Cb EC 5' BK	71^{60}	71^{78} $C0^{18}$ 5' BK cb face	114^{25} wly Meet	61^{34}
			100' wly	61^{46} 69^{52} $C8^{06}$
℄ Box Type B2 inlet	66^{50} 1e 18" pipe	$71.^{98}$ $C5^{48}$	75' wly	61^{71} 70^{44} $C-8^{73}$
Mid Pt 18" Pipe	67^{00}	71^{86} $C4^{86}$ 5' ANGly	50' wly	61^{96} 70^{70} $C-8^{74}$
			25' wly	62^{19} 71^{09} $C8^{90}$
℄ Type H inlet 5' BK cb face	67^{50} 1e 18" pipe	71.60 $C4^{10}$	℄ Box Type B2 inlet	62^{44} 1e 42" pipe $71.^{98}$ $C-9^{54}$
	70^{46} grate	$C1^{14}$		71^{02} grate $C-0^{96}$
	71^{30} cb	$C0^{30}$		71^{85} cb $C-0^{13}$
	71^{30}	71^{58} $C0^{28}$ Nly		
	71^{30}	71^{56} $C0^{26}$ Sly		

BM

Cb EC

£ Box T

Mid Pt

£ Type
5'

586
116
420

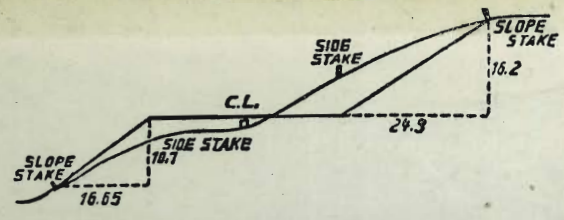
7960
436

8396
325
8071

8396
7911
485

8396
310
8086

8396
460
7933



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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