

MISC. ROAD SURVEYS.

Book 1

~~2~~

400

LEVEL

W 14

Table showing the difference of latitude and departure in running 80 chains at any course from 1 to 60 minutes.

MINUTES	LKS.	MINUTES	LKS.
1.....	2 $\frac{1}{3}$	21.....	49
2.....	4 $\frac{2}{3}$	22.....	51 $\frac{1}{3}$
3.....	7	23.....	53 $\frac{2}{3}$
4.....	9 $\frac{1}{3}$	24.....	56
5.....	11 $\frac{2}{3}$	25.....	58 $\frac{1}{3}$
6.....	14	26.....	60 $\frac{2}{3}$
7.....	16 $\frac{1}{3}$	27.....	63
8.....	18 $\frac{2}{3}$	28.....	65 $\frac{1}{3}$
9.....	21	29.....	67 $\frac{2}{3}$
10.....	23 $\frac{1}{3}$	30.....	70
11.....	25 $\frac{2}{3}$	31.....	72 $\frac{1}{3}$
12.....	28	32.....	74 $\frac{2}{3}$
13.....	30 $\frac{1}{3}$	33.....	77
14.....	32 $\frac{2}{3}$	34.....	79 $\frac{1}{3}$
15.....	35	35.....	81 $\frac{2}{3}$
16.....	37 $\frac{1}{3}$	36.....	84
17.....	39 $\frac{2}{3}$	37.....	86 $\frac{1}{3}$
18.....	42	38.....	88 $\frac{2}{3}$
19.....	44 $\frac{1}{3}$	39.....	91
20.....	46 $\frac{2}{3}$	40.....	93 $\frac{1}{3}$
		41.....	95 $\frac{2}{3}$
		42.....	98
		43.....	100 $\frac{1}{3}$
		44.....	102 $\frac{2}{3}$
		45.....	105
		46.....	107 $\frac{1}{3}$
		47.....	109 $\frac{2}{3}$
		48.....	112
		49.....	114 $\frac{1}{3}$
		50.....	116 $\frac{2}{3}$
		51.....	119
		52.....	121 $\frac{1}{3}$
		53.....	123 $\frac{2}{3}$
		54.....	126
		55.....	128 $\frac{1}{3}$
		56.....	130 $\frac{2}{3}$
		57.....	133
		58.....	135 $\frac{1}{3}$
		59.....	137 $\frac{2}{3}$
		60.....	140

TABLE FOR RUNNING ON SLOPES.

In the following table the first column shows the angle, the second the number of links to be added to a chain on the slopes, to make one chain, horizontal measurement.

Angle	Cor. in Links						
0		0		0		0	
4	0.24	11	1.88	18	5.14	25	10.54
5	0.38	12	2.24	19	5.76	26	11.26
6	0.55	13	2.63	20	6.42	27	12.24
7	0.76	14	3.06	21	7.11	28	13.37
8	0.98	15	3.53	22	7.85	29	14.34
9	1.24	16	4.02	23	8.64	30	15.47
10	1.55	17	4.56	24	9.47	35	22.07

16

17

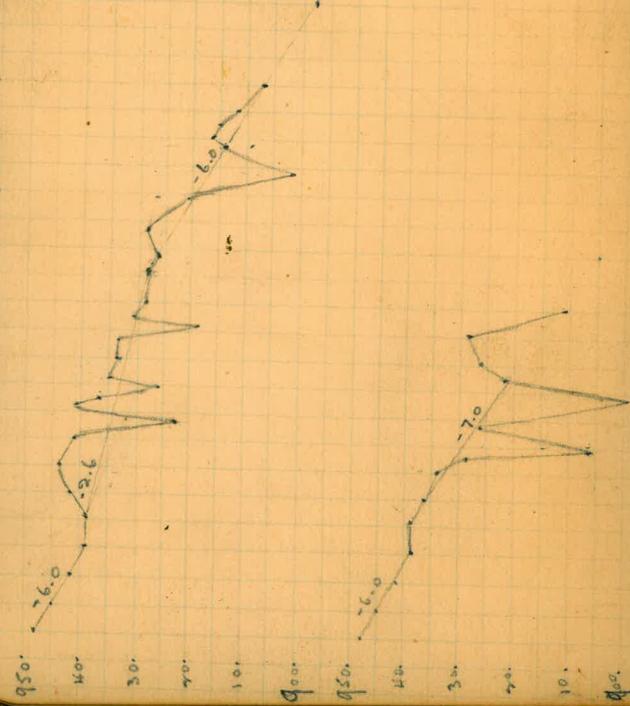
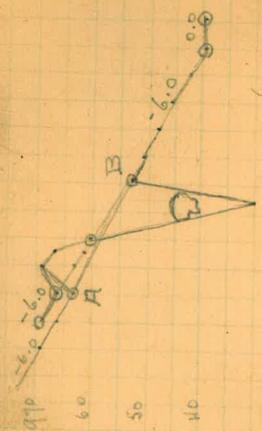
Monday Sept 24 - Time line 1-2

to the top of the hill back of the

to the 119 + 96 4/5 of the way 3-6

to the top of the hill to the top 7-10

95
94
93
92
91
90
89
88
87
86
85
84
83
82
81
80
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77
76
75
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14
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12
11
10
9
8
7
6
5
4
3
2
1
0



Synopsis of Lines.

"P" Line Total Line from Saddle west of Sandell's Cabin to Ward's Line 3-6

"X" Line From High Summit west of Sandell's Cabin to King's Line 7-10

"T" Line From Sawyer Saddle to County Road. 11-13

"H" Line From County Road to Sawm Saddle. 14-17

"Change in King's Line" Sta 24+40 to 28-33

"V" Line Sawm Saddle Dulzura Pass to Shecker Valley (Join Permit County Road west of Shecker House) 34-47

Grade Notes Sawm Saddle constructed Road 47-48

"C" Line Levels for Profile of Road from Dulzura Pass to Shecker Valley (unfinished) 50-65

"D" Line Branch of "C" Line at 7+50 66-77

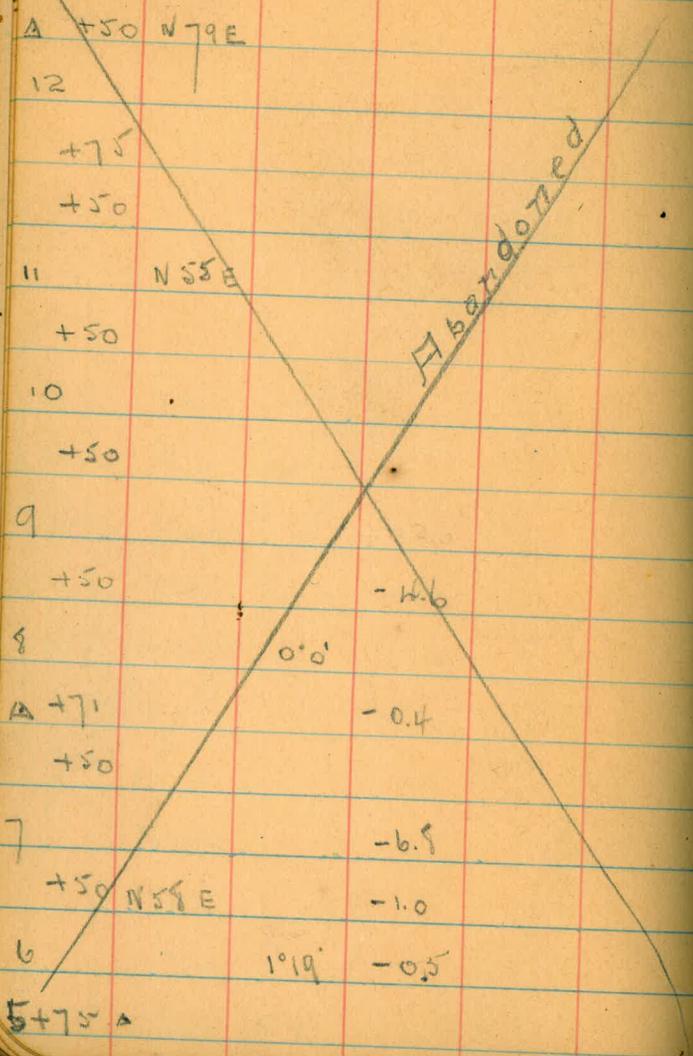
Apr. 10, 1907.

Sta Magto. Var. \swarrow

5	+50		-0.6
5			-2.7
	+50		-5.1
4			-7.3
	+50		-2.1
3			
	+75	N 61 E	
Δ	+50	N 66 E 20	
	+25	N 66 E	
2		N 66 E	+0.2
	+75	N 66 E	-0.6
	+50	N 66 E	-1.75
	+25	N 66 E	-1.3
1		N 66 E	
	+75	N 67 E	
	+50	N 75 E	
	+25	N 85 E 1045'	

Flotation

Sta Onaplo Vent \swarrow cur. Fee



○ boulder

3. Trial line from saddle back of
"P" line

Sandells Cabin to Ward's line.

0		1000		= assumed elevation
	5.0	1005		
+50			996.5	8.5
1			993.0	12.0
0		139	991.1	
	1.1	992.2		
+50			989.5	27
2			986.0	6.2
+50			982.5	9.7
3			979.0	13.2
0		124	979.8	
	1.8	981.6		
+50			975.5	6.1
H			972.0	9.6
+50			968.5	13.1
0		12.5	969.1	
	0.3	969.4		
5			965.0	4.4

4 "P" hine

969.4

961.5

5+50

961.5

7.9

Wach

6+11

957.3

12.1

0

12.7

956.7

3.2

959.9

+50

957.3

2.6

+90

957.3

2.6

x

7+50

953.1

6.8

8

949.6

10.3

+50

11.3

948.6

946.1

13.8

+2.5

0

11.6

948.3

2.1

950.4

942.6

9

3.2

3.2

942.6

7.8

+50

6.3

939.1

10

9.7

935.6

+50

12.7

932.1

18.3

0

12.7

937.7

6.5

944.2

5

"P" Line

944.2

11

.89

+50

11.6

0

12.6

931.6

09

932.5

12

2.7

+50

6.2

13

9.0

+50

11.1

14

12.0

0

11.8 920.7

29

923.6

+50

2.9

15

3.1

+50

4.6

16

6.0

+50

7.0

17

7.4

6 " P. LINE

9226

17+50

9.0

18

10.2

+50

11.9

19

12.9

0

12.6 911.0

4.4 913.4

+50

3.7

20

4.1

+30

4.9 910.5

= Sta 119+96 of Ward's Survey

7 From High Summit To King's Summit

"X" line

0			1000.0		
	3.1	1003.1			
0 +50			63	996.5	6.6 +0.3
1				993.0	10.1
+50				989.5	13.6
0			12.5	990.6	
	0.7	991.3		986.0	5.3
2				986.0	5.3
+50				982.5	8.8
3				979.0	12.3
0			12.8	978.5	
	0.2	978.7			
+50				975.5	3.2
4				972.0	6.7
+50				968.5	10.2
5				965.0	13.7
0			12.6	966.1	
	0.4	966.5			

8	"X" wine			
	966.5			
+50			961.5	5.0
6			958.0	8.5
+50			954.5	12.0
0		12.8	953.7	
	0.5	954.2		
7			951.0	3.2
+50			947.5	6.7
8			944.0	10.2
+50			940.5	13.7
0		12.4	941.8	
	0.9	942.7		
9			937.0	5.7
+50			933.5	9.2
10			930.0	12.7
0		12.5	930.2	
	4.2	934.4		
+50			926.5	7.9

"X" Line

highest pt in same section 3.3 931.1
934.4

11 923.0 11.4

0 12.5 921.9

1.3 923.2

+50 919.5 3.7

-7.0

12 916.0 7.2

+50 912.5 10.7

0 12.2 911.0

1.0 912.0

13 909.0 3.0

+50 4.5 907.5

14 6.2 905.8

+50 8.0 904.0

15 7.2 904.8

+50 6.3 905.7

16 8.7 903.3

+50 6.0 906.0

17 5.3 906.7

For Proportion

gulf 16+23 sec. 898.6

"X" wine

912.0

0

5.4 906.6

1.5 908.1

1
7
0

17+50

903.2

4.0

18

899.7

8.4

17 +50

896.2

11.9

0

117 896.4

X18+70 = 293 Kings wine

11 From Lower Daddle to County Road

T line

From x line page 9

Sta 0			931.1		
	1.7	932.8			
	+50		928.1	4.7	
1			925.1	7.7	
	+50		922.1	10.7	
2			919.1	13.7	
0			12.2	920.6	
	0.0	920.6			1.0
	+50		916.1	4.5	
3			913.1	7.5	
	+50		910.1	10.5	
4			907.1	13.5	
0			12.7	907.9	
	1.0	908.9			
	+50		904.1	4.8	
5			901.1	7.8	
	+50		898.1	10.8	
6			895.1	13.8	

12

T Sine

5705°W

908.9

0

124 8.965

0.9 897.4

1

6+50

892.1

5.3

6
0

7

889.1

8.3

+50

886.1

11.3

x

0

12.7 884.7

6.4 891.1

Angle of depression 1° 8'

8

7.0

+50

8.1

9

10.2

+50

13.3

0

13.0 878.1

1.0 879.1

100
Profiling.

10

3.6

+50

4.1

11

4.7

+50

4.9

13

8791

12

7.3

+50

7.8

13

7.9

+50

7.6

14

7.5

+50

8.3

15

10.1

+50

10.1

869.0

0

9.9

869.2

T. S. S. S.

14 "A" Line From County Road to
Sta 1

869
869.2

Lower Saddle.

= 15+50 on "T" line

12.6 881.8

+50

872

9.8

2

875

6.8

+50

878

3.8

3 0

1.2 890.6

0.2

12.6 893.2

+
5
0

3

881

12.2

+50

884

9.2

4

887

6.2

+50

887

6.2

*

5

887

6.2

+50

887

6.2

6

887

6.2

+50

887

6.2

7

887

6.2

+50

887

6.2

*

0

5.6 887.6

15

A sim

887.6

12.5 900.1

8 889 11.1

+50 891 9.1

9 893 7.1

+50 895 5.1

10 897 3.1

0 0.5 899.6

12.5 912.5

+50 899

11 901 11.5

+50 903 9.5

12 905 7.5

+50 907 5.5

13 909 3.5

0 2.1 910.4

12.5 922.9

+50 911 11.9

16.

Flume

9229

14

+50

+87

15+37

+87

16+37

+87

17+37

5.8 936.9

931.1

x

18

+50

4.9

5.2

19

+50

6.7

8.8

20

+50

10.4

12.2

0

12.1

9248

1.9 926.7

For Professor

17 "A" line

926.7

21 3.2

+50 4.3

22 5.6

+50 8.1

23 12.2

0 12.75 914.45

2.0 916.45

+50 3.5

24 6.9

+70 7.0 909.45

= X 13+00

Note Station on X line from
13+00 to end changed to corre-
spond to number consecutively on
"A" line

"A" 29+90 = 2930 Kings line

29+90
32290

Y18 Change of line

284+40	8.1
283+90	10.1
+40	7.7
282+40	8.3
281+60	11.3



280	100.0	100.0
19	101.9	
279+11	20	99.9 98.2
279	37	98.7 98.0
278	5.6	96.3 96.0
277+72	6.2	95.7 96.5
277	44	97.5 96.7
0	42	97.7

1257 110.27

276+48	13.6	96.5 97.0
276	11.7	98.6 99.6
275	7.3	103.0 102.6

-2.0
+0.4
9.7 +1.4

(In old road)

For Profile

x
-1.7
+0.7
x +0.3
-0.8
+ +0.8
0.6
x -0.5
+ -0.4

19

Chang in King Sun.

110.27

774+52 4.2 106.1 105.0

+1.1 X

274 5.2 105.1 105.0

+0.1 X

273 2.1 108.2 107.7

+0.5

0 153 108.74

+2.6

640 115.14

272 3.5 111.6 110.4

+1.2

271 1.6 113.5 113.0

+0.5 X

270 5.7 109.4 110.0

-0.6

269 7.7 107.4 107.0

+0.4 X

268 7.0 108.1 106.0

+2.1

267 9.4 105.7 105.0

+0.7 X

266 9.2 105.9 105.0

+0.9 X

0 9.5 105.99

12.50 118.49

265 10.7 107.8 107.8

264 5.1 113.4 113.4

0 0.73 117.76

20

Change in King Sun

117.76

17.70 130.46

263 116 118.9 119.9

262 10.2 120.3 123.0

261 +35 1.6 128.9 127.0

0 14.5 129.01

19.0 130.91

260 4.6 126.3 126.0

259 9.7 121.7 120.6

258 +68 13.7 117.2 118.9

258 14.1 116.8 115.2

0 12.0 118.11

0.95 119.06

257 9.3 109.8 109.8

256 12.6 106.5 104.0

0 12.0 106.16

0.32 106.78

255 +59 7.3 99.5 103.1

x

-2.7 +

+1.9

x

1.0

+0.3

+1.1

-1.7

+1.6

1.0

1.0

+2.5

x

1.0

-3.6

Change in King's Sea

106.78

255		5.1	101.7	101.7			
254		7.3	99.5	100.4		-0.9	
253		10.2	96.6	99.1		-2.5	
252		9.0	97.8	97.8			
251 + 25		3.3	103.5	100.0		+3.5	
251		5.4	101.4	99.6		+1.8	
250 + 62		7.2	99.6	99.6			
250		9.2	97.6	98.0		-0.4	
0		9.7	97.4				
	370	100.61					
249		3.7	97.4	97.0		+0.4	
248 + 22		2.7	97.9	96.2		+1.7	
248		4.6	96.0	96.0		0.0	
247 + 21		8.8	91.8	95.2		-3.4	border at left
247		9.3	92.3	95.00		-2.7	
246 + 30		3.9	96.7	95.6		+1.1	
246		4.7	95.9	95.9			grad
245		3.9	96.7	97.15		-0.5	

change in King Liu

100.61

0		2.37	98.24		
	8.00	106.24			
244		5.9	100.3	98.40	+1.99
243+19		6.6	99.6	99.40	+0.2
242		4.4	101.8	99.65	+2.1
242+75		3.1	103.1	99.96	+3.1
242		5.3	100.9	100.9	grade x
241		6.7	99.5		
240		9.0	97.2		
0		8.83	97.41		at Sta 240
	13.0	110.41			
239+50		13.9	96.5		
239		7.5	102.9		
238		5.3	105.1		
237		7.1	103.2		
236		13.1	97.3		
0		13.03	97.38		at 236

boulders at left

Change in King Sun

97.38

857 10595

235 2.8 102.2

234 2.8 103.2

20 0.70 105.25

7.25 112.50

233 7.8 104.7

232 5.5 107.0

231+92 6.8 105.7

+97 9.9 102.6

+77 7.5 105.0

231 7.8 104.7

0 7.67 104.93

6.17 111.00

230 5.0 106.0

0 7.62 103.38

233+40

230+85

229+22

24 Rising on 6% around wash out.

104.83

12.12 116.95

734

1032

733 +50

1062

10.8

733

1092

7.8

1122

4.8

Abandoned

II

T.P. on page 23

103.38

12.95 116.33

779

7.5

108.8

0

0.62

115.71

12.07 127.78

228+50

11.0

116.8

229

4.4

123.4

227+50

1.8

126.0

227

3.7

124.1

226+50

3.0

124.8

226

2.6

125.2

Change in King's

From page 23.

Profile around Washout.

Apr 12th 1907

S.L. of 228+50

	127.78		
225+50		2.8	125.0
225		5.0	122.8
224+50		11.9	115.9
⊙		12.80	114.98
	0.31	115.29	
224+05		6.4	108.9
B.M.		4.97	110.32
223+50		7.5	107.8
+11		14.0	101.3
223		12.0	103.3
⊙		5.76	110.03
	9.47	119.50	
222+50		7.0	112.5
222		7.9	111.6
221+50		9.7	109.8
221		10.4	109.1
⊙		10.27	109.23

Note - This line, from 224+05 to
229, plants around top of perpendicular
earth bank where cottonwood has cut in.

2'R 224+41

Note in oak tree 3' in dia
3' h 223+15

gutch - requires culvert

15'R 222+60

Creek bed at left of line

26.

109.23

1.85 111.08

220+50 6.3 104.8

220 7.1 104.0

219+50 6.1 105.0

0 6.92 104.16

4.97 113.13

219 7.6 105.5

218+50 4.0 109.1

218 6.3 106.8

217+50 5.7 107.4

0 7.90 105.23

5.66 100.89

217 4.4 106.5

216+50 5.2 105.7

216 3.4 107.5

215+50 1.6 109.3

0 0.93 110.06

change in King
Site

King's 220+16 = 220+50

Rocky bank at Right of line

from 220 to 216+50

219+75

4' 2" 216+65

215+15

27

110.06

9.00 119.06

215 79 111.2

214+50 93 110.8

214 92 109.9

213+50 84 110.7

213 61 113.0

212+50 5.0 114.1

0 5.63 113.43

3.64 117.07

212 27 114.4

211+50 56 111.5

211 49 112.2

0 3.58 113.49

10.70 124.19

210+50 14.2 110.0

210+03 14.8 109.4

209+50 13.7 110.5

Change in King Price

25 212+00

Outlet of Gorge from Dechen Tear
(Big bendin.)

on Rock 3' R 211

27 28

124.19

209

124 111.8

0

11.99 112.20

8.98

121.18

208+50

8.7 112.5

208

13.3 107.9

207+50

9.6 111.6

207

11.0 110.2

206+50

10.6 110.6

206

9.0 112.2

205+50

8.7 112.5

0

5.75 115.93

9.02

124.95

205

12.8 112.2

204+50

12.0 113.0

204

11.7 113.3 113.25

203+50

116.75

203

119.75

change
in King line

Rocks at left of line

b'k 208+75

See sketch a huge mass of solid
granite

35' R 205

x
+
0

on Rock.

201 + 85

10 R 200 + 60

29.

124.95

0

8.34

116.61

8.74

125.35

203 + 50

11.3

114.1

203

11.7

113.7

202 + 50

11.8

113.6

202

10.1

115.25

0

10.28

115.07

127.4

127.81

201 + 50

10.8

117.0

+ 10

119.4

8.4

200 + 50

123.01

4.8

0

0.62

127.19

+
5
0

10.86

138.05

200

126.01

18.04

199 + 50

129.01

9.04

199

132.01

6.04

0

29.1

135.14

135.14

12.44 147.58

197 + 50

135.01

12.57

198

11.3

136.3

197 + 50

10.9

136.7

197

10.1

137.5

196 + 50

9.9

137.7

196

9.3

138.3

195 + 50

7.5

140.1

0

6.72

140.86

11.60 152.46

195

13.3

139.2

194 + 50

12.7

139.8

194

13.6

138.9

193 + 72

13.5

139.0

0

12.81

139.65

5.99 145.64

193

5.5

140.1

Change in King Sim

+
0.9

x

x

On F lat

6 P

195 + 50

5 R

193 + 37

145.64

192+50		5.1	140.5
192		5.0	140.6
191+50		4.7	140.9
191		4.1	141.5
190+50		3.8	141.8
190		2.9	142.7
189+65		3.3	142.3
+50		3.5	142.1
0		4.4	141.5
	4.13		145.28
189		4.0	141.3
188+50		4.1	141.2
188		3.9	141.4
187+50		4.2	141.1
187		4.9	140.4
186+50		6.4	138.9
186		6.7	138.6

Change in King Size

On Floor.

Shade at left of road.

182

189

	145.28			
185+50		8.2	137.1	
185		9.5	135.8	
0		9.56	135.72	
	1.35	137.07		
184+50		14	135.7	
184		2.1	135.0	
183+50		17	135.4	
183		3.1	134.0	
182+50		5.6	131.5	
182		4.6	132.5	
181+50		5.0	132.1	129.5
181			126.5	10.6
180+68			124.4	
0		9.70	127.37	
	9.78	136.15		
180+50			123.5	12.7
180		9.7	126.5	

Change in
King Sun

5' L 184+83

Bank at Right
Level at left.

on rock 15' L 180+50

136.15

179+50

9.0 126.2

179

10.0 126.2

178+50

10.9 125.3

0

9.73 126.42

10.52 136.94

9.77 127.22

0.62 136.32

17.30 148.62

0.16 148.46

Change in King Side

on rock

178+50

= Bm on Rock 25' north of fence

= Bm on Rock 1' south of fence under oak

34 Lower line - Dalgona Pinn to Shickler's
Stake marked "V"

3.01 1173.94

1170.93

= T.P. page 54 6' P on Rock 42+10

42+50

1167.0 6.9

+79

1165.3 8.6

43+05

25.9 1148.0

1
0
0

Bottom of gulch

43+30

1162.2 11.7

+50

1161.0 12.9

Huge split rock immediately at right

0

0.41 1162.15 12.20 1161.74

on Rock

43+94

44

1158.0 4.2

+50

1155.0 7.2

45

1152.0 10.2

+50

1149.0 13.2

0

1.08 1150.58 12.65 1149.50

on peg

45+80

46

1146.0 4.6

+50

1143.0 7.6

47

1140.0 10.6

+50

1137.0 13.6

0

1.32 1139.32 12.58 1138.00

on peg

47+64

48

1134.0 5.3

1139.32

48+50

1131.0

8.3

49

1128.0

11.3

1
5
0

0

7.21

1133.97

12.56

1126.76

on Rock

49+13

+50

1125.0

9.0

50

1122.0

12.0

x

0

5.15

1127.57

11.55

1122.42

on Rock

50+02

+50

1120.5

7.1

1
4
0

51

1119.0

8.6

+50

1117.5

10.1

52

1116.0

11.6

0

2.24

1117.56

12.25

1115.32

+50

1114.5

3.1

x

= Sta B of Transit Line

53

1111.5

6.1

0

0.52

1110.57

7.51

1110.05

on Rock

2 1/2 R

53+00

+50

1108.5

2.1

1
8
0

54

1105.5

5.1

+50

1102.5

8.1

1110.57

55 1099.5 11.1

0 124 1099.23 12.58 1097.99

+50 1096.5 2.7

56 1093.5 5.7

+50 1090.5 8.7

57 1087.5 11.7

0 046 1087.69 12.00 1087.23

+50 1084.5 3.2

58 1081.5 6.2

0 9.13 1081.22 9.60 1079.09

+50 1081.5 6.7

+81 1081.5 6.7

0 153 1080.82 8.93 1079.29

59 1080.4 0.4

+50 1077.4 3.4

60 1074.4 6.4

+50 1071.4 9.4

V. Sin -

on peg 55+27

.19
11.4

on peg 7' IP 57+90

x = Vert V Sta 5

on peg 10' R 58+85

37.

V Sim

108092

60+75

10714

9.4

x

61+17

5.7

1075.1

10714

9.4

+3.7

0

Sharp bend in gulch

+50

10714

9.4

x

62

10684

12.4

0

292

1070.80

1294

1067.88

on Rock + L

62+29

+50

1065.4

5.4

1

5

0

63

1062.4

8.4

+50

1059.4

11.4

0

109

1059.29

12.61

1058.19

on Peg

63+85

64

1056.4

2.9

+50

1053.4

5.9

65

1053.4

5.9

0

0

x

Gulch

+50

1050.4

8.9

66

1047.4

11.9

0

0.50

1047.02

12.76

1046.52

on peg

65+90

+50

1044.4

2.6

1

5

0

67

1041.4

5.6

1047.02

67+50					1038.4	8.6	
0	2.33	1037.89	1146	1035.56			
68					1055.4	2.5	
+50					1032.4	5.5	
69			7.5	1030.4	1029.4	8.5	+1.0
+23			6.7	1031.2	1028.0	9.9	+3.2
+50			7.6	1030.3	1026.4	11.5	+3.9
0	144	1079.02	1031	1027.58			
70			8.7	1020.3	1023.4	5.6	-3.1
+20			6.4	1022.6	1022.2	6.8	+0.4
+50			6.9	1022.1	1020.4	8.6	+1.7
71					1017.4	11.6	
0	101	1017.07	12.96	1016.06			
+50					1014.4	2.7	
72					1011.4	5.7	
+50					1008.4	8.7	
73					1005.4	11.7	

✓ Sum

on peg.

67+72

1.00

on Rock

15' P

69+50

Big Boulder immediately at right

on Rock

6' P

71+19

1017.07

73 1.60 1006.70 1197 1005.10

73 + 50

1002.4 4.3

74

999.4 7.3

+6.0

+ 50

996.4 10.3

= Dur ✓ Sta 19

en peg 73+37

75 630 1000.49 12.51 994.19

75

993.4 7.1

5R en peg 74+55

76 594 995.44 10.99 989.50

+50

990.4 5.0

en peg 75+44

76

987.4 8.0

Disintegrated T loose rock

+50

984.4 11.0

77

981.4 14.0

78 154 984.85 12.43 983.01

+50

978.4 6.5

en peg 77+55

78

975.4 9.5

+50

972.4 12.5

79

969.4 15.5

		984.85		
o	1.38	974.01	12.22	972.63
79+50				968.4
80				963.4
+50		5.1	968.9	961.1
o	4.15	973.51	4.65	969.36
+75		6.3	967.2	959.9
o	0.81	963.95	10.37	963.14
81			10.3.6	960.4
82+15			10.5	953.5
				953.5
o	10.72	971.78	2.89	961.06
+50			6.2	965.6
+85			9.7	962.1
83			10.5	961.2
o	15.8	967.64		961.06
82+50				951.3
o	1.82	953.00	11.46	951.18

963.4
 3
 960.4
 7
 909.7

1
 0
 0

x
 +7.8

1
 F
 0
 +7.3

1
 0
 0

11.3

V. S. in

on peg 79+23

on Rock 90+42

on Rock + L' 81+22

+1.6 note - Bottom of gulch = 81+70
 This point is 25' below grade; the top
 of the benches are 10' below grade

on peg 82+48

82+48

on Rock 92+87

953.00

✓ Sine

83				948.3	4.7			
+50				945.3	7.7			
94				942.3	10.7			
0	364	944.74	11.90	941.10				
+50				939.3	5.4			on Rock 84+50
85+04				939.2	5.4			
+50				936.6	8.1			Above H Big Boulder.
86				933.6	11.1			
0	891	941.90	11.75	937.99				
85+50				936.1	5.8			on rock 86+03
86			82	933.7	9.3	+11.0		
+28			135	928.4	930.6	11.3	-7.6	
0	062	933.61		937.99				
+46				906.4				only approximately
+90				926.3	7.3			
87+38				899.3				only approximately
87+75			11.3	927.3	920.3	13.3		

Auxiliary Line Around Down
side Washes.

✓ Line

	12.80	945.80	937.99		See Book 2 to change of line.	
85 +50			7.9	942.9	938.1	4.8
86			1.5	944.3	936.8	+ 7.5
+50			4.7	941.1	935.5	+ 5.6
86 +80			2.7	928.1	934.8	Bottom of gulch no 1
87 +10			4.3	941.5	934.0	27.5 narrow ridge
0	2.00	935.52	12.28	933.52		
+18				937.5	933.7	= one of Ward's steps
+35			6.6	928.9	932.4	Bottom of gulch no 2
+47			7.8	927.7	933.1	Bottom of gulch no 3
+60			0.7	934.8	932.7	grade
88			2.2	933.3	931.7	grade
+37			2.9	937.6	930.7	+1.9
+59			17.6	917.9	930.2	Bottom of gulch no 4
+77			5.0	930.5	929.7	grade
89			7.2	928.3	929.1	grade
+56			7.8	927.7	927.7	= Ward's steps

935.52

89+71

13.0

922.5

= 87+75 on 12% Sim

0

H.38

932.37

7.58

927.94

on peg

89+56

Remaining 9 1/2% hire

Sum 9

932.37

88

6.6

925.7

= 89+31

+50

5.0

928.2

= 90+31

89

11.6

920.7

920.7

1/50

+0.5 = 90+5.1

0

0.48

920.24

12.56

919.76

on peg

89+06

+55

18.8

901.4

= 91+26

Bottom of gulch

90

914.2

6.0

= 91+81

92

4.5

915.7

913.1

+26

+75

5.0

915.7

+50

8.7

912.0

910.1

10.1

+19

93

907.1

13.1

on peg

92+85

0

1.86

909.50

12.60

907.64

+50

904.1

5.2

90950

94

901.1

84

+50

898.1

114

-6.0

0

1.88 898.99 1240 897.10

en pag

94+56

95

895.1

3.9

+50

892.1

6.9

96

889.1

9.9

+50

886.1

12.9

0

1.09 887.43 1265 886.33

1.4

en pag

96+50

97

883.1

4.3

+50

880.1

7.3

98

877.1

10.3

+50

874.1

13.3

0

1.08 876.13 1237 875.05

en pag

98+32

99

871.1

5.0

+50

868.1

8.0

100

865.1

11.0

0

5.22 869.75 1260 863.53

10.1 P

en pag

99+85

✓ Sino

868.75

100+50

862.1

6.7

101

859.1

9.7

+50

856.1

12.7

0 0.40 856.77 12.38 856.37

+55.5

on peg

101+75

= 3 wire fence

102

853.1

3.7

+50

850.1

6.7

103

847.1

9.7

+50

844.1

12.7

0 0.26 845.16 11.97 844.50

2' P

on peg

102+50

104

841.1

4.1

+50

836.1

7.1

105

835.1

10.1

+50

832.1

13.1

0 2.44 835.26 12.34 832.82

4' L

on peg

105+50

106

829.1

6.2

+50

826.1

9.2

835.26

107				823.1	12.2		
0	0.83	823.82	12.7	822.99		on peg	107+0.7
+50				820.1	2.7		
108				817.1	6.7		
+50				814.1	9.7	1.5 0	
109				811.1	12.7		
0	1.37	812.77	12.42	811.40		on peg	109+10
+50				806.1	4.7		
110				805.1	7.7		
+50				802.1	10.7		
0	0.43	802.63	10.57	802.20			110+50
111				799.1	3.5		
+50		4.8	797.8	797.5	5.1	+0.3	
112		4.4	798.2	795.8	6.8	+2.4	
+50		3.5	799.1	794.2	8.4	+4.9	
113		7.1	795.5	793.6	10.0	+2.9	
+30		10.8	791.8	791.6	11.0		

County Road.

10263

928 793.35

x

Grade Stakes for Johnson.
(Sawing road)

6.67 1246.97 1240.3

29+50 2.0 1245.0 1245.0

30 5.0 1242.0 1242.0

+50 5.9 1241.1 1239.0

31 6.7 1240.3 1236.0

+50 8.7 1238.3 1233.0

+75 9.6 1237.4 1231.5

32 1230.0

0 1.77 1237.67 1.07 1236.90

+50 4.1 1232.8 1227.0

+75 6.6 1231.1 1225.5

33 8.4 1229.3 1224.0

+25 10.2 1222.5

+50 10.5 1227.2 1221.0

Grade Stakes for
Sawing Road.

on peg

113+26

Apr. 15th 1907

= Ground at Sta. 31+00

grade W. Hestie

" Watson

+21 Lake

+4.3 Birch

+5.3

+5.9

+5.8

+5.3 1230.8 = old elev. 0.3 discrepancy

+5.3

+4.6

+6.2

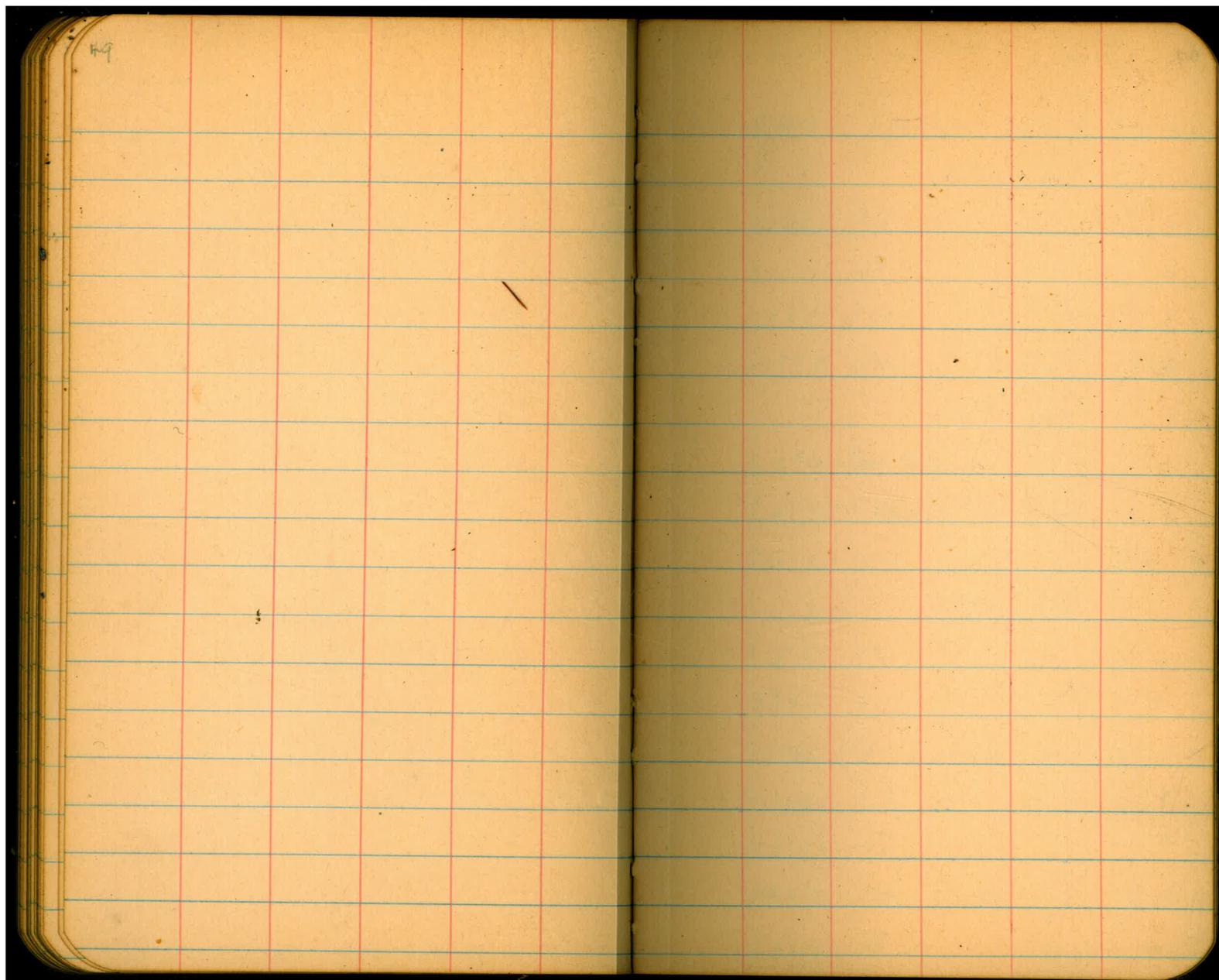
Grade Taken for
Sawing Road.

48

1237.67

34			125	12252	12150	+7.2
0	155	1226.57	1265	122502		
+55			2.8	1228.8	1216.8	+7.3
+50			4.1	1222.8	1215.0	+7.5
35			6.8	1219.8	1212.0	+7.8
+50			8.5	1217.8	1209.0	+8.8
0	228	1216.37	1248	1214.09		
+50					1204.0	7.4
36					1206.0	10.4
+50					1203.0	13.4
0	156	1206.05	1188	1204.49		
37					1200	6.1
+70					1195.8	10.3
38 +70			12.1	1194.0	1192.8	13.3

on Rock Kill mark
1 foot discrepancy.



So. Levels for Profile of Road from
"C" line

Sta	0		1400.00	
	1.66	1401.66		
1			3.8	1397.9
2			7.6	1394.1
3			13.8	1387.9
⊙			12.76	1389.0
	0.26	1389.16		
4			6.5	1382.7
5			12.5	1376.7
⊙			12.73	1376.43
	0.58	1377.01		
6			5.7	1371.3
7			11.4	1365.6
⊙	1.06	1365.20	12.87	1364.14
8			3.8	1361.4
9			8.6	1356.6
⊙	1.18	1353.57	12.81	1352.39
10			3.5	1350.1

Dulzina Pass into Shickel Valley

Apr. 18-1907

to 23

Assumed elev. of intersection with County Road

5' w 280

Condition Excellent

Minor only to be brushed out

4' w 506

7+35

9+65

135357

11			8.7	13449	
+30			11.4	13422	
12			14.0	13396	
0	0.19	1341.00	12.76	1340.91	
13			7.6	1333.4	
14			13.0	13280	
0	1.43	1329.91	12.52	13284.8	13+95
15			7.0	1322.9	
16			12.8	1317.1	
0	0.33	1317.34	12.90	1317.01	16+00
+85			6.2	1311.1	
17+50			8.4	1308.9	
18+25			12.6	1304.7	
0	0.35	1304.93	12.76	1304.58	19+32
19			3.0	1301.9	
20			9.1	1295.8	
21			14.1	1290.8	

e sin

130493

0	0.03	1292.13	1273	1292.10		
---	------	---------	------	---------	--	--

21+25

22			6.4	1285.7		
----	--	--	-----	--------	--	--

+75			10.3	1281.8		
-----	--	--	------	--------	--	--

0	1.05	1280.43	1275	1279.38		
---	------	---------	------	---------	--	--

23+25

23+75			4.1	1276.3		
-------	--	--	-----	--------	--	--

24+50			8.8	1271.6		
-------	--	--	-----	--------	--	--

25			11.3	1269.1		
----	--	--	------	--------	--	--

0	144	1268.98	1289	1267.54		
---	-----	---------	------	---------	--	--

disintegrated

25+13

26			4.9	1264.1		
----	--	--	-----	--------	--	--

27			11.2	1257.8		
----	--	--	------	--------	--	--

0	0.69	1256.99	1268	1256.30		
---	------	---------	------	---------	--	--

27+30

28			5.1	1251.9		
----	--	--	-----	--------	--	--

29			9.2	1247.8	1248	
----	--	--	-----	--------	------	--

+50			12.2	1244.8	1245	
-----	--	--	------	--------	------	--

0	2.83	1247.19	1263	1244.36		
---	------	---------	------	---------	--	--

29+70

30			3.8	1243.4	1242	
----	--	--	-----	--------	------	--

+14

1
5
0

31			6.9	1240.8	1236	
----	--	--	-----	--------	------	--

+4.8

e line

		1247.19					
31+75			10.1	1237.1	1231.5	+5.6	
o	0.28	1234.70	12.77	1234.42			32+25
32+75			39	1230.8		+5.3	
33+25			7.6	1227.1		+4.6	
34			10.0	1224.7		+6.7	
+25			11.4	1223.3		+6.8	
o	0.90	1222.88	12.62	1222.08			34+50
35			3.3	1219.6		+7.6	
36			7.6	1215.3		+9.3	
37			11.8	1211.1	1200.00	+11.1	
o			11.70	1211.18			Slow!
				1222.08			
	0.85	1222.93					
o			11.50	1211.18			
	1.35	1212.48					
37+15			1.3	1211.2			
o 37+25			12.93	1199.55	1200.00		

1734.42
840
1478.2
144.2

	1.67	1201.22		1199.55		
37+35			7.2	1193.0		
+45			11.6	1189.6		
⊙	2.50	1191.50	12.22	1189.00		
+75			7.0	1184.5		
+95			12.2	1179.3		
⊙	4.51	1195.50	0.51	1190.99		
38+20				1192.8	2.7	
+50				1191.0	4.5	South + loose rocks
39				1188.0	7.5	
+50				1185.0	10.5	1 5 0
40				1182.0	13.5	gully
⊙	0.29	1183.43	12.36	1183.14		40+00
+50				1179.0	4.4	In gully
41				1176.0	7.4	
+50				1173.0	10.4	
42				1170.0	13.4	
⊙	4.27	1175.20	12.50	1170.93		6 R on Rock 42+10

C. Sim

1175.20

42 +50 6.1 1169.1

+80 9.0 1166.2

43 21.0 1154.2

Bottom of Wash

+75 7.3 1167.9

+50 8.4 1166.8

Boulders shown about prominently

44 14.5 1160.7

0 2.68 1165.23 1265 1162.55

5' 114+00

+50 7.2 1158.0

45 9.0 1156.2

+50 9.9 1155.4

46 12.0 1153.2

0 4.90 1159.74 1039 1154.84

+50 8.0 1151.7

47 9.0 1150.7

+50 10.0 1149.7

48 10.0 1149.7

+50 10.2 1149.5

		1159.74		
49			94	1150.3
0	383	1154.27	930	1150.44
+50			8.2	1146.1
50			2.6	1151.7
+50			39	1150.4
51			6.6	1147.7
0	274	1149.69	732	1146.95
+50			4.6	1145.1
52			4.1	1145.6
+50			9.5	1140.2
53			15.0	1134.7
+50			14.8	1134.9
+93			13.9	1135.9
54+29			8.9	1140.9
0	138	1138.23	1284	1136.85
+65			73	1135.9
55			61	1132.1

Loose Rock + Plant

49+00

51+00

Found slate on rock BM no 107/6193

6' R 50+96

Follows Ward's line

= 54 + 56 Ward's line

Top of Ridge

4' R 54+60

1138.23

55+50			96	1128.6
56			13.5	1124.7
0	148	1128.42	1129	1126.94
+30			10.6	1117.8
+46			4.6	1123.8
+50			4.2	1124.2
+90			6.0	1122.4
57+37			44	1124.0
0	463	1128.61	444	1123.98
58			6.3	1122.3
+50			9.1	1119.5
59			12.2	1116.4
0	1.03	1118.09	1155	1117.06
+50			47	1113.4
60			11.8	1106.3
0	261	1109.01	11.69	1106.40
+50			64	1102.6

3'R 55+80

Bottom of Draw
= 57 of Ward's line

Note - Line changed from

56+50 to 61+43

3'R 57+27

on Stake 59+00

on Jump 60+15

		1109.01		
S	60+90		9.4	1099.6
	61+05		16.1	1092.9
	+43		10.0	1099.0
	62		12.1	1096.9
	B.M		12.59	1096.42
		1.36		1097.78
	63		7.5	1090.3
	+50		9.0	1088.8
	64		13.1	1084.7
	⊙	1.11	1086.15	12.74
	+50		3.7	1082.5
	65		4.2	1082.0
	+50		7.2	1079.0
	66		6.1	1080.1
	⊙	1.60	1079.47	8.28
	+50		8.6	1070.9
	+67		5.5	1074.0

e. Sum

Bottom of Draw

Sum follows Ward's Stake position again

on Stake 10' h 62+63

1090

1088

1086

on rock H.L

64+15

gully with shoulders

peg.

66+20

Draw.

1079.47

67 8.1 1071.4

+50 12.1 1067.4

68 15.4 1064.1

0 5.33 1073.00 11.50 1067.67

+50 7.1 1065.9

69 7.6 1064.4

+50 6.8 1066.2

70 7.1 1065.9

+50 7.5 1065.5

0 9.29 1074.85 7.44 1065.56

71 9.5 1065.4

+50 6.6 1068.3

72 6.8 1065.1 1068.1

0 12.78 1065.90 1.73 1073.12

+50 1071.1 14.8

73 1074.1 11.8

+50 1077.1 8.8

on rock

68+43

Broad Saddle

Earth + Boulders

page

3:11

70+60

*

on Rock 4' R

72+30

Abandoned
See page 66

+5.0

107590

74				10803	58
o	1263	1096.58	195	1083.95	
+50			128	1083.8	
75			11.1	1085.5	
+50			86	1088.0	
76			4.8	1091.8	
+50			36	1093.0	
o	8.11	1101.82	287	1093.71	
77			49	1096.9	
+09			45	1097.3	
+50				1093.4	8.4
78				1089.9	11.9
o	215	1091.54	1243	1089.39	
+50				1086.4	5.1
79				1082.9	8.6
+50				1079.4	12.1
o	398	1083.21	1231	1079.23	

e Surr

on Rock 4' R 74+20

on pag 76+60

Saddle: will stand 5' cur.

Drawing with details

on pag 3' L 79+90

1083.21

80

1075.9

7.3

+50

1072.4

10.8

$\frac{1}{0}$

81

1.68

1072.53

12.36

1070.85

1068.9

3.6

Disintegrated

on Rock "R"

80+65

+50

1065.4

7.1

82

1061.9

10.6

x

8

395

1063.94

12.54

1059.99

82+47

+50

3.4

+77

3.4

1060.5

x

Hogback, above koulder

83

1058.9

5.0

$\frac{1}{0}$

+50

1055.4

8.5

x

84

7.8

1056.1

1051.9

12.0

+50

7.8

1056.1

x

85

1054.6

9.3

+50

1053.1

10.8

$\frac{1}{0}$

Same - low koulder, all right

86

1051.6

12.3

8

0.70

1052.84

11.50

1052.14

86+50

105284

86+50

1050.1 2.7

1
0
0

87

1048.6 4.2

+50

1047.1 5.7

Saddle - big boulder at right.

88

1045.6 7.2

x

o

153

1047.50 6.87 1045.97

on Rock 4R 88+15

+50

1042.1 5.4

89

1038.6 9.9

1
0

+50

1035.1 12.4

Loose boulders

o

216

1037.44 12.22 1035.28

on Rock 89+50

90

1031.6 5.8

+50

1028.1 9.3

91

1024.6 12.8

o

255

1027.74 12.25 1025.19

on Rock 91+25

+50

1021.1 6.6

92

1017.6 10.1

+50

1014.1 13.6

o

066

1015.53 12.87 1014.87

on Rock 92+50

1015.53

93				1010.6	4.9
+40				1007.8	7.7
+50				1007.1	8.4
94				1003.6	11.9

0	2.05	1005.19	12.39	1003.14	
---	------	---------	-------	---------	--

+50				1000.1	5.1
-----	--	--	--	--------	-----

95				996.6	8.6
----	--	--	--	-------	-----

+50				993.1	12.1
-----	--	--	--	-------	------

0	0.80	993.16	12.83	992.36	
---	------	--------	-------	--------	--

96				989.6	3.6
----	--	--	--	-------	-----

+50				986.1	7.1
-----	--	--	--	-------	-----

97				982.6	10.6
----	--	--	--	-------	------

0	0.20	981.38	11.98	981.18	
---	------	--------	-------	--------	--

+50				979.1	2.3
-----	--	--	--	-------	-----

98				975.6	5.8
----	--	--	--	-------	-----

+50				972.1	9.3
-----	--	--	--	-------	-----

99				968.6	12.8
----	--	--	--	-------	------

c. 500

on rock 3' L 94+35

loose boulders + disintegrated

on rock 95+50

on peg 8' L 97+20

981.38

0	0.00	968.83	12.55	968.83
---	------	--------	-------	--------

99+00

99+50

965.1 3.7

Flux at 99+12

100

961.6 7.2

Scalloping Boulder

+50

958.1 10.7

0	1.04	957.52	12.35	956.48
---	------	--------	-------	--------

on peg

100+73

101

954.6 2.9

+50

951.1 6.4

102

947.6 9.9

0	3.57	948.94	12.15	945.37
---	------	--------	-------	--------

on Rock 15'R

102+15

+50

944.1 4.8

103

940.6 8.3

+50

937.1 11.8

Boulders + Disturbed

0	1.19	938.10	12.03	936.91
---	------	--------	-------	--------

on Rock 4'L

104+00

104

933.6 4.5

+50

930.1 9.0

105

926.6 11.5

0	0.33	915.95	12.48	925.62
---	------	--------	-------	--------

on peg

105+45

97595

105 +50

973.1

2.9

106

919.6

6.4

+50

916.1

9.9

107

912.6

13.4

0

1290 913.05

on peg

107+48

66

Branch line Paralleling Ward's line
"D" line

	1.60	1074.72		1073.12	
73			9.5	1065.2	
+50			18.1	1056.6	
74			11.1	1063.6	
+24			12.0	1062.7	
○	0.70	1062.09	12.33	1062.39	
+50				1060.9	2.2
75				1057.4	5.7
+50				1053.9	9.2
76				1050.4	12.7
○	12.23	1052.04	12.27	1050.82	
+50				1046.9	5.1
77				1043.4	9.6
+50				1039.9	12.1
○	37.6	1042.91	12.99	1039.15	
78				1036.4	6.5
+27				1036.4	6.5
+50				1036.4	6.5

Tying on "C" line at Sta 72+50

= T.P. on page 59

Very Bottom of Rocky gulch
Saddle.

x

Drainage grade Sill + Sarge loose Boulder

on Rock S'R 74+28

on Rocks 76+50

on pg 77+57

Sharp Bend in Draw

104291

79

+50

10329

10.0

-

1079.4

13.5

7.0

0

046

1030.38

1299

10299.2

80

+50

1025.9

4.5

1072.4

8.0

x Immense Boulder at base

0

541

1074.94

1085

1019.53

on rock

80 + 7.0

+85

16.5

1008.4

Very Bottom of Wash.

81 + 05

9.0

1015.9

+50

8.0

1016.9

Round ridge

+75

13.2

1011.7

Bottom of Draw

82

10.0

1014.9

+50

7.1

1017.8

Top of Rounded Ridge

+95

9.3

1015.6

Brink of Canon (west side)

0

612

1073.46

7.60

1017.34

on peg

82 + 85

83 + 15

23' lower than Brink

Bottom of Canon

+50

5.0

1018.5

x

(East side)

0

13.27

1034.87

186

1021.60

on rock

10' W

82 + 85

Stakes Marked E

Auxiliary line Around Cañon, commencing at 82+00
1034.87

82+50	12.1	1022.8
83	10.0	1024.9
+30	8.2	1026.7
+76	6.0	1028.9
84	4.7	1030.2
+33	5.0	1029.9
+65	10.2	1024.7

Running D line at 83+50

571 1023.05 1017.34

84		1016.5	6.6	
+50		1014.5	8.6	
85		1012.5	10.6	
+50		1010.5	12.6	
0	17.1	1012.72	12.04	1011.01
86		1007.0	5.7	
+50		1003.5	9.2	
0	36.8	1007.34	9.06	1003.66

D line

High point bet. 2 Boulders

Vert Sta 5

= T.P. on page 67

1
0

Pass bet. 2 Boulders

1
7
0

on Post

76+70

1007.34

87

+50

+95

o

142

996.34

1242

994.92

88+50

89

+50

o

335

999.76

993

986.41

90

+50

o

369

980.73

1272

977.04

91

+50

92

o

4.15

972.97

1191

968.82

+50

93

1000.0

996.5

996.5

992.6

989.1

985.6

982.1

978.6

975.1

971.6

968.1

964.6

961.1

7.3

10.8

10.8

3.7

7.2

10.7

7.7

11.2

5.6

9.1

12.6

8.4

11.9

D line

Approximate level to

which a bunch of rocks can

be built into a table. 88+10

how Boulder at night.

on Rock 6 R

89+55

on Peg

90+62

Klatish Wash

97297

0 0.86 961.43 1240 960.57

93+50 957.6 3.8

94 954.1 7.3

+50 950.6 10.8

95 947.1 14.3

0 121 950.33 1231 949.12

+50 943.6 6.7

96 940.1 10.2

+50 936.6 13.7

0 0.68 938.24 1277 937.56

97 933.1 5.1

+50 929.6 8.6

98 926.1 12.1

0 0.34 926.36 1272 926.02

+50 923.6 3.8

99 919.1 7.3

+50 915.6 10.8

in pag

93+05

1
0

on rock

95+12

Behind Big Boulder

in rock 6' L 97+30

just below roof of Boulder.

3 wire fence

in pag

98+05

Merges with Ward's line here

x

976.26

0	174	915.40	1270	913.66
100			36	911.8
+50			49	910.5
101			78	907.6
+50			16.8	898.6
10+55			17.8	897.6
102			123	903.1

on req. 99+75

Bottom of Gully

0	0.77	904.55	1162	903.78
+50			36	901.0
103			81	895.8
+16			149	889.7
+50			118	892.8
104			133	891.3

on req. 102+105

Bottom of gully

0	102	893.74	1233	892.52
+50			5.0	888.2
105			6.6	886.6
+50			10.0	883.2

on req. 103+94

993.24

106			12.3	880.9
0	253	993.52	12.25	880.99
+50			4.7	878.8
107			6.9	876.6
+50			14.1	869.4
108			12.9	870.6
0	101	871.72	12.81	870.71
+50			3.9	867.8
109			6.7	865.0
+50			9.0	863.7
+72			8.7	863.0
110			11.8	859.9
0	144	860.53	12.63	859.09
+50			4.4	856.1
+50			13.5	847.0
111			5.5	855.0
+50			8.2	852.3

on peg.

106+0.9

guleh

on peg

107+0.6

Flax ridge

on peg.

110+1.5

guleh

860.53

0 3.11 850.73 1291 847.62

on Peg.

111 + 93

112 8.2 842.5

+06 11.1 839.6

guleh

+50 14.6 846.1

113 6.2 844.5

+50 11.6 839.1

114 11.2 839.5

+50 13.7 837.0

0 1.87 839.73 1287 837.86

on peg.

114 + 37

115 5.7 834.0

+50 10.2 829.5

116 11.3 828.4

+04 11.5 828.2

= Wards 114

0 1.86 829.49 1210 827.63

on Peg. H.P.

116 + 06

+50 3.0 826.5

117 6.2 823.3

+50 11.2 819.3

74

929.49

118			11.9	817.6
+50			14.3	815.2
0	0.40	817.02	12.87	816.62
119			4.1	812.9
+50			6.8	810.2
120			9.8	807.2
+50			12.8	804.2
0	0.52	805.07	12.47	804.55
121			2.8	802.3
+50			7.4	797.7
122			7.2	797.9
+50			8.3	796.8
123			13.6	791.5
0	0.90	793.84	12.13	792.94
+50			5.3	788.5
124			7.6	786.2
+50			10.7	783.1

D Sun

on Post 118+77

on peg 4.2 120+55

on peg 122+91

793.84

125			13.2	780.6
0	131	782.26	17.89	780.95
+50			3.5	778.9
126			5.7	775.6
+50			9.6	772.7
127			10.3	772.0
+50			13.3	769.0
0	046	770.30	12.42	769.84
128			2.6	766.7
+50			6.9	762.4
129			8.6	761.7
+50			9.6	760.7
130			12.4	757.9
0	246	760.32	12.44	757.86
+50			6.0	754.3
+90			8.2	752.1
131			9.1	751.2

"D" line

on page

124+95

in Sweet Water

Along Sheeklers River

on page

127+40

on page

130+00

crossed "A" line (constructed)

760.32

131 + 50		17.2	748.1
0	8.30	751.56	12.06 748.26
132		5.0	746.6
+ 32		5.0	746.6
+ 50		4.9	746.7
133		4.8	746.8
+ 20		6.6	745.0
+ 30		9.1	742.5
+ 45		5.1	746.5
+ 50		5.0	746.6
134		4.0	747.6
+ 50		2.7	747.9
135		4.9	746.7
+ 50		6.5	745.1
136		6.7	744.9
0	4.71	749.21	7.06 744.50
+ 50		3.4	745.8

on peg

131 + 50

3 wire fence

quitch

Grain Field

49

136 + 00

77

749.21

137

5.0

744.2

+07

3 wire fence

+70

9.7

739.5

0

044

963

739.58

cupg.

137+70

6

"D" Sun

TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100.00	0.44	100.00	0.87	99.99	1.31	89
1	99.98	1.75	99.98	2.18	99.97	2.62	99.95	3.05	88
2	99.94	3.49	99.92	3.93	99.91	4.36	99.88	4.80	87
3	99.86	5.23	99.84	5.67	99.81	6.10	99.79	6.54	86
4	99.76	6.98	99.73	7.41	99.69	7.85	99.66	8.28	85
5	99.62	8.72	99.58	9.15	99.54	9.58	99.50	10.02	84
6	99.45	10.45	99.41	10.89	99.36	11.32	99.31	11.75	83
7	99.25	12.19	99.20	12.62	99.14	13.05	99.09	13.49	82
8	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	15.64	98.70	16.07	98.63	16.50	98.56	16.93	80
10	98.48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98.16	19.08	98.08	19.51	97.99	19.94	97.90	20.36	78
12	97.81	20.79	97.72	21.22	97.63	21.64	97.53	22.07	77
13	97.44	22.60	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	24.19	96.92	24.62	96.81	25.04	96.70	25.46	75
15	96.59	25.88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	27.56	96.00	27.98	95.88	28.40	95.76	28.52	73
17	95.63	29.24	95.50	29.65	95.37	30.07	95.24	30.49	72
18	95.11	30.90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35.43	69
21	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.66	68
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38.67	67
23	92.05	39.07	91.88	39.47	91.71	39.87	91.53	40.27	66
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	43.84	89.69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	46.95	88.09	47.33	87.88	47.72	87.67	48.10	61
29	87.46	48.48	87.25	48.86	87.04	49.24	86.82	49.62	60
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	52.99	84.57	53.36	84.34	53.73	84.10	54.10	57
33	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	60.18	79.60	60.53	79.34	60.88	79.07	61.22	52
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	45
45	70.71	70.71							44
Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees.
	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		

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