

Sutherland + San Vicente
Conduit Level Notes.

? Bench Marks

Profile Levels

on Line Changes

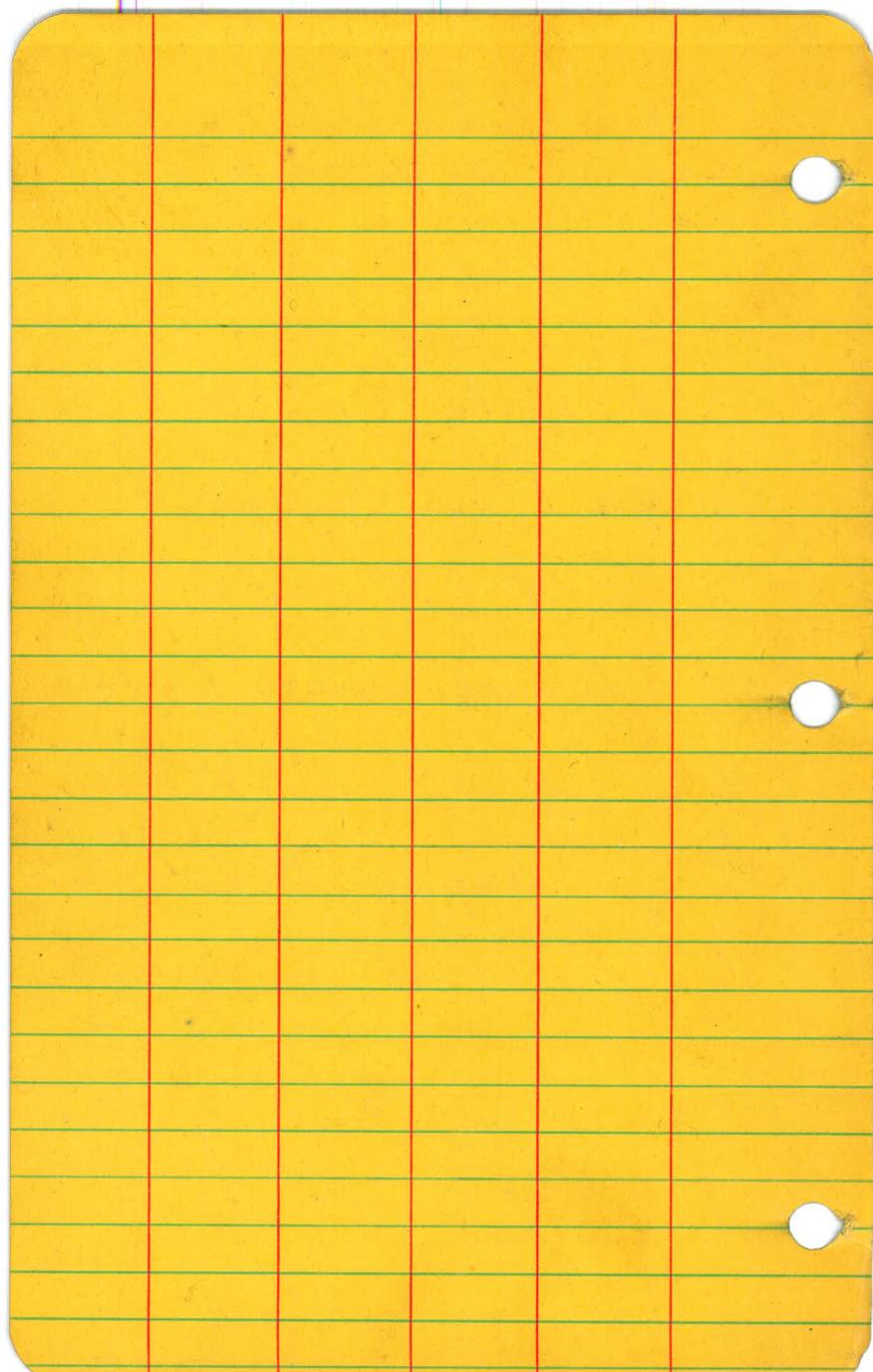
on P. Line - + H. Line

L. Sta. 440+24.74 to 493+9^N

H. " N. Portal ^{over tunnel.} Tunnel to S. Portal

P. " 226+28.55 to 323+37.42

P. " 625+42.09 to 649+48



1
Dec. 13, 1927

Simpson

Bailey

Goodbody

Profile Levels over tunnel
Line starting at North
Portal and going to South
Portal

H Line

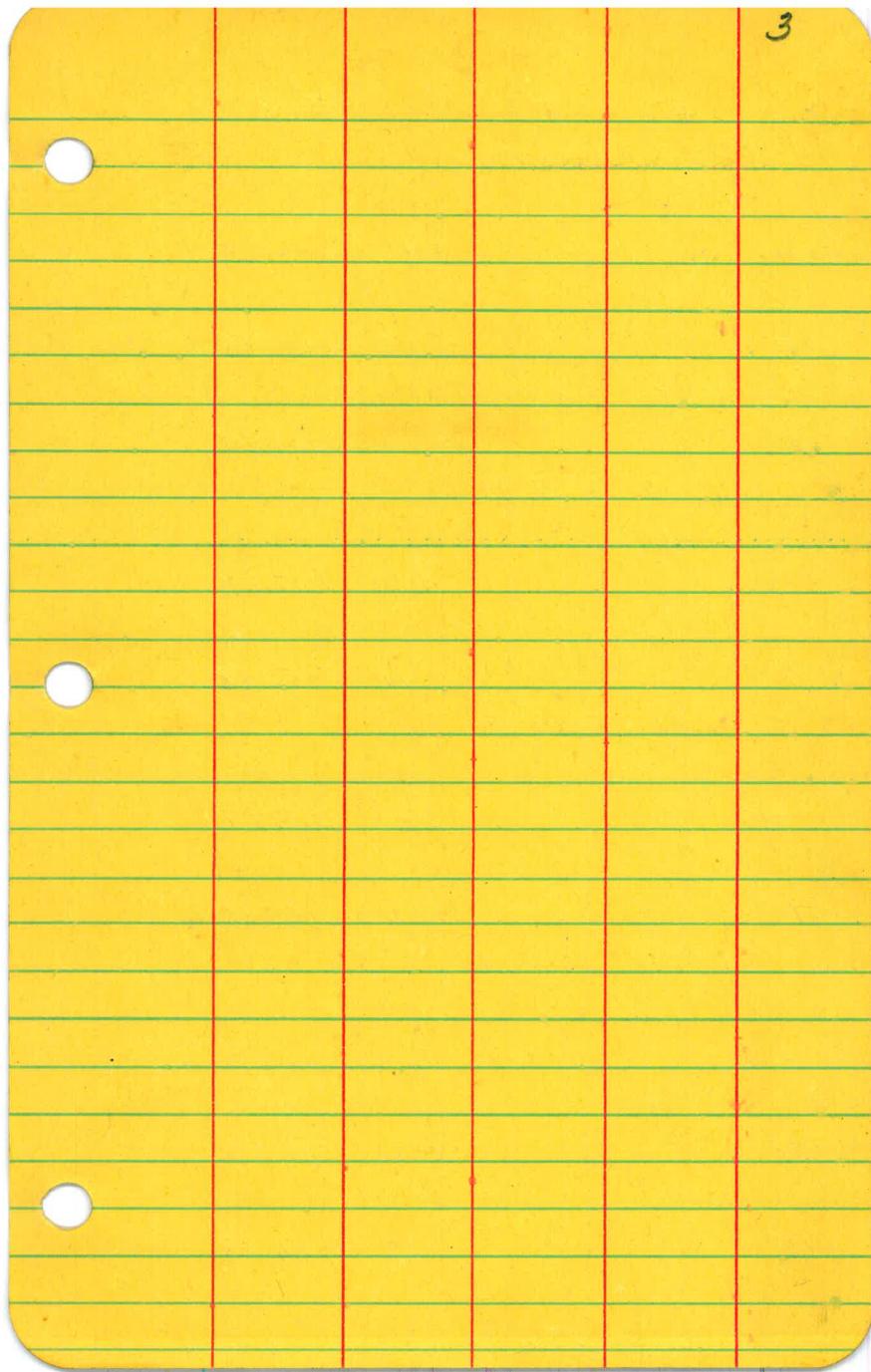
| Sta | + | - | Elev. |
|--------|-----------------------------|---------|--------------------|
| | | | 1936.10 = B.M. #16 |
| | 0.26 | 1936.36 | |
| | | 12.70 | 1923.66 |
| | 0.44 | 1924.10 | |
| | | 12.37 | 1911.73 |
| | 0.60 | 1912.33 | |
| 143+50 | ⁵⁶ Tunnel Portal | 19.7 | 1892.6 |
| T.F. | | 0.68 | 1911.65 |
| | 11.81 | 1923.46 | |
| 144+00 | | 10.7 | 1912.8 |
| T.F. | | 0.34 | 1923.12 |
| | 12.24 | 1935.36 | |
| +50 | | 7.1 | 1928.3 |
| T.F. | | 0.15 | 1935.21 |
| | 13.09 | 1948.30 | |
| 145+00 | | 3.9 | 1944.4 |
| T.F. | | 0.23 | 1948.07 |

(Starting from) S.D. B.M. #16
Nail in Oak Tree, about 35' Left of
Old Sta 143+50 (Doc. Copied)
Near North Portal of Tunnel.

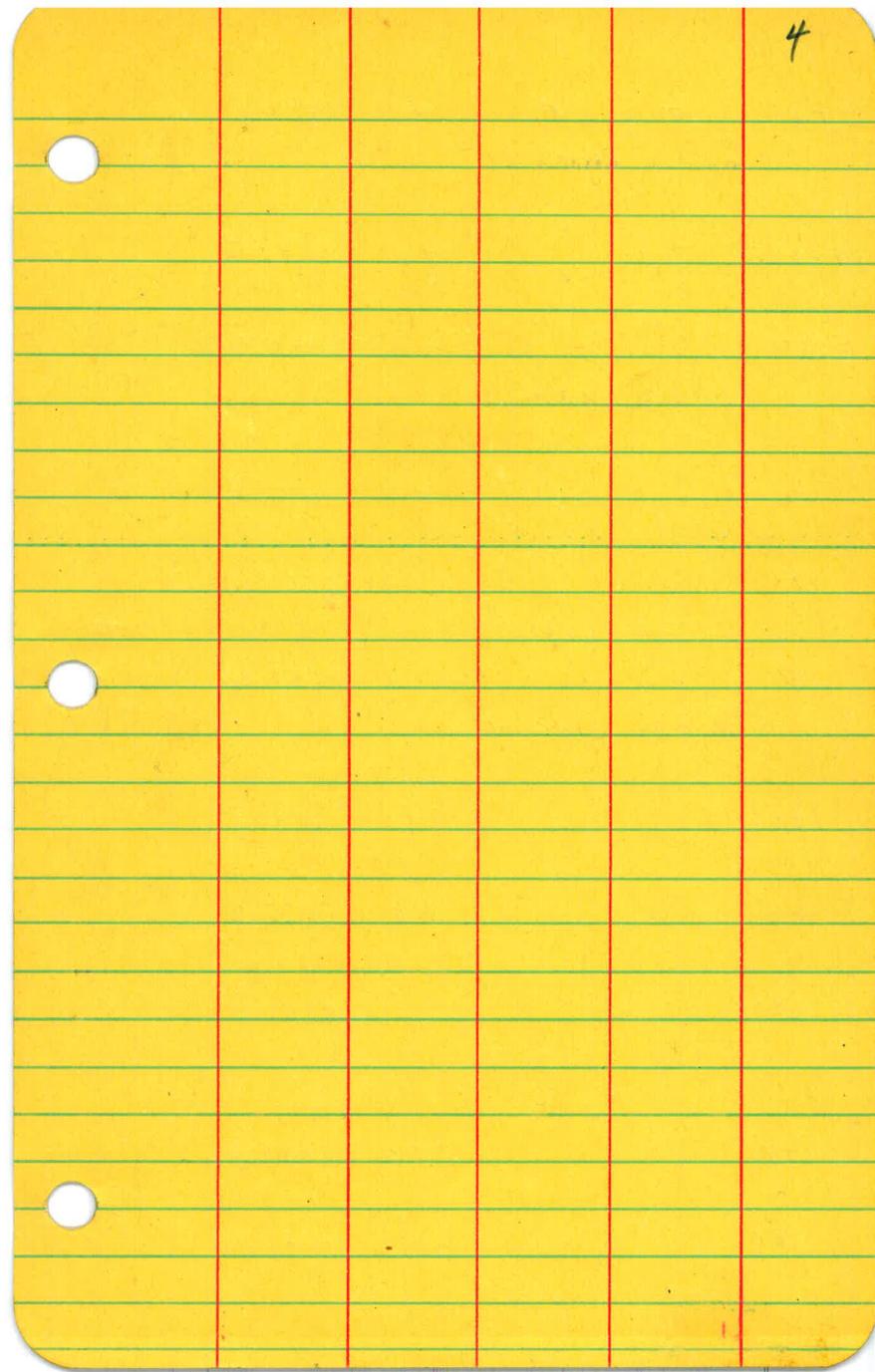
New Nail in Oak Tree
Set King - 4-3-52. 1935-95

North Portal of tunnel

| Sta | + | π | - | Elev |
|--------|-------|---------|------|---------|
| | | | | 1948.07 |
| | 12.38 | 1960.45 | | |
| T.F. | | | 0.09 | 1960.36 |
| | 12.43 | 1972.79 | | |
| 145+50 | | | 10.1 | 1962.7 |
| 146+00 | | | 0.0 | 1972.8 |
| T.F. | | | 0.12 | 1972.67 |
| | 12.32 | 1984.99 | | |
| T.F. | | | 0.35 | 1984.64 |
| | 12.99 | 1997.61 | | |
| +50 | | | 5.4 | 1992.2 |
| T.F. | | | 0.43 | 1997.18 |
| | 12.80 | 2009.98 | | |
| T.F. | | | 0.26 | 2009.72 |
| | 11.91 | 2021.63 | | |
| 147+00 | | | 9.2 | 2012.4 |
| T.F. | | | 0.27 | 2021.36 |
| | 13.08 | 2034.94 | | |



| Sta. | + | T | - | Elev. |
|--------|-------|---------|------|---------|
| | | 2034.44 | | |
| 147+50 | | | 1.9 | 2032.5 |
| | 7.1 | | 0.31 | 2034.13 |
| | 11.85 | 2045.98 | | |
| | 7.1 | | 0.29 | 2045.69 |
| | 11.30 | 2056.99 | | |
| 148+00 | | | 4.6 | 2052.4 |
| | 7.1 | | 0.11 | 2056.88 |
| | 12.66 | 2069.54 | | |
| +50 | | | 1.8 | 2067.7 |
| | 7.1 | | 0.09 | 2069.45 |
| | 12.83 | 2082.28 | | |
| 149+00 | | | 3.1 | 2080.2 |
| | 7.1 | | 0.42 | 2081.86 |
| | 12.79 | 2094.65 | | |
| | 7.1 | | 0.07 | 2094.58 |
| | 12.21 | 2106.79 | | |



| Sta | + | - | Elev. |
|---------------|-------|---------|---------|
| | | 2106.79 | |
| 149+50 | | 9.6 | 2097.2 |
| TF | | 0.05 | 2106.74 |
| | 13.14 | 2119.88 | |
| 150+00 | | 4.3 | 2115.6 |
| TF | | 0.84 | 2119.04 |
| | 12.55 | 2131.59 | |
| TF | | 0.36 | 2131.23 |
| | 10.83 | 2142.06 | |
| +42 | | 8.1 | 2134.0 |
| +60 | | 9.9 | 2132.2 |
| TF | | 0.77 | 2141.29 |
| | 12.44 | 2153.73 | |
| +70 | | 11.3 | 2142.4 |
| TF | | 0.25 | 2153.48 |
| | 12.87 | 2166.35 | |

North edge of mesa Grande Rd.

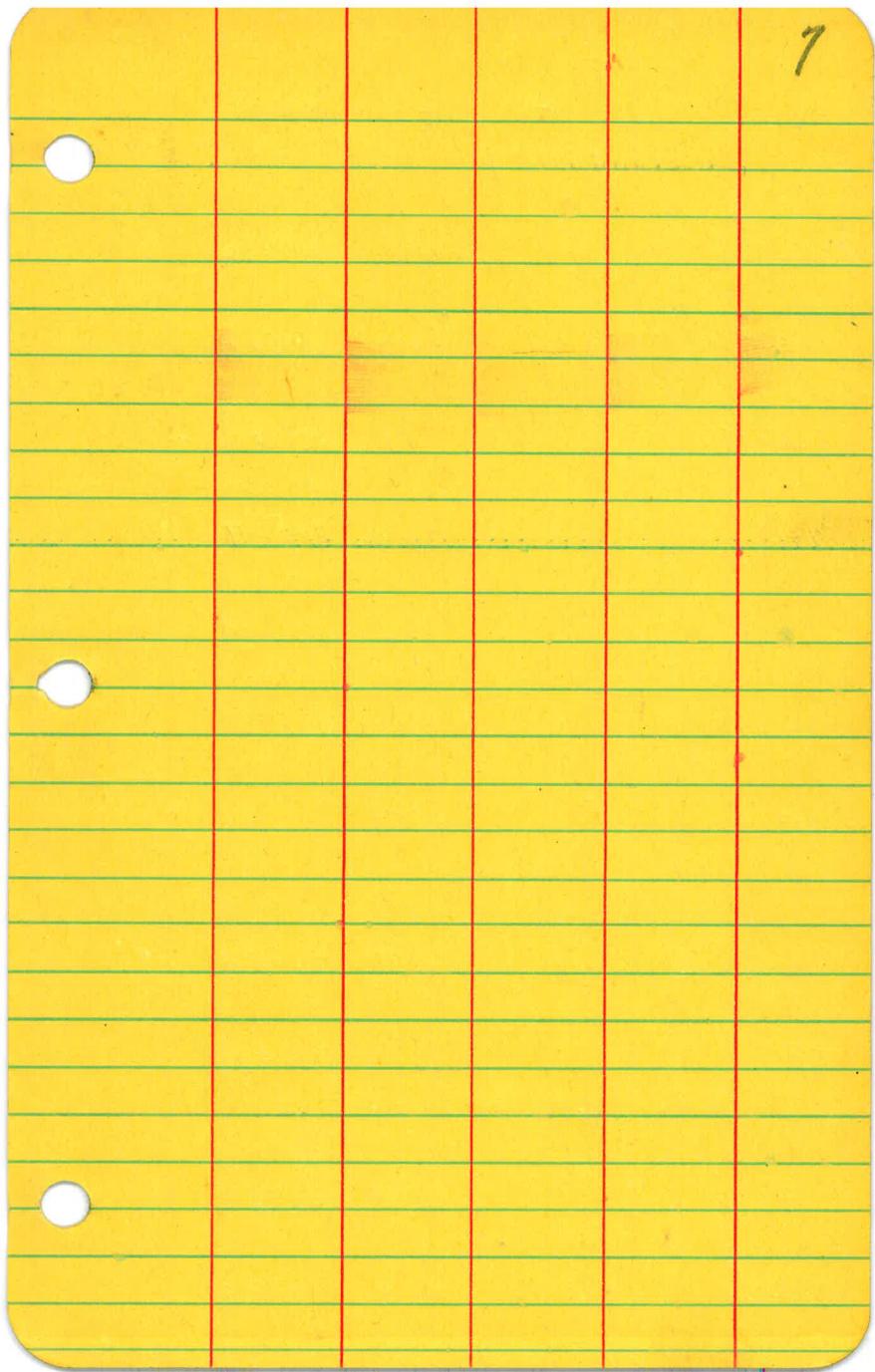
South " " " " "

| Sta | + | κ | - | Elev |
|--------|-------|---------|-------|-----------------|
| | | 2166.35 | | |
| 151+00 | | | 11.8 | 2154.6 |
| TP | | | 0.33 | 2166.02 |
| | 12.54 | 2178.56 | | |
| +50 | | | 1.9 | 2177.2 |
| TP | | | 0.18 | 2178.38 |
| | 13.12 | 2191.50 | | |
| TP | | | 0.24 | 2191.26 |
| | 12.71 | 2203.97 | | |
| 152+00 | | | 11.1 | 2192.9 |
| +43 | | | 2.2 | 2201.8 |
| TP | | | 1.45 | 2202.52 = check |
| | 0.83 | 2203.22 | | 2202.39 |
| TP | | | 13.09 | 2190.13 |
| | 1.46 | 2191.59 | | |
| 153+00 | | | 4.5 | 2187.1 |

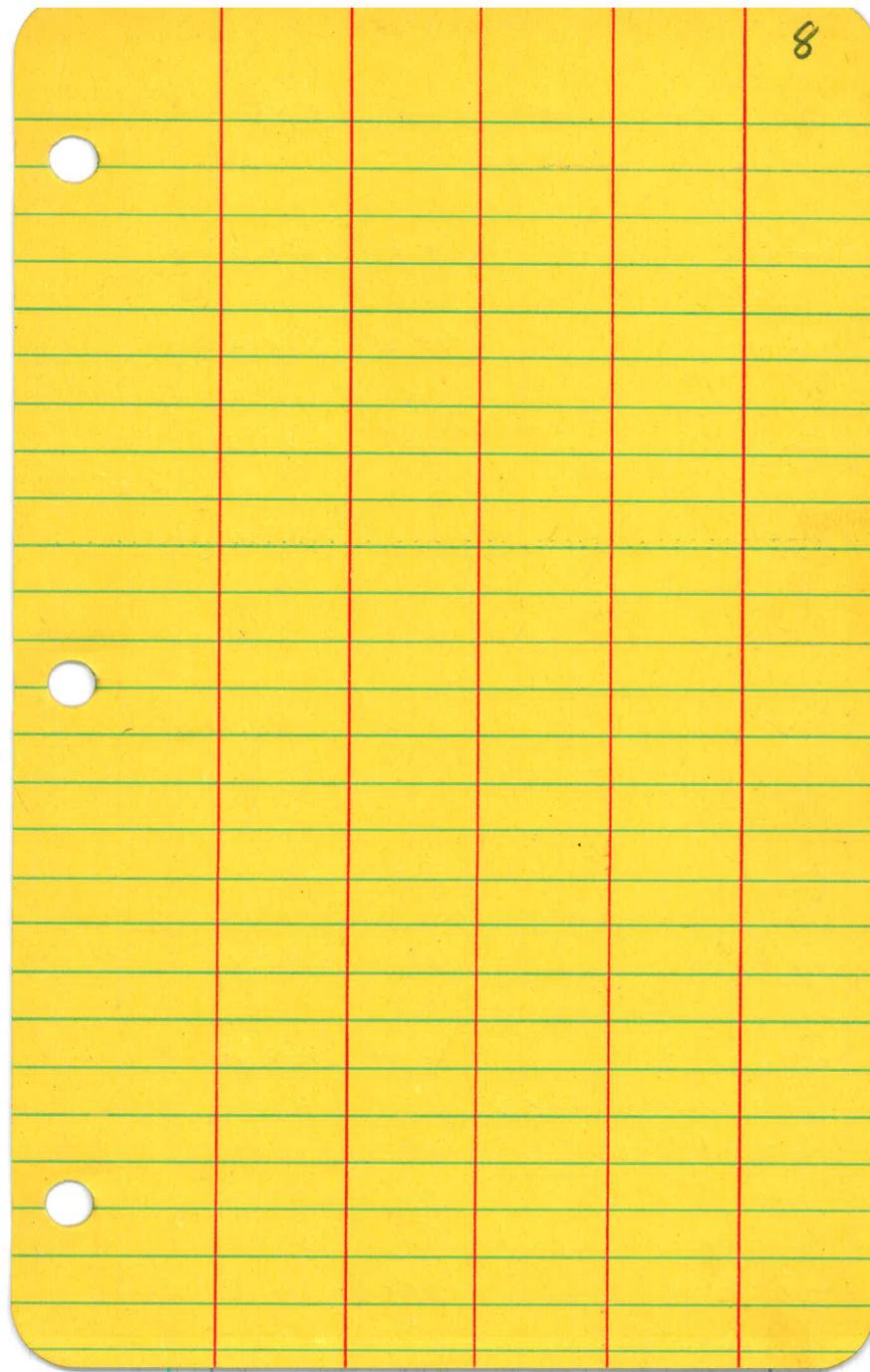
CHECK ON Print Pt. "J" El. = 2202.39

| Sta. | + | π | - | Elev. |
|--------|------|---------|-------|---------|
| | | 2191.59 | | |
| | TF | | 12.89 | 2178.70 |
| | 0.89 | 2179.57 | | |
| 153+50 | | | 11.0 | 2168.6 |
| | TF | | 12.87 | 2166.70 |
| | 0.03 | 2166.73 | | |
| | TF | | 12.61 | 2154.12 |
| | 0.20 | 2154.32 | | |
| 154+00 | | | 1.6 | 2152.7 |
| | TF | | 12.60 | 2141.72 |
| | 0.65 | 2142.37 | | |
| +50 | | | 8.9 | 2133.5 |
| +65 | | | 16.5 | 2125.9 |
| 155+00 | | | 19.5 | 2127.9 |
| | TF | | 12.41 | 2129.96 |
| | 9.31 | 2139.27 | | |
| +50 | | | 12.3 | 2127.0 |

7

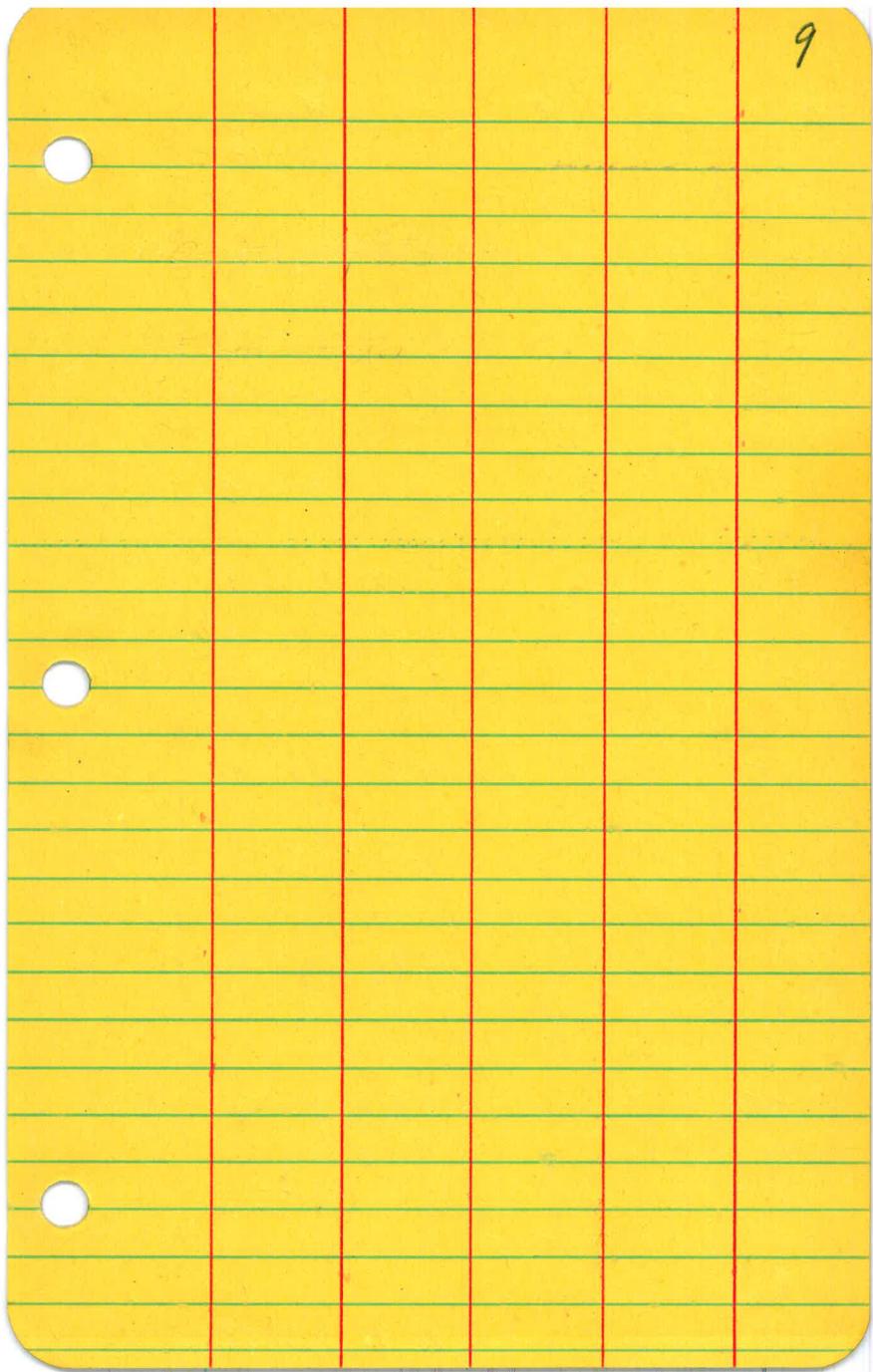


| Sta. | + | π | - | Elev. |
|--------|------|---------|-------|---------|
| | | 2139.27 | | |
| 156+00 | | | 13.1 | 2126.2 |
| +50 | | | 18.3 | 2121.0 |
| +65 | | | 21.1 | 2118.2 |
| 157+00 | | | 16.4 | 2122.9 |
| +50 | | | 13.2 | 2126.1 |
| 158+00 | | | 14.0 | 2125.3 |
| TR | | | 12.58 | 2126.69 |
| | 1.45 | 2128.14 | | |
| +50 | | | 11.7 | 2116.4 |
| TR | | | 12.44 | 2115.70 |
| | 0.44 | 2116.14 | | |
| +90 | | | 12.0 | 2104.1 |
| 159+00 | | | 16.9 | 2099.2 |

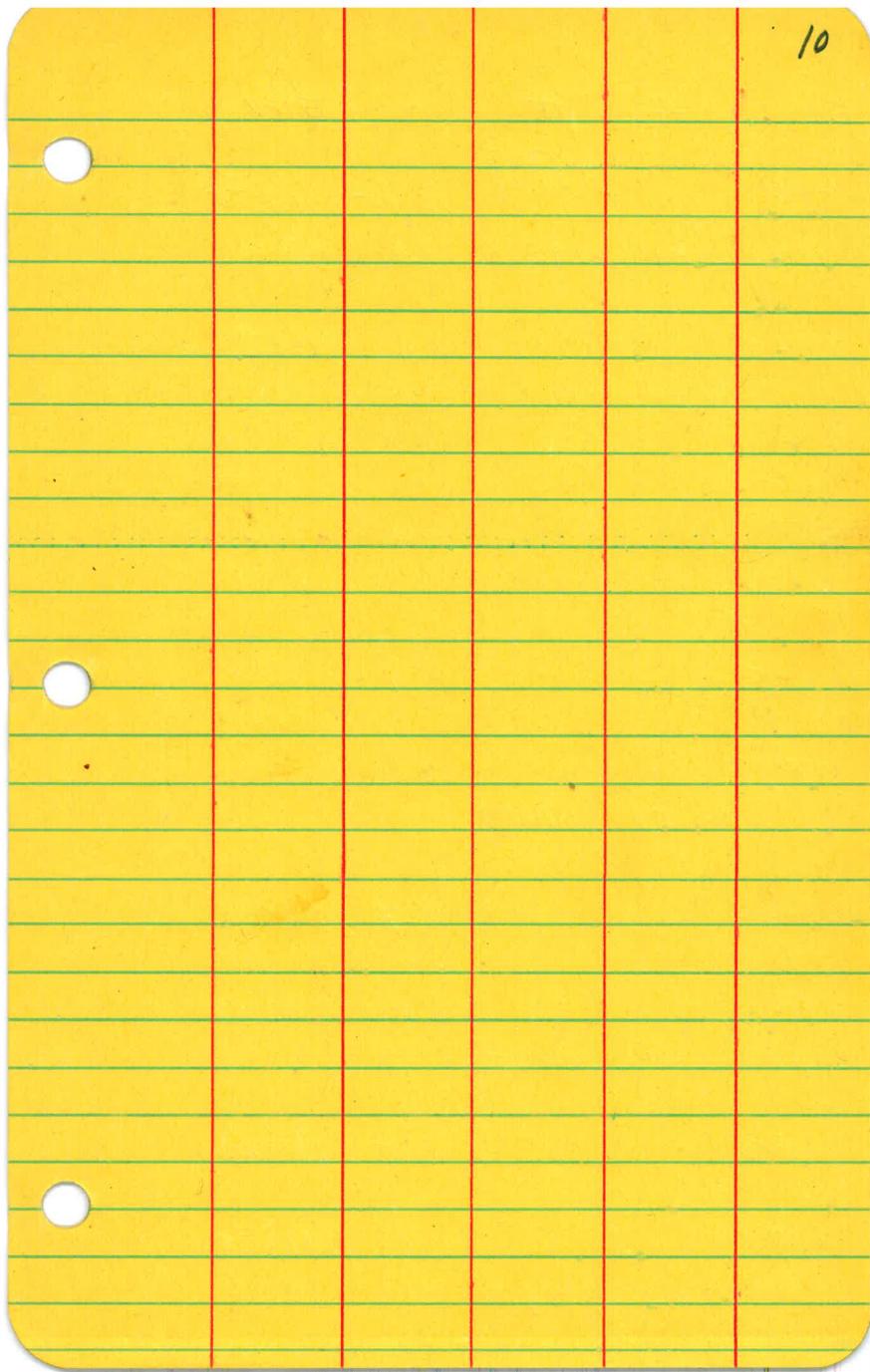


| Sta. | + | π | - | Elev. |
|--------|------|---------|-------|-----------|
| | | 2116.14 | | |
| 159+50 | | | 17.9 | 2098.2 |
| +72 | | | 20.8 | 2095.3 |
| 160+00 | | | 14.9 | 2101.2 |
| +50 | | | 16.1 | 2105.0 ✓ |
| +80 | | | 10.9 | 2105.2 |
| T.F. | | | 13.04 | 2103.10 ✓ |
| | 2.66 | 2105.76 | | |
| 161+50 | | | 5.2 | 2100.6 |
| 162+00 | | | 10.0 | 2095.8 |
| T.F. | | | 12.68 | 2093.08 |
| | 0.95 | 2094.03 | | |
| +50 | | | 7.0 | 2087.0 |
| T.F. | | | 12.85 | 2081.18 |

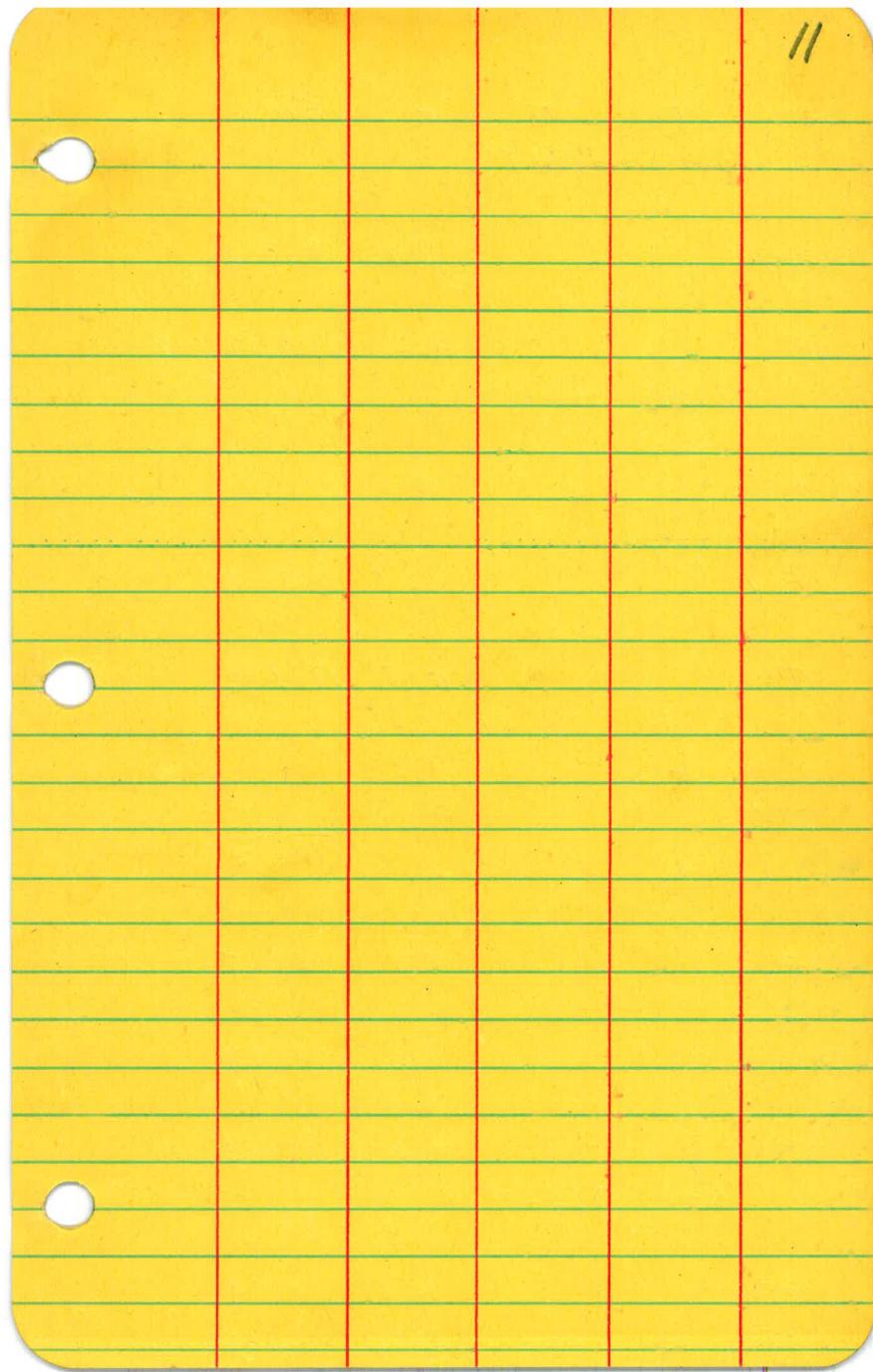
9



| Sta. | + | - | Elev. |
|--------|------|---------|---------|
| | | | 2081.18 |
| | 0.38 | 2081.56 | |
| 163+00 | | 2.6 | 2079.0 |
| +50 | | 8.9 | 2072.7 |
| 164+00 | | 14.2 | 2067.4 |
| +50 | | 17.5 | 2064.1 |
| 165+00 | | 15.3 | 2066.3 |
| +50 | | 14.8 | 2066.8 |
| 166+00 | | 13.8 | 2067.8 |
| TP | | 12.94 | 2068.62 |
| | 0.16 | 2068.78 | |
| +50 | | 7.7 | 2061.1 |
| TP | | 12.92 | 2055.86 |
| | 0.64 | 2056.50 | |
| 167+00 | | 12.9 | 2043.6 |



| Sta. | + | T | - | Elev. |
|--------|------|---------|-------|---------|
| | | 2056.50 | | |
| TR | | | 12.95 | 2043.55 |
| | 0.34 | 2043.89 | | |
| 167+50 | | | 6.2 | 2037.7 |
| 168+00 | | | 8.8 | 2035.1 |
| TR | | | 12.47 | 2031.42 |
| | 0.47 | 2031.89 | | |
| +50 | | | 6.9 | 2025.0 |
| TR | | | 12.67 | 2019.22 |
| | 0.57 | 2019.79 | | |
| 169+00 | | | 6.7 | 2013.1 |
| TR | | | 12.37 | 2007.42 |
| | 0.15 | 2007.57 | | |
| +50 | | | 6.5 | 2001.1 |
| TR | | | 12.83 | 1994.74 |
| | 0.03 | 1994.77 | | |



| Sta. | + | x | - | Elev. |
|--------|------|---------|-------|--------------------|
| | | 1994.97 | | |
| 170+00 | | | 7.4 | 1987.4 |
| T.H. | | | 12.23 | 1982.54 |
| | 0.01 | 1982.55 | | |
| +50 | | | 10.0 | 1972.6 |
| +61 | | | 12.5 | 1970.1 |
| T.H. | | | 12.75 | 1969.80 |
| | 2.14 | 1971.94 | | |
| T.H. | | | 9.21 | 1962.73 = check on |
| | 0.46 | 1963.28 | | 1962.82 B.M.#18 |
| +75 | | | 1.8 | 1961.5 |
| 171+00 | | | 1.6 | 1961.7 |
| T.H. | | | 12.65 | 1950.63 |
| | 1.39 | 1952.02 | | |
| +50 | | | 16.6 | 1935.4 |
| +56 | | | 23.6 | 1928.4 |

Check on B.M. #18 - El. 1962.82 ✓
Spike driven in ground. Edge of
Road near Sta (172+30)

| Sta. | + | * | - | Elev. | |
|----------------------|------|---------------|-------|---------|---|
| | | 1952.02 | | | |
| 171+89 | | | 11.1 | 1940.9 | |
| TR | | | 12.58 | 1939.44 | |
| | 1.36 | 1940.80 | | | |
| 172+00 | | | 6.9 | 1933.9 | |
| TR | | | 12.76 | 1928.04 | |
| | 0.63 | 1928.67 | | | |
| TR | | | 12.56 | 1916.11 | |
| | 0.50 | 1916.61 | | | |
| +50 | | | 9.3 | 1907.3 | |
| 173+02 ⁴⁴ | | tunnel | 15.4 | 1901.2 | X |
| | | Portal. | | | |
| | | South Portal. | | | |

Index

P-Line-

Pages 1 to 73 incl.

" 106 to 121 incl.

P' Line

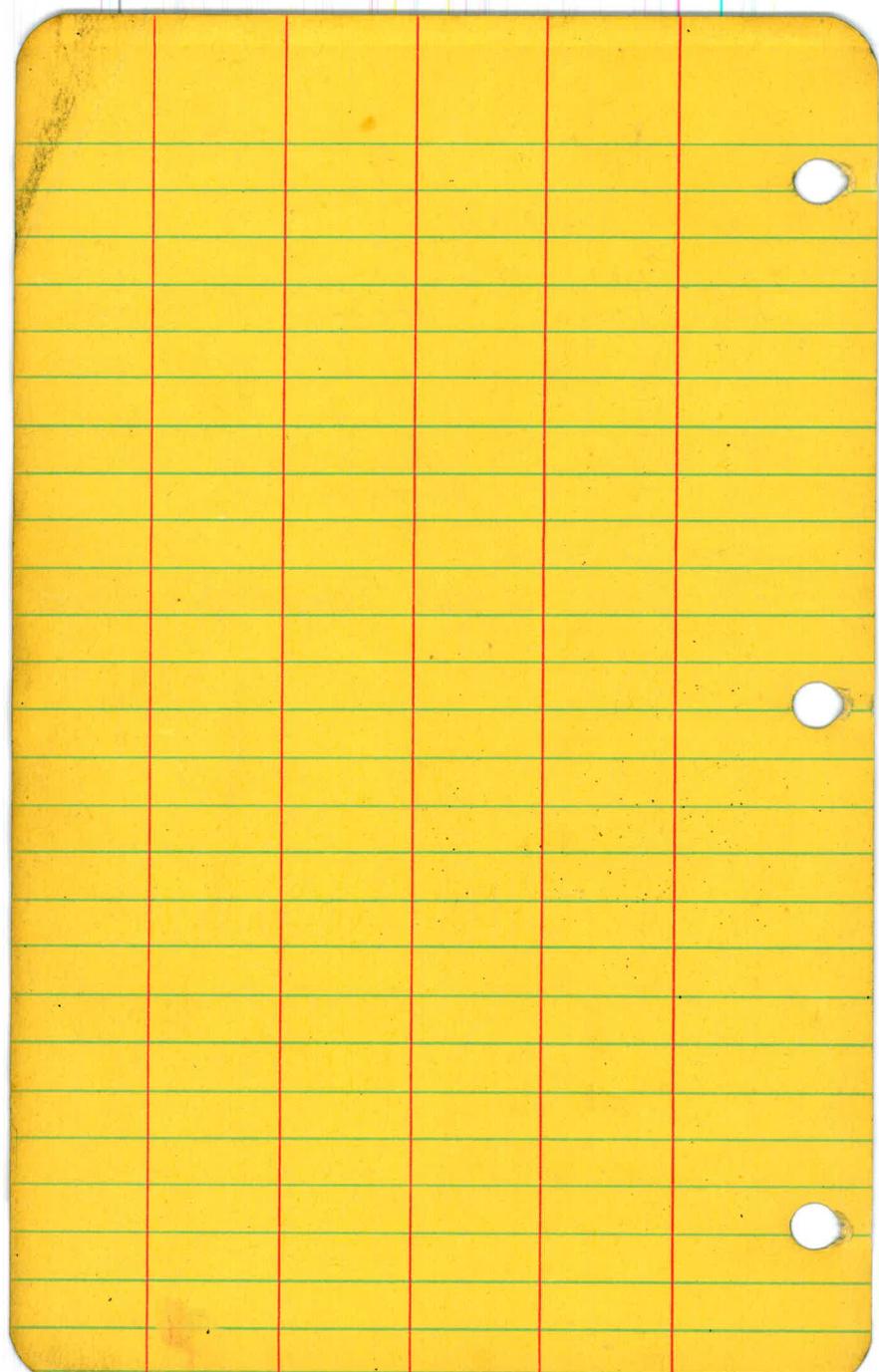
Pages 73 to 105 incl.

Sta 493+

Line Change

Sta. 203+ to 244

Pages 122 to 127 incl.



①

Nov 18, 1927

Simpson-T

Clavert-Rod

Profile Levels over
Pipe Line — Line KNOWN
By the Letter "P"
Starting from B.M. # 18
Elev. = 1962.820

| Sta. | + | π | - | Elev. |
|----------------------|-------|----------|--------|---------------------|
| | | | | 1962.820 = B.M. #18 |
| | 1.831 | 1964.651 | | |
| T.F. | | | 12.288 | 1952.363 |
| | 1.556 | 1953.919 | | |
| T.F. | | | 12.313 | 1941.606 |
| | 6.397 | 1948.003 | | |
| 171+87 ⁵⁵ | | | 7.0 | 1941.0 |
| 172+00 | | | 14.9 | 1933.6 |
| T.F. | | | 12.164 | 1935.839 |
| | 0.567 | 1936.406 | | |
| T.F. | | | 12.807 | 1923.599 |
| | 0.920 | 1924.519 | | |
| T.F. | | | 12.400 | 1912.119 |
| | 0.311 | 1912.430 | | |
| +50 | | | 5.0 | 1907.4 |
| 173+00 | | | 8.3 | 1904.1 |
| +50 | | | 14.9 | 1898.0 |
| 174+00 | | | 14.8 | 1897.6 |

See Page 13 for Des.

Beginning of Pipeline

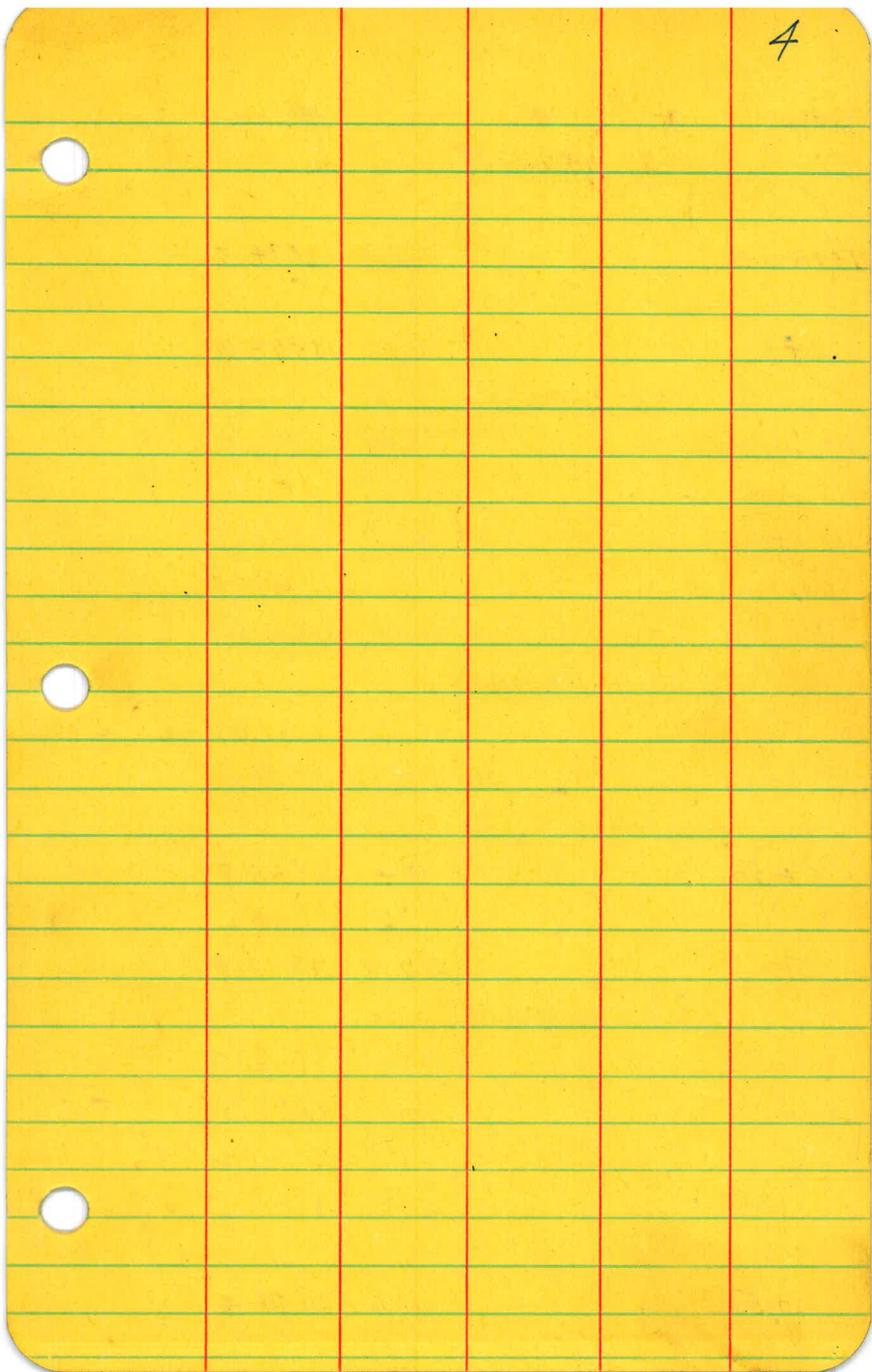
| Sta. | + | - | Ele. |
|--------|-------|-----------------------|-----------------------|
| | | 1912.430 [✓] | |
| 174+25 | | 19.7 | 1892.7 [✓] |
| +50 | | 3.9 | 1908.5 [✓] |
| T.F. | | 0.800 | 1911.630 [✓] |
| | 5.364 | 1916.994 [✓] | |
| +75 | | 0.2 | 1916.8 [✓] |
| 175+00 | | 3.8 | 1913.2 [✓] |
| +50 | | 24.5 | 1892.5 [✓] |
| 176+00 | | 4.4 | 1912.6 [✓] |
| +50 | | 6.4 | 1910.6 [✓] |
| 177+00 | | 11.0 | 1906.0 [✓] |
| T.F. | | 10.290 | 1906.704 [✓] |
| | 1.530 | 1908.234 [✓] | |
| +50 | | 7.6 | 1900.6 [✓] |

20

1940

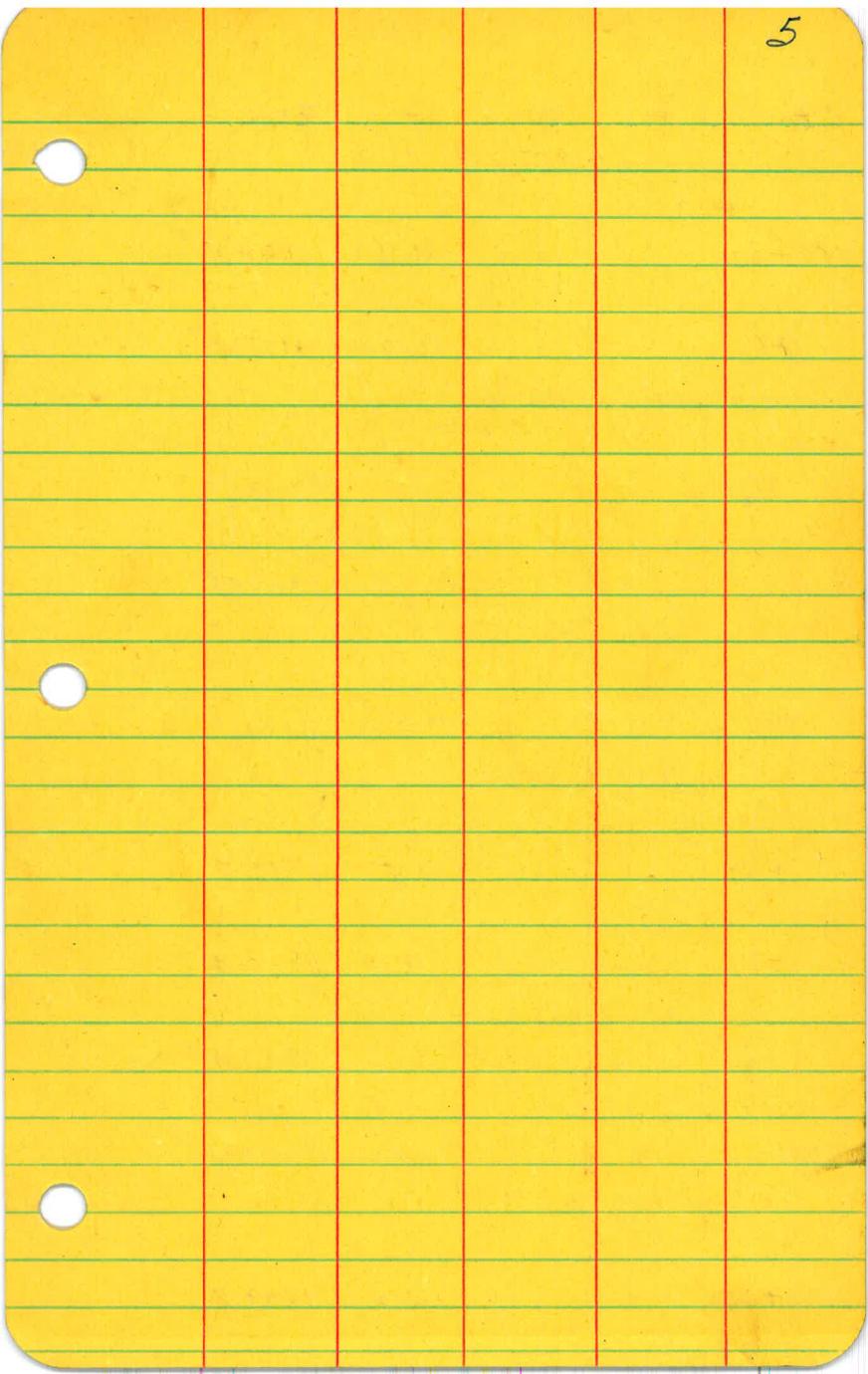
1880

| Sta. | + | π | - | Elev. |
|--------|-------|-----------------------|--------|-----------------------|
| | | 1908.234 [✓] | | |
| 178+00 | | | 13.3 | 1894.9 [✓] |
| T.F. | | | 12.756 | 1895.478 [✓] |
| | 1.854 | 1897.332 [✓] | | |
| +50 | | | 12.8 | 1884.5 [✓] |
| T.F. | | | 12.816 | 1884.516 [✓] |
| | 0.603 | 1885.119 [✓] | | |
| T.F. | | | 12.558 | 1872.561 [✓] |
| | 0.503 | 1873.064 [✓] | | |
| 179+00 | | | 13.0 | 1860.1 [✓] |
| +50 | | | 18.3 | 1854.8 [✓] |
| 180+00 | | | 9.6 | 1863.5 [✓] |
| T.F. | | | 0.573 | 1872.491 [✓] |
| | 5.698 | 1878.189 [✓] | | |
| +50 | | | 4.2 | 1874.0 [✓] |

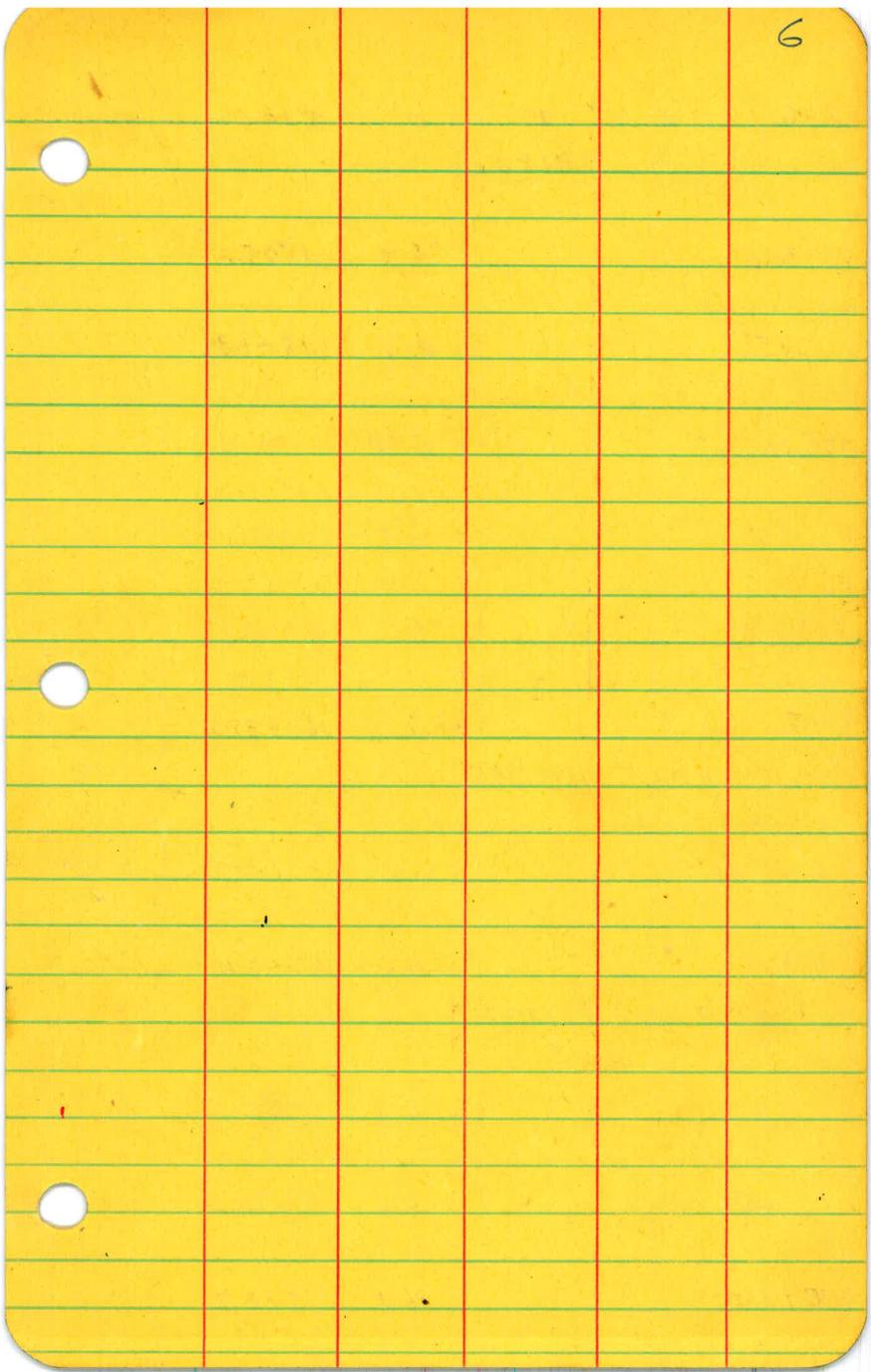


| Sta. | + | π | - | Elev. |
|--------|-------|-----------------------|--------|-----------------------|
| | | 1878.189 [✓] | | |
| 181+00 | | | 3.7 | 1874.5 [✓] |
| +50 | | | 5.0 | 1873.2 [✓] |
| 182+00 | | | 7.5 | 1870.7 [✓] |
| +50 | | | 10.9 | 1867.3 [✓] |
| T.P. | | | 12.927 | 1865.362 [✓] |
| | 0.574 | 1865.936 [✓] | | |
| 183+00 | | | 3.2 | 1862.7 [✓] |
| +50 | | | 9.4 | 1856.5 [✓] |
| T.P. | | | 12.772 | 1853.164 [✓] |
| | 1.245 | 1854.409 [✓] | | |
| 184+00 | | | 17.9 | 1836.5 [✓] |
| +05 | | | 21.9 | 1832.5 [✓] |
| +50 | | | 10.0 | 1844.4 [✓] |

5



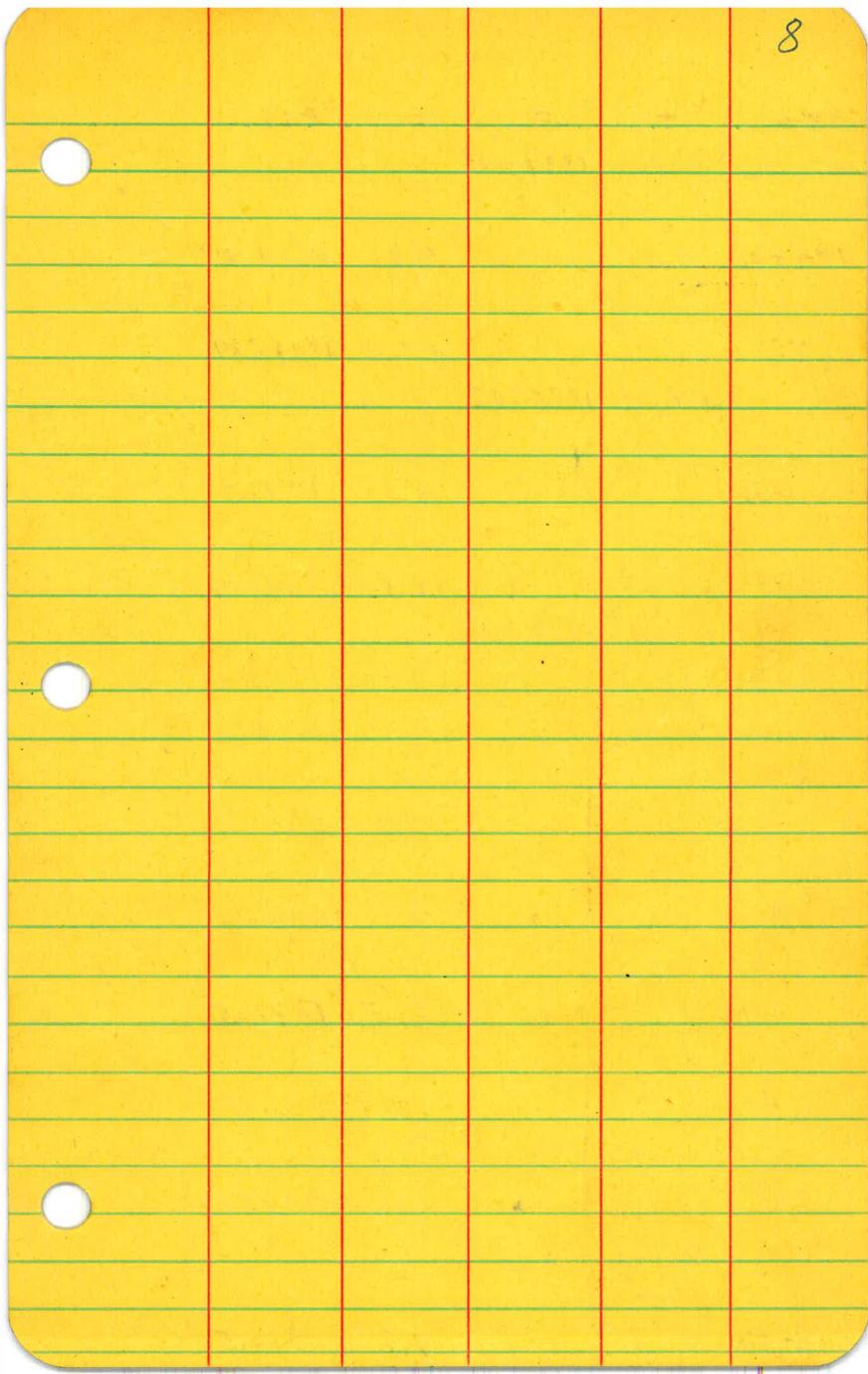
| Sta. | + | π | - | Elev. |
|--------|-----------|------------|--------|------------|
| | | 1854.409 | | |
| 185+00 | | | 11.9 | 1842.5 ✓ |
| TF | | | 12.875 | 1841.534 ✓ |
| | 1.047 | 1842.581 ✓ | | |
| +50 | | | 10.1 | 1832.5 ✓ |
| TF | | | 12.326 | 1830.255 ✓ |
| | 1.440 | 1831.695 ✓ | | |
| TF | | | 12.232 | 1819.463 ✓ |
| | 0.928 | 1820.391 ✓ | | |
| 186+00 | | | 1.5 | 1818.9 ✓ |
| +37 | creek Bed | | 12.1 | 1808.3 ✓ |
| +50 | | | 8.0 | 1812.4 ✓ |
| TF | | | 10.812 | 1809.579 ✓ |
| | 2.253 | 1811.832 ✓ | | |
| 187+00 | | | 2.6 | 1809.2 ✓ |



| Sta. | + | - | Elev. |
|--------|-------|------------|--------------------------|
| | | 1811.832 ✓ | |
| 187+16 | | 6.6 | 1805.2 ✓ |
| +50 | | 2.5 | 1809.3 ✓ |
| 188+00 | | 5.4 | 1806.4 ✓ |
| +50 | | 6.9 | 1804.9 ✓ |
| 189+00 | | 13.3 | 1798.5 ✓ |
| T.P. | | 1.462 | 1810.370 ✓ |
| | 0.015 | 1810.385 ✓ | |
| B.M. | | 1.310 | 1809.075 = E.I. B.M. #21 |
| T.P. | | 0.015 | 1810.370 ✓ |
| | 7.001 | 1817.371 ✓ | |
| +20 | | 6.9 | 1810.5 ✓ |
| +50 | | 5.1 | 1812.3 ✓ |
| 190+00 | | 4.7 | 1812.7 ✓ |

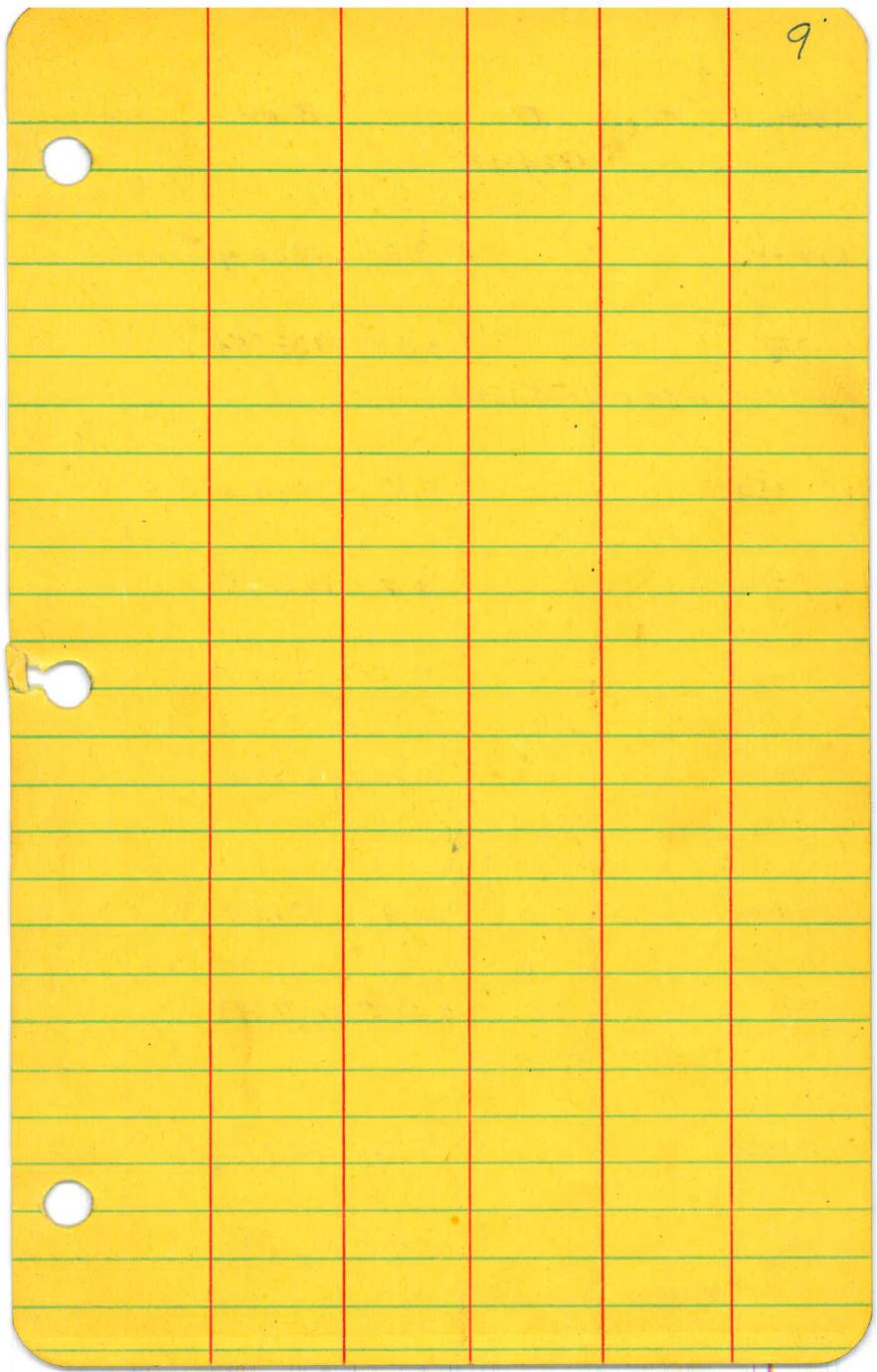
B.M. # P-1 - SPIKE IN
Large Oak tree
30' East of Sta - 188+50
Elev. = 1809.075

| Sta. | + | π | - | Elev. |
|--------|-------|----------|-------|------------|
| | | 1817.371 | | |
| 190+50 | | | 1.1 | 1816.3 ✓ |
| TR | | | 1.150 | 1816.221 ✓ |
| | 8.986 | 1825.207 | | |
| 191+00 | | | 8.1 | 1817.1 ✓ |
| +50 | | | 6.6 | 1818.6 ✓ |
| +75 | | | 12.0 | 1813.2 ✓ |
| 192+00 | | | 1.6 | 1823.6 ✓ |
| TR | | | 0.307 | 1824.900 ✓ |
| | 9.695 | 1834.595 | | |
| +50 | | | 4.4 | 1830.2 ✓ |
| TR | | | 0.885 | 1833.710 ✓ |
| | 3.404 | 1837.114 | | |
| 193+00 | | | 2.1 | 1835.0 ✓ |
| +50 | | | 6.6 | 1830.5 ✓ |



| Sta. | + | π | - | Elev. |
|--------|--------|------------|--------|------------|
| | | 1837.114 ✓ | | |
| 194+00 | | | 9.9 | 1827.2 ✓ |
| T.F. | | | 12.277 | 1824.837 ✓ |
| | 0.688 | 1825.525 ✓ | | |
| +50 | | | 3.8 | 1821.7 ✓ |
| T.F. | | | 12.858 | 1812.667 ✓ |
| | 1.172 | 1813.839 ✓ | | |
| 195+00 | | | 3.5 | 1810.3 ✓ |
| +25 | | | 4.0 | 1809.8 ✓ |
| +50 | | | 9.8 | 1804.0 ✓ |
| +70 | | | 21.3 | 1792.5 ✓ |
| 196+00 | | | 12.9 | 1800.9 ✓ |
| T.F. | | | 0.201 | 1813.638 ✓ |
| | 10.812 | 1824.450 ✓ | | |
| +50 | | | 7.9 | 1816.5 ✓ |

9



| Sta. | + | π | - | Elev. |
|--------|--------|------------|-------|------------|
| | | 1824.456 ✓ | | |
| 197+00 | | | 3.0 | 1821.4 ✓ |
| TF | | | 0.696 | 1823.754 ✓ |
| | 11.404 | 1835.158 ✓ | | |
| +50 | | | 11.9 | 1823.3 ✓ |
| 198+00 | | | 4.4 | 1830.8 ✓ |
| +50 | | | 7.7 | 1827.5 ✓ |
| TF | | | 8.736 | 1826.422 ✓ |
| | 12.416 | 1838.838 ✓ | | |
| 199+00 | | | 12.9 | 1825.9 ✓ |
| TF | | | 1.695 | 1837.193 ✓ |
| | 10.905 | 1848.048 ✓ | | |
| +50 | | | 5.4 | 1842.6 ✓ |
| TF | | | 0.896 | 1847.152 ✓ |
| | 8.920 | 1856.072 ✓ | | |



| Sta | + | π | - | Elev |
|--------|------------------|----------|--------|------------|
| | | 1856.072 | | |
| 200+00 | | | 5.8 | 1850.3 ✓✓ |
| | +50 | | 5.6 | 1850.5 ✓✓ |
| 201+00 | | | 6.5 | 1849.6 ✓✓ |
| | +50 | | 10.0 | 1846.1 ✓✓ |
| T.F. | | | 12.855 | 1843.217 ✓ |
| | 1.166 | 1844.383 | | |
| | +85 | | 4.7 | 1839.7 ✓✓ |
| 202+20 | | | 31.8 | 1812.6 ✓✓ |
| | +50 | | 9.2 | 1835.2 ✓✓ |
| T.F. | | | 0.518 | 1843.865 ✓ |
| | 6.713 | 1850.578 | | |
| | +67 ² | P.I. | 9.8 | 1840.8 ✓✓ |
| 203+00 | | | 4.6 | 1846.0 ✓ |

Level Notes

Line Change

From Sta 203+00 to

Equation $214 + 03.41 =$
 $214 + 07.07$ Ahead

| Sta. | + | HI | - | EV | Base Elev. ✓ |
|--------------|------|--------------------|-------|----|-------------------------------|
| BM22 | | | | | 1905.093 1905.9 |
| | 0.3 | 1905.39 +906.20 | | | |
| T.P. | | | 12.74 | | 1892.65 +893.46 |
| | 0.21 | 1892.66 +893.67 | | | |
| R15.70 BM | | | 3.79 | | 1889.67 +889.88 |
| 207+56 | | | 7.8 | | 1885.1 +885.9 |
| 207+50 | | | 7.1 | | 1885.8 +886.6 |
| 207+25 | | | 6.6 | | 1886.3 +887.1 |
| 207+0 | | | 5.2 | | 1887.7 +888.5 |
| 206+50 | | | 8.4 | | 1884.5 +885.3 |
| 206+0 | | | 12.9 | | 1880.0 +880.8 |
| TP | | | 12.54 | | 1880.35 +881.13 |
| | 0.46 | 1880.72 +881.53 | | | |
| 205+50 | | | 6.9 | | 1873.8 +874.6 |
| TP | | | 12.61 | | 1868.11 +868.22 |
| | 1.61 | 1869.72 +870.53 | | | |

BM#22

In Power Pole #1413 50' Left of Sta 210+00

On Road to Ranch.

In Road

In Road

1871.53

- 12.61

1858.92

+ 1.61

1860.53

PT - Edge old Road 14'

| ENV | + | #1 | - |
|--------|---------------|-------------------------------|---------------------------------|
| | | 1869.72 1870.53 | |
| 20510 | | | 6.2 |
| | | | 1863.5 ✓ 1864.3 |
| TP | | 1858.82 | 12.47 |
| | 1.57 | 1859.63 | |
| | | | 1857.25 ✓ 1858.06 |
| 204+50 | | | 12.5 |
| | | | 1846.3 ✓ 1847.1 |
| | Hand Level | | 1846.3 1847.1 |
| | 0.0 | 1846.3 1847.1 | |
| 20410 | | | 12.6 |
| | | | 1833.7 1834.5 |
| 203+80 | | | 12.6 |
| | | | 1833.7 1834.5 |
| 203+65 | | | 23.0 |
| | | | 1823.3 1824.1 |
| 203+50 | | | 7.6 |
| | | | 1838.7 1839.5 |
| | Resume Levels | | |
| | | 1858.82 1859.63 | |
| 203+0 | | | 13.7 |
| | | | 1845.1 ✓ 1845.9 |

124

17 Wash 30' Wide

202465

Wash

WASH

| | + | H.I. | - | Elev |
|--------|-------|---------------------------------|--------|---------------------------------|
| BM | | | | 1889.07 1889.88 |
| | 0.33 | 1889.40 ✓ 1890.21 | | |
| T.P. | | | 12.60 | 1876.80 ✓ 1877.61 |
| | 0.63 | 1877.43 ✓ 1878.44 | | |
| 208+0 | | | 7.0 | 1870.4 1871.2 |
| 208+25 | | | 14.5 | 1862.9 1863.7 |
| 208+50 | | | 16.0 | 1861.4 1862.2 |
| 208+60 | | | 19.5 | 1857.9 1858.7 |
| 208+90 | | | 12.5 | 1864.9 1865.7 |
| TA | | | 11.780 | 1865.680 1866.46 |
| | 0.940 | 1866.59 1867.40 | | |
| 209+00 | | | 2.8 | 1863.8 1864.6 |
| +28 | | | 6.0 | 1860.6 1861.4 |
| +40 | | | 12.7 | 1853.9 1854.7 |
| +60 | | | 9.1 | 1857.5 1858.3 |

125

2/1

30

12

67

58

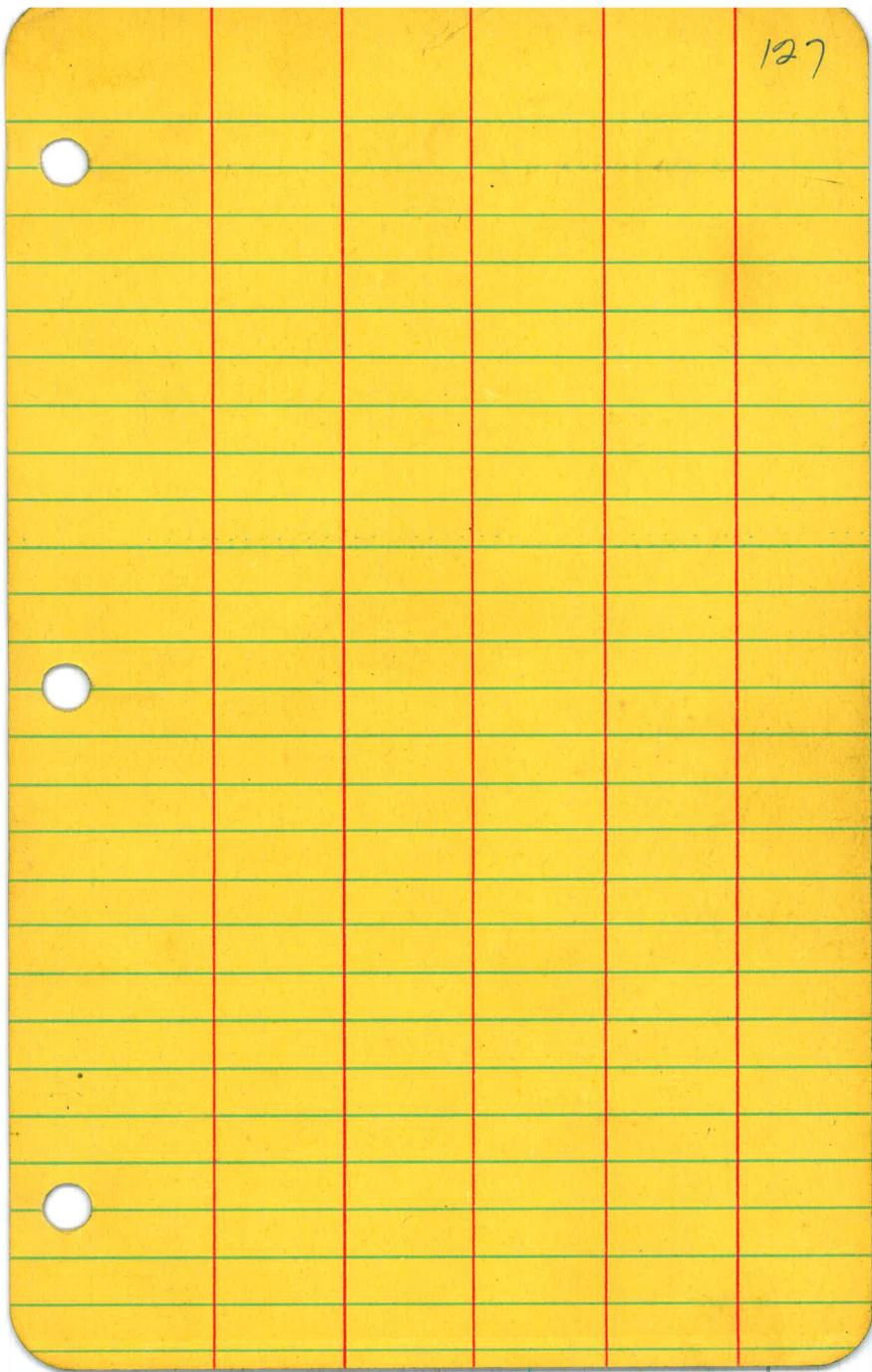
| Sta. | + | T | - | Elev. |
|--------|------|-------------------------------|--------|--------------------------------|
| | | 1866.52 1867.40 | | |
| 209+75 | | | 8.5 | 1858.1 1858.9 |
| TH | 1.66 | 1855.75 1856.54 | 12.500 | 1854.090 1854.90 |
| 210+00 | | | 6.8 | 1849.0 1849.8 |
| +30 | | | 20.5 | 1835.3 1836.1 |
| +50 | | | 14.6 | 1841.2 1842.0 |
| +70 | | | 7.6 | 1848.2 1849.0 |
| 211+00 | | | 11.2 | 1844.6 1845.4 |
| +10 | | | 9.4 | 1846.2 1847.2 |
| TH | 1.70 | 1844.84 1845.65 | 12.61 | 1843.14 1843.95 |
| +50 | | | 17.8 | 1827.0 1827.8 |
| - +70 | | | 1.6 | 1843.2 1844.0 |

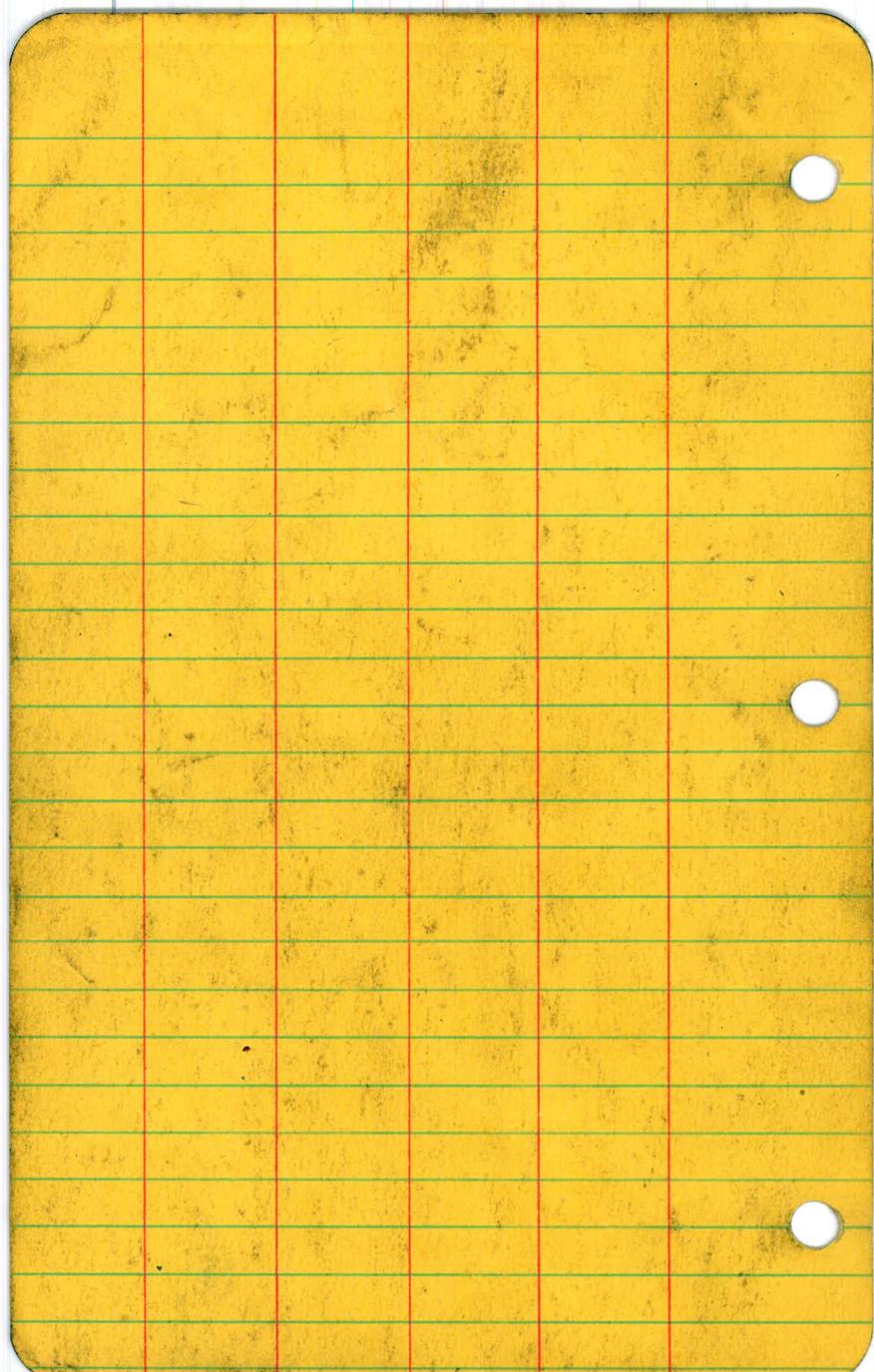
126

¢ of wash

| Sta | + | 1844.84 1845.65 | - | Elev. |
|-----------|--------------|--|------|-----------------------------|
| 212+00 | | | 6.5 | 1838.3 1839.1 |
| +40 | | | 12.7 | 1832.1 1832.7 |
| +65 | | | 21.6 | 1823.2 1824.0 |
| +80 | | | 13.9 | 1830.9 1831.7 |
| 213+10 | | | 11.8 | 1833.0 1833.8 |
| +50 | | | 14.5 | 1830.3 1831.7 |
| 214+00 | | | 15.9 | 1828.9 1829.7 |
| +03 | ² | ⁰⁷ | 16.1 | 1828.7 1829.5 |
| Equation. | | | | |

127





15

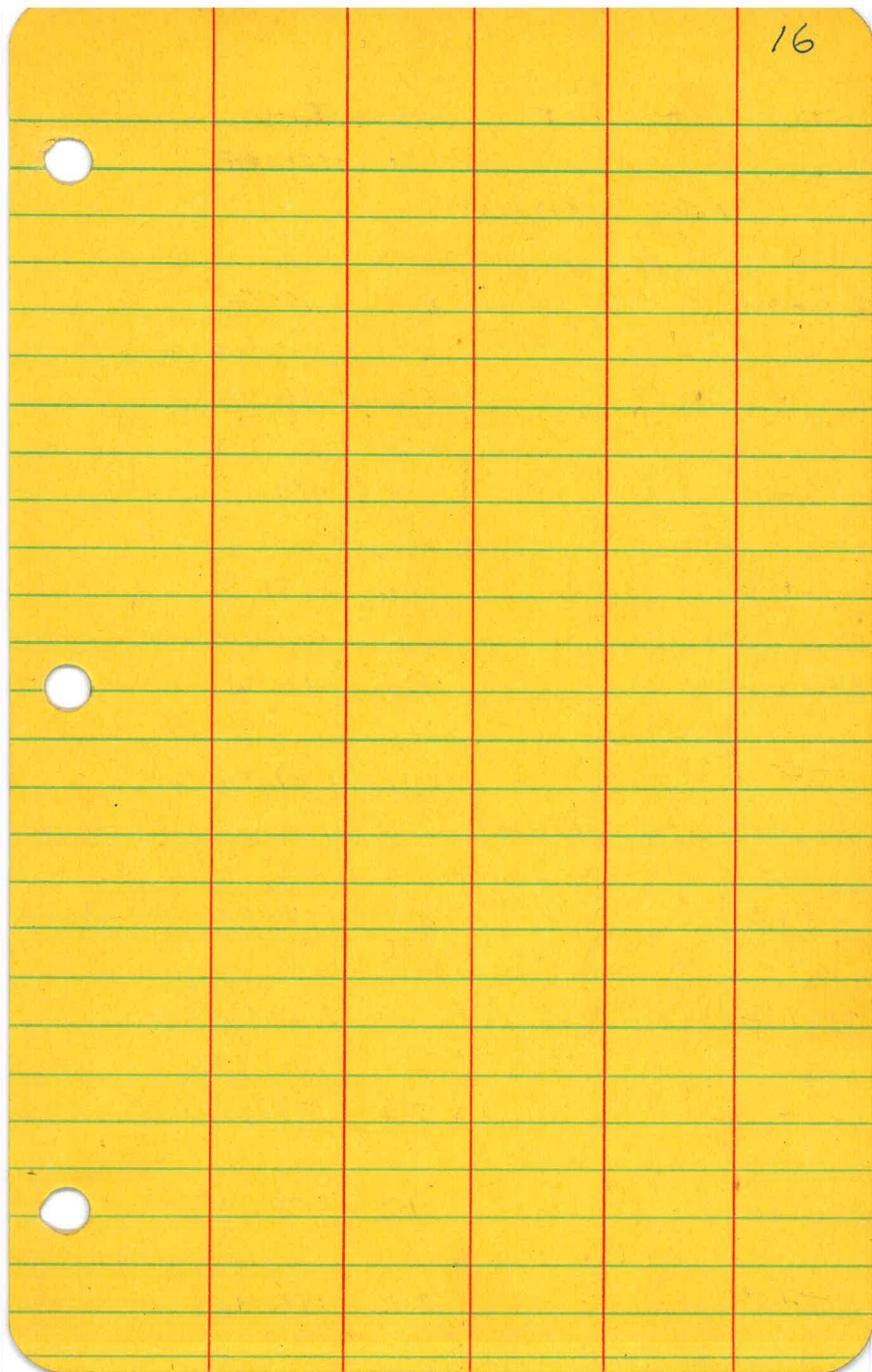
Nov 21 - 1927

Cool And Cloudy

Simpson - T

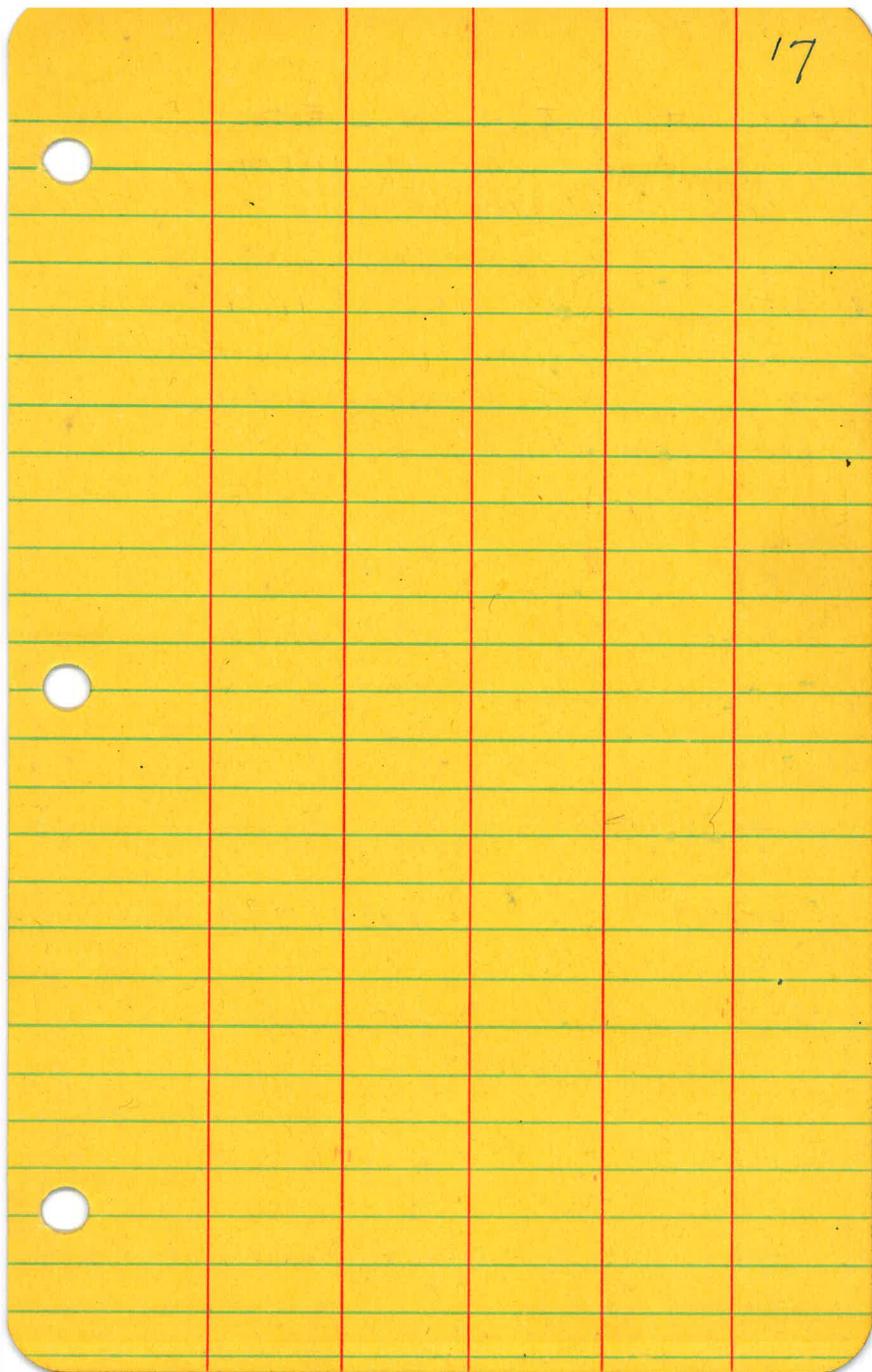
Clavert - Red

| Sta. | + | π | - | Elev. |
|--------------------------|-------|----------|--------|------------|
| | 1.800 | 1830.689 | | 1828.889 ✓ |
| 214+07 ² P.I. | | | 1.8 | 1828.9 ✓ |
| +50 | | | 3.6 | 1827.1 ✓ |
| 215+00 | | | 7.4 | 1823.3 ✓ |
| +50 | | | 11.2 | 1819.5 ✓ |
| 216+00 | | | 12.1 | 1818.6 ✓ |
| T.F. | | | 12.231 | 1818.458 ✓ |
| | 0.103 | 1818.561 | | |
| +30 | | | 10.9 | 1807.7 ✓ |
| +50 | | | 7.7 | 1810.9 ✓ |
| 217+00 | | | 8.0 | 1810.6 ✓ |
| +50 | | | 10.1 | 1808.5 ✓ |
| T.F. | | | 9.717 | 1808.844 ✓ |



| Sta | + | T | - | Elev. |
|--------|-------|------------|--------|------------|
| | | | | 1808.844 ✓ |
| | 1.567 | 1810.411 ✓ | | |
| 218+00 | | | 4.5 | 1805.9 ✓ |
| | +50 | | 8.6 | 1801.8 ✓ |
| 219+00 | | | 10.1 | 1800.3 ✓ |
| | +50 | | 9.4 | 1801.0 ✓ |
| 220+00 | | | 8.6 | 1801.8 ✓ |
| | TF | | 10.725 | 1799.686 ✓ |
| | 1.682 | 1801.368 ✓ | | |
| | +50 | | 3.9 | 1797.5 ✓ |
| 221+00 | | | 3.7 | 1797.7 ✓ |
| | +50 | | 7.4 | 1794.0 ✓ |
| 222+00 | | | 11.2 | 1790.2 ✓ |
| | TF | | 12.428 | 1788.940 ✓ |

17



| Sta. | + | π | - | Elev. |
|--------|-------|------------|--------|------------|
| | | | | 1788.940 ✓ |
| | 0.807 | 1789.747 ✓ | | |
| 222+50 | | | 8.6 | 1781.1 ✓ |
| TH | | | 12.640 | 1777.107 ✓ |
| | 0.256 | 1777.363 ✓ | | |
| 223+00 | | | 7.2 | 1770.2 ✓ |
| +50 | | | 17.6 | 1759.8 ✓ |
| +75 | | | 33.0 | 1744.4 ✓ |
| 224+00 | | | 21.2 | 1756.2 ✓ |
| +50 | | | 4.1 | 1773.3 ✓ |
| TH | | | 4.533 | 1772.830 ✓ |
| | 7.325 | 1780.155 ✓ | | |
| 225+00 | | | 8.2 | 1772.0 ✓ |
| +50 | | | 12.3 | 1767.9 ✓ |
| 226+00 | | | 3.9 | 1776.3 ✓ |

paid-

| Sta. | + | T | - | Elev. |
|--------|--------------------|------------|--------|------------|
| | | 1780.155 ✓ | | |
| T.F. | | | 0.767 | 1779.388 ✓ |
| | 3.456 | 1782.844 ✓ | | |
| 226+34 | ⁰⁸ P.I. | | 3.6 | 1779.2 ✓ |
| | | | 0.5 | 1782.3 ✓ |
| +50 | | | 3.1 | 1779.7 ✓ |
| 227+00 | | | 7.2 | 1775.6 ✓ |
| +50 | | | 10.1 | 1772.7 ✓ |
| 228+00 | | | 11.6 | 1771.2 ✓ |
| | | | 9.1 | 1773.7 ✓ |
| T.F. | | | 11.510 | 1771.334 ✓ |
| | 1.210 | 1772.544 ✓ | | |
| +50 | | | 4.9 | 1767.6 ✓ |
| 229+00 | | | 10.5 | 1762.0 ✓ |
| +50 | | | 8.3 | 1764.2 ✓ |
| 230+00 | | | 10.5 | 1762.0 ✓ |

JAN. 7, 1928

Simpson

Clavert.

Profile Levels over Line
Change, starting from
226+28⁵⁵ — THIS IS "P" LINE
to Sta. 323+37.42

P. Line

| Sta. | + | T | Rod on Line | Rod on L Rod. 15 ^{ft.} of LINE ELEV. | ① |
|---------------------------|------|---------|----------------|---|---------|
| | | | | | 1905.09 |
| | 0.54 | 1905.63 | | | |
| TF | | | 12.61 | | 1893.02 |
| | 1.17 | 1894.19 | | | |
| TF | | | 11.53 | | 1882.66 |
| | 2.19 | 1884.85 | | | |
| TF | | | 12.53 | | 1872.32 |
| | 0.57 | 1872.89 | | | |
| TF | | | 12.52 | | 1860.37 |
| | 0.07 | 1860.44 | | | |
| TF | | | 12.89 | | 1847.55 |
| | 0.24 | 1847.79 | | | |
| TF | | | 13.05 | | 1834.74 |
| | 0.11 | 1834.85 | | | |
| TF | | | 12.41 | | 1822.44 |
| | 0.56 | 1823.00 | | | |
| TF | | | 12.84 | | 1810.16 |
| | 0.75 | 1810.91 | | | |
| TF | | | 11.89 | | 1799.02 |
| | 1.09 | 1800.11 | | | |
| TF | | | 12.65 | | 1787.46 |
| | 0.38 | 1787.84 | | | |
| 226+28 ⁶³ P.I. | | | 7.7 | 5.8 | 1780 .1 |

①
Simpson
Claret.

= E.I. - S. D. B.M. # 22
In Power Pole # 14113 - 50' Left
of Sta 210+00 (On Road to Ranch)
Balanced Elev. 1905.093

= B.M. # "P" 13 - Nail in 8"x8"
U.S. Forest Reserve Sign
Post. - Elev. = 1799.02

Md. El.

1782 .0

| Sta. | + | π | Red on Line | Red on E Pd. 15° P.P. - Line | Elev. ② |
|--------|-------------------------|---------|------------------|------------------------------------|--|
| | | 1787.84 | | | |
| 226+50 | | | 8.1 | 7.0 | 1779.7 |
| 227+00 | | | 12.2 | 9.8 | 1775.6 |
| T.F. | | | 11.67 | | 1776.17 |
| | 0.33 | 1776.50 | | | |
| +50 | | | 3.2 | 0.7 | 1773.3 |
| 228+00 | | | 4.7 | 3.4 | 1771.8 |
| +50 | | | 8.9 | 6.7 | 1767.6 |
| +98 | <u>55</u> | | 12.9 | 9.0 | 1763.6 |
| 229+03 | 12" C.M. P. Culvert. | | 12.9 = Flow Line | | 1763.6 |
| 229+50 | | | 12.8 | 11.0 | 1763.7 |
| T.F. | | | 12.73 | | 1763.77 |
| | 0.14 | 1763.91 | | | |
| 230+00 | | | 3.0 | 1.1 | 1760.9 |

Rd El.

2

1780 .8

1778 .0

1775 .8

1773 .1

1770 .1

1767 .5

1765 .5

1762 .8

1764 .0

1764 .14

1763 .83

| Sta. | + T | T | Rod on Line | Rod on $\frac{1}{2}$ Rod. 15" Rod - Line | Elcv. (3) |
|---------------------|------------------------|---------|-----------------|--|--|
| | | 1763.91 | | | |
| 230+50 | | | 6.8 | 4.0 | 1757.1 |
| | 180 ⁵ P.I. | | 8.5 | 5.7 | 1756.4 |
| 231+50 | | | 10.8 | 8.7 | 1753.1 |
| 232+00 | | | 13.6 | 11.4 | 1750.3 |
| | T.P. | | 12.92 | | 1750.99 |
| | 0.40 | 1751.39 | | | |
| | +50 | | 2.7 | 1.8 | 1748.1 |
| 233+00 | | | 5.6 | 4.6 | 1745.8 |
| | +50 | | 8.6 | 7.3 | 1742.8 |
| | +95 ⁴⁵ P.I. | | 12.2 | 9.6 | 1739.2 |
| | T.P. | | 10.99 | | 1740.42 |
| | 0.95 | 1741.37 | | | |
| 234+21 ² | 12" C.M.P. Culvert. | | 6.2 = Flow Line | | 1735.2 |

Rd El.

3

1759 .9

1758.2

1755.2

1751.5

1749.6

1746.8

1744 .1

1741.8

| Sta. | + | π | Rod on Line | Rod on & Rd. 15 th R th + - Line | Elev. |
|------------------------|------------------------|---------|----------------|--|---------|
| | | 1741.37 | | | |
| 234+21 ² | | | 9.1 | | 1732.3 |
| +50 | | | 5.4 | | 1736.0 |
| 235+00 | | | 3.8 | 3.9 | 1737.6 |
| +50 | | | 5.5 | | 1735.9 |
| 236+00 | | | 7.4 | 7.9 | 1734.0 |
| +22 ²⁴ B.C. | | | 8.2 | | 1733.2 |
| +50 | | | 10.3 | 10.6 | 1731.1 |
| 7 th | | | 12.45 | | 1728.92 |
| | 0.65 | 1729.57 | | | |
| +75 | | | 0.0 | | 1729.6 |
| +94 | 12" C.M.P. CULVERT. | | 4.7 | = Flow line | 1724.9 |
| 237+00 | | | 6.8 | 2.0 | 1722.8 |
| +27 ³⁵ E.C. | | | 2.4 | | 1727.2 |

Red. El.

④

1737.5

1733.5

1730.8

1727.6

(5)

| Sta. | + | + | Rod on LINE | Rod on ϕ of Rd. 13 ⁵⁰ ft LINE | Elev. |
|--------|-----------------------|---------|----------------|---|---------|
| | | 1729.57 | | | |
| 237+50 | | | 3.6 | 1726.0 | 1726.0 |
| 238+00 | | | 6.7 | 7.0 | 1722.9 |
| +50 | | | 9.0 | | 1720.6 |
| +85 | ⁹³ P.I. | | 12.4 | 11.9 | 1717.2 |
| TH | | | 12.93 | | 1716.64 |
| | 0.27 | 1716.91 | | | |
| 239+50 | | | 3.6 | 2.3 | 1714.3 |
| 240+00 | | | 5.0 | | 1711.9 |
| +50 | | | 6.9 | 6.8 | 1710.0 |
| 241+00 | | | 8.5 | | 1708.4 |
| +15 | ¹⁹ P.I. | | 9.6 | | 1707.3 |
| +50 | | | 11.9 | 11.5 | 1705.0 |
| TH | | | 11.11 | | 1705.80 |

Rd. El.

1722.6

1717.7

1714.6

1710.1

1705.4

(6)

| Sta. | + | + | Rod on LINE | Rod on & Rd. 15 ² Rt. of - LINE E/CV. | |
|------------------------|------|---------|----------------|--|---------------------|
| | | | | | 1705.80 |
| | 0.38 | 1706.18 | | | |
| 242+00 | | | 4.5 | | 1701.7 ✓ |
| +50 | | | 6.9 | 6.2 | 1699.7 ³ |
| 243+00 | | | 9.0 | | 1697.2 ✓ |
| +50 | | | 10.7 | 10.6 | 1695.5 ✓ |
| 244+00 | | | 12.5 | | 1693.7 ✓ |
| T.F. | | | 12.62 | | 1693.56 |
| | 1.09 | 1694.65 | | | |
| +50 | | | 3.4 | 3.9 | 1691.2 ✓ |
| 245+00 | | | 6.3 | | 1688.3 ✓ |
| +12 ⁸¹ P.I. | | | 7.3 | | 1687.3 ✓ |
| +50 | | | 9.8 | 9.2 | 1684.8 ✓ |
| 246+00 | | | 11.9 | | 1682.7 ✓ |

Rd. El.

1700.0

1695.6

1690.7

1685.4 ✓

⑦

| Sta. | + | π | Rod on Line - | Rod on 2 nd Rd. 15' R.H. of Line | Elev. |
|--------|-------------------------------|---------|---------------|---|------------------|
| | | 1694.65 | | | |
| T.F. | | | 12.39 | | 1682.31 |
| | 0.18 | 1682.49 | | | |
| 246+50 | | | 2.0 | 2.0 | 1680.5 ✓ |
| 247+00 | | | 5.1 | | 1677.4 ✓ |
| +30 | | | 14.0 | | 1668.5 ✓ |
| +30 | 8" x 10" x 20" Culvert Bridge | | 17.0 = | 1668.5 Flow Line - East End | |
| | | | 13.4 = | 1669.1 West End | |
| +50 | | | 11.0 | 6.0 | 1671.5 1676.5 |
| 248+00 | | | 8.3 | | 1674.2 ✓ |
| +50 | | | 9.3 | 9.4 | 1673.2 ✓ |
| 249+00 | | | 11.0 | | 1674.5 ✓ |
| T.F. | | | 10.28 | | 1672.21 |
| | 0.50 | 1672.71 | | | |
| +50 | | | 3.5 | 3.2 | 1669.2 |

Ad. El.

⑧

1680.5 ✓

1676.5 ✓

1673.1 ✓

T.P. Nail in fence Post - 299 + 30.

1669.5 ✓

⑧

| sta | + | π | Rod on N — Line | Rod on E Pd. 15° Pt. of — Line | Elev. |
|-------------------|--------------------------|---------|--------------------|--------------------------------------|---------|
| | | 1672.71 | | | |
| 250+00 | | | 9.1 | 1663.6 | |
| +10 | 24" C.M.P. Culvert. | | 9.3 = Flow Line | | 1663.4 |
| +37 ³² | B.C. | | 8.9 | | 1663.8 |
| +40 | | | 16.6 | 5.5 | 1656.1 |
| +40 | 16" Concrete Culvert. | | 12.7 = Flow Line | | 1660.0 |
| +50 | | | 11.8 | | 1660.9 |
| T.F. | | | 6.91 | | 1665.80 |
| | 1.79 | 1667.39 | | | |
| 251+00 | | | 3.7 | | 1663.9 |
| +50 | | | 4.4 | 2.3 | 1663.2 |
| 252+00 | | | 6.0 | | 1661.6 |
| +50 | | | 7.1 | 6.0 | 1660.5 |
| +77 | 7° P.T. | | 8.2 | | 1659.4 |

8

WARM AND WINDY

JAN. 9, 1928

Simpson

Clavert

Rd. E1.

1667.2[✓]

1665.3[✓]

1661.6[✓]

(9)

| Sta. | + | π | Rod on Line | Rod on 2 of Rd. 15° Rt. of Line | Elev. |
|-------------------------|------|---------|----------------|---------------------------------------|---------|
| | | 1667.59 | | | |
| 252+90 | | | 12.7 | | 1654.9 |
| 253+00 | | | 9.3 | | 1658.3 |
| +50 | | | 11.0 | 10.0 | 1656.6 |
| 254+00 | | | 13.2 | | 1654.4 |
| T.F. | | | 12.80 | | 1654.79 |
| | 0.31 | 1655.10 | | | |
| +50 | | | 2.2 | 1.3 | 1652.9 |
| +69 ³² -B.C. | | | 3.3 | | 1651.8 |
| +75 | | | 3.5 | | 1651.6 |
| 255+00 | | | 4.6 | | 1650.5 |
| +25 | | | 6.0 | | 1649.1 |
| +50 | | | 7.2 | 5.6 | 1647.9 |
| +75 | | | 7.9 | | 1647.2 |

1657.6 ✓

1653.8

1649.5

| Sta. | + | π | Rod on Line | Rod on $\frac{1}{2}$ of Rd. 15 ² R of Line | Elev. |
|--------|------------------------|---------|----------------|---|---------------------------|
| | | 1655.10 | | | |
| 256+00 | | | 8.6 | | 1646.5 |
| | +25 | | 9.6 | | 1645.5 |
| | +50 | | 13.0 | 8.1 | 1642.1 |
| | +75 | | 9.9 | | 1645.2 |
| 257+00 | | | 10.8 | | 1644.3 |
| | T.H. | | 5.29 | | 1649.81 1649.86 = B.M. |
| | 0.24 | 1650.10 | | | |
| | +05 ¹⁴ E.C. | | 5.8 | | 1644.3 |
| | +50 | | 6.2 | 5.4 | 1643.9 |
| 258+00 | | | 5.8 | | 1644.3 |
| | +50 | | 6.9 | 7.0 | 1643.2 |
| 259+00 | | | 8.3 | | 1641.8 |

Rd. El.

1647.0^v

= check on S.D. B.M. # P-3
El. = 1649.86

1644.7

1643.1

(11)

| Sta. | + | π | Rad on - Line | Rad on & of Rad on RT. of - Line | Elev. |
|--------|------------------------|---------|------------------|--|---------------------------|
| | | 1650.10 | | | |
| 259+50 | | | 10.7 | 9.2 | 1639.4 |
| TF | | | 8.91 | | 1641.19 |
| | 4.75 | 1645.94 | | | |
| 260+00 | | | 8.5 | | ^{37.4} 1641.6 |
| +50 | | | 7.5 | 6.0 | 1638.4 |
| 261+00 | | | 6.7 | | 1639.2 |
| +50 | | | 6.2 | 5.0 | 1639.7 |
| +75 | 16" C.M.P. culvert. | | 7.5 = Flow. | Line | 1638.4 |
| 262+00 | | | 5.0 | | 1640.9 |
| +50 | | | 4.6 | 4.5 | 1641.3 |
| 263+00 | | | 4.0 | | 1641.9 |
| +50 | | | 2.1 | 2.2 | 1643.8 |
| TF | | | 2.03 | | 1643.91 |

Rd. E1.

1640.9

1639.9

1640.9

1641.9

1643.7

| Sta. | + | π | Red on LINE | Red on & Rd. 15° Rt. of Line | Elev. |
|--------|------------------------|--------------------|----------------|------------------------------------|---------|
| | | | | | 1643.91 |
| | 7.60 | 1651.51 | | | |
| 263+95 | ⁸⁵ BC. | | 6.1 | | 1645.4 |
| 264+25 | | | 6.1 | | 1645.4 |
| | +50 | | 6.2 | 5.1 | 1645.3 |
| | +75 | | 6.7 | | 1644.8 |
| 265+00 | | | 11.8 | | 1639.7 |
| 265+00 | 12" G.M.P. culvert. | | 8.7 = | Flow Line | 1642.8 |
| | +25 | | 4.8 | | 1646.7 |
| | +50 | | 5.3 | 4.2 | 1646.2 |
| | +63 | ⁶⁸ E.C. | 4.8 | | 1646.7 |
| 266+00 | | | 5.1 | | 1646.4 |
| | +50 | | 4.7 | 2.1 | 1646.8 |
| TR | | | 1.95 | | 1649.36 |

(12)

Rd. Fl.

1646 A

1647 .3

1649 A

| Sta. | + | π | Redon Line | Redon & of Rd. 15° R. of Line Elev. | (13) |
|-------------------|------------------------|---------|---------------|---|----------------|
| | | | | | 1649.56 |
| | 8.73 | 1658.29 | | | |
| 267+00 | | | 10.5 | | 1647.8 |
| +50 | | | 8.8 | 6.6 | 1649.5 |
| 268+00 | | | 6.8 | | 1651.5 |
| +50 | | | 5.0 | 4.3 | 1653.3 |
| +95 ^e | 12" C.M.P. Culvert. | | 8.3 | = Flow | 1650.0 Line |
| 269+00 | | | 8.6 | | 1649.7 |
| +50 | | | 2.9 | 3.1 | 1655.4 |
| 77 | | | 2.91 | | 1655.38 |
| | 3.41 | 1658.79 | | | |
| 270+00 | | | 3.1 | | 1655.7 |
| +50 | | | 7.5 | 4.1 | 1651.3 |
| +60 ²⁰ | PI. | | 77 | | 1651.1 |

1651.7

1654.0

1655.2

1654.7

(14)

| Sta. | + | π | Rod on Line | Rod on & Rd 15° Rt. of Line | Elev |
|--------|------|--------------------------|----------------|-----------------------------------|----------|
| | | 1658.79 | | | |
| 271+00 | | | 6.7 | | 1652.1 ✓ |
| | +50 | | 9.8 | 7.6 | 1649.0 ✓ |
| 272+00 | | | 13.9 | | 1644.9 ✓ |
| | T.P. | | 12.73 | | 1646.66 |
| | 0.79 | 1647.45 | | | |
| | +50 | | 5.6 | 1.0 | 1641.9 ✓ |
| 273+00 | | | 5.8 | | 1641.7 ✓ |
| | +50 | | 5.4 | 27 | 1642.1 ✓ |
| 274+00 | | | 9.7 | | 1638.1 ✓ |
| | +50 | | 7.6 | 5.1 | 1639.9 ✓ |
| 275+00 | | | 8.3 | | 1639.2 ✓ |
| | +50 | | 12.5 | 9.9 | 1635.0 ✓ |
| +63 | | 14" Concrete Culvert. | 16.2 | = Flow Line | |

1651.2

1646.5

1644.8

1642.4

1637.6

1631.3

(15)

| Sta. | + | π | Rod on - LINE | Rod on & of Rod, 15' Rod - Line | Elev. |
|--------|------|--------------------------|------------------|---------------------------------------|---------|
| | | 1647.45 | | | |
| T.F. | | | 11.31 | | 1636.14 |
| | 3.84 | 1639.98 | | | |
| 276+00 | | | 7.3 | | 1632.7 |
| +50 | | | 6.9 | 4.2 | 1633.1 |
| 277+00 | | | 8.9 | | 1631.1 |
| +45 | | 12" Concrete Culvert. | 11.4 | = Flow Line | 1628.6 |
| +50 | | | 9.5 | 7.1 | 1630.5 |
| 278+00 | | | 8.2 | | 1631.8 |
| +50 | | | 5.3 | 3.6 | 1634.7 |
| 279+00 | | | 5.6 | | 1634.4 |
| +50 | | | 5.2 | 2.4 | 1634.8 |
| T.F. | | | 2.58 | | 1637.40 |
| | 2.37 | 1639.77 | | | |
| 280+00 | | | 5.3 | | 1634.5 |

Rd. El.

1635.8

1632.9

1636.4

1637.6

(16)

| Sta. | + | x | Rod on Line | Rod on & Rd. 15' Pt. of Line | Elev. |
|--------|------|---------|----------------|------------------------------------|---------|
| | | 1639.77 | | | |
| 280+50 | | | 7.2 | 5.0 | 1632.6 |
| 281+00 | | | 10.1 | | 1629.7 |
| +50 | | | 14.2 | 10.4 | 1625.6 |
| T.F. | | | 12.41 | | 1627.36 |
| | 0.37 | 1627.73 | | | |
| 282+00 | | | 4.0 | | 1623.7 |
| +50 | | | 7.7 | 4.4 | 1620.0 |
| 283+00 | | | 10.5 | | 1617.2 |
| +50 | | | 12.8 | 10.0 | 1614.9 |
| T.F. | | | 12.23 | | 1615.50 |
| | 2.20 | 1617.70 | | | |
| 284+00 | | | 5.1 | | 1612.6 |
| +50 | | | 6.0 | 3.8 | 1611.7 |

Rd. El.

1634.8

1629 A

1623.3

1617.7

1613.9

(17)

| Sta | + | T | Rod on LINE | Rod on P Rd. 15° Plot - Line Elev. | Elev. |
|--------|------|---------|----------------|--|---------|
| | | 1617.70 | | | |
| 285+00 | | | 8.0 | | 1609.7 |
| | +50 | | 10.3 | 8.3 | 1607.4 |
| 286+00 | | | 12.1 | | 1605.6 |
| | +50 | | 14.2 | 12.1 | 1603.5 |
| TF | | | 9.77 | | 1607.93 |
| | 2.36 | 1610.62 | | | 1607.96 |
| 287+00 | | | 7.7 | | 1602.9 |
| | +50 | | 8.6 | 7.3 | 1602.0 |
| 288+00 | | | 10.3 | | 1600.3 |
| | +50 | | 10.4 | 8.8 | 1600.2 |
| 289+00 | | | 10.1 | | 1600.5 |
| | +50 | | 8.9 | 8.2 | 1601.7 |
| 290+00 | | | 6.0 | | 1604.6 |

1609 A

1605.6

= Check on BM # P-5

Elev. = 1607.96

1603.3

1601.8

1602.4

| Sta. | + | x | Red on Line | Red on & Rd. 15-Rt. 4 Line Elev. | (18) |
|-------------------------|------|---------|----------------|--|------------------------|
| | | 1610.62 | | | |
| 290+50 | | | 4.5 | 4.7 | 1604.1 ⁶ |
| 291+00 | | | 4.4 | | 1604.2 ⁶ |
| +50 | | | 4.0 | 5.1 | 1606.6 [✓] |
| 292+00 | | | 8.0 | | 1602.6 [✓] |
| T.F. | | | 12.61 | | 1598.01 |
| | 0.56 | 1598.57 | | | |
| +50 | | | 1.5 | 1.2 | 1597.7 [✓] |
| 293+00 | | | 6.5 | | 1592.7 [✓] |
| +50 | | | 10.7 | 10.5 | 1587.9 ^{88.0} |
| T.F. | | | 12.43 | | 1586.14 |
| | 1.85 | 1587.99 | | | |
| 294+00 | | | 4.2 | | 1583.8 |
| +19 ²¹ -P.I. | | | 5.6 | | 1582.4 |

Rd. El.

1605.9 ✓

1605.5 ✓

1597.3 ✓

1588.7 ✓

| Sta | + | π | Rod on Line | Rod on \angle Road | Elel. |
|--------|---------------------|---------|----------------|--|---------|
| | | 1587.99 | | | (19) |
| 294+50 | | | 6.1 | | 1581.9 |
| +59 | $\frac{52}{-}$ P.I. | | 6.1 | | 1581.9 |
| 295+00 | | | 7.8 | | 1580.2 |
| +50 | | | 10.0 | | 1578.0 |
| 296+00 | | | 11.6 | $\frac{11\frac{1}{2}}{12\frac{1}{2}}$ Dist. over | 1576.4 |
| T.F. | | | 12.58' | | 1575.4' |
| | 1.69 | 1577.10 | | | |
| +50 | | | 2.2 | | 1574.9 |
| 297+00 | | | 3.8 | | 1573.3 |
| +50 | | | 4.9 | | 1572.2 |
| 298+00 | | | 5.8 | $\frac{5\frac{1}{2}}{13\frac{1}{2}}$ | 1571.3 |
| +50 | | | 6.3 | | 1570.8 |
| 299+00 | | | 7.1 | | 1570.0 |

19

1576.8

1572.0

| Sta. | + | τ | Rod on Line | Rod on & Rd. | Elev. |
|--------|------|---------|----------------|--------------------|---------|
| | | 1577.10 | | | |
| 299+50 | | | 8.1 | | 1569.0 |
| 300+00 | | | 9.2 | $\frac{86}{120} L$ | 1567.9 |
| TH | | | 9.03 | | 1568.07 |
| | 1.70 | 1569.77 | | | |
| +50 | | | 2.9 | | 1563.9 |
| 301+00 | | | 3.8 | | 1566.0 |
| +50 | | | 4.9 | | 1564.9 |
| 302+00 | | | 5.9 | $\frac{59}{100} L$ | 1563.9 |
| TH | | | 7.42 | | 1562.35 |
| | 0.08 | 1562.43 | | | |
| +50 | | | 0.0 | | 1562.4 |
| 303+00 | | | 0.9 | | 1561.5 |
| +50 | | | 1.9 | | 1560.5 |

(20)

20

1568.5

1559.4

| Sta. | + | + | Rod on Line | Rod on & Rd | Elev. |
|--------|------|---------|----------------|-----------------------|---------|
| | | 1562.73 | | | |
| 304+00 | | | 3.6 | $\frac{3^2}{10^2} L$ | 1558.8 |
| | +50 | | 5.0 | | 1557.4 |
| 305+00 | | | 6.3 | | 1556.1 |
| 306+00 | | | 7.9 | $\frac{7^2}{11^2} L$ | 1554.5 |
| 307+00 | | | 10.2 | | 1552.2 |
| 308+00 | | | 12.2 | $\frac{11^2}{10^2} L$ | 1550.2 |
| | T.R. | | 11.75 | | 1550.68 |
| | 0.85 | 1551.53 | | | |
| 309+00 | | | 2.8 | | 1548.7 |
| 310+00 | | | 4.6 | $\frac{4^2}{11^2} L$ | 1546.9 |
| 311+00 | | | 6.7 | | 1544.8 |
| 312+00 | | | 8.2 | $\frac{7^2}{11^2} L$ | 1543.3 |
| 313+00 | | | 9.9 | | 1541.6 |

(21)

1559.2

1554.7

1550.7

1547.0

1543.7

| Sta. | + | π | Radon line - | Radon & Rd. - | 22 Elev |
|--------|------|---------|--------------------|--------------------------|----------------------------------|
| | | 1551.53 | | | |
| T.H. | | | 10.18 | | 1541.35 |
| | 1.03 | 1542.38 | | | |
| 314+00 | | | 2.3 | $\frac{2.7}{12^\circ L}$ | 1540.1 |
| 315+00 | | | 4.3 | | 1538.1 |
| 316+00 | | | 5.7 | $\frac{5.7}{11^\circ L}$ | 1536.7 |
| 317+00 | | | 7.5 | | 153 8 ⁴ .9 |
| 318+00 | | | 8.5 | $\frac{8.4}{10^\circ L}$ | 1533.9 |
| 319+00 | | | 10.0 | | 1532.4 |
| T.H. | | | 10.10 | | 1532.28 |
| | 2.16 | 1534.44 | | | |
| 320+00 | | | 3.1 | $\frac{3.0}{11^\circ L}$ | 1531.3 |
| 321+00 | | | 4.5 | | 1529.9 |
| 322+00 | | | 5.8 | $\frac{5.7}{11^\circ L}$ | 1528.6 |
| 323+00 | | | 6.6 | | 1527.8 |

1540.0

1536.7

1539.0

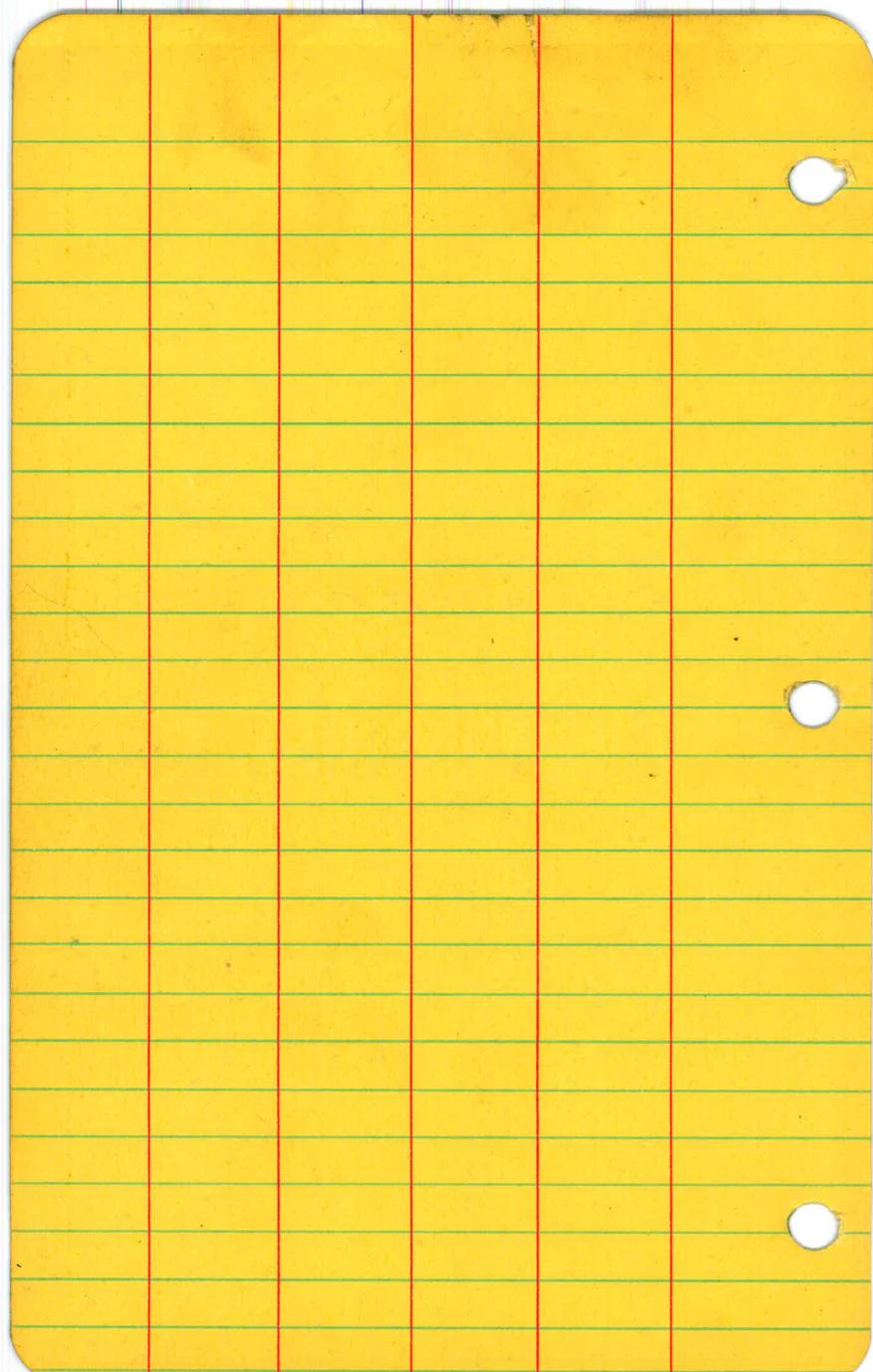
1531.4

1528.7

| Sta. | + | π | Rod on Line | Rod on Rd | Elev. |
|--------|-----------------------|---------|-------------------|--------------|---------|
| | | 1534.44 | | | |
| 323+37 | ⁴² P.I. | | 7.5 | | 1526.9 |
| | | | Int. of Base Line | | |
| T.F. | | | 7.28 | | 1527.16 |
| | 3.08 | 1530.24 | | | |
| T.F. | | | 9.83 | | 1520.41 |
| | 2.27 | 1522.68 | | | |
| | | | 5.19 | | 1517.79 |

Check on B.M. #

$$\text{Elev.} = 1517.56 - 1517.84$$



Center of Road opp 316+00

Center of Road opp 318+00

Center of Road opp 320+00

| Sta. | + | π | - | Elev. |
|--------|-------|----------|-------|----------|
| | | 1539.023 | | |
| T.F. | | | 7.328 | 1531.695 |
| | 3.651 | 1535.346 | | |
| 320+50 | | | 4.3 | 1531.0 ✓ |
| 321+00 | | | 5.2 | 1530.1 ✓ |
| +50 | | | 5.5 | 1529.8 ✓ |
| 322+00 | | | 6.2 | 1529.1 ✓ |
| | | | 6.2 | 1529.1 ✓ |
| +50 | | | 6.7 | 1528.6 ✓ |
| 323+00 | | | 8.2 | 1527.1 ✓ |
| +50 | | | 8.2 | 1527.1 ✓ |
| T.F. | | | 8.050 | 1527.296 |
| | 2.570 | 1529.866 | | |
| +83 | P.I. | | 2.6 | 1527.3 ✓ |
| 324+00 | | | 2.8 | 1527.1 ✓ |

43

Center of Rd. opp 322+00

x start plotting here ✓
7/1

| Sta. | + | I | - | Elev. |
|--------|---|----------|-------|----------|
| | | 1529.866 | | |
| 324+50 | | | 3.5 | 1526.4 |
| | | | 3.1 | 1526.8 ✓ |
| 325+00 | | | 3.9 | 1526.0 ✓ |
| +50 | | | 4.0 | 1525.9 ✓ |
| 326+00 | | | 4.6 | 1525.3 ✓ |
| | | | 4.7 | 1525.2 ✓ |
| +50 | | | 5.1 | 1524.8 ✓ |
| 327+00 | | | 5.8 | 1524.1 ✓ |
| +50 | | | 6.7 | 1523.2 ✓ |
| 328+00 | | | 7.3 | 1522.6 ✓ |
| | | | 8.3 | 1521.6 ✓ |
| +50 | | | 7.8 | 1522.1 ✓ |
| TF | | | 9.263 | 1520.603 |

center of Rd. opp. 330+00

center of Rd. opp 332+00

B.M. # P-7 — Large spike in
Power Pole # 19079 — 40' East
of Sta. 332+20
Elev. = 1517.564

Point N

| Sta | + | π | - | Elev. | |
|--------|-------|----------|-------|----------|---|
| | | | | 1517.564 | |
| | 1.335 | 1518.899 | | | |
| 333+50 | | | 4.2 | 1514.7 | ✓ |
| 334+00 | | | 5.1 | 1513.8 | ✓ |
| | | | 4.0 | 1514.9 | ✓ |
| +50 | | | 5.9 | 1513.0 | ✓ |
| 335+00 | | | 7.3 | 1511.6 | ✓ |
| +50 | | | 8.7 | 1510.2 | ✓ |
| 336+00 | | | 7.0 | 1511.9 | ✓ |
| | | | 4.9 | 1514.0 | ✓ |
| +50 | | | 6.4 | 1512.5 | ✓ |
| 337+00 | | | 6.1 | 1512.8 | ✓ |
| +50 | | | 7.2 | 1511.7 | ✓ |
| T.P. | | | 7.573 | 1511.326 | |

46

center of Rd. opp. 334+00

center of Rd. opp 336+00

Revised
2/

| Sta. | + | π | - | Elev |
|--------|-------|----------|-----|----------|
| | | | | 1511.326 |
| | 0.971 | 1512.297 | | |
| 338+00 | | | 1.8 | 1510.5 ✓ |
| | | | 1.9 | 1510.4 ✓ |
| +50 | | | 2.0 | 1510.3 ✓ |
| 339+00 | | | 3.1 | 1509.2 ✓ |
| +50 | | | 4.2 | 1508.1 ✓ |
| 340+00 | | | 5.5 | 1506.8 ✓ |
| | | | 5.1 | 1507.2 ✓ |
| +50 | | | 6.2 | 1506.1 ✓ |
| 341+00 | | | 6.8 | 1505.5 ✓ |
| +50 | | | 7.5 | 1504.8 ✓ |
| 342+00 | | | 8.6 | 1503.7 ✓ |
| | | | 8.0 | 1504.3 ✓ |

47

center of Rd opp 338+00

center of Rd opp 340+00

center of Rd opp 342+00

center
of Rd

| Sta. | + | π | - | Elev. |
|--------|-------|----------|-------|----------|
| | | 1512.297 | | |
| 342+50 | | | 8.7 | 1503.6 ✓ |
| 343+00 | | | 9.2 | 1503.1 ✓ |
| TR | | | 9.597 | 1502.700 |
| | 1.944 | 1504.644 | | |
| +50 | | | 2.7 | 1501.9 ✓ |
| 344+00 | | | 3.0 | 1501.6 ✓ |
| | | | 3.2 | 1501.4 ✓ |
| +50 | | | 3.5 | 1501.1 ✓ |
| 345+00 | | | 4.2 | 1500.4 ✓ |
| +50 | | | 4.6 | 1500.0 ✓ |
| 346+00 | | | 5.5 | 1499.1 ✓ |
| | | | 5.5 | 1499.1 ✓ |
| +50 | | | 6.2 | 1498.4 ✓ |

48

center of Rd. opp 344+00

center of Rd. opp 346+00

center
m.

| Sta. | + | π | - | Elev. |
|--------|-------|----------|-------|-----------------------|
| | | 1509.699 | | |
| 347+00 | | | 6.8 | 1497.8 ✓ |
| +50 | | | 7.8 | 1496.8 ✓ |
| 348+00 | | | 8.3 | 1496.5 ✓ |
| +50 | | | 9.8 | 1494.8 ✓ |
| | | | 8.6 | 1496.0 ✓ |
| 349+00 | | | 9.9 | 1494.7 ✓ |
| +50 | | | 10.4 | 1494.2 ✓ |
| 7H | | | 8.040 | 1496.604 = B.M. # R-8 |
| | 0.382 | 1496.986 | | |
| 350+00 | | | 3.4 | 1493.6 ✓ |
| | | | 2.6 | 1494.4 ✓ |
| +50 | | | 4.1 | 1492.9 ✓ |
| 351+00 | | | 3.9 | 1493.1 ✓ |

49

Center of Rd. opp 348+50

B.M. # P. 8 - Large spike
in Power Pole # 14074 -
40' East of Sta. 349+80
Elev. = 1496.604

Center of Rd. opp 350+00

Plotter
M

| Sta. | + | π | - | Elev. |
|--------|-------|----------|-------|----------|
| | | 1496.986 | | |
| 351+50 | | | 4.3 | 1492.7 ✓ |
| 352+00 | | | 5.1 | 1491.9 ✓ |
| | | | 5.0 | 1492.0 ✓ |
| +50 | | | 5.9 | 1491.1 ✓ |
| 353+00 | | | 7.1 | 1489.9 ✓ |
| +50 | | | 7.6 | 1489.4 ✓ |
| 354+00 | | | 7.8 | 1489.2 ✓ |
| | | | 6.6 | 1490.4 ✓ |
| +50 | | | 8.5 | 1488.5 ✓ |
| TP | | | 7.680 | 1489.306 |
| | 3.118 | 1492.424 | | |
| 355+00 | | | 4.5 | 1487.9 ✓ |
| +50 | | | 4.9 | 1487.5 ✓ |

center of Rd. opp 352+00

center of Rd opp 354+00

| Sta | + | π | - | Elev. |
|---------------|-------|----------|-------|----------|
| | | 1492.424 | | |
| 356+00 | | | 5.1 | 1487.3 ✓ |
| | | | 4.1 | 1488.3 ✓ |
| +50 | | | 5.4 | 1487.0 ✓ |
| 357+00 | | | 5.7 | 1486.7 ✓ |
| 7F | | | 6.790 | 1485.634 |
| | 3.715 | 1489.349 | | |
| +50 | | | 2.9 | 1486.4 ✓ |
| 358+00 | | | 3.2 | 1486.1 ✓ |
| | | | 2.3 | 1487.0 ✓ |
| +50 | | | 3.6 | 1485.7 ✓ |
| 359+00 | | | 3.2 | 1486.1 ✓ |
| +50 | | | 4.6 | 1484.7 ✓ |
| 360+00 | | | 4.9 | 1484.4 ✓ |

Nov. 23, 1927

Windy And Cold

Simpson - Inst.

Clavert - Rad

center of Rd. opp 356+00

center of Rd. opp 358+00

| Sta | + | T | - | Elev. |
|--------|---|----------|-------|-----------------------|
| | | 1489.349 | | |
| | | | 4.6 | 1484.7 ✓ |
| 360+50 | | | 5.3 | 1484.0 ✓ |
| 361+00 | | | 5.8 | 1483.5 ✓ |
| 362+00 | | | 5.5 | 1483.8 ✓ |
| | | | 4.5 | 1484.8 ✓ |
| 363+00 | | | 4.3 | 1485.0 ✓ |
| 364+00 | | | 5.2 | 1484.1 ✓ |
| | | | 4.5 | 1484.8 ✓ |
| 365+00 | | | 4.3 | 1485.0 ✓ |
| 366+00 | | | 3.7 | 1485.6 ✓ |
| | | | 4.0 | 1485.3 ✓ |
| 367+00 | | | 4.6 | 1484.7 ✓ |
| TF | | | 4.293 | 1485.056 = B.M. # P-9 |

52

center of Rd opp 360+00

center of Rd opp 362+00

center of Rd opp 364+00

center of Rd opp 366+00

B.m. # P-9 - Nail in Power Pole # 14069

40' East of Sta. 367+30

Elev. = 1485.056

| Sta. | + | π | - | Elev |
|--------|-------|----------|-------|----------|
| | | | | 1485.056 |
| | 2.901 | 1487.957 | | |
| 368+00 | | | 5.0 | 1483.0 ✓ |
| | | | 4.1 | 1483.9 ✓ |
| 369+00 | | | 5.3 | 1482.7 ✓ |
| 370+00 | | | 8.4 | 1479.6 ✓ |
| | | | 8.1 | 1479.9 ✓ |
| 371+00 | | | 4.8 | 1483.2 ✓ |
| IF | | | 4.833 | 1483.124 |
| | 5.618 | 1488.742 | | |
| 372+00 | | | 5.1 | 1483.6 ✓ |
| | | | 4.8 | 1483.9 ✓ |
| 373+00 | | | 4.7 | 1484.0 ✓ |
| 374+00 | | | 5.8 | 1482.9 ✓ |

Center of Rd. opp 368+00

Center of Rd opp 370+00

Center of Rd. opp 372+00

| Sta | + | π | - | Elev |
|--------|-------|----------|-------|----------|
| | | 1488.792 | | |
| | | | 4.6 | 1489.1 ✓ |
| TF | | | 0.407 | 1488.335 |
| | 8.691 | 1497.026 | | |
| 375+00 | | | 7.4 | 1489.6 ✓ |
| 376+00 | | | 3.8 | 1493.2 ✓ |
| | | | 3.7 | 1493.3 ✓ |
| 377+00 | | | 4.9 | 1492.1 ✓ |
| 378+00 | | | 5.3 | 1491.7 ✓ |
| | | | 5.5 | 1491.5 ✓ |
| 379+00 | | | 6.9 | 1490.1 ✓ |
| TF | | | 7.126 | 1489.900 |
| | 2.810 | 1492.710 | | |
| 380+00 | | | 6.8 | 1485.9 ✓ |

center of Rd opp 374+00

center of Rd opp 376+00

center of Rd opp 378+00

| Sta | + | π | - | Elev. |
|--------|-------|----------|--------|----------|
| | | 1492.710 | | |
| | | | 4.6 | 1488.1 ✓ |
| 381+00 | | | 4.0 | 1488.7 ✓ |
| 382+00 | | | 10.0 | 1482.7 ✓ |
| TF | | | 11.670 | 1481.040 |
| | 0.520 | 1481.560 | | |
| | | | 0.0 | 1481.6 ✓ |
| 383+00 | | | 6.3 | 1475.3 ✓ |
| 384+00 | | | 9.9 | 1471.7 ✓ |
| | | | 9.4 | 1472.2 ✓ |
| 385+00 | | | 12.4 | 1469.2 ✓ |
| TF | | | 11.808 | 1469.752 |
| | 4.767 | 1474.519 | | |
| 386+00 | | | 5.2 | 1469.3 ✓ |

center of Rd. opp 380+00

center of Rd. opp 382+00

center of Rd. opp 384+00

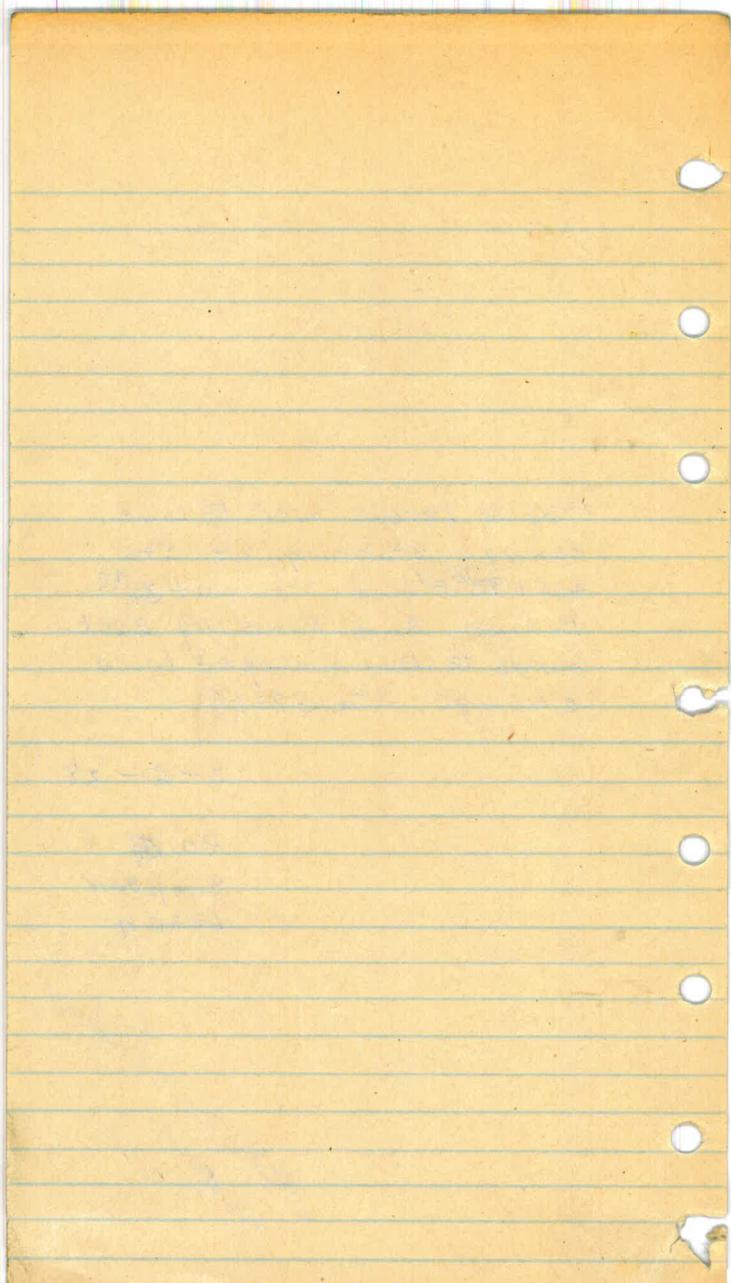
| Sta | + | π | - | Elev |
|--------|------------------------|----------|-------|----------|
| | | 1474.519 | | |
| | | | 5.2 | 1469.3 ✓ |
| 387+00 | | | 4.8 | 1469.7 ✓ |
| 388+00 | | | 4.3 | 1470.2 ✓ |
| | | | 4.3 | 1470.2 ✓ |
| 389+00 | | | 4.3 | 1470.2 ✓ |
| | T.F. | | 3.979 | 1470.540 |
| | 5.960 | 1476.500 | | |
| 390+00 | | | 5.2 | 1471.3 ✓ |
| | | | 5.3 | 1471.2 ✓ |
| 391+00 | | | 5.2 | 1471.3 ✓ |
| | +53 ²⁸ P.I. | | 5.0 | 1471.5 ✓ |
| 392+00 | | | 4.8 | 1471.7 ✓ |
| 393+00 | | | 7.6 | 1468.9 ✓ |

Profile Levels over P-Line
change, starting at Sta
415+92⁹² P-Line, sta 410+34⁴⁰
P-Line, And Running Back-
wards to Beginning of Line
change, Sta. 393+⁹

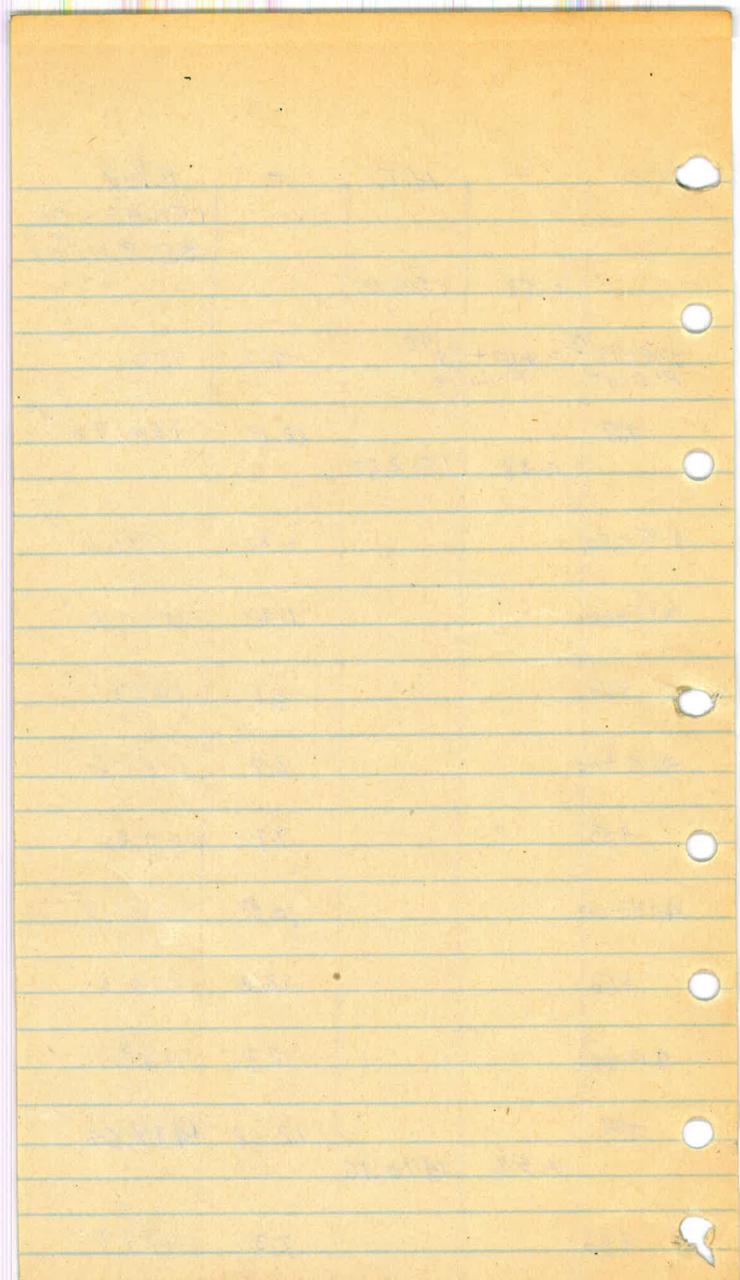
2-6-28

P.O. G
Simpson
Leach

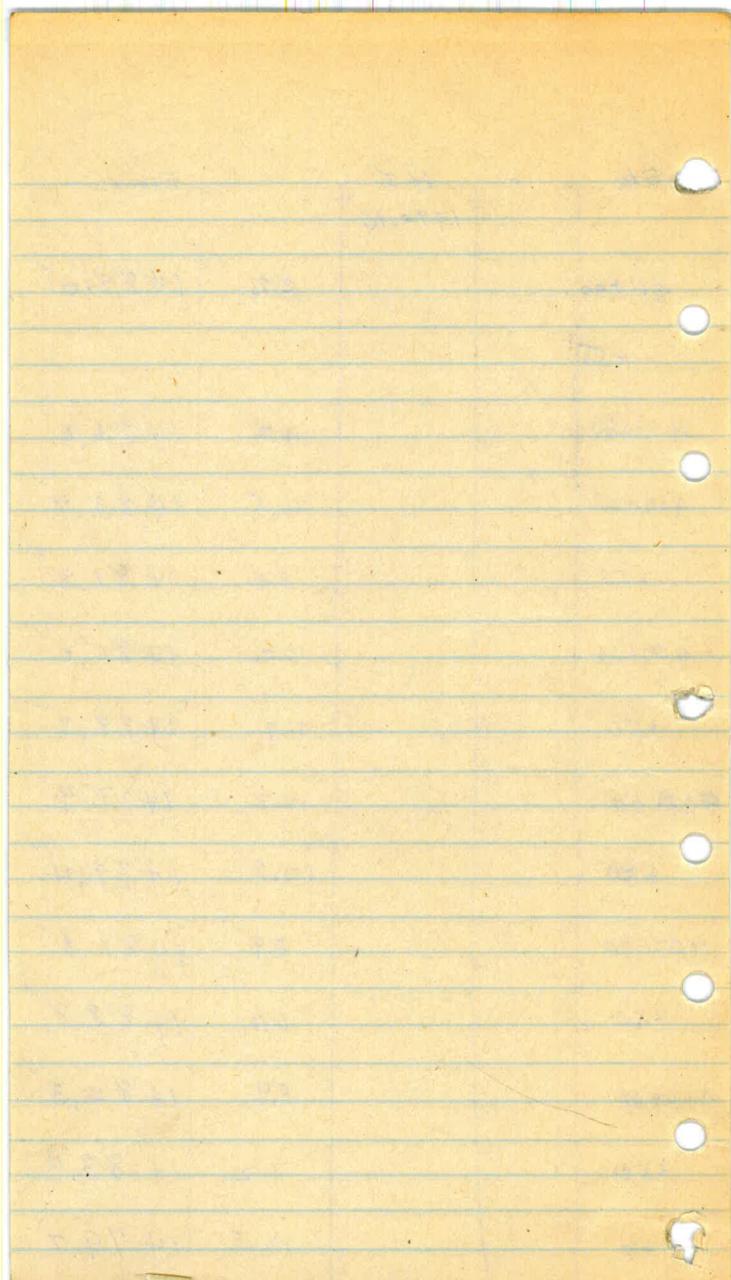
Plotted & checked
2/11/28



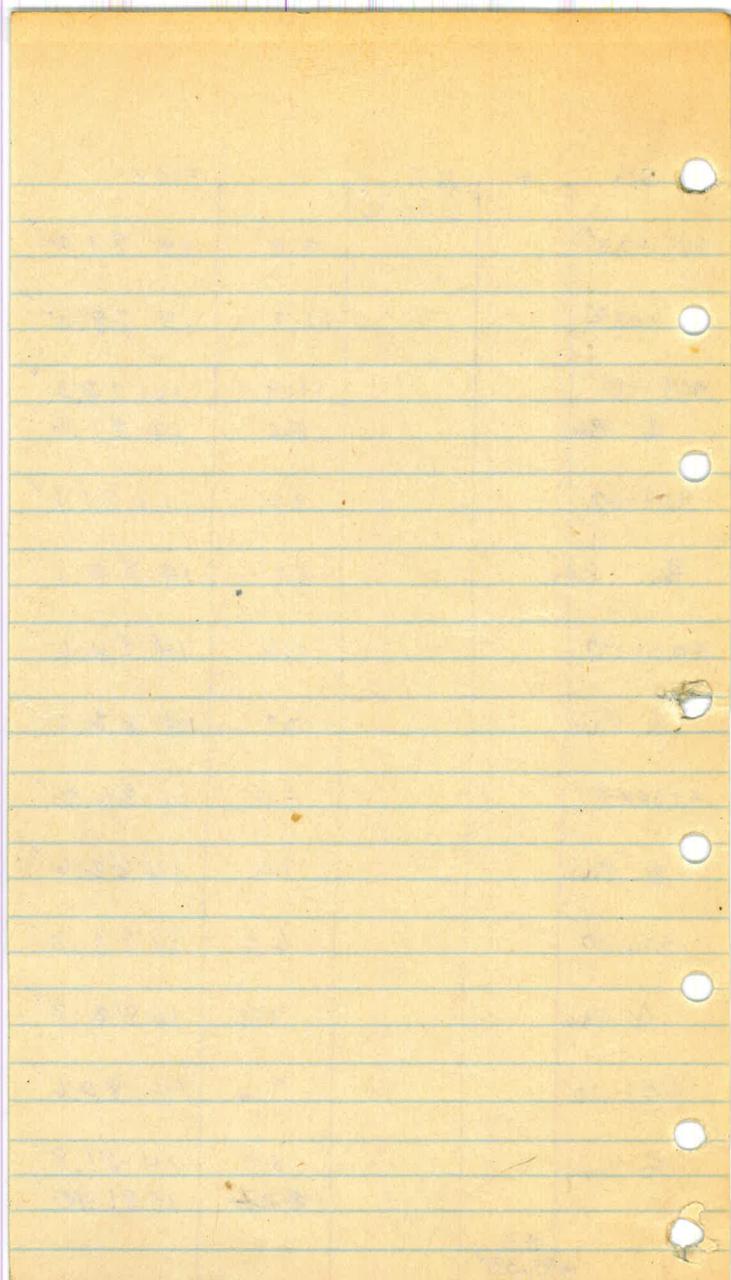
| Sta. | + | H.I. | - | Elev. |
|--------------------------------|----------------------------------|-----------|-------|-------------------------------|
| | | | | 1511.43 = El. S.D.B.M. #28 |
| | 2.58 | 1514.01 ✓ | | |
| 415+92 ⁹² P-Line | = 410+34 ⁹⁰ P-Line | | 12.2 | 1501.8 ✓ |
| T.P. | | | 12.18 | 1501.83 ✓ |
| | 0.39 | 1502.22 ✓ | | |
| 415+50 | | | 0.8 | 1501.4 ✓ |
| 415+00 | | | 1.4 | 1500.8 ✓ |
| +50 | | | 4.1 | 1498.1 ✓ |
| 414+00 | | | 6.8 | 1495.4 ✓ |
| +50 | | | 9.7 | 1492.5 ✓ |
| 413+00 | | | 10.5 | 1491.7 ✓ |
| +50 | | | 12.2 | 1490.0 ✓ |
| 412+00 | | | 12.7 | 1489.5 ✓ |
| T.P. | | | 12.58 | 1489.64 ✓ |
| | 0.52 | 1490.16 ✓ | | |
| +50 | | | 2.3 | 1487.9 ✓ |



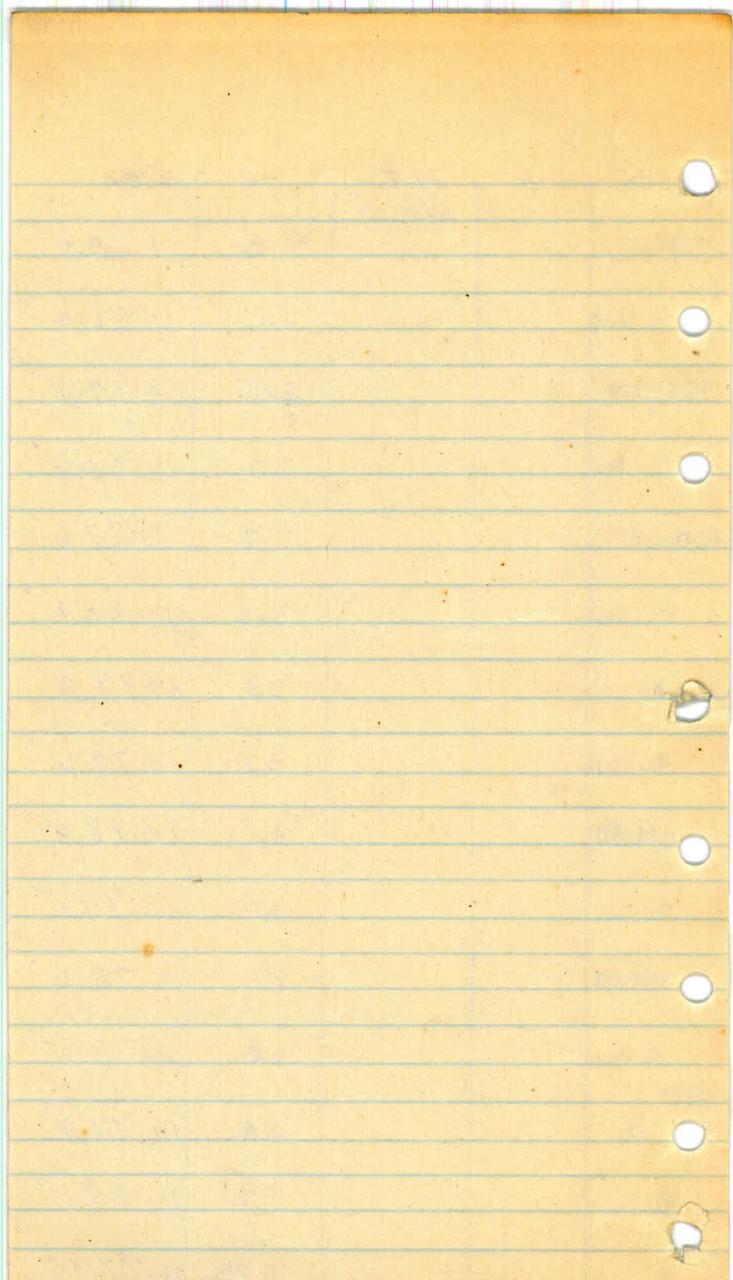
| Sta | + | H.I. | - | Elev. |
|--------|---|---------|------|----------|
| | | 1490.16 | | |
| 911+00 | | | 2.2 | 1488.0 ✓ |
| +50 | | | | |
| 410+50 | | | 4.2 | 1486.0 ✓ |
| 410+00 | | | 6.5 | 1483.7 ✓ |
| +50 | | | 8.4 | 1481.8 ✓ |
| 409+00 | | | 10.2 | 1480.0 ✓ |
| +50 | | | 11.9 | 1478.3 ✓ |
| 408+00 | | | 12.3 | 1477.9 ✓ |
| +50 | | | 10.8 | 1479.4 ✓ |
| 407+00 | | | 8.9 | 1481.3 ✓ |
| +50 | | | 6.4 | 1483.8 ✓ |
| 406+00 | | | 5.9 | 1484.3 ✓ |
| +50 | | | 7.2 | 1483.0 ✓ |
| +40 | | | 10.5 | 1479.7 ✓ |



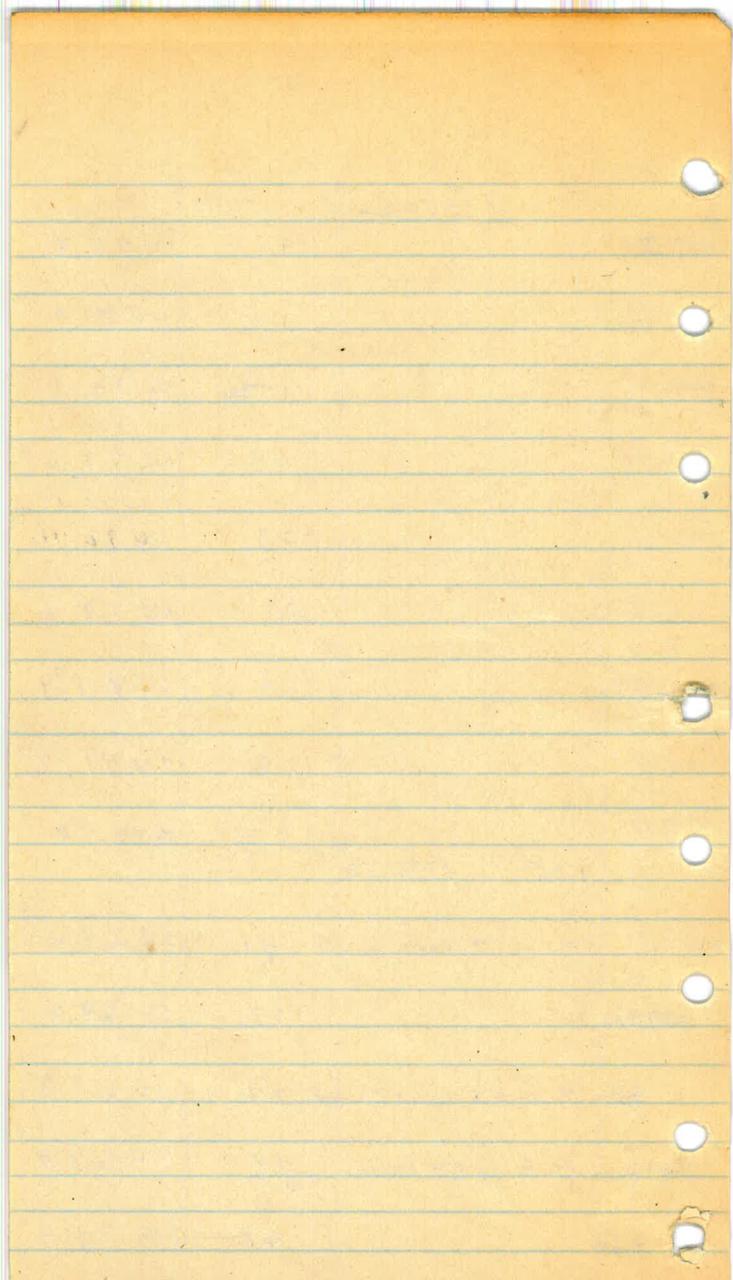
| Sta | + | H.I. | - | Elev. |
|----------------------|---|-----------|-------|-----------|
| 405+23 ⁸¹ | | 1490.16 ✓ | 9.0 | 1481.2 ✓ |
| +03 ⁸¹ | | | 11.7 | 1478.5 ✓ |
| 404+50 | | | 11.9 | 1478.3 ✓ |
| ⊕ Pav. | | | 8.6 | 1481.6 ✓ |
| 404+00 | | | 9.1 | 1481.1 ✓ |
| ⊕ Pav. | | | 8.1 | 1482.1 ✓ |
| 403+50 | | | 5.6 | 1484.6 ✓ |
| ⊕ Pav. | | | 7.7 | 1482.5 ✓ |
| 403+00 | | | 4.0 | 1486.2 ✓ |
| ⊕ Pav. | | | 7.0 | 1482.6 ✓ |
| 402+50 | | | 6.9 | 1483.3 ✓ |
| ⊕ Pav. | | | 7.9 | 1482.3 ✓ |
| 402+00 | | | 9.6 | 1480.6 ✓ |
| ⊕ Pav. | | | 8.3 | 1481.9 ✓ |
| | | 1481.16 | 18.26 | 1481.90 ✓ |
| | | 143 | | |
| | | 1483.33 ✓ | | |

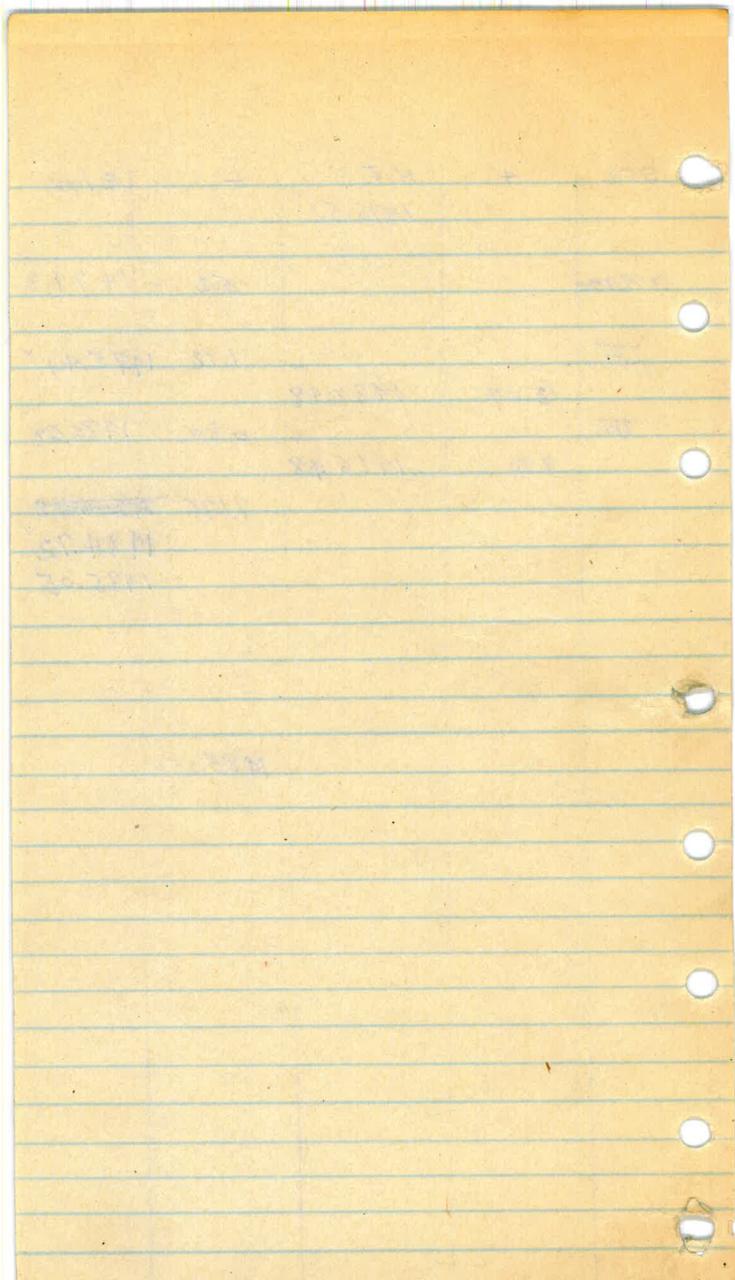


| Sta | + | H.I. | - | Elev. |
|-------------------|---|---------|-----|----------|
| 407+50 | | 1423.33 | 4.3 | 1479.0 ✓ |
| ⊕ Pav. | | | 2.1 | 1481.2 ✓ |
| 407+00 | | | 5.5 | 1477.8 ✓ |
| ⊕ Pav. | | | 2.7 | 1480.6 ✓ |
| 400+50 | | | 5.7 | 1477.6 ✓ |
| ⊕ Pav. | | | 3.2 | 1480.1 ✓ |
| 400+00 | | | 3.4 | 1479.9 ✓ |
| ⊕ Pav. | | | 3.7 | 1479.6 ✓ |
| 399+50 | | | 4.5 | 1478.8 ✓ |
| ⊕ Pav. | | | 4.2 | 1479.1 ✓ |
| 399+00 | | | 4.7 | 1478.6 ✓ |
| ⊕ Pav. | | | 4.8 | 1478.5 ✓ |
| 399 | | | | |
| +50 | | | 5.4 | 1477.9 ✓ |
| ⊕ Pav. | | | 5.2 | 1478.1 ✓ |
| + | | | 6.2 | 1477.1 ✓ |



| | | | | |
|--------|------------------------------------|-----------|------|-----------|
| 3 | | 1483.33 ✓ | | |
| 398+00 | | | 9.1 | 1474.2 ✓ |
| +50 | | | 11.4 | 1471.9 ✓ |
| 397+00 | | | 11.7 | 1472.1 ✓ |
| +50 | | | 10.9 | 1472.4 ✓ |
| 396+00 | | | 10.9 | 1472.4 ✓ |
| +50 | | | 10.7 | 1472.6 ✓ |
| 395+00 | | | 11.4 | 1471.9 ✓ |
| +50 | | | 11.6 | 1471.7 ✓ |
| T.P. | | | 8.75 | 1474.58 ✓ |
| | 1.95 | 1476.53 ✓ | | |
| 394+15 | S.B. of S ^a Maria Creek | | 7.1 | 1469.4 ✓ |
| 394+00 | | | 7.3 | 1469.2 ✓ |
| +50 | E of S ^a Maria Creek | | 7.7 | 1468.8 ✓ |
| 393+00 | N.B. of S ^a Maria Creek | | 7.6 | 1468.9 ✓ |
| +50 | | | 4.8 | 1471.7 ✓ |

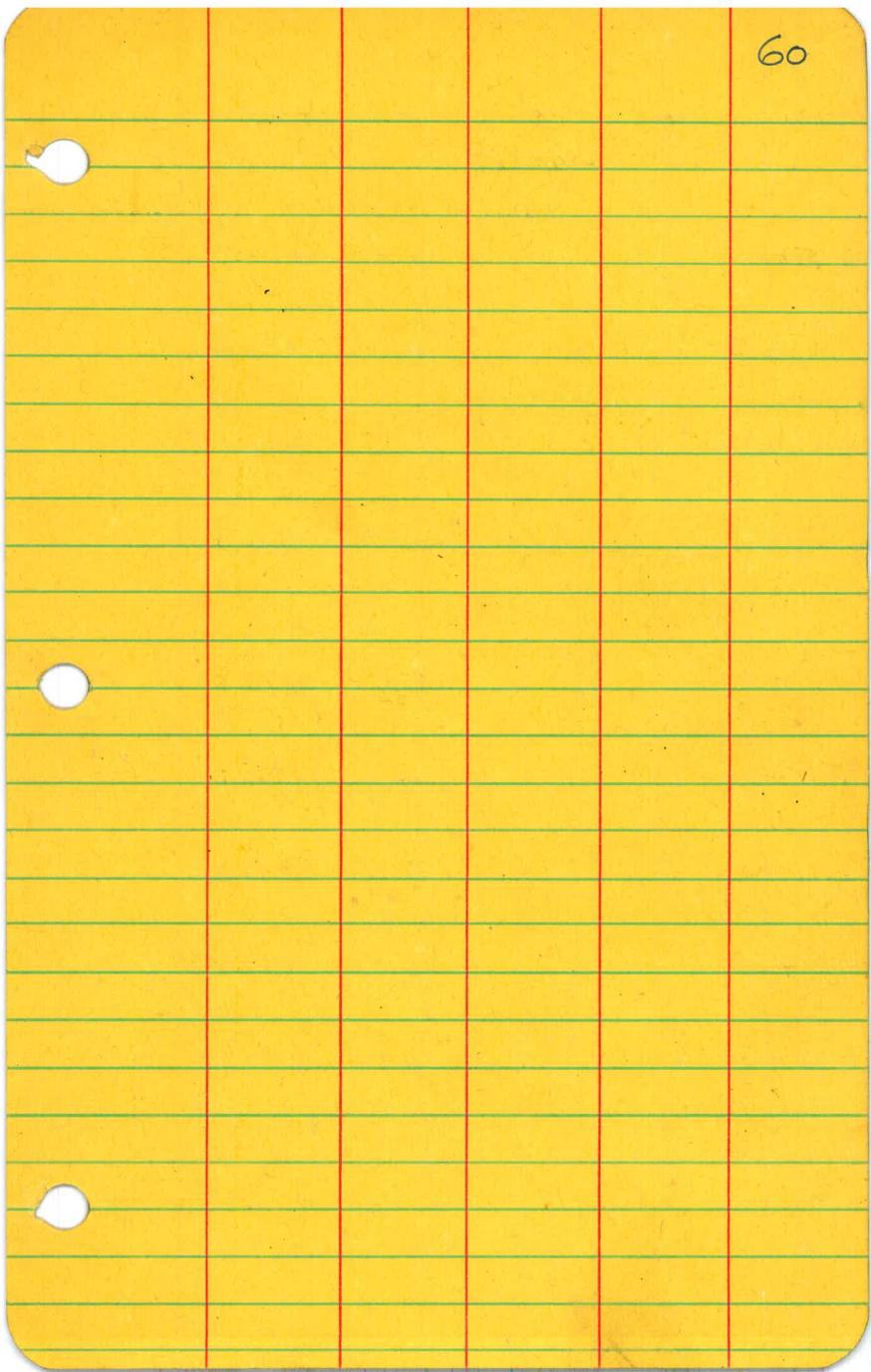




59

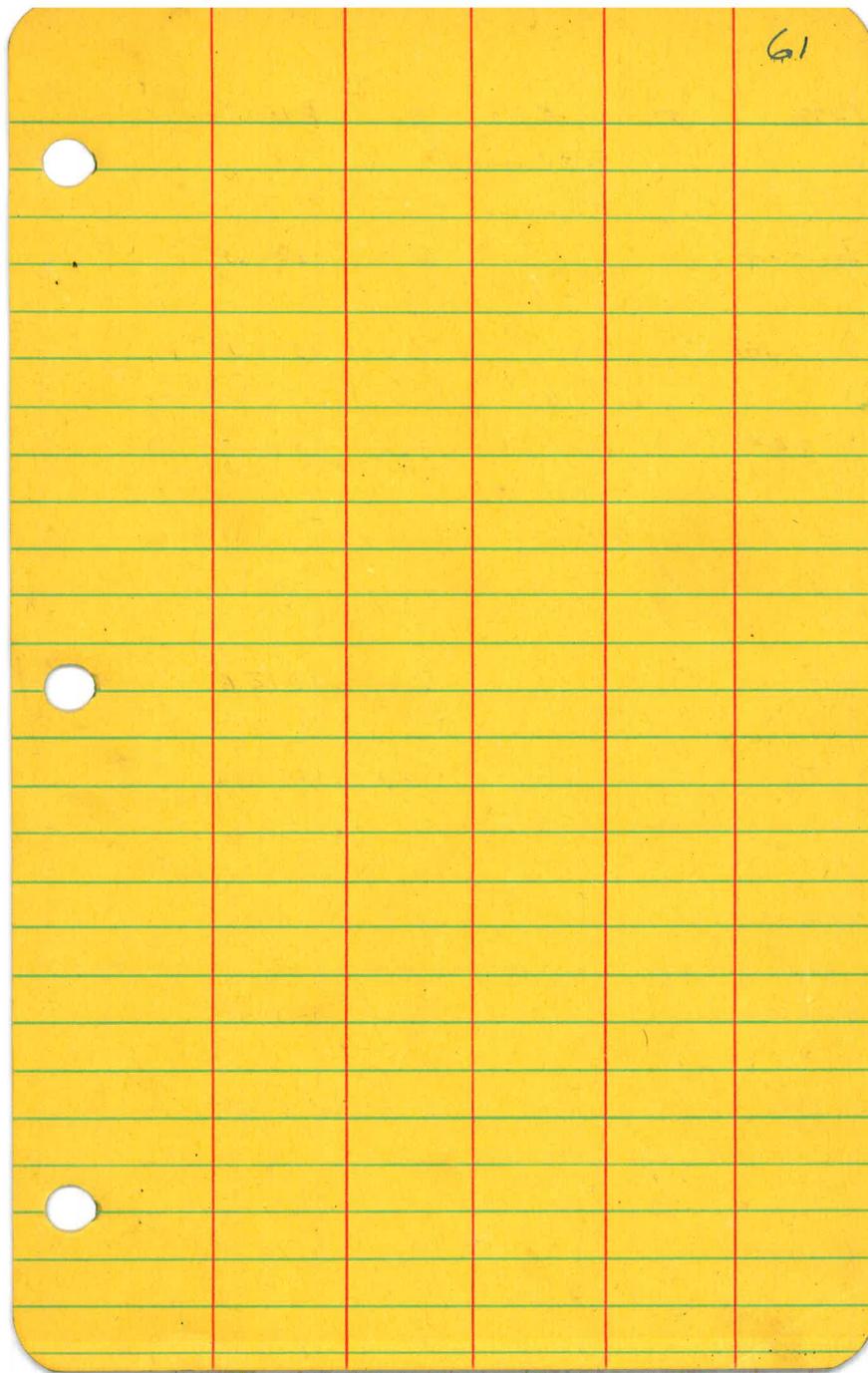
| Sta. | + | π | - | Elev. |
|--------|-------|----------|--------|----------|
| | | 1518.969 | | |
| | TF | | 12.325 | 1506.644 |
| | 2.474 | 1509.118 | | |
| 408+50 | | | 2.8 | 1506.3 ✓ |
| 409+00 | | | 3.4 | 1505.7 ✓ |
| +50 | | | 4.1 | 1505.0 ✓ |
| 410+00 | | | 5.4 | 1503.7 ✓ |
| +50 | | | 6.9 | 1502.2 ✓ |
| 411+00 | | | 8.7 | 1500.4 ✓ |
| +50 | | | 10.3 | 1498.8 ✓ |
| | TF | | 10.127 | 1498.991 |
| | 1.676 | 1500.667 | | |
| 412+00 | | | 2.9 | 1497.8 ✓ |
| +50 | | | 5.8 | 1494.9 ✓ |

Removal
N 6-28

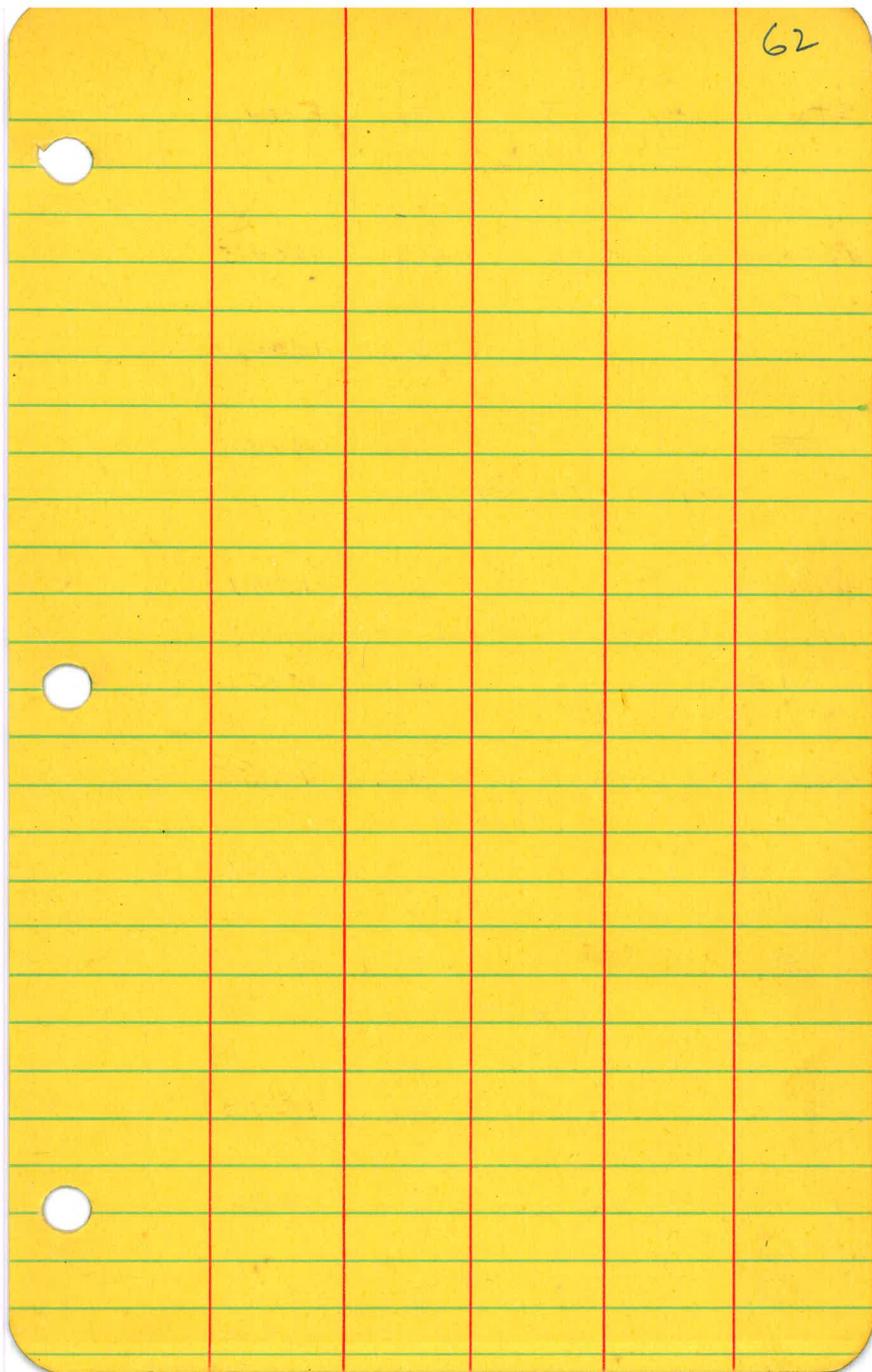


| Sta. | + | Σ | - | Elev. |
|--------|--------|----------|-------|----------|
| | | 1500.667 | | |
| 413+00 | | | 6.5 | 1494.2 ✓ |
| +50 | | | 7.3 | 1493.4 ✓ |
| 414+00 | | | 8.7 | 1492.0 ✓ |
| TR | | | 8.399 | 1492.268 |
| | 4.532 | 1496.800 | | |
| +50 | | | 4.2 | 1492.6 ✓ |
| 415+00 | | | 4.4 | 1492.4 ✓ |
| 416+00 | | | 5.5 | 1491.3 ✓ |
| 417+00 | | | 6.6 | 1490.2 ✓ |
| 418+00 | | | 6.1 | 1490.7 ✓ |
| 419+00 | | | 1.0 | 1495.8 ✓ |
| TR | | | 0.847 | 1495.953 |
| | 11.492 | 1507.495 | | |

61



| Sta. | + | π | - | Elev. |
|--------|--------|----------|-------|----------|
| | | 1507.445 | | |
| 420+00 | | | 6.9 | 1500.5 ✓ |
| 421+00 | | | 2.3 | 1505.1 ✓ |
| TH | | | 1.390 | 1506.055 |
| | 9.147 | 1515.202 | | |
| 422+00 | | | 5.8 | 1509.4 ✓ |
| 423+00 | | | 3.1 | 1512.1 ✓ |
| TH | | | 1.320 | 1513.882 |
| | 12.887 | 1526.769 | | |
| 424+00 | | | 10.7 | 1516.1 ✓ |
| 425+00 | | | 6.0 | 1520.8 ✓ |
| TH | | | 0.462 | 1526.307 |
| | 8.924 | 1535.231 | | |
| 426+00 | | | 8.6 | 1526.6 ✓ |
| | | | 5.1 | 1530.1 ✓ |



| Sta. | + | π | - | Elev. |
|------------------------|-------|----------|-------|----------|
| | | 1535.231 | | |
| 427+00 | | | 4.7 | 1530.5 ✓ |
| +50 | | | 3.2 | 1532.0 ✓ |
| T.P. | | | 0.559 | 1534.672 |
| | 5.415 | 1540.087 | | |
| 428+00 | | | 3.0 | 1537.1 ✓ |
| +50 | | | 4.0 | 1536.1 ✓ |
| 429+00 | | | 4.6 | 1535.5 ✓ |
| +50 | | | 2.3 | 1537.8 ✓ |
| T.P. | | | 0.780 | 1539.307 |
| | 9.911 | 1549.218 | | |
| 430+00 | | | 6.9 | 1542.3 ✓ |
| +27 ¹⁵ P.I. | | | 4.4 | 1544.8 ✓ |
| +50 | | | 3.6 | 1545.6 ✓ |

1
JAN. 12, 1928

Simpson

Brooks

Clavert.

P. Line

Profile Levels over Line

change, starting from
Sta 440+24 ~~to~~ to 493+59.95

This is "P" Line

| Sta | + | x | - | Elev. |
|----------------------|--------|---------|------|-----------------|
| | | | | 1531.52 = Elev. |
| | 7.44 | 1538.96 | | S.D.B.M. - P-10 |
| 440+24 ⁷⁹ | PI | | 9.3 | 1529.7 |
| +50 | ↳ Road | | 7.0 | 1532.0 |
| +75 ⁹⁷ | | | 6.9 | 1532.1 |
| 441+00 | | | 5.8 | 1533.2 |
| +50 | | | 2.7 | 1536.3 |
| TI | | | 0.25 | 1538.71 |
| | 9.72 | 1548.43 | | |
| 442+00 | | | 9.2 | 1539.2 |
| +50 | | | 7.9 | 1540.5 |
| | | | 7.8 | 1540.6 |
| 443+00 | | | 5.8 | 1542.6 |
| +50 | | | 4.5 | 1543.9 |

- Shot on E Rd. opp. 442+50

| Sta | + | π | - | Elev. |
|--------|------|---------|------|-----------|
| | | 1548.43 | ✓ | |
| 944+00 | | | 4.7 | 1543.7 ✓ |
| +50 | | | 6.9 | 1541.5 ✓ |
| 945+00 | | | 9.1 | 1539.3 ✓ |
| | | | 9.0 | 1539.4 ✓ |
| +50 | | | 9.0 | 1539.4 ✓ |
| 946+00 | | | 7.7 | 1540.7 ✓ |
| +50 | | | 8.2 | 1540.2 ✓ |
| 947+00 | | | 7.3 | 1541.1 ✓ |
| | | | 7.4 | 1541.0 ✓ |
| TPA | | | 7.13 | 1541.30 ✓ |
| | 7.25 | 1548.55 | | |
| +50 | | | 5.0 | 1543.6 ✓ |
| 948+00 | | | 3.4 | 1545.2 ✓ |

Shot on E Rd opp 44500

Shot on E Rd opp 44700

| Sta. | + | π | - | Elev. |
|--------|------|-----------|-------|-----------|
| | | 1548.55 ✓ | | |
| | | | 2.8 | 1545.8 ✓ |
| 448+50 | | | 3.4 | 1545.2 ✓ |
| 449+00 | | | 6.7 | 1541.9 ✓ |
| +50 | | | 7.7 | 1540.9 ✓ |
| 450+00 | | | 10.9 | 1538.2 ✓ |
| | | | 9.0 | 1539.6 ✓ |
| +50 | | | 12.3 | 1536.3 ✓ |
| 451+00 | | | 13.3 | 1535.3 ✓ |
| T.B | | | 11.77 | 1536.78 ✓ |
| | 1.32 | 1538.10 ✓ | | |
| +50 | | | 3.6 | 1534.5 ✓ |
| 452+00 | | | 5.2 | 1532.9 ✓ |
| | | | 4.1 | 1534.0 ✓ |

4

Shot on £ Rd opp 498+25

£ Rd opp. 450+00

£ Rd. opp 452+00

| Sta. | + | π | - | Elev. |
|------------------------------|------|-----------|------|-----------------------|
| | | 1538.10 ✓ | | |
| +52+50 | | | 6.6 | 1531.5 ✓ |
| +53+00 | | | 8.7 | 1529.4 ✓ |
| +46 ⁵⁰ P.I. | | | 9.2 | 1528.9 ✓ |
| +60 ² ϕ Road | | | 9.3 | 1528.8 ✓ |
| +91 ⁶⁸ P.I. | | | 9.4 | 1528.7 ✓ |
| T.P. | | | 7.93 | 1530.17 ✓ |
| | 0.33 | 1530.54 ✓ | | 1530.21 - B.M. # P-11 |
| +54+50 | | | 3.3 | 1527.2 ✓ |
| +55+00 | | | 3.4 | 1527.1 ✓ |
| +50 | | | 4.3 | 1526.2 ✓ |
| +56+00 | | | 4.8 | 1525.7 ✓ |
| | | | 4.6 | 1525.9 ✓ |
| +50 | | | 5.3 | 1525.2 ✓ |

= CHECK on S. D. B. M. # P-11
Elev. = 1530.21

± Rd opp 456+00

| Sta. | + | + | - | Elev. |
|--------|-------------------------|-----------|------|----------------------|
| | | 1530.54 ✓ | | |
| 457+00 | | | 7.1 | 1523.4 ✓ |
| +44 | 24" concrete culvert | | 11.0 | 1519.5 = Flow Line ✓ |
| | | | 7.2 | 1523.3 ✓ |
| +50 | | | 9.0 | 1521.5 ✓ |
| +70 | | | 11.8 | 1518.7 ✓ |
| 458+00 | | | 8.7 | 1521.8 ✓ |
| +50 | | | 7.6 | 1522.9 ✓ |
| 459+00 | | | 5.5 | 1525.0 ✓ |
| T.P. | | | 0.59 | 1529.95 ✓ |
| | 9.31 | 1539.26 ✓ | | |
| +50 | | | 10.6 | 1528.7 ✓ |
| 460+00 | | | 8.4 | 1530.9 ✓ |
| +50 | | | 6.7 | 1532.6 ✓ |

= £ Rd. opp 957+99

| Sta. | + | π | - | Elev. |
|--------|------|--------------------------|-------|----------------------|
| | | 1539.26 ✓ | | |
| 461+00 | | | 5.8 | 1533.5 ✓ |
| | | | 3.0 | 1536.3 ✓ |
| +50 | | | 6.6 | 1532.7 ✓ |
| 462+00 | | | 8.2 | 1531.1 ✓ |
| +50 | | | 10.1 | 1529.2 ✓ |
| 463+00 | | | 12.6 | 1526.7 ✓ |
| | | | 12.6 | 1526.7 ✓ |
| TH. | | | 12.73 | 1526.53 ✓ |
| | 4.63 | 1531.16 ✓ | | |
| +50 | | | 8.1 | 1523.1 ✓ |
| 464+00 | | | 11.3 | 1519.9 ✓ |
| +34 | | | 19.5 | 1516.7 ✓ |
| +34 | | 12" Concrete Culvert. | 14.1 | 1517.1 ✓ = Flow Line |

£ Rd. opp 461+00

£ Rd. opp 463+00

| Sta. | + | π | - | Elev. |
|--------|------|---------|------|-----------|
| | | 1531.16 | | |
| 464+50 | | | 12.6 | 1518.6 ✓ |
| | | | 11.5 | 1519.7 ✓ |
| 465+00 | | | 10.7 | 1520.5 ✓ |
| +50 | | | 8.2 | 1523.0 ✓ |
| 466+00 | | | 4.6 | 1526.6 ✓ |
| TR | | | 0.29 | 1530.87 ✓ |
| | 4.63 | 1535.50 | | |
| +50 | | | 5.2 | 1530.3 ✓ |
| 467+00 | | | 3.2 | 1532.3 ✓ |
| +25 | | | 2.5 | 1533.0 ✓ |
| | | | 1.8 | 1533.7 ✓ |
| 468+00 | | | 5.0 | 1530.5 ✓ |
| +50 | | | 7.8 | 1527.7 ✓ |

4 Rd. opp. - 467+56

4 Rd opp 467+25

| Sta | + | x | - | Elev. |
|--------|-----|---------|------|-----------|
| | | 1535.50 | | |
| 469+00 | | | 9.5 | 1526.0 ✓ |
| +50 | | | 9.9 | 1525.6 ✓ |
| | | | 9.2 | 1526.3 ✓ |
| 470+00 | | | 12.0 | 1523.5 ✓ |
| FF | | | 11.2 | 1523.78 ✓ |
| | 407 | 1527.85 | | |
| +50 | | | 5.3 | 1522.6 ✓ |
| 471+00 | | | 3.2 | 1524.7 ✓ |
| +50 | | | 1.7 | 1526.2 ✓ |
| 472+00 | | | 1.5 | 1526.4 ✓ |
| | | | 3.2 | 1524.7 ✓ |
| +50 | | | 3.2 | 1524.7 ✓ |
| 473+00 | | | 6.0 | 1521.9 ✓ |

£ Rd opp 469+50

£ Rd. opp. 472+00

| Sta. | + | π | - | Elev. |
|----------------|------|---------|-------|---------------|
| | | 1527.85 | | |
| 473+50 | | | 10.3 | 1517.6 ✓ |
| 7.F | | | 12.77 | 1515.08 ✓ |
| | 0.45 | 1515.53 | | |
| 474+00 | | | 1.0 | 1514.5 ✓ |
| +50 | | | 4.2 | 1511.3 ✓ |
| 475+00 | | | 6.2 | 1509.3 ✓ 11.4 |
| | | | 7.5 | 1508.0 ✓ |
| +50 | | | 7.5 | 1508.0 ✓ |
| 476+00 | | | 8.1 | 1506.8 ✓ |
| +50 | | | 8.8 | 1506.7 ✓ |
| 477+00 | | | 9.0 | 1506.5 ✓ |
| | | | 7.6 | 1507.9 ✓ |
| +50 | | | 8.0 | 1507.5 ✓ |

E. Rd. opp. 475+00

E. Rd. opp. 477+00

| Sta. | + | π | - | Elev |
|--------|------|---------|------|-----------|
| | | 1515.53 | | |
| 478+00 | | | 8.2 | 1507.3 ✓ |
| +50 | | | 9.2 | 1506.3 ✓ |
| TH | | | 9.62 | 1505.91 ✓ |
| | 9.09 | 1515.00 | | |
| 479+00 | | | 9.3 | 1505.7 ✓ |
| | | | 9.7 | 1505.3 ✓ |
| +50 | | | 8.9 | 1506.1 ✓ |
| 480+00 | | | 8.1 | 1506.9 ✓ |
| +50 | | | 6.3 | 1508.7 ✓ |
| 481+00 | | | 3.3 | 1511.7 ✓ |
| | | | 1.4 | 1513.6 ✓ |
| TH | | | 0.37 | 1514.63 ✓ |
| | 6.77 | 1521.40 | | |

£ Rd. app 479400

£ Rd app 481400

| Sta. | + | π | - | Elev. |
|--------|---|---------|-----|----------|
| | | 1521.40 | | |
| 481+50 | | | 7.5 | 1513.9 ✓ |
| 482+00 | | | 5.7 | 1515.7 ✓ |
| +50 | | | 7.7 | 1517.0 ✓ |
| | | | 4.1 | 1517.3 ✓ |
| 483+00 | | | 6.0 | 1515.4 ✓ |
| +50 | | | 8.2 | 1513.2 ✓ |
| 484+75 | | | 9.0 | 1512.4 ✓ |
| 484+00 | | | 8.0 | 1513.4 ✓ |
| +50 | | | 4.8 | 1516.6 ✓ |
| | | | 4.8 | 1516.6 ✓ |
| 485+00 | | | 5.5 | 1515.9 ✓ |
| +50 | | | 8.1 | 1513.3 ✓ |

⊕ Rd opp 482+50

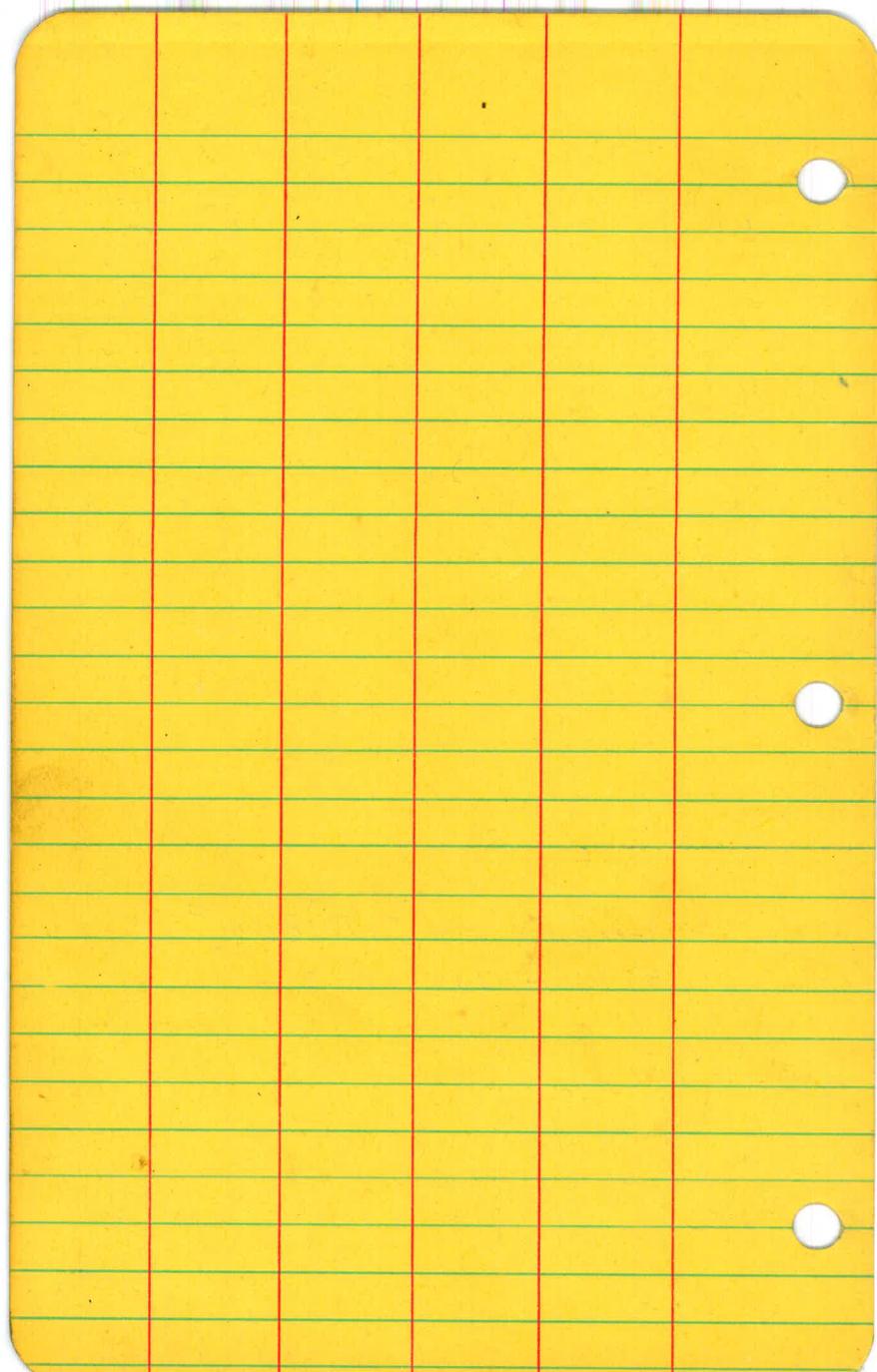
⊕ Rd opp 484+50

| Sta. | + | ∓ | - | Elev. |
|--------|------|-----------|-------|-----------|
| | | 1521.40 ✓ | | |
| 486+00 | | | 9.4 | 1512.0 ✓ |
| +50 | | | 11.2 | 1510.2 ✓ |
| T.I. | | | 12.50 | 1508.90 ✓ |
| | 2.06 | 1508.96 ✓ | | |
| 487+00 | | | 0.0 | 1508.96 ✓ |
| +50 | | | 1.6 | 1507.4 ✓ |
| 488+00 | | | 3.3 | 1505.7 ✓ |
| +50 | | | 5.9 | 1503.1 ✓ |
| 489+00 | | | 8.3 | 1500.7 ✓ |
| | | | 8.3 | 1500.7 ✓ |
| +50 | | | 9.5 | 1499.5 ✓ |
| 490+00 | | | 8.8 | 1500.2 ✓ |
| +50 | | | 9.8 | 1499.2 ✓ |

E. Rd opp 489+00

| Sta. | + | x | - | Elev |
|--------|---------------------------|-----------|-------|-----------|
| | | 1508.96 ✓ | | |
| 491+00 | | | 9.1 | 1499.9 ✓ |
| | +50 | | 10.4 | 1498.6 ✓ |
| 492+00 | | | 10.6 | 1498.4 ✓ |
| | +50 | | 11.7 | 1497.3 ✓ |
| 493+00 | | | 13.4 | 1495.6 ✓ |
| | +50 | | 12.6 | 1496.4 ✓ |
| | + <u>62</u> ²³ | | 12.7 | 1496.3 ✓ |
| | +59 ⁹⁵ | | | |
| | | | 12.81 | 1498.15 ✓ |
| | | | | 1498.18 |

= CHECK ON S. D. B. M. #
Elev. = 1498.18

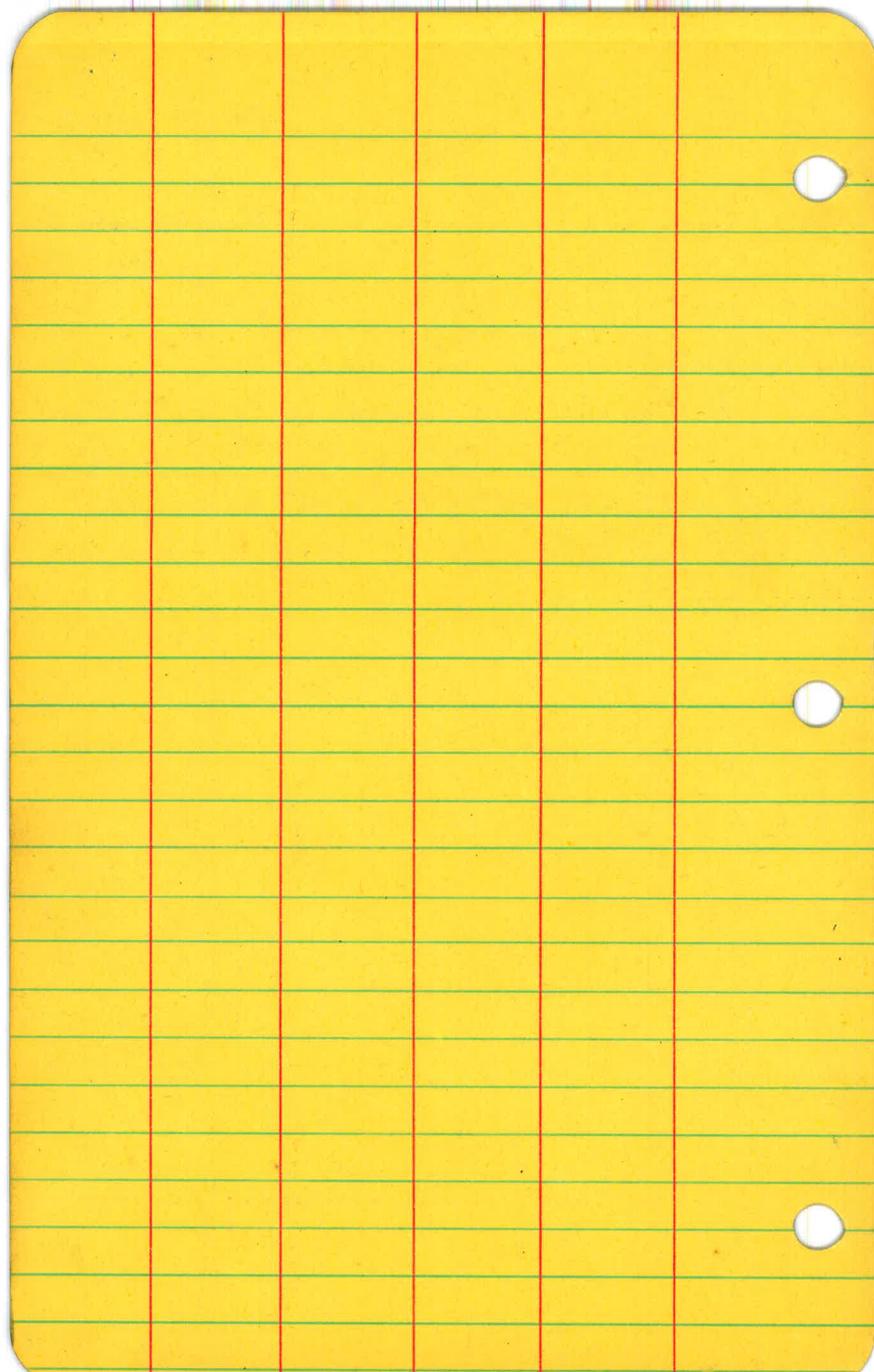


73

Dec 2, 1927

Simpson - π
Clavett - Rod

Profile Levels over Line change
Known as "P" Line. Beginning
at Sta 493+54⁷² "P" Line and
Running west along Road.



74

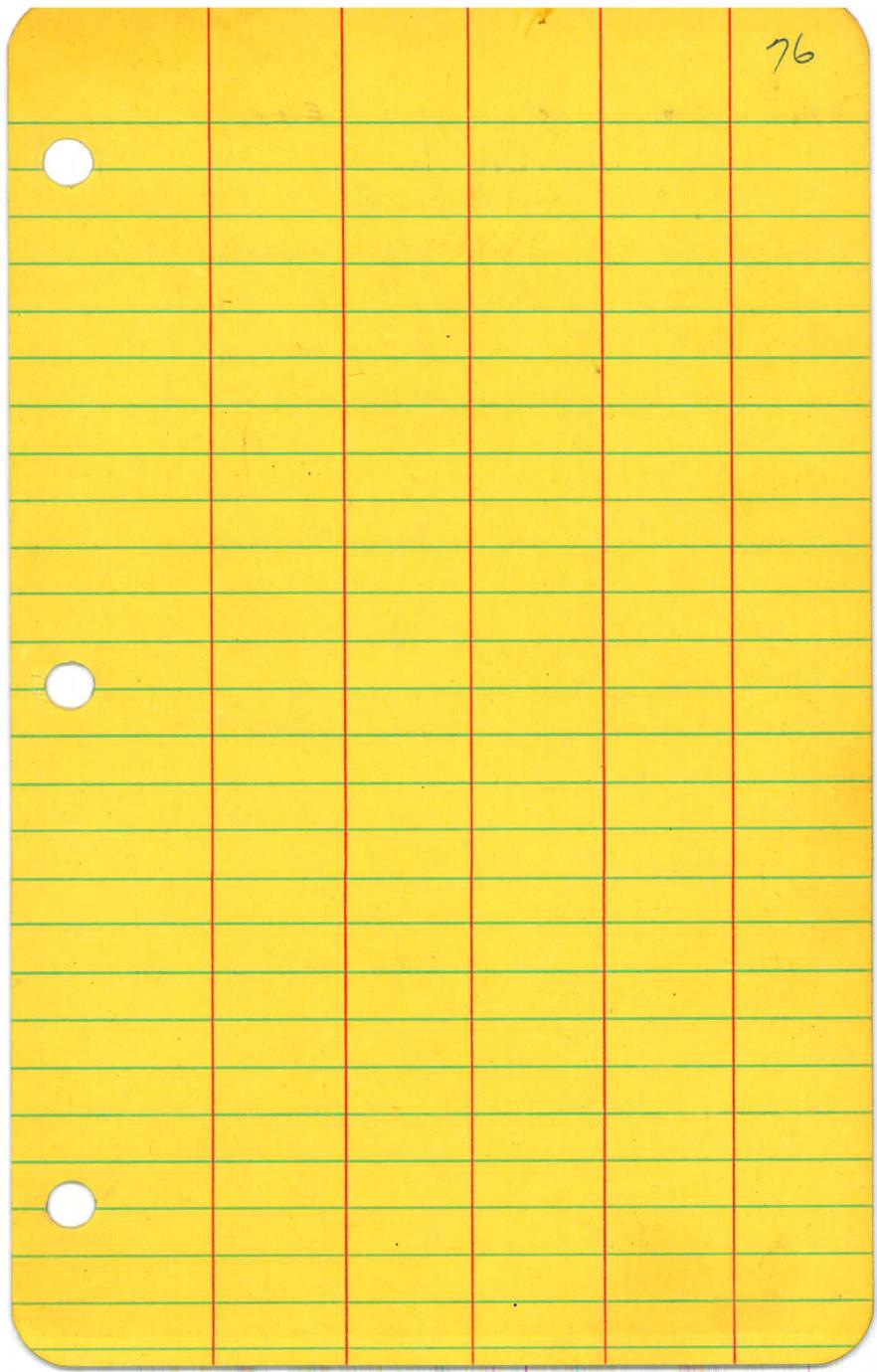
| Sta. | + | - | Elev. |
|----------------------|-------|----------|-----------------------|
| | | | 1498.179 = B.M. P-12. |
| | 3.528 | 1501.707 | |
| 493+54 ²¹ | | 5.5 | 1496.2 ✓ |
| 494+00 | | 6.0 | 1495.7 ✓ |
| +50 | | 6.0 | 1495.7 ✓ |
| +87 | | 7.7 | 1494.0 ✓ |
| 495+00 | | 6.0 | 1495.7 ✓ |
| +50 | | 7.4 | 1494.3 ✓ |
| 496+00 | | 8.0 | 1493.7 ✓ |
| +50 | | 8.1 | 1493.6 ✓ |
| 497+00 | | 7.2 | 1494.5 ✓ |
| +50 | | 5.1 | 1496.6 ✓ |
| 498+00 | | 3.1 | 1498.6 ✓ |
| TA | | 3.035 | 1498.672 |

Starting from B.M. # P-12
Nail in fence Post. N.E. Cor. of X Roads. 45'E
493+25. Elev. 1498.179
Starting of "P" line

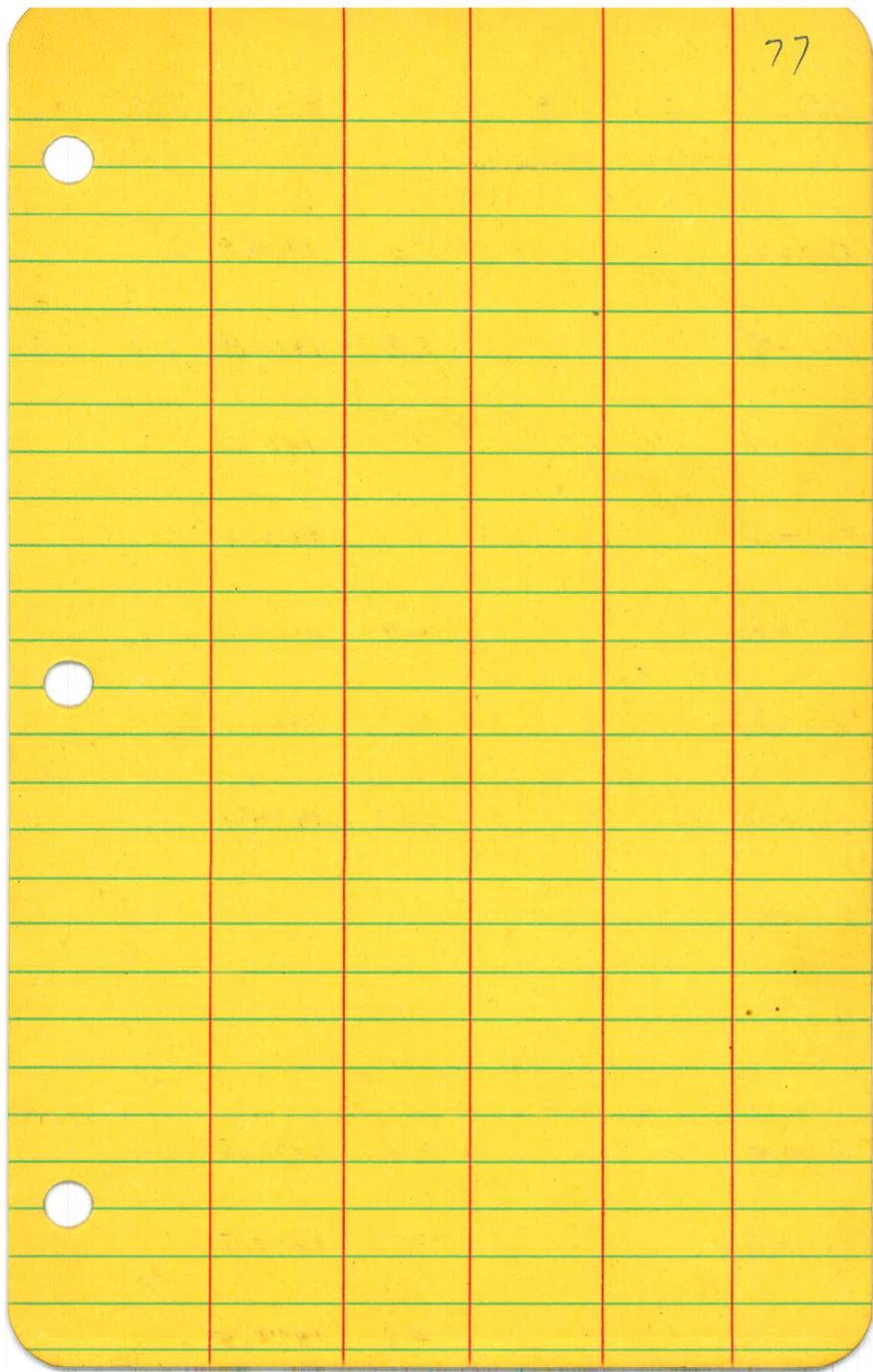
center of wash

| Sta. | + | π | - | Elev. |
|--------|-------|----------|--------|----------|
| | | | | 1498.672 |
| | 7.093 | 1505.765 | | |
| 498+50 | | | 5.1 | 1500.7 ✓ |
| 499+00 | | | 3.6 | 1502.2 ✓ |
| +50 | | | 3.8 | 1502.0 ✓ |
| 500+00 | | | 5.3 | 1500.5 ✓ |
| +50 | | | 7.4 | 1498.4 ✓ |
| 501+00 | | | 9.3 | 1496.5 ✓ |
| +50 | | | 12.1 | 1493.7 ✓ |
| TH | | | 12.367 | 1493.398 |
| | 1.390 | 1494.738 | | |
| 502+00 | | | 3.3 | 1491.4 ✓ |
| +50 | | | 4.5 | 1490.2 ✓ |
| 503+00 | | | 5.2 | 1489.5 ✓ |

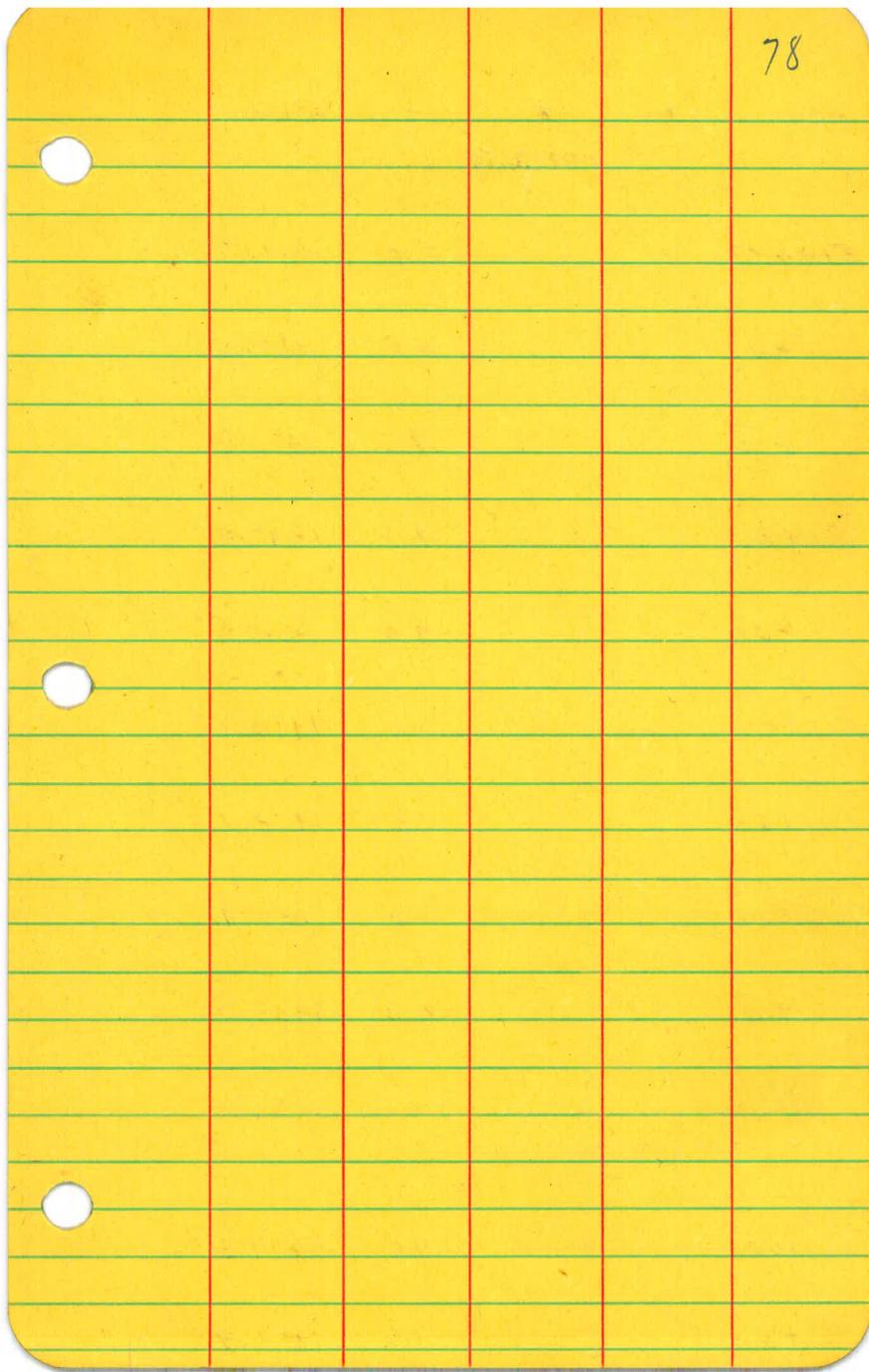
76



| Sta. | + | π | - | Elev. |
|--------|-------|----------|--------|----------|
| | | 1494738 | | |
| 503+50 | | | 5.2 | 1489.5 ✓ |
| 504+00 | | | 6.3 | 1488.4 ✓ |
| +50 | | | 7.9 | 1486.8 ✓ |
| 505+00 | | | 9.7 | 1485.0 ✓ |
| +50 | | | 11.7 | 1483.0 ✓ |
| 506+00 | | | 12.1 | 1482.6 ✓ |
| TR | | | 12.880 | 1481.858 |
| | 2 490 | 1484.298 | | |
| +50 | | | 2.8 | 1481.5 ✓ |
| 507+00 | | | 3.2 | 1481.1 ✓ |
| +50 | | | 3.4 | 1480.9 ✓ |
| 508+00 | | | 3.6 | 1480.7 ✓ |
| +50 | | | 4.9 | 1479.4 ✓ |

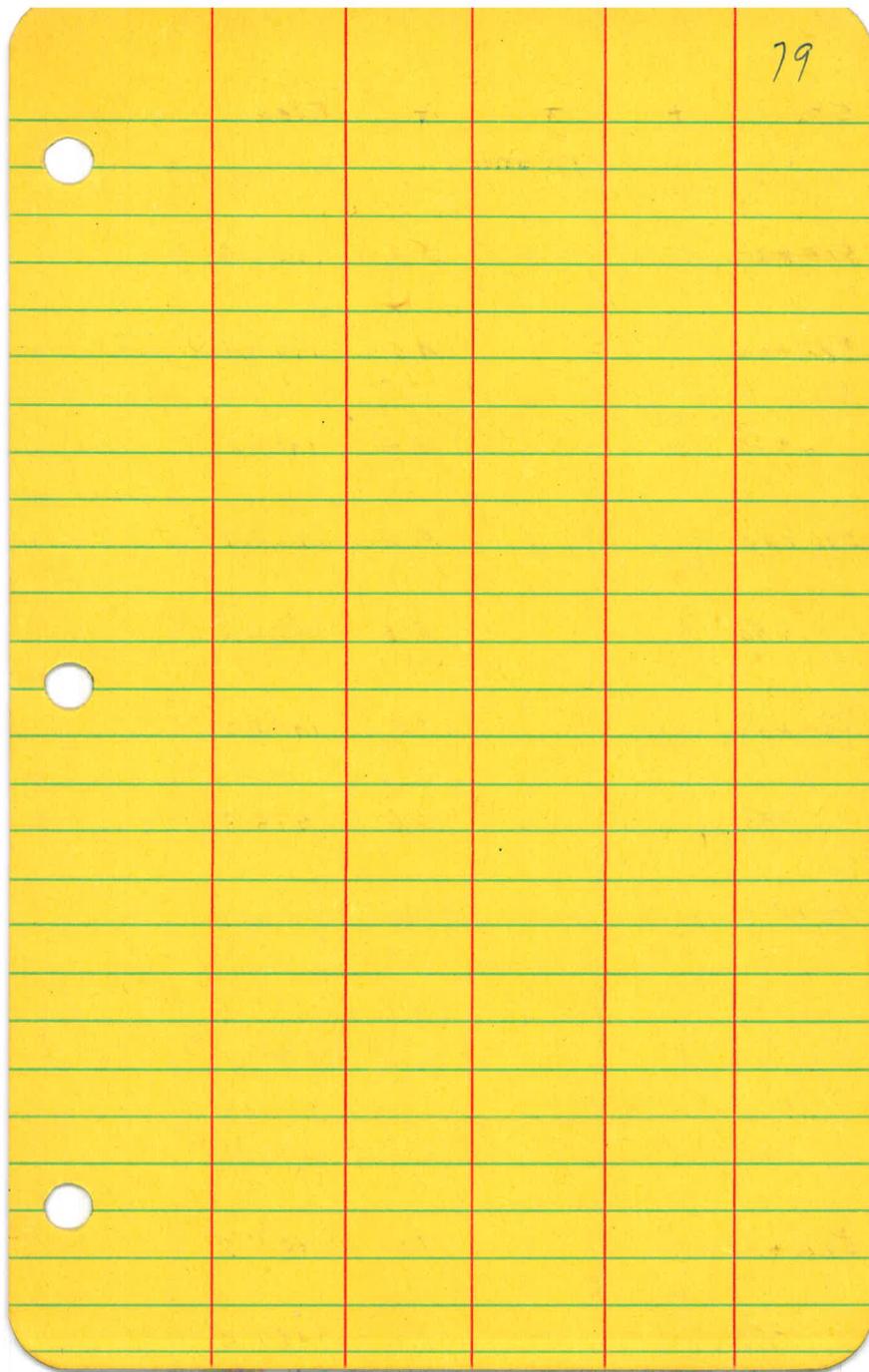


| Sta | + | π | - | Elev. |
|--------|-------|----------|--------|----------|
| | | 1484.298 | | |
| 509+00 | | | 5.4 | 1478.9 ✓ |
| +50 | | | 5.9 | 1478.4 ✓ |
| 510+00 | | | 7.1 | 1477.2 ✓ |
| +50 | | | 8.3 | 1476.0 ✓ |
| 511+00 | | | 9.4 | 1474.9 ✓ |
| +50 | | | 9.6 | 1474.7 ✓ |
| 512+00 | | | 10.2 | 1474.1 ✓ |
| +50 | | | 11.4 | 1472.9 ✓ |
| 7F | | | 11.315 | 1472.983 |
| | 3.275 | 1476.258 | | |
| 513+00 | | | 3.7 | 1472.6 ✓ |
| +50 | | | 3.8 | 1472.5 ✓ |
| 514+00 | | | 4.8 | 1471.5 ✓ |



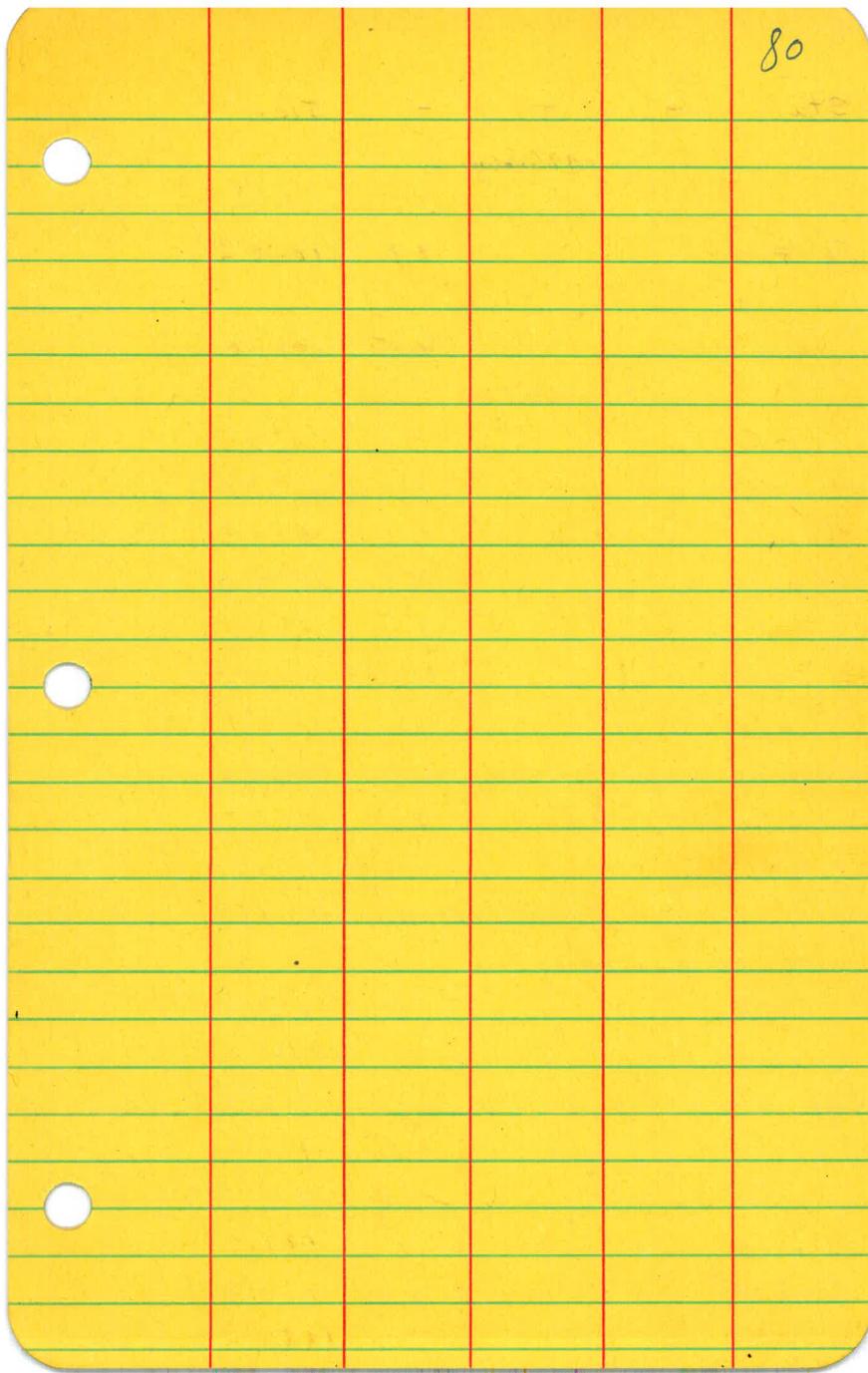
| Sta | + | π | - | Elev. |
|--------|--------|----------|-------|----------|
| | | 1476.258 | | |
| 514+50 | | | 5.0 | 1471.3 ✓ |
| 515+00 | | | 4.8 | 1471.5 ✓ |
| +50 | | | 4.4 | 1471.9 ✓ |
| 516+00 | | | 4.3 | 1472.0 ✓ |
| +50 | | | 4.2 | 1472.1 ✓ |
| 517+00 | | | 3.0 | 1473.3 ✓ |
| +50 | | | 3.6 | 1472.7 ✓ |
| 518+00 | | | 2.6 | 1473.7 ✓ |
| +50 | | | 0.3 | 1476.0 ✓ |
| TP | | | 0.262 | 1475.996 |
| | 12.950 | 1488.946 | | |
| 519+00 | | | 9.6 | 1479.3 ✓ |
| +50 | | | 7.0 | 1481.9 ✓ |

79



| Sta. | + | x | - | Elev. |
|--------|-------|----------|--------|----------|
| | | 1488.946 | | |
| 519+83 | P.I. | | 5.3 | 1483.6 ✓ |
| 520+00 | | | 4.5 | 1484.4 ✓ |
| +50 | | | 4.4 | 1484.5 ✓ |
| 521+00 | | | 6.5 | 1482.4 ✓ |
| +50 | | | 8.4 | 1480.5 ✓ |
| 522+00 | | | 11.0 | 1477.9 ✓ |
| +50 | | | 12.6 | 1476.3 ✓ |
| T.P. | | | 12.464 | 1476.482 |
| | 0.384 | 1476.866 | | |
| 523+00 | | | 2.4 | 1479.5 ✓ |
| +50 | | | 4.7 | 1472.2 ✓ |
| 524+00 | | | 7.0 | 1469.9 ✓ |
| +50 | | | 8.7 | 1468.2 ✓ |

80



| Sta. | + | π | - | Elev. |
|--------|-------|----------|--------|----------|
| | | 1476.866 | | |
| 525+00 | | | 11.7 | 1465.2 ✓ |
| TH | | | 12.850 | 1464.016 |
| | 0.870 | 1464.886 | | |
| +50 | | | 2.1 | 1462.8 ✓ |
| 526+00 | | | 5.9 | 1459.0 ✓ |
| +50 | | | 9.6 | 1455.3 ✓ |
| 527+00 | | | 12.3 | 1452.6 ✓ |
| TH | | | 12.205 | 1452.681 |
| | 0.238 | 1452.919 | | |
| +50 | | | 2.3 | 1450.6 ✓ |
| 528+00 | | | 3.1 | 1449.8 ✓ |
| +50 | | | 3.6 | 1449.3 ✓ |
| 529+00 | | | 4.2 | 1448.7 ✓ |

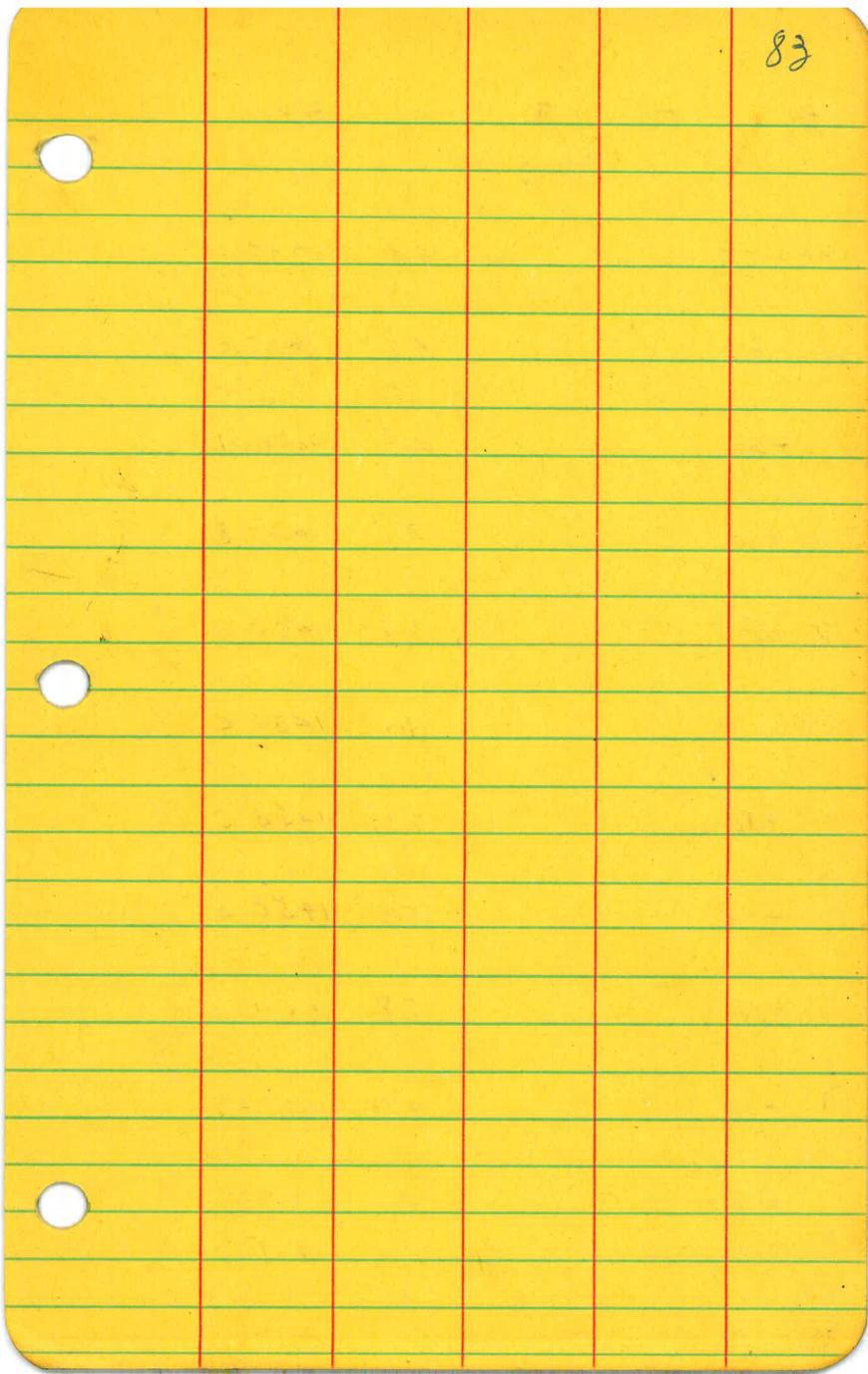
81

| Sta | + | π | - | Elev. |
|--------|-------|----------|-------|------------|
| | | 1452.919 | | |
| 529+50 | | | 4.8 | 1448.1 ✓ |
| 530+00 | | | 6.0 | 1446.9 ✓ |
| +50 | | | 6.8 | 1446.1 ✓ |
| 531+00 | | | 7.6 | 1445.3 ✓ |
| +50 | | | 7.6 | 1445.3 ✓ |
| 532+00 | | | 8.0 | 1444.9 ✓ |
| +50 | | | 8.6 | 1444.3 ✓ |
| TH | | | 9.060 | 1443.859 ✓ |
| | 0.030 | 1443.889 | | |
| 533+00 | | | 0.0 | 1443.9 ✓ |
| +50 | | | 0.9 | 1443.0 ✓ |
| 534+00 | | | 2.6 | 1441.3 ✓ |
| +50 | | | 3.7 | 1440.2 ✓ |

B.M.

| Sta. | + | π | - | Elev. |
|--------|-------|----------|-------|----------|
| | | 1443.889 | | |
| 535+00 | | | 3.8 | 1440.1 ✓ |
| +50 | | | 4.9 | 1439.0 ✓ |
| 536+00 | | | 5.7 | 1438.2 ✓ |
| +50 | | | 6.1 | 1437.8 ✓ |
| 537+00 | | | 6.4 | 1437.5 ✓ |
| +50 | | | 6.7 | 1437.2 ✓ |
| 538+00 | | | 7.1 | 1436.8 ✓ |
| +50 | | | 7.3 | 1436.6 ✓ |
| 539+00 | | | 7.8 | 1436.1 ✓ |
| TA | | | 7.536 | 1436.353 |
| | 9.455 | 1440.808 | | |
| +50 | | | 4.3 | 1436.5 ✓ |
| 540+00 | | | 4.5 | 1436.3 ✓ |

83



| Sta | + | π | - | Elev. |
|-----|-----|----------|-----|----------|
| | | 1490.808 | | |
| 540 | +50 | | 4.6 | 1436.2 ✓ |
| 541 | +00 | | 4.8 | 1436.0 ✓ |
| | +50 | | 4.7 | 1436.1 ✓ |
| 542 | +00 | | 5.0 | 1435.8 ✓ |
| | +50 | | 4.8 | 1436.0 ✓ |
| 543 | +00 | | 4.8 | 1436.0 ✓ |
| | +50 | | 7.5 | 1433.3 ✓ |
| 544 | +00 | | 5.5 | 1435.3 ✓ |
| | +50 | | 5.8 | 1435.0 ✓ |
| 545 | +00 | | 6.9 | 1433.9 ✓ |
| | +50 | | 5.8 | 1435.0 ✓ |
| 546 | +00 | | 4.5 | 1436.3 ✓ |

84

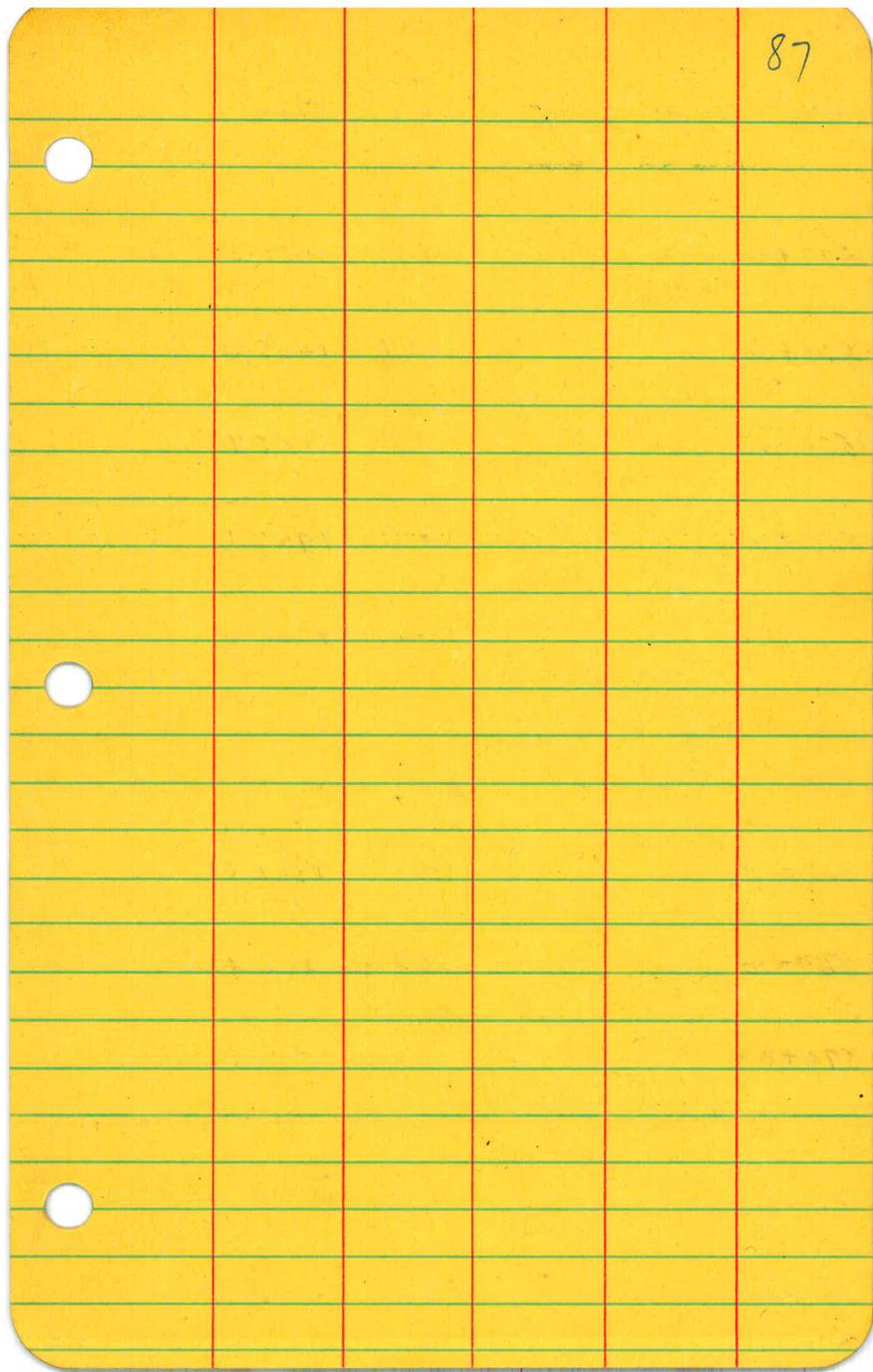
| Sta | + | - | Elev |
|--------|---------|----------|----------|
| | | 1443.029 | |
| 555+00 | | 4.9 | 1438.1 ✓ |
| 556+00 | | 4.2 | 1438.8 ✓ |
| 557+00 | | 2.4 | 1440.6 ✓ |
| 558+00 | | 1.9 | 1441.1 ✓ |
| TP | | 1.880 | 1441.149 |
| | 8.070 | 1449.219 | |
| 555+42 | culvert | 12.6 | 1436.6 ✓ |
| 559+00 | | 7.8 | 1441.4 ✓ |
| 560+00 | | 6.8 | 1442.4 ✓ |
| 561+00 | | 3.4 | 1445.8 ✓ |
| TP | | 0.313 | 1448.906 |
| | 11.887 | 1460.793 | |
| 562+00 | | 9.9 | 1450.9 ✓ |

86

Flow Line 12" concrete culvert.

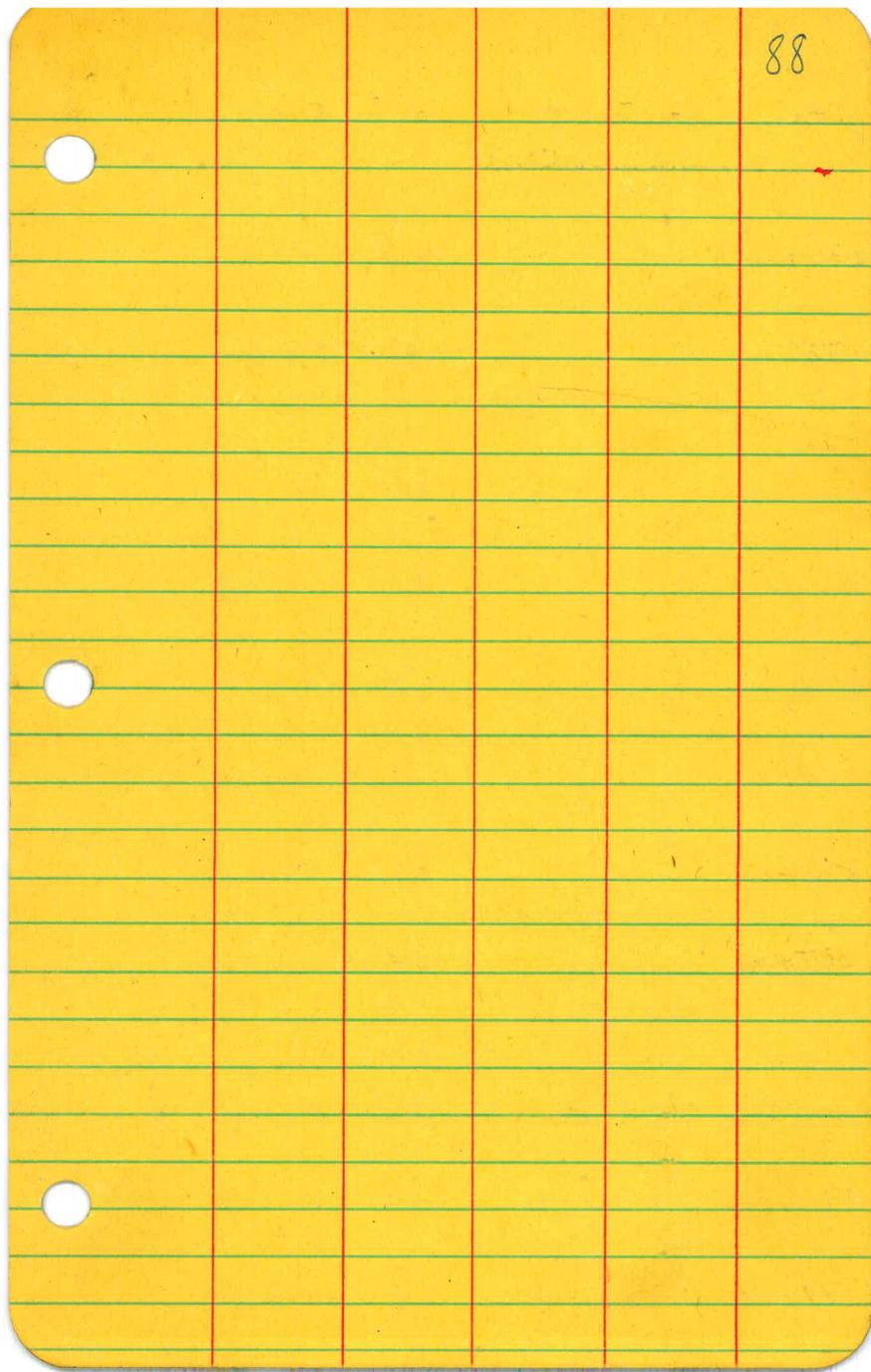
| Sta | + | T | - | Elev. |
|--------|-------|----------|-------|----------|
| | | 1460.793 | | |
| 563+00 | | | 5.0 | 1455.8 ✓ |
| 564+00 | | | 4.7 | 1456.1 ✓ |
| 565+00 | | | 3.9 | 1456.9 ✓ |
| 566+00 | | | 3.7 | 1457.7 ✓ |
| 567+00 | | | 6.1 | 1454.7 ✓ |
| TR | | | 5.638 | 1455.155 |
| | 1.010 | 1456.165 | | |
| 568+00 | | | 4.4 | 1451.8 ✓ |
| 569+00 | | | 5.8 | 1450.4 ✓ |
| 570+00 | | | 5.1 | 1451.1 ✓ |
| 571+00 | | | 3.0 | 1453.2 ✓ |
| TR | | | 0.00 | 1456.165 |
| | 9.995 | 1466.160 | | |

87

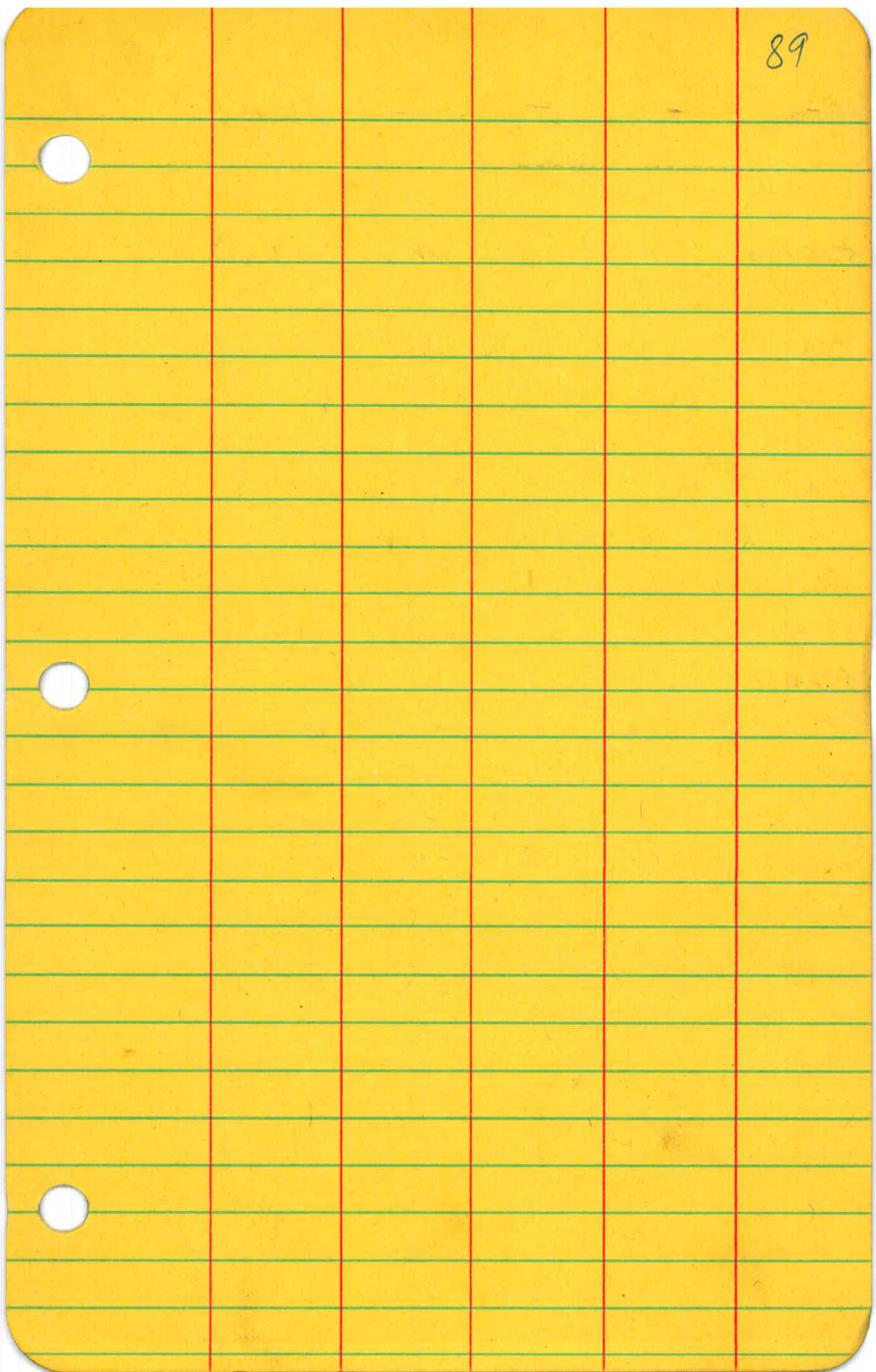


| Sta. | + | π | - | Elev. | |
|--------|-----------------|----------|--------|----------|---|
| | | 1466.160 | | | |
| 572+00 | | | 9.9 | 1456.3 | ✓ |
| 573+00 | | | 10.9 | 1455.3 | ✓ |
| 574+00 | | | 7.3 | 1458.9 | ✓ |
| 575+00 | | | 0.1 | 1466.1 | ✓ |
| T.# | | | 0.235 | 1465.925 | |
| | 4.890 | 1470.815 | | | |
| 576+00 | $\frac{18}{PI}$ | | 1.0 | 1469.8 | ✓ |
| 576+00 | | | 3.2 | 1467.6 | ✓ |
| 577+00 | | | 8.4 | 1462.4 | ✓ |
| T.# | | | 12.712 | 1458.103 | |
| | 1.287 | 1459.390 | | | |
| 578+00 | | | 3.6 | 1455.8 | ✓ |
| 579+00 | | | 9.9 | 1449.5 | ✓ |

88



| Sta. | + | T | - | Elev. |
|--------|--------------------|----------|--------|----------|
| | | 1459.390 | | |
| 580+00 | | | 12.7 | 1446.7 ✓ |
| TP | | | 12.936 | 1446.959 |
| | 6.012 | 1452.966 | | |
| 581+00 | | | 5.7 | 1446.8 ✓ |
| 582+00 | | | 6.2 | 1446.3 ✓ |
| 583+00 | | | 5.4 | 1447.1 ✓ |
| 584+00 | | | 6.2 | 1446.3 ✓ |
| 585+00 | | | 8.7 | 1443.8 ✓ |
| TP | | | 9.940 | 1442.526 |
| | 3.602 | 1446.128 | | |
| +86 | ⁸² P.I. | | 3.6 | 1442.5 ✓ |
| 586+00 | | | 3.9 | 1442.2 ✓ |
| 587+00 | | | 3.4 | 1442.7 ✓ |

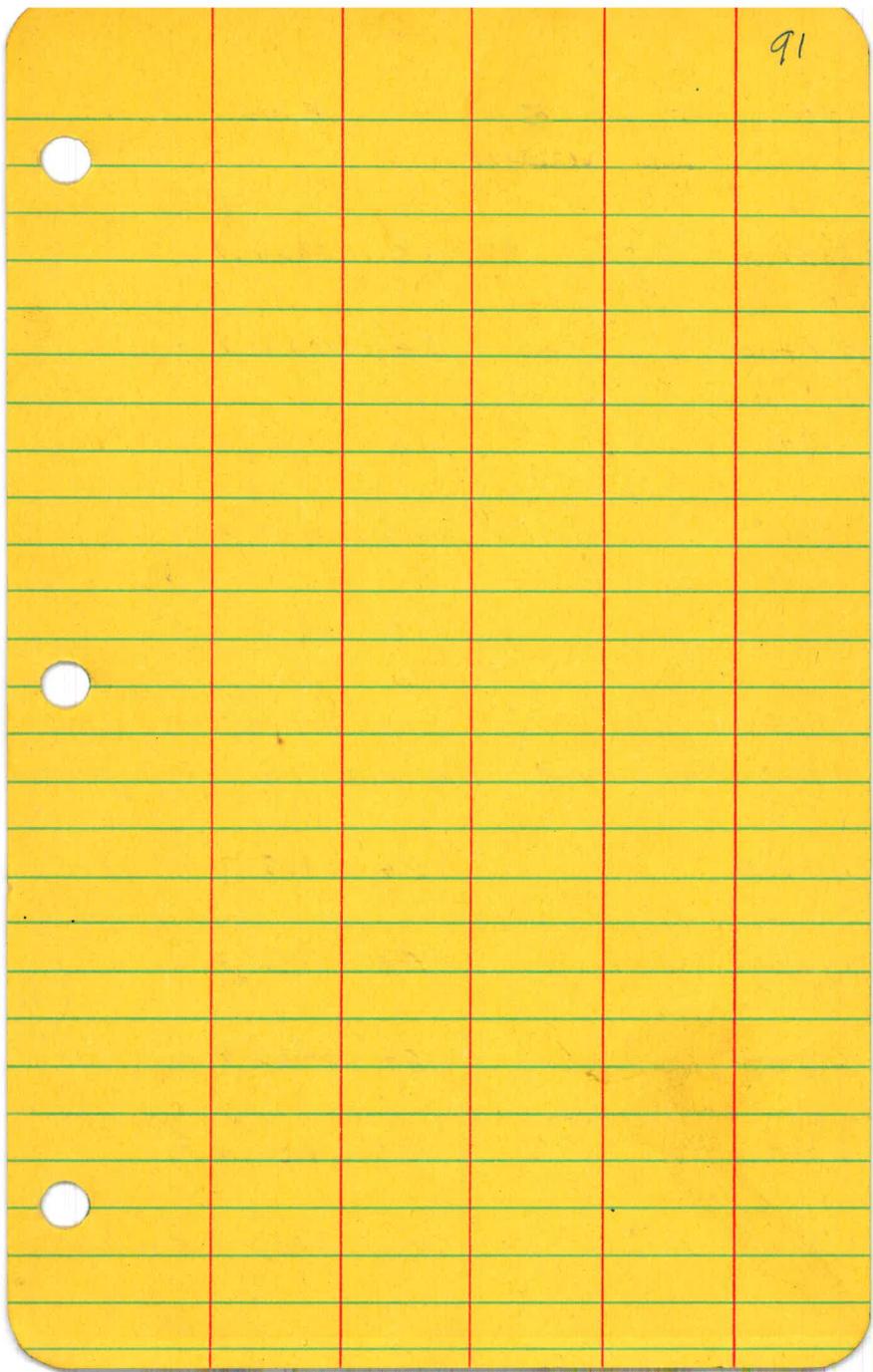


| Sta. | + | π | - | Elev. |
|--------|-------|----------|-------|------------------------------|
| | | 1446.128 | | |
| 588+00 | | | 4.6 | 1441.5 ✓ |
| 589+00 | | | 4.8 | 1441.3 ✓ |
| TF | | | 5.380 | 1440.748 = check 1440.580 |
| | 5.380 | 1445.960 | | |
| 590+00 | | | 5.3 | 1440.7 ✓ |
| 591+00 | | | 4.8 | 1441.2 ✓ |
| 592+00 | | | 7.2 | 1438.8 ✓ |
| TF | | | 7.587 | 1438.373 |
| | 0.198 | 1438.571 | | |
| 593+00 | | | 1.2 | 1437.4 ✓ |
| 594+00 | | | 3.8 | 1434.8 ✓ |
| 595+00 | | | 4.1 | 1434.5 ✓ |
| 596+00 | | | 4.9 | 1433.7 ✓ |

90

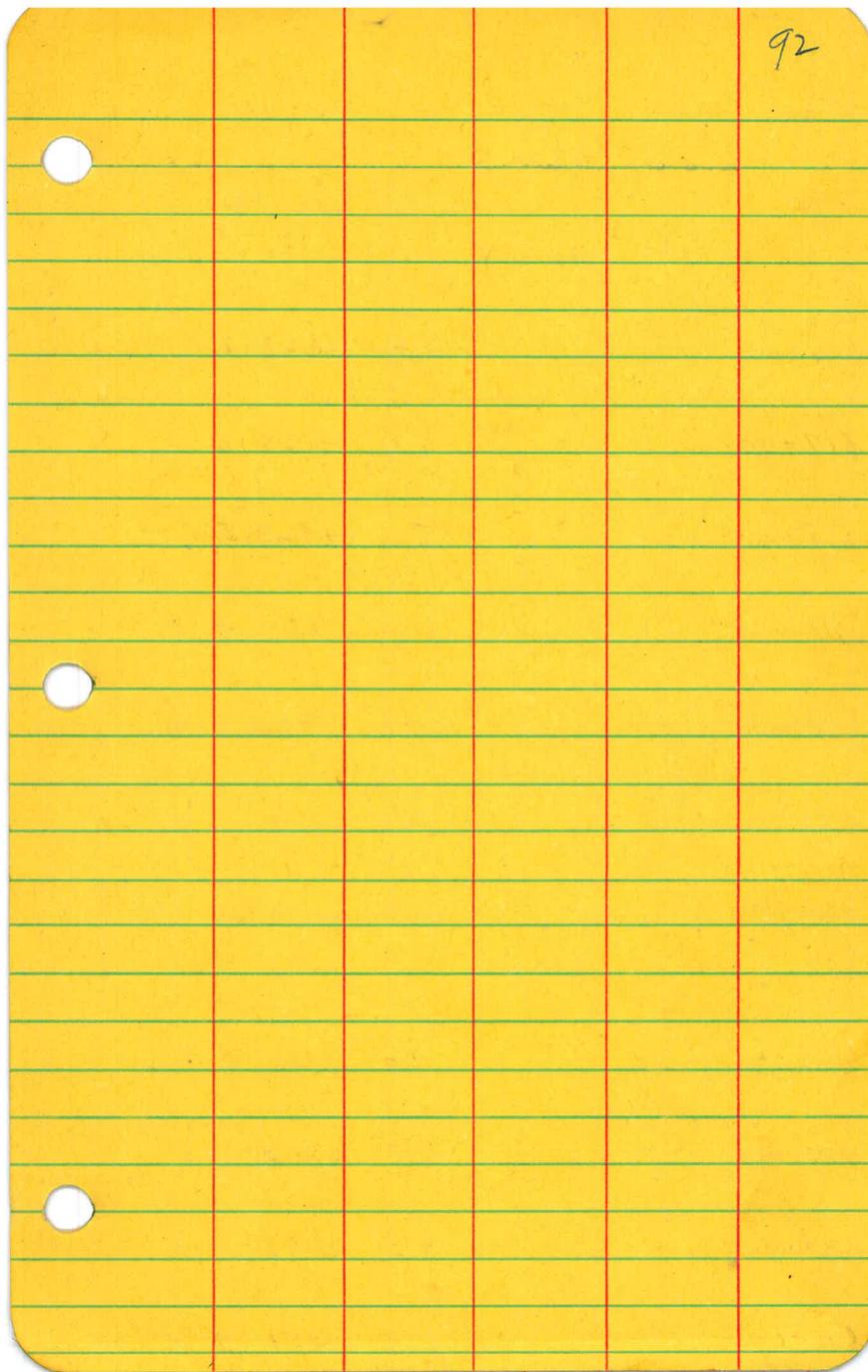
Check on Sec Pt # 57 — E1. 1440.58
We are starting off sec. Elev. 1440.58

| Sta | + | - | Elev |
|--------|----------|----------|----------|
| | 1438.571 | | |
| 597+00 | | 6.3 | 1432.3 ✓ |
| 598+00 | | 3.4 | 1435.2 ✓ |
| T.H. | | 4.009 | 1434.567 |
| | 5.732 | 1440.299 | |
| 599+00 | | 3.1 | 1437.2 ✓ |
| +50 | | 1.2 | 1439.1 ✓ |
| 600+00 | | 3.3 | 1437.0 ✓ |
| 601+00 | | 7.6 | 1432.7 ✓ |
| 602+00 | | 8.5 | 1431.8 ✓ |
| 603+00 | | 9.4 | 1430.9 ✓ |
| T.H. | | 9.390 | 1430.909 |
| | 1.566 | 1432.475 | |
| 604+00 | | 2.6 | 1429.9 ✓ |



| Sta | + | π | - | Elev. |
|--------|-------|----------|-------|----------|
| | | 1432.475 | | |
| 605+00 | | | 2.6 | 1429.9 ✓ |
| 606+00 | | | 5.4 | 1427.1 ✓ |
| 607+00 | | | 6.7 | 1425.8 ✓ |
| 608+00 | | | 8.0 | 1424.5 ✓ |
| 609+00 | | | 6.7 | 1425.8 ✓ |
| T.P. | | | 6.374 | 1426.101 |
| | 5.010 | 1431.111 | | |
| 610+00 | | | 5.4 | 1425.7 ✓ |
| 611+00 | | | 5.4 | 1425.7 ✓ |
| 612+00 | | | 5.2 | 1425.9 ✓ |
| 613+00 | | | 4.5 | 1426.6 ✓ |
| 614+00 | | | 5.0 | 1426.1 ✓ |
| 615+00 | | | 6.1 | 1425.0 ✓ |

92



| Sta. | + | π | - | Elev. |
|--------|-------|----------|--------|----------|
| | | 1431.111 | | |
| T.F. | | | 4.240 | 1426.871 |
| | 7.688 | 1434.559 | | |
| 616+00 | | | 6.4 | 1428.2 ✓ |
| 617+00 | | | 4.4 | 1430.2 ✓ |
| 618+00 | | | 5.1 | 1429.5 ✓ |
| 619+00 | | | 8.7 | 1425.9 ✓ |
| 620+00 | | | 10.7 | 1423.9 ✓ |
| 621+00 | | | 10.5 | 1424.1 ✓ |
| T.F. | | | 10.955 | 1423.604 |
| | 7.178 | 1430.782 | | |
| 622+00 | | | 7.0 | 1423.8 ✓ |
| 623+00 | | | 5.8 | 1425.0 ✓ |
| 624+00 | | | 3.5 | 1427.3 ✓ |
| 625+00 | | | 2.9 | 1427.9 ✓ |

576+00

"P" A.C.

10' to center
of Road.

Same Elev.

575+50

Road

15' to center of

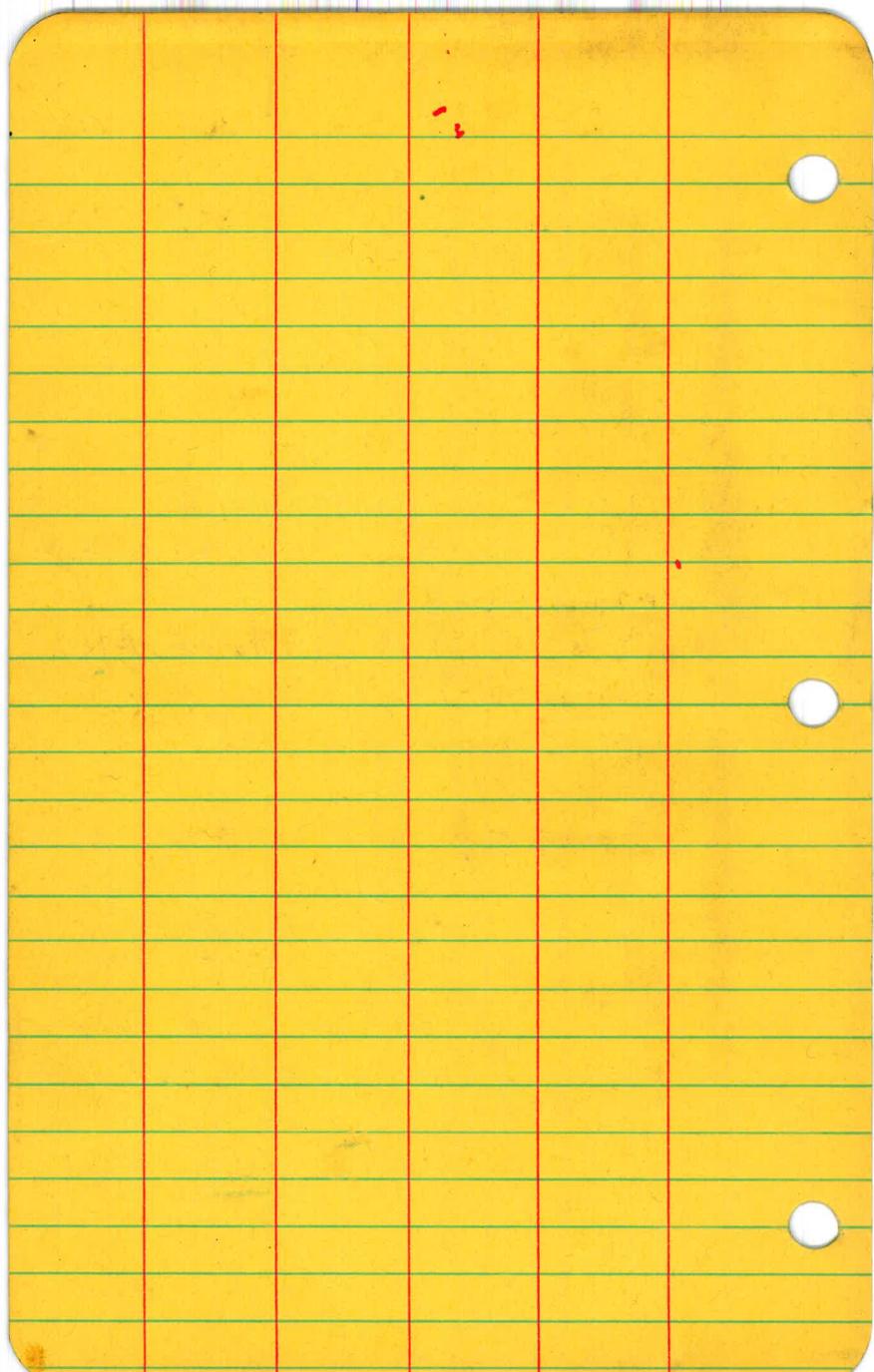
Road is 2'

Lower than
Line here

575+00
Edge of
Road

11' to center
of Road

Same Elev.



1
JAN 16, 1928
SIMPSON
BROOKS

Profile Levels on
Line change starting
from Sta 625+42.9
"P" Line to 649+48

P. Line

Rec'd 1/16/28
Blatt 1/19/28

| Sta. | + | π | - | Elev. |
|--------|--|---------|-------|---------|
| | | | | 1430.12 |
| | 3.50 | 1433.62 | | |
| 625+42 | ^{PI} P.O.T. originally P.I. | | 4.8 | 1428.8 |
| +82 | ^{PI} P.I. | | 3.7 | 1429.9 |
| 626+00 | | | 4.6 | 1429.0 |
| +50 | | | 4.7 | 1428.9 |
| 627+00 | | | 5.4 | 1428.2 |
| +50 | | | 7.6 | 1426.0 |
| 628+00 | | | 9.5 | 1424.1 |
| +50 | | | 10.9 | 1422.7 |
| 629+00 | | | 11.0 | 1422.6 |
| T.P. | | | 10.29 | 1423.33 |
| | 0.51 | 1423.84 | | |
| +50 | | | 2.5 | 1421.3 |

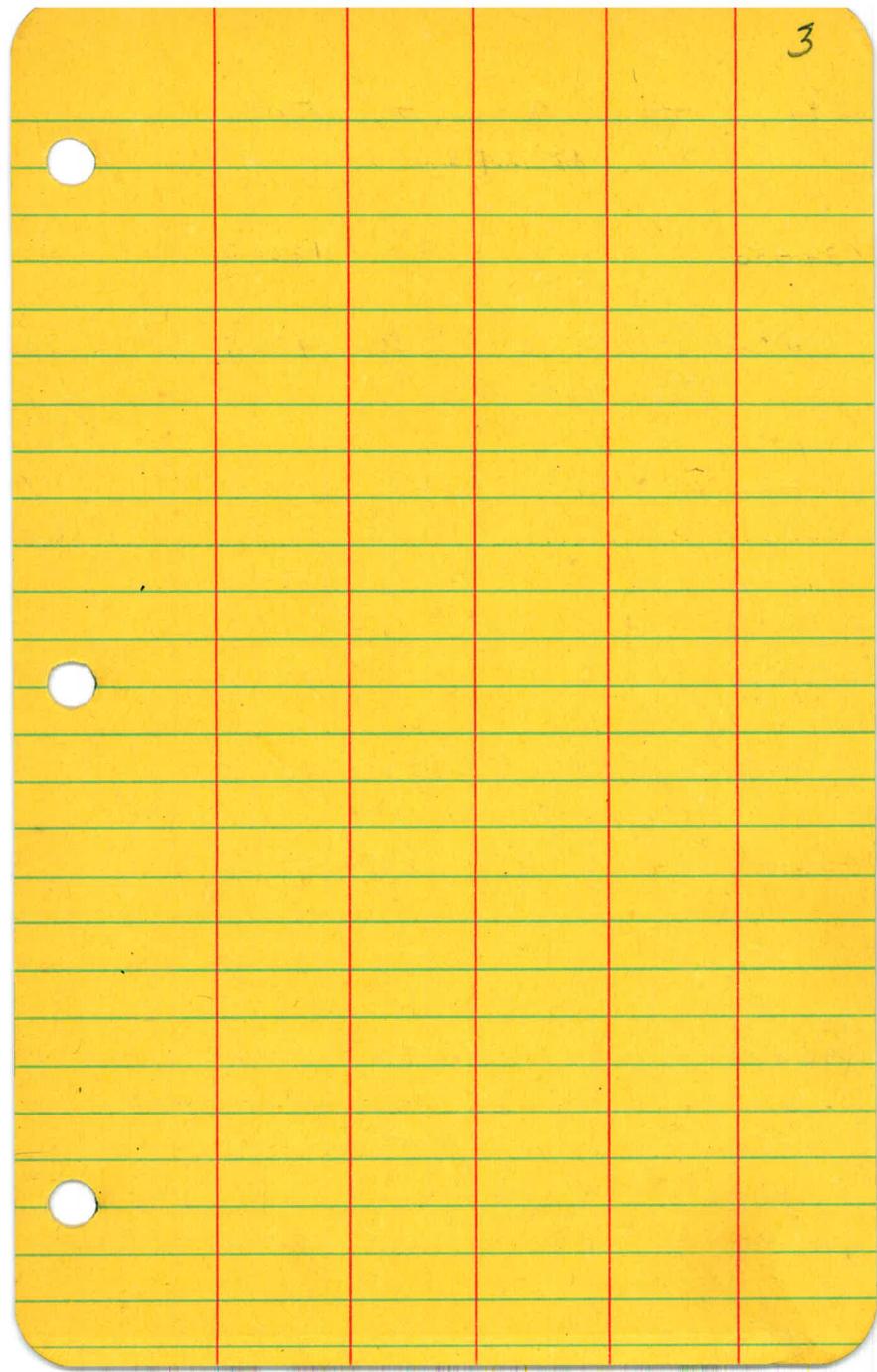
2

E. I. S. D. B. M.

checked
2/1/72

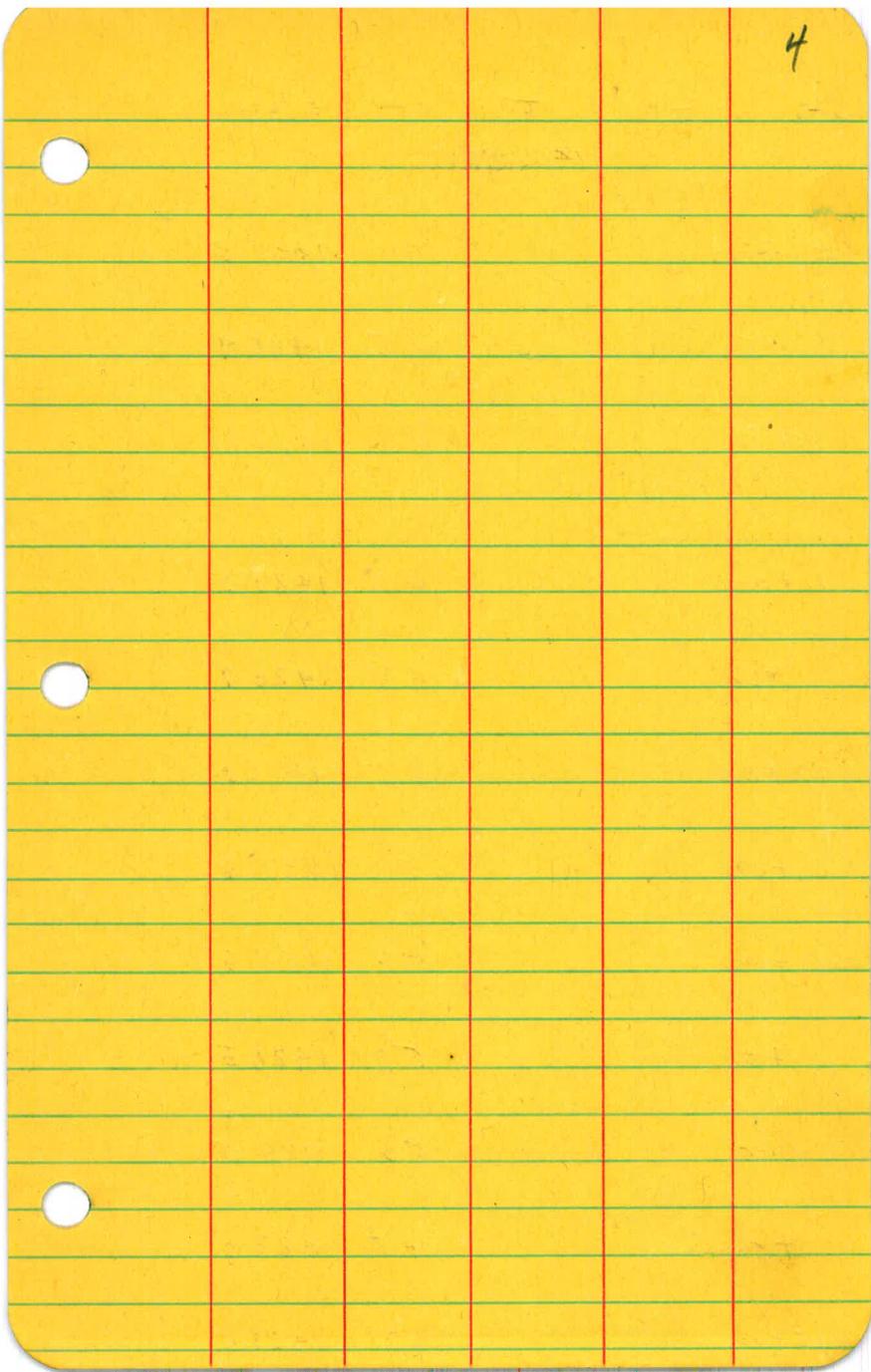
| Sta. | + | π | - | Elev. |
|-----------|-----------------|----------------------|------|---------------------|
| | | 1423.84 [✓] | | |
| 630+00 | | | 3.5 | 1420.3 [✓] |
| +50 | | | 7.2 | 1416.6 [✓] |
| +80 | £ | creek | 16.0 | 1407.8 [✓] |
| Deck of | 15 ⁹ | X18 ⁰ | 8.1 | 1415.7 [✓] |
| | | Bridge | | |
| Creek Bed | under | Bridge | 15.1 | 1408.7 [✓] |
| 631+00 | | | 12.8 | 1411.0 [✓] |
| +50 | | | 11.7 | 1412.1 [✓] |
| 632+00 | | | 10.8 | 1413.0 [✓] |
| +50 | | | 10.4 | 1413.4 [✓] |
| 633+00 | | | 10.6 | 1413.2 [✓] |
| +50 | | | 9.4 | 1414.4 [✓] |
| 634+00 | | | 6.0 | 1417.8 [✓] |

3

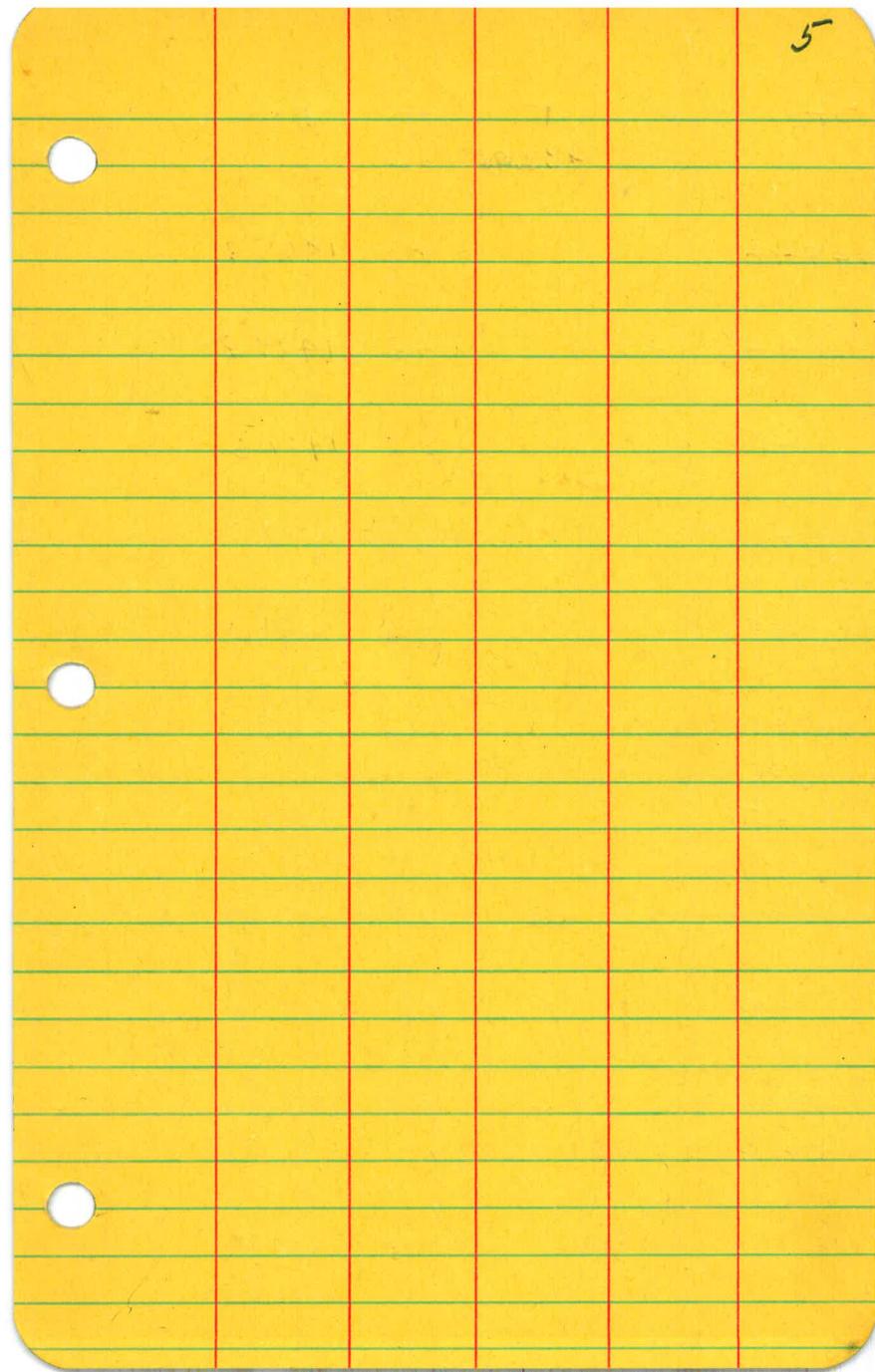


| Sta. | + | \bar{x} | - | Elev. |
|---------------|------|-----------|------|-----------|
| | | 1423.84 | | |
| 634+50 | | | 2.6 | 1421.2 ✓ |
| TF | | | 2.56 | 1421.28 ✓ |
| | 5.64 | 1426.92 | | |
| 635+00 | | | 4.2 | 1422.7 ✓ |
| +50 | | | 6.8 | 1420.1 ✓ |
| 636+00 | | | 6.7 | 1420.2 ✓ |
| +50 | | | 7.4 | 1419.5 ✓ |
| 637+00 | | | 6.5 | 1420.4 ✓ |
| +50 | | | 5.2 | 1421.7 ✓ |
| 638+00 | | | 5.3 | 1421.6 ✓ |
| +50 | | | 5.2 | 1421.7 ✓ |
| 639+00 | | | 3.5 | 1423.4 ✓ |
| +50 | | | 1.8 | 1425.1 ✓ |

4



| Sta. | t | T | - | Elev. |
|--------|------|----------------------|------|----------------------|
| | | 1426.92 [✓] | | |
| 640+00 | | | 1.4 | 1425.5 [✓] |
| | +50 | | 0.5 | 1426.4 [✓] |
| | | | 0.59 | 1426.33 [✓] |
| | 7.13 | 1433.46 | | |
| 641+00 | | | 6.5 | 1427.0 [✓] |
| | +50 | | 6.8 | 1426.7 [✓] |
| 642+00 | | | 6.5 | 1427.0 [✓] |
| | +50 | | 5.9 | 1427.6 [✓] |
| 643+00 | | | 4.9 | 1428.6 [✓] |
| | +50 | | 5.2 | 1428.3 [✓] |
| 644+00 | | | 5.0 | 1428.5 [✓] |
| | +50 | | 4.5 | 1429.0 [✓] |
| 645+00 | | | 4.3 | 1429.2 [✓] |



| Sta | + | τ | - | Elev. |
|--------------------|---|-----------|------|-----------|
| | | 1433.46 ✓ | | |
| 645+50 | | | 7.3 | 1429.2 ✓ |
| 646+00 | | | 4.2 | 1429.3 ✓ |
| +50 | | | 3.9 | 1429.6 ✓ |
| 647+00 | | | 3.2 | 1430.3 ✓ |
| +50 | | | 2.1 | 1431.4 ✓ |
| 648+00 | | | 2.3 | 1431.2 ✓ |
| +50 | | | 2.0 | 1431.5 ✓ |
| 649+00 | | | 1.6 | 1431.9 ✓ |
| +50 | | | 1.2 | 1432.3 ✓ |
| 650+48 | | | 0.8 | 1432.7 ✓ |
| End of Line change | | | | |
| | | | 0.63 | 1432.83 ✓ |
| | | | | 1432.855 |

96

BM # P5 - Nail in white 4'x4'
MONUMENT - 15' South of SP 649+80
Elev. = 1432.855

| Sta. | + | π | - | Elev. |
|--------|-------|----------|-------|----------|
| | | | | 1432.855 |
| | 5.310 | 1438.165 | | |
| 650+00 | | | 6.0 | 1432.2 ✓ |
| 651+00 | | | 5.4 | 1432.8 ✓ |
| 652+00 | | | 4.4 | 1433.8 ✓ |
| | | | 5.0 | 1433.2 ✓ |
| 653+00 | | | 4.3 | 1433.9 ✓ |
| 654+00 | | | 4.1 | 1434.1 ✓ |
| | | | 4.9 | 1433.3 ✓ |
| 655+00 | | | 6.5 | 1431.7 ✓ |
| 656+00 | | | 9.5 | 1428.7 ✓ |
| T.P. | | | 9.166 | 1428.999 |
| | 2.085 | 1431.084 | | |

Center of Rd opp. 652+00

center of Rd 654+00

| Sta. | + | ∓ | - | Elev. |
|----------------|-------|----------|-------|----------|
| | | 1431.084 | | |
| 657+00 | | | 2.8 | 1428.3 ✓ |
| 658+00 | | | 4.7 | 1426.4 ✓ |
| 659+00 | | | 4.3 | 1426.8 ✓ |
| 660+00 | | | 4.9 | 1426.7 ✓ |
| 661+00 | | | 5.8 | 1425.3 ✓ |
| 662+00 | | | 5.1 | 1426.0 ✓ |
| 7.1 | | | 3.795 | 1427.289 |
| | 4.877 | 1432.166 | | |
| 663+00 | | | 4.3 | 1427.9 ✓ |
| 664+00 | | | 3.1 | 1429.1 ✓ |
| | | | 3.6 | 1428.5 ✓ |
| +50 | | | 2.5 | 1429.7 ✓ |
| | | | 3.9 | 1428.3 ✓ |

center of Rd opp. 664 + 00

center of Rd opp 664 + 50

| Sta. | + | π | - | Elev. |
|--------|-------|----------|-------|----------|
| | | 1432.166 | | |
| 665+00 | | | 3.2 | 1429.0 ✓ |
| 666+00 | | | 7.3 | 1424.9 ✓ |
| | | | 6.9 | 1425.3 ✓ |
| 667+00 | | | 8.9 | 1423.3 ✓ |
| 668+00 | | | 9.8 | 1422.4 ✓ |
| TF | | | 9.178 | 1422.988 |
| | 3.670 | 1426.658 | | |
| 669+00 | | | 9.4 | 1422.3 ✓ |
| 670+00 | | | 6.0 | 1420.7 ✓ |
| 671+00 | | | 5.8 | 1420.9 ✓ |
| 672+00 | | | 4.9 | 1421.8 ✓ |
| 673+00 | | | 5.8 | 1420.9 ✓ |
| 674+00 | | | 6.7 | 1420.0 ✓ |

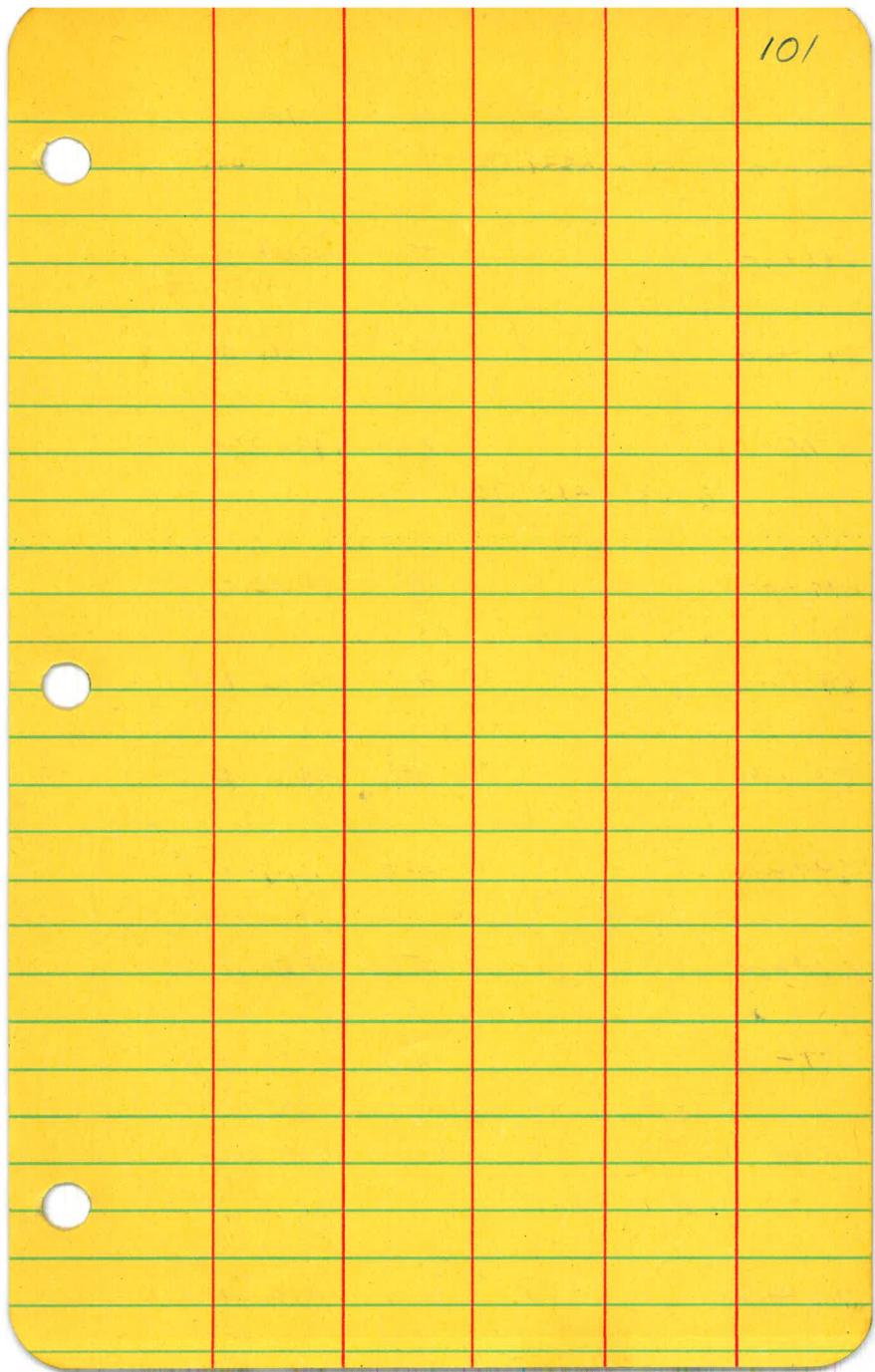
99

center of Rd opp 666+00

| Sta. | + | π | - | Elev. |
|------------------------|--------|----------|-------|---------------------|
| | | 1426.658 | | |
| TF | | | 6.835 | 1419.823 |
| | 3.718 | 1423.541 | | |
| 675+00 | | | 4.8 | 1418.7 ✓ |
| 676+00 | | | 5.1 | 1418.9 ✓ |
| 677+00 | | | 5.1 | 1418.9 ✓ |
| 678+00 | | | 7.1 | 1416.9 ✓ |
| TF | | | 7.093 | 1416.498 = BM # P-6 |
| | 11.110 | 1427.608 | | |
| +02 ²⁴ P.I. | | | 11.1 | 1416.7 ⁵ |
| 679+00 | | | 11.1 | 1416.7 ⁵ |
| 680+00 | | | 7.4 | 1420.2 ✓ |
| 681+00 | | | 5.3 | 1422.3 ✓ |
| 682+00 | | | 5.1 | 1422.5 ✓ |

B.M. # P-6 - nail in 2"x4"
monument - 17' south west
of Sta 678+02²⁴
Elevation = 1416.498.

| Sta. | + | T | - | Elev. |
|--------|-------|----------|-------|----------|
| | | 1427.608 | | |
| 683+00 | | | 3.0 | 1423.6 ✓ |
| 684+00 | | | 1.7 | 1425.9 ✓ |
| T.F. | | | 1.350 | 1426.258 |
| | 7.122 | 1433.380 | | |
| 685+00 | | | 7.2 | 1426.7 ✓ |
| 686+00 | | | 6.7 | 1426.7 ✓ |
| 687+00 | | | 5.2 | 1428.2 ✓ |
| 688+00 | | | 5.4 | 1428.0 ✓ |
| 689+00 | | | 5.6 | 1427.7 ✓ |
| T.F. | | | 4.272 | 1429.108 |
| | 5.490 | 1434.598 | | |
| 690+00 | | | 5.8 | 1428.8 ✓ |
| 691+00 | | | 4.6 | 1430.0 ✓ |



| Sta. | + | T | - | Elev. |
|--------|--------|----------|-------|----------|
| | | 1434.592 | | |
| 692+00 | | | 5.1 | 1429.5 ✓ |
| 693+00 | | | 3.8 | 1430.8 ✓ |
| TA | | | 1.278 | 1433.320 |
| | 12.206 | 1445.526 | | |
| 694+00 | | | 12.5 | 1433.0 ✓ |
| 695+00 | | | 9.9 | 1435.6 ✓ |
| 696+00 | | | 5.2 | 1440.3 ✓ |
| 697+00 | | | 4.2 | 1441.3 ✓ |
| 698+00 | | | 5.6 | 1439.9 ✓ |
| 699+00 | | | 8.1 | 1437.4 ✓ |
| TA | | | 7.210 | 1438.316 |
| | 7.420 | 1445.736 | | |
| 700+00 | | | 6.3 | 1439.4 ✓ |

102

| Sta. | + | π | - | Elev. |
|--------|-----------------|-------------|--------|-----------------------|
| | | 1445.736 | | |
| 700+50 | | | 5.0 | 1440.7 ✓ |
| 701+00 | | | 7.3 | 1438.4 ✓ |
| +50 | | | 8.3 | 1437.4 ✓ |
| TP | | | 12.070 | 1433.666 |
| | 2.585 | 1436.251 | | |
| 702+00 | | | 9.7 | 1428.6 ✓ |
| +50 | | | 15.9 | 1420.9 ✓ |
| +86 | $\frac{53}{50}$ | END of Line | 21.2 | 1415.1 ✓ |
| TP | | | 12.060 | 1424.191 - B.M. # P-7 |

on ledge of Rock running E. and W.

B.M. # P[#] 7 - High Point on
Large Boulder - 10' west
of Sta. 702+71. El. = 1424.191

