#774

MICROFILMED
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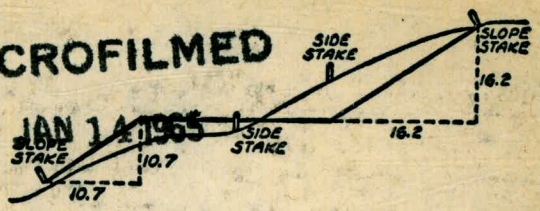

Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32 20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34 20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35 10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36 00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

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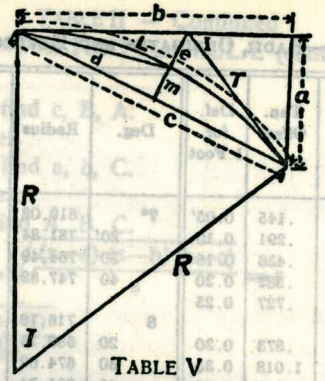


TABLE V

CURVE FORMULÆ FOR SIMPLE CURVES

COMPILED BY J. CALVIN LOCKE, C. E.

(1) $c = \sqrt{2Ra}$ (2) $c = \sqrt{a^2+b^2}$

(3) $c = \sqrt{2R\,(R-\sqrt{(R+b)\,(R-b)}} = \sqrt{2R\,(R-\sqrt{R^2-b^2})}$

(4) $c = 2\sqrt{m\,(2R-m)}$

(5) $c = 2R \sin {}^1/_2\, I$ (6) $c = 2T \cos {}^1/_2\, I$

(7) $e = R \operatorname{exsec} {}^1/_2\, I$

(8) $e = R \tan {}^1/_2\, I \tan {}^1/_4\, I$ (9) $e = T \tan {}^1/_4\, I$

(10) $b = \sqrt{a\,(2R-a)}$

(11) $b = \sqrt{\left(c+\frac{c^2}{2R}\right)\left(c-\frac{c^2}{2R}\right)} = \sqrt{c^2-\frac{c^4}{4R^2}}$

(12) $b = R \sin I$ (13) $b = a \cot {}^1/_2\, I$

(14) $R = \frac{a^2+b^2}{2a} = \frac{c^2}{2a}$ (15) $R = \frac{d^2}{2m} = \frac{c^2+4m^2}{8m}$

(16) $d = \sqrt{R\,(2R-\sqrt{(2R+c)\,2R-c)}} = \sqrt{R\,(2R-\sqrt{4R^2-c^2})}$

(17) $d = \sqrt{2Rm}$ (18) $d = 2R \sin {}^1/_4\, I$ (19) $m = \frac{d^2}{2R}$

(20) $m = R \mp \sqrt{\left(R+\frac{c}{2}\right)\left(R-\frac{c}{2}\right)} = R \mp \sqrt{R^2-\frac{c^2}{4}}$

(21) $m = R \operatorname{vers} {}^1/_2\, I$ (22) $m = R \sin {}^1/_2\, I \tan {}^1/_4\, I$ (23) $m = {}^1/_2\, c \tan {}^1/_4\, I$

(24) $a = \frac{c^2}{2R}$ (25) $a = R - \sqrt{(R+b)\,(R-b)} = R - \sqrt{R^2-b^2}$

(26) $a = 2R\,(\sin^2 {}^1/_2\, I)^2$ (27) $a = R \operatorname{vers} I$ (28 $a = R \sin I \tan {}^1/_2$

(29) $a = b \tan {}^1/_2\, I$ (30) $a = T \sin I$ (31) $T = R \tan {}^1/_2\, I$

(32) $I = \frac{L}{R} \times 57.295780$ (33) $R = \frac{L}{I} \times 57.295780$

(34) $L = IR \times 0.01745329$ (35) $L = \frac{8d-c}{3}$

(36 Area Seg. $= \frac{LR-R^2 \sin I}{2} = \frac{LR-Rb}{2}$

TABLE VI

SINES, COSINES, TANGENTS, COTANGENTS

deg.	sin 0′	tan 0′	sin 10′	tan 10′	sin 20′	tan 20′	sin 30′	tan 30′	sin 40′	tan 40′	sin 50′	tan 50′	deg.
0	0000	0000	0029	0029	0058	0058	0087	0087	0116	0116	0145	0145	89
1	175	0175	0204	0204	0233	0233	0262	262	291	291	320	320	88
2	349	349	378	378	407	407	436	437	465	466	494	495	87
3	523	524	552	553	581	582	610	612	640	641	669	670	86
4	698	699	727	729	756	758	785	787	814	816	843	846	85
5	872	875	901	904	929	934	958	963	987	992	1016	1022	84
6	1045	1051	1074	1080	1103	1110	1132	1139	1161	1169	190	198	83
7	219	228	248	257	279	287	305	317	334	346	363	376	82
8	392	405	421	435	449	465	478	495	507	524	536	554	81
9	564	584	593	614	622	644	650	673	679	703	708	733	80
10	736	763	765	793	794	823	822	853	851	883	880	914	79
11	908	944	937	974	965	2004	994	2035	2022	2065	2051	2095	78
12	2079	2126	2108	2156	2136	186	2164	217	193	247	221	278	77
13	250	309	278	339	306	370	334	401	363	432	391	462	76
14	419	493	447	524	476	555	504	586	532	617	560	648	75
15	588	679	616	711	644	742	672	773	700	805	728	836	74
16	756	867	784	899	812	931	840	962	868	994	896	3026	73
17	924	3057	952	3089	939	3121	3007	3153	3035	3185	3062	217	72
18	3090	249	3118	281	3145	314	173	346	201	378	228	411	71
19	256	443	283	476	311	508	338	541	365	574	393	607	70
20	420	640	448	673	475	706	502	739	529	772	557	805	69
21	584	839	611	872	638	906	665	939	692	973	719	4006	68
22	746	4040	773	4074	800	4108	827	4142	854	4176	881	210	67
23	907	245	934	279	961	314	987	348	4014	383	4041	417	66
24	4067	452	4094	487	4120	522	4147	557	173	592	200	628	65
25	226	663	253	699	279	734	305	770	331	806	358	841	64
26	384	877	410	913	436	950	4462	986	488	5022	514	5059	63
27	540	5095	566	5132	592	5169	617	5206	643	243	669	280	62
28	695	317	720	354	746	392	772	430	797	467	823	505	61
29	848	543	874	581	899	619	924	658	950	696	975	735	60
30	5000	774	5025	5812	5050	851	5075	890	5100	930	5125	969	59
31	150	6009	175	6048	200	6088	225	6128	250	6168	275	6208	58
32	299	249	324	289	348	330	5373	371	398	412	422	453	57
33	446	494	471	536	495	577	519	619	544	661	568	703	56
34	592	745	616	787	640	830	664	873	688	916	712	959	55
35	736	7002	760	7046	783	7089	807	7133	831	7177	854	7221	54
36	878	265	901	310	925	355	948	400	972	445	995	490	53
37	6018	536	6041	581	6065	627	6088	673	6111	720	6134	766	52
38	157	813	180	860	202	907	225	954	248	8002	271	8050	51
39	293	8098	316	8146	338	8195	361	8243	383	292	406	342	50
40	428	391	450	441	472	491	494	541	517	591	539	642	49
41	561	693	583	744	604	796	626	847	648	899	670	952	48
42	691	9004	713	9057	734	9110	756	9163	777	9217	799	9271	47
43	820	325	841	380	862	435	884	490	905	545	926	601	46
44	947	657	967	713	988	770	7009	827	7030	884	7050	942	45
45	7071	1.0000	7092	1.0058	7112	1.0117	133	1.0176	153	1.0235	173	1.0295	44
deg.	60′ cos	60′ cot	50′ cos	50′ cot	40′ cos	40′ cot	30′ cos	30′ cot	20′ cos	20′ cot	10′ cos	10′ cot	deg.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

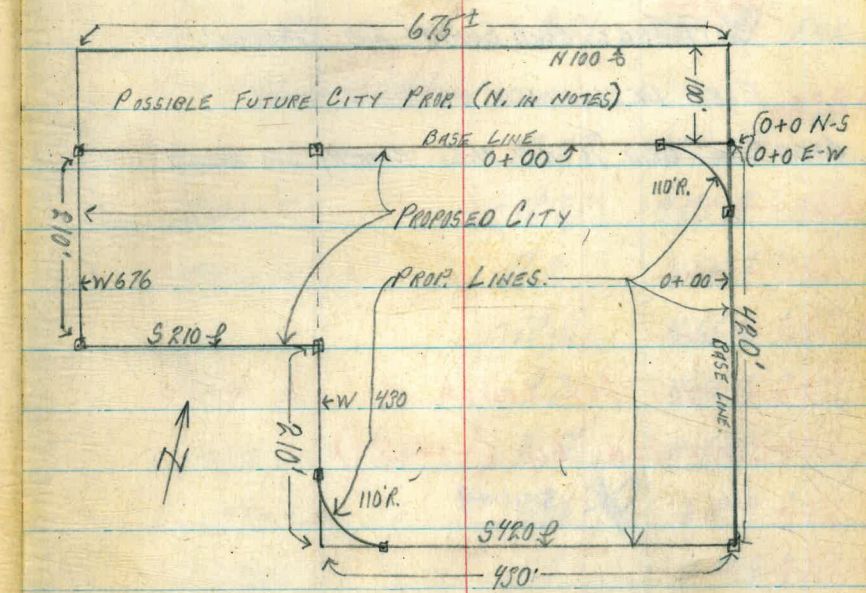
Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	.26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

FOR EXTERNALS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

NE COT. O-E W O-N-S 1.

PROPOSED BAY VIEW RESERVOIR, X-SECTIONS



X-SECTIONS STARTED AT POINT SHOWN ABOVE, AND RAN OUT ALONG N-S LINES.

MAY 6: MR. BEERMAN GAVE INSTRUCTIONS TO OMIT X-SECTIONS IN THE ADDITIONAL 100 FT. STRIP ACROSS N. END AND THE 1.18 ACRE PARCEL ON THE WEST END, AND TO COVER THE MAIN 4 ACRE AREA IN 20 FT. SQUARES.

D. Leonard,

B.M.: Conc. Mon. 41.5' left of E.C. 41+52 on City Eng's. Road Survey for Soledad Drive.

Elev. determined by King's Party.

0+00 for grid is at N.E. Corner; see sketch on Page 1.

* Wrong elev for bench. All elevations corrected by (-14.53)

JK 5/11/49

DML

May 6, 1949 Leonard - Notes Payne - T Carver - Rod P.

Bay View Reservoir Site, X-Sections

B.M.	+12.83	~~471.80~~ 456.77		~~456.47~~ 443.94 * Conc. Mon.
T.P.			-9.51	~~461.97~~ 447.46 Rock
	+3.87	~~465.86~~ 451.33		
0+00	N.E. Cor.		-13.28	~~452.58~~ 438.05 Hub
East Line	20S		-12.2	~~453.7~~ 439.1
"	40S		-11.2	~~454.7~~ 440.1
"	60S		-10.8	~~456.6~~ 441.0
"	80S		-9.2	~~456.7~~ 442.1
"	100S		-8.7	~~457.~~ 442.6
"	120S		-8.6	~~457.3~~ 442.7
"	140S		-7.9	~~456.0~~ 443.4
"	160S		-7.7	~~456.~~ 443.6
"	180S		-7.1	~~456.~~ 444.2
"	200S		-6.4	~~457.5~~ 444.9
"	220S		-5.3	~~460.6~~ 446.0
"	240S		-4.5	~~461.4~~ 446.8
"	260S		-4.1	~~461.8~~ 447.2
"	280S		-3.7	~~462.~~ 447.6
"	300S		-3.4	~~462.6~~ 447.9

			451.33 ~~465.86~~	
E.Line	320S	-3.1	~~462.8~~	448.2
"	340S	-2.7	~~465.2~~	448.6
"	360S	-2.6	~~465.5~~	448.7
"	380S	-2.0	~~465.9~~	449.3
"	400S	-1.9	~~464.0~~	449.4
"	420S	-1.29	~~464.57~~	OH Hub
20W.	420S	-2.1	~~465.8~~	449.2
"	400S	-2.1	~~465.8~~	449.2
"	380S	-2.9	~~463.0~~	448.4
"	360S	-3.6	~~462.3~~	447.7
"	340S	-4.0	~~461.9~~	447.3
"	320S	-4.1	~~461.8~~	447.2
"	300S	-4.2	~~461.7~~	447.1
"	280S	-4.5	~~461.4~~	446.8
"	260S	-4.6	~~461.3~~	446.7
"	240S	-4.6	~~461.3~~	446.7
"	220S	-5.5	~~460.4~~	445.8
"	200S	-6.2	~~459.7~~	445.1
"	180S	-6.7	~~451.2~~	444.6

			451.33 ~~465.86~~	
20W	160S	-6.8	~~459.1~~	444.5
"	140S	-7.8	~~458.1~~	443.5
"	120S	-8.1	~~457.8~~	443.2
"	100S	-8.8	~~457.1~~	442.5
"	80S	-9.0	~~456.9~~	442.3
"	60S	-10.0	~~455.9~~	441.3
"	40S	-10.0	~~455.9~~	441.3
"	20S	-11.0	~~454.9~~	440.3
"	00	-13.1	~~452.8~~	438.2
40W	00	-12.5	~~453.4~~	438.8
	20S	-11.5	~~454.4~~	439.8
	40S	-10.5	~~455.4~~	440.8
	60S	-9.9	~~456.0~~	441.4
	80S	-9.0	~~456.9~~	442.3
	100S	-8.1	~~457.8~~	443.2
	120S	-7.5	~~458.4~~	443.8
	140S	-6.8	~~459.1~~	444.5
	160S	-6.5	~~459.4~~	444.8

		451.33 ~~465.86~~		
40W	180s	-6.5	~~459.4~~	444.8
	200s	-6.0	~~459.9~~	445.3
	220s	-5.6	~~460.3~~	445.7
	240s	-5.2	~~460.7~~	446.1
	260s	-5.2	~~460.7~~	446.1
	280s	-5.0	~~460.9~~	446.3
	300s	-4.2	~~461.7~~	447.1
	320s	-4.6	~~461.3~~	446.7
	340s	-4.4	~~461.5~~	446.9
	360s	-4.0	~~461.9~~	447.3
	380s	-3.2	~~462.7~~	448.1
	400s	-2.1	~~463.8~~	449.2
	420s	-1.9	~~464.0~~	449.4
60W	420s	-2.0	~~463.9~~	449.3
	400s	-2.9	~~463.0~~	448.4
	380s	-2.9	~~463.0~~	448.4
	360s	-4.5	~~461.4~~	446.8
	340s	-4.7	~~461.2~~	446.6

		451.33 ~~465.86~~		
60W	320s	-4.9	~~461.0~~	446.4
	300s	-5.3	~~460.6~~	446.0
	280s	-5.5	~~460.4~~	445.8
	260s	-5.6	~~460.3~~	445.7
	240s	-5.7	~~460.2~~	445.6
	220s	-5.4	~~460.5~~	445.9
	200s	-5.7	~~460.2~~	445.6
	180s	-5.5	~~460.4~~	445.8
	160s	-5.7	~~460.2~~	445.6
	140s	-6.3	~~459.6~~	445.0
	120s	-7.1	~~458.8~~	444.2
	100s	-8.0	~~457.9~~	443.3
	80s	-8.6	~~457.3~~	442.7
	60s	-9.5	~~456.4~~	441.8
	40s	-10.0	~~456.9~~	441.3
	20s	-11.2	~~454.7~~	440.1
	00	-10.9	~~455.0~~	440.4

			451.33 ~~465.86~~	
80W	00	-9.2	~~456.1~~	442.1
	20s	-9.8	~~456.1~~	441.5
	40s	-9.4	~~456.5~~	441.9
	60s	-8.6	~~451.3~~	442.7
	80s	-7.9	~~450.0~~	443.4
	100s	-6.5	~~451.4~~	444.8
	120s	-6.9	~~451.0~~	444.4
	140s	-6.5	~~451.6~~	445.0
	160s	-5.1	~~460.5~~	446.2
	180s	-4.7	~~461.2~~	446.6
	200s	-5.0	~~460.9~~	446.3
	220s	-5.1	~~460.5~~	446.2
	240s	-5.3	~~460.6~~	446.0
	260s	-5.9	~~460.0~~	445.4
	280s	-5.8	~~460.1~~	445.5
	300s	-5.5	~~460.4~~	445.8
	320s	-5.4	~~460.5~~	445.9
	340s	-5.1	~~460.5~~	446.2
	360s	-4.5	~~461.4~~	446.8

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80W	380s	-4.3	~~461.6~~	447.0
	400s	-3.2	~~462.7~~	448.1
	420s	-2.4	~~463.5~~	448.9
100W	420s	-2.3	~~463.6~~	449.0
	400s	-3.3	~~462.6~~	448.0
	380s	-4.6	~~461.3~~	446.7
	360s	-5.1	~~460.8~~	446.2
	340s	-5.2	~~460.7~~	446.1
	320s	-5.6	~~460.3~~	445.7
	300s	-5.8	~~460.1~~	445.5
	280s	-6.9	~~460.0~~	445.4
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	220s	-5.5	~~460.4~~	445.8
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	180s	-5.3	~~460.6~~	446.0
	160s	-5.8	~~460.1~~	445.5
	140s	-6.2	~~460.7~~	445.1

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100W	120S	-6.0	~~454.9~~	445.3
	100S	-6.0	~~454.9~~	445.3
	80S	-7.0	~~458.9~~	444.3
	60S	-7.4	~~458.6~~	443.9
	40S	-8.3	~~451.6~~	443.0
	20S	-8.4	~~451.6~~	442.9
	00	-7.7	~~450.2~~	443.6
120W	00	-6.6	~~450.3~~	444.7
	20S	-7.2	~~450.1~~	444.1
	40S	-7.3	~~458.6~~	444.0
	60S	-6.4	~~451.5~~	444.9
	80S	-5.5	~~460.4~~	445.8
	100S	-5.3	~~460.6~~	446.0
	120S	-5.2	~~460.7~~	446.1
	140S	-5.6	~~460.3~~	445.7
	160S	-5.5	~~460.4~~	445.8
	180S	-5.8	~~460.1~~	445.5
	200S	-5.7	~~460.2~~	445.6

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120W	220S	-5.9	~~460.0~~	445.4
	240S	-6.0	~~454.9~~	445.3
	260S	-5.8	~~460.1~~	445.5
	280S	-5.7	~~460.2~~	445.6
	300S	-5.9	~~460.0~~	445.4
	320S	-5.0	~~460.9~~	446.3
	340S	-5.3	~~460.6~~	446.0
	360S	-5.2	~~460.7~~	446.1
	380S	-5.0	~~460.9~~	446.3
	400S	-3.8	~~462.1~~	447.5
	420S	-2.2	~~463.7~~	449.1
140W	420S	-2.7	~~463.2~~	448.6
	400S	-4.8	~~461.1~~	446.5
	380S	-4.6	~~461.3~~	446.7
	360S	-5.4	~~460.5~~	445.9
	340S	-5.3	~~460.6~~	446.0
	320S	-4.7	~~461.2~~	446.6
	300S	-5.9	~~460.0~~	445.4

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140W	280S	-5.8	~~460.1~~	445.5
	260S	-6.1	~~459.5~~	445.2
	240S	-6.1	~~459.8~~	445.2
	220	-6.1	~~459.8~~	445.2
	200S	-6.2	~~459.7~~	445.1
	180S	-6.5	~~460.4~~	445.8
	160S	-4.9	~~461.0~~	446.4
	140S	-4.6	~~461.3~~	446.7
	120S	-4.4	~~461.5~~	446.9
	100S	-4.7	~~461.2~~	446.6
	80S	-5.7	~~460.2~~	445.6
	60S	-6.3	~~459.6~~	445.0
	40S	-6.3	~~459.6~~	445.0
	20S	-6.0	~~459.9~~	445.3
	00	-5.0	~~460.9~~	446.3
			447.41 ~~461.94~~	
T.P. Rock.		-3.92		
+5.99		453.40 ~~467.93~~		

		453.40 ~~467.93~~	
160W	00	-5.6	~~462.3~~ 447.8
	20S	-6.9	~~461.0~~ 446.5
	40S	-7.5	~~460.4~~ 445.9
	60S	-7.7	~~460.2~~ 445.7
	80S	-7.5	~~460.4~~ 445.9
	100S	-7.0	~~460.9~~ 446.4
	120S	-6.5	~~461.4~~ 446.9
	140S	-6.2	~~461.7~~ 447.2
	160S	-6.7	~~461.2~~ 446.7
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	200S	-8.3	~~459.6~~ 445.1
	220S	-8.7	~~459.2~~ 444.7
	240S	-8.7	~~459.2~~ 444.7
	260S	-8.5	~~459.4~~ 444.9
	280S	-8.1	~~459.8~~ 445.3
	300S	-8.0	~~459.9~~ 445.4
	320S	-7.7	~~460.2~~ 445.7
	340S	-7.5	~~460.4~~ 445.9
	360S	-7.5	~~460.4~~ 445.9

		453.40 ~~467.93~~			
160W	380s		-7.1	~~460.8~~	446.3
	400s		-6.7	~~461.2~~	446.7
	420s		-5.7	~~462.2~~	447.7
180W	420s		-5.9	~~462.0~~	447.5
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	260s		-8.6	~~459.3~~	444.8
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	220s		-8.9	~~459.0~~	444.5
	200s		-8.7	~~459.2~~	444.7
	180s		-7.4	~~460.5~~	446.0
	160s		-7.2	~~460.7~~	446.2
	140s		-7.0	~~460.9~~	446.4

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180W	120s		-7.0	~~460.9~~	446.4
	100s		-7.1	~~460.8~~	446.3
	80s		-7.1	~~460.8~~	446.3
	60s		-7.0	~~460.9~~	446.4
	40s		-6.6	~~461.3~~	446.8
	20s		-5.6	~~462.3~~	447.8
	00		-4.7	~~463.2~~	448.7
200W	00		-3.8	~~464.1~~	449.6
	20s		-4.9	~~463.0~~	448.5
	40s		-5.4	~~462.5~~	448.0
	60s		-6.5	~~461.4~~	446.9
	80s		-6.9	~~461.0~~	446.5
	100s		-6.7	~~461.2~~	446.7
	120s		-7.4	~~460.5~~	446.0
	140s		-7.9	~~460.0~~	445.5
	160s		-8.2	~~459.7~~	445.2
	180s		-8.7	~~459.2~~	444.7
	200s		-9.1	~~458.8~~	444.3

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200W	220 S	-9.1	~~458.8~~	~~444.3~~
	240S	-8.9	~~459.0~~	~~444.5~~
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	280S	-7.7	~~460.2~~	445.7
	300S	-8.1	~~459.8~~	445.3
	320S	-7.9	~~460.0~~	445.5
	340S	-7.3	460.6	446.1
	360S	-6.4	~~461.5~~	447.0
	380S	-6.7	461.2	446.7
	400S	-6.2	~~461.7~~	447.2
	420S	-5.5	~~462.4~~	447.9
220W	420S	-5.5	~~462.4~~	447.9
	400S	-5.4	~~462.5~~	448.0
	380S	-6.2	~~461.7~~	447.2
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220W	280S	-7.8	460.1	~~445.6~~
	260S	-8.4	~~459.5~~	~~445.0~~
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	60S	-6.0	~~461.9~~	~~447.4~~
	40S	-5.1	~~462.8~~	~~448.3~~
	20S	-4.2	~~463.7~~	~~449.2~~
	00	-3.1	~~464.8~~	450.3
T.B.M. Hub	S200 W200 } Approx Log.	-8.98	458.95	~~444.2~~
CHECK T.B.M.	+8.98			
	467.93			

~~453.40~~
~~467.8~~

240W	00	-2.5	~~465.4~~	450.9
	20s	-4.0	~~463.9~~	449.4
	40s	-5.0	~~462.9~~	448.4
	60s	-5.6	~~462.3~~	447.8
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	200s	-9.2	~~458.7~~	444.2
	220s	-9.0	~~458.9~~	444.4
	240s	-8.5	~~459.4~~	444.9
	260s	-8.1	~~459.8~~	445.3
	280s	-6.7	~~461.2~~	446.7
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	320s	-6.4	~~461.5~~	447.0
	340s	-5.4	~~462.6~~	448.0
	360s	-5.2	~~462.7~~	448.2

~~453.40~~
~~467.8~~

240W	380s	-5.6	~~462.2~~	447.8
	400s	-5.3	~~462.6~~	448.1
	420s	-5.1	~~462.8~~	448.3
260W	420s	-4.7	~~463.2~~	448.7
	400s	-4.5	~~463.4~~	448.9
	380s	-4.1	~~463.8~~	449.3
	360s	-5.5	~~462.4~~	447.9
	340s	-6.1	~~461.8~~	447.3
	320s	-6.5	~~461.4~~	446.9
	300s	-6.9	~~461.0~~	446.5
	280s	-7.5	~~460.4~~	445.9
	260s	-7.5	~~460.4~~	445.9
	240s	-7.2	~~460.7~~	446.2
	220s	-8.8	~~459.1~~	444.6
	200s	-9.0	~~458.9~~	444.4
	180s	-9.2	~~458.7~~	444.2
	160s	-9.1	~~458.8~~	444.3
	140s	-8.5	~~459.4~~	~~444.9~~ 459.4

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260W	120s	-7.8	~~460.1~~	445.6
	100s	-7.0	~~460.9~~	446.4
	80s	-6.2	~~461.7~~	447.2
	60s	-5.8	~~462.1~~	447.6
	40s	-4.9	~~463.0~~	448.5
	20s	-3.8	~~464.1~~	449.6
	00	-2.1	~~465.8~~	451.3
280W	00	-2.5	~~465.6~~	451.1
	20s	-3.9	~~464.0~~	449.5
	40s	-5.1	~~462.8~~	448.3
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	80s	-6.2	~~461.7~~	447.2
	100s	-7.6	~~460.3~~	445.8
	120s	-8.0	~~459.9~~	445.4
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	280s	-7.2	~~460.7~~	446.2
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300W	420s	-5.7	~~462.2~~	447.7
	400s	-5.7	~~462.2~~	447.7
	380s	-5.7	~~462.2~~	447.7
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	340s	-5.9	~~462.0~~	447.5
	320s	-6.1	~~461.8~~	447.3
	300s	-6.1	~~461.8~~	447.3

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300W	280s	-6.6	~~461.3~~	446.8
	260s	-6.8	~~461.1~~	446.6
	240s	-7.1	~~460.8~~	446.3
	220s	-7.4	~~460.5~~	446.0
	200s	-9.0	~~458.9~~	444.4
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	120s	-8.4	~~459.5~~	445.0
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	80s	-7.2	~~460.7~~	446.2
	60s	-6.5	~~461.4~~	446.9
	40s	-5.3	~~462.6~~	448.1
	20s	-3.8	~~464.1~~	449.6
	00	-2.4	~~465.5~~	451.0
320W	00	-2.1	~~465.8~~	450.7
	20s	-3.8	~~464.1~~	449.6
	40s	-5.6	~~462.4~~	447.9

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	80s	-7.5	~~460.6~~	446.1
	100s	-8.0	~~459.9~~	445.4
	120s	-7.9	~~460.0~~	445.5
	140s	-8.8	~~459.1~~	444.6
	160s	-9.4	~~458.5~~	444.0
	180s	-9.3	~~458.6~~	444.1
	200s	-8.9	~~459.0~~	444.5
	220s	-6.8	~~461.1~~	446.6
	240s	-6.9	~~461.0~~	446.5
	260s	-6.1	~~461.8~~	447.3
	280s	-5.9	~~462.0~~	447.5
	300s	-4.7	~~463.2~~	448.7
	320s	-5.1	~~462.8~~	448.3
	340s	-5.5	~~462.4~~	448.1
	360s	-5.2	~~462.7~~	448.2
	380s	-5.7	~~462.2~~	447.7
	400s	-5.2	~~462.7~~	448.2
	420s	-5.6	~~462.3~~	447.8

		453.40 ~~467.93~~			
340W	420s		-5.1	~~462.8~~	448.3
	400s		-4.9	~~463.0~~	448.5
	380s		-4.7	~~463.2~~	448.7
	360s		-4.4	~~463.5~~	449.0
	340s		-4.5	~~463.4~~	448.9
	320s		-4.3	~~463.6~~	449.1
	300s		-5.6	~~462.3~~	447.8
	280s		-6.3	~~462.6~~	~~461.6~~ 447.1
	260s		-7.0	~~460.9~~	446.4
	240s		-7.6	~~460.3~~	445.8
	220s		-8.1	~~459.8~~	445.3
	200s		-9.4	~~458.5~~	444.0
	180s		-9.7	~~458.2~~	443.7
	160s		-9.7	~~458.2~~	443.7
	140s		-9.4	~~458.5~~	444.0
	120s		-8.8	~~459.1~~	444.6
	100s		-8.4	~~459.5~~	445.0
	80s		-7.3	~~460.6~~	446.1
	60s		-6.3	~~461.6~~	447.1

		453.40 ~~467.93~~			
340W	40s		-6.0	~~461.9~~	447.4
	20s		-4.6	~~463.3~~	448.8
	00		-3.2	~~464.7~~	450.2
360W	00		-3.4	~~464.5~~	450.0
	20s		-5.0	~~462.9~~	448.4
	40s		-6.0	~~461.9~~	447.4
	60s		-7.1	~~460.8~~	446.3
	80s		-7.7	~~460.2~~	445.7
	100s		-8.4	~~459.5~~	445.0
	120s		-9.1	~~458.8~~	444.3
	140s		-10.0	~~457.9~~	443.4
	160s		-10.1	~~457.8~~	443.3
	180s		-10.2	~~457.7~~	443.2
	200s		-9.5	~~458.4~~	443.9
	220s		-8.4	~~459.5~~	445.0
	240s		-7.5	~~460.4~~	445.9
	260s		-6.6	~~461.3~~	446.8
	280s		-6.4	~~461.5~~	447.0

		453.40 ~~467.93~~		
360W	300s	-5.6	~~467.3~~	447.8
	320s	-5.3	~~467.6~~	448.1
	340s	-4.7	~~463.2~~	448.7
	360s	-3.9	~~464.0~~	449.5
	380s	-3.8	~~464.1~~	449.6
	400s	-4.0	~~463.9~~	449.4
	420s	-4.1	~~463.8~~	449.3
380W	420s	-3.6	~~464.5~~	449.8
	400s	-3.4	~~464.5~~	450.0
	380s	-3.5	~~464.4~~	449.9
	360s	-4.0	~~463.9~~	449.4
	340s	-4.5	~~463.4~~	448.9
	320s	-4.8	~~463.1~~	448.6
	300s	-5.5	~~462.4~~	447.9
	280s	-6.9	~~461.0~~	446.5
	260s	-6.9	~~461.0~~	446.5
	240s	-8.5	~~459.4~~	444.9
	220s	-9.5	~~458.4~~	443.9

		453.40 ~~467.93~~		
380W	200s	-9.7	~~456.2~~	443.7
	180s	-11.0	~~456.9~~	442.4
	160s	-10.7	~~457.2~~	442.7
	140s	-10.6	~~457.3~~	442.8
	120s	-9.8	~~458.1~~	443.6
	100s	-9.0	~~458.9~~	444.4
	80s	-8.5	~~459.4~~	444.9
	60s	-7.0	~~460.9~~	446.4
	40s	-6.4	~~461.5~~	447.0
	20s	-5.4	~~462.5~~	448.0
	00	-4.2	~~463.7~~	449.2
400W	00	-4.7	~~463.2~~	448.7
	20s	-5.4	~~462.5~~	448.0
	40s	-6.5	~~461.4~~	446.9
	60s	-7.4	~~460.5~~	446.0
	80s	-8.7	~~459.2~~	444.7
	100s	-9.5	~~458.4~~	443.9
	120s	-10.3	~~457.6~~	443.1

			453.40 ~~467.93~~	
400W	140s	-11.4	~~456.5~~ 442.0	
	160s	-11.7	~~456.2~~ 441.7	
	180s	-11.9	~~456.0~~ 441.5	
	200s	-11.2	~~456.7~~ 442.2	
	220s	-10.0	~~457.9~~ 443.4	
	240s	-9.0	~~458.9~~ 444.4	
	260s	-8.7	~~459.2~~ 444.7	
	280s	-7.6	~~460.3~~ 445.8	
	300s	-6.8	~~461.1~~ 446.6	
	320s	-5.8	~~462.1~~ 447.6	
	340s	-5.0	462.9 448.4	
	360s	-3.8	~~464.1~~ 449.6	
	380s	-3.3	~~464.6~~ 450.1	
	400s	-3.4	~~464.5~~ 450.0	
	420s	-3.1	~~464.8~~ 450.3	
420W	420s	-4.3	~~463.6~~ 449.1	
	400s	-3.9	~~464.0~~ 449.5	
	380s	-3.7	~~464.2~~ 449.7	

			453.40 ~~467.93~~	
420W	360s	-4.1	~~463.8~~ 449.3	
	340s	-5.2	~~462.7~~ 448.2	
	320s	-5.8	~~462.1~~ 447.6	
	300s	-7.0	~~460.9~~ 446.4	
	280s	-7.8	~~460.1~~ 445.6	
	260s	-9.2	~~458.7~~ 444.2	
	240s	-9.6	~~458.3~~ 443.8	
	220s	-9.4	~~458.5~~ 444.0	
	200s	-10.9	~~457.0~~ 442.5	
	180s	-13.4	~~454.5~~ 440.0	
	160s	-12.6	~~455.3~~ 440.8	
	140s	-11.6	~~456.3~~ 441.8	
	120s	-10.9	~~457.0~~ 442.5	
	100s	-10.0	~~457.9~~ 443.4	
	80s	-9.3	~~458.6~~ 444.1	
	60s	-8.0	~~459.9~~ 445.4	
	40s	-6.7	~~461.2~~ 446.7	
	20s	-5.7	~~462.2~~ 447.7	
	00	-4.8	~~463.1~~ 448.6	

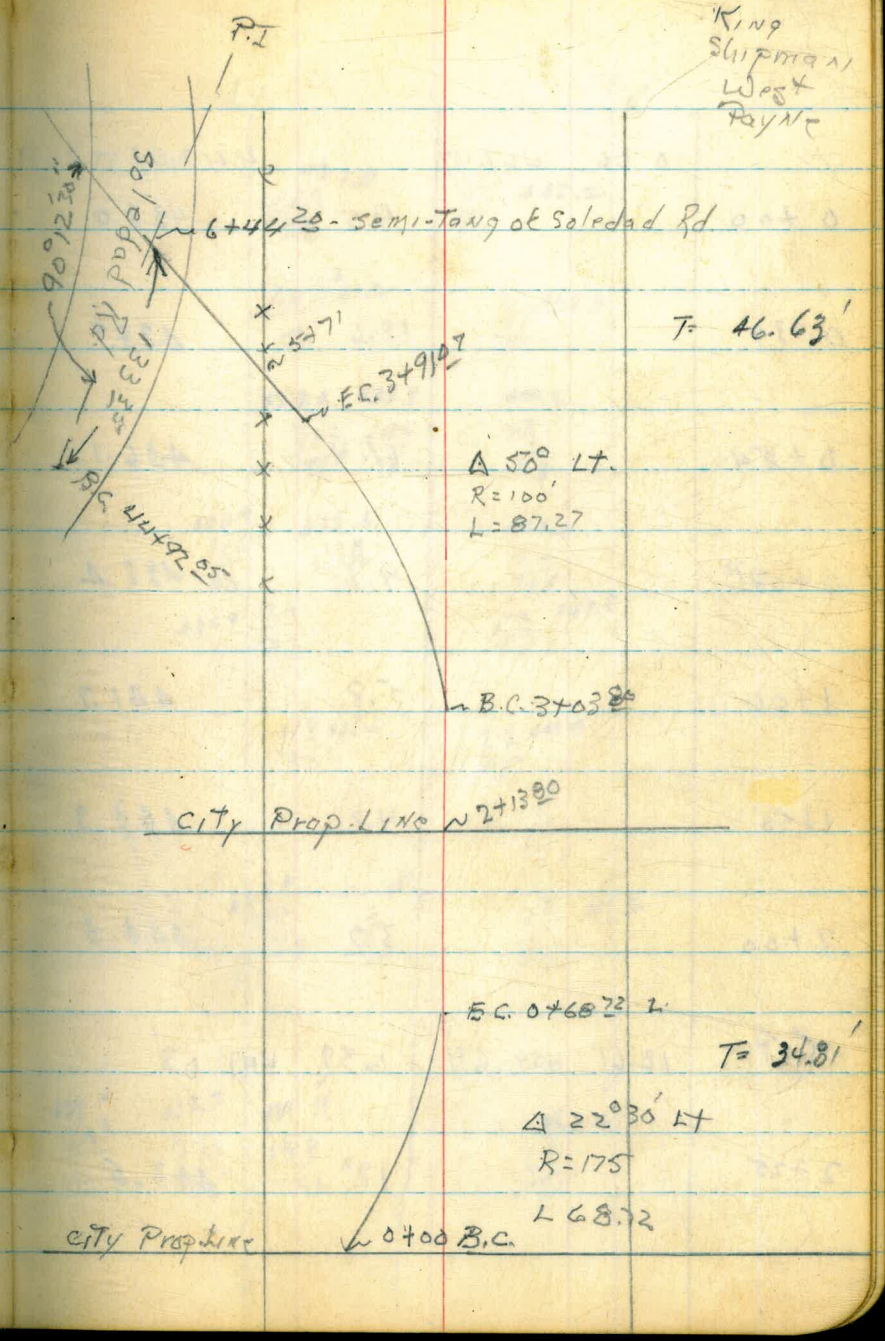
		453.40 ~~467.98~~		
430W	00	-5.55	~~468.38~~	447.85 ON HUB.
	20S	-6.3	~~461.6~~	447.1
	40S	-7.1	~~460.8~~	446.3
	60S	-8.3	~~459.6~~	445.1
	80S	-9.6	~~458.3~~	443.8
	100S	-10.2	~~457.7~~	443.2
	120S	-11.0	~~456.9~~	442.4
	140S	-11.9	~~456.0~~	441.5
	160S	-13.3	~~454.6~~	440.1
	180S	-13.8	~~454.1~~	439.6
	200S	-12.7	~~455.2~~	440.7
	220S	-10.5	~~457.4~~	442.9
	240S	-10.0	~~457.9~~	443.4
	260S	-8.4	~~459.5~~	445.0
	280S	-7.6	~~460.3~~	445.8
	300S	-7.2	~~460.7~~	446.2
	320S	-6.2	~~461.7~~	447.2
	340S	-5.2	~~462.7~~	448.2
	360S	-4.0	~~463.9~~	449.4

		453.40 ~~467.98~~		
430 W	380S		-5.8	~~464.1~~ ~~449.6~~
	400S		-4.1	~~463.8~~ ~~449.3~~
	420S		-4.3	~~463.6~~ 449.1
CHECK T.P.			-5.95	447.44 = 447.45 ~~461.98~~ = ~~461.99~~
CHECK B.M.	(LONG SHOT)		-9.50	443.90 ~~458.45~~ = 443.94 ~~458.49~~ RECORD.

corrected 5-11-49 by DML

Bay View Res. Access Road

5-23-49 17.



						Lt		Rt
	0.06	447.47		447.41	Page 7 - This Bk			
0+00			9.5	438.0		431.5 / 16.0 / 50	5.3 / 30' 442.2	
0+34			18.6	428.9		26.3 / 50' 421.2	8.6 / 32 438.9	
0+54			11.4	436.1		429.3 / 18.2 / 50' 432.9 / 14.6 / 13'	440.2 / 7.3 / 26	
0+68.72			9.1	438.4		430.9 / 16.6 / 50' 435.3 / 11.8 / 20'	441.1 / 6.4 / 25'	
						434.9 / 12.6 / 50'	5.0 / 25 442.5	
1+00			5.8	441.7				
						11.9 / 50' 435.6	2.6 / 25 444.9	
1+50			4.2	443.3		19'		
2+00			3.2	444.3		428.4 / 19' / 48' 440.9 / 6.6 / 20	0.3 / 25' 447.2	
T.P.	12.61	459.69	6.39	447.08				
2+25			17.2	442.5	439.4 / 20.3 / 50' 432.7 / 27.0 / 26'	439.9 / 19.8 / 12	453.6 / 6.1 / 25'	

		459.69		
2450			18.4	441.3
3+03.80 B.C			9.8	449.9
3+50			6.4	453.3
E.C. 3+91.07			2.2	457.5
4+00			1.6	458.1
T.P	12.71	471.60	0.80	458.89
4+50			9.4	462.2
5+00			2.9	468.7
T.P	12.03	481.41	2.22	469.38
5+50			4.1	477.3

443.2	Lt.	435.4		447.9	Rt.
16.3 / 50'		24.3 / 16'		11.8 / 25'	
		451.6		451.4	
		8.1 / 50'		8.3 / 25'	
		453.4		456.0	
		6.3 / 50'		3.7 / 50'	
		456.7		458.5	
		3.0 / 50'		1.2 / 50'	
		458.4		458.9	
		1.3 / 50'		0.8 / 50'	
		463.1		462.3	
		8.5 / 50'		9.3 / 50'	
		469.7		468.8	
		1.9 / 50'		2.8 / 50'	
		477.8		477.9	
		3.6 / 50'		3.5 / 50'	

481.41

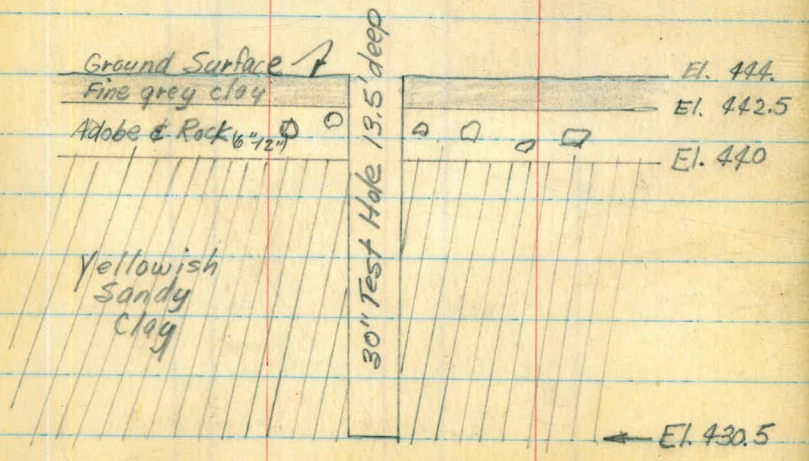
T.P. Fence 5+71	7.92	485.82	3.51	477.90
			6.2	479.6
6+00			4.3	481.5
END 6+44.20			3.9	481.9
T.P.	0.66	473.88	12.60	473.22
T.P.	0.55	461.58	12.85	461.03
T.P.	1.51	450.99	12.10	449.48
			7.12	443.87

443.94 conc mon

	LT	RT
	479.0	484.8
	6.8 / 50	1.0 / 50
	479.1	484.4
	6.7 / 50	1.4 / 50

Bayview Reservoir Soil Test Hole #1
(S 210, W 227)

Soil Sample No.	Elev.	Revised Sample No.	Description
1	443	BVR-1	Dry powdery clay (silt) (greyish)
2	440	BVR-2	Yellow sandy clay } mostly sand, some clay
3	437	BVR-3	" " " }
4	431.5	BVR-4	" " " }
5	442	BVR-5	Adobe with few rocks (black adobe)
Density #1	444	BVR-D1	Top soil dry powdery clay & adobe
#2	436.0	BVR-D2	Yellow sandy clay (mostly sand)



(over)

BAY VIEW RESERVOIR
SOIL TESTS

Clear-Warm 22.
8.15.49
RM

printer $7\frac{50}{}$ x6
MA 7^{50} x4
Cons & pers $\frac{\$}{5}$ hour

(= 12.69 #)

BVR-D1 used 12# 11 oz sand @ 100 #/cu ft

Sample weighs 13# 1.5½ oz

less can 1# 14 oz

net soil wt = 12# 1½ oz

= 12.09 #

(= 8.41 #)

BVR-D2 used 8# 6½ oz sand @ 100 #/cu ft

Sample weighs 11# 1½ oz

less can 1# 14 oz

net soil wt = 9# 3½ oz

= 9.22 #

BAY VIEW RESERVOIR
SOILS TESTS (CONT)

Vol of hole = $\frac{12.69}{100}$ = .1269 cu ft

Wt of soil = 12.09 #

Density of soil = $\frac{12.09}{.1269}$ = 95.3 #/cu ft

at field moisture

Vol of hole = $\frac{8.41}{100}$ = .0841

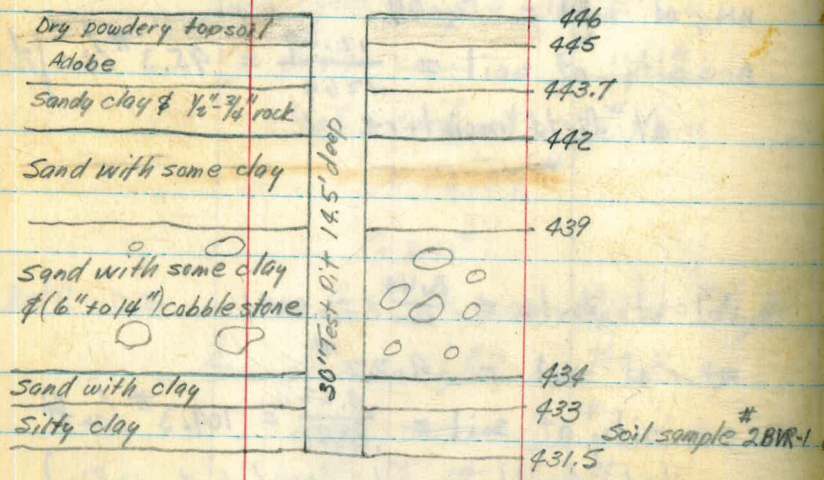
Wt of soil = 9.22 #

Density of soil = $\frac{9.22}{.0841}$ = 109.3 #/cu ft

at field moisture (about 12%)

BAY VIEW RESERVOIR
(Soil Tests cont.)

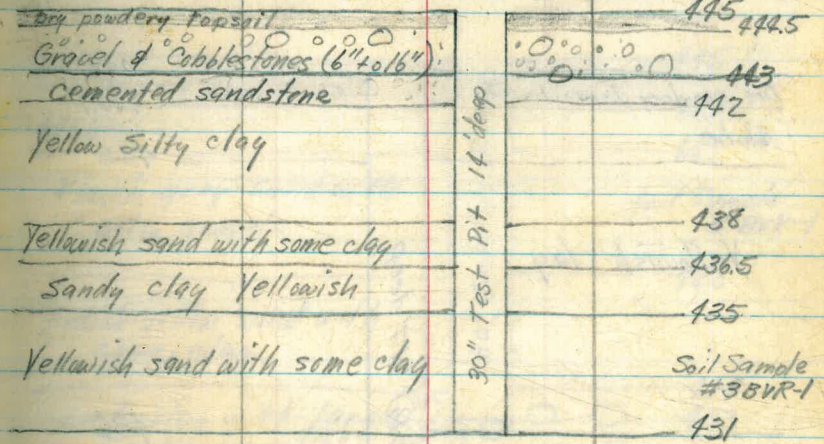
Test Pit # 2-BVR W104 S320 (SE corner)



Soil Sample # 2-BVR-1 silty clay yellowish

8.23.49
PM

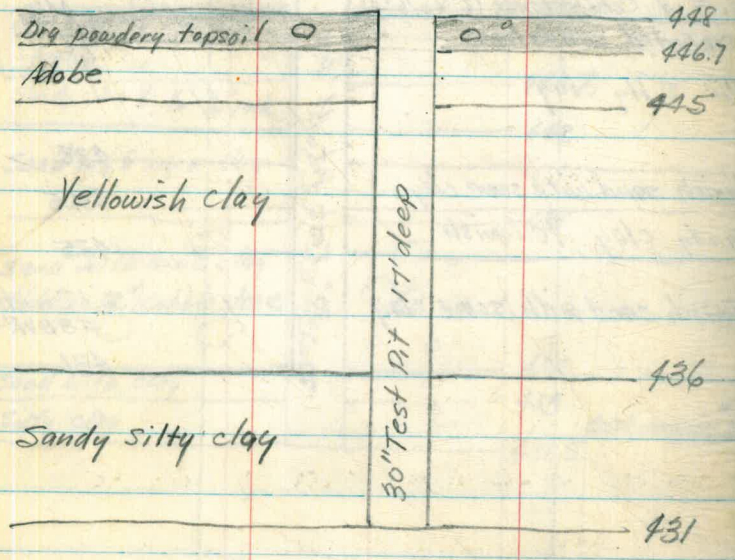
Test Pit # 3 BVR W113 S 130 (NE corner)



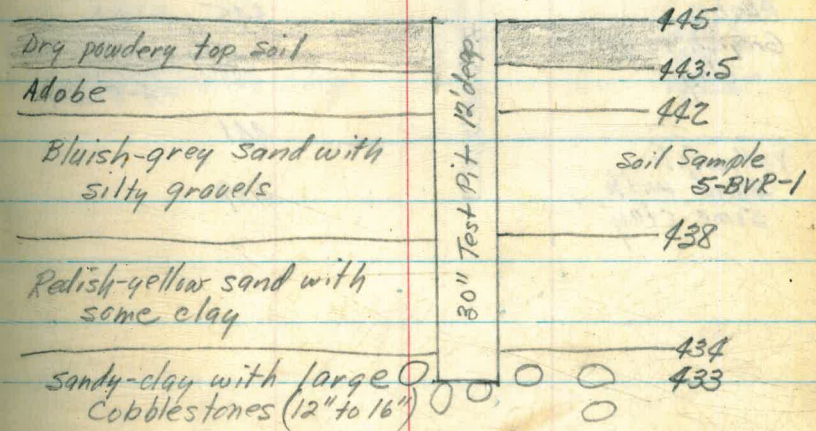
Soil Sample # 3-BVR-1 Yellowish sand - little clay

8.24.49
RM

Test Pit 4-BVR W315 S320 (SW corner)



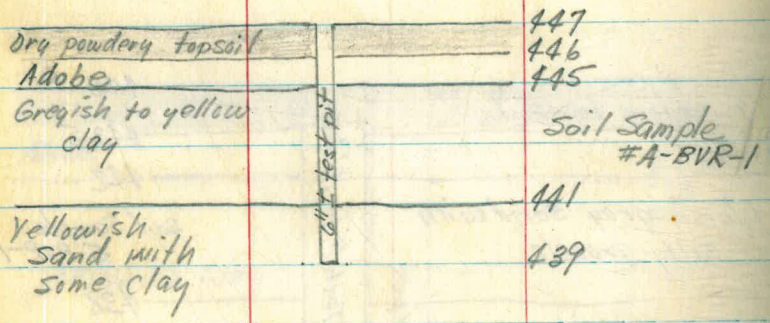
Test Pit 5-BVR W315 S107 (NW corner)



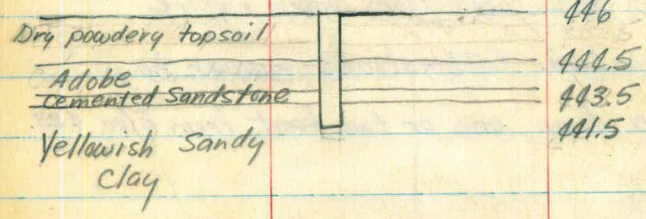
This test pit was abandoned at Elev. 433 because of several large cobblestones which require hand excavation. Cobblestones appear to extend on down one or two feet from Elev. 433.

Soil Sample 5-BVR-1 Bluish-grey sand with silty gravels

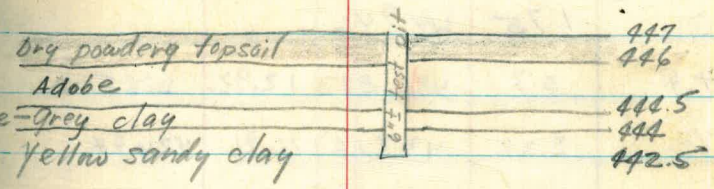
Test Pit A-BVR W210 S70 (North side)



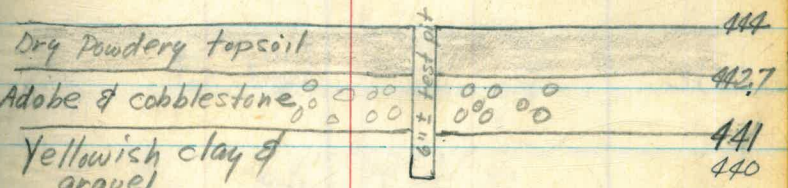
Test Pit B-BVR W70 S210 (East side)



Test Pit C-BVR W210 S350 (South Side)



Test Pit D-BVR W355 S215 (West Side)



X-Sects. Bay View Res.
see Sketch Next Page

B.M.	1.75	44946			447.71
T.P.	0.31	436.85	12.92	436.54	
T.P.	2.22	427.16	11.91	424.94	
T.P.	0.26	414.51	12.91	414.25	
T.P.	0.61	402.57	12.55	401.96	
T.B.M.			7.23	395.38	
0+00			7.2		
0+16			13.8		
0+32			14.3		
0+50			15.7		
0+73			22.1		
1+00			8.2		

Rainey King Shipman 9-12-49

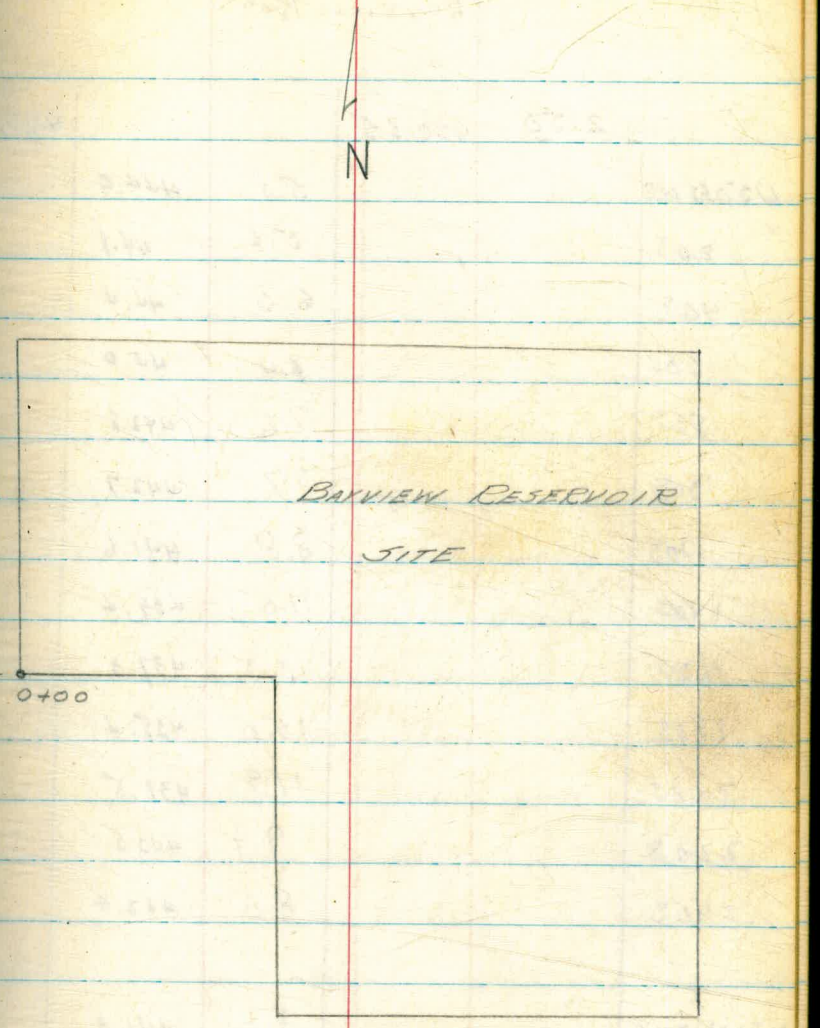
	Lt	Rt
El on Rock		
on Hub 0+00		
	0.00 / 20 6.1 / 8.5	10.5 / 8 11.5 / 15 11.5 / 21' 0.0 / 46'
	0.3 / 30' 3' / 21' 10.5 / 5'	14.4 / 4' 11.8 / 7' 4.0 / 22
	9.0 / 10.0 14.3 / 4'	12.7 / 4' 7.5 / 16'
	8.4 / 18 11.6 / 9.0	17.0 / 3 16.3 / 4.0 8.9 / 22
	10.3 / 20 16.6 / 8'	11.1 / 11.0 6.0 / 19'
	16.7 / 46 22.6 / 33 25.6 / 30 22.9 / 28 13.6 / 13	4.2 / 21

Additional x sections for Bayview Reservoir

			402.57		
T.P.	12.95	415.24 414.24	0.28	402.29	
T.P.	12.13	426.72 425.72	0.65	414.59 413.59	
T.P.	11.10	~~436.04~~	0.98	425.94 424.94	
	11.53	448.19	0.38	436.66 ~~435.66~~	
			0.52	447.67	447.21

Base line

0+00



Additional X-sects.
Bay View Res

9-26-49

King
Shipman
West

30

	2.50	450.35			447.85
450W 00S			5.5	444.9	
20S			5.6	44.8	
40S			6.0	44.4	
60S			6.4	44.0	
80S			7.6	442.8	
100S			7.7	442.7	
120S			8.8	441.6	
140S			11.0	439.4	
160S			13.1	437.3	
180S			15.0	435.4	
200S			11.9	438.5	
220S			9.9	440.5	
240S			8.0	442.4	
470W 240S			9.1	441.3	
220S			11.6	438.8	
200S			13½	436.2	
180S			19.1	431.3	

450.35

160S				20.2	430.2
140S				12.9	437.5
120S				10.9	439.5
100S				9.7	440.7
80S				9.2	441.2
60S				9.1	441.3
40S				8.6	441.8
20S				7.8	442.6
470W 00S				9.7	440.7
20N				14.4	436.0
40N				13.3	437.1
60N				9.3	441.1
80N				2.6	447.8
W450 80N				1.1	449.3
60N				3.7	446.7
40N				5.0	445.4
20N				6.6	443.8

		450.35		
		440.00		
W490	2.59	439.95	12.99	437.36
80S			9.1	430.9
20N			5.3	434.7
40N			+1.3	441.3
60N			+6.3	446.3
80N			+9.0	449.3
W490 20S			4.1	435.9
40S			1.2	431.8
60S			1.9	431.1
80S			2.3	437.7
100S			2.5	437.5
120S			3.7	436.3
140S			8.5	431.5
1465			15.7	424.3
160S			16.6	423.4
180S			9.4	430.6
200S			5.0	435.0
220S			1.8	438.2

439.95

W 510			
5220		5.0	435.0
5200		9.3	430.7
5180		17.6	422.4
5173		20.1	419.9
5160		16.5	423.5
5140		9.7	430.7
5120		6.7	433.7
S 100		5.8	434.2
S 80		5.5	434.5
S 60		6.4	433.6
S 40		9.2	430.8
S 20		14.7	425.3
S 00		6.8	433.2
N 20'		0.4	
	10.52 449.32	1.15	438.80
		1.47	437.85

Nov. 28 1949
Beatty
Rogers
Finney

BAYVIEW RESERVOIR

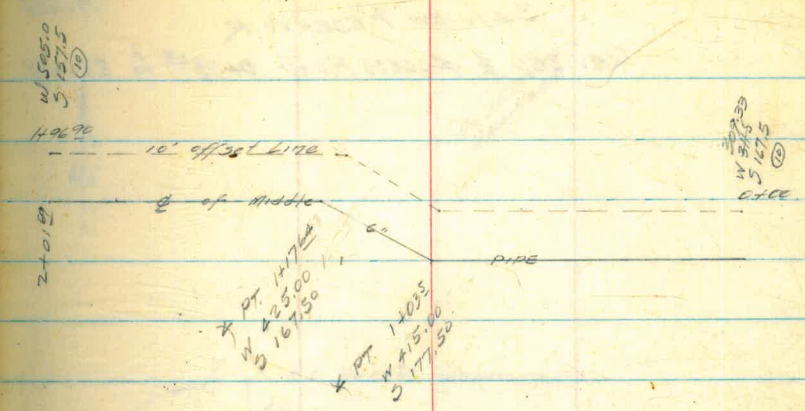
STAKES & GRADES FOR ℄ 5 - 6" Conc Drain Pipes

(0-25 HUB)

B.M		0.84	445.16	444.32		
0+00	Begin		0.7	444.5	427.00	C175
+50			1.6	443.6	426.25	C174
1+00	∡ PT 22°30' RT		4.1	441.1	425.50	C15[illegible]
+25	∡ PT. 22°30' LT.		4.9	440.3	425.12	C15[illegible]
+50			9.3	435.9	424.74	C11[illegible]
1+96.90	END		17.3	427.9	424.04	C3[illegible]
CK NE Cor Chamber			9.07	436.09 =	436.07	

RESTAKED JAN 30 1950

B.M		2.95	447.27	444.32		
0+00	52.17		W-~~31.5~~ 309.33 S-177.5 2.8 Begin 5-6" Conc Dr.	444.5	INV. GRD. 427.0	C175
0+50			3.7	443.6	426.1	C175
1+03.5			∡ PT. 45° RT 6.9	440.40	425.1	C15[illegible]
1+17.64			∡ PT. 45° LT 7.0	439.9	424.8	C15[illegible]
1+50			11.8	435.5	424.3	C11[illegible]
1+97.64			W505.00 S167.5 21.6 END 5-6" Conc Dr.	425.7	423.60	C2[illegible]



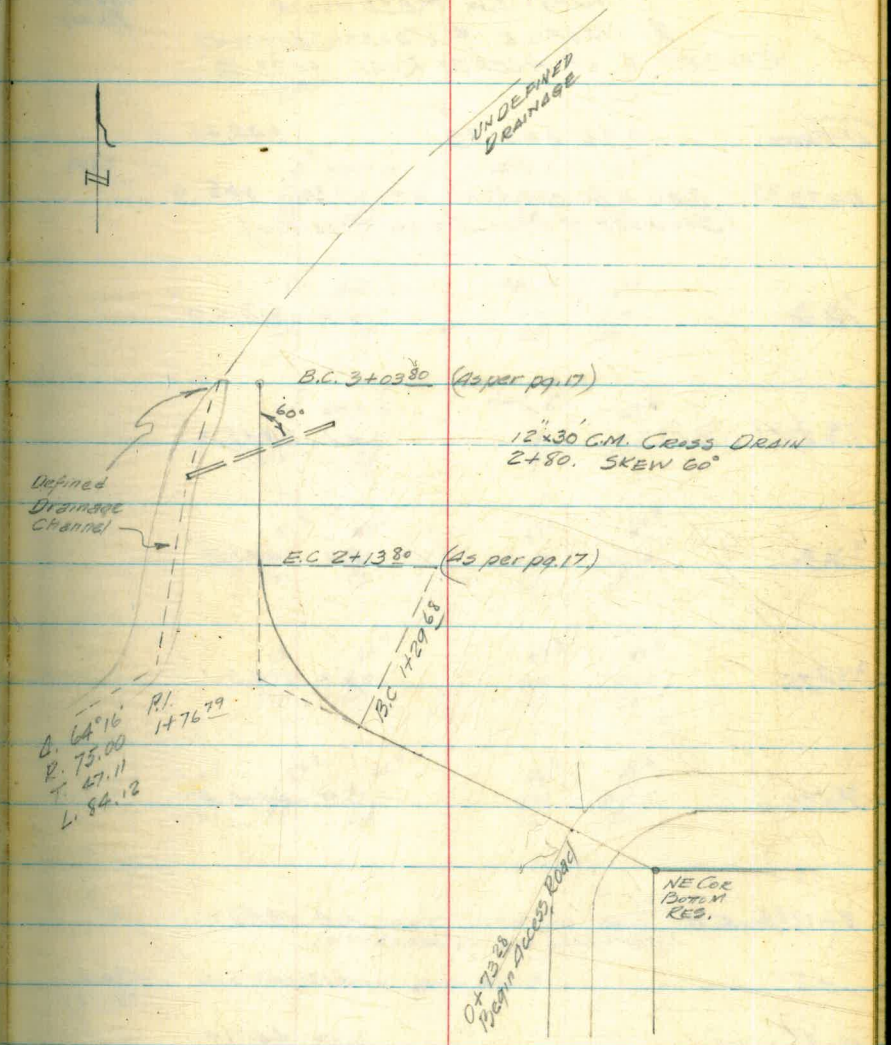
444.32 447.41
3.61 0.47
Si 447.93 447.88
8.94 3.61
SET BM 438.99 444.27

		INV. GRADE	2/16/50	8.92
		427.00		439.01
				12.65
				426.36 Bottom 20" pipe
		426.03		
℄ Elev				
8.4	438.9	.0186 425.04		
8.6	438.7	424.78		
14.1	433.2	.015 424.30		
22.2	425.1	423.59		

DEC. 27 1949
BEATTY
ROGERS
FINNEY

BAYVIEW RESERVOIR

REVISED R ACCESS ROAD 0+73.28 to 2+13.80



DEC 27, 1929
BEATTY
ROGERS
FINNEY

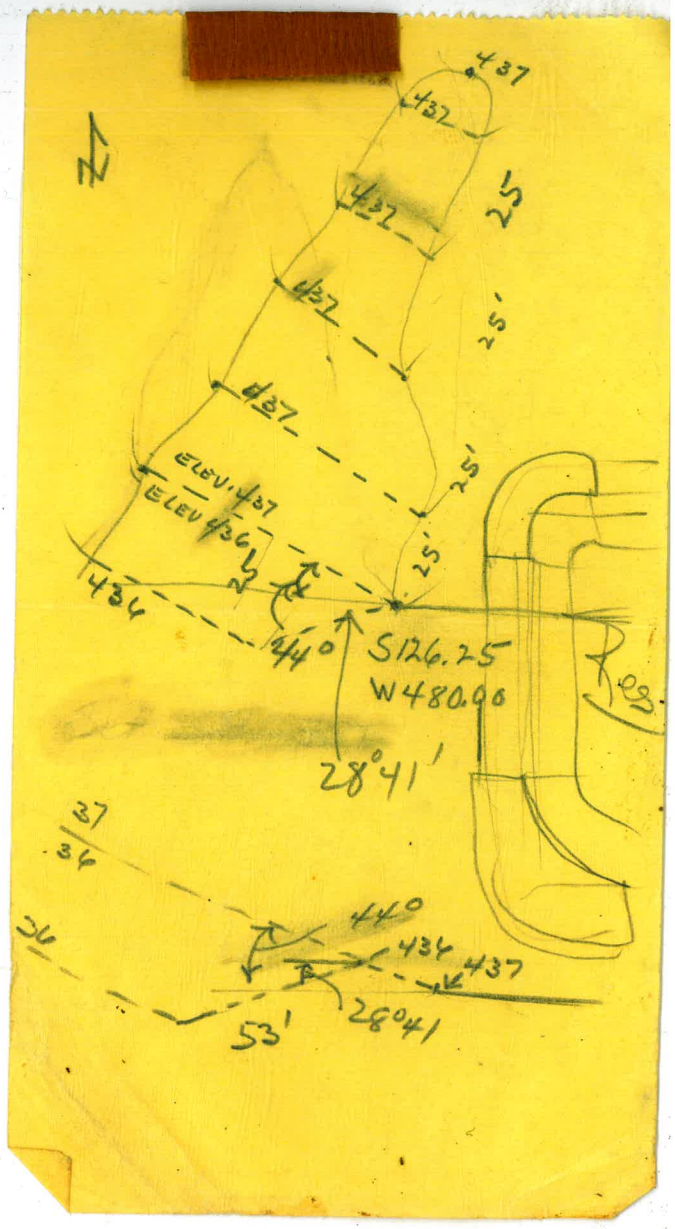
BAYVIEW RESERVOIR
℄ PROFILE & CROSS-SECTIONS
REVISED ℄ OF ACCESS ROAD 0+73 TO

℄P (ROCK)	0.92	448.33 ✓	447.41
0+73 2.3	BEGIN ACCESS ROAD AT (Shoulder of Road Around Reservoir)	3.3	445.0 ✓
1+00		3.6	444.7 ✓
1+29.68 (B.C)		3.1	445.2 ✓
+50		3.0	445.3 ✓
+75		3.2	445.1 ✓
2+00		3.9	444.4 ✓
2+13.80 E.C.		4.4	443.9 ✓
+25		5.7	442.6 ✓ = (442.5 pg 18)
CK ℄P		0.92	447.41

	Left		Right		
448.3	-42.9	444.3 ✓	446.2 ✓	47.0	
	5.4	4.0	2.1	1.3	
	50	25 ×	25	50	
	42.7	443.6 ✓	446.4 ✓	47.6	
	5.6	4.7	1.9	0.7	F 11.7
	50	25 ×	25	50	
	42.5 ✓	443.5 ✓	446.5 ✓	47.6	
	5.8	4.8	1.8	0.7	F 9.3
	50	25 ×	25	50	
	41.6	43.2	47.0	47.9	
	6.7	5.1	1.3	0.4	F 6.7
	50	25 ×	25	50	
	38.1	41.7	47.3	48.1	
	10.2	6.6	1.0	0.2	F 5.4
	50	25 ×	25	50	
	28.6	37.7 41.0	48.3	48.4	
	19.7	10.6 7.3	0.0	+0.1	F 3.2
	50	32 24 ×	32	50	

— X-SECT ON SAME LINE AS GRID 00 SOUTH (UNNECESSARY FOR QUANTITIES)

— FOR X-SECTION SEE pg. 18


N
437
437
437
437
437
437
25'
25'
25'
25'
ELEV. 437
ELEV 436
434
440
S126.25
W480.00
28°41'
37
34
440
434
437
36
53'
28°41

1/27/50 - Fair & Warmer
Rainey
Beatty
Rogers
Finney

Bayview Res.

Slope stakes for Access Road

447.41
4.18
Id. 451.59

1+00		444.7	456.2 S 456.4 ℄		F12.6 443.7 26.9	F11.7 — ℄	F10.0 446.2 23.0	In 443.7 OUT
1+29.7 (B.C.)		445.2	453.9 S 454.1 ℄		F10.0 443.9 23.0	F9.3 — ℄	F7.5 446.4 19.2	
1+50		445.3	451.8 S 452.0 ℄		F8.2 443.6 20.3	F6.7 — ℄	F5.5 446.3 16.2	
1+75		445.1	449.5 S 449.7 ℄	(RT.)	F3.2 446.3 12.8	F5.4 — ℄	F6.5 443.0 17.7	(LT.)
2+00		444.4	447.4 S 447.6 ℄		F4.7 442.7 15.0	F3.2 — ℄	F1.7 445.7 10.5	
2+13.8 E.C		443.9	447.1 S 447.3 ℄		F13.3 433.8 28.0	F3.2 — ℄	F1.6 445.5 10.4	
2+50		442.7	445.0 D 445.7 S 445.9 ℄	CMP. Cross Drain Restaked see pg.	F9.2 436.5 21.8	F3.2 — ℄	C1.5 446.5 10.8	(C0.8 2.8)
3+03.8 (B.C)		449.9	446.4 D 447.1 S 447.3 ℄	(F0.8 ② 440.7 Gr 439.9 EL) (C2.0 3.5)	18.40 C2.9 449.3 11.5	← 11.60 → C2.6 — ℄	Ditch Shldr. ② EL GR C4.3 450.7 12.2	(C3.4 4.2)
3+50		453.3	450.0 D 450.7 S 450.9 ℄	(C2.6 3.7)	C3.5 453.5 11.7	C2.4 — ℄	C3.8 453.8 11.9	(C2.9 3.9)

2+85.8 (C5.7) 449.4 443.7

Bayview Res

Slope Stakes for Access Road

4+00	458.1	456.3 D 457.2 E
+50	462.2	462.6 D 463.3 S 463.5 E
5+00	468.7	468.9 D 469.5 S 469.7 E
+50	477.3	475.1 D 475.8 S 476.0 E
6+00	481.5	480.2 D 480.9 S 481.1 E

1/27/50

38

(C1 0 / 2.9 Shld.)	C1 9 / 458.2 / 10.9 Ditch	Co 9 / – / C	C2 0 / 458.7 / 11.0 Ditch	(C1 1 / 3.0 Shldr.)
	F0 7 / 462.6 / 9.1	F1 3 / – / E	F0 9 / 462.4 / 9.3	
	F1 3 / 468.2 / 10.0	F1 0 / – / E	Co 2 / 469.1 / 10.1 Ditch	(F0 7 / 2.1 Shldr.)
(Co 6 / 2.8)	C1 5 / 476.6 / 10.8	C1 3 / – / E	C2 9 / 478.0 / 11.5	(C2 0 / 3.5)
(F0 1 / 2.4)	Co 8 / 481.0 / 10.4	Co 4 / – / C	C2 1 / 482.3 / 11.0	(C1 2 / 3.0)

Bayview Reservoir

Slope Stakes For Fill Slope to Road Around Reservoir

B.M.	8.07	452.39 ✓	444.32	(0-25 Bayview)	Slope Staked to 457.0
S 310	W 384.3	3.8	448.6 ✓	F 8.4 16.8	72.3
S 260	W 390.5	6.9	445.5 ✓	F 11.5 23.0	80.5
S 210	W 395.9	9.6	442.8	F 14.8 28.4	88.9
S 160	W 397.9	10.6	441.8	F 15.8 30.4	87.9
S 117	W 395.1	9.2	443.2	F 13.8 27.6	85.1
S 117	W 310. 30° RT	7.0	445.4	F 11.6 23.0	81.5
S 117	W 310 60° RT	5.5	446.9	F 10.1 20.2	77.7
S 41.7	W 310	4.3	448.1	F 8.9 17.8	69.2
S 42.3	W 264	4.0	448.4	F 8.6 17.8	74.7
S 41.7	W 214	4.3	448.1	F 8.9 17.8	75.3
S 37.5	W 164	6.4	446.0	F 11.0 22.0	79.5
S 32.7	W 114	8.8	443.6	F 13.4 26.8	84.3
S 117	W 114 30° RT	10.8	441.6	F 15.4 30.8	88.3
S 117	W 114 60° RT	10.3	442.1	F 14.9 29.8	87.3

	452.39				
S 117 W 29		9.1	443.3	F 13.7 27.4	84.9
S 160 W 32		7.5	444.9	F 12 24.2	81.7
S 210 W 33		7.1	445.3	F 11 23.4	80.9
S 260 W 35		6.1	446.3	F 10.7 21.2	78.9
S 310 W 36		5.2	447.2	F 9.8 19.6	77.1
S 310 W 114	30° RT	5.5	446.9	F 10 20.2	77.7
S 310 W 114	60° RT	5.4	447.0	F 8.2 20.0	79.5
S 388 W 114		5.8	446.6	F 10.4 20.8	78.3
S 387 W 164		5.4	447.0	F 10 20	77.8
S 386 W 214		4.9	447.5	F 9.5 19.0	76.5
S 383 W 264		3.2	449.2	F 7.8 15.6	73.1
S 386 W 310		4.8	447.6	F 9.4 18.8	76.3
S 310 - W 310	30° RT	3.0	449.4	F 7.6 15.2	72.7
S 310 - W 310	60° RT	3.4	449.0	F 8.0 16.0	73.5
SET BM		2.22	450.17 ✓		SW COR
CK BM.		8.07	442.32 ✓		

BENCH ELEVATIONS

BM.	8.57	456.05		447.48 (ROCK)	(BK. 772 pg. 44)
CK BM.			5.88	450.17 (SW PIPE)	
~~CK BM.~~	DESTROYED		~~0.90~~	~~455.15~~ (NOR PIPE)	
CK BM. (-0+25.55 (HUB)			11.71	~~444.34 = 444.37~~	(RAIN SWELLED) Hub ?
BM	3.61	447.95		444.34	
SET TBM			8.94	439.01	

NE COR VAL CHAMBER ✓

2/28/50

CHECK El. of 30" Inlet PIPE AS LAID

BM	0.52	448.43		447.91
TP	1.29	447.55	2.17	446.26
NOR END Top 30" Inlet pipe			12.73	434.82
" " Bott. " " "				431.61 = 431.65
30. " Top " " "			12.81	434.76
" " Bott. " " "				431.53 = 431.65

BAYVIEW RES.

INLET PIPE STAKED

B.M.		4.17	454.34		450.17	(SW. PIPE)
		INV. & GRADE = 432.00				
CK		BOTT. OF PIPE	431.65	GR. ROD	22.69	
CK	0+00 BEGIN PIPE	W 138.00 S 314.18	(=10' offset WEST)	8.10	446.24	C 14.6
CK	0+00	W 118.00 S 314.18	(=10' offset EAST)	8.50	445.84	C 14.2
B	0+26.32	W 138. S 340.5	(℄ CUT-OFF WALL)	8.20	446.14	C 14.5
SE						
	0+46.32	W 138. S 360.5	(℄ CUT-OFF WALL)	8.30	446.04	C 14.4
	0+66.32	W 138. S 380.5	(℄ CUT-OFF WALL)	7.54	446.80	C 15.15
B	0+80.27 END PIPE	W 138.00 S 394.45	(=10' offset WEST)	7.65	446.69	C 15.0
	0+80.27	W 118.00 S 394.45	(=10' offset EAST)	7.42	446.92	C 15.3
	CK BM			10.00	444.34	

1

FEB. 7 1950
BEATTY
PAYNE

2/7/50

42

FINE GRADE FOR INLET

P	4.16	448.50		444.34
P	0.65	436.20	12.95	435.55
	(REINF. STEEL PINS SET TO BOTTOM OF PIPE)			
0+00	(W 138.00 S 314.18)		4.55	
0+26.32	" S 340.5)		4.55	
0+46.32	" S 360.5)		4.55	
0+66.32	" S 380.5)		4.55	
0+80.27	W 138.00 S 394.45)		4.55	
P	12.52	448.34	0.38	435.82
OK P			4.00	444.34

2/27/50

FINE GRADE FOR OUTLET

B.M.	0.02	439.03		439.01
P	3.70	429.90	12.83	426.20
W 306.00			2.90	427.00
W 309.32			2.90	427.00
W 339.5			3.46	426.44
W 359.5			3.83	426.07
W 379.5	SLOPE		4.20	425.70
W 410.			4.76	425.14
W 415.00	K PT		4.85	425.05
P	9.50	439.06	0.34	429.56
OK BM			0.02	439.04

SPILLWAY DRAIN LINE STAKED

TBN		8.54	447.55		439.01	
0+00	(10' offset)	S 149.5 W 332.25		3.5	444.1	441.00 / 440.80 C33
0+20.25		S 149.5 W 352.5		4.0	443.6	440.20 C32
0+40.25		S 149.5 W 372.5		4.4	443.2	439.60 C31
0+74.25		S 149.5 W 406.5		6.0	441.6	438.50 C30
0+76.75				6.1	441.5	438.63 / 438.43 C30
CK TP				3.21	444.34	

MAR. 1 1950

FINE GRADE 6" OUTLET DRAINS

TP	W 210. S 177.5	5.06	430.20		425.14
TP	W 415.00 S 177.50	5.15	430.20		425.05
W 425.00 S 167.5				5.40	424.80
W 465. S 167.5				6.00	424.20
W 501.50 S 167.5				6.55	423.60
W 505. S 167.5				6.60	423.60
TP		10.67	440.34	0.53	429.67
CK BN.				1.31	439.03 = 439.01

FEB 15, 1950
BEATTY
ROGERS
DAYNE

on chamber

MAR 9 1950

END of 30" RCP OUTLET { Top W 309.57 / Bott W 309.51 } S 177.5

BN		0.11	439.12		439.01
W 421.00 S 177.5			Top	10.00	429.12
			Inv.		426.77
W 309.57 S 177.5			Top	7.84	431.28
			Inv.	10.69	428.43
			Bott	11.04	428.08 = 428.15

MAR 3 1950

FINE GRADE Bottom 30" RCP OUTLET

TP		6.17	430.97		424.80
W 305.33 S 177.50	(a) END 30" pipe			2.75	428.22 ✓
W 335.33				3.90	427.63 / 427.59 / 427.07 F.52
W 356.33				4.20	427.30 / 427.20 / 426.77 F.43
W 377.33				4.61	426.99 / 426.81 / 426.36 F.45
W 420				4.88	426.79 / 426.09
Inv. 24" pipe				4.40	426.57
TP		12.76 / 1.56	439.12	6.17	424.80
				0.13	438.99 = 439.01

SLOPE STAKES SET FOR
EXCAVATION of RESERVOIR
ALSO X-SECTIONS of STRIPPED AREA OF FILL SECTION

BM.	1.79	451.96		450.17	
SET BM	2.49	450.40	4.05	447.91	
	GR. ROD = 7.8		7.8	442.6	
W 91.2	S 335.8				
W 91.2	S 317.5				
W 91.2	S 247.5				
W 91.2	S 177.5				
W 91.2	S 109.5				
W 91.2	S 91.2				
CK BM	12.33	451.34	11.40	439.00	= 439.01
		GR. Rod	6.7	444.6	2/27/50
S 91.2	W 91.2 (45° NE)				
S 91.2	W 112.5				

FEB. 24, 1950

S 317.5
W 86.7

SW. PIPE

East PIPE

W 91.2

WEST. EAST.

	45.9	C32	45.8	46.1	46.8		
	4.5	4.6		4.3	3.6		
	3	4.8		45	50		
	45.5	C30	45.6	45.7	46.5	47.4	
	4.9	4.8		4.7	3.9	3.0	
	3	4.5		33	56	57	
	45.3	C28	45.4	45.3	45.5	46.4	
	5.1	5.0		5.1	4.9	4.0	
	7	4.2		39	54	55.	
46.2	45.8	C36	46.2	46.1	46.3	45.3	44.2	44.9
4.2	4.6	4.2		4.3	4.1	5.1	6.2	5.5
6	5	5.4		10	25	40	57	58
45.0		C21	44.7	43.5	43.4	42.9	43.4	
5.4		5.7		6.9	7.0	7.5	7.0	
4		3.1		24	40	59	60	
		C13		43.1	42.9	42.4	42.9	
		6.3		7.3	7.5	8.0	7.5	
		2.0		18	33	56	57	

NE COR
VAL CHAM.

SOUTH NORTH

44.1	40.8	41.5	
7.2	10.5	9.8	
	55	56	
45.1	C06	45.2	45.6	42.8	43.7
6.2	6.1		5.7	8.5	7.6
10	0.9		11.	55.	56.

FEB 27 1950

SLOPE STAKES & X-SECTIONS (CONT'D)

451.34

S 91.2 W 162.25

S 91.2 W 212.00

S 91.2 W 261.75

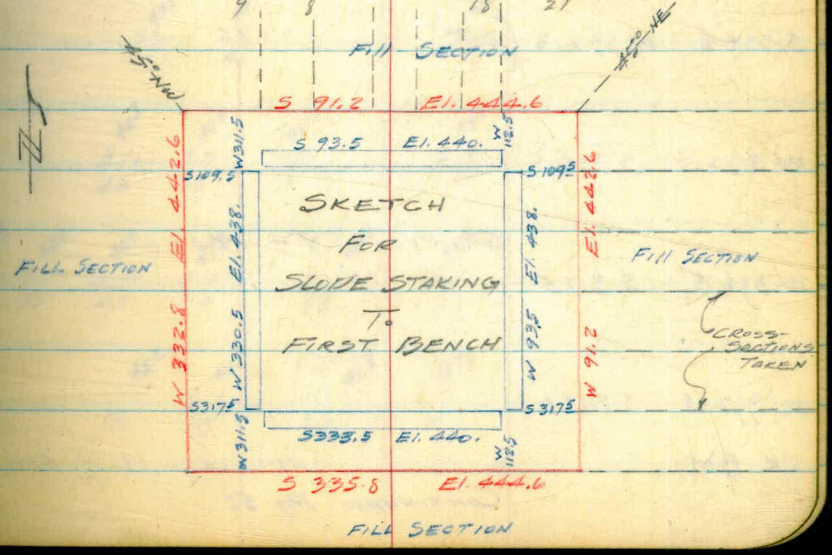
S 91.2 W 311.50

S 91.2 W 332.8

S 91.2 W 332.8 (NW 45°)

CK BM (EAST PIPE) 3.43 447.91 = 447.91

	46^{2} 5.1 10		C12 45^{8} 5.5 1.8	45^{7} 5.6 20	45^{4} 5.9 50	46^{2} 5.1 51		
	46^{3} 5.0 10	46^{7} 4.6 3	C13 45^{9} 5.4 1.9	46^{5} 4.8 29	47^{0} 4.3 30	47^{1} 4.2 48	48^{0} 3.3 4.9	
	46^{5} 4.8 10	46^{6} 4.7 4	C17 46^{3} 5.0 2.6	47^{7} 3.6 47	48^{4} 2.9 48			
			C08 45^{4} 5.9 1.2	46^{0} 5.3 15	45^{8} 5.5 18	46^{9} 4.4 37	47^{1} 4.2 47	48^{2} 3.1 48
	45^{5} 5.8	45^{3} 6.0	46^{4} 4.9 15	46^{0} 5.3 17	46^{7} 4.6 43	47^{1} 4.2 45		
	45^{5} 5.8 9	45^{2} 6.1 8	45^{5} 5.8 18	45^{9} 5.4 21	Begin Road Fill.			



Slope Stakes & Cross-Sections

BM	4.07	451.98		447.91							
		GR. Rod	7.4	444.6							
S 335.8	W 162.5								C1 2 45 8		
									6.2		
									1.8		
					47 6						
					4.4						
"					51						
					47 2	47 3	47 1	46 9	C1 7 46 3		45 9
"	W 212.5				4.8	4.7	4.9	5.1	5.7		6.
					50	31	28	18	2.6		10
"											
					47 4	48 7	47 7	47 5	C2 6 47 2		46 5
"	W 262.5				2.6	3.3	4.3	4.5	4.8		5.5
					49	48	30	15	3.9		10
					47 6	47 4	47 0	47 5	C2 9 47 5		47 3
"	W 311.5				4.4	4.6	50	4.5	4.5		4.7
					50	42	40	25	4.4		10
					48 1	48 1	48 2	48 0	48 3	48 2	48 3 48 6
S 335.8	W 332.8				3.9	3.9	3.8	4.0	3.7	3.8	3.7 3.4
					50	42	34	32	18	14	4 10
								49 8	49 2		48 2
S 335.8	W 332.8 (45°)							2.2	2.8		3.8
								41	40		10
								48 9	48 2	48 5	48 2
W 332.8	S 335.8							3.1	3.8	3.5	3.8
								44	43	10	10
		GR Rod	9.4	442.6							
					48 6	48 3	48 0	47 6	C5 6 48 2		48 6
W 332.8	S 317.5				3.4	3.7	4.0	4.4	3.8		3.4
					53	50	45	24	84		10
							45 0	45 9	C3 3 45 9		45 9
W 332.8	S 247.5						7.0	6.1	6.1		6.1
							50	25	5.0		10
CK BM			1.79	450.19 = 450.17							

CONTINUED Pg. 52

MAR. 9, 1950

FINE GRADE 15" SPILLWAY DRAIN

1. BM	9.97	448.98		439.01
S	W 330.25 S 159.50	(= ② Inlet)	8.09	440.89
0+00	W. 332.25 S 159.50	(Inlet)		440.83
0+18.25	W 350.5 S 159.5	(② cut-off wall)	8.70	440.28
0+38.25	W 370.5 S 159.5	(" " ")	9.30	439.68
0+72.25	W 404.5 S 159.5	(" " ")	10.32	438.66
0+76.75	W 409. S 159.5	(END Pipe)	10.45	438.53
CK			9.97	439.01

S

S

W

W

W

C

S 17
42.5
S- 59.5

W 310 = W- 310
56.5
253.5

439.12
9.77
429.35 TP
28
429.63 H.
23.60

452.25 BM.
1.05
453.30
9.59 TP
443.71
2.32
446.03 H.

310
205
515
409
106

Mar. 3 1950
Beatty
Rogers
Payne

℄ Profile of Access Road
As Excavated To Date, Mar. 3, 1950

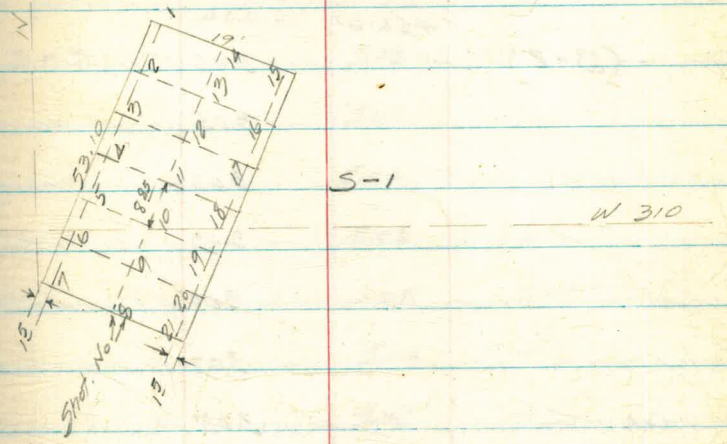
BM	10.74	449.75	439.01	NE Cor Val Chan
TP	6.92	453.82	2.85 446.90	
Set TBM			1.57 452.25	1½" I.D at Cor of Contractors Shop Bldg.
2+50			7.5 446.3	
+69			6.5 447.3	
+80			7.2 446.6	
3+00			5.7 448.1	
+25			4.7 449.1	
+50			3.0 450.8	
+70			0.0 453.8	
TP	12.34	465.83	0.33 453.49	
4+00			8.5 457.3	
+50			3.0 462.8	
TP	12.80	478.24	0.39 465.44	
5+00			8.8 469.4	
+50			2.0 476.2	
TP	4.69	482.61	0.32 477.92	
6+00			1.9 480.7	
+15			1.0 481.6	
+30			1.0 481.6	

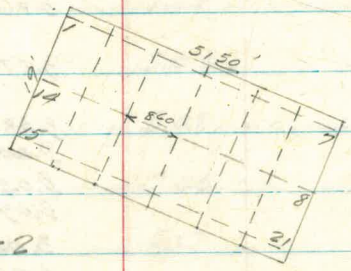
482.61

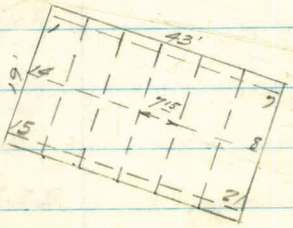
TP	0.24	469.76	13.09	469.52
TP	0.19	456.88	13.07	456.69
			12.92	443.94 = 443.94 pg. 21

Elevations of Concrete Floors For Pouring Precast Columns, Beams.

TBN	436	456.61	452.25
1.	(S-1)	1.93	
2.		1.92	
3.		1.94	
4.		1.92	
5.		1.93	
6		1.93	
7		1.93	
8		1.93	
9		1.92	
10		1.92	
11.		1.89	
12		1.92	
13		1.91	
14		1.92	
15		1.94	
16		1.91	
17		1.91	
18		1.90	
19		1.94	
20		1.93	
21.		1.92	







Elevations of Concrete Floors (Cont'd.)

456.61

1.	(S-2)	3.05
2		3.05
3		3.05
4		3.03
5		3.07
6		3.07
7	Cor	3.05
8		3.06
9		3.07
10		3.08
11		3.04
12		3.05
13		3.03
14		3.06
15.		3.05
16		3.02
17		3.05
18		3.05
19		3.09
20		3.07
21.		3.05

456.61

1	(S-3)	5.08
2		5.07
3		5.06
4		5.05
5		5.08
6		5.04
7		5.06
8		5.07
9		5.05
10		5.08
11		5.05
12		5.07
13		5.07
14		5.12
15		5.08
16		5.08
17		5.07
18		5.05
19.		5.07
20.		5.05
21.		5.06
CK BM		4.36 452.25 = 452.25

3/9/50

Access Road
Restaked 12" CMP Cross Drain

BM.	0.72	452.97	452.25	
2+40	70° Skew Rt.			
	Inlet ℄ 12.77 Rt =			443.3
	(4' offset)	6.4	446.6	C33
	Outlet ℄			437.3
4+16.0	(4' offset)	21.0	432.0	F53
0+00	= 12.77 Rt (Inlet)	7.2	445.8	
+03		7.6	445.4	
+06		7.1	445.9	
+19		7.1	445.9	
+23		7.8	445.2	
+40	= 27.23 Lt Outlet	19.0	434.0	

4/6/50 51

Profile of Trench Excavated for 12" CMP Cross Drain Previous to Grade Change of Access Road.

℄ @ Inlet	0.00	446.6	446.6
0+00 (= 4' offset Inlet)		0.0	446.6
+015		0.3	446.3
+03		3.8	442.8
+24		9.0	437.6
+41		11.2	435.4
0+48 (= 4' offset Outlet)		14.6	432.0

Note: Original Grade of 12 CMP Cross Drain shown on opposite page, raised 2° Ft. To Conform to revised grade of Access Road.

Mar. 30, 1950
Beatty
Rogers
Payne

SLOPE STAKES & X-SECTIONS (Cont'd from Pg. 46)

B.M.	5.22	457.47		452.25	pipe: Nor.	
		GR. ROD	14.9	442.60		
S 91^{2} W 332^{8}						C2^{7} 45^{3} 12.2 4^{1}
					(S 100. Edge of Road Slope as filled to date)	
S 109^{5} W 332^{8}					54^{0} 3.5 23	C2^{0} 44^{6} 12.9 3^{0} 54^{3} 3.2 3 53^{7} 3.8 30 53^{0} 4.5 65
TP	1.89	447.78	11.58	445.89		
		GR. ROD	5.2	442.60		
S 161^{5} W 332^{8}					43^{6} 4.2 23	C1^{0} 43^{6} 4.2 1^{5} 41^{4} 6.4 56 41^{3} 6.5 60
S 213^{5} W 332^{8}					44^{5} 3.3 23 45^{0} 2.8 13 44^{9} 2.9 C	C2^{1} 44^{7} 3.1 3^{2} 44^{7} 3.1 4 43^{2} 4.6 62 43^{6} 4.2 77
S 240 W 332^{8}					44^{8} 3.0 23 45^{0} 2.8 C	45^{5} 2.3 22 44^{7} 3.1 52 44^{0} 3.8 59 44^{2} 3.6 77
					(S 243 Edge of Road fill as filled to date)	
S 265^{5} W 332^{8}						C4^{1} 46^{7} 1.1 6^{2}
S 317^{5} W 332^{8}						C9^{5} 52^{1} +4.3 14^{3}
S 335^{8} W 332^{8}						C10^{2} +5.0 15^{3}
CK BM			8.77	439.01	on Val. Chamber	

3/30/50

BM	5.22	457.47		452.25	
		GR Rod	0.5	457.0	
S 117 W 367.5					
TP	1.89	447.78	11.58	445.89	
		GR. Rod	+9.2	457.00	
S 161.5 W 367.5					
S 213.5 W 367.5					
S 265.5 W 367.5					
S 310. W 367.5					
TP			8.77	439.01	

F14' 14.6 28Z

F15' 5.9 30Z

F13.8 4.6 27.6

F11.5 2.3 23.0

F8.4 +0.8 17.6

on val Chamber

4/6/50

Cross Sections Showing Excavation of Access Road Made previous to GRADE CHANGE of ACCESS Road

3+03.80 BC.

3+50

4+00

(0.0 Area of Excav. 2+75)

449.3	448.1	448.2	449.4	450.7	450.7
1.4	2.6	2.5	1.3	0.0	0.0
11.5	9	8	8	11	12.2

453.5	451.3	451.0	450.8	451.3	453.8	453.8
0.3	2.5	2.8	3.0	2.5	0.0	0.0
11.7	9	8	6	9	11	11.9

458.2	457.3	457.3		457.6	458.3
0.1	1.0	1.0		0.7	0.0
10.9	10	8		9	11

(0.0 Area of Excav. 4+30)

April 14 1950
Beatty
Rogers

Slope Stakes for Access Road
Revised To Grade Change

BM	1.57	453.82	452.25					
0+83^{2}				℄ Grd 456.2	Shldr Grd. 456.0	Gr Rod		
1+00				455.0	454.8	1.0	F5^{6} 6.6 16.4	
1+48				451.4	451.2	2.6	Co^{0} 3.6 10	
1+66^{2}	∡ PT.			451.2	451.0	2.8	(F4^{0} 6.8 14.0) (F0^{6} 3.4 8.9)	
1+87^{3}				451.2	451.0	2.8	F11^{6} 14.4 25.4	
2+00				450.2	450.0	3.8	F10^{0} 13.8 23.0	
2+50				448.0	447.8	6.0	F10^{4} 16.4 23.6	F0^{9} 6.9 9.2
3+03				450.3	450.1	3.7	F1^{2} 4.9 9.8	Co^{5} 5.2 10^{3}
3+50				454.1	453.9	+0.1	Co^{3} 0.6 10^{1}	Co^{2} 0.7 10.1
4+00				458.1	457.9	+3.3	C1^{6} +4.9 10.8	C2^{0} +5.3 11.0

Cuts Set for Columns Row W 327.50
Elev. To Top of Footings

BM.		5.29	457.54	452.25	
W 327.5	S 96.5		5.22	452.32	449.38
"	S 114.5		11.73	445.81	443.07
(1)	263	448.10	12.07	445.47	
"	S 132.5		3.94	446.16	"
"	S 150.5		4.22	443.88	"
"	S 168.5		4.82	443.28	"
"	S 186.5		4.53	443.57	"
"	S 204.5		4.78	443.32	"
"	S 222.5		~~4.42~~	443.38 / ~~443.68~~	"
"	S 240.5		4.77	443.33	"
"	S 258.5		4.63	443.47	"
"	S 276.5		4.69	443.41	"
"	S 294.5		4.17	444.37	"
"	S 312.5		3.65	444.46	"
(1)	11.16	457.36	1.90	446.20	
"	S 330.5		8.47	448.89	449.36

C294

C274

460 25
449.38
10.87

~~C269~~ Rev C279

C081

96.5
73.0
23.5

445.03
789
452.92

C021

C050

954
338

C025

~~C061~~ C032 Replaced 5/15/50

9.27
442.65

C026 C004

C040

C034

C086

C138

C049

MAY 15, 1950

CUTS FOR GUTTER – ℄ 177.50

B.M.	5.43	457.68		452.25		
TP	1.08	446.11	12.65	445.03		
TP	0.81	436.10	10.82	435.29		
TBM			4.81	431.29		Top 30" RCP OUTLET
W 115	S 171.5	= 6	3.5	432.6	430.17	c 2.4
W 149	"	= 6	5.6	430.5	430.00	c 0.5
W 200	"	= 6	5.3	430.8	429.75	c 1.0
W 250	"	= 6	5.0	431.1	429.50	c 1.6
W 300	"	= 6	4.4	431.7	429.25	c 2.4
W 309	S 171.5	= 6	2.4	433.7	428.20	c 5.5

Cuts Set For Columns - Row S 96.50

Elev To Top of Footing

TP		0.98	446.01	445.03	
W 327.5	S 96.5	—	—	449.38	
W 306.5		0.90		445.05	C_{0}^{96}
W 285.5		0.64		"	C_{0}^{32}
W 264.5	(0.96)	0.61		"	C_{0}^{35}
W 243.5		0.35	4	"	C_{0}^{61}
W 222.5		0.55		"	C_{0}^{42}
W 201.5		0.55		"	C_{0}^{44}
W 180.5		0.26		"	C_{0}^{70}
W 159.5		0.23		"	C_{0}^{73}
	(453.57)				
W 138.5		7.48	446.09	"	C_{1}^{06}
W 117.5		6.17	447.40	445.05	C_{2}^{35}
W 96.5		0.45	453.12	449.38	C_{3}^{74}

Cuts For Columns Row W 96.5

	446.01			
	(453.57)			
S 96.5		3.21	450.36	449.38	C_{0}^{98}
	446.01			
S 114.5		1.33	443.01		C_{1}^{61}
S 132.5		2.40	"		C_{0}^{54}
S 150.5	(2.94)	2.41	"		C_{0}^{53}
S 168.5		2.24	"		C_{0}^{70}
S 186.5		2.17	"		C_{0}^{77}
S 204.5		1.95	"		C_{0}^{99}
S 222.5		2.42	"		C_{0}^{52}
S 240.5		2.26	"		C_{0}^{68}
S 258.5		2.28	"		C_{0}^{66}
S 276.5		2.72	"		C_{0}^{22}
S 294.5		2.66	"		C_{0}^{28}
S 312.5		0.71	"		C_{2}^{23}
TP	8.27	453.57	0.71	445.30	
S 330.5			1.94	449.63	449.38	C_{2}^{25}

CUTS FOR COLUMNS - ROW S 330.5

Elev To Top Footing.

(4)		7.89	452.92		445.03	
W 327.5	S 330.5		1.34	451.58	449.38	C_{220}
W 306.5	"		6.83	446.09	445.05	C_{104}
W 285.5	"		7.31	"		C_{056}
W 264.5	"		6.98	"		C_{089}
W 243.5	"	7.87	7.40	"		C_{047}
W 222.5	"		7.74	"		C_{013}
W 201.5	"		7.29	"		C_{058}
W 180.5	"		7.58	"		C_{029}
W 159.5	"		8.20	"		F_{033}
W 138.5	"		8.53	"		F_{066}
W 117.5	"		7.69	"		C_{018}
W 96.5	"		4.55	448.37	449.38	F_{101}
			1.79	451.63		C_{235}

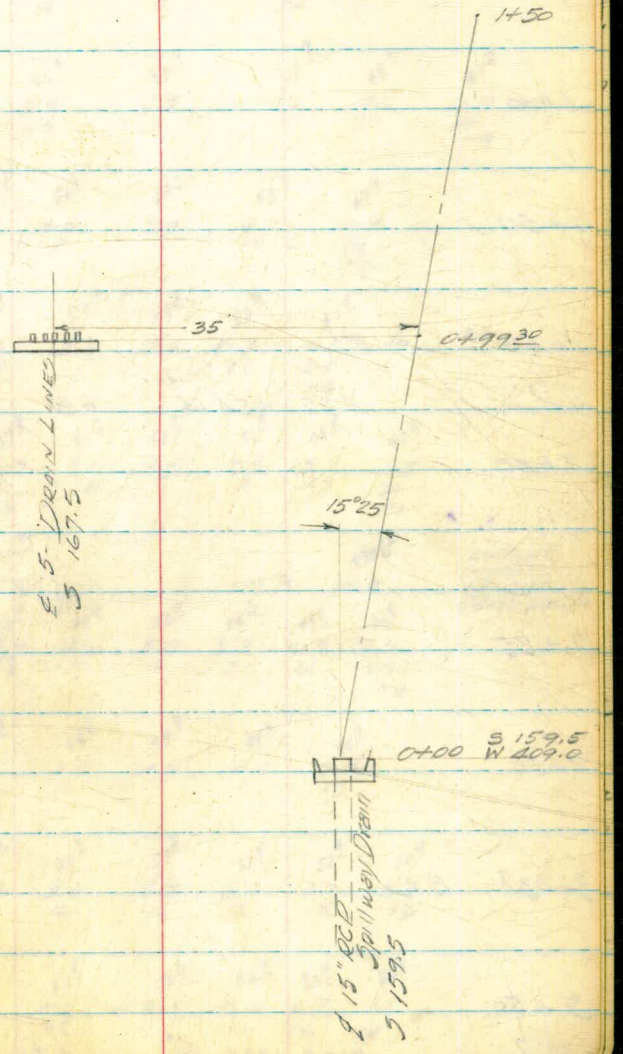
9.85 3.54 7.55 0.93 5.9 2.95

May 29 1950
Beatty
Carver

℄ Profile, Extension of 15" Spillway Drain

B.M.	2.92	441.93	439.01 NE Cor Val Cham.
0+00	Invert 15" RCP	3.22	438.71
+02		3.1	438.8
+04		0.8	441.1
+17		1.3	440.6
+35		1.1	440.8
+50		1.9	440.0
+65		2.6	439.3
+82		4.0	437.9
+82		3.5	438.4
+93		8.5	433.4
1+00		9.4	432.5
+15		9.9	432.0
+34		12.4	429.5
1+50		15.0	426.9

Reduced 10/31/50 RM



JUNE 2 1950

CROSS-SECTIONS OF ACCESS ROAD AS CONSTRUCTED

BM 5.95 458.20 452.25

0+63.18

1+00

1+50

1+66.63 ℄ PT.

PT 2.35 454.14 6.41 451.79

2+00

2+25

2+50

3+03.8 B.C.

3+50

PT 12.28 466.12 0.30 453.84

56.3 / 1.9 / 12

56.9 / 1.3 / C

56.8 / 1.4 / 24

39.7 / 18.5 / 87 / NG.

45.5 / 12.7 / 36

49.8 / 5.4 / 33

55.4 / 2.8 / 12

55.9 / 2.3 / C

55.7 / 2.5 / 10

48.4 / 10.0 / 29

47.3 / 10.9 / 40 / NG

37.1 / 21.1 / 97

40.6 / 17.6 / 62

46.3 / 12.0 / 33

52.6 / 5.6 / 20

53.0 / 5.2 / 6

54.2 / 4.0 / 3

54.3 / 3.9 / C

53.5 / 4.7 / 16

47.8 / 10.4 / 32 / NG

Section Taken on Split of ℄

39.4 / 18.8 / 39 / NG

53.0 / 5.2 / 7

53.0 / 5.2

53.3 / 4.9 / 22

47.7 / 10.5 / 35 / NG

37.8 / 16.3 / 31 / NG

51.0 / 3.1 / 10

51.7 / 3.4 / C

51.8 / 2.3 / 9

48.4 / 5.7 / 17

47.6 / 6.5 / 26 / NG

Inlet Invert 12" CMP Cross Dr. 444.92 / 8.2

439.24 / 14.9

OUTLET INVERT 12" CMP CROSS DRAIN

38.5 / 15.6 / 28

49.9 / 4.2 / 11

50.5 / 3.6 / C

50.3 / 3.8 / 7.

47.8 / 6.3 / 14

46.9 / 7.2 / 22 / NG

41.3 / 12.8 / 23

49.6 / 4.5 / 10

49.7 / 4.4 / C

49.2 / 4.9 / 6.

46.7 / 7.4 / 13

49.6 / 4.5 / 25

49.2 / 4.9 / 14

50.2 / 3.4 / 10.

51.3 / 2.8 / C

51.5 / 2.6 / 7

50.4 / 3.7 / 12

50.8 / 3.3 / 13

53.5 / 0.6 / 18

54.2 / +0.1

53.9 / 0.2 / 10

53.4 / 0.7 / 12

54.0 / 0.1 / 14

X-Sections of Access Road (Cont'd)

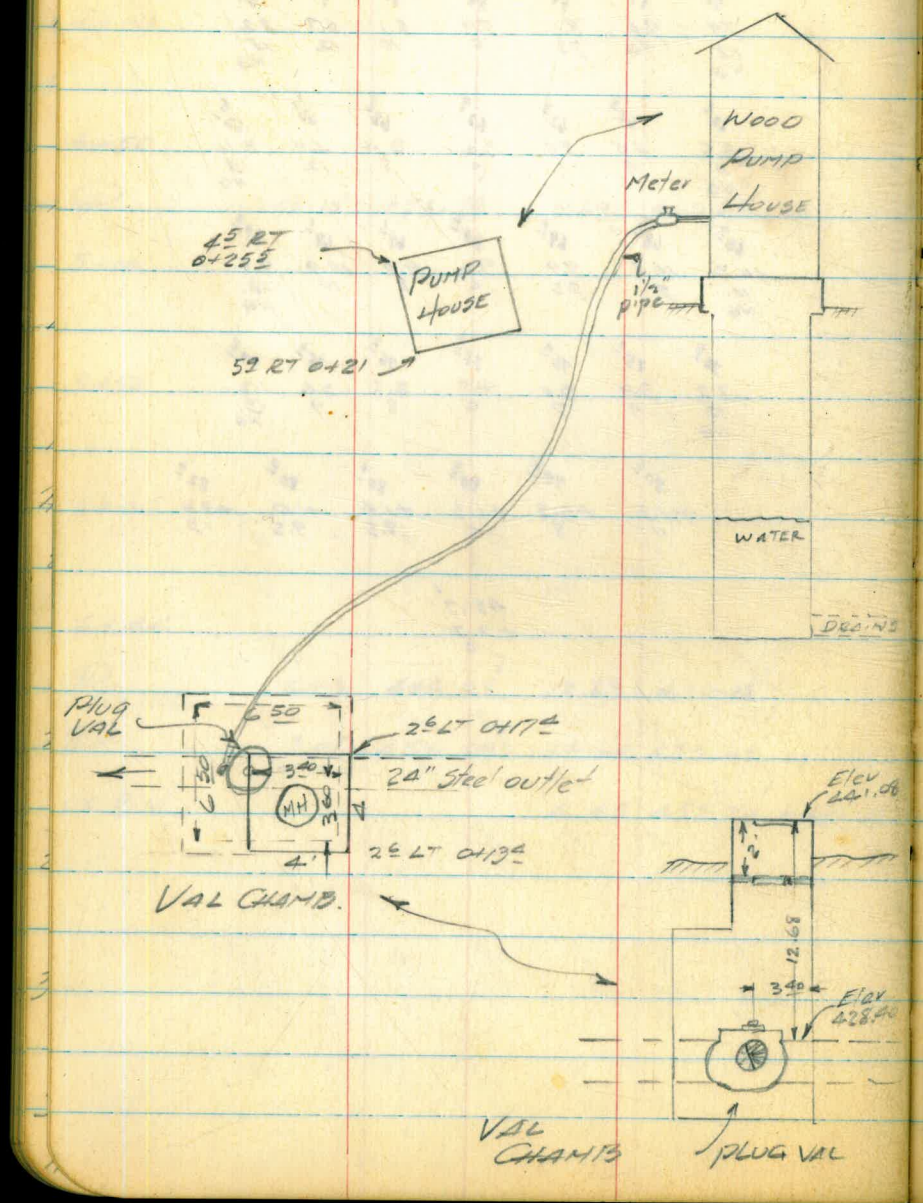
466.12

4+00				
4+50				
H	13.15	478.98	0.29	465.83
5+00				
5+50				
6+00				
6+44				
H	0.13	466.28	12.83	466.15
H	3.01	456.69	12.60	453.68
CK B.M.			4.45	452.24 = 452.25

58+	57+	58+	58+	58+	57+	57+
7.9	9.0	8.1	7.9	8.1	8.7	8.2
12	9.6	7.5	C	10	12	15
NG						NG
62+	61+	62+	62+	62+	62+	62+
3.5	4.5	3.5	3.2	3.4	4.0	3.6
11	9	6	C	8	12	15
NG						NG
68+	68+	69+	69+	69+	68+	69+
10.3	10.8	9.9	9.6	9.9	10.9	9.8
10.	9	7.5	C	8	10	18.
NG						NG
76+	75+	76+	76+	76+	75+	77+
2.2	3.9	3.0	2.7	2.8	3.4	1.2
12	9	7	C	8	9	13.
NG						NG
	80+	79+	80+	80+	80+	82+
	+1.5	+0.8	+1.3	+1.4	+1.0	+3.0
	11	8	C	8.5	9.5	13.

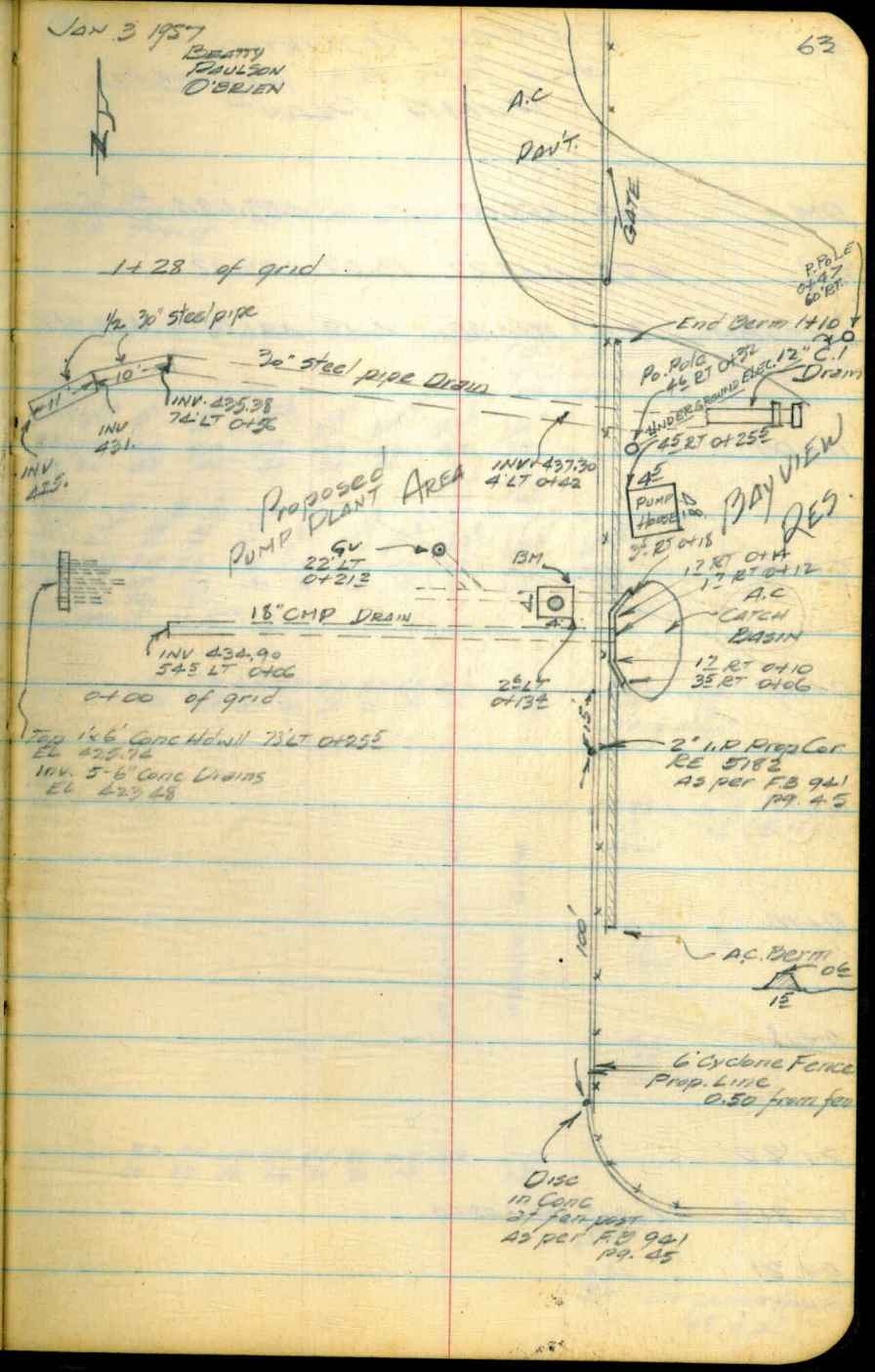
481.7
+2.7
C

Bayview Reservoir
Proposed Site For Pump Plant



Jan 3 1957

Beatty Paulson O'Brien



Bayview Reservoir
Grd Topo for Proposed Pump Plant

1/3/57

64

BM	1.07	458.09	457.024	City Datum
TP	0.25	445.27	13.07	445.02
Set TBM	3.47	441.55	4.19	441.08 = 439.01

NW Cor Res. on Buttress Block
F.B. 799-15

NE Cor Valve chamber

Note: This does not check TBM shown 439.41. But Top of Chamber has been raised 2' ft.

0+00

431.1
135
80

436.6 437.6 438.0 438.2 438.8 439.7 440.3 440.9 440.9
8.0 7.0 6.6 6.4 5.8 4.9 4.3 3.7 3.7
70 60 50 40 30 20 10 ℄ 0.5
Prop. line Bdry Fen

0+06

11.80
60

433.75 434.00 436.75 438.2 438.8 439.8 439.9 440.5 440.6 440.57
10.80 10.55 8.15 7.80 6.4 5.8 5.0 4.7 4.1 4.0 3.98
56.5 56.5 54.5 50 40 30 20 10 ℄ 0.5 3.5
Conc Apron Conc Apron Top 18" CMP Top 18" CMP Cor. Hdwl

0+10

9.0 7.3 6.5 6.3 5.8 5.3 4.8 4.4 4.2 3.98 6.0
60 58 50 40 30 20 10 ℄ 0.5 19 17
Face Hdwl

0+12

3.98 6.10
17 17 (℄ 18" CMP)
Hdwl

Property Line

Fence Line

0+14

4.00 6.10
17 17
Hdwl

0+18

4.00
35
Cor Hdwll

0+20

9.9 7.9 6.2 5.4 5.5 5.6 4.8 4.7 4.5
60 57 50 40 30 20 10 ℄ 0.5

0+21.5 22' out, G.V. Casing

441.23
3.32
5.9 Cor pump house
45 x 48

0+21

A1

Bayview Res
Cont'd

444.55

0+25.5

423.48 21.13 73 Inv. 6" Conc Drain

425.74 18.81 73 Top 1'x6' Hdwll

3.32
4.5 Cor pumphouse

0+30 10.6 6.9 6.0 4.8 4.9 4.9 4.6 4.2
60 55 50 40 30 20 10 c

0+32 4.6 Ely to Po. Pole

0+40 8.0 5.4 5.2 4.6 4.3 4.2 4.1 3.3 3.1
60 56 50 40 30 20 10 c 0.5

439.80

0+42 3.75 4.75
5 4 c
Top 30" Steel pipe Drain

0+45 c

2.62 0.44
21 32
Top 12" C.I. Drain

0+50 435.38 10.0 6.6 5.0 4.6 4.2 3.6 3.3 3.1 2.5 2.4
70 60 56 50 40 30 20 10 c 0.5

0+56 9.17 74 Inv. 30" Steel Drain

0+60 6.6 5.1 4.9 4.0 3.3 2.8 2.6 2.0 1.4 1.2
70 68 60 50 40 30 20 10 c 0.5

0+70 9.0 4.7 4.7 3.7 3.1 2.6 2.2 1.5 0.0 +0.2
80 70 60 50 40 30 20 10 c 0.5

446.1

0+80 9.3 7.9 5.9 4.8 3.8 2.8 2.3 1.3 +0.2 +0.7 +1.5
90 80 70 60 50 40 30 20 15 10 c

447.6

0+90 10.2 7.8 6.4 6.1 5.7 5.2 4.4 3.6 2.5 1.5 0.0 +2.3 +2.5 +3.0
120 110 100 90 80 70 60 50 40 30 20 14 10 c

449.4

1+00 10.8 9.2 7.9 6.6 6.0 5.6 5.0 4.4 3.6 2.4 0.8 +1.2 +4.4 +4.2 +4.8
125 120 110 100 90 80 70 60 50 40 30 20 14 10 c

Bayview Res
Cont'd.

444.55

1+10

150 82 72 66 62 56 53 46 37 13 00 +30 +56 +62 +65 (451.1)
125 118 110 100 90 80 70 60 50 40 30 20 16 10 C

1+20

140 75 66 63 61 58 49 20 +0.5 +70 +75 +77 +10.2 (454.8)
120 110 100 90 80 70 60 50 40 22 10 5 C AC

1+28 So. Gate Post

134 68 67 67 65 59 40 0.3 +7.7 +8.0 +8.8 +9.8 +10.1 (454.7)
120 110 100 90 80 70 60 50 26 20 10 75 C
AC AC

P 0.82 432.11 13.26 431.29

P 12.23 437.97 6.37 425.74

P 8.78 445.23 1.52 436.45

CK TBM 4.15 441.08

- 12.68

Top 24" outlet pipe in Val Chamber 428.40

NW Cor Howl 5-6" Conc Drains

432.11
8.63
423.48

NE Cor Val Chamber

10.0
11.0

BAYVIEW RESERVOR
GRID TOPO FOR PROPOSED PUMP HOUSE (CONT'D)

RT

TBM 12.76 453.84 441.08 N.E. COR. VAL. CHAMB. PG. 64

NOTE: SEE PG. 63-66 FOR DETAIL & OTHER SECTIONS - THESE SECTIONS ARE CONT'D FROM PG. 64-66

0+00			12.9 C	12.9 0.5	12.5 2.5 A.C. BERM	13.1 4 GUTTER	12.4 10	11.9 20	11.0 30	9.6 35.5 TOE SLOPE	7.2 40	1.7 50	+3.1 57.5 TOP SLOPE	+3.2 60	+3.3 63 Edge A.C.	+2.3 65 GUTTER	+3.1 67	+3.3 81 RES.
0+10			13.7 C	13.7 0.5	14.9 7.5 DRAIN BASIN	13.7 10	13.3 11.5 Edge A.C.	12.5 20	11.2 30	10.0 34.6 TOE SLOPE	7.5 40	1.2 50	+3.3 58 TOP SLOPE	+3.4 61 Edge A.C.	+3.3 63	+2.4 65 GUTTER	+3.3 67	+3.6 80 RES.
0+20			13.9 C	13.9 0.5	13.5 2.5 TOP BERM	14.2 3.5 BOTTOM BERM	14.0 6.2 Edge A.C.	13.4 10	12.6 20	11.0 30	9.6 35.5 TOE SLOPE	7.1 40	1.9 50	+3.1 58 TOP SLOPE	+3.3 61	+3.4 63	+2.3 65 GUTTER	+3.1 67	+3.5 80 RES.
CK. TBM	12.77	453.85	12.76	441.08														
0+30			13.5 C	13.5 0.5	12.9 2 TOP BERM	13.6 3.5 GRD	12.9 10	11.8 20	10.6 30	9.6 35 TOE SLOPE	7.8 40	2.0 50	+3.3 59 TOP SLOPE	+3.3 61 Edge A.C.	+3.1 63	+2.3 65 GUTTER	+3.0 67	+3.3 80 RES.
0+40			12.7 C	12.7 0.5	12.1 2 TOP BERM	12.5 3 GRD.	11.9 10	11.1 20	10.4 30	9.6 35 TOE SLOPE	7.6 40	2.0 50	+3.2 59 TOP SLOPE	+3.3 61 Edge A.C.	+3.4 63	+2.1 65 GUTTER	+3.3 67	+3.6 80 RES.
0+45								10.84 26.5 TOP 12" C.I. DRAIN		9.41 32.8 TOP 12" CEM. DRAIN		+2.1 64 CATCH BASIN		0.55 64 ℄ 12" DRAIN				
0+47	60' RT. P. POLE																	
0+50					11.2 2 TOP BERM	11.6 4	11.5 10	10.9 20	10.2 30	8.6 36.4 TOE SLOPE	7.4 40	2.2 50	+3.2 59 TOP SLOPE	+3.3 61 Edge A.C.	+3.3 62.5	+1.9 65 GUTTER	+2.9 67	+3.4 80 RES.
0+60			10.7 C	10.7 0.5	10.1 1.8 TOP BERM	10.8 3 GUTTER	10.4 10	10.4 20	10.1 30	8.7 38 TOE SLOPE	8.0 40	2.6 50	+3.3 60 TOP SLOPE	+3.3 61 Edge A.C.	+3.3 62	+2.0 64.5 GUTTER	+2.8 67	+3.3 80 RES.
0+70			9.3 C	9.3 0.5	8.7 1.5 TOP BERM	9.6 3.7 GUTTER	8.9 10	9.3 20	9.0 30	7.8 38	7.0 40	6.5 43.4 TOE SLOPE	3.1 50	+3.4 60	+3.4 61 Edge A.C.	+3.3 63	+2.0 65 GUTTER	+2.8 67	+3.3 80 RES.

PROP. LINE

FENCE LINE

BAYVIEW RESERVOIR (CONT'D) 1/28/57 SHOREY

BT

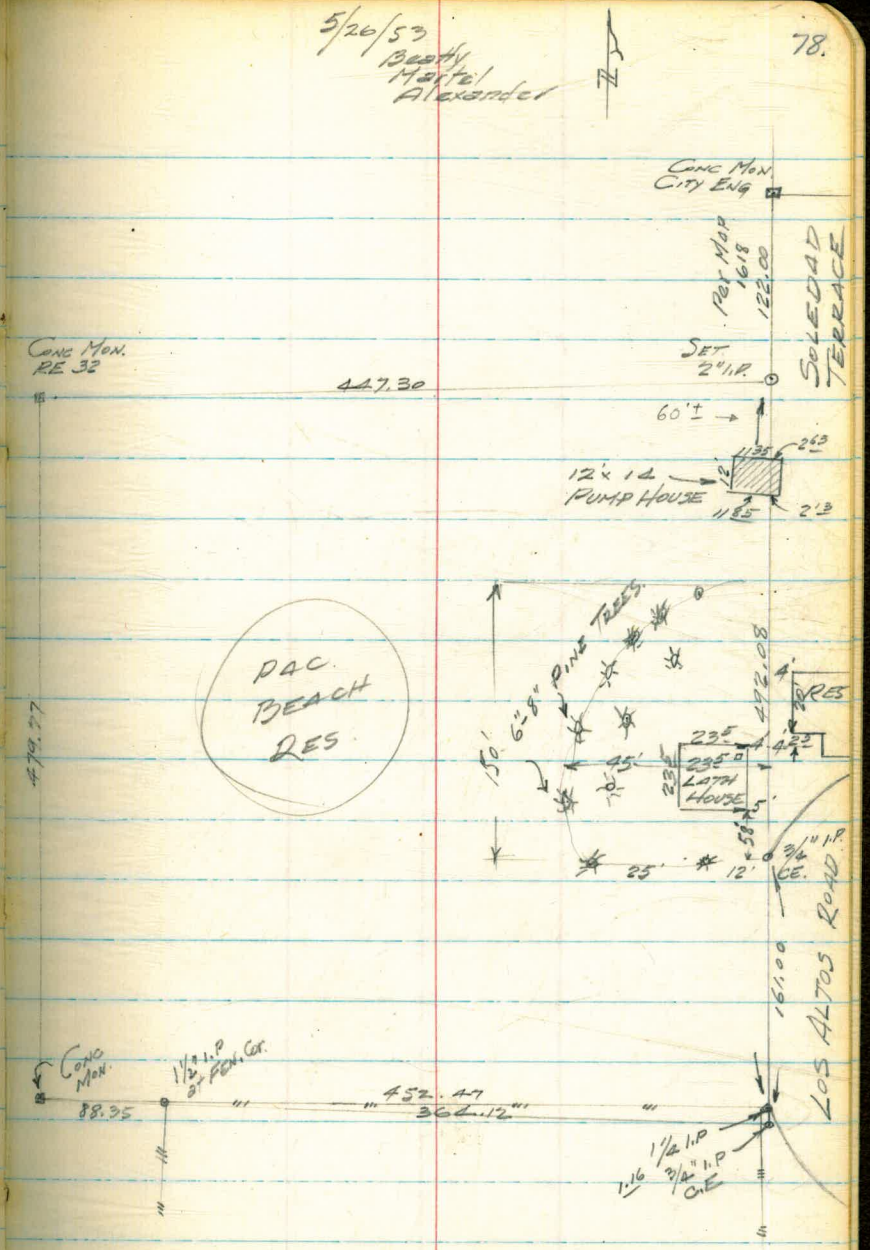
Station	BS	H.I.	FS	Elev.	Readings (rod / distance)	Remarks
		453.85				
0+80					7.9/C; 7.9/0.5; 7.3/1.3 TOP BERM; 7.9/3.6; 8.1/10; 7.3/20; 6.3/30; 5.7/40; 4.1/47.4 TOE SLOPE; 2.9/50; +3.2/61 Top Slope; +3.2/62 Edge A.C.; +3.2/63; +2.2/65.5; +2.8/68; +3.3/80.5 RES.	
0+90					6.4/C; 6.4/0.5; 5.8/1.4 TOP BERM; 6.3/3; 6.3/10; 5.1/12; 4.5/20; 3.5/30; 2.6/40; +0.2/50; +2.9/58; +3.6/62 Edge A.C.; +3.6/66; +3.1/70; +3.4/82 RES.	
TP	9.64	460.06	3.43	450.42		
1+00					10.9/C; 10.9/0.5; 10.6/1.3 TOP BERM; 11.1/3; 9.2/10; 7.5/20; 7.2/30; 5.5/40; 4.2/47.8 Edge A.C. ROAD; 4.1/50; 2.8/68; 3.2/71.5; 2.9/84.8 RES.	
1+10					9.2/C; 9.2/0.5; 8.9/1.2 END OF BERM; 5.7/10; 4.8/20; 4.8/22.3 EDGE A.C. ROAD; 4.5/30; 4.0/40; 3.5/50; 3.0/60; 2.7/70; 2.8/72.5; 3.1/76; 2.9/93 RES.	
1+20					6.1/C; 5.5/0.5 A.C. ROAD; 5.1/10; 4.7/20; 4.4/30; 4.0/40; 3.5/50; 3.2/60; 2.9/70; 2.9/80; 2.9/82; 3.1/86; 3.1/90; 3.0/100	
1+22					3.9/82 ℄ DRAIN PIPE UNDER A.C. ROAD	
1+28					5.5/C; 5.4/0.5; 5.2/10 ON A.C. ROAD; 4.8/20 ON A.C. ROAD; 4.4/30 ON A.C. ROAD; 4.2/40 Edge A.C. ROAD; 3.9/50; 3.5/60; 3.3/70; 2.9/76; 4.2/77; 4.1/79; 3.1/81; 2.9/86	
CK.			3.04	457.02 = 457.024		N.W. COR. RES. BUTTRESS BLK. PG. 64

PROP. LINE

FENCE LINE

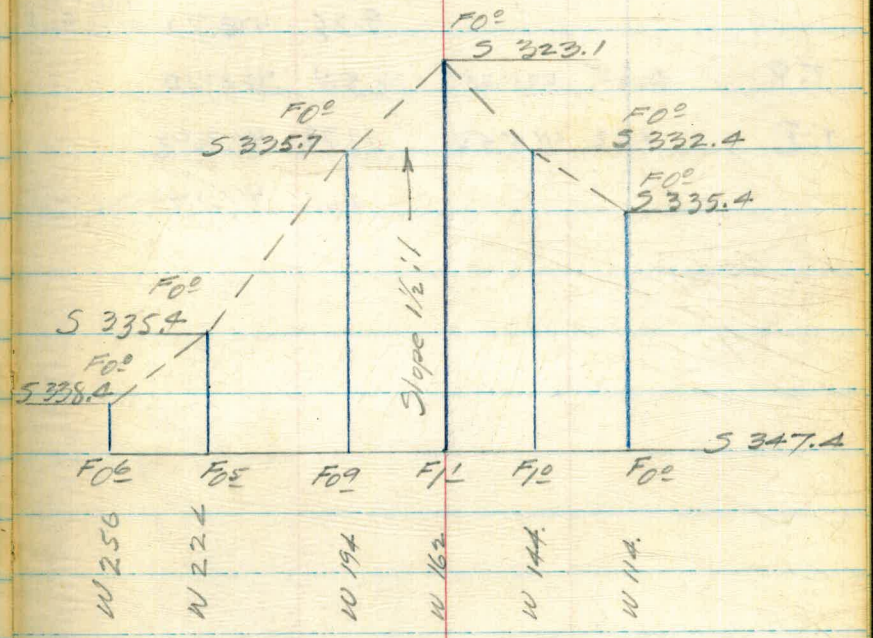
PAC BEACH RES.
Ely 5 Acres Lot 6

5/26/53
Beatty
Martel
Alexander



May 12-50

Slope Deficiency SE. Cor Res

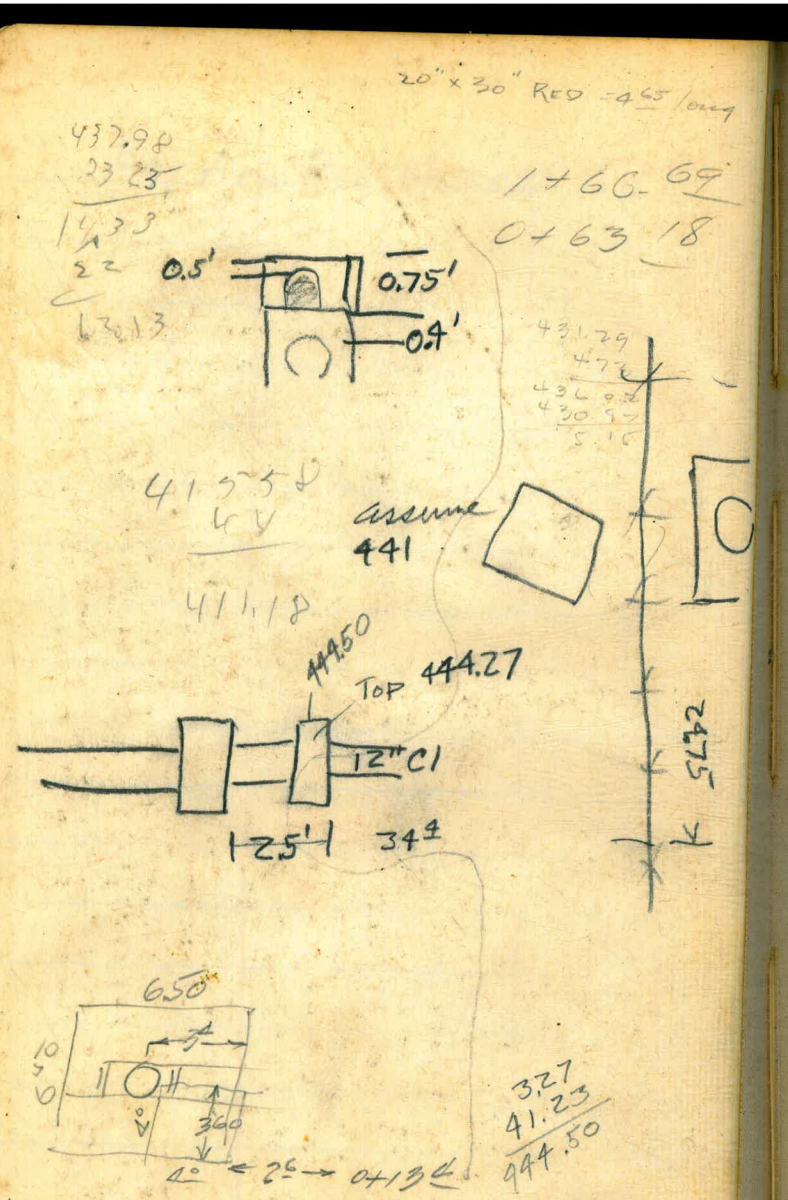


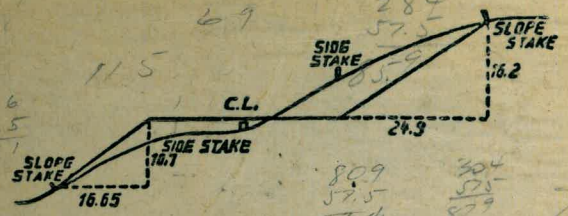
	2.37	460.84		458.47	
	1.29	449.74	12.39	448.45	
	0.63	437.98	12.41	437.33	
			9.26	428.72	Na, / 1N. Post
T.P.	0.35	425.75	12.58	425.40	
T.P.	1.62	415.58	11.79	413.96	
			4.41	411.17 – Top old	Res.

Bay View Res. Access Rd/ R17-21

T. P.

T. P.





DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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