WATER QUALITY TECHNICAL REPORT FOR TORREY MEADOWS DRIVE OVERCROSSING

Prepared for:





Prepared by:

TYLININTERNATIONAL

August 17, 2015

CERTIFICATION

This Hydrology and Hydraulics Analysis report has been prepared under the direction of the following Registered Civil Engineer. The Registered Civil Engineer (Engineer) attests to the technical information contained herein and the engineering data upon which the following design, recommendations, conclusions, and decisions are based.

Jeff Burdick, PE

RCE C75396

Exp: 12/31/2015

Registered Civil Engineer

T.Y. Lin International

404 Camino Del Rio South, Suite 700

San Diego, CA 92108

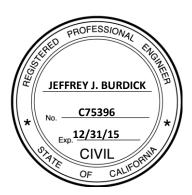


Table of Contents

List of Figures	3
List of Appendices	
Section 1	
General Information	
Project Description	
Figure 1. Site Map	5
Soil Erosion Potential and Mitigation	
Site Slope	
Site Data and Storm Water Quality Design Issues	7
Preservation of Existing Vegetation	7
Non-storm Water Discharges	8
Section 2	
Pollutants and Conditions of Concern	8
Pollutants of Concern from the Project Area	8
Conditions of Concern	8
Section3	Ç
Proposed Permanent Storm Water Best Management Practices (BMPs)	g
BMPs Analysis and Description	
Hydrology Calculations to Determine Treatment Flow Rate and Volume	10
Acceptance of Maintenance Responsibility	11
Inspection, Operation, and Maintenance Plan	11
Annual Maintenance Cost	11
Code or Requirement Conflicts	12
Section4	12
Proposed Temporary Construction Site BMPs	12
Section 5	13
Conclusion	

List of Figures

Figure 1- Site Map

List of Appendices

Appendix A- Vicinity Map and FEMA FIRMETTE

Appendix B- Storm Water Requirements Applicability Checklist

Appendix C- Temporary Water Pollution Control Plan

Appendix D- Erosion Control Plan

Appendix E- Existing Condition Hydrologic Analyses, As-Builts and Map

Appendix F- Proposed Condition Hydrologic Analyses and Map

Appendix G- Proposed Drainage Plan and Profiles

Appendix H- Proposed Preliminary Hydro modification and Treatment Control BMP Map

Appendix I- Preliminary Hydro modification Analysis

Appendix J- Simple Sizing Method for Biofiltration BMPs

Appendix K- BMP Inspection, Operation and Maintenance Plan

Appendix L- Drainage Study

Section 1

General Information

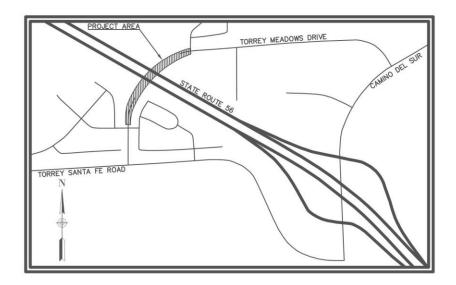
Project Description

The City of San Diego, in cooperation with the California Department of Transportation (Caltrans) District 11 and Kilroy Realty, is proposing to construct a bridge overcrossing State Route 56 (SR-56) to connect Torrey Meadows Drive in the Torrey Highlands community of San Diego. The purpose of the project is to connect the divided community of Torrey Highlands, which is currently bisected by SR-56. In addition, the execution of this project would physically integrate Torrey Highlands to the greater Rancho Peñasquitos and Santaluz communities north of State Route 56. The proposed bridge would provide residents an alternate way of entering and leaving their cul-de-sac community.

The build alternative proposes constructing a bridge overcrossing at Torrey Meadows Drive over SR-56. The proposed bridge would be a two-span, cast-in-place concrete bridge, 53 feet wide and 337 feet long. This would allow for a two-lane over crossing, with 6' sidewalks as required by the Caltrans Bridge Design Standards. Torrey Meadows Drive would be extended from the north and

south into Caltrans Right-of-Way to connect to the proposed bridge. The total disturbed soil area (DSA) was calculated to include new slopes, removal of existing roadway, and new roadway. The total DSA for the project is 1.5 acres. The proposed project will increase the impervious surface area by 0.8 acres. The project is located within the City of San Diego urban Municipal Separate Storm Sewer System (MS4) area.

Figure 1. Site Map



Site Map- Not to scale

Soil Erosion Potential and Mitigation

Much of the topography within the affected area consists of level terrain with the exception of two
prominent slopes on either side of SR-56. The project risk level was determined by the GIS Map
Method (EPA Rainfall Erosibity Calculator & GIS Map). Based on the summary table below, the
project risk is expected to be Level 2 (RL-2).

	Sediment Risk Factor			Receivin Ri	_		
Alternative	R	K	LS	Risk Factor	RWQCB	Risk Factor	Combined Risk
2	35	0.32	3.67	Medium	9	High	Level 2

- The Soil Conservation Service classifies soils within the project area as possessing a severe potential for erosion by water.
 - Available mitigation methods during construction include: timing of grading to avoid the rainy season, use of sand bags and/or hay bales in graded areas, silt fences, temporary drainage facilities, prompt seeding and re-vegetation of graded areas.
 - Available measures for the post-construction phase include: adequate maintenance of permanent drainage facilities and adequate maintenance of permanent vegetative cover.

Site Slope

- Existing slopes vary from 2:1 to 3:1 and flatter. Proposed improvements will create new slopes and modify existing slopes. Profiles and layouts were reviewed to minimize impact to existing slopes and requirement of new high cut/fill slopes. New slopes will be graded at 4:1 or flatter in fill and 2:1 or flatter in cut wherever feasible to enhance aesthetics and facilitate re-vegetation.
- Because slopes are proposed greater than 4:1, an erosion control plan is required.
- Proposed grading will potentially increase erosion at the site. The following construction activities
 will be considered to offer slope/surface protection; new proposed fill slopes will maintain similar
 height and inclination as existing slopes wherever feasible. The proposed slopes will not be high
 enough to warrant the implementation of benches or terraces. The flows will be collected in stabilized
 drains or channels to protect slopes.

Vegetated surfaces will be designed to minimize overland and concentrated flow depths and velocities, and maximize contact time between water and vegetated surfaces. This will enhance infiltration and pollutant removal opportunities.

If feasible, topsoil (duff) and vegetation removed during construction will be stripped and stockpiled. These materials will be used in the surface preparation prior to seeding operations. Slope roughening, terracing, rounding, and stepping will be implemented where necessary.

- Vegetation along SR-56 mainline consists mostly of groundcover, shrubs, with scattered trees.
 Vegetation removal will be necessary to implement project improvements.
- Hard surfaces (rock blankets, pervious paving, etc) are not anticipated to maintain slope/surfacing protection. Vegetation should provide adequate erosion protection for all disturbed soil area.
- Further consideration for DPP BMPs will be examined in the PS&E phase.

Site Data and Storm Water Quality Design Issues

- The proposed overcrossing is located within the jurisdictional boundary of the San Diego Regional Water Quality Control Board (SDRWQCB). The project is part of the Peñasquitos Hydrologic Unit, in the Miramar Reservoir Hydrologic Area, identified as Hydrologic Sub-Area 906.10. More specifically, the project is located within the Carmel Valley-Poway Creek Watershed. The Carmel Valley-Poway Creek Watershed is a high risk receiving watershed.
- The project drains into the Carmel Valley-Poway Creek Watershed, which is the receiving body of water and is a tributary of Hydrologic Sub-area 906.10. Runoff flows through McGonigle Canyon to Los Peñasquitos Lagoon.
- No seasonal construction, construction exclusion dates or restrictions required by federal, state, or local regulatory agencies are known at this time.
- According to the Storm Water Requirements Applicability Checklist (SWRAC) this construction site
 is high priority, see Appendix B. The project requires an approved Storm Water Pollution Prevention
 Plan (SWPPP) due to the amount of new impervious surfaces produced by the improvements and the
 amount of disturbed soil area affected.
- There are no Drinking Water Reservoirs and/or Recharge Facilities within project limits.
- There are no known local agency requirements for this project at this point.
- The project is located in the north-central portion of San Diego County, which is part of the South Coast hydrologic region. Climate data was taken from 1971-2000. January is the coldest month, with a mean temperature of 55.3°. August is the hottest month, with a mean temperature of 72.3°. The average annual rainfall in the region is 11.97 inches, with wide annual variations and most of the precipitation falling between the months of November and March.
 - According to the Caltrans Project Planning and Design Guide, the rainfall intensity for calculation of water quality flow from areas discharging to flow-based Best Management Practices (BMPs) is 0.2" per hour.

Preservation of Existing Vegetation

Clearing and grubbing will occur where appropriate over the entire disturbed soil area. Steps have
been taken to minimize disturbed area. Proposed construction follows existing contours to minimize
cut and fill. All landscape within Caltrans right-of-way that is disturbed or removed will be replaced
following Caltrans Replacement planting policy. As an interim measure, erosion control will be
applied to all disturbed areas following Caltrans Policy and Procedures.

• There are no known Environmentally Sensitive Areas (ESAs) present within the project limits.

Non-storm Water Discharges

Landscaping features may be added to the project site in the future and it is possible that the landscaped areas could result in non-storm water discharges due to irrigation. Plans will include application methods of irrigation water that will minimize runoff of excess irrigation water into the storm water conveyance system.

Section 2

Pollutants and Conditions of Concern

Pollutants of Concern from the Project Area

- The Los Peñasquitos Lagoon is included on the 2010 Clean Water Act (CWA) Section 303(d) List of Water Quality Limited Segments Requiring Total Maximum Daily Loads (TMDLs). For sedimentary siltation the list was accessed using the Caltrans Water Quality Planning Tool (WQPT). Pollutants of concern include sediment and dissolved solids. Total Maximum Daily Loads (TMDLs) have not been implemented for Los Peñasquitos Lagoon at this time.
- The targeted Design Constituents (TDCs) for this project is sediment.
- A written request for section 401 water quality certification is not necessary since there are no wetlands within the project area.

Conditions of Concern

- The following measures will be utilized to avoid or reduce potential storm water impacts.
 - Erosion from slopes will be minimized using the following methods: disturbing existing slopes only when necessary, minimizing cut and fill areas to reduce slope length, incorporating retaining walls, providing cut and fill slopes flat enough to allow re-vegetation and limit erosion to pre-construction rates, rounding and shaping slopes to reduce concentrated flow, and collecting concentrated flows in stabilized drains and channels. Construction items requiring extensive soil disturbance will be scheduled outside of the rainy season as much as practically feasible.
 - Permanent storm water pollution controls will be installed as early in the construction process as feasible to provide additional protection and possibly utilize them in addressing construction storm water impacts.
- There are three Vortechnics hydrodynamic separators located in the project area to treat storm water runoff from the existing developments.

Section 3

Proposed Permanent Storm Water Best Management Practices (BMPs)

BMPs Analysis and Description

In order to achieve certain performance standards as required in Model BMP Design Manual San Diego Region for Permanent Site Design, Storm Water Treatment and Hydro modification Management, dated January 2015, biofiltration basins are utilized due to their efficiency of water storage and treatment.

- Site conditions provide adequate areas for the installation of water quality and hydro modification treatment devices to fully address the projects proposed increased impervious area.
- The proposed hydro modification BMPs are biofiltration basins located in various locations on the project as shown in Appendix H. Biofiltration facilities use a combination of filtration through soil media and plant roots to treat water. Soil media is recommended to have a surface area of .04 times the impervious area based on 5 in/hr for infiltration through the soil media. The biofiltration facilities consist of vegetated basins with 18" soil media and 18" gravel media for filtration and storage of storm flows. The biofiltration basin has been designed as a volume based system that provides both surface and subsurface storage. Biofiltration basins are sized based on the County of San Diego's BMP Sizing Calculator. Outputs can be found in the Table 3 and in greater detail in Appendix B. The proposed BMPs make use of the existing drainage infrastructure.
- For the purposes of selecting Treatment Control BMPs, Pollutants of Concern are grouped as coarse sediment and trash, pollutants that tend to associate with fine particles, and pollutants that remain dissolved according to Table B.6-2 of the Model BMP Design Manual San Diego Region Appendix B (reproduced below as Table 1).

Table 1 – Grouping of Pollutants						
Pollutant	Coarse Sediment and Trash	Pollutants that tend to associate with fine particles during treatment	Pollutants that tend to be dissolved following treatment			
Sediment	X	X				
Nutrients		X	X			
Heavy Metals		X				
Organic Compounds		X				
Trash & Debris	X					
Oxygen Demanding		X				
Bacteria		X				
Oil & Grease Pesticides		X X				

Hydrology Calculations to Determine Treatment Flow Rate and Volume

According to the calculations for the project site, the storm water runoff can be treated in biofiltration facilities onsite. The design capture volume (DCV) is the hydrologic method used to calculate the storage of the hydro modification system, which is designed to store the volume of storm water runoff resulting from the 85th percentile, 24-hour storm event onsite. Table 3 shows the DCV requirement per DMA.

Ta	Table 3- Worksheet B.2-1 Design Capture Volume						
Design Capture Volume		Worksheet B-2.1 Model BMP Design Manual January 2015					
	DMA 1 DMA 2 DMA 3 DM 4					DMA 4	
1	85th percentile 24-hr storm depth from Figure B.1	d= inches	0.62	0.62	0.62	0.62	
2	Area tributary to BMPs	A= acres	1.13	0.79	0.50	0.48	
3	Area weighted runoff factor (estimate using section B.1 and B.2.1)	C= unitless	1.0	1.0	1.0	1.0	
4	Street trees volume reduction	TCV= cubic-feet (10ft ³ /tree)	120	120	110	100	
5	Rain barrels volume reduction	RCV= cubic-feet	0	0	0	0	
6	Calculate DVC= (C x d x A x 43560 x (1/12))-TCV- RCV	DCV= cubic-feet	2413.73	1661.21	1014.83	973.94	

Table 4 below, shows the proposed and required sizing of the hydromodification BMPs for the project. The onsite storage exceeds the required storage calculated from Table 3 for the DCV, see Appendix J for additional calculations. In addition, the BMPs have been sized per the County of San Diego BMP Sizing Calculator Methodology to meet the flow control requirement of $0.1Q_2$ and Q_{10} , see Appendix I.

Table 4- Required and Proposed BMP Sizing					
			Area Required		
			Design		
	Proposed	Area Required	Capture		
	BMP Area	Flow Control	Volume		
	(sf)	(sf)	(sf)		
BMP #1.1	3835.03	3519.20	312.12		
BMP# 1.2	2344.31	3319.20	312.12		
BMP #2	2218.81*	3702.34	214.81		
BMP #3	2987.61	1871.79	131.23		
BMP #4	2427.08	1808.47	125.94		

m 4 1	11 504 03	10 001 00	704.10
Total	11,594.03	10,901.80	784.10

*BMP#1.1 treats the square footage not covered by BMP#2;

BMP#1.1, 1.2 and 2 are directed to the same outfall.

The project discharges to two locations of McGonigle Canyon Creek. This first location of discharge is located on the south side of SR-56. Storm water runoff for outfall 1 is treated by BMP#1.1 and 1.2 (biofiltration basins A and B) and BMP#2 (biofiltration basin C), see Appendix H for locations; as well as in the existing Vortechnics hydrodynamic separator treatment facility. Although, the proposed BMPs exceed the requirement, the hydrodynamic separator has additional capacity to treat additional runoff, if needed. The second location of discharge is located on the north side of SR-56. Storm water runoff is treated by BMP #3(biofiltration basin D) and BMP#4 (biofiltration basin E) before discharging into the McGonigle Creek; it should be noted that the treatment for outfall 1 and 2 exceed the minimum requirement for both DCV and Flow Control. Additional calculations are provided in Appendices J and I.

Acceptance of Maintenance Responsibility

At the time a construction permit is issued, it is recommended that a statement for accepting responsibility for interim O&M of facilities is obtained from the contractor. The responsible party to implement and maintain BMPs in perpetuity will be transferred to the City of San Diego upon notice of completion.

Inspection, Operation, and Maintenance Plan

An example of an Inspection, Operation, and Maintenance Plan (IOMP) is provided in Appendix K.

Annual Maintenance Cost

Since rainfall amounts can vary wildly from year to year, it is difficult pinpoint a reliable annual maintenance cost. For planning purposes maintenance costs assume average annual rainfall. A breakdown of the estimate for annual maintenance costs has been included in Appendix K. A summary of the general range for annual operation and maintenance costs for each BMP is shown in Table 5.

Table 5 - Summary of Annual Maintenance Cost				
BMP Frequency		Annual Cost (each)		
Biofiltration Basin A	2/YR	\$5,900		
Biofiltration Basin B	2/YR	\$4,100		
Biofiltration Basin C	2/YR	\$4,100		

Biofiltration Basin D	2/YR	\$4,100
Biofiltration Basin E	2/YR	\$4,100

Code or Requirement Conflicts

There are no conflicts with codes or requirements other than the items addressed to implement the proposed facilities.

Section 4

Proposed Temporary Construction Site BMPs

- Construction Site Best Management Practices (BMPs) are to be applied during construction activities
 to reduce the pollutants in storm water discharges throughout construction. These Construction Site
 BMPs provide both temporary erosion and sediment control, as well as control for potential pollutants
 other than sediment. The following categories of BMPs are designed to be used for controlling
 potential pollutants on construction sites: Soil Stabilization Practices; Sediment Control Practices;
 Tracking Control Practices; Wind Erosion Control; Non-Storm water Controls; and Waste
 Management and Material Pollution Controls.
- Dewatering is not anticipated for this project.
- Turbidity and pH are not considered design pollutants for this project, therefore, Active treatment systems (ATS) will not be considered for the project.
- Concurrence with the District Construction Storm Water Coordinator will occur in the PS&E phase.
- The project risk level was determined by the GIS Map Method (EPA Rainfall Erosivity Calculator &
 GIS Map). The project risk is expected to be Level 2 (RL-2). Therefore, the following items are not
 applicable: Receiving Water Bioassessment and Sampling, and Analysis for Suspended Sediment
 Concentration (SSC).
- Funds allocated incorporate construction items required by the new permit, which includes funds for separate bid line items (Prepare Storm Water Pollution Prevention Plan, Job Site Management, Storm Water Annual Report, Rain Event Action Plan, Storm Water Sampling and Analysis Day, Movein/Move-out (Temporary Erosion Control), Temporary Fiber Roll, Temporary Concrete Washout, Temporary Construction Entrance, Temporary Check Dam, Temporary Drainage Inlet Protection, Street Sweeping, Water Pollution Control Maintenance Sharing, Additional Water Pollution Control, and Storm Water Sampling and Analysis.)

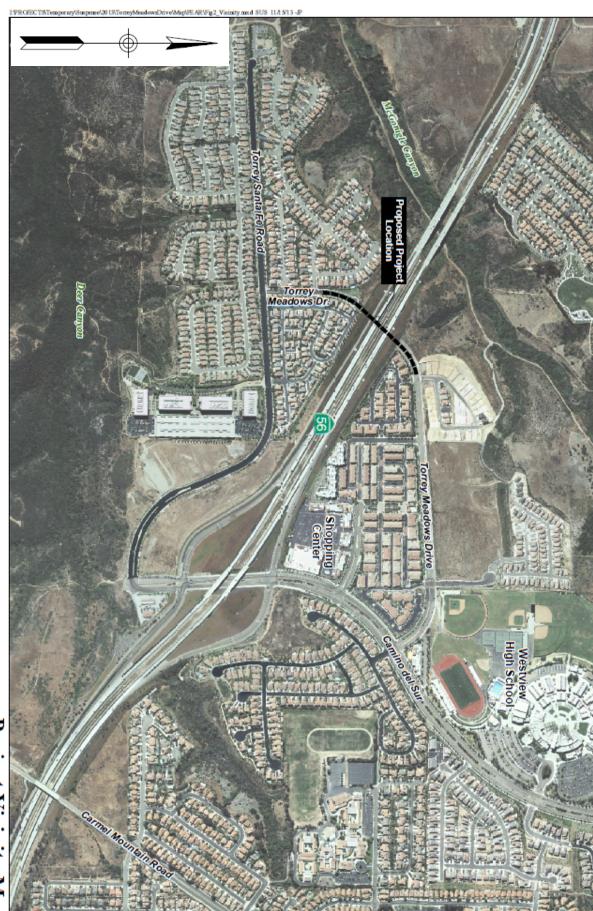
Section 5

Conclusion

The proposed hydro modification treatment facilities meet the requirements per the Model BMP Design Manual San Diego Region for Permanent Site Design, Storm Water Treatment and Hydro modification Management, dated January 2015.

Appendix A Vicinity Map and FEMA FIRMETTE





Project Vicinity Map







MAP SCALE 1" = 1000"

500

1,000

1,500

2,000

Z 1 GRAM

PANEL 1335G

AND INCORPORATED AREAS SAN DIEGO COUNTY, FLOOD INSURANCE RATE MAP CALIFORNIA

PR

PANEL 1335 OF 2375

CONTAINS: (SEE MAP INDEX FOR FIRM PANEL LAYOUT)

SAN DIEGO COUNTY SAN DIEGO, CITY OF COMMUNITY

INSURANCE

NUMBER 060284 060295

PANEL 1335 1335 SUFFIX െ ഒ

Notice to User. The Map Number shown below should be used when placing map orders, the Community Number shown above should be used on insurance applications for the subject community.

MAP REVISED MAP NUMBER 06073C1335G

MAY 16, 2012

Federal Emergency Management Agency

This is an official copy of a portion of the above referenced food map. It was extracted using F-MIT On-Line. This map does not reflect changes or amendments which may have been made subsequent to the date on the title block. For the latest product information about National Flood Insurance

Appendix B Storm Water Requirements Applicability Checklist



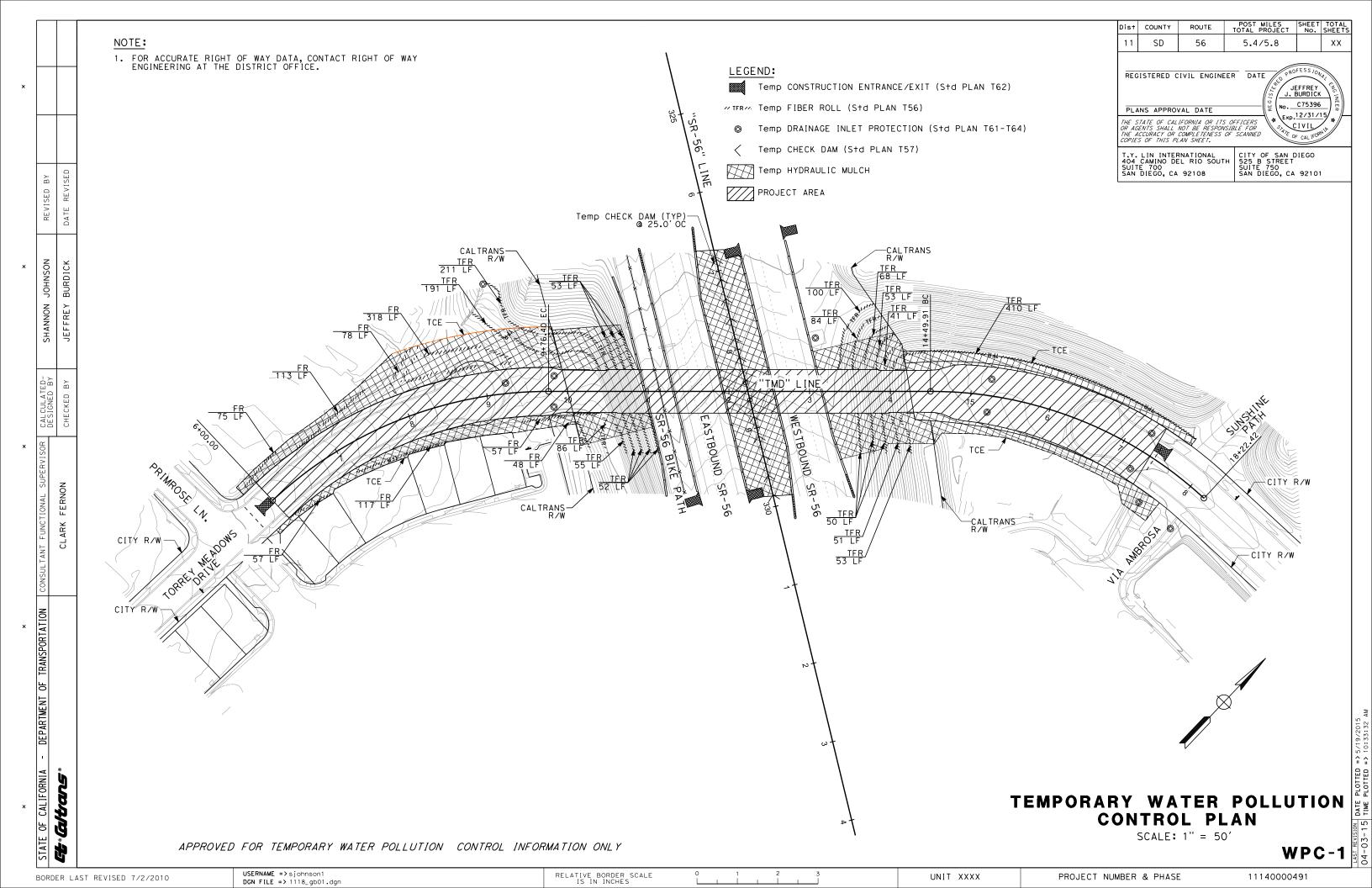
Storm Water Requirements Applicability Checklist

FORM **DS-560**JANUARY 2011

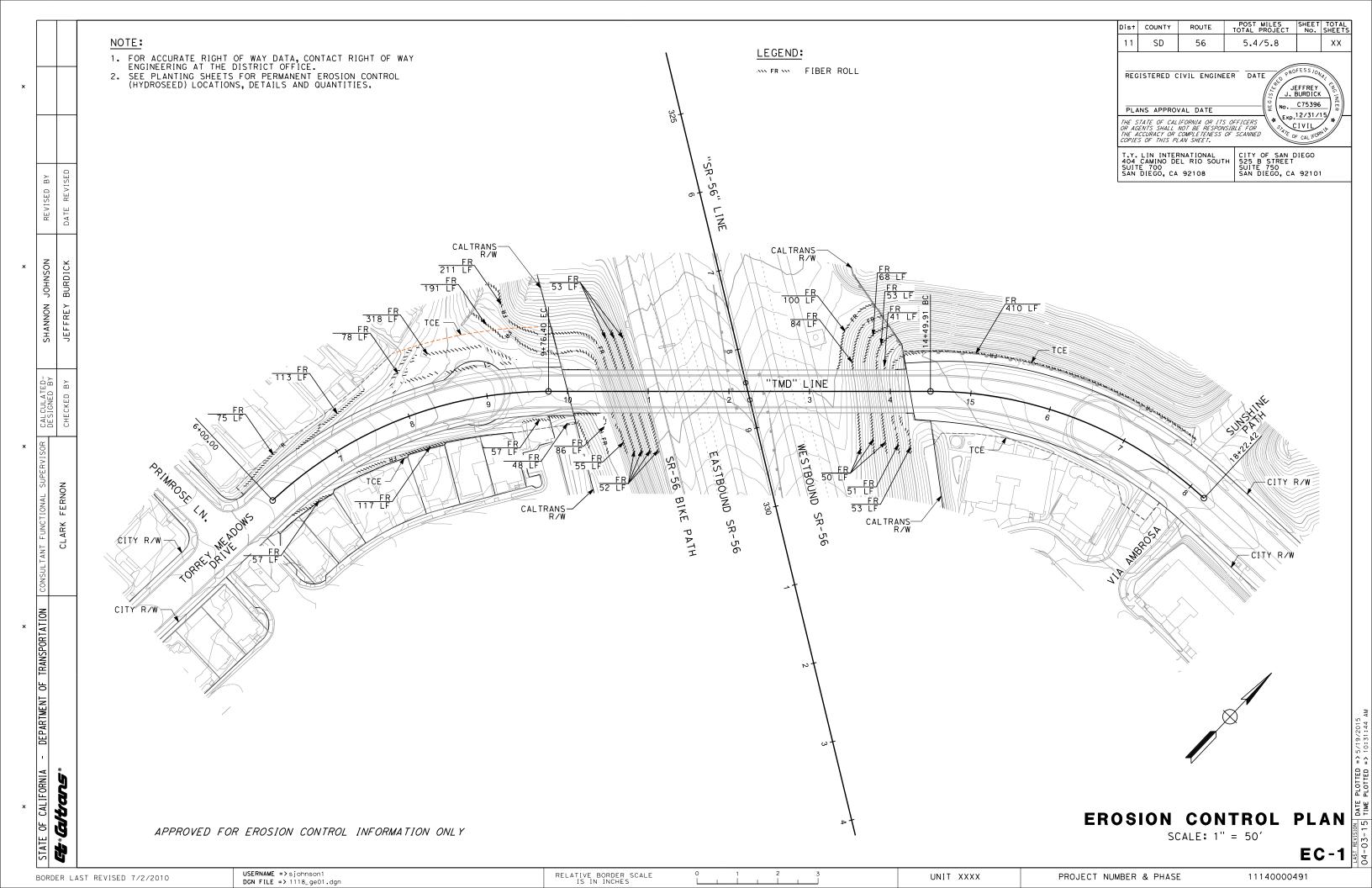
Project Address: Project Number (for City Use Only): **SECTION 1. Permanent Storm Water BMP Requirements:** Additional information for determining the requirements is found in the Storm Water Standards Manual. Part A: Determine if Exempt from Permanent Storm Water BMP Requirements. Projects that are considered maintenance, or are otherwise not categorized as "development projects" or "redevelopment projects" according to the Storm Water Standards manual are not required to install permanent storm water BMPs. If "Yes" is checked for any line in Part A, proceed to Part C and check the box labeled "Exempt Project." If "No" is checked for all of the lines, continue to Part B. The project is not a Development Project as defined in the Storm Water Standards Manual: ☐ Yes ☐ No for example habitat restoration projects, and construction inside an existing building. The project is only the construction of underground or overhead linear utilities. ☐ Yes ☐ No 3. The project qualifies as routine maintenance (replaces or renews existing surface materials because of failed or deteriorating condition). This includes roof replacement, pavement spot repairs and resurfacing treatments such as asphalt overlay or slurry seal, and replacement ☐ Yes ☐ No of damaged pavement. The project only installs sidewalks, bike lanes, or pedestrian ramps on an existing road, ☐ Yes ☐ No and does not change sheet flow condition to a concentrated flow condition. Part B: Determine if Subject to Priority Development Project Requirements. Projects that match one of the definitions below are subject to additional requirements including preparation of a Water Quality Technical Report. If "Yes" is checked for any line in Part B, proceed to Part C and check the box labeled "Priority Development Project." If "No" is checked for all of the lines, continue to Part C and check the box labeled "Standard Development Project." Residential development of 10 or more units. Yes No Commercial development and similar non-residential development greater than one acre. Hospitals; laboratories and other medical facilities; educational institutions; recreational facilities; municipal facilities; commercial nurseries; multi-apartment buildings; car wash facilities; mini-malls and other business complexes; shopping malls; hotels; office buildings; public warehouses; automotive Yes No dealerships; and other light industrial facilities. 3. Heavy industrial development greater than one acre. Manufacturing plants, ☐ Yes ☐ No food processing plants, metal working facilities, printing plants, and fleet storage areas. Automotive repair shop. Facilities categorized in any one of Standard Industrial 4. ☐ Yes ☐ No Classification (SIC) codes 5013, 5014, 5541, 7532-7534, or 7536-7539. 5. Restaurant. Facilities that sells prepared foods and drinks for consumption, including stationary lunch counters and refreshment stands selling prepared foods and drinks for immediate consumption ☐ Yes ☐ No (SIC code 5812), and where the land area for development is greater than 5,000 square feet. Hillside development greater than 5,000 square feet. Development that creates 5,000 square feet of impervious surface and is located in an area with known erosive soil conditions and where ☐ Yes ☐ No the development will grade on any natural slope that is twenty-five percent or greater. Water Quality Sensitive Area. Development located within, directly adjacent to, or discharging directly to a Water Quality Sensitive Area (as depicted in Appendix C) in which the project either creates 2,500 square feet of impervious surface on a proposed project site or increases the area of imperviousness of a proposed project site to 10% or more of its naturally occurring condition. "Directly adjacent" is defined as being situated within 200 feet of the Water Quality Sensitive Area. "Discharging directly to" is defined as outflow from a drainage conveyance system that is composed entirely of flows from the subject development or redevelopment site, and not commingled with flows from adjacent lands. \square Yes Parking lot with a minimum area of 5,000 square feet or a minimum of 15 parking spaces and potential exposure to urban runoff (unless it meets the exclusion for parking lot reconfiguration ☐ Yes ☐ No on line 11).

Pag	Page 2 of 2 City of San Diego • Development Services Department • Storm Water Requirements Applicability Checklist				
9.		way. New paved surface in excess of 5,000 square feet omobiles, trucks, motorcycles, and other vehicles road reconfiguration on line 11).	☐ Yes ☐ No		
10.		that is: (a) 5,000 square feet or more or (b) has (ADT) of 100 or more vehicles per day.	☐ Yes ☐ No		
11.	impervious surface and the existing is not considered Significant Redewithout a change to the footprint of	oject installs and/or replaces 5,000 square feet or more ng site meets at least one of the categories above. The evelopment if reconfiguring an existing road or parking of an existing developed road or parking lot. The exist curb or the outside edge of pavement when there is no	project g lot ing		
12.		roject. Any other project not covered in the categories ore and is not excluded by the criteria below.	☐ Yes ☐ No		
and j	fertilizers, such as slope stabilizatio e linear pathways that are for infred	pervious surface and where added landscaping does n n using native plants. Calculation of the square footag quent vehicle use, such as emergency maintenance acce y sheet flow to surrounding pervious surfaces.	e of impervious surface need not in-		
Par	rt C: Select the appropriate cate	gory based on the outcome of Parts A & B.			
1.	If "Yes" is checked for any line in I	Part A, then check this box. Continue to Section 2.	☐ Exempt Project		
2.	If "No" is checked for all lines in P Continue to Section 2.	art A, and Part B, then check this box.	☐ Standard Development Project		
3.	lines in Part B, then check this box	Part A, and "Yes" is checked for at least one of the x. Continue to Section 2. See the Storm Water in determining if Hydromodification Management	☐ Priority Development Project		
For		If "Yes" is checked for any line in Part D, then co	ntinue to Part E.		
Par 1.	Is the project subject to California	hase Storm Water Requirements. 's statewide General NPDES Permit for Storm Water ruction Activities? (See State Water Resources Controfor rules on enrollment)	l Yes 🖵 No		
2.	Does the project propose grading of	or soil disturbance?	☐ Yes ☐ No		
3.	Would storm water or urban runo construction area, including wash	ff have the potential to contact any portion of the ing and staging areas?	☐ Yes ☐ No		
4.		ction materials that could negatively affect water (such as, paints, solvents, concrete, and stucco)?	☐ Yes ☐ No		
5.	Check this box if "Yes" is checked	for line 1. Continue to Part E.	SWPPP Required		
6.	Check this box if "No" is checked f Continue to Part E.	for line 1, and "Yes is checked for any line 2-4.	☐ WPCP Required		
7.	Check this box if "No" is checked f	or all lines 1-4. Part E does not apply.	☐ No Document Required		
Part E: Determine Construction Site Priority This prioritization must be completed with this form, noted on the plans, and included in the SWPPP or WPCP. The City reserves the right to adjust the priority of the projects both before and during construction. [Note: The construction priority does NOT change construction BMP requirements that apply to projects; rather, it determines the frequency of inspections that will be conducted by City staff.]					
	a) Projects where the site is 50 acres or more and grading will occur during the wet season b) Projects 1 acre or more and tributary to an impaired water body for sediment (e.g., Peñasquitos watershed) c) Projects 1 acre or more within or directly adjacent to or discharging directly to a coastal lagoon or other receiving water within a Water Quality Sensitive Area. d) Projects subject to phased grading or advanced treatment requirements.				
2 Medium Priority. Projects 1 acre or more but not subject to a high priority designation.					
	B Low Priority. Projects requiring ne of Owner or Agent (Please Print	a Water Pollution Control Plan but not subject to a mo	edium or high priority designation.		
Sign	nature:	Date:			

Appendix C Temporary Water Pollution Control Plan



Appendix D Erosion Control Plan



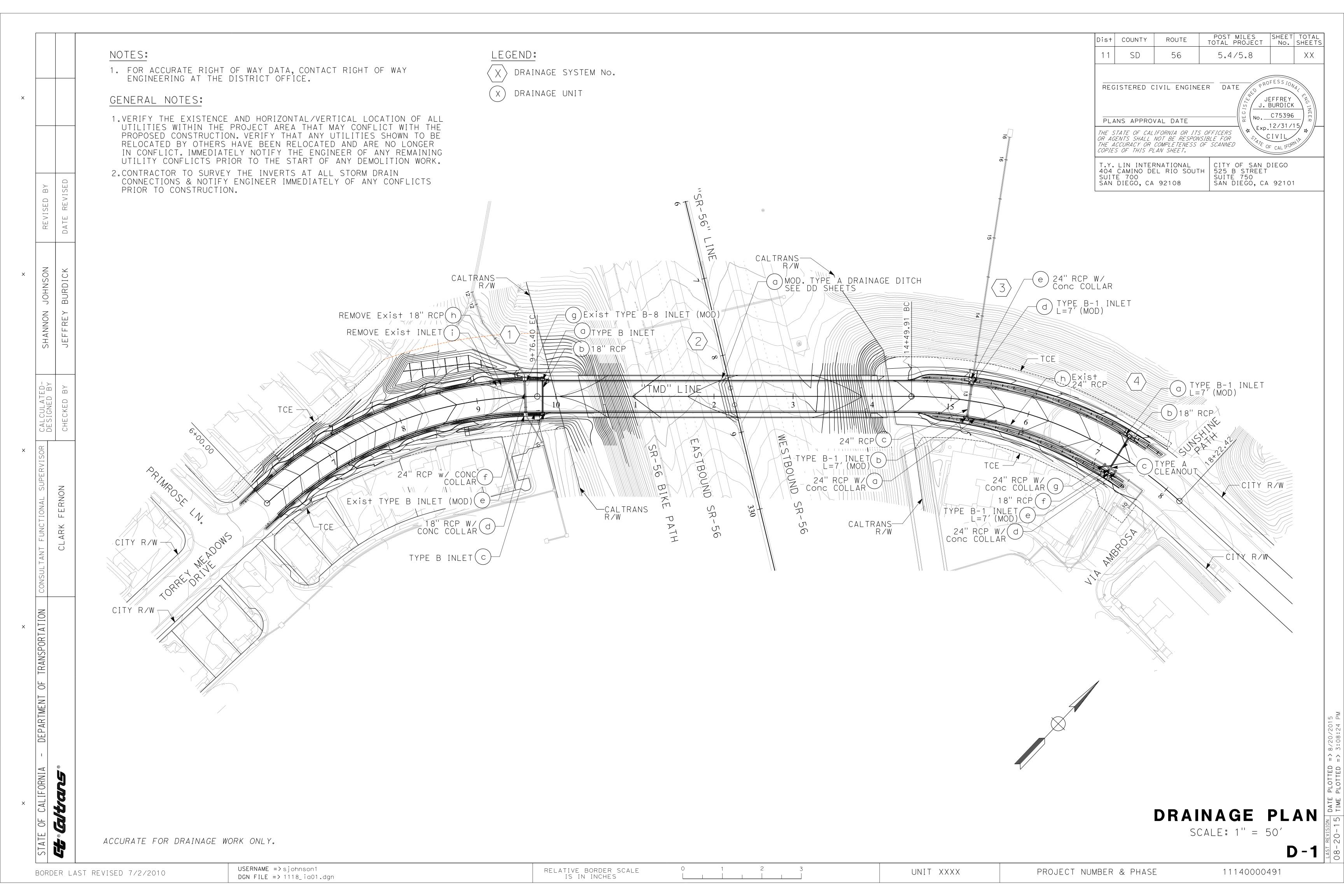
Appendix E Existing Condition Hydrology Map (Additional Information in Drainage Study)

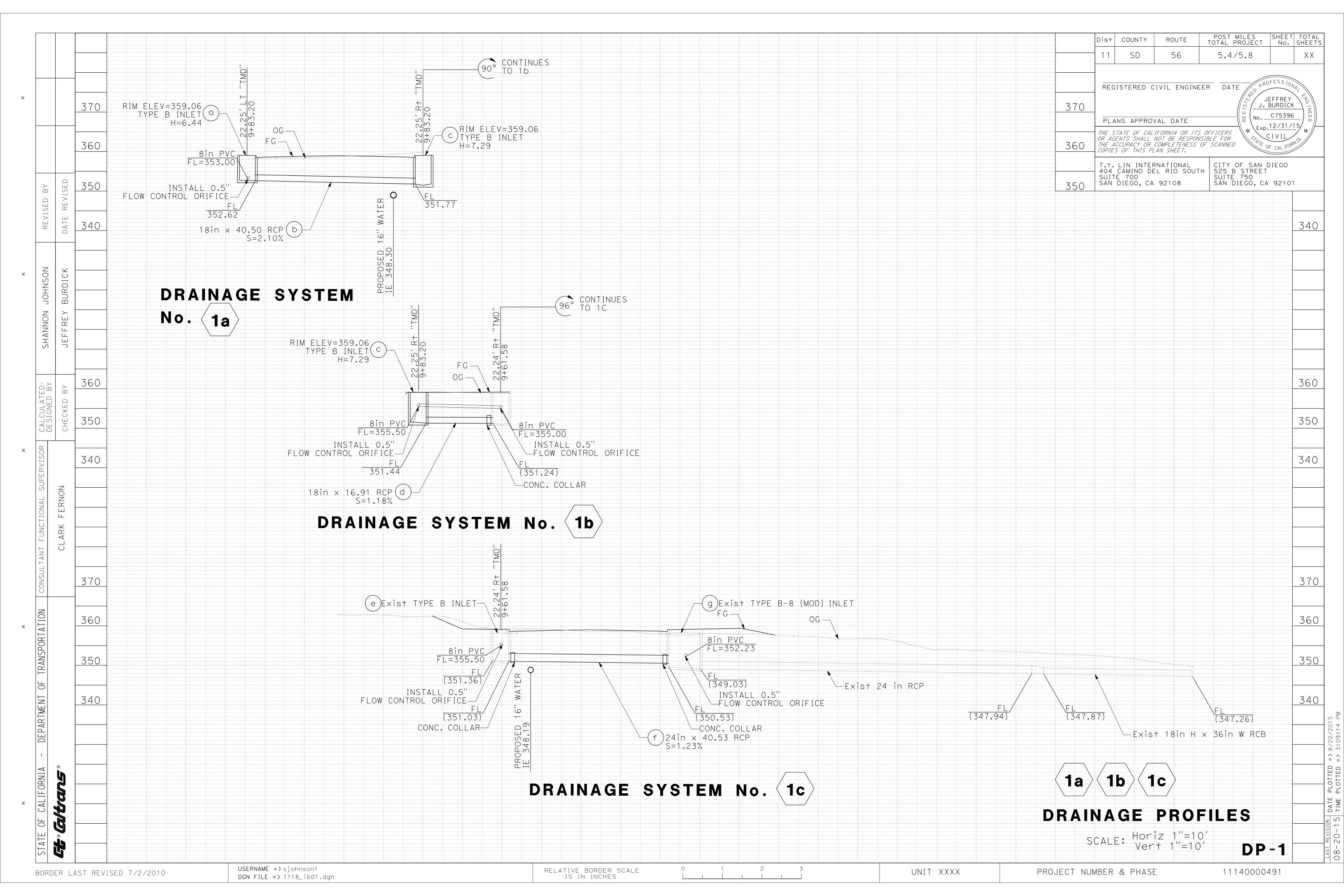


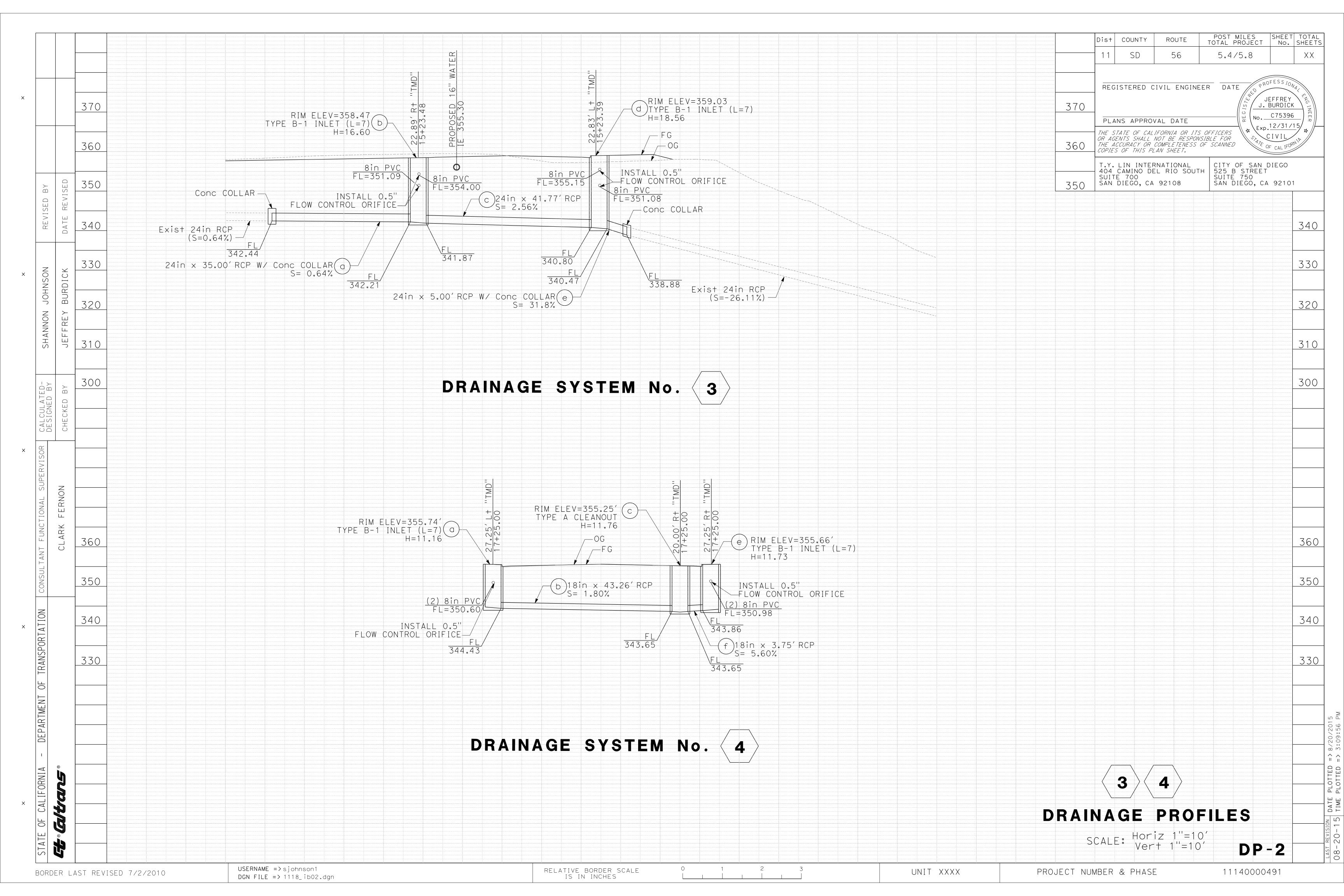
Appendix F Proposed Hydrology Map (Additional Information in Drainage Study)

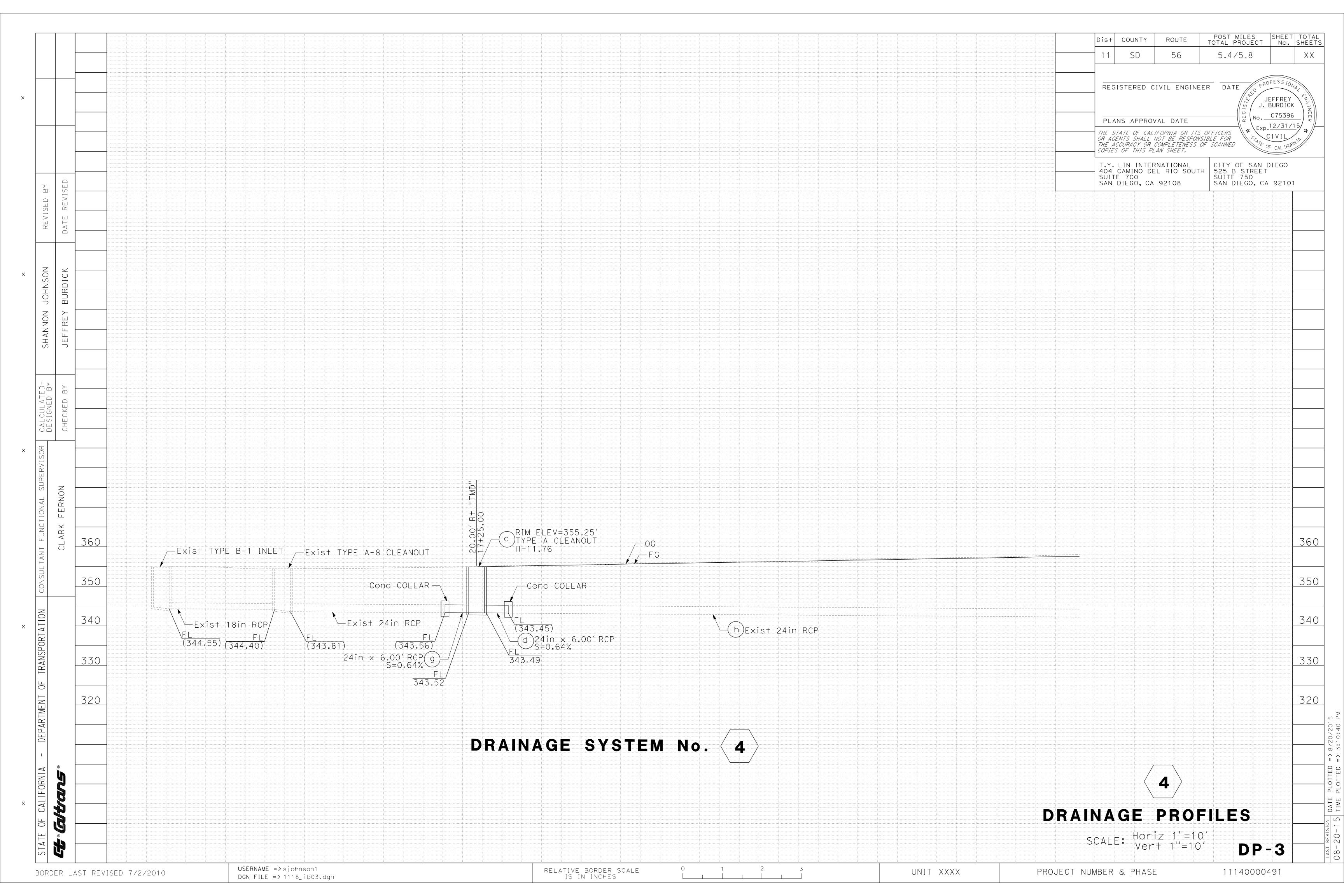


Appendix G Proposed Drainage Plan and Profiles

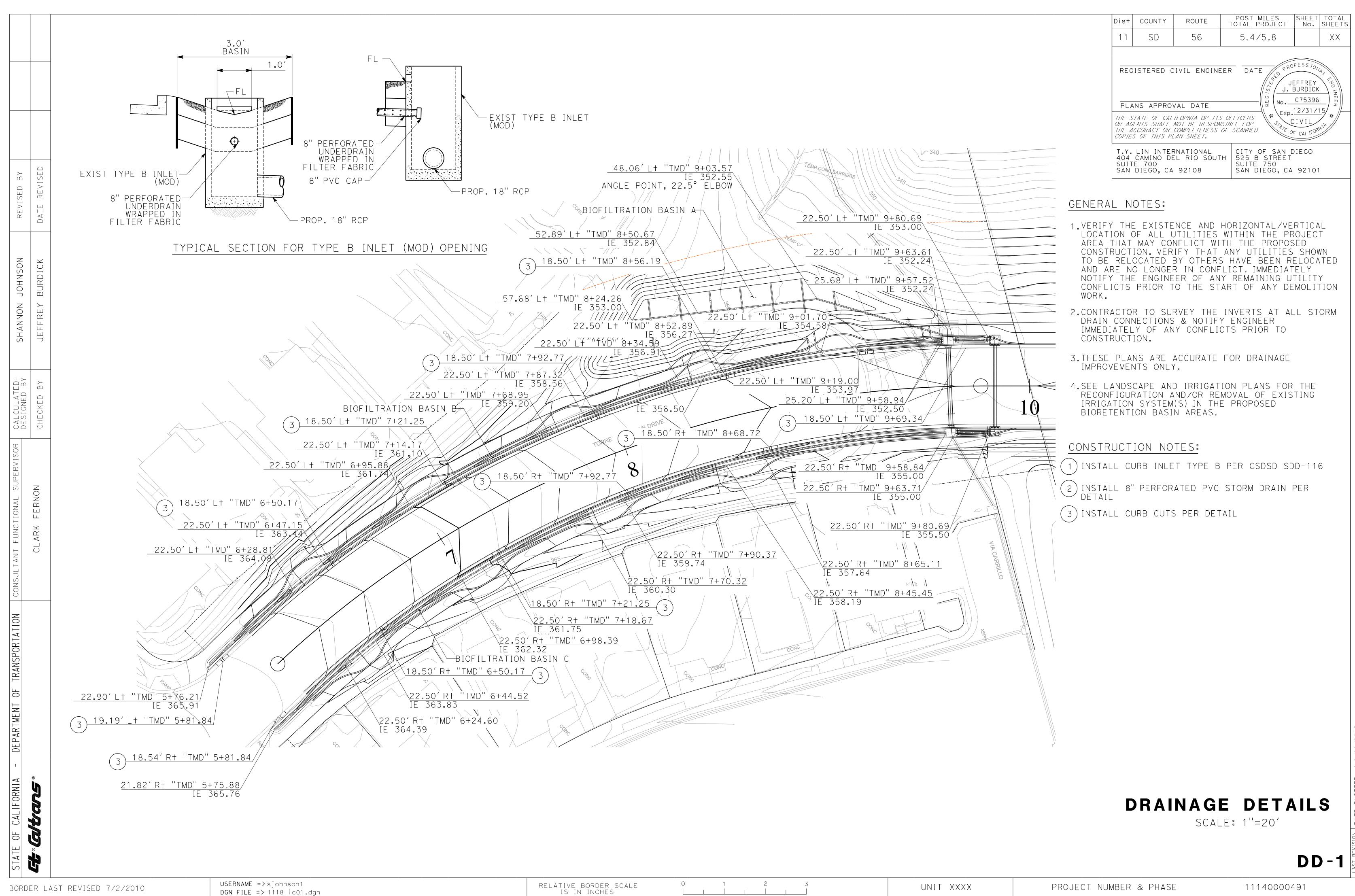








Appendix H Proposed Preliminary Hydro modification and Treatment Control BMP Map



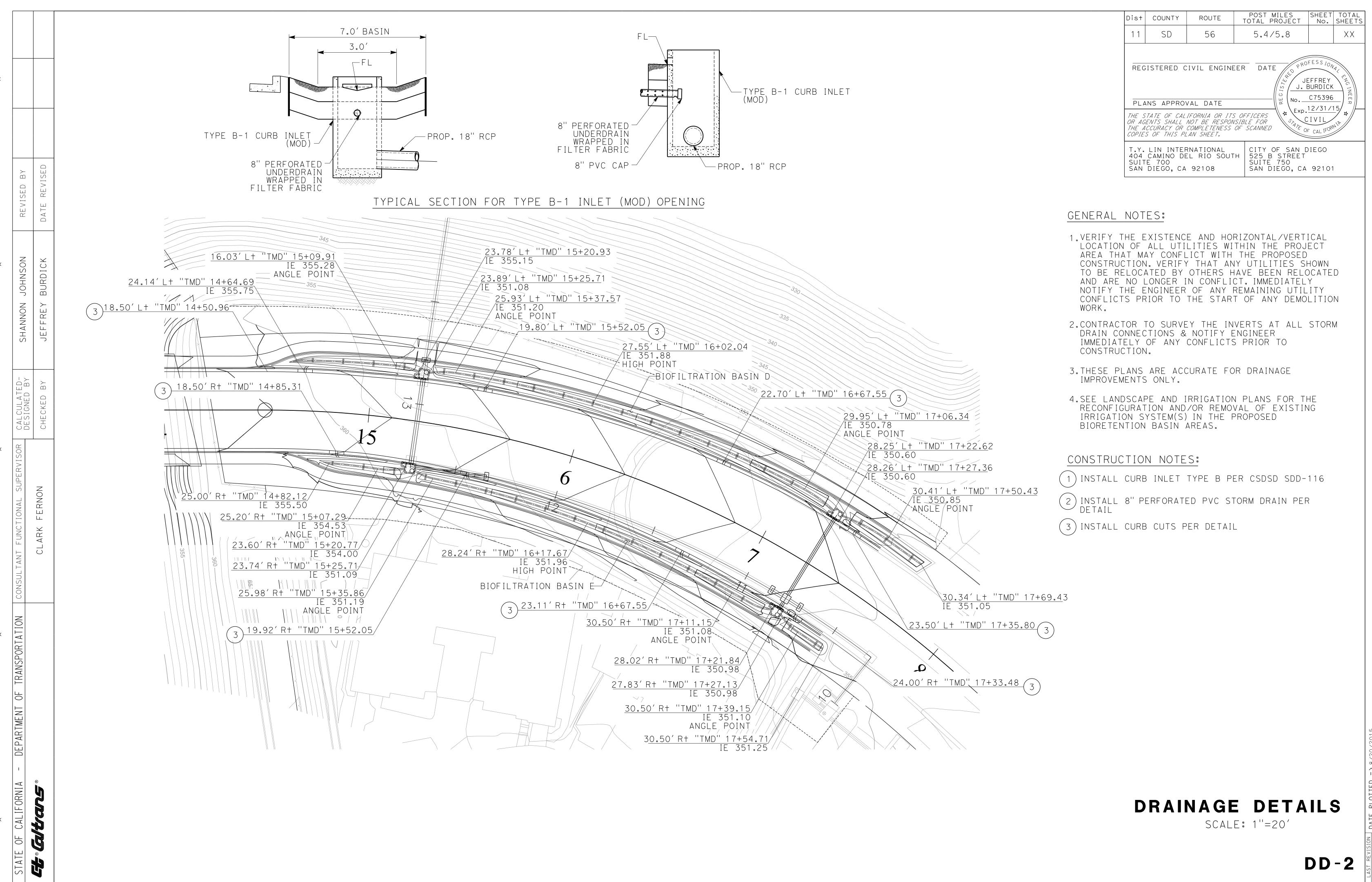
BORDER LAST REVISED 7/2/2010

DGN FILE => 1118_ic01.dgn

11140000491

PROJECT NUMBER & PHASE

UNIT XXXX



RELATIVE BORDER SCALE
IS IN INCHES

UNIT XXXX

PROJECT NUMBER & PHASE

11140000491

Appendix I Preliminary Hydro modification Analysis (BMP Sizing Calculator)

BMP Sizing Spreadsheet V1.04

Project Name:	Torrey Meadows Drive Overcrossing
Project Applicant:	T.Y. Lin International
Jurisdiction:	County of San Diego
Parcel (APN):	
Hydrologic Unit:	Penasquitos
Rain Gauge:	Oceanside
Total Project Area (sf):	116883.73
Channel Susceptibility:	High

BMP Sizing Spreadsheet V1.04							
Project Name:	orrey Meadows Drive Overcrossin	Penasquitos					
Project Applicant:	T.Y. Lin International	Rain Gauge:	Oceanside				
Jurisdiction:	County of San Diego	Total Project Area:	116883.73				
Parcel (APN):		Low Flow Threshold:	0.1Q2				
BMP Name:	BMP #1.1 (Basin A)	ВМР Туре:	Bioretention				
BMP Native Soil Type:	D	BMP Infiltration Rate (in/hr):	0.024				

		Areas D	raining to BMP			HMP Sizing Factors				Minimum BMP S	ize
DMA Name	Area (sf)	Soil Type	Slope	Post Project Surface Type	Runoff Factor (Table 4-2)	Surface Area	Surface Volume	Subsurface Volume	Surface Area (sf)	Surface Volume (cf)	Subsurface Volume (cf)
1.1	7100.415	D	Flat	Landscape	0.1	0.13	0.1083	0.078	92	77	55
1.2	12825.33	D	Flat	Concrete	1.0	0.13	0.1083	0.078	1667	1389	1000
Total BMP Area	19925.745						1	Minimum BMP Size	1759.598295	1466	1056
		1						Proposed BMP Size*	3835.03	2397	2301
								'	Soil Matrix Depth		in
								Minim	um Ponding Depth		in
									um Ponding Depth		in
									ted Ponding Depth		in

BMP's must be adapted and applied to the conditions specific to the development project such as unstable slopes or the lack of available head. Designated Staff have final review and approval authority over the project design.

BMP Sizing Spreadsheet V1.04							
Project Name: Meadows Drive Overcr Hydrologic Unit: Penasquitos							
Project Applicant:	T.Y. Lin International	Rain Gauge:	Oceanside				
Jurisdiction:	County of San Diego	Total Project Area:	116883.73				
Parcel (APN):		Low Flow Threshold:	0.1Q2				
BMP Name	BMP #1.1 (Basin A)	BMP Type:	Bioretention				

DMA	DMA Rain Gauge		Existing C	Condition	Q2 Sizing Factor	DMA Area (ac)	Orifice Flow - %Q ₂	Orifice Area (in2)
Name		Soil Type	Cover	Slope	(cfs/ac)		(cfs)	
1.1	Oceanside	D	Scrub	Flat	0.175	0.163	0.003	0.07
1.2	Oceanside	D	Scrub	Flat	0.175	0.294	0.005	0.13

0.008	0.20	0.50
Tot. Allowable	Tot. Allowable	Max Orifice
Orifice Flow	Orifice Area	Diameter
(cfs)	(in2)	(in)

0.008	0.20	0.50
Actual Orifice Flow	Actual Orifice Area	Selected
Actual Office Flow	Actual Offfice Area	Orifice Diameter
(cfs)	(in2)	(in)

Drawdown (Hrs)	66.2

BMP Sizing Spreadsheet V1.04							
Project Name:	orrey Meadows Drive Overcrossing	Hydrologic Unit:	Penasquitos				
Project Applicant:	T.Y. Lin International	Rain Gauge:	Oceanside				
Jurisdiction:	County of San Diego	Total Project Area:	116883.73				
Parcel (APN):		Low Flow Threshold:	0.1Q2				
BMP Name:	BMP #1.2 (Basin B)	ВМР Туре:	Bioretention				
BMP Native Soil Type:	D	BMP Infiltration Rate (in/hr):	0.024				

		Areas D	raining to BMP			HMP Sizing Factors			Minimum BMP Size		
DMA Name	Area (sf)	Soil Type	Slope	Post Project Surface Type	Runoff Factor (Table 4-2)	Surface Area	Surface Volume	Subsurface Volume	Surface Area (sf)	Surface Volume (cf)	Subsurface Volume (cf)
1.1	7100.415	D	Flat	Landscape	0.1	0.13	0.1083	0.078	92	77	55
1.2	12825.33	D	Flat	Concrete	1.0	0.13	0.1083	0.078	1667	1389	1000
Total BMP Area	19925.745						1	Minimum BMP Size	1759.598295	1466	1056
TOTAL BINIP Area	19925.745	1									1407
								Proposed BMP Size*	2344.31	1465	
								A 411	Soil Matrix Depth		in
									um Ponding Depth		in
									um Ponding Depth		in
								Selec	ted Ponding Depth	6.00	in

BMP's must be adapted and applied to the conditions specific to the development project such as unstable slopes or the lack of available head. Designated Staff have final review and approval authority over the project design.

BMP Sizing Spreadsheet V1.04							
Project Name:	Meadows Drive Overcr	Hydrologic Unit:	Penasquitos				
Project Applicant:	T.Y. Lin International	Rain Gauge:	Oceanside				
Jurisdiction:	County of San Diego	Total Project Area:	116883.73				
Parcel (APN):		Low Flow Threshold:	0.1Q2				
BMP Name	BMP #1.2 (Basin B)	BMP Type:	Bioretention				

DMA	Rain Gauge	0 11 7	Existing C		Q2 Sizing Factor	DMA Area (ac)	Orifice Flow - %Q ₂	Orifice Area (in2)
Name		Soil Type	Cover	Slope	(cfs/ac)		(cfs)	
1.1	Oceanside	D	Scrub	Flat	0.175	0.163	0.003	0.07
1.2	Oceanside	D	Scrub	Flat	0.175	0.294	0.005	0.13

0.008	0.20	0.50
Tot. Allowable	Tot. Allowable	Max Orifice
Orifice Flow	Orifice Area	Diameter
(cfs)	(in2)	(in)

0.008	0.20	0.50		
Actual Orifice Flow	Actual Orifice Area	Selected		
Actual Office Flow	Actual Offlice Area	Orifice Diameter		
(cfs)	(in2)	(in)		

Drawdown (F	Hrs)	40.5

	BMP Sizing Spreadsheet V1.04								
Project Name:	orrey Meadows Drive Overcrossing	Penasquitos							
Project Applicant:	T.Y. Lin International	Rain Gauge:	Oceanside						
Jurisdiction:	County of San Diego	Total Project Area:	116883.73						
Parcel (APN):		Low Flow Threshold:	0.1Q2						
BMP Name:	BMP #2 (Basin C)	ВМР Туре:	Bioretention						
BMP Native Soil Type:	D	BMP Infiltration Rate (in/hr):	0.024						

		Areas D	raining to BMP			HMP Sizing Factors			Minimum BMP Size		
DMA Name	Area (sf)	Soil Type	Slope	Post Project Surface Type	Runoff Factor (Table 4-2)	Surface Area	Surface Volume	Subsurface Volume	Surface Area (sf)	Surface Volume (cf)	Subsurface Volume (cf)
2.1	6662.17	D	Flat	Landscape	0.1	0.13	0.1083	0.078	87	72	52
2.2	27813.29	D	Flat	Concrete	1.0	0.13	0.1083	0.078	3616	3012	2169
Total BMP Area	34475.46						J.	Minimum BMP Size	3702.33591	3084	2221
TOTAL DIVIP ATEA	34473.40							Proposed BMP Size*	2218.81	1109	1331
								Proposed bivir size			
								A dimina	Soil Matrix Depth		in
									um Ponding Depth um Ponding Depth		in
									ted Ponding Depth		in
								Selec	tea Ponding Depth	0.00	in

BMP's must be adapted and applied to the conditions specific to the development project such as unstable slopes or the lack of available head. Designated Staff have final review and approval authority over the project design.

BMP Sizing Spreadsheet V1.04								
Project Name:	Meadows Drive Overcr	Hydrologic Unit:	Penasquitos					
Project Applicant:	T.Y. Lin International	Rain Gauge:	Oceanside					
Jurisdiction:	County of San Diego	Total Project Area:	116883.73					
Parcel (APN):		Low Flow Threshold:	0.1Q2					
BMP Name	BMP #2 (Basin C)	BMP Type:	Bioretention					

DMA Name	Rain Gauge	Soil Type	Existing C Cover	ondition Slope	Q2 Sizing Factor (cfs/ac)	DMA Area (ac)	Orifice Flow - %Q ₂ (cfs)	Orifice Area (in2)
2.1	Oceanside	D	Scrub	Flat	0.175	0.153	0.003	0.07
2.2	Oceanside	D	Scrub	Flat	0.175	0.639	0.011	0.27
_								

0.014	0.34	0.66		
Tot. Allowable	Tot. Allowable	Max Orifice		
Orifice Flow	Orifice Area	Diameter		
(cfs)	(in2)	(in)		

0.008	0.20	0.50		
Actual Orifice Flow	Actual Orifice Area	Selected Orifice Diameter		
(cfs)	(in2)	(in)		

Drawdown (Hrs)	38.3	

BMP Sizing Spreadsheet V1.04								
Project Name:	orrey Meadows Drive Overcrossing	Penasquitos						
Project Applicant:	T.Y. Lin International	Rain Gauge:	Oceanside					
Jurisdiction:	County of San Diego	Total Project Area:	116883.73					
Parcel (APN):		Low Flow Threshold:	0.1Q2					
BMP Name:	BMP #3 (Basin D)	ВМР Туре:	Bioretention					
BMP Native Soil Type:	D	BMP Infiltration Rate (in/hr):	0.024					

		Areas D	raining to BMP				HMP Sizing Fa	ctors	Minimum BMP Size		
DMA Name	Area (sf)	Soil Type	Slope	Post Project Surface Type	Runoff Factor (Table 4-2)	Surface Area	Surface Volume	Subsurface Volume	Surface Area (sf)	Surface Volume (cf)	Subsurface Volume (cf)
3.1	8191.52	D	Flat	Landscape	0.1	0.13	0.1083	0.078	106	89	64
3.2	13579.29	D	Flat	Concrete	1.0	0.13	0.1083	0.078	1765	1471	1059
									.		
Total BMP Area	21770.81						1	Minimum BMP Size	1871.79746	1559	1123
TOTAL DIVIF ATEA	21/70.01	J						Proposed BMP Size*	2987.61	1494	1793
								1 Toposca Bivir Size	Soil Matrix Depth		in
								Minim	um Ponding Depth		in
									um Ponding Depth		in
									ted Ponding Depth		in
								Selec	tea i onanig Deptii	0.00	
											l

BMP's must be adapted and applied to the conditions specific to the development project such as unstable slopes or the lack of available head. Designated Staff have final review and approval authority over the project design.

	BMP	Sizing Spreadsheet V1.0	04
Project Name:	Meadows Drive Overcr	Hydrologic Unit:	Penasquitos
Project Applicant:	T.Y. Lin International	Rain Gauge:	Oceanside
Jurisdiction:	County of San Diego	Total Project Area:	116883.73
Parcel (APN):		Low Flow Threshold:	0.1Q2
BMP Name	BMP #3 (Basin D)	BMP Type:	Bioretention

DMA	Rain Gauge	Soil Type	Existing C	ondition Slope	Q2 Sizing Factor (cfs/ac)	DMA Area (ac)	Orifice Flow - %Q ₂	Orifice Area (in2)
Name		3011 Type	Cover	Siope	(CIS/aC)		(cfs)	
3.1	Oceanside	D	Scrub	Flat	0.175	0.188	0.003	0.08
3.2	Oceanside	D	Scrub	Flat	0.175	0.312	0.005	0.13

0.009	0.21	0.52
Tot. Allowable	Tot. Allowable	Max Orifice
Orifice Flow	Orifice Area	Diameter
(cfs)	(in2)	(in)

0.008	0.20	0.50
Actual Orifice Flow	Actual Orifice Area	Selected
Actual Offfice Flow	Actual Offlice Area	Orifice Diameter
(cfs)	(in2)	(in)

Drawdown (Hrs)	51.6

BMP Sizing Spreadsheet V1.04						
Project Name:	orrey Meadows Drive Overcrossing	Penasquitos				
Project Applicant:	T.Y. Lin International	Rain Gauge:	Oceanside			
Jurisdiction:	County of San Diego	Total Project Area:	116883.73			
Parcel (APN):		Low Flow Threshold:	0.1Q2			
BMP Name:	BMP #4 (Basin E)	ВМР Туре:	Bioretention			
BMP Native Soil Type:	D	BMP Infiltration Rate (in/hr):	0.024			

		Areas D	raining to BMP				HMP Sizing Fa	ctors		Minimum BMP S	ize
DMA Name	Area (sf)	Soil Type	Slope	Post Project Surface Type	Runoff Factor (Table 4-2)	Surface Area	Surface Volume	Subsurface Volume	Surface Area (sf)	Surface Volume (cf)	Subsurface Volume (cf)
4.1	7638.55	D	Flat	Landscape	0.1	0.13	0.1083	0.078	99	83	60
4.2	13147.43	D	Flat	Concrete	1.0	0.13	0.1083	0.078	1709	1424	1025
T-+-I DAAD A	20705.00							Minimum DNAD Cina	1000 16705	4507	4005
Total BMP Area	20785.98	J						Minimum BMP Size	1808.46705	1507	1085
								Proposed BMP Size*	2427.08	1214	1456
									Soil Matrix Depth		in
									um Ponding Depth		in
									um Ponding Depth		in .
								Selec	ted Ponding Depth	6.00	in

BMP's must be adapted and applied to the conditions specific to the development project such as unstable slopes or the lack of available head. Designated Staff have final review and approval authority over the project design.

BMP Sizing Spreadsheet V1.04						
Project Name:	Meadows Drive Overcr	Hydrologic Unit:	Penasquitos			
Project Applicant:	T.Y. Lin International	Rain Gauge:	Oceanside			
Jurisdiction:	County of San Diego	Total Project Area:	116883.73			
Parcel (APN):		Low Flow Threshold:	0.1Q2			
BMP Name	BMP #4 (Basin E)	BMP Type:	Bioretention			

DMA Name	Rain Gauge	Soil Type	Existing C Cover	Condition Slope	Q2 Sizing Factor (cfs/ac)	DMA Area (ac)	Orifice Flow - %Q ₂ (cfs)	Orifice Area (in2)
4.1	Oceanside	D	Scrub	Flat	0.175	0.175	0.003	0.07
4.2	Oceanside	D	Scrub	Flat	0.175	0.302	0.005	0.13

0.008	0.20	0.51
Tot. Allowable	Tot. Allowable	Max Orifice
Orifice Flow	Orifice Area	Diameter
(cfs)	(in2)	(in)

0.008	0.20	0.50
Actual Orifice Flow	Actual Orifice Area	Selected
Actual Office Flow	Actual Offlice Area	Orifice Diameter
(cfs)	(in2)	(in)

Drawdown (F	lrs)	41.9	

Appendix J
Simple Sizing Method for Biofiltration BMPs



DMA 1

Simple Sizing Method for Biofiltration BMPs Model BMP Desi	Worksheet B-5.1 Model BMP Design Manual January 2015			
1 Remaining DCV after implementing retention BMPs	2413.73	cubic-feet		
Partial Retention				
2 Infiltration rate from Worksheet D.5-1 if partial infiltration is feasible	0	in/hr		
3 Allowable drawdown time for aggregate storage below the underdrain	36	hours		
4 Depth of runoff that can be infiltrated [Line 2 x Line 3]	0	inches		
5 Aggregate pore space	0.4	in/in		
6 Required depth of gravel below the underdrain [Line 4/ Line 5]	0	inches		
7 Assumed surface area of the biofiltration BMP		sq-ft		
8 Media retained pore space	0.1	in/in		
9 Volume retained by BMP [[Line 4 + (Line 12 x Line 8)]/12] x Line 7	0	cubic-feet		
10 DCV that requires biofiltration [Line 1 -Line 9]	2413.725	cubic-feet		
BMP Parameters				
11 Surface Ponding [6 inch minimum, 12 inch maximum]	6	inches		
12 Media Thickness [18 inches minimum]	24	inches		
Aggregate Storage above underdrain invert (12 inches typical)- use 0 inches for sizing if the aggregate is not over the entire bottom surface area 14 Media available pore space 15 Media filtration rate to be used for sizing	12 0.2 5	inches in/in in/hr		
Baseline Calculations		111/111		
16 Allowable Routing Time for sizing	6	hours		
17 Depth filtered during storm [Line 15 x Line 16]	30	inches		
Depth of Detention Storage 18 [Line 11 +(Line 12 x Line 14) + (Line 13 x Line 15)] 19 Total Depth Treated [Line 17 + Line 18]	70.8 100.8	inches inches		
Option 1-Biofilter 1.5 times the DCV	•			
20 Required biofiltered volume [1.5 x Line 10]	3620.588	cubic-feet		
21 Required Footprint [Line 20/Line 19] x 12	431.0224	sq-ft		
Option 2-Store 0.75 of remaining DCV in pores and ponding				
20 D 1 10 (C) XX 1 F0 75 X1 101	1810.294			
22 Required Storage (surface + pores) Volume [0.75 x Line 10]	1010.294	cubic-feet		
22 Required Storage (surface + pores) Volume [0.75 x Line 10] 23 Required Footprint [Line 22/Line 18] x 12	306.8295	cubic-feet sq-ft		
23 Required Footprint [Line 22/Line 18] x 12				

DMA 2

Simple Sizing Method for Biofiltration BMPs Model BM	Worksheet B-5.1 Model BMP Design Manual January 2015			
1 Remaining DCV after implementing retention BMPs	1661.21	cubic-feet		
Partial Retention	1001.21	cusic feet		
2 Infiltration rate from Worksheet D.5-1 if partial infiltration is feasible	e 0	in/hr		
3 Allowable drawdown time for aggregate storage below the underdrain		hours		
4 Depth of runoff that can be infiltrated [Line 2 x Line 3]	0	inches		
5 Aggregate pore space	0.4	in/in		
6 Required depth of gravel below the underdrain [Line 4/ Line 5]	0	inches		
7 Assumed surface area of the biofiltration BMP		sq-ft		
8 Media retained pore space	0.1	in/in		
9 Volume retained by BMP [[Line 4 + (Line 12 x Line 8)]/12] x Line 7	7 0	cubic-feet		
10 DCV that requires biofiltration [Line 1 -Line 9]	1661.215	cubic-feet		
BMP Parameters				
11 Surface Ponding [6 inch minimum, 12 inch maximum]	6	inches		
12 Media Thickness [18 inches minimum]	18	inches		
Aggregate Storage above underdrain invert (12 inches typical)- use 0) inches			
13 for sizing if the aggregate is not over the entire bottom surface area	12	inches		
14 Media available pore space	0.2	in/in		
15 Media filtration rate to be used for sizing	5	in/hr		
Baseline Calculations				
16 Allowable Routing Time for sizing	6	hours		
17 Depth filtered during storm [Line 15 x Line 16]	30	inches		
Depth of Detention Storage				
18 [Line 11 +(Line 12 x Line 14) + (Line 13 x Line 15)]	69.6	inches		
19 Total Depth Treated [Line 17 + Line 18]	99.6	inches		
Option 1-Biofilter 1.5 times the DCV	•			
20 Required biofiltered volume [1.5 x Line 10]	2491.822	cubic-feet		
21 Required Footprint [Line 20/Line 19] x 12	300.2196	sq-ft		
Option 2-Store 0.75 of remaining DCV in pores and ponding		-		
22 Required Storage (surface + pores) Volume [0.75 x Line 10]	1245.911	cubic-feet		
23 Required Footprint [Line 22/Line 18] x 12	214.8123	sq-ft		
Footprint of the BMP				
24 Impervious area draining to the BMP	27813.29	sq-ft		
25 Footprint of the BMP = Minimum (Line 21, Line 23, 3% of Line 24)	214.81	sq-ft		

DMA 3

Simple Sizing Method for Biofiltration BMPs	Worksheet B-5.1 Model BMP Design Manual January 2015			
1 Remaining DCV after implementing retention BM	MPs	1014.83	cubic-feet	
Partial Retention				
2 Infiltration rate from Worksheet D.5-1 if partial i		0	in/hr	
3 Allowable drawdown time for aggregate storage		36	hours	
4 Depth of runoff that can be infiltrated [Line 2 x L	Line 3]	0	inches	
5 Aggregate pore space		0.4	in/in	
6 Required depth of gravel below the underdrain [I	Line 4/ Line 5]	0	inches	
7 Assumed surface area of the biofiltration BMP			sq-ft	
8 Media retained pore space		0.1	in/in	
9 Volume retained by BMP [[Line 4 + (Line 12 x I	Line 8)]/12] x Line 7	0	cubic-feet	
10 DCV that requires biofiltration [Line 1 -Line 9]		1014.825	cubic-feet	
BMP Parameters				
11 Surface Ponding [6 inch minimum, 12 inch maximum, 12 i	mum]	6	inches	
12 Media Thickness [18 inches minimum]		18	inches	
Aggregate Storage above underdrain invert (12 in	nches typical)- use 0 inches			
13 for sizing if the aggregate is not over the entire be	ottom surface area	12	inches	
14 Media available pore space		0.2	in/in	
15 Media filtration rate to be used for sizing		5	in/hr	
Baseline Calculations				
16 Allowable Routing Time for sizing		6	hours	
17 Depth filtered during storm [Line 15 x Line 16]		30	inches	
Depth of Detention Storage				
18 [Line 11 +(Line 12 x Line 14) + (Line 13 x Line	15)]	69.6	inches	
19 Total Depth Treated [Line 17 + Line 18]	· •	99.6	inches	
Option 1-Biofilter 1.5 times the DCV				
20 Required biofiltered volume [1.5 x Line 10]		1522.238	cubic-feet	
21 Required Footprint [Line 20/Line 19] x 12		183.4021	sq-ft	
Option 2-Store 0.75 of remaining DCV in pores an	nd ponding			
22 Required Storage (surface + pores) Volume [0.75		761.1188	cubic-feet	
23 Required Footprint [Line 22/Line 18] x 12	-	131.2274	sq-ft	
Footprint of the BMP				
24 Impervious area draining to the BMP		13579.29	sq-ft	
25 Footprint of the BMP = Minimum (Line 21, Line	23, 3% of Line 24)	131.23	sq-ft	

DMA 4

Simple Sizing Method for Biofiltration BMPs	Model BMP Desi January 2	Worksheet B-5.1 Model BMP Design Manual January 2015			
1 Remaining DCV after implementing retention B	MPs	973.94	cubic-feet		
Partial Retention					
2 Infiltration rate from Worksheet D.5-1 if partial i		0	in/hr		
3 Allowable drawdown time for aggregate storage		36	hours		
4 Depth of runoff that can be infiltrated [Line 2 x I	Line 3]	0	inches		
5 Aggregate pore space		0.4	in/in		
6 Required depth of gravel below the underdrain [l	Line 4/ Line 5]	0	inches		
7 Assumed surface area of the biofiltration BMP			sq-ft		
8 Media retained pore space		0.1	in/in		
9 Volume retained by BMP [[Line 4 + (Line 12 x l	Line 8)]/12] x Line 7	0	cubic-feet		
10 DCV that requires biofiltration [Line 1 -Line 9]		973.9421	cubic-feet		
BMP Parameters					
11 Surface Ponding [6 inch minimum, 12 inch maxi	imum]	6	inches		
12 Media Thickness [18 inches minimum]	12 Media Thickness [18 inches minimum]				
Aggregate Storage above underdrain invert (12 in	nches typical)- use 0 inches				
13 for sizing if the aggregate is not over the entire b	ottom surface area	12	inches		
14 Media available pore space		0.2	in/in		
15 Media filtration rate to be used for sizing		5	in/hr		
Baseline Calculations					
16 Allowable Routing Time for sizing		6	hours		
17 Depth filtered during storm [Line 15 x Line 16]		30	inches		
Depth of Detention Storage					
18 [Line 11 +(Line 12 x Line 14) + (Line 13 x Line	15)]	69.6	inches		
19 Total Depth Treated [Line 17 + Line 18]		99.6	inches		
Option 1-Biofilter 1.5 times the DCV					
20 Required biofiltered volume [1.5 x Line 10]		1460.913	cubic-feet		
21 Required Footprint [Line 20/Line 19] x 12		176.0136	sq-ft		
Option 2-Store 0.75 of remaining DCV in pores an	nd ponding				
22 Required Storage (surface + pores) Volume [0.75]	5 x Line 10]	730.4566	cubic-feet		
23 Required Footprint [Line 22/Line 18] x 12		125.9408	sq-ft		
Footprint of the BMP					
24 Impervious area draining to the BMP		13147.43	sq-ft		
25 Footprint of the BMP = Minimum (Line 21, Line	e 23, 3% of Line 24)	125.94	sq-ft		

Appendix K
BMP Inspection, Operation and Maintenance
Plan

PERMANENT BMP INSPECTION, OPERATION, AND MAINTENANCE REQUIREMENTS:

ВМР	ROUTINE ACTION	MAINTENANCE INDICATOR	MAINTENANCE ACTIVITY	FREQUENCY	RESPONSIBLE PARTY
Bioretention	Inspection of bioretention	Visual observation for	Remove sediment, trash and	2/year. Prior to the	Owner
	facilities	evidence of erosion,	debris to prevent clogging	start and at the end	
		standing water, trash and	and standing water. Prune	of the wet season.	
		debris, sediment, clogging,	and weed excessive		
		and condition of	vegetation. Repair		
		vegetation.	bioretention basin to ensure		
			proper function.		

	BMP: Bioretention Area MAINTENANCE ACTIVITIES												
ROUTINE ACTION	MAINTENANCE INDICATOR	FIELD MEASUDEMENT	MEASUREMENT FREQUENCY	MAINTENANCE ACTIVITY	Frequency (# of times per year)	Hours per Event	Average Labor Crew Size	Avg. (Pro- Rated) Labor Rate/Hr. (\$)	Equipment	Equipment Cost/Hour (\$)	Materials & Incidentals Cost or Disposal Cost/Event (\$)	Total cost per visit (\$)	Total cost per year (\$)
Vegetation Management for Aesthetics (optional)	Average vegetation height greater than 12-inches, emergence of trees or woody vegetation,	side slope area	Annually, prior to start of wet season	Cut vegetation to an average height of 6-inches and remove trimmings. Remove any trees, or woody vegetation.	1.0	2.0	2	\$ 74.97	Utility Truck	\$ 14.39	\$ 50.00	\$ 379	\$ 379
Soil Repair	Evidence of erosion	Visual observation	Annually, prior to start of wet season	Reseed/revegetate barren spots prior to wet season.	1.0	4.0	2	\$ 74.97	Utility Truck	\$ 14.39	\$ 150.00	\$ 807	\$ 807
Standing Water	Standing water for more than 96 hrs	Visual observation	Annually, 96 hours after a target storm (0.60 in) event	Drain facility. Corrective action prior to wet season. Consult engineers if immediate solution is not evident.	1.0	1.0	2	\$ 74.97	Utility Truck	\$ 14.39		\$ 164	\$ 164
Trash and Debris	Trash and Debris present	Visual observation	Annually, prior to start of wet season	Remove and dispose of trash and debris	1.0	2.0	2	\$ 74.97	Utility Truck	\$ 14.39		\$ 329	\$ 329
Sediment Management	Sediment depth exceeds 10% of the facility design	Measure depth at apparent maximum and minimum	Annually, prior to start of wet season	Remove and properly dispose of sediment. Regrade if necessary. (expected every 2 years)	0.5	8.0	2	\$ 74.97	Utility Truck, 10-15 yd Truck, Backhoe	\$ 56.02	\$ 400.00	\$ 2,048	\$ \$ 1,024
Underdrains	Evidence of Clogging	Visual Observation	Annually, prior to start of wet season	Corrective action prior to wet season. Consult engineers if immediate solution is not evident.	1.0	0.5	2	\$ 74.97	Utility Truck	\$ 14.39		\$ 82	\$ 82
General Maintenance Inspection	inlet structures, outlet structures, side slopes or other features damaged, significant erosion, burrows, emergence of trees or woody vegetation, graffiti or vandalism, fence damage, etc.	Visual observation	Annually, prior to start of wet season	Corrective action prior to wet season. Consult engineers if immediate solution is not evident.	1.0	1.0	2	\$ 74.97	Utility Truck	\$ 14.39		\$ 164	\$ 164
Reporting				•	1.0	3.0	1	\$ 74.97				\$ 225	T
				Average Annual Total		32.0							\$ 3,174

Equipment	Equipment Cost
Utility Truck	\$14.39/hr
10-15 yd truck	\$28.27/hr
Backhoe	\$13.36/hr
Vactor	\$62.70/hr
Sweeper	\$123.26/hr

\$74.97/hr

Labor Rate

Small Bioretention (500 sf)	32.0	\$ 3,174
Medium Bioretention (2000 sf)	44.0	\$ 4,078
Large Bioretention (4000 sf)	68.0	\$ 5,877

Appendix L
Drainage Study





Torrey Meadows Drive

DRAFT Drainage Study

August 2015

Prepared by: T.Y. Lin International 404 Camino Del Rio South, Suite 700 San Diego, Ca 92108 (619) 692-1920

Prepared for:



City of San Diego 525 B Street, Suite 750 San Diego, Ca 92101

Caltrans District 11 4050 Taylor Street San Diego, 92110

	<u> </u>	
Jeff Burdick, P.E.	DATE	
REGISTERED CIVIL ENGINEER		



Table of Contents

L	IST OF APPENDICES	ii
Α	ACRONYMS	iv
1.	INTRODUCTION	
1.1	Study Overview and Purpose	1
1.2		
1.3	Existing Site Description	2
1.4	Hydrologic Setting	2
1.5	FÉMA Flood Plain Information	2
2.	METHODOLOGY	
2.1	Compliance with Regulations	3
2.2		
2.3	, ,	
2.4		
3.	EXISTING DRAINAGE CONDITIONS	
4.	PROPOSED DRAINAGE CONDITIONS	8
5.	CONCLUSION	9
6	REFERENCES	c



LIST OF APPENDICES

APPENDIX A: VICINITY MAP AND FEMA FIRMETTE

APPENDIX B: EXISTING CONDITION HYDROLOGIC ANALYSES, AS-BUILTS, AND MAP

APPENDIX C: PROPOSED CONDITION HYDROLOGIC ANALYSES AND MAPS

APPENDIX D: DRAINAGE PLANS AND PROFILES

APPENDIX E: PROPOSED PRELIMINARY HYDRO MODIFICATION AND TREATMENT

CONTROL BMP MAP



ABBREVIATIONS

ac Acre(s) ac-ft Acre feet

cfs Cubic feet per second

CY Cubic yard(s)

ft Feet in Inch(es)

in/hr Inch(es) per hour

min Minute(s) SF Square feet

ACRONYMS

A Drainage Area
C Runoff Coefficient
cfs Cubic feet per second

FEMA Federal Emergency Management Agency

FHWA Federal Highway Administration FIRM FEMA Flood Insurance Rate Maps

FS Finished Surface
HGL Hydraulic Grade Line
HSG Hydrologic Soil Groups

I Rainfall Intensity

MODRAT Modified Rational Method

NOAA National Oceanic and Atmospheric Administration

NRCS Natural Resources Conservation Service

P₂₄ 24-Hour Precipitation Q Discharge / Runoff

RCP Reinforced Concrete Pipe

ROW Right-of-way

SCS Soil Conservation Service T_c Time of Concentration

TC Top of Curb

USDOT United States Department of Transportation

USLE Universal Soil Loss Equation

V Volume



1. INTRODUCTION

1.1 Study Overview and Purpose

Project Purpose and Description

The City of San Diego, in cooperation with the California Department of Transportation (Caltrans) District 11 and Kilroy Realty, is evaluating alternatives to connect segments of Torrey Meadows Drive to the north and south of State Route 56 (SR-56) with a bridge over the highway. The project proposes to construct a bridge overcrossing SR-56 0.5 miles west of Camino del Sur (PM 6.12) in the Torrey Highlands community of San Diego.

The purpose of the project is to connect the divided community of Torrey Highlands, which is currently bisected by SR-56. In addition, the execution of this project would physically integrate Torrey Highlands to the greater Rancho Peñasquitos and Santaluz communities north of SR-56. The proposed bridge would provide residents an alternative way of entering and leaving their cul-de-sac community.

Purpose of Study

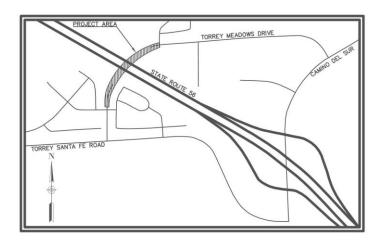
The objectives of this drainage study are as follows:

- To quantify the magnitude and frequency of flows from tributary areas including new systems for off-site and on-site flows.
- Ensure the design storm is conveyed without causing objectionable backwater or tailwater, damage to surrounding properties, excessive flow velocities, excessive scour, impacts to traffic, hydroplaning effects, or flooding of other facilities.

1.2 Location

The project is located in San Diego County in the City of San Diego on SR-56 0.5 miles feet west of Camino del Sur (PM 6.12) in the Torrey Highlands community.

Figure 1: Location Map





1.3 Existing Site Description

Torrey Meadows Drive is a collector street located in a mixed-use development overlooking State Route 56. Currently, Torrey Meadows Drive is 40' wide with on-street parking allowed along the entirety of both segments. Torrey Meadows Drive is on relatively flat terrain and is located 35 feet above SR-56, forming a depression between both segments. The gap between the north and south segments of Torrey Meadows Drive is traversed by SR-56, the SR-56 Bike Trail, a drainage ditch, and two slopes with grades steeper than 4:1. North of SR-56, Torrey Meadows Drive can only be accessed through Camino Del Sur and Via Sabbia. Similarly, south of SR-56, Torrey Meadows Drive is only accessible via Torrey Santa Fe Road. At this moment, there are no signalized intersections within the project limits, or within immediate proximity to the site.

1.4 Hydrologic Setting

The project is located within an area designated by the San Diego Regional Water Quality Control Board as the Peñasquitos Hydrologic Unit, in the Miramar Reservoir Hydrologic Area, identified as Hydrologic Sub-Area 906.10. More specifically, the project is located within the Carmel Valley-Poway Creek Watershed. The watershed encompassing the project area drains into McGonigle Canyon Creek, a tributary of Poway Creek, which discharges directly into the Pacific Ocean.

Runoff from local streets is conveyed by curb and gutter to numerous storm drain inlets which ultimately discharge into McGonigle Canyon Creek. Prior to discharge into McGonigle Canyon Creek, storm water is treated in a series of Vortechnics hydrodynamic separator treatment facilities.

Runoff in State Route 56 is conveyed by concrete and grass lined drainage swales into grated inlets along the shoulders of the highway. The grated inlets connect to storm drains that flow under SR-56 to a concrete-lined drainage ditch that runs along the centerline of the roadway. Finally, runoff collected in the drainage ditch is flows west along the median to its final discharge point at McGonigle Canyon.

1.5 FEMA Flood Plain Information

The FEMA Flood Insurance Rate Maps (FIRM) show that the project area lies in Zone X (See **Appendix A**). Zone X delineates areas of 0.2% annual chance flood, areas of 1% annual chance flood with average depths of less than one foot, or with drainage areas less than one square mile.



2. METHODOLOGY

2.1 Compliance with Regulations

All rainfall, storm runoff, storm drain capacity calculations, and detention calculations comply with the criteria for design outlined in the latest version of the Caltrans' Highway Design Manual (HDM).

2.2 Hydrologic Criteria

Existing Conditions

Due to the recent development of the Torrey Highlands property, the Shaw Properties, the LMXU property, and the recent construction of SR-56, the existing hydrology within the project area is well documented. The existing hydrology studies prepared for the associated developments are intended to facilitate full build-out conditions, and the existing drainage facilities were designed to convey the 100-year storm event. Therefore, limited existing drainage condition calculations were performed, and 100-year storm event peak discharges were determined from the associated drainage studies and as-builts. The existing drainage studies have been reviewed and incorporated into this study. The as-built information showing the existing 100-year storm event peak discharges are attached in **Appendix B**.

Design Storm

The HDM separates runoff into two categories: roadway drainage and cross drainage. Roadway drainage, consisting of storm water collected, conveyed and removed from the traveled way, shoulders and adjacent regions, is facilitated by inlets, asphalt dikes, curb and gutters, overside drains and roadside ditches. These drainage structures are designed for the 25-year storm event with allowable water spread less than the shoulder width. Cross drainage, which describes storm water transferred from one side of a roadway to the other, is conveyed through cross culverts. The designs storm for cross drainage are typically the 10-year and 100-year events.

The design storms analyzed for this study were the 25-year frequency storm event for roadway drainage and the 100-year frequency storm event for sizing of drainage systems.

Time of Concentration

The time of concentration (T_c) is the time it takes for rain in the most hydrologically remote part of the watershed to reach the outlet. It is the cumulative sum of travel times required for sheet flow, shallow concentrated flow and channel flow. The recommended minimum time of concentration is 5 minutes.

Sheet Flow

As described in Section 816.6 of the HDM, sheet flow is flow of uniform depth over plane surfaces and usually occurs for some distance after rain falls on the ground. The maximum flow depth is usually less than 0.8 inches - 1.2 inches. For unpaved areas, sheet flow normally exists for a distance less than 80 feet - 100 feet. An upper limit of 300 feet is recommended for paved areas. Travel time for sheet flow can be estimated using the Kinematic Wave Solution:



$$T_{t(sh)} = \frac{0.42 * L^{4/5} * n^{4/5}}{P_2^{1/2} * S^{2/5}}$$

Where: $T_{t(sh)}$ = Sheet flow travel time in minutes

L = Length of flow path length in feet

n = Manning's roughness coefficient (HDM Table 816.6A)

 P_2 = 2-year, 24-hour rainfall depth in inches (NOAA Atlas 14, Volume 6, V2)

S = Slope of flow path in ft/ft

Shallow Concentrated Flow

As described in Section 816.6 of the HDM, shallow concentrated flow occurs after short distances when sheet flow tends to concentrate in rills and gullies. At this point, the Upland Method is typically used when calculating velocity for shallow concentrated flow. Average velocities for the Upland Method can be taken directly from HDM Figure 816.6 or may be calculated from the following equation:

$$V = 3.28 * k * S^{1/2}$$

Where: V = Velocity in ft/sec

k = Intercept Coefficient (HDM Table 816.6B)

S = Slope of flow path in ft/ft

Travel time can be calculated from the following equation:

$$T_{t(sc)} = \frac{L}{60 * V}$$

Where: $T_{t(sc)}$ = Shallow concentrated flow travel time in minutes

V = Velocity in ft/sec

L = Length of flow path length in feet

Channel Flow

Channel Flow travel times can be estimated using the Manning Equation if the channel characteristics and geometry are known.

$$V = \frac{1.486 * R^{2/3} * S^{1/2}}{n}$$

Where: V = Mean velocity in ft/sec

n = Manning's roughness coefficient (HDM Table 864.3A)

S = Slope of flow path in ft/ft

R = Hydraulic Radius (feet) which is equivalent to A/WP

A = Cross-sectional area (sqft) WP = Wetted perimeter (feet)



Travel time for channel flow can be calculated as follows:

$$T_{t(ch)} = \frac{L}{60 * V}$$

Where: $T_{t(ch)}$ = Channel Flow travel time in minutes

V = Velocity in ft/sec

L = Length of flow path length in feet

Peak Discharge

The Rational Method was utilized to estimate the peak discharge (Q) for all design flows. The Rational Method was selected since all drainage areas are substantially smaller than 300 acres. According to the HDM, the Rational Method incorporates the following formula:

$$Q = C * i * A$$

Where: Q =Design discharge in cubic feet per second

C = Coefficient of runoff

i = Rainfall intensity in inches per hour for the selected storm frequency

A = Area in acres

Runoff coefficients (C) for permeable areas were developed from HDM figure 819.2A. Runoff coefficients (C) for impermeable areas were developed from HDM table 819.2B.

The project is approximately located at latitude/longitude: 32.9656°/-117.1658°. The IDF curves were produced using NOAA Atlas 14, Volume 6, Version 2. The curves are included in Figure 2 and the formulas are as follows:

$$i_{(10)} = 0.681 * (T_c/60)^{-0.612}$$

$$i_{(25)} = 0.836 * (T_c/60)^{-0.610}$$

$$i_{(100)} = 1.054 * (T_c/60)^{-0.600}$$

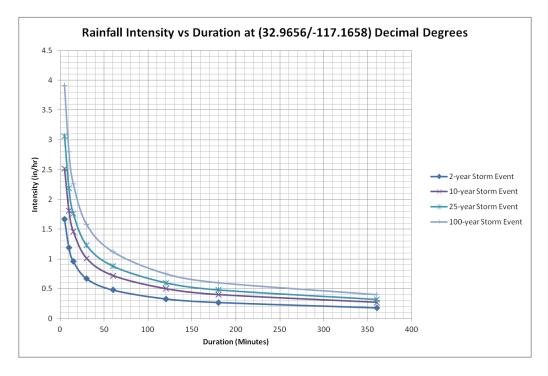


Figure 2: Storm IDF Curves

2.3 Hydraulic Calculations

All hydraulic calculations in this study were determined using the methodology presented in the Caltrans HDM and the FHWA Urban Drainage Design Manual, Hydraulic Engineering Circular Number 22 (HEC-22), Third Edition. All calculations and software outputs are included in **Appendix C**.

Storm Drain Calculations

Storm drain calculations were completed using StormCAD V8i (SELECT series 2) developed by Bentley.

Inlet Capacity and Gutter Flow

Inlet capacity and gutter flow calculations were determined using FlowMaster V8i (SELECTseries1) software developed by Bentley. This software performs calculations based on Chapter 4 of HEC-22.

Open Channels

Open Channel flow calculations were determined using FlowMaster V8i (SELECTseries1) software developed by Bentley. This software performs calculations based on Chapter 4 of HEC-22. HDM table 866.2 was used to determine freeboard requirements.

2.4 Biofiltration Systems Analysis

The proposed improvements will increase the total impervious area for the project site. The County of San Diego's Hydromodification Determination matrix requires hydromodification and water quality be incorporated with the proposed improvements. According to the calculations for



the project site, the storm water runoff can be treated in biofiltration facilities onsite. The County of San Diego's BMP sizing calculator was utilized for sizing the proposed biofiltration basins. Additional analysis for the hydromodification and water quality treatment is provided in the Water Quality Technical Report (WQTR).

3. EXISTING DRAINAGE CONDITIONS

Due to the recent development of the Torrey Highlands property, the Shaw Properties, the LMXU Property, and the recent construction of SR-56, the existing hydrology within the project area is well documented. The existing hydrology studies prepared for the associated developments are intended to facilitate full build-out conditions, and the existing drainage facilities were designed to convey the 100-year storm event. Therefore, limited existing drainage condition calculations were performed, and 100-year storm event peak discharges were determined from the associated drainage studies and as-builts. The existing drainage studies are located in the project files and the as-built information showing the 100-year storm event peak discharges are attached in **Appendix B**.

The entire project lies within four basins that ultimately discharge into different locations along McGonigle Canyon Creek. McGonigle Canyon Creek drains into Poway Creek, which eventually discharges into the Pacific Ocean. Existing onsite drainage facilities include inlets, brow ditches, reinforced concrete storm drains (RCP), concrete lined channels, and Vortechnics storm water treatment facilities.

South of SR-56

Existing Basin 1, located south of SR-56, receives runoff from Torrey Meadows Drive and the Shaw Property Unit 2 Development. Runoff from Torrey Meadows Drive is conveyed in concrete curb and gutter to a curb inlet located in the cul-de-sac at the terminus of Torrey Meadows Drive. The Shaw Property Unit 2 drains to a series of curb inlets, 18" RCP and 24" RCP storm drain pipes, which ultimately converge with the drainage of Torrey Meadows Drive. A Vortechnics hydrodynamic separator treats the runoff at the point where the Shaw Property Unit 2 and Torrey Meadows Drive runoff converge. The treated runoff is then conveyed in an 18"x36" reinforced concrete box (RCB) culvert and discharged into a concrete lined brow ditch. The brow ditch runs northwesterly to McGonigle Canyon Creek where the system ultimately discharges. According to the Shaw Property Unit 2 Hydrology Study, prepared by Hunsaker & Associates dated January 20, 2003, the 100-year storm event peak discharge for Basin 1 is 15.13 cubic feet per second (cfs).

North of SR-56

Existing Basin 2, located north of SR-56, receives runoff from the Shaw Property Unit 1 Development. The Shaw Property Unit 1 drains to a series of curb inlets, 18" RCP and 24" RCP storm drain pipes. Prior to discharge into McGonigal Canyon Creek, runoff is treated in a Vortechnics hydrodynamic separator located at the intersection of Via Ambrosa and Torrey Meadows Drive. According to the Shaw Property Unit 1 Hydrology Study, prepared by Hunsaker & Associates dated January 15, 2003, the 100-year storm event peak discharge for Basin 2 is 13.33 cfs.

Existing Basin 3, located north of SR-56, receives runoff from Torrey Meadows Drive, the Shaw Property Unit 1, and the LMXU Property. Runoff from Torrey Meadows Drive flows to the east



and is conveyed in concrete curb and gutter to curb inlets located near the intersection of Via Sabbia and Torrey Meadows Drive. The Shaw Property Unit 1 and the LMXU property drain to a series of curb inlets, 18" RCP, 30" RCP and 42" RCP storm drain pipes along Via Sabbia. Prior to discharge into McGonigle Canyon Creek, runoff is treated in a Vortechnics hydrodynamic separator located to the east of the intersection of Via Sabbia and Torrey Meadows Drive. According to the LMXU As-Builts, prepared by Hunsaker & Associates dated June 16, 2003, the 100-year storm event peak discharge for Basin 3 is 104.82 cfs.

SR-56

Existing Basin 4 receives runoff from SR-56 and the SR-56 bike path. Runoff generally flows from east to west and is conveyed along the shoulder of SR-56 and in a series of concrete lined channels in the median of SR-56. The runoff is collected in grate inlets and is eventually discharged to McGonigle Canyon Creek to the west. This watershed is not impacted by the proposed project and therefore no calculations or analysis were performed.

4. PROPOSED DRAINAGE CONDITIONS

The proposed drainage system has been designed to maintain a spread width less than the shoulder width of 8 feet and maximize the use of the existing drainage system. The overall existing drainage patterns are maintained, where possible. Storm water quality treatment and detention basins have been included in the design in addition to the Vortechnics hydrodynamic separators that treat the water prior to discharge.

South of SR-56

The proposed drainage system number 1 consists of modifying the existing drainage system south of SR-56 to capture the additional flows from Torrey Meadows Drive. Roadway runoff from Torrey Meadows Drive sheet flows into the curb and gutter and is conveyed to curb inlets at the low point near station 9+83. The inlets connect to 18" and 24" RCP storm drains that eventually connect to the existing system. In addition, there are curb cut outs on both sides of the roadway to capture runoff from Torrey Meadows Drive, which is treated by biofiltration basins in the parkway area to satisfy the County of San Diego's hydromodification requirements. Peak flows to the existing system have been increased by 3.22 cfs for the 100-year storm event. Analysis of the existing system has shown that there is sufficient capacity to handle the additional flow. Detailed drainage calculations can be found in **Appendix C**. Draft drainage design plans can be found in **Appendix D**.

North of SR-56

The proposed drainage system numbers 3 and 4 consists of modifying the existing drainage system north of SR-56 to capture the additional flows from Torrey Meadows Drive. Roadway runoff from Torrey Meadows Drive sheet flows into the curb and gutter and is conveyed to ongrade curb inlets at stations 15+25 and 17+25. The inlets connect to 18" and 24" RCP storm drains that eventually connect to the existing system. In addition, there are curb cut outs on both sides of the roadway to capture runoff from Torrey Meadows Drive, which is treated by biofiltration basins in the parkway area to satisfy the County of San Diego's hydromodification requirements. Peak flows to the existing system have been increased by 3.27 cfs for the 100-year storm event. Analysis of the existing system has shown that there is sufficient capacity to handle the additional flow. Detailed drainage calculations can be found in **Appendix C**. Draft drainage design plans can be found in **Appendix D**.



SR-56

There are minimal impacts to the existing drainage on SR-56. Improvements to the drainage system on SR-56 include reconstructing a drainage channel that will be removed during construction of the structure foundations. The channel will be reconstructed in-kind. The proposed project will reduce the tributary area to the SR-56, therefore this system was not analyzed.

5. CONCLUSION

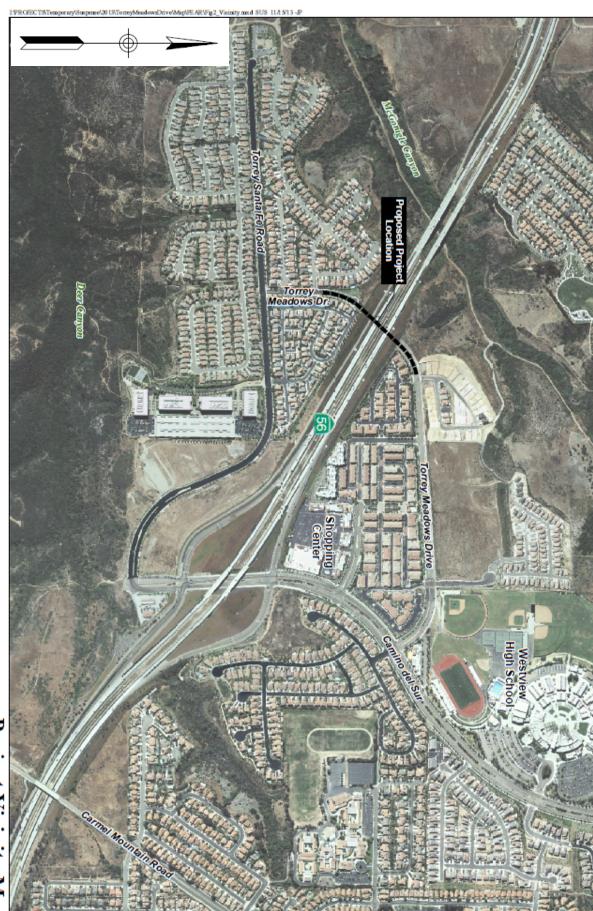
The proposed drainage system has been designed to maintain spread widths within the shoulder for the 25-year storm and sized to convey the 100-year storm. In addition, drainage improvements have been designed to meet the County of San Diego's hydromodification requirements. Modifications to the existing drainage system to accommodate the roadway improvements and bridge construction consist of concrete channels, inlets, RCP storm drains and biofiltration basins. The overall existing drainage patterns are maintained. The project leads to an overall increase in 25-year and 100-year peak due to an increase in impervious surface area. The increase in peak flow will be retained onsite using biofiltration basins meeting the County of San Diego's Model BMP Design Manual requirements.

6. REFERENCES

- 1. Urban Drainage Design Manual Hydraulic Engineering Circular No. 22, U.S. Department of Transportation, Federal Highway Association, August 2001.
- 2. FlowMaster V8i (SELECTseries 1) [08.11.01.03], Bentley Systems, Inc., November 2009.
- 3. StormCAD V8i (SELECTseries 2) [08.11.02.35], Haestad Methods Solution Center, May 2010.
- 4. Highway Design Manual, California Department of Transportation, March 2014.
- 5. Model BMP Design Manual San Diego Region, County of San Diego, Public DRAFT January 2015.

APPENDIX A

VICINITY MAP AND FEMA FIRMETTE



Project Vicinity Map







MAP SCALE 1" = 1000"

500

1,000

1,500

2,000

Z 1 GRAM

PANEL 1335G

AND INCORPORATED AREAS SAN DIEGO COUNTY, FLOOD INSURANCE RATE MAP CALIFORNIA

PR

PANEL 1335 OF 2375

CONTAINS: (SEE MAP INDEX FOR FIRM PANEL LAYOUT)

SAN DIEGO COUNTY SAN DIEGO, CITY OF COMMUNITY

INSURANCE

NUMBER 060284 060295

PANEL 1335 1335 SUFFIX െ ഒ

Notice to User. The Map Number shown below should be used when placing map orders, the Community Number shown above should be used on insurance applications for the subject community. MAP NUMBER

MAP REVISED MAY 16, 2012

06073C1335G

Federal Emergency Management Agency

This is an official copy of a portion of the above referenced food map. It was extracted using F-MIT On-Line. This map does not reflect changes or amendments which may have been made subsequent to the date on the title block. For the latest product information about National Flood Insurance

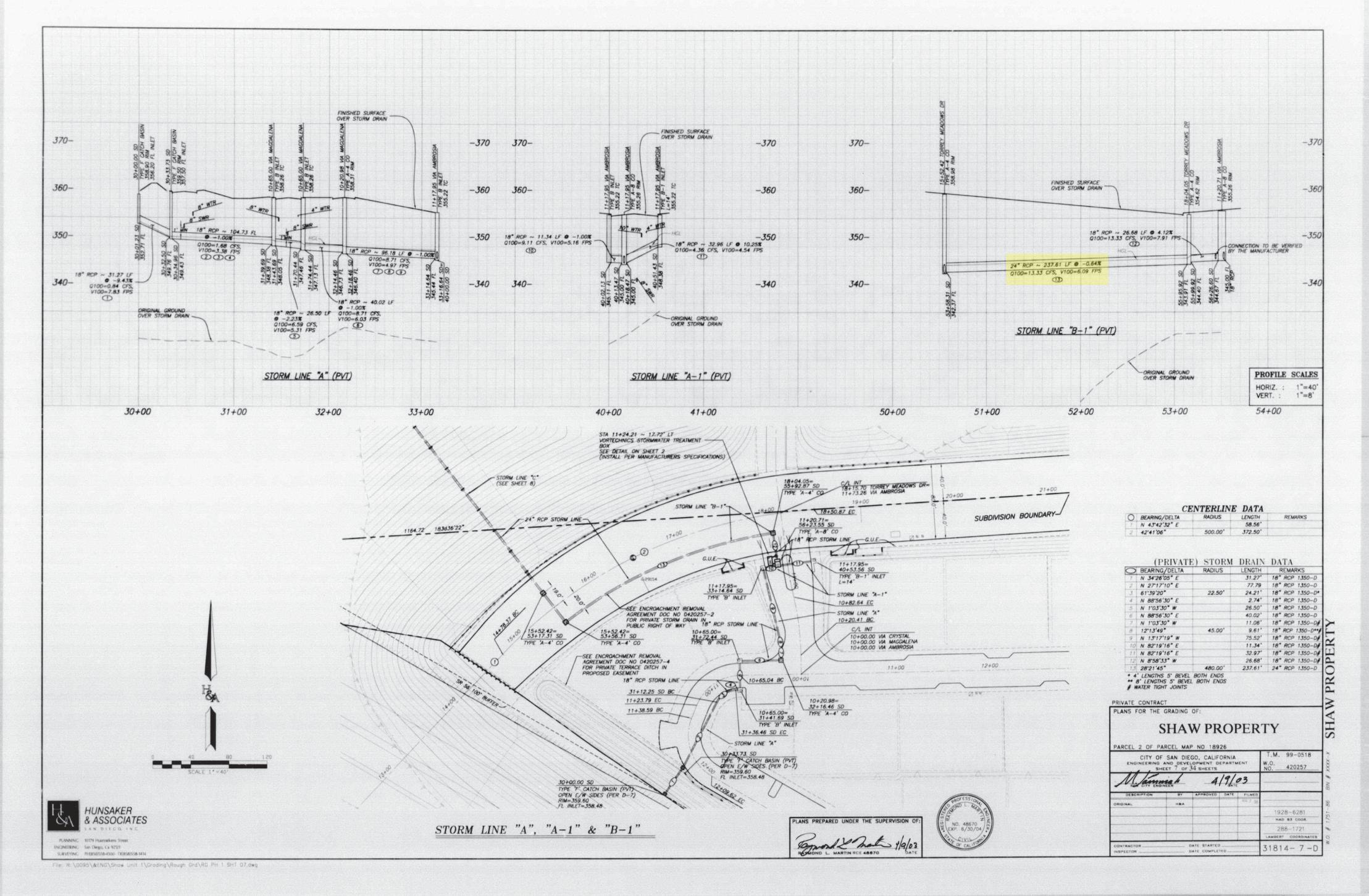
APPENDIX B

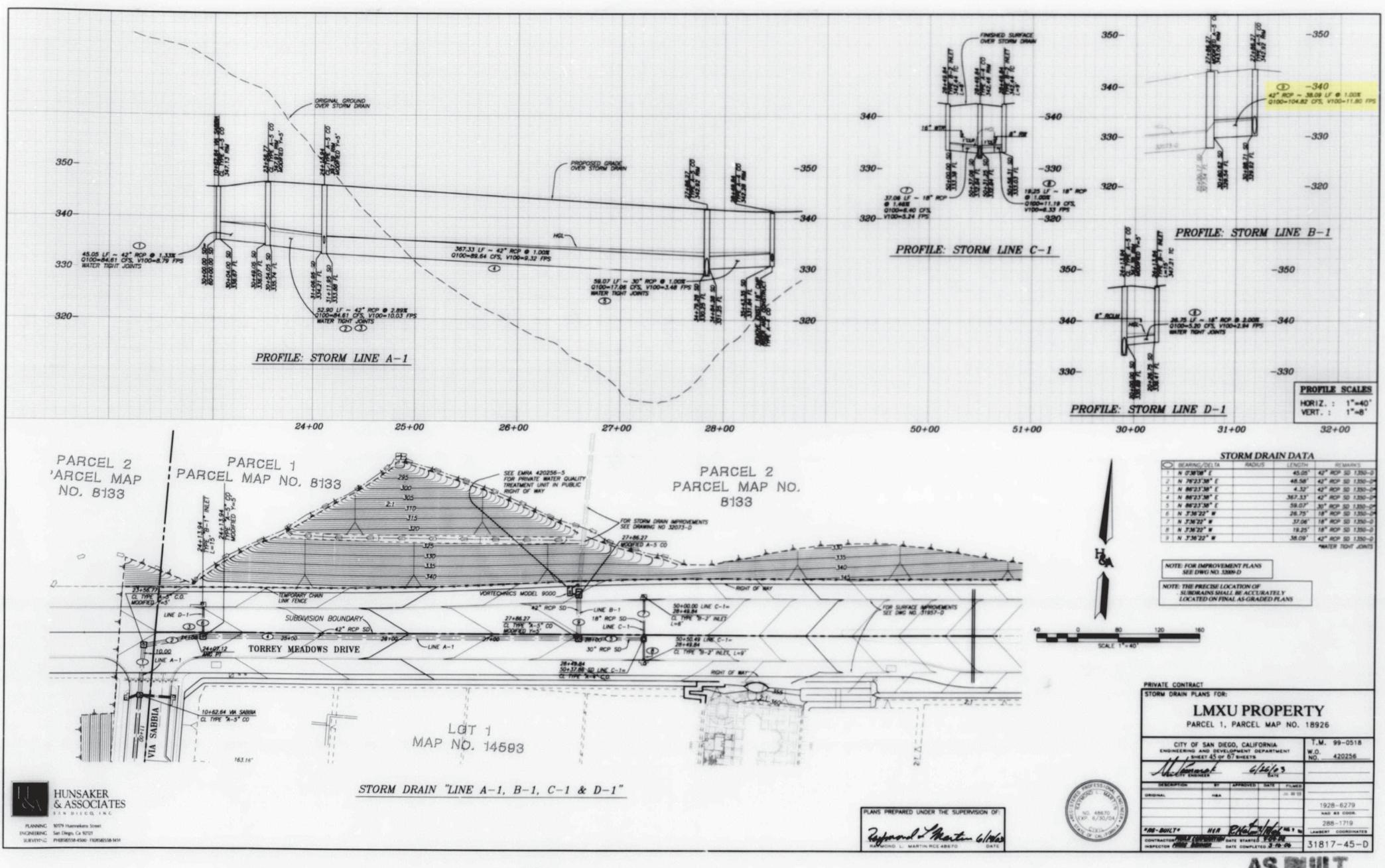
EXISTING CONDITION HYDROLOGIC ANALYSES, AS-BUILTS, AND MAP



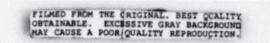
FLOW RATES FOR EXISTING CONDITIONS

Watershed No.	Drainag	e Areas	Q(100)	Notes
	(sq ft)	(acres)	cfs	
1.01	58279	1.338	3.060	Q100 from As-Built Plan 32139
1.OS	-	-	12.660	Q100 from As-Built Plan 32139
2.OS	-	-	13.330	Q100 from As-Built Plan 31814
3.OS	-	1	76.290	Q100 from As-Built Plan 31817
3.01	45899	1.054	5.200	Q100 from As-Built Plan 31817
3.02	119922	2.753	8.320	Q100 from As-Built Plan 31817

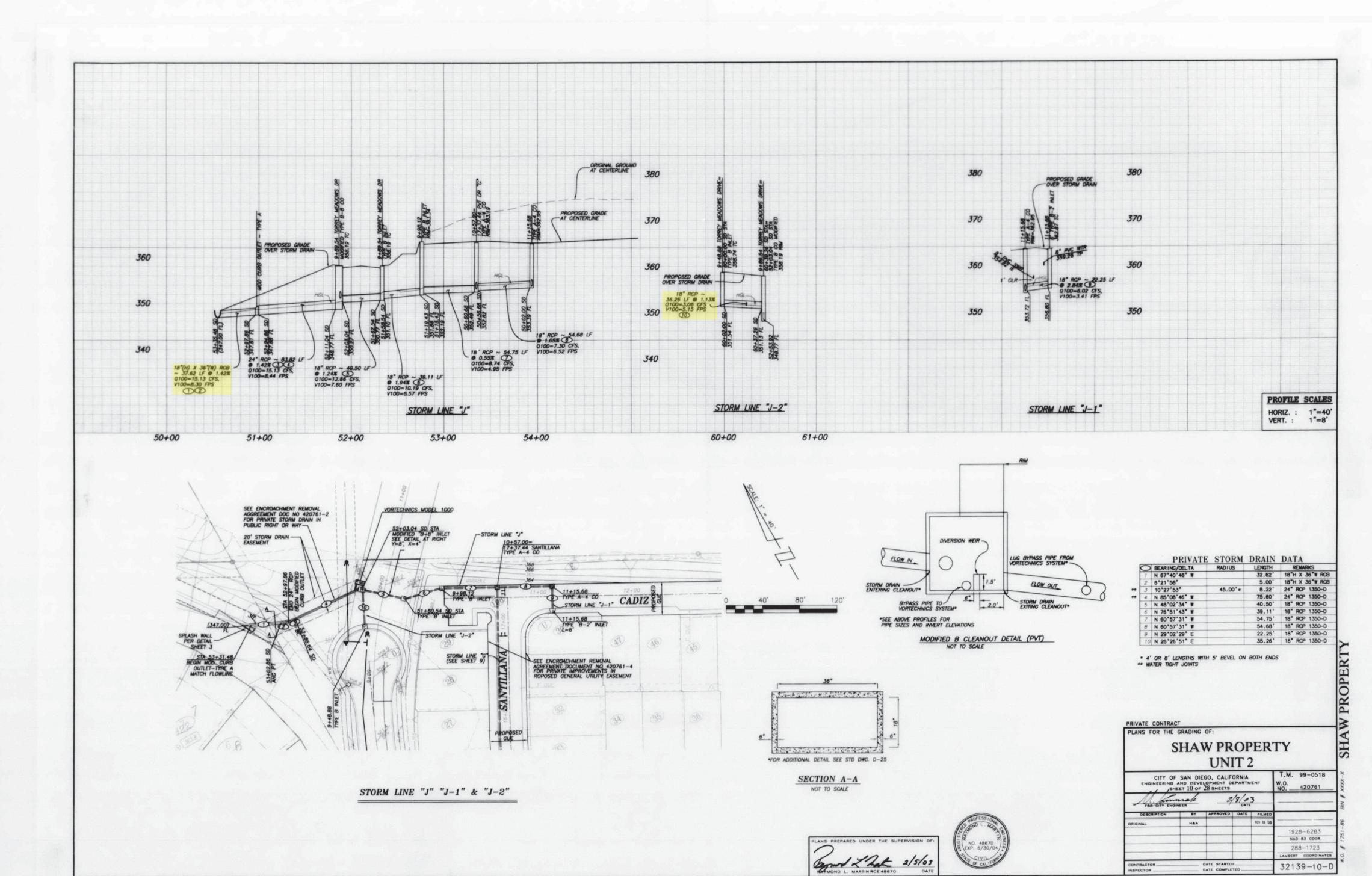




AS BUILT







R: \0095\&Eng\Shaw Unit 2\GRD\Rough Grd\RG PH 2 SHT 10.dwg[1275]Feb-07-2003: 08: 32

FILMED FROM THE ORIGINAL. BEST QUALITY OBTAINABLE. EXCESSIVE GRAY BACKGROUND MAY CAUSE A FOOR QUALITY REPRODUCTION.



APPENDIX C

PROPOSED CONDITION HYDROLOGIC ANALYSES AND MAP



FLOW RATES FOR PROPOSED CONDITIONS

No.								Sh	eet Flow	,				s	Shallow	Concen	trated	Flow	10000 10000 10000 10000 10000 10000 10000 10000			CI	nannel	Flow					Total Time of Concentration											Water
10 10 10 10 10 10 10 10		Drain	nage Aı	reas	L	n	i(2)	i(10	0) i(2	5) i	i(100)	s	Tt	L	s	к	v	Tt	L	. C	Channel Section	s	n	Α	WP	R	v	Tt		•		C(2)	C(10)	C(25)	C(100)	Q(2)	Q(10)	Q(25)	Q(100)	Water Quality Storm
Section Control Cont		(sq ft	t) (ac	cres) (ft)		(in/hr)	(in(h	hr) (in/l	hr) ((in/hr)	(ft/ft)	(min)	(ft)	(%)	(ft/s) (ft/s) (min) (ft)	t)		(ft/ft)		(sq ft)	(ft)	(ft)	(ft/s)	(min)	(minutes)	(minutes)	-					cfs	cfs	cfs	cfs	cfs
160	1.01	7244.0	.06 0.	.166 1	43 0.0	016	1.8	3.1	1 3.8	8	4.7	0.020	2.86				-	0.00	63	3	Curb & Gutter	0.036	0.013	0.170	2.18	0.078	8 3.956	0.26	3.1	5.0	0.93	0.93	0.93	1.00	1.00	0.285	0.483	0.633	0.778	0.0310
March Marc	1.02	1432.0	.04 0.	.033 2	27 0.0	016	1.8	3.1	1 3.8	8	4.7	0.020	0.76				-	0.00	59	9	Curb & Gutter	0.036	0.013	0.170	2.18	0.078	8 3.956	0.25	1.0	5.0	0.95	0.95	0.95	1.00	1.00	0.057	0.097	0.125	0.154	0.0062
The color		1504.6	.68 0.		_		1.8	3.1	1 3.8	8	4.7	_	-				-	0.00	_	_		-	0.013	0.170	2.18	0.078	8 3.956	0.28						1.00	1.00			0.131	0.162	0.0066
Column C			.01							_	4.7						-	0.00		_		_	0.013	0.170	2.18	0.078	8 3.956	0.29										0.130		0.0065
March 1,000 1,00					_				_	-	4.7	0.020					-	0.00		_		+	0.013	0.170	2.18	0.07	8 3.956	0.25										0.120	00	0.0060
1886 1887 1888 1889										-		0.020	-				-	0.00				_	0.013	0.170	2.18	0.07	3.956											0.115		0.0058
1.00 1.00									_	_		_					-	0.00		_		+	0.013	1.000	3.24	0.07	9 4 290													0.0392
1.11 10.000 1.8 2.1									_	-		1	-					_					0.030		3.24	0.30	9 4 290													0.0029
100 100			0		_					-+		1						_		_			0.030	1.000	3.24	0.309	9 4.290											1		0.0038
19 19 19 19 19 19 19 19				.207				3.1	1 3.8	8	4.7	0.020	2.08					0.00	_		Biofiltration 2		0.030	73.500	33.16	3 2.21	7 15.955	0.15	2.2	5.0	0.24	0.24	0.24	0.26	0.30	0.092	0.155	0.208	0.291	0.0100
1.60 1.60	1.12		_	.008	2 0.0	016	1.8	3.1	1 3.8	8	4.7	0.020	0.08					0.00	71	1	Biofiltration 1	0.036	0.030	1.000	3.24	0.309	9 4.290	0.28	0.4	5.0	0.15	0.15	0.15	0.17	0.19	0.002	0.004	0.005	0.007	0.0002
1.15	1.13	358.08	81 ⁰ .	.008	2 0.0	016	1.8	3.1	1 3.8	8	4.7	0.020	0.10					0.00	45	5	Biofiltration 1	0.036	0.030	1.000	3.24	0.309	9 4.290	0.18	0.3	5.0	0.15	0.15	0.15	0.17	0.19	0.002	0.004	0.005	0.007	0.0002
1.17	1.14	145.9	.91 0.	.003	2 0.0	040	1.8	3.1	1 3.8	8	4.7	0.020	0.23					0.00	30	0	Biofiltration 1	0.036	0.030	1.000	3.24	0.309	9 4.290	0.12	0.4	5.0	0.15	0.15	0.15	0.17	0.19	0.001	0.002	0.002	0.003	0.0001
1.17 157.76 1.00		178.2			_				_	8	4.7	0.020	0.44					_		_		+	0.030	1.000	3.24	0.309	9 4.290	0.08			0.63	0.63	0.63	0.69				0.011	0.015	0.0005
130 145			.00		_				_	-		1	1					_				_	0.013	0.170	2.18	0.078	8 3.956													0.0400
150 150									_	-+		1	0.77					_		_		_	0.013	0.170	2.18	0.078	8 3.956													0.0060
1922 1923 1924 1924 1925										-		1	0.66					_		_		-	0.013	0.170	2.18	0.078	3.956													0.0063
121			. 10		_				_	-		1						_		_			0.013	0.170	2.18	0.07	3.956													0.0062
122 (17.77) (17.70) (1										-		1	0.50					_				_	0.013	0.170	2.18	0.07	3.956	1.28						-				+	1.116	0.0064
122 147.2 0.03 0.00			.00		_					_			0.56					_		_		+	0.013	1.000	2.10	0.07	0 3.950	0.23										0.907	0.052	0.0455
1.24 155.15 1.05									_	-		1	-					_		_		_	0.030	1.000	3.24	0.30	9 4.290	0.23						_				0.057	0.032	0.0018
1.28 249.5 0.90 10 0.070 118 3.1 38 47 0.00 119 0.00 129 0.00 0.00 100 0.00 0.00 0.00 0.00 0.00																							0.030	1.000	3.24	0.309	9 4 290	0.30												0.0025
126 244.4 1 000 19																			_				0.030		3.24	0.309	9 4.290													0.0032
1920 99,129 001 10 0015 18 31 33 47 0.00 0.44 0.00				_							4.7							_	_				0.030	1.000	3.24	0.309	9 4.290	0.34	1.5					0.48					0.145	0.0049
202 415-05 033 29 016 18 31 38 47 020 068 1 000 173 Cure & Cuiner DOTS 015 073 078 018 077 257 018 079 079 079 089 089 089 080 080 080 080 080 080 08	1.27		_	.012	16 0.0	013	1.8	3.1	1 3.8	8	4.7	0.020	0.43					0.00	21	1	Biofiltration 1	0.036	0.030	1.000	3.24	0.309	9 4.290	0.08	0.5	5.0	0.33	0.33	0.33	0.36	0.41	0.007	0.013	0.017	0.024	0.0008
204 2707 3 005	2.01		_	.141 2	22 0.0	016	1.8	3.1	1 3.8	8	4.7	0.020	0.63					0.00	173	3	Curb & Gutter	0.015	0.013	0.170	2.18	0.078	8 2.557	1.12	1.8	5.0	0.79	0.79	0.79	0.87	0.98	0.204	0.346	0.464	0.649	0.0222
2.05 1485.92 034 036 036 036 036 036 036 036 036 036 036	2.02	1425.6	.67 0.	.033	23 0.0	016	1.8	3.1	1 3.8	8	4.7	0.020	0.66					0.00	63	3	Curb & Gutter	0.015	0.013	0.170	2.18	0.078	8 2.557	0.41	1.1	5.0	0.95	0.95	0.95	1.00	1.00	0.057	0.097	0.125	0.153	0.0062
2.05 1485.92 0.34 28 0.040 1.8 3.1 3.8 4.7 0.020 1.84 0.000 5.2 Curb & Gutter 0.017 0.018 0.017 0.218 0.072 2.746 0.32 2.0 0.05 0.05 0.05 0.05 0.05 0.05 0.000 0.000 0.010	2.03	666.58	82 0.	.015	25 0.0	016	1.8	3.1	1 3.8	8	4.7	0.020	0.71					0.00	28	3	Curb & Gutter	0.015	0.013	0.170	2.18	0.078	8 2.557	0.18	0.9	5.0	0.95	0.95	0.95	1.00	1.00	0.027	0.045	0.058	0.072	0.0029
207 13415 201 15 0.040 18 3.1 3.8 47 0.020 0.83	2.04	2707.5	53 0.	.062 2	25 0.0	016	1.8	3.1	1 3.8	8	4.7	0.020	0.71					0.00	117	7	Curb & Gutter	0.015	0.013	0.170	2.18	0.078	8 2.557	0.76	1.5	5.0	0.95	0.95	0.95	1.00	1.00	0.109	0.184	0.236	0.291	0.0118
2.07 141.53 0.031 15 0.040 1.8 3.1 3.8 4.7 0.020 0.77 0.00 52 Biofiliration 3 0.017 0.030 0.000 7.47 0.080 4.985 0.17 1.1 5.0 0.30 0.30 0.30 0.30 0.30 0.30 0.30		1485.9	92 0.	.034 2			1.8	3.1	1 3.8	8	4.7	0.020	1.64					0.00	_		Curb & Gutter		0.013	0.170	2.18	0.078	8 2.746	0.32	2.0	5.0	0.95	0.95	0.95	1.00	1.00	0.060	0.101	0.130	0.160	0.0065
2.08 318192 0.072 12 0.040 18 3.1 3.8 4.7 0.020 0.84										-+		_						_		_					+									+						0.0032
2.09 1208 66 0.28 11 0.016 1.8 3.1 3.8 4.7 0.020 0.37 0.00 50 Biolification 3 0.017 0.030 0.007 0.78										_		_	-					_																+				+		
2.10 742.15 0.170 21 0.040 1.8 3.1 3.8 4.7 0.020 1.31 0.00 26 Curb & Gutter 0.017 0.018 0.170 2.18 0.078 2.746 1.25 2.6 5.0 0.75 0.75 0.75 0.75 0.83 0.04 0.26 0.40 0.57 0.75 0.75 0.75 0.75 0.75 0.75 0.7																		_	_																					
2.11 745.04 0.017 25 0.040 1.8 3.1 3.8 4.7 0.020 1.49 0.00 27 Curb & Gutter 0.017 0.018 0.170 2.18 0.078 2.746 0.16 1.7 5.0 0.95 0.95 0.95 0.95 1.00 1.00 0.030 0.051 0.065 0.080 0.21 0.050 0.0																						_			1													+		
2.12 643.42 0.016 18 0.016 18 0.016 18 0.016 18 0.016 18 0.016 18 0.016 18 0.016 18 0.017 0.018 0.017 0.018 0.017 0.018 0.017 0.018 0.017 0.018																		_		_																				
2.13 2610.42 0.060 25 0.016 1.8 3.1 3.8 4.7 0.020 0.71 0.00 107 Curb & Gutter 0.017 0.013 0.170 2.18 0.078 2.746 0.66 1.4 5.0 0.95 0.95 0.95 0.95 1.00 1.00 0.065 0.177 0.228 0.281 0.214 1.434 0.033 29 0.040 1.8 3.1 3.8 4.7 0.020 0.68 0.00 64 0.00 46 0.00 46 0.00 0.00 46 0.00 0.00			_						_	_								_	_	_			0.013											+				+		
2.14										_		_						_					0.013											_						
2.15 1607.62 0.037 24 0.016 1.8 3.1 3.8 4.7 0.020 0.68 0.00 54 Biofiltration 3 0.017 0.030 5.000 7.47 0.669 4.985 0.18 0.9 5.0 0.30 0.30 0.30 0.30 0.30 0.30 0.30							-					_							_	_			0.013											+						
2.16							-											_	_				0.030		+									+				_	1	
2.17 2890.53 0.066 12 0.040 1.8 3.1 3.8 4.7 0.020 0.85																		_	_	_					1	+	_							+				+		
2.18			-	1000000									_					_		_					+									_						
3.01 605.043 0.014 27 0.016 1.8 3.1 3.8 4.7 0.020 0.76 0.00 20 Curb & Gutter 0.017 0.013 0.170 2.18 0.076 0.12 0.9 5.0 0.95 0.95 0.95 0.95 1.00 1.00 0.024 0.041 0.053 0.065 0.00 0.00 0.00 0.00 0.00 0.00 0.0							-						_					_	_	_				5.000	7.47	0.669	9 4.985	0.16						_						
3.02 766.236 0.018 10 0.016 1.8 3.1 3.8 4.7 0.020 0.34 0.00 36 Biofiltration 3 0.017 0.030 5.000 7.47 0.669 4.985 0.12 0.5 5.0 0.33 0.33 0.33 0.36 0.41 0.011 0.018 0.024 0.034 0.33 0.33 589.685 0.014 27 0.040 1.8 3.1 3.8 4.7 0.020 1.57 0.000 19 Curb & Gutter 0.017 0.013 0.170 2.18 0.078 2.746 0.11 1.7 5.0 0.95 0.95 0.95 0.95 1.00 1.00 1.00 0.024 0.040 0.051 0.063 0.30 0.33 0.33 0.36 0.41 0.011 0.018 0.024 0.040 0.051 0.063 0.30 0.30 0.30 0.30 0.30 0.30 0.3	3.01						1.8						_					0.00	20	0				0.170	2.18	0.078	8 2.746	0.12	0.9	5.0	0.95	0.95	0.95	1.00	1.00	0.024	0.041	0.053	0.065	0.0026
3.04 702.076 0.016 12 0.016 1.8 3.1 3.8 4.7 0.020 0.40 0.00 35 Biofiltration 3 0.017 0.030 5.000 7.47 0.669 4.985 0.12 0.5 5.0 0.36 0.36 0.36 0.39 0.45 0.011 0.018 0.024 0.03	3.02	766.23	36 0.	.018	10 0.0	016	1.8	3.1	1 3.8	8	4.7	0.020	0.34					0.00	36	3	Biofiltration 3	0.017	0.030	5.000	7.47	0.669	9 4.985	0.12	0.5	5.0	0.33	0.33	0.33	0.36	0.41	0.011	0.018	0.024	0.034	0.0012
3.05 25483.2 0.585 28 0.016 1.8 3.1 3.8 4.7 0.020 0.77 0.00 624	3.03																	_											1.7		0.95									
3.06 108884 2.500 12 0.040 1.8 3.1 3.8 4.7 0.020 0.82 0.00 609																															0.36			_						
1.0S																		_		_		_			-	_														
2.08		10888	84 2.	.500			1.8	3.1	1 3.8	8	4.7	0.020	0.82					0.00		_		0.017	0.013	0.170	2.18	0.078	8 2.746	3.70	4.5	5.0	0.70	0.70	0.70	0.77	0.88	3.221	5.453	7.322		0.3499
		-	_						-		-						-	-					-	-	-	-	-	-		-				-	-			-		
3.05					_				-		-		-					-					-	-		-		-						-	-			-		
	3.08	-		-	-	-			-		-	-	-	-	-	-	-	-	-		-	-	-	-	-	-	-	-	-	-	-			-	-			-	76.290	

FLOW RATES FOR PROPOSED CONDITIONS

						She	et Flo	w				S	hallow C	oncent	rated F	low			CI	nannel	Flow					Total Time of Concentration	- Design Time of										Water
Watershed No.	Draina	ige Area	s L	n	i(2)	i(10) i(:	(25)	i(100)	s	Tt	L	s	к	v	Tt	L	Channel Section	s	n	A	WP	R	v	Tt	Тс	Concentration	Runoff Coefficient C	C(2)	C(10)	C(25)	C(100)	Q(2)	Q(10)	Q(25)	Q(100)	Quality Storm
	(sq ft)	(acres	(ft)		(in/hı) (in(h	r) (in	n/hr) ((in/hr)	(ft/ft)	(min)	(ft)	(%)	(ft/s)	(ft/s)	(min)	(ft)		(ft/ft)		(sq ft)	(ft)	(ft)	(ft/s)	(min)	(minutes)	(minutes)						cfs	cfs	cfs	cfs	cfs

INTENSITY

SHEET FLOW

Rainfall Intensity for 25 year storm (in/hr)

Rainfall Intensity for i(100) =100 year storm (in/hr)

 $T_{t} = \frac{0.42 L^{4/5} n^{4/5}}{P_{2}^{1/2} S^{2/5}}$

Time of travel (min) Length of flow path (ft) Roughness Coefficient

T_t = Time of travel (min)
K = Intercept Coefficient
- HDM Table 816.6B Siope (ft/ft) V = Velocity (ft/s)
2-year, 24-hour rainfall depth (in L = Length of flow path (ft)
- NOAA Atlas 2, Vol XI S = Slope (percent)

TIME OF CONCENTRATION

SHALLOW CONCENTRATED FLOW

Tc(25) = Tc(100) = Total time of Travel for 25 years storm Total time of Travel for 100 years storm **CHANNEL FLOW**

 $T_{t} = \frac{L}{60 \text{ V}}$

T_t = Time of travel (min) n = Roughness Coefficient - HDM Table 864.3A

Slope (ft/ft)

 $\begin{array}{lll} S = & Slope \mbox{ (ft/ft)} \\ A = & Cross \mbox{ sectional flow area (sq ft)} \\ WP = & Wetted \mbox{ perimeter (ft)} \\ R = & Hydraulic \mbox{ radius (ft/ft)} \\ L = & Length \mbox{ of flow path (ft)} \\ V = & Velocity \mbox{ (ft/s)} \\ \end{array} \begin{array}{ll} V = \frac{A}{WP} \\ V = \frac{1.486}{n} R^{2/3} S^{1/2} \end{array}$

DISCHARGE Q = CiA

j =

C = Standard Run-Off Coefficient C(25) = C(100) = 25 Years Storm Run-Off Coefficient 100 Years Storm Run-Off Coefficient

Rainfall Intensity (in/hr)

Q(25) =25 Years StormTotal Discharge Q(100) =100 Years Storm Total Discharge

Discharge (cfs) Q = C = HDM Table 819.2B Runoff Coefficient

-i(WQ) = 0.2 in/hrTable 3.2-1Caltrans Treatment BMP Training Handout, Version

HDM Table 819.2B

Tributary Area (acres) 1.4.2, dated May 2003

EXISTING VS. PROPOSED FLOW RATES

Existing Watershed No.	Proposed Watershed No.	EXISTING Q(100)	PROPOSED Q(100)	Change in Q(100)
		cfs	cfs	cfs
1.00	1.00	15.720	18.944	3.224
2.00	2.00	13.330	16.603	3.273
3.00	3.00	89.810	89.121	-0.689
То	tal:	118.860	124.668	5.808

PROPOSED DRAINAGE ANALYSIS

#	Inlet/Drainage Unit	Design Storm	ې Q from watershed	ය Additional Q	Additional flow from:	cts Q Total	ය ශ් Q Bypass	sp Q Interecept	Slope	Road Cross Slope	% Gutter Cross	th Spread	Geometry Notes:	Design Notes:
	1.01cc	25	0.6326			0.63	0.54	0.09	3.56%	2.00%	8.33%	2.74	1" Curb Cut Gutter Depression	On Grade
	1.02cc	25	0.1251	0.54	Bypass from 1.01cc	0.67	0.57	0.10	3.56%	2.00%	8.33%	2.88	1" Curb Cut Gutter Depression	On Grade
	1.03cc	25	0.1314	0.57	Bypass from 1.02cc	0.70	0.63	0.07	3.56%	2.00%	8.33%	2.99	1" Curb Cut Gutter Depression	On Grade
	1.04cc	25	0.1304	0.63	Bypass from 1.03cc	0.76	0.7	0.06	3.56%	2.00%	8.33%	3.2	1" Curb Cut Gutter Depression	On Grade
	1.05cc	25	0.1202	0.7	Bypass from 1.04cc	0.82	0.71	0.11	3.56%	2.00%	8.33%	3.39	1" Curb Cut Gutter Depression	On Grade
	1.06cc	25	0.1202	0.71		0.83	0.71	0.11	3.56%	2.00%	8.33%	3.42		On Grade
	1.07a	25	0.7954	0.71	Bypass from 1.05cc	1.52	0.72	1.52	1.66%	2.00%	6.25%	3.42	1" Curb Cut Gutter Depression	
				0.72	Bypass from 1.06cc	1	- 0.00					-	Type B, 3" Depression	In Sag
	1.13ci	25	0.2007	-		0.20	0.02	0.18	3.56%	2.00%	8.33%	1.62	Type A Curb Inlet/Outlet	On Grade
	1.14ci	25	0.0073	0.02	Bypass from 1.13ci	0.03	0	0.03	3.56%	2.00%	8.33%	0.8	Type A Curb Inlet/Outlet	On Grade
	1.16cc	25	0.8026	-		0.80	0.69	0.11	3.56%	2.00%	8.33%	3.33	1" Curb Cut Gutter Depression	On Grade
	1.17cc	25	0.1194	0.69	Bypass from 1.16cc	0.81	0.7	0.11	3.56%	2.00%	8.33%	3.36	1" Curb Cut Gutter Depression	On Grade
	1.18cc	25	0.1265	0.7	Bypass from 1.17cc	0.83	0.72	0.11	3.56%	2.00%	8.33%	3.42	1" Curb Cut Gutter Depression	On Grade
	1.19cc	26	0.1245	0.72	Bypass from 1.18cc	0.84	0.73	0.11	3.56%	2.00%	8.33%	3.45	1" Curb Cut Gutter Depression	On Grade
	1.20cc	25	0.1277	0.73	Bypass from 1.19cc	0.86	0.75	0.11	3.56%	2.00%	8.33%	3.53	1" Curb Cut Gutter Depression	On Grade
	1.21c	25	0.9238	0.75	Bypass from 1.20cc	1.67	-	1.67	1.66%	2.00%	6.25%	3.33	Type B, 3" Depression	In Sag
	2.01cc	25	0.4644	-		0.46	0.36	0.10	1.73%	2.00%	8.33%	2.86		On Grade
	3d	25	0.1908	0.36	Bypass from 2.01cc	0.55	0.08	0.47	1.66%	2.00%	6.25%	3.95	Type B-1, L=7, 3" Depression	On Grade
	2.03cc	25	0.0582	0.08	Bypass from 3d	0.14	0.09	0.05	1.73%	2.00%	8.33%	1.18	1" Curb Cut Gutter Depression	On Grade
	2.04cc	25	0.2365	0.09	Bypass from 2.03cc	0.33	0.25	0.08	1.73%	2.00%	8.33%	2.04	1" Curb Cut Gutter Depression	On Grade
	4a	25	0.3276	0.25	Bypass from 2.04cc	0.58	0.09	0.49	1.66%	2.00%	6.25%	4.06	Type B-1, L=7, 3" Depression	On Grade
	3.01cc	25	0.0528	0.09	Bypass from 4a	0.14	0.09	0.05	1.73%	2.00%	8.33%	1.18	1" Curb Cut Gutter Depression	On Grade
	2.10cc	25	0.5373	1		0.54	0.43	0.11	1.73%	2.00%	8.33%	3.26	1" Curb Cut Gutter Depression	On Grade
	3b	25	0.1120	0.43	Bypass from 2.10cc	0.54	0.08	0.46	1.66%	2.00%	6.25%	3.90	Type B-1, L=7, 3" Depression	On Grade
	2.12cc	25	0.0562	0.08	Bypass from 3b	0.14	0.09	0.05	1.73%	2.00%	8.33%	1.18	1" Curb Cut Gutter Depression	On Grade
	2.13cc	25	0.2280	0.09	Bypass from 2.12cc	0.32	0.24	0.08	1.73%	2.00%	8.33%		1" Curb Cut Gutter Depression	On Grade
	4e	25	0.3013	0.24	Bypass from 2.13cc	0.54	0.08	0.46	1.66%	2.00%	6.25%	3.90		On Grade
	3.03cc	25	0.0515	0.08	Bypass from 4e	0.13	0.09	0.04	1.73%	2.00%	8.33%		1" Curb Cut Gutter Depression	On Grade
	1.01cc 1.02cc	100	0.7785 0.1539	0.67	Bypass from 1.01cc	0.78	0.67 0.71	0.11 0.11	3.56% 3.56%	2.00%	8.33% 8.33%		1" Curb Cut Gutter Depression 1" Curb Cut Gutter Depression	On Grade On Grade
	1.03cc	100	0.1617	0.07	Bypass from 1.02cc	0.82	0.76	0.11	3.56%	2.00%	8.33%	3.54	1" Curb Cut Gutter Depression	On Grade
	1.04cc	100	0.1604	0.76	Bypass from 1.03cc	0.92	0.70	0.12	3.56%	2.00%	8.33%	3.69	1" Curb Cut Gutter Depression	On Grade
	1.05cc	100	0.1479	0.8	Bypass from 1.04cc	0.95	0.83	0.12	3.56%	2.00%	8.33%		1" Curb Cut Gutter Depression	On Grade
	1.06cc	100	0.1420	0.83	Bypass from 1.05cc	0.97	0.85	0.12	3.56%	2.00%	8.33%	3.82	1" Curb Cut Gutter Depression	On Grade
	1.07a	100	0.9655	0.85	Bypass from 1.06cc	1.82	-	1.82	1.66%	2.00%	6.25%	3.45		In Sag
	1.13ci	100	0.2807	-	Dumas from 4.40 '	0.28	0.05	0.23	3.56%	2.00%	8.33%		Type A Curb Inlet/Outlet	On Grade
	1.14ci	100 100	0.0102	0.05	Bypass from 1.13ci	0.06	0 0.87	0.06	3.56%	2.00%	8.33%	1.03 3.88	Type A Curb Inlet/Outlet	On Grade
	1.16cc 1.17cc	100	0.9876 0.1470	0.87	Bypass from 1.16cc	0.99 1.02	0.87	0.12 0.12	3.56% 3.56%	2.00% 2.00%	8.33% 8.33%	3.88	1" Curb Cut Gutter Depression 1" Curb Cut Gutter Depression	On Grade On Grade
	1.17cc	100	0.1557	0.9	Bypass from 1.17cc	1.02	0.94	0.12	3.56%	2.00%	8.33%	4.05	1" Curb Cut Gutter Depression	On Grade
	1.19cc	100	0.1533	0.94	Bypass from 1.18cc	1.09	0.96	0.13	3.56%	2.00%	8.33%		1" Curb Cut Gutter Depression	On Grade

1.20cc	100	0.1571	0.96	Bypass from 1.19cc	1.12	0.99	0.13	3.56%	2.00%	8.33%	4.21	1" Curb Cut Gutter Depression	On Grade
1.21c	100	1.1396	0.90	Bypass from 1.20cc	2.13	0.99	2.13	1.66%	2.00%	6.25%	3.65	Type B, 3" Depression	In Sag
			0.99	Bypass IIOIII 1.20CC		0.50							· · ·
2.01cc	100	0.6493	- 0.50		0.65	0.53	0.12	1.73%	2.00%	8.33%		1" Curb Cut Gutter Depression	On Grade
3d	100	0.2459	0.53	Bypass from 2.01cc	0.78	0.05	0.73	1.66%	2.00%	6.25%	4.08	Type B-1, L=7, 3" Depression	On Grade
2.03cc	100	0.0716	0.05	Bypass from 3d	0.12	0.08	0.04	1.73%	2.00%	8.33%		1" Curb Cut Gutter Depression	On Grade
2.04cc	100	0.2910	0.08	Bypass from 2.03cc	0.37	0.28	0.09	1.73%	2.00%	8.33%		1" Curb Cut Gutter Depression	On Grade
4a	100	0.3022	0.28	Bypass from 2.04cc	0.58	0.02	0.56	1.66%	2.00%	6.25%	3.29	Type B-1, L=7, 3" Depression	On Grade
3.01cc	100	0.0650	0.02	Bypass from 4a	0.09	0.05	0.04	1.73%	2.00%	8.33%		1" Curb Cut Gutter Depression	On Grade
2.10cc	100	0.7513	-		0.75	0.63	0.12	1.73%	2.00%	8.33%	4.11	1" Curb Cut Gutter Depression	On Grade
3b	100	0.1456	0.63	Bypass from 2.10cc	0.78	0.05	0.73	1.66%	2.00%	6.25%	4.08	Type B-1, L=7, 3" Depression	On Grade
2.12cc	100	0.0691	0.05	Bypass from 3b	0.12	0.08	0.04	1.73%	2.00%	8.33%	1.12	1" Curb Cut Gutter Depression	On Grade
2.13cc	100	0.2805	0.08	Bypass from 2.12cc	0.36	0.27	0.09	1.73%	2.00%	8.33%	2.25	1" Curb Cut Gutter Depression	On Grade
4e	100	0.4003	0.27	Bypass from 2.13cc	0.67	0.03	0.64	1.66%	2.00%	6.25%	3.67	Type B-1, L=7, 3" Depression	On Grade
3.03cc	100	0.0634	0.03	Bypass from 4e	0.09	0.06	0.03	1.73%	2.00%	8.33%	0.87	1" Curb Cut Gutter Depression	On Grade
				1									

Worksheet for Curb Inlet On Grade - 1.01cc_25

Pro	ect	Descr	iption

Solve For Efficiency

	In	put	Data
--	----	-----	------

Discharge	0.63	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	15.13	%
Intercepted Flow	0.10	ft³/s
Bypass Flow	0.54	ft³/s
Spread	2.74	ft
Depth	0.15	ft
Flow Area	0.15	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.32	ft/s
Equivalent Cross Slope	0.07743	ft/ft
Length Factor	0.09	
Total Interception Length	11.48	ft

Worksheet for Curb Inlet On Grade -1.02cc_25

Solve For Efficiency

Input I	Data
---------	------

Discharge	0.67	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	14.73	%
Intercepted Flow	0.10	ft³/s
Bypass Flow	0.57	ft³/s
Spread	2.88	ft
Depth	0.15	ft
Flow Area	0.15	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.34	ft/s
Equivalent Cross Slope	0.07691	ft/ft
Length Factor	0.08	
Total Interception Length	11.80	ft

Worksheet for Curb Inlet On Grade -1.03cc_25

Proj			

Solve For Efficiency

In	put	Data

Discharge	0.70	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	14.42	%
Intercepted Flow	0.10	ft³/s
Bypass Flow	0.60	ft³/s
Spread	2.99	ft
Depth	0.15	ft
Flow Area	0.16	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.35	ft/s
Equivalent Cross Slope	0.07647	ft/ft
Length Factor	0.08	
Total Interception Length	12.06	ft

Worksheet for Curb Inlet On Grade -1.04cc_25

Project Description

Solve For Efficiency

Input Data

Discharge	0.76	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	13.85	%
Intercepted Flow	0.11	ft³/s
Bypass Flow	0.65	ft³/s
Spread	3.20	ft
Depth	0.16	ft
Flow Area	0.17	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.38	ft/s
Equivalent Cross Slope	0.07558	ft/ft
Length Factor	0.08	
Total Interception Length	12.58	ft

Worksheet for Curb Inlet On Grade -1.05cc_25

Project Description

Solve For Efficiency

	In	put	Data
--	----	-----	------

Discharge	0.82	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	13.34	%
Intercepted Flow	0.11	ft³/s
Bypass Flow	0.71	ft³/s
Spread	3.39	ft
Depth	0.16	ft
Flow Area	0.19	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.40	ft/s
Equivalent Cross Slope	0.07468	ft/ft
Length Factor	0.08	
Total Interception Length	13.08	ft

Worksheet for Curb Inlet On Grade -1.06cc_25

Pro	iect	Desc	rir	\ti∩n
1 10	JOGE	Desc	JΙΙΡ	, uoi i

Solve For Efficiency

In	put	Data

Discharge	0.83	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	13.26	%
Intercepted Flow	0.11	ft³/s
Bypass Flow	0.72	ft³/s
Spread	3.42	ft
Depth	0.16	ft
Flow Area	0.19	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.41	ft/s
Equivalent Cross Slope	0.07453	ft/ft
Length Factor	0.08	
Total Interception Length	13.16	ft

Worksheet for Inlet1.07a_25 **Project Description** Solve For Spread Input Data Discharge 1.52 ft³/s Gutter Width 1.50 ft 0.06 Gutter Cross Slope ft/ft Road Cross Slope 0.02 ft/ft Local Depression 3.00 in Local Depression Width 7.00 ft Grate Width 1.50 ft Grate Length 2.95 ft P-50 mm (P-1-7/8") Grate Type 50.00 % Clogging Curb Opening Length 84.00 in 5.00 Opening Height in Curb Throat Type Horizontal Throat Incline Angle 90.00 degrees **Options** Calculation Option Use Both Results 3.21 ft Spread Depth 0.06 ft

Берит	0.00 1
Gutter Depression	0.06 ft
Total Depression	0.31 ft
Open Grate Area	1.99 ft²
Active Grate Weir Length	4.45 ft

Worksheet for Curb Inlet/outlet On Grade -1.13ci_25

Project Description

Solve For Efficiency

Input Data

Discharge	0.20	ft³/s
Slope	0.03600	ft/ft
Gutter Width	2.00	ft
Gutter Cross Slope	0.05	ft/ft
Road Cross Slope	0.01	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	36.00	in
Local Depression	3.00	in
Local Depression Width	1.00	ft

Efficiency	87.96	%
Intercepted Flow	0.18	ft³/s
Bypass Flow	0.02	ft³/s
Spread	1.62	ft
Depth	0.08	ft
Flow Area	0.07	ft²
Gutter Depression	0.08	ft
Total Depression	0.33	ft
Velocity	3.04	ft/s
Equivalent Cross Slope	0.17500	ft/ft
Length Factor	0.69	
Total Interception Length	4.34	ft

Worksheet for Curb Inlet/outlet On Grade -1.14ci_25

D	4	D		4.1
Pro	IPCT	Des	crir	าบาก
	COL	200	OI IP	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,

Solve For Efficiency

Input Data

Discharge	0.03	ft³/s
Slope	0.03600	ft/ft
Gutter Width	2.00	ft
Gutter Cross Slope	0.05	ft/ft
Road Cross Slope	0.01	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	36.00	in
Local Depression	3.00	in
Local Depression Width	1.00	ft

Efficiency	100.00	%
Intercepted Flow	0.03	ft³/s
Bypass Flow	0.00	ft³/s
Spread	0.80	ft
Depth	0.04	ft
Flow Area	0.02	ft²
Gutter Depression	0.08	ft
Total Depression	0.33	ft
Velocity	1.89	ft/s
Equivalent Cross Slope	0.17500	ft/ft
Length Factor	1.53	
Total Interception Length	1.96	ft

Worksheet for Curb Inlet On Grade -1.16cc_25

Pro	iect	Desc	rir	\ti∩n
1 10	JOGE	Desc	JΙΙΡ	, uoi i

Solve For Efficiency

In	put	Data

Discharge	0.80	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	13.51	%
Intercepted Flow	0.11	ft³/s
Bypass Flow	0.69	ft³/s
Spread	3.33	ft
Depth	0.16	ft
Flow Area	0.18	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.39	ft/s
Equivalent Cross Slope	0.07498	ft/ft
Length Factor	0.08	
Total Interception Length	12.91	ft

Worksheet for Curb Inlet On Grade -1.17cc_25

Solve For Efficiency

Input Data

Discharge	0.81	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	13.42	%
Intercepted Flow	0.11	ft³/s
Bypass Flow	0.70	ft³/s
Spread	3.36	ft
Depth	0.16	ft
Flow Area	0.18	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.40	ft/s
Equivalent Cross Slope	0.07483	ft/ft
Length Factor	0.08	
Total Interception Length	13.00	ft

Worksheet for Curb Inlet On Grade -1.18cc_25

Project Description

Solve For Efficiency

Input D	ata
---------	-----

Discharge	0.83	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	13.26	%
Intercepted Flow	0.11	ft³/s
Bypass Flow	0.72	ft³/s
Spread	3.42	ft
Depth	0.16	ft
Flow Area	0.19	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.41	ft/s
Equivalent Cross Slope	0.07453	ft/ft
Length Factor	0.08	
Total Interception Length	13.16	ft

Worksheet for Curb Inlet On Grade -1.19cc_25

Project Description

Solve For Efficiency

In	put	Data

Discharge	0.84	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	13.18	%
Intercepted Flow	0.11	ft³/s
Bypass Flow	0.73	ft³/s
Spread	3.45	ft
Depth	0.16	ft
Flow Area	0.19	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.41	ft/s
Equivalent Cross Slope	0.07438	ft/ft
Length Factor	0.08	
Total Interception Length	13.24	ft

Worksheet for Curb Inlet On Grade -1.20cc_25

Pro	iect	Desc	rir	\ti∩n
1 10	JOGE	Desc	JΙΙΡ	, uoi i

Solve For Efficiency

In	put	Data

Discharge	0.86	ft³/s
Slope	0.03560	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	13.06	%
Intercepted Flow	0.11	ft³/s
Bypass Flow	0.75	ft³/s
Spread	3.53	ft
Depth	0.17	ft
Flow Area	0.20	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.40	ft/s
Equivalent Cross Slope	0.07401	ft/ft
Length Factor	0.07	
Total Interception Length	13.37	ft

Worksheet for Inlet1.21c_25 **Project Description** Solve For Spread Input Data Discharge 1.67 ft³/s Gutter Width 1.50 ft Gutter Cross Slope 0.06 ft/ft Road Cross Slope 0.02 ft/ft Local Depression 3.00 in Local Depression Width 7.00 ft Grate Width 1.50 ft Grate Length 2.95 ft P-50 mm (P-1-7/8") Grate Type 50.00 % Clogging Curb Opening Length 84.00 in 5.00 Opening Height in Curb Throat Type Horizontal Throat Incline Angle 90.00 degrees **Options** Calculation Option Use Both Results

Results		
Spread	3.33	ft
Depth	0.08	ft
Gutter Depression	0.06	ft
Total Depression	0.31	ft
Open Grate Area	1.99	ft²
Active Grate Weir Length	4.45	ft

Worksheet for Curb Inlet On Grade -2.01cc_25

Project	Description
---------	-------------

Solve For Efficiency

Input Data

Discharge	0.46	ft³/s
Slope	0.01730	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	21.15	%
Intercepted Flow	0.10	ft³/s
Bypass Flow	0.36	ft³/s
Spread	2.86	ft
Depth	0.15	ft
Flow Area	0.15	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	3.01	ft/s
Equivalent Cross Slope	0.07700	ft/ft
Length Factor	0.12	
Total Interception Length	8.08	ft

Worksheet for Inlet 3d_25

Project Description

Solve For Efficiency

Input Data

Discharge		0.55	ft³/s
Slope		0.01660	ft/ft
Gutter Width		1.50	ft
Gutter Cross Slope		0.06	ft/ft
Road Cross Slope		0.02	ft/ft
Roughness Coefficient		0.013	
Local Depression		3.00	in
Local Depression Width		7.00	ft
Grate Width		1.50	ft
Grate Length		2.95	ft
Grate Type	P-50 mm (P-1-7/8")		
Clogging		50.00	%
Curb Opening Length		5.00	in

Options

Calculation Option Use Both
Grate Flow Option Exclude None

Efficiency	84.80	%
Intercepted Flow	0.47	ft³/s
Bypass Flow	0.08	ft³/s
Spread	3.95	ft
Depth	0.14	ft
Flow Area	0.20	ft²
Gutter Depression	0.06	ft
Total Depression	0.31	ft
Velocity	2.70	ft/s
Splash Over Velocity	6.93	ft/s
Frontal Flow Factor	1.00	
Side Flow Factor	0.05	
Grate Flow Ratio	0.84	
Equivalent Cross Slope	0.05764	ft/ft
Active Grate Length	1.48	ft
Length Factor	0.00	
Total Interception Length	10.24	ft

Worksheet for Curb Inlet On Grade -2.03cc_25

Proj			

Solve For Efficiency

Input I	Data
---------	------

Discharge	0.14	ft³/s
Slope	0.01730	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	34.23	%
Intercepted Flow	0.05	ft³/s
Bypass Flow	0.09	ft³/s
Spread	1.18	ft
Depth	0.10	ft
Flow Area	0.06	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	2.40	ft/s
Equivalent Cross Slope	0.07943	ft/ft
Length Factor	0.21	
Total Interception Length	4.81	ft

Worksheet for Curb Inlet On Grade -2.04cc_25

Pro	iect	Descri	ption
	000		P (10)

Solve For Efficiency

Input Data

Discharge	0.33	ft³/s
Slope	0.01730	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	24.50	%
Intercepted Flow	0.08	ft³/s
Bypass Flow	0.25	ft³/s
Spread	2.04	ft
Depth	0.14	ft
Flow Area	0.11	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	2.93	ft/s
Equivalent Cross Slope	0.07914	ft/ft
Length Factor	0.14	
Total Interception Length	6.92	ft

Worksheet for Curb Inlet On Grade -2.10cc_25

Proj	ect	Desci	ſip	tion
------	-----	-------	-----	------

Solve For Efficiency

	In	put	Data
--	----	-----	------

Discharge	0.54	ft³/s
Slope	0.01730	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	19.59	%
Intercepted Flow	0.11	ft³/s
Bypass Flow	0.43	ft³/s
Spread	3.26	ft
Depth	0.16	ft
Flow Area	0.18	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	3.04	ft/s
Equivalent Cross Slope	0.07530	ft/ft
Length Factor	0.11	
Total Interception Length	8.76	ft

Worksheet for Curb Inlet On Grade -2.13cc_25

Solve For Efficiency

In	put	Data

Discharge	0.32	ft³/s
Slope	0.01730	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	24.82	%
Intercepted Flow	0.08	ft³/s
Bypass Flow	0.24	ft³/s
Spread	1.96	ft
Depth	0.13	ft
Flow Area	0.11	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	2.91	ft/s
Equivalent Cross Slope	0.07923	ft/ft
Length Factor	0.15	
Total Interception Length	6.82	ft

Worksheet for Curb Inlet On Grade -3.01cc_25

Pro	ect	Descr	iption

Solve For Efficiency

Input Data

Discharge	0.14	ft³/s
Slope	0.01730	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	34.23	%
Intercepted Flow	0.05	ft³/s
Bypass Flow	0.09	ft³/s
Spread	1.18	ft
Depth	0.10	ft
Flow Area	0.06	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	2.40	ft/s
Equivalent Cross Slope	0.07943	ft/ft
Length Factor	0.21	
Total Interception Length	4.81	ft

Worksheet for Curb Inlet On Grade - 3.03cc_25

Pro	iect	Desc	rin	tion
	COL		,, ,,	uon

Solve For Efficiency

Input Data

Discharge	0.13	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	28.80	%
Intercepted Flow	0.04	ft³/s
Bypass Flow	0.09	ft³/s
Spread	1.00	ft
Depth	0.08	ft
Flow Area	0.04	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	3.10	ft/s
Equivalent Cross Slope	0.07943	ft/ft
Length Factor	0.17	
Total Interception Length	5.81	ft

Worksheet for Inlet 4e_25

Project Description

Solve For Efficiency

Input Data

Discharge		0.54	ft³/s
Slope		0.01660	ft/ft
Gutter Width		1.50	ft
Gutter Cross Slope		0.06	ft/ft
Road Cross Slope		0.02	ft/ft
Roughness Coefficient		0.013	
Local Depression		3.00	in
Local Depression Width		7.00	ft
Grate Width		1.50	ft
Grate Length		2.95	ft
Grate Type	P-50 mm (P-1-7/8")		
Clogging		50.00	%
Curb Opening Length		5.00	in

Options

Calculation Option Use Both Grate Flow Option Exclude None

Efficiency	85.19	%
Intercepted Flow	0.46	ft³/s
Bypass Flow	0.08	ft³/s
Spread	3.90	ft
Depth	0.14	ft
Flow Area	0.20	ft²
Gutter Depression	0.06	ft
Total Depression	0.31	ft
Velocity	2.70	ft/s
Splash Over Velocity	6.93	ft/s
Frontal Flow Factor	1.00	
Side Flow Factor	0.05	
Grate Flow Ratio	0.84	
Equivalent Cross Slope	0.05782	ft/ft
Active Grate Length	1.48	ft
Length Factor	0.00	
Total Interception Length	10.14	ft

Worksheet for Inlet 4a_25

Project Description

Solve For Efficiency

Input Data

Discharge		0.58	ft³/s
Slope		0.01660	ft/ft
Gutter Width		1.50	ft
Gutter Cross Slope		0.06	ft/ft
Road Cross Slope		0.02	ft/ft
Roughness Coefficient		0.013	
Local Depression		3.00	in
Local Depression Width		7.00	ft
Grate Width		1.50	ft
Grate Length		2.95	ft
Grate Type	P-50 mm (P-1-7/8")		
Clogging		50.00	%
Curb Opening Length		5.00	in

Options

Calculation Option Use Both
Grate Flow Option Exclude None

Efficiency	83.64	%
Intercepted Flow	0.49	ft³/s
Bypass Flow	0.09	ft³/s
Spread	4.06	ft
Depth	0.15	ft
Flow Area	0.21	ft²
Gutter Depression	0.06	ft
Total Depression	0.31	ft
Velocity	2.72	ft/s
Splash Over Velocity	6.93	ft/s
Frontal Flow Factor	1.00	
Side Flow Factor	0.05	
Grate Flow Ratio	0.83	
Equivalent Cross Slope	0.05709	ft/ft
Active Grate Length	1.48	ft
Length Factor	0.00	
Total Interception Length	10.53	ft

Worksheet for Curb Inlet On Grade - 1.01cc_100

D.==		D	:	4:
Pro	ect	Des	crip	tion

Solve For Efficiency

Input Data

Discharge	0.78	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	13.68	%
Intercepted Flow	0.11	ft³/s
Bypass Flow	0.67	ft³/s
Spread	3.26	ft
Depth	0.16	ft
Flow Area	0.18	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.39	ft/s
Equivalent Cross Slope	0.07528	ft/ft
Length Factor	0.08	
Total Interception Length	12.75	ft

Worksheet for Curb Inlet On Grade -1.02cc_100

Project	Descri	ption
---------	--------	-------

Solve For Efficiency

In	put	Data

Discharge	0.82	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	13.34	%
Intercepted Flow	0.11	ft³/s
Bypass Flow	0.71	ft³/s
Spread	3.39	ft
Depth	0.16	ft
Flow Area	0.19	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.40	ft/s
Equivalent Cross Slope	0.07468	ft/ft
Length Factor	0.08	
Total Interception Length	13.08	ft

Worksheet for Curb Inlet On Grade -1.03cc_100

Pro	iect	Desc	rir	\ti∩n
1 10	JOGE	Desc	JΙΙΡ	, uoi i

Solve For Efficiency

ı	n	put	Data

Discharge	0.87	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	12.95	%
Intercepted Flow	0.11	ft³/s
Bypass Flow	0.76	ft³/s
Spread	3.54	ft
Depth	0.17	ft
Flow Area	0.20	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.42	ft/s
Equivalent Cross Slope	0.07394	ft/ft
Length Factor	0.07	
Total Interception Length	13.49	ft

Worksheet for Curb Inlet On Grade -1.04cc_100

Proj	ect	De	scri	ntio	n
1 10	COL	\mathcal{L}	3011	Puo	

Solve For Efficiency

In	put	Data

Discharge	0.92	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	12.58	%
Intercepted Flow	0.12	ft³/s
Bypass Flow	0.80	ft³/s
Spread	3.69	ft
Depth	0.17	ft
Flow Area	0.21	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.44	ft/s
Equivalent Cross Slope	0.07321	ft/ft
Length Factor	0.07	
Total Interception Length	13.89	ft

Worksheet for Curb Inlet On Grade -1.05cc_100

Pro	ect	De	scr	in	tio	n
1 10	COL	\mathcal{L}	301	יעו	uv	

Solve For Efficiency

	In	put	Data
--	----	-----	------

Discharge	0.95	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	12.38	%
Intercepted Flow	0.12	ft³/s
Bypass Flow	0.83	ft³/s
Spread	3.77	ft
Depth	0.17	ft
Flow Area	0.21	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.45	ft/s
Equivalent Cross Slope	0.07277	ft/ft
Length Factor	0.07	
Total Interception Length	14.13	ft

Worksheet for Curb Inlet On Grade -1.06cc_100

Solve For Efficiency

In	put	Data

Discharge	0.97	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	12.24	%
Intercepted Flow	0.12	ft³/s
Bypass Flow	0.85	ft³/s
Spread	3.82	ft
Depth	0.17	ft
Flow Area	0.22	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.46	ft/s
Equivalent Cross Slope	0.07249	ft/ft
Length Factor	0.07	
Total Interception Length	14.29	ft

Worksheet for Inlet1.07a_100

Project Description	
Solve For	Spread

Input	Data

Discharge		1.82	ft³/s
Gutter Width		1.50	ft
Gutter Cross Slope		0.06	ft/ft
Road Cross Slope		0.02	ft/ft
Local Depression		3.00	in
Local Depression Width		7.00	ft
Grate Width		1.50	ft
Grate Length		2.95	ft
Grate Type	P-50 mm (P-1-7/8")		
Clogging		50.00	0/_

Clogging 50.00 %
Curb Opening Length 84.00 in
Opening Height 5.00 in

Curb Throat Type Horizontal

Throat Incline Angle 90.00 degrees

Options

Calculation Option Use Both

Spread	3.45	ft
Depth	0.09	ft
Gutter Depression	0.06	ft
Total Depression	0.31	ft
Open Grate Area	1.99	ft²
Active Grate Weir Length	4.45	ft

Worksheet for Curb Inlet/outlet On Grade -1.13ci_100

D 1	4	D		42
₽r∩	ΙΔΟΤ	LIDEC	rın	tion
1 10	I C C L	Desc	עוו	เเบเ

Solve For Efficiency

In	put	Data

Discharge	0.28	ft³/s
Slope	0.03600	ft/ft
Gutter Width	2.00	ft
Gutter Cross Slope	0.05	ft/ft
Road Cross Slope	0.01	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	36.00	in
Local Depression	3.00	in
Local Depression Width	1.00	ft

Efficiency	80.82	%
Intercepted Flow	0.23	ft³/s
Bypass Flow	0.05	ft³/s
Spread	1.84	ft
Depth	0.09	ft
Flow Area	0.08	ft²
Gutter Depression	0.08	ft
Total Depression	0.33	ft
Velocity	3.31	ft/s
Equivalent Cross Slope	0.17500	ft/ft
Length Factor	0.60	
Total Interception Length	5.00	ft

Worksheet for Curb Inlet/outlet On Grade -1.14ci_100

Proj			

Solve For Efficiency

In	put	Data

Discharge	0.06	ft³/s
Slope	0.03600	ft/ft
Gutter Width	2.00	ft
Gutter Cross Slope	0.05	ft/ft
Road Cross Slope	0.01	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	36.00	in
Local Depression	3.00	in
Local Depression Width	1.00	ft

Efficiency	100.00	%
Intercepted Flow	0.06	ft³/s
Bypass Flow	0.00	ft³/s
Spread	1.03	ft
Depth	0.05	ft
Flow Area	0.03	ft²
Gutter Depression	0.08	ft
Total Depression	0.33	ft
Velocity	2.25	ft/s
Equivalent Cross Slope	0.17500	ft/ft
Length Factor	1.15	
Total Interception Length	2.62	ft

Worksheet for Curb Inlet On Grade -1.16cc_100

Proi	1 [\	-: 1	L:
Prol	ect i	JASCI	ım	non

Solve For Efficiency

	In	put	Data
--	----	-----	------

Discharge	0.99	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	12.12	%
Intercepted Flow	0.12	ft³/s
Bypass Flow	0.87	ft³/s
Spread	3.88	ft
Depth	0.17	ft
Flow Area	0.22	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.47	ft/s
Equivalent Cross Slope	0.07221	ft/ft
Length Factor	0.07	
Total Interception Length	14.44	ft

Worksheet for Curb Inlet On Grade -1.17cc_100

Project Description	
---------------------	--

Solve For Efficiency

Input Data	l	nı	ρι	ıt	D	a	ta
------------	---	----	----	----	---	---	----

Discharge	1.02	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	11.93	%
Intercepted Flow	0.12	ft³/s
Bypass Flow	0.90	ft³/s
Spread	3.95	ft
Depth	0.17	ft
Flow Area	0.23	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.48	ft/s
Equivalent Cross Slope	0.07179	ft/ft
Length Factor	0.07	
Total Interception Length	14.68	ft

Worksheet for Curb Inlet On Grade -1.18cc_100

Solve For Efficiency

In	put	Data

Discharge	1.06	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	11.69	%
Intercepted Flow	0.12	ft³/s
Bypass Flow	0.94	ft³/s
Spread	4.05	ft
Depth	0.18	ft
Flow Area	0.24	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.50	ft/s
Equivalent Cross Slope	0.07125	ft/ft
Length Factor	0.07	
Total Interception Length	14.98	ft

Worksheet for Curb Inlet On Grade -1.19cc_100

_		_		
ν_{ro}	IDCt.	Des	crin	tınn
1 10		$\mathcal{L}_{\mathcal{L}}}}}}}}}}$	UID	UOU

Solve For Efficiency

Input I	Data
---------	------

Discharge	1.09	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	11.52	%
Intercepted Flow	0.13	ft³/s
Bypass Flow	0.96	ft³/s
Spread	4.13	ft
Depth	0.18	ft
Flow Area	0.24	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.51	ft/s
Equivalent Cross Slope	0.07085	ft/ft
Length Factor	0.07	
Total Interception Length	15.21	ft

Worksheet for Curb Inlet On Grade -1.20cc_100

Project Description	ı
---------------------	---

Solve For Efficiency

	In	put	Data
--	----	-----	------

Discharge	1.12	ft³/s
Slope	0.03560	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	11.39	%
Intercepted Flow	0.13	ft³/s
Bypass Flow	0.99	ft³/s
Spread	4.21	ft
Depth	0.18	ft
Flow Area	0.25	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	4.50	ft/s
Equivalent Cross Slope	0.07037	ft/ft
Length Factor	0.06	
Total Interception Length	15.40	ft

Worksheet for Inlet1.21c_100

Solve For Spread

Input Data

Discharge		2.13	ft³/s
Gutter Width		1.50	ft
Gutter Cross Slope		0.06	ft/ft
Road Cross Slope		0.02	ft/ft
Local Depression		3.00	in
Local Depression Width		7.00	ft
Grate Width		1.50	ft
Grate Length		2.95	ft
Grate Type	P-50 mm (P-1-7/8")		

Clogging $50.00\,$ % Curb Opening Length $84.00\,$ in Opening Height $5.00\,$ in

Curb Throat Type Horizontal

Throat Incline Angle 90.00 degrees

Options

Calculation Option Use Both

Spread	3.65	ft
Depth	0.11	ft
Gutter Depression	0.06	ft
Total Depression	0.31	ft
Open Grate Area	1.99	ft²
Active Grate Weir Length	4.45	ft

Worksheet for Curb Inlet On Grade -2.01cc_100

Solve For Efficiency

Input Data

Discharge	0.65	ft³/s
Slope	0.01730	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	17.86	%
Intercepted Flow	0.12	ft³/s
Bypass Flow	0.53	ft³/s
Spread	3.73	ft
Depth	0.17	ft
Flow Area	0.21	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	3.08	ft/s
Equivalent Cross Slope	0.07295	ft/ft
Length Factor	0.10	
Total Interception Length	9.66	ft

Worksheet for Inlet 3d_100

Project Description

Solve For Efficiency

Input Data

Discharge		0.78	ft³/s
Slope		0.01660	ft/ft
Gutter Width		2.00	ft
Gutter Cross Slope		0.06	ft/ft
Road Cross Slope		0.02	ft/ft
Roughness Coefficient		0.013	
Local Depression		3.00	in
Local Depression Width		7.00	ft
Grate Width		2.00	ft
Grate Length		2.95	ft
Grate Type	P-50 mm (P-1-7/8")		
Clogging		50.00	%
Curb Opening Length		5.00	in

Options

Calculation Option Use Both Grate Flow Option Exclude None

Efficiency	92.97	%
Intercepted Flow	0.73	ft³/s
Bypass Flow	0.05	ft³/s
Spread	4.08	ft
Depth	0.17	ft
Flow Area	0.25	ft²
Gutter Depression	0.09	ft
Total Depression	0.34	ft
Velocity	3.10	ft/s
Splash Over Velocity	6.93	ft/s
Frontal Flow Factor	1.00	
Side Flow Factor	0.04	
Grate Flow Ratio	0.93	
Equivalent Cross Slope	0.06435	ft/ft
Active Grate Length	1.48	ft
Length Factor	0.00	
Total Interception Length	11.10	ft

Worksheet for Curb Inlet On Grade -2.03cc_100

Pro	iect	Desc	rir	\ti∩n
1 10	JOGE	Desc	JΙΙΡ	, uoi i

Solve For Efficiency

Input I	Data
---------	------

Discharge	0.12	ft³/s
Slope	0.01730	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	36.29	%
Intercepted Flow	0.04	ft³/s
Bypass Flow	0.08	ft³/s
Spread	1.12	ft
Depth	0.09	ft
Flow Area	0.05	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	2.31	ft/s
Equivalent Cross Slope	0.07943	ft/ft
Length Factor	0.22	
Total Interception Length	4.51	ft

Worksheet for Curb Inlet On Grade -2.04cc_100

Project	Description
---------	-------------

Solve For Efficiency

Input Data

Discharge	0.37	ft³/s
Slope	0.01730	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	23.34	%
Intercepted Flow	0.09	ft³/s
Bypass Flow	0.28	ft³/s
Spread	2.32	ft
Depth	0.14	ft
Flow Area	0.13	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	2.96	ft/s
Equivalent Cross Slope	0.07864	ft/ft
Length Factor	0.14	
Total Interception Length	7.29	ft

Worksheet for Curb Inlet On Grade -2.10cc_100

Pro	iect	Desc	rir	\ti∩n
1 10	JOGE	Desc	JΙΙΡ	, uoi i

Solve For Efficiency

In	put	Data

Discharge	0.75	ft³/s
Slope	0.01730	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	16.60	%
Intercepted Flow	0.12	ft³/s
Bypass Flow	0.63	ft³/s
Spread	4.11	ft
Depth	0.18	ft
Flow Area	0.24	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	3.13	ft/s
Equivalent Cross Slope	0.07095	ft/ft
Length Factor	0.10	
Total Interception Length	10.43	ft

Worksheet for Inlet 3b_100

Project Description

Solve For Efficiency

Input Data

Discharge		0.78	ft³/s
Slope		0.01660	ft/ft
Gutter Width		2.00	ft
Gutter Cross Slope		0.06	ft/ft
Road Cross Slope		0.02	ft/ft
Roughness Coefficient		0.013	
Local Depression		3.00	in
Local Depression Width		7.00	ft
Grate Width		2.00	ft
Grate Length		2.95	ft
Grate Type	P-50 mm (P-1-7/8")		
Clogging		50.00	%
Curb Opening Length		5.00	in

Options

Calculation Option Use Both
Grate Flow Option Exclude None

92.97	%
0.73	ft³/s
0.05	ft³/s
4.08	ft
0.17	ft
0.25	ft²
0.09	ft
0.34	ft
3.10	ft/s
6.93	ft/s
1.00	
0.04	
0.93	
0.06435	ft/ft
1.48	ft
0.00	
11.10	ft
	0.73 0.05 4.08 0.17 0.25 0.09 0.34 3.10 6.93 1.00 0.04 0.93 0.06435 1.48 0.00

Worksheet for Curb Inlet On Grade -2.12cc_100

Pro	iect	Desc	rir	\ti∩n
1 10	JOGE	Desc	JΙΙΡ	, uoi i

Solve For Efficiency

Input Data

Discharge	0.12	ft³/s
Slope	0.01730	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	36.29	%
Intercepted Flow	0.04	ft³/s
Bypass Flow	0.08	ft³/s
Spread	1.12	ft
Depth	0.09	ft
Flow Area	0.05	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	2.31	ft/s
Equivalent Cross Slope	0.07943	ft/ft
Length Factor	0.22	
Total Interception Length	4.51	ft

Worksheet for Curb Inlet On Grade -3.01cc_100

Project Description

Solve For Efficiency

Input Data

Discharge	0.09	ft³/s
Slope	0.01730	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	40.42	%
Intercepted Flow	0.04	ft³/s
Bypass Flow	0.05	ft³/s
Spread	1.00	ft
Depth	0.08	ft
Flow Area	0.04	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	2.15	ft/s
Equivalent Cross Slope	0.07943	ft/ft
Length Factor	0.25	
Total Interception Length	4.00	ft

Worksheet for Inlet 4e_100

Project Description

Solve For Efficiency

Input Data

Discharge		0.67	ft³/s
Slope		0.01660	ft/ft
Gutter Width		2.00	ft
Gutter Cross Slope		0.06	ft/ft
Road Cross Slope		0.02	ft/ft
Roughness Coefficient		0.013	
Local Depression		3.00	in
Local Depression Width		7.00	ft
Grate Width		2.00	ft
Grate Length		2.95	ft
Grate Type	P-50 mm (P-1-7/8")		
Clogging		50.00	%
Curb Opening Length		5.00	in

Options

Calculation Option Use Both Grate Flow Option Exclude None

Efficiency	95.43	%
Intercepted Flow	0.64	ft³/s
Bypass Flow	0.03	ft³/s
Spread	3.67	ft
Depth	0.16	ft
Flow Area	0.22	ft²
Gutter Depression	0.09	ft
Total Depression	0.34	ft
Velocity	3.05	ft/s
Splash Over Velocity	6.93	ft/s
Frontal Flow Factor	1.00	
Side Flow Factor	0.04	
Grate Flow Ratio	0.95	
Equivalent Cross Slope	0.06558	ft/ft
Active Grate Length	1.48	ft
Length Factor	0.00	
Total Interception Length	10.30	ft

Worksheet for Curb Inlet On Grade - 3.03cc_100

Solve For Efficiency

In	put	Data

Discharge	0.09	ft³/s
Slope	0.03600	ft/ft
Gutter Width	1.50	ft
Gutter Cross Slope	0.08	ft/ft
Road Cross Slope	0.02	ft/ft
Roughness Coefficient	0.013	
Curb Opening Length	12.00	in
Local Depression	1.00	in
Local Depression Width	3.00	ft

Efficiency	33.18	%
Intercepted Flow	0.03	ft³/s
Bypass Flow	0.06	ft³/s
Spread	0.87	ft
Depth	0.07	ft
Flow Area	0.03	ft²
Gutter Depression	0.09	ft
Total Depression	0.18	ft
Velocity	2.83	ft/s
Equivalent Cross Slope	0.07943	ft/ft
Length Factor	0.20	
Total Interception Length	4.98	ft

Worksheet for Inlet 4a_100

Project Description

Solve For Efficiency

Input Data

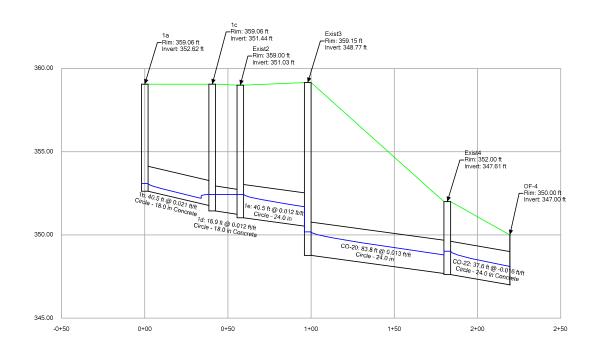
Discharge		0.58	ft³/s
Slope		0.01660	ft/ft
Gutter Width		2.00	ft
Gutter Cross Slope		0.06	ft/ft
Road Cross Slope		0.02	ft/ft
Roughness Coefficient		0.013	
Local Depression		3.00	in
Local Depression Width		7.00	ft
Grate Width		2.00	ft
Grate Length		2.95	ft
Grate Type	P-50 mm (P-1-7/8")		
Clogging		50.00	%
Curb Opening Length		5.00	in

Options

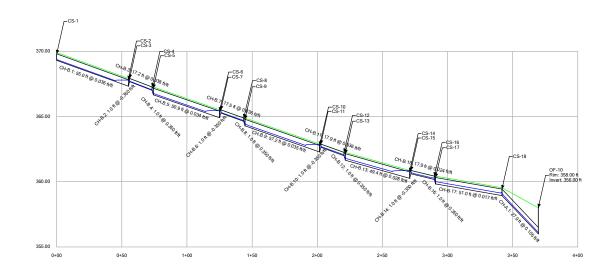
Calculation Option Use Both Grate Flow Option Exclude None

Efficiency	97.34	%
Intercepted Flow	0.56	ft³/s
Bypass Flow	0.02	ft³/s
Spread	3.29	ft
Depth	0.15	ft
Flow Area	0.19	ft²
Gutter Depression	0.09	ft
Total Depression	0.34	ft
Velocity	3.00	ft/s
Splash Over Velocity	6.93	ft/s
Frontal Flow Factor	1.00	
Side Flow Factor	0.04	
Grate Flow Ratio	0.97	
Equivalent Cross Slope	0.06653	ft/ft
Active Grate Length	1.48	ft
Length Factor	0.00	
Total Interception Length	9.61	ft

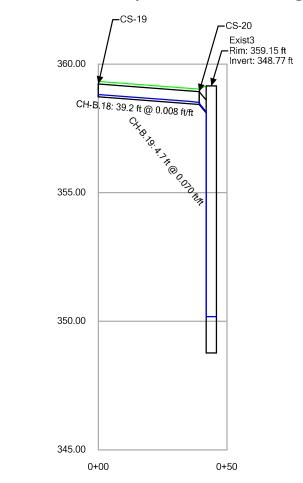
Profile Report Engineering Profile - Profile - 1 (1118_TMD_Drainage_25yr.stsw)



Profile Report Engineering Profile - Profile - 2 (1118_TMD_Drainage_25yr.stsw)



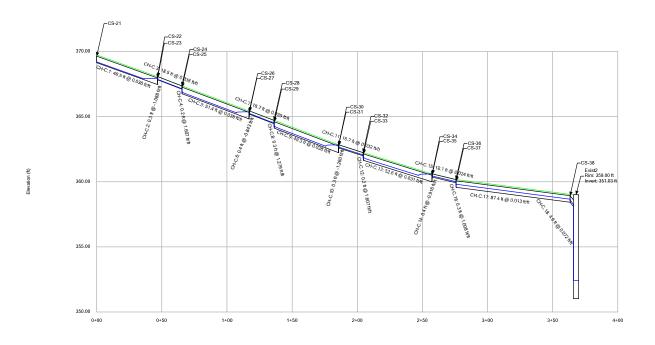
Profile Report Engineering Profile - Profile - 3 (1118_TMD_Drainage_25yr.stsw)



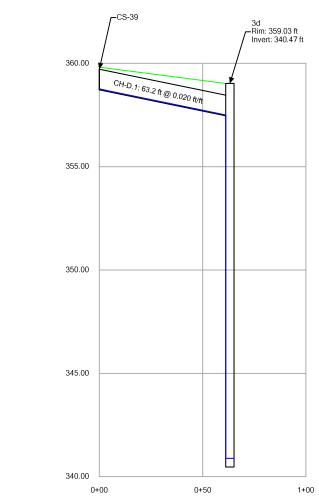
Station (ft)

Elevation (ft)

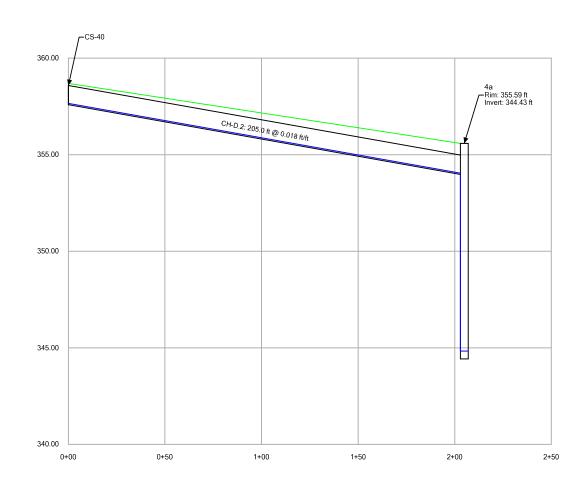
Profile Report Engineering Profile - Profile - 4 (1118_TMD_Drainage_25yr.stsw)



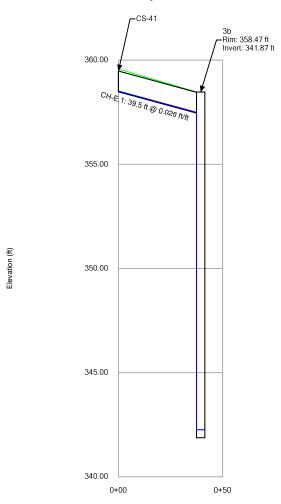
Profile Report Engineering Profile - Profile - 5 (1118_TMD_Drainage_25yr.stsw)



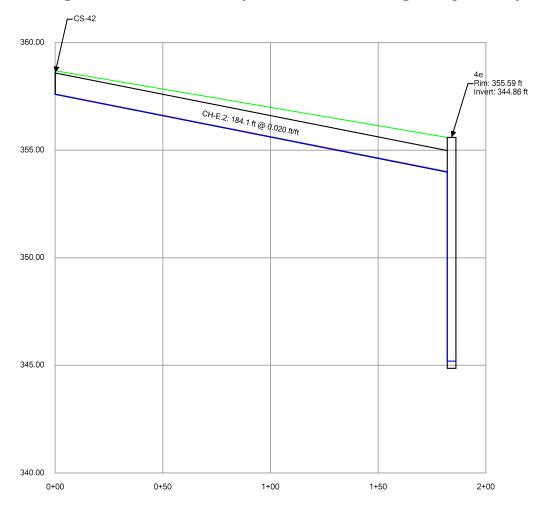
Profile Report Engineering Profile - Profile - 6 (1118_TMD_Drainage_25yr.stsw)



Profile Report Engineering Profile - Profile - 7 (1118_TMD_Drainage_25yr.stsw)



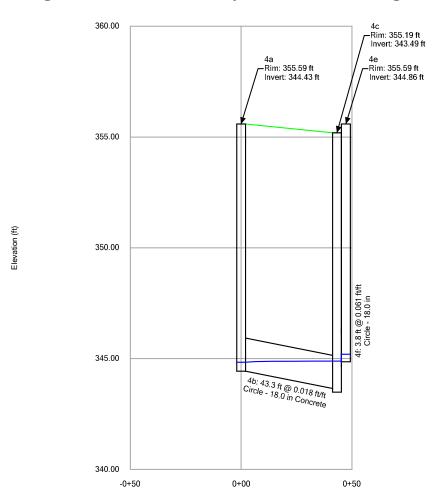
Profile Report Engineering Profile - Profile - 8 (1118_TMD_Drainage_25yr.stsw)



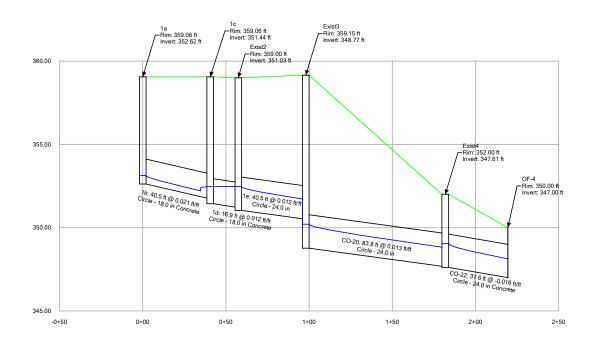
Profile Report Engineering Profile - Profile - 9 (1118_TMD_Drainage_25yr.stsw)



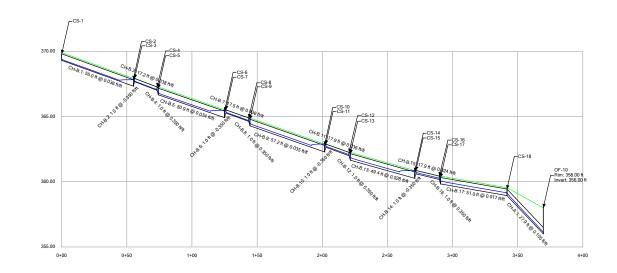
Profile Report Engineering Profile - Profile - 10 (1118_TMD_Drainage_25yr.stsw)



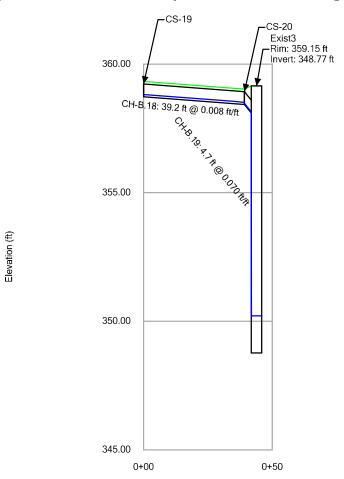
Profile Report Engineering Profile - Profile - 1 (1118_TMD_Drainage_100yr.stsw)



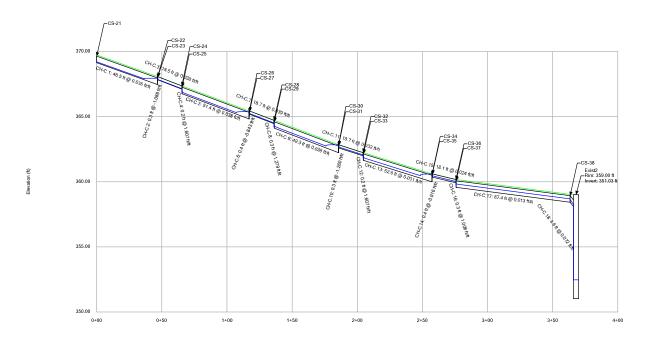
Profile Report Engineering Profile - Profile - 2 (1118_TMD_Drainage_100yr.stsw)



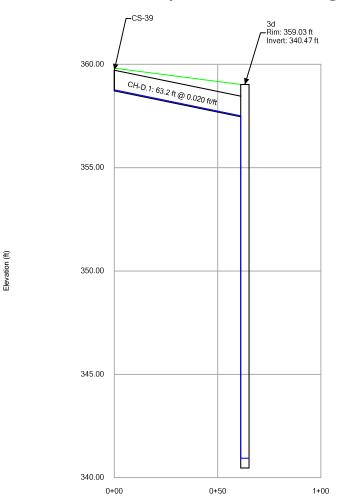
Profile Report Engineering Profile - Profile - 3 (1118_TMD_Drainage_100yr.stsw)



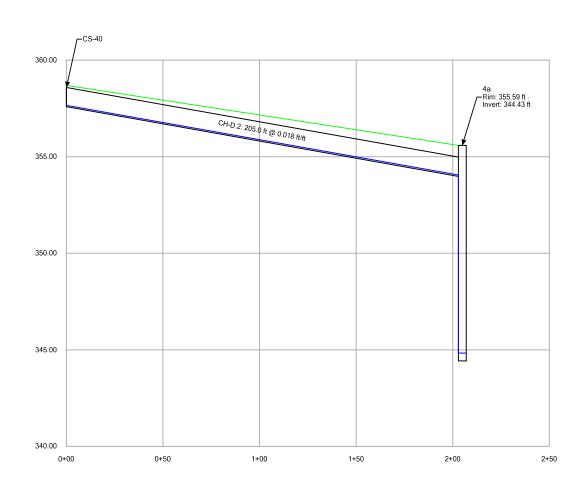
Profile Report Engineering Profile - Profile - 4 (1118_TMD_Drainage_100yr.stsw)



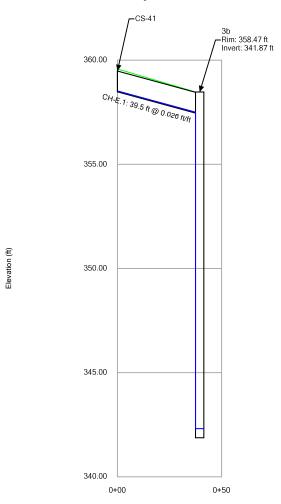
Profile Report Engineering Profile - Profile - 5 (1118_TMD_Drainage_100yr.stsw)



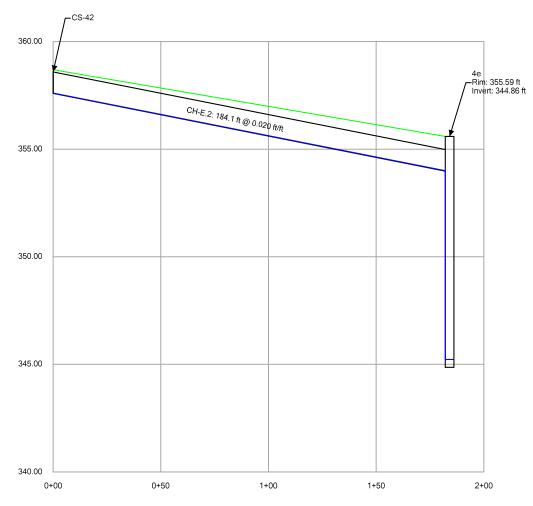
Profile Report Engineering Profile - Profile - 6 (1118_TMD_Drainage_100yr.stsw)



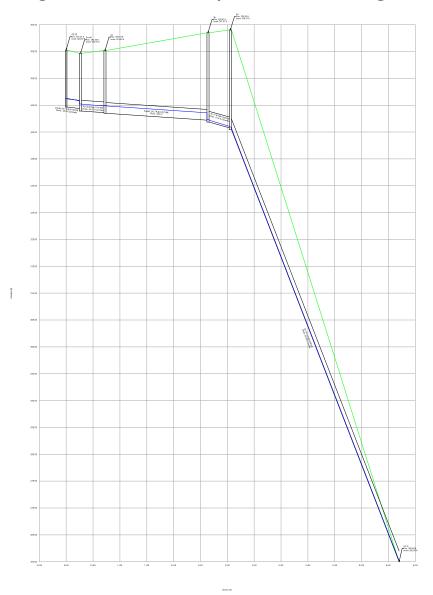
Profile Report Engineering Profile - Profile - 7 (1118_TMD_Drainage_100yr.stsw)



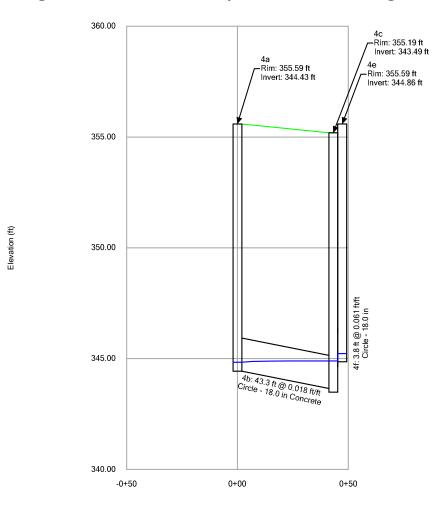
Profile Report Engineering Profile - Profile - 8 (1118_TMD_Drainage_100yr.stsw)



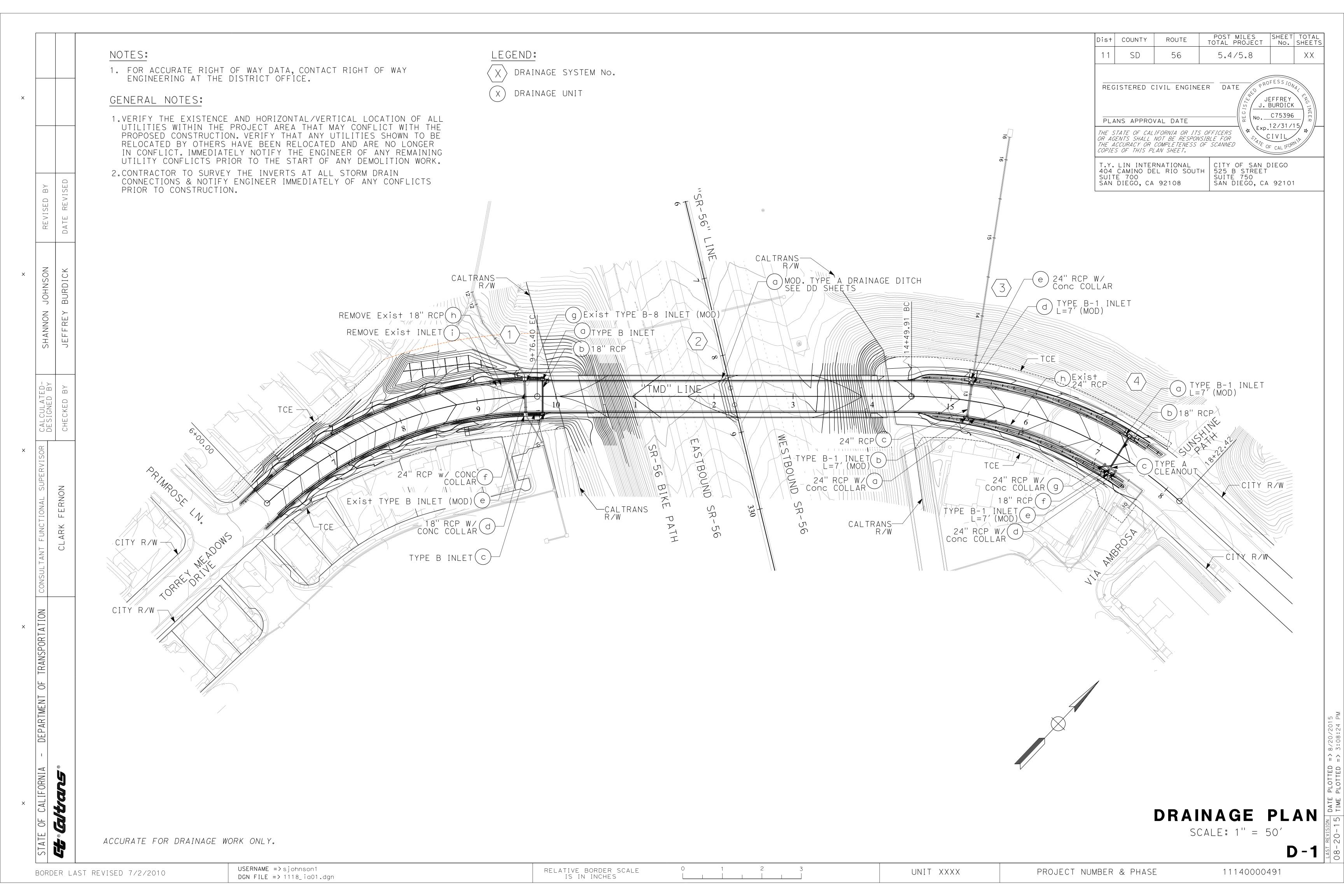
Profile Report Engineering Profile - Profile - 9 (1118_TMD_Drainage_100yr.stsw)

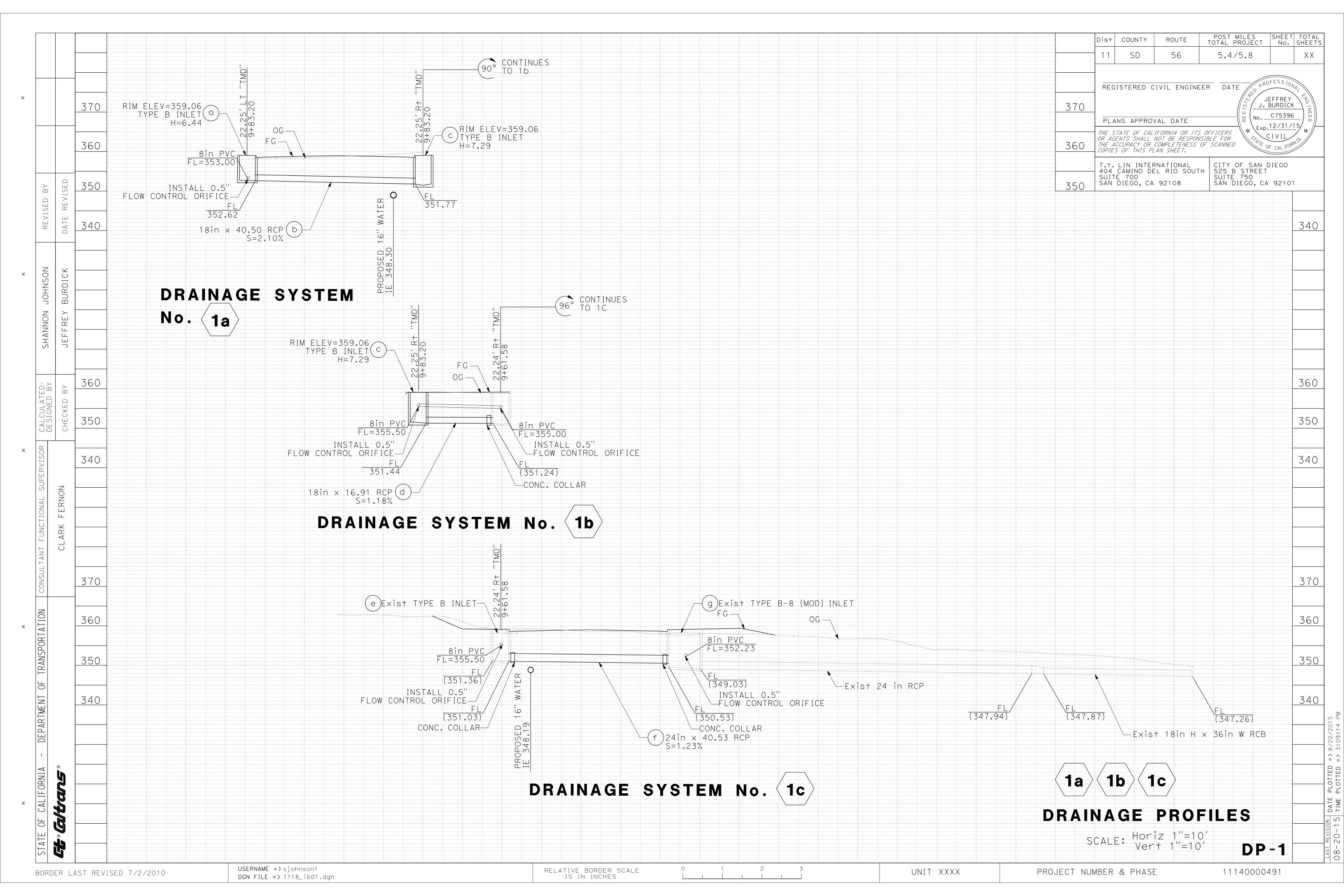


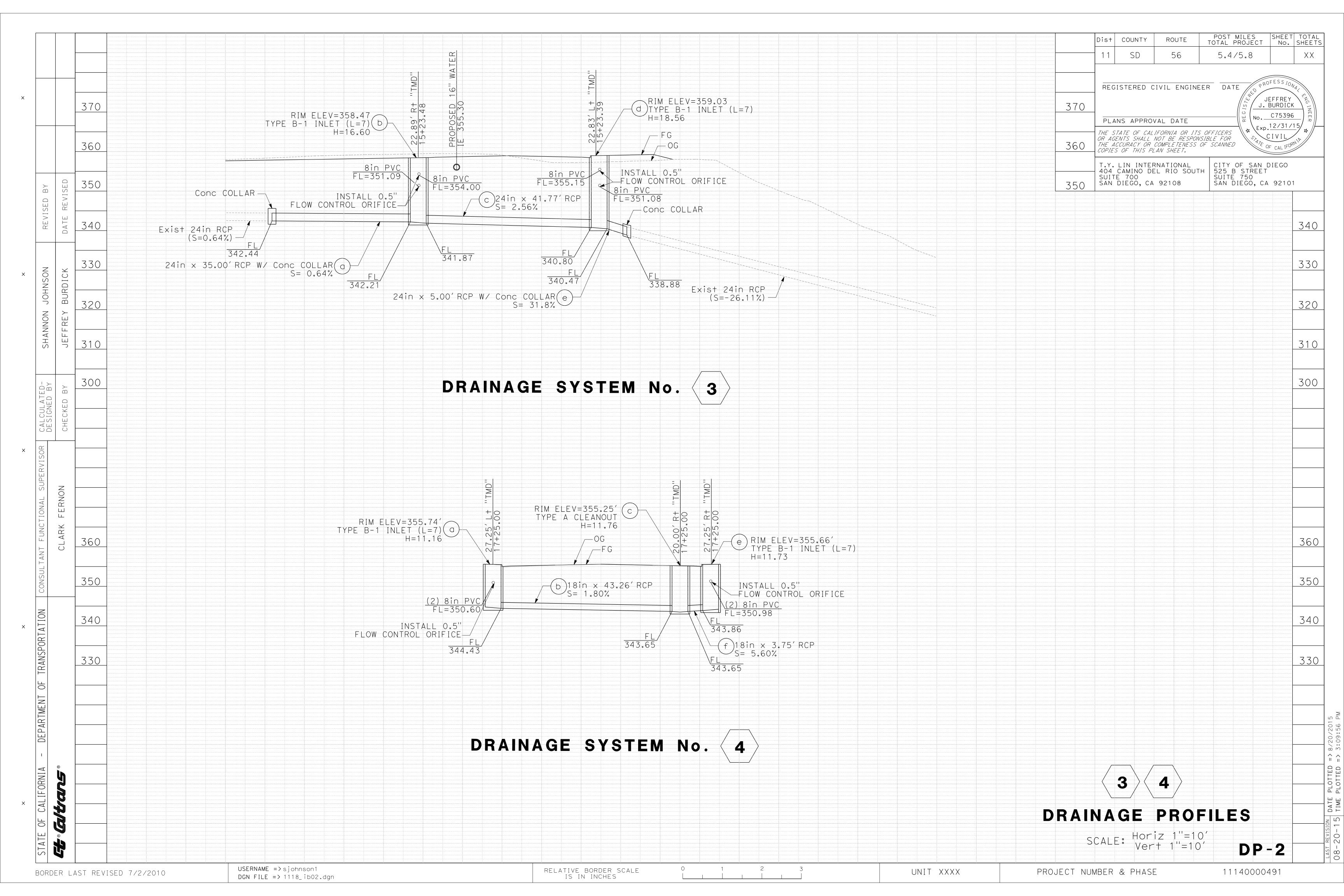
Profile Report Engineering Profile - Profile - 10 (1118_TMD_Drainage_100yr.stsw)

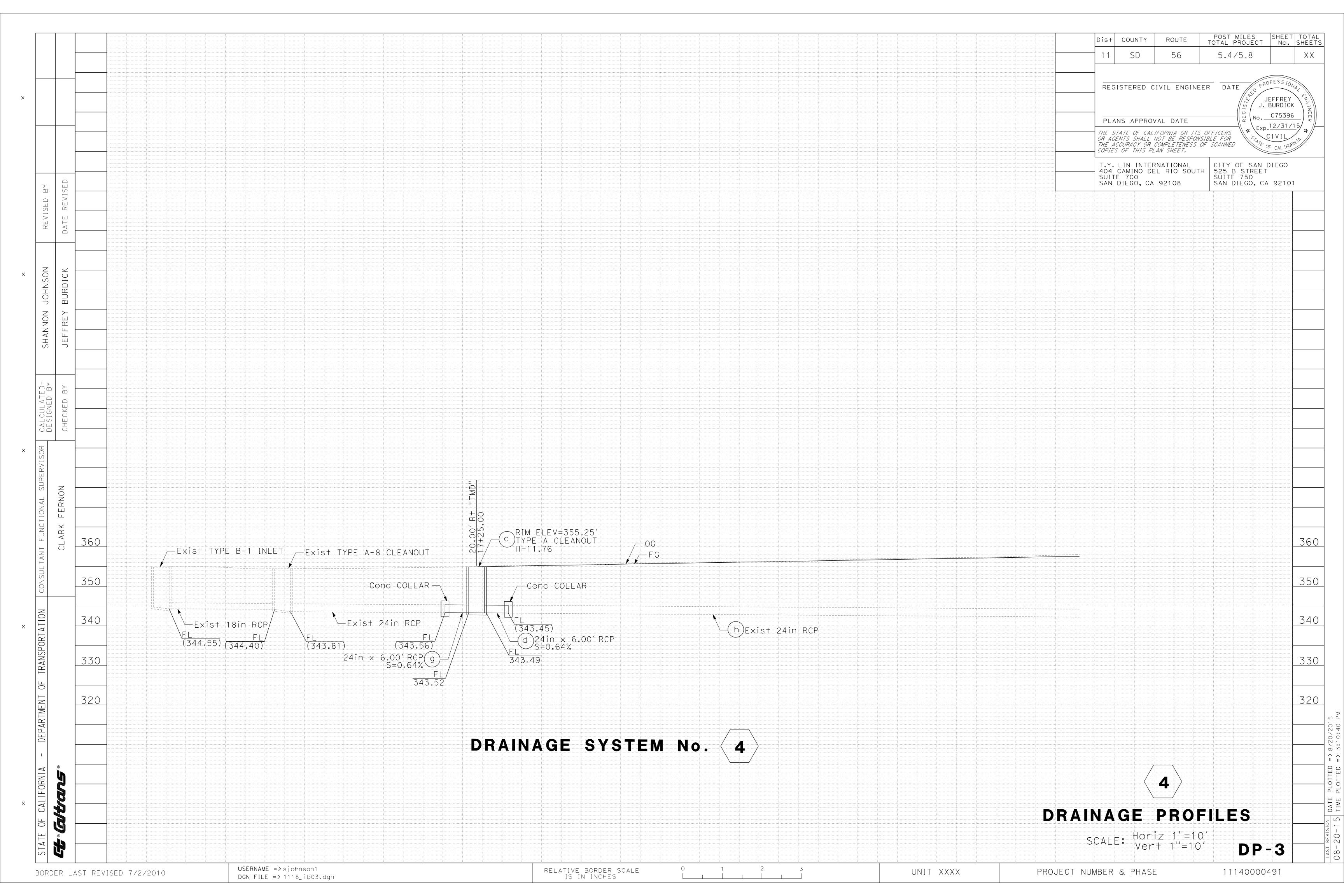


APPENDIX D PROPOSED DRAINAGE PLANS



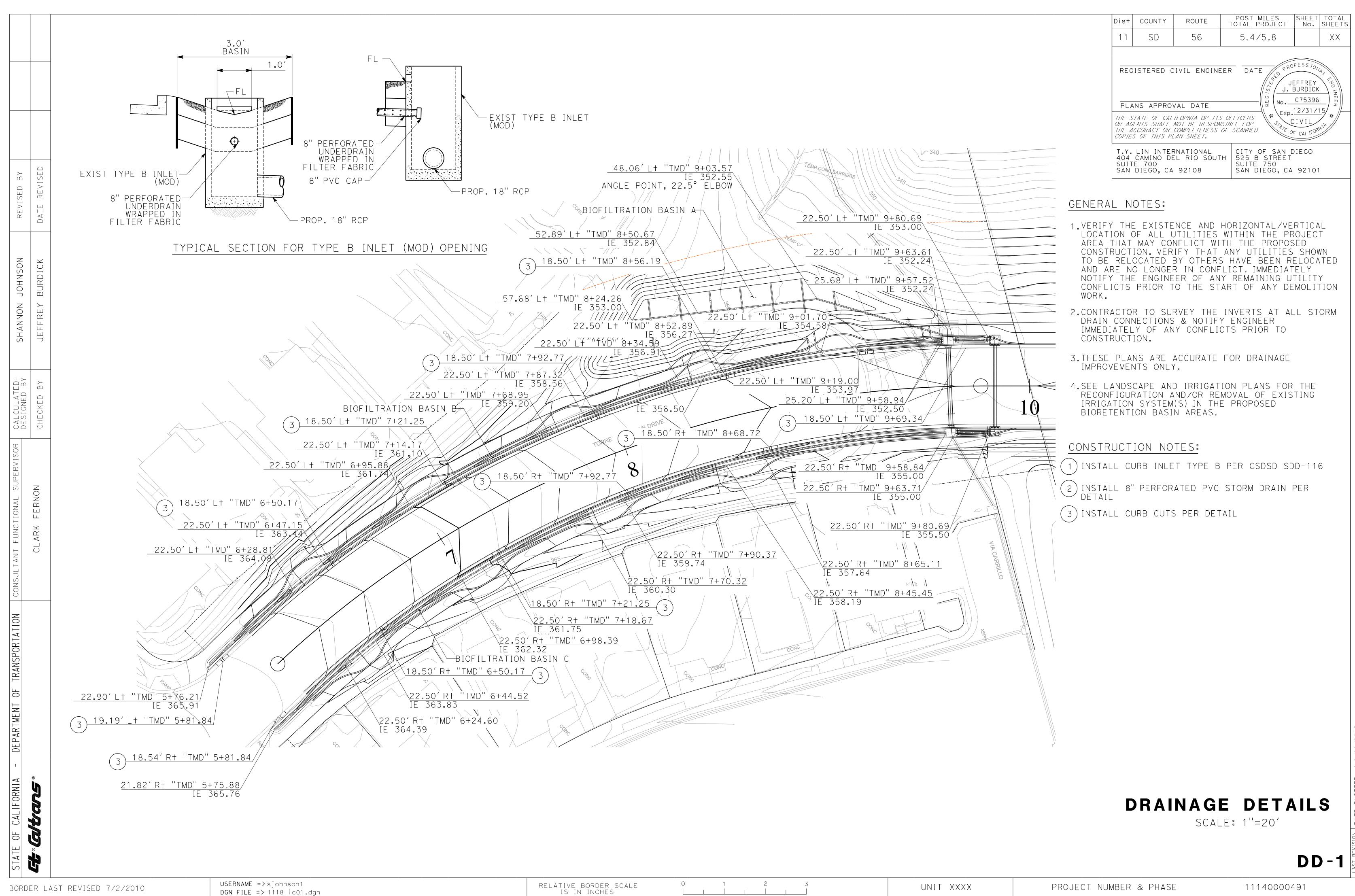






APPENDIX E

PROPOSED PRELIMINARY HYDRO MODIFICATION AND TREATMENT CONTROL BMP MAP



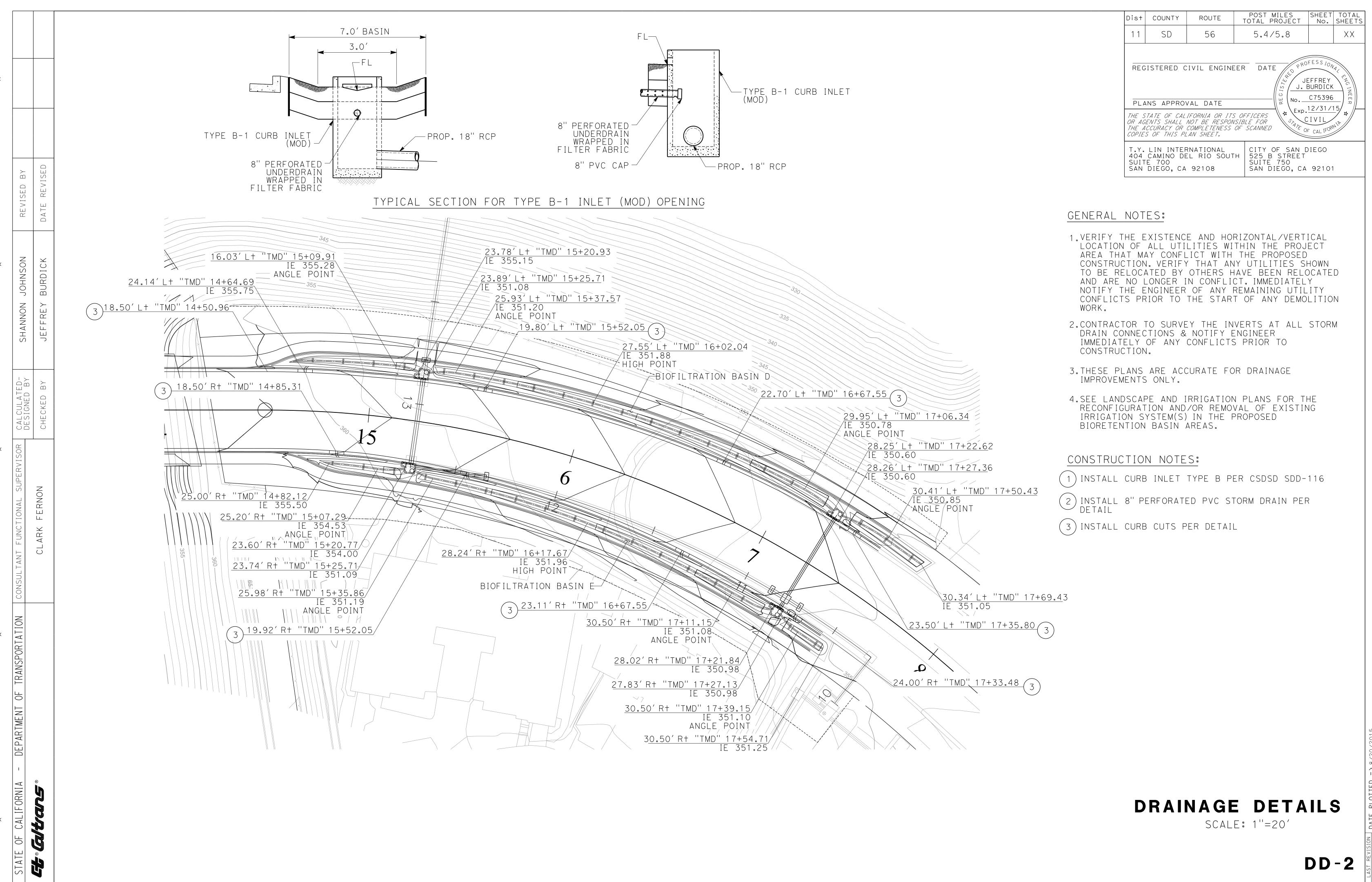
BORDER LAST REVISED 7/2/2010

DGN FILE => 1118_ic01.dgn

11140000491

PROJECT NUMBER & PHASE

UNIT XXXX



UNIT XXXX

PROJECT NUMBER & PHASE

11140000491